The Sizewell C Project

9.54 SZC Co. Comments on Submissions from Earlier Deadlines (Deadlines 2-4) Appendices

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SUMMARY OF THE CONTROL AND APPROVAL OF HIGHWAY MATTERS

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Deadline 5

SUMMARY OF THE CONTROL AND APPROVAL OF HIGHWAY MATTERS IN THE SIZEWELL C DCO

The purpose of this note is to explain the framework of approval for highway matters proposed in the Deadline 5 version of the dDCO (Rev 5) and the controls it will afford to Suffolk County Council ('SCC') and East Suffolk Council ('ESC'). In particular, it is intended to address many of the issues which underlie SCC's Deadline 3 comments on the dDCO relating to highways.

1. THE HIGHWAY WORKS, AND REQUIREMENTS AND OBLIGATIONS CONTROLLING THEIR DESIGN AND DELIVERY

Highway works authorised by the dDCO

1.1 The table below sets out all of the highway works authorised by the dDCO and the plans and requirements which relate to or control their design, delivery or removal[1]. The requirements referred to are set out in the form put forward in the Deadline 5 dDCO (Rev 5 and Rev 6):

Work No. and description	Relevant requirements and plans
Work No. 1A(I) – SSSI crossing	Requirements Requirement 12C – layout, scale and appearance to be approved by East Suffolk Council, following consultation with the EA and Natural England. Details to be in accordance with the plans and specifications referred to in this requirement. Requirement 5 – see below. Plans The plans referred to in Requirement 12C, which will also be listed as Approved Plans (Schedule 7), Part 1 in Rev 5 dDCO.
Work No. 1B: Main site - New four arm roundabout and site access points from the B1122 Abbey Road	Requirements Requirement 13A – see below Plans Approved Plans (Schedule 7), Part 1, under heading 'Highway Plans'
Work No. 1C: Main site – Lover's Lane realignment and junction "Works associated with Lover's Lane, to include— (a) realignment of the junction of the B1122 Abbey Road and Lover's Lane;	Requirements Requirement 13A – see below Plans Approved Plans (Schedule 7), Part 1, under heading 'Highway Plans'

[1] where temporary ie Work No. 9(b) and Work No. 4A(c)

(b) realignment of Lover's Lane; (c) provision of a mammal culvert under Lover's Lane; and (d) creation of a right turn into Leiston Household Waste Recycling Centre."	
Work No. 4A(c): Temporary realignment of Buckleswood Road	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 2
Work No. 9(b): Temporary highway works relating to northern park and ride: "Highway works including a roundabout, realignment of a section of the A12 and Willow Marsh Lane; realignment of private access track; revised kerbs, road markings, new highway signage, footways and paved areas; and site reinstatement, including landscaping and reinstatement of the existing A12 alignment following cessation of operational use."	Requirements Requirement 22 – see below Requirement 21 (2) "Work No. 9(a) (northern park and ride) must not be brought into use until Work No. 9(b) (related highway works) is open for public use." Requirement 24 – Requires the removal of these highway works, together with the rest of the northern park and ride site) within 12 months of completion of the SZC construction works. Plans Approved Plans (Schedule 7), Part 4
Work No. 10(b): Highway works relating to southern park and ride: "Highway works, including revised kerbs, road markings, new highways signage, to the B1078, the northbound slip road between B1078 and the A12, and the A12 northbound carriageway."	Requirements Requirement 22 – see below Requirement 21 (3) "Work No. 10(a) (southern park and ride) must not be brought into use until Work No. 10(b) (related highway works) is open for public use." Plans Approved Plans (Schedule 7), Part 5
Work No. 11: Two village bypass: including tie-ins to existing roads and footbridge east of Farnham Hall	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 6
Work No. 12: **Sizewell link road**: including tie-ins to existing roads and footbridge connecting to Pretty Road	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 7
Work No. 13(b): Highway works relating to freight management facility: "Highway works to Felixstowe Road to include widening of the highway and temporary site access"	Requirements Requirement 22 – see below Requirement 21 "(4) Work No. 13(a) (freight management facility) must not be brought into

	use until Work No. 13(b) (related highway works) is open for public use." Plans Approved Plans (Schedule 7), Part 8
Work No. 14 – **Yoxford roundabout**	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 9
Work No. 15: **A12/B1119 junction at Saxmundham: "**Improvements to the A12 and B1119 junction to include maintenance of vegetation along the highway boundary, alteration of the B1119 at the junction with the A12 and provision of additional or alterations to existing signage and road markings"	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 9
Work No. 16: A1094/B1069 junction south of Knodishall: "Improvements to the A1094 and B1069 junction to include maintenance of vegetation along the highway boundary and provision of additional or alterations to existing signage and road markings"	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 9
Work No. 17: A12/A144 junction south of Bramfield: "Improvements to the A12 and A144 junction to include provision of central reservation island and waiting area on the A12, widening of the A12, provision of pedestrian walkways and dropped kerbs and provision of a verge"	Requirements Requirement 22 – see below Plans Approved Plans (Schedule 7), Part 9

1.2 Requirement 13A will provide as follows in relation to the highway works comprised in Work 1B and 1C:

13A Main development site: Highway works

(1)Construction of any part of Work No.1B and Work No. 1C must not be commenced until details of the layout and highway alignment, including details of the surface and foul water drainage system for that part have been submitted to and approved by Suffolk County Council.

(2) The layout and highway alignment details referred to in paragraph (1) must be in accordance with the plans listed in Schedule 7 (Approved plans), within the limits of deviation shown on the relevant plans set out in Schedule 4 (Works Plans) and in general accordance with Chapter 5 of the Main Development Site Design and Access Statement unless otherwise agreed with Suffolk County Council.

(3) The details of the surface and foul water drainage system referred to in paragraph (1) must be based on sustainable drainage principles and be in accordance with the Drainage Strategy, unless otherwise agreed with Suffolk County Council.

(4) Work No. 1B and Work No. 1C must be carried out in accordance with the approved details.

1.3 Requirement 22 provides as follows in relation to the highway works comprised in Work Nos. 4A(c), 9(b), 10(b), 11,12,13(b),14,15,16 and 17:

22 Highway works

(1) Construction of any part of Work Nos. 4A(c) (temporary realignment of Buckleswood Road), 9(b) (highway works related to northern park and ride), 10(b) (highway works related to southern park and ride), 11 (two village bypass), 12 (Sizewell link road), 13(b) (highway works related to freight management facility), 14 (Yoxford roundabout), 15, 16 and 17 (other highway improvements) must not be commenced until details of the layout and highway alignment, including details of the surface and foul water drainage system for that part have been submitted to and approved by Suffolk County Council.

(2) The layout and highway alignment details referred to in paragraph (1) must be in accordance with the plans listed in Schedule 7 (Approved Plans) and in general accordance with the relevant tables in the Associated Development Design Principles and (in respect of Work No. 11 and Work No. 12) within the vertical limits of deviation specified in article 4 of this Order, unless otherwise agreed with Suffolk County Council.

(3) The details referred to in paragraph (1) must be based on sustainable drainage principles and be in accordance with the Drainage Strategy.

(4) The relevant tables in Associated Development Design Principles referred to in paragraph (2) are as follows:

(i) for Work No. 4A(c) (temporary realignment of Buckleswood Road), Table 2.1 and Table 3.8;
(ii) for Work No. 9(b) (highway works related to northern park and ride), Table 2.1 and Table 3.1;
(iii) for Work No. 10(b) (highway works related to southern park and ride), Table 2.1 and Table 3.2;
(vi) for Work No. 11 (two village bypass), Table 2.1 and Table 3.4;
(v) for Work No. 12 (Sizewell link road), Table 2.1 and Table 3.5;
(vi) for Work No. 13(b) (freight management facility), Table 2.1 and Table 3.3;
(vii) for Work No. 14 (Yoxford roundabout) Table 2.1 and Table 3.6; and
(viii) for Work Nos. 15, 16 and 17 (other highway improvements), Table 2.1 and Table 3.7.

(5) Work Nos. 4A(c) (temporary realignment of Buckleswood Road), 9(b) (highway works related to northern park and ride), 10(b) (highway works related to southern park and ride), 11 (two village bypass), 12 (Sizewell link road), 13(b) (highway works related to freight management facility), 14 (Yoxford roundabout), 15, 16 and 17 (other highway improvements) must be carried out in accordance with the approved details.

1.4 Requirements 5 and 18 reflect the amended position in requirements 13A and 22 as follows:

5 Project wide: Surface and foul water drainage

(1) No part of the authorised development (save for Work Nos. 1B, 1C, 4A(c), 9(b), 10(b), 11, 12 , 13(b), 14, 15, 16 or 17) may be commenced until details of the surface and foul water drainage system for that part (including management and maintenance arrangements, means of pollution control, sewage treatment works and a programme of construction and implementation) have been submitted to and approved by East Suffolk Council, following consultation with the Environment Agency, the relevant Statutory Nature Conservation Body, the East Suffolk Internal Drainage Board, the Lead Local Flood Authority and the drainage authority.

(2) Following approval pursuant to paragraph (1) above, East Suffolk Council shall provide details of the approved surface and foul water drainage system to Suffolk County Council, and no part of the authorised development approved pursuant to paragraph (1) above may be commenced until the details of the approved management and maintenance arrangements and means of pollution control for that part have been endorsed by Suffolk County Council in its capacity as the Lead Local Flood Authority and the drainage authority.

(3) The surface and foul water drainage proposals must be based on sustainable drainage principles and must be in accordance with the Drainage Strategy.

(4) Any approved surface and foul water drainage system must be constructed and maintained in accordance with the approved details.

18 Rail infrastructure

(1) Work No. 4 (rail works) (save for Work No. 4A(c)) must be carried out in accordance with the plans listed in Schedule 7 (Approved Plans) and in general accordance with Table 2.1 and Table 3.8 of the Associated Development Design Principles, save to the extent that alternative plans or details are submitted to and approved by East Suffolk Council

(2) Any alternative plans or details referred to in paragraph (1), must be in general accordance with Table 2.1 and Table 3.8 of the Associated Development Design Principles, and within the vertical limits of deviation specified in article 4 of this Order.

Highway works required by the Deed of Obligation

1.5 In addition, among other things, Schedule 16 of the Deed of Obligation sets up working groups to facilitate the design of further highway schemes at Wickham Market, Leiston, and Marlesford and Little Glemham. The Deed provides that SZC Co. will pay for delivery by SCC of the schemes agreed through these groups.

1.6 Schedule 16 also requires SZC Co to pay to SCC the 'B1078 Road Safety Contribution' for delivery by SCC of: the A14 signage strategy, improvements at the A140/B1078 junction, the B1078/B1079 junction at Otley, the B1078/Ashbocking Road junction, the B1078/B1079 junction at Clopton and the B1078 at Charsfield.

1.7 The delivery of all of these highway schemes referred to in Schedule 16 is therefore controlled and executed by SCC rather than SZC Co, and therefore the comments made in Section 2 below in relation to design approval and delivery are not relevant to this class of highway works.

Delivery of highway works in accordance with Implementation Plan

1.8 In addition to Requirement 21 (which requires delivery of highway works connected with the two park and ride sites and the freight management facility prior to use of those facilities), Schedule 9 of the Deed of Obligation places a duty on SZC Co. to use 'reasonable endeavours' to carry out and complete the 'Key Environmental Mitigation' in accordance with the Implementation Plan. The 'Key Environmental Mitigation' is defined to include the Sizewell link road, the Two village bypass, the Yoxford roundabout and the other DCO highway improvements (Work Nos. 15,16 and 17).

2. THE DESIGN APPROVAL PROCESS

2.1 Section 1 above sets out the highway works which are authorised by the dDCO, the plans approved by the dDCO which illustrate and authorise the details of those works, and the

requirements which require or allow approval of further or different detailed plans. In summary:

2.1.1 SZC Co. must seek ESC's approval of the details of the layout, scale and external appearance of the SSSI Crossing, and such details must accord with the various plans and section drawings referred to (Requirement 12C);

2.1.2 SZC Co. must seek SCC's approval of the details of the layout and highway alignment, including drainage details of Work No. 1B and Work No. 1C, and such details must accord with the approved plans and Chapter 5 of the DAS and must be situated within the limits of deviation shown on the Works Plans (Requirement 13A);

2.1.3 SZC Co. must seek SCC's approval of the details of the layout and highway alignment, including drainage details of other highway works is controlled by Requirement 22, which provides that SZC must carry out the works in accordance with the plans listed in Schedule 7 (Approved Plans), and such details must accord with the approved plans and the Associated Development Design Principles and (in respect of Work No 11 and 12) the vertical limits of deviation.

2.1.4 Drainage relating to each of the highway works must be approved by SCC pursuant to Requirements 13A (Work No.1B and 1C) and Requirement 22 (all other highway works).

2.2 Further, it may be necessary for other details to be approved by SCC prior to commencement of construction of some or all of these highway works. In a non-DCO context, this very detailed level of approval would ordinarily be given via a s278 or s38 Highway Act agreement. A s278 agreement authorises a developer to enter existing highway and carry out works (with a 'lawful excuse' for the purpose of the Highway Act 1980) such that the obstruction of the highway by such works is not an offence. Section 278 agreements also ordinarily provide a procedure for the auditing and sign-off of the works from a safety perspective as they are carried out, and a duty to maintain the highway works for a period of 12 months after which the works are adopted by the highway authority. Section 38 agreements are similar, but relate to the creation of highway on land not already dedicated as highway land.

2.3 The DCO (being a form of 'statutory authority') will in principle give SZC Co. the legal right to enter existing highway land, and non-highway land, to carry out the defined highway works without SCC's consent via a 238/s38 agreement or otherwise. However, it will be important to SZC Co. that it completes all highway works to detailed specifications which will 'reasonably satisfy' SCC for the purpose of article 20 (Construction and maintenance of new and altered street), in order to trigger the start of the 12 month period of maintenance after which the works are automatically adopted by SCC pursuant to article 20 unless otherwise agreed (see excerpt from article 20 below):

Construction and maintenance of new and altered streets

20.—(1) Any street to be constructed under this Order must be completed to the reasonable satisfaction of the highway authority and must, unless otherwise agreed between the undertaker and the highway authority, be maintained by and at the expense of the undertaker for a period of 12 months from its completion and at the expiry of that period by and at the expense of the highway authority.

(2) Where a street is altered or diverted under this Order, the altered part of the street must, when completed to the reasonable satisfaction of the highway authority, unless otherwise agreed, be

maintained by and at the expense of the undertaker for a period of 12 months from its completion and at the expiry of that period by and at the expense of the highway authority.

2.4 Article 21 dDCO empowers SCC to enter into agreements with SZC Co. in relation to a number of highway matters including *'the construction of any new street authorised by this Order'* and '*alterations'* of streets authorised by the Order. For this reason, SZC Co has always intended to enter into agreements with SCC relating to the DCO highway works pursuant to article 21, which would have similar content to s278/s38 agreements. This is the approach NNB Generation Company (HPC) Limited has taken in relation to the DCO highway works authorised by the Hinkley Point C DCO.

2.5 SZC Co. see it as very much in their interest to enter into such agreements with SCC. However, in order to give SCC further assurance that SZC Co. will enter into such agreements before starting the highway works, we propose additional drafting in article 21 which provides as follows:

"(3) The undertaker will not commence Work No. 1A(l), 1B, 1C, 9(b), 10(b), 11, 12, 13(b), 14, 15, 16 or 17 prior to entering into an agreement pursuant to paragraph (1) which provides details of the specification of the works which will reasonably satisfy the highway authority for the purpose of article 20(1) or article 20(2), and related provisions in relation to the maintenance and adoption of such works pursuant to that article."

2.6 As a corollary to this commitment by SZC Co, we propose to include drafting in the Deed of Obligation which commits SCC to entering into article 21 agreements with SZC Co. on reasonable terms, subject to dispute resolution in the case of disagreement.

2.7 We are aware that SCC has requested commuted sums to cover future maintenance costs in respect of some of the highway works. This is a matter of ongoing discussion between the parties. We are mindful of the interaction between future maintenance costs to SCC and commitments made under the Landscape and Ecology Management Plans for the Sizewell Link Road and the Two Village Bypass, secured by Requirement 22A. Following the ISHs we are proposing a revised Requirement 22A:

22A Associated developments: Landscape works

(1) Work No. 11 and Work No. 12 must not be commenced until details of the landscape works for that work have been submitted to and approved by East Suffolk Council.

(2) The details referred to in paragraph (1) must be in accordance with the Approved Plans (Schedule 7), unless otherwise agreed by East Suffolk Council.

(3) Landscape works must be carried out in accordance with the approved details.

(4) Landscape works in relation to Work No. 11 must be managed in accordance with the Two Village Bypass Landscape and Ecology Management Plan, unless otherwise agreed with East Suffolk Council.

(5) Landscape works in relation to Work No. 12 must be managed in accordance with the Sizewell Link Road Landscape and Ecology Management Plan unless otherwise agreed with East Suffolk Council.

3. TRAFFIC REGULATION ORDER

3.1 Article 22 and Schedule 20 of the dDCO provide SZC Co. with powers in relation to traffic regulation. Article 22 provides that the undertaker can make the traffic regulation orders specified in Schedule 20, relating to changes to speed limits for specific streets. In the

event that the undertaker needs other traffic regulations to be put in place, SCC's consent would be required pursuant to article 22(2). In either case, the undertaker must give at least 28 days' notice to the chief officer of police and SCC and advertise in such manner as SCC specify within 7 days of SCC receiving the undertaker's notice.

3.2 These provisions would not preclude the making of TROs by SCC outside of the DCO in the ordinary way.

3.3 The full text of article 20 is set out below for reference:

Traffic regulation measures

22.—(1) Subject to the provisions of this article, the undertaker may at any time, for the purposes of the authorised development make provision, in respect of those streets specified in column (2) and (3) of Schedule 14 (Traffic regulation measures), as to the speed limit of those streets as specified in column (4) of that Schedule.

(2) Without limiting the scope of the specific powers conferred by paragraph (1) but subject to the provisions of this article and the consent (such consent not to be unreasonably withheld) of the traffic authority in whose area the street is situated, which consent may be subject to reasonable conditions, the undertaker may, for the purposes or in connection with the authorised development—

(a) revoke, amend or suspend in whole or in part any order made, or having effect as if made, under the 1984 Act in so far as it is inconsistent with any prohibition, restriction or other provision made by the undertaker under this article;

(b) permit, prohibit or restrict the stopping, parking, waiting, loading or unloading of vehicles on any road;

(c) authorise the use as a parking place of any road;

(d) make provision as to the direction or priority of vehicular traffic on any road;

(e) permit or prohibit vehicular access to any road; and

(f) place traffic signs on or near a street (including on private land), subject to and in conformity with the directions issued by the Secretary of State pursuant to powers conferred by section 64, 65 and 85 of the 1984 Act, and in particular where such traffic signs are required for the safe design, management or operation of level crossings upgraded as part of Work Nos. 4B or 4C.

either at all times or at times, on days or during such periods as may be specified by the undertaker, in respect of streets within and outside the Order limits.

(3) Before complying with the provisions of paragraph (4) the undertaker must consult the chief officer of police and the traffic authority in whose area the street is situated.

(4) The undertaker must not exercise the powers in paragraphs (1) and (2) unless it has—

(a) given not less than 28 days' notice in writing of its intention so to do to the chief officer of police and to the traffic authority in whose area the street is situated; and

(b) advertised its intention in such manner as the traffic authority may specify in writing within 7 days of its receipt of notice of the undertaker's intention as provided for in sub-paragraph (a).

(5) Any prohibition, restriction or other provision made by the undertaker under paragraphs (1) and (2) has effect as if duly made by—

(a) the traffic authority in whose area the street is situated as a traffic regulation order under the 1984 Act; or

(b) Suffolk County Council as an order under section 32 of the 1984 Act (Power of local authorities to provide parking places), and the instrument by which it is effected may specify savings and exemptions (in addition to those mentioned in Schedule 14) to which the prohibition, restriction or other provision is subject,

is deemed to be a traffic order for the purposes of Schedule 7 to the Traffic Management Act 2004 (Road traffic contraventions subject to civil enforcement).

(6) Expressions used in this article and in the 1984 Act have the same meaning in this article as in that Act.

(7) If the traffic authority fails to notify the undertaker of its decision within 28 days of receiving an application for consent under paragraph (2), that authority is deemed to have granted consent.

Herbert Smith Freehills LLP

APPENDIX B

ACA DRAINAGE STRATEGY TECHNICAL NOTE (DCO TASK 4)

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GLOSSARY

2D/ 3D/ 4D	2-/ 3-/ 4-Dimensional
ACA	Ancillary Construction Area (known as "LEEIE" or "Land East of Eastlands Industrial Estate" in the DCO application)
AD	Associated Development
BOD	Basis of Design
BYLOR	Bouygues Travaux Publics / Laing O'Rourke (Joint Venture)
CDM	Construction (Design & Management) Regulations 2015
CIRIA	Construction Industry Research and Information Association
DCO	Development Consent Order
EA	Environment Agency
ECI	Early Contractor Involvement
EDF	Electricité de France
EPRTM	Trade name for reactor type proposed for SZC
ESC	East Suffolk Council
EW	Enabling Works
EWBD	Enabling Works Basic Design
HGV	Heavy Goods Vehicle
IDB	Internal Drainage Board
IDT	Integrated Design Team
LEEIE	Land East of the Eastlands Industrial Estate (referred to as the "ACA" or "Ancillary Construction Area" in this document
LLFA	Lead Local Flood Authority
mAOD	Metres Above Ordnance Datum
MCA	Main Construction Area
MW	Megawatt
NNB	Nuclear New Build
PIMP	Percentage Impermeable
QS	Quantity Survey (/ -or/ -ing)
RSPB	Royal Society for the Protection of Birds
SCC	Suffolk County Council
SFR	Safety Functional Requirement
SHE	Safety, Health and Environment
SSSI	Site of Specific Scientific Interest
SuDS	Sustainable Drainage Systems
SZB	Sizewell B
SZC	Sizewell C
TCA	Temporary Construction Area
TSS	Total Suspended Solids
WBS	Work Breakdown Structure (Package)
WMZ	Water Management Zone

OVERVIEW – SECOND REVISION

The Sizewell C (SZC) Development Consent Order (DCO) has been submitted and included a site wide Outline Drainage Strategy. This technical note aims to provide a more detailed background of the proposed Ancillary Construction Area (ACA) site (also known as Land East of Eastlands Industrial Estate (LEEIE)) and explain the development of the surface water management proposals for the site while it is operational.

The ACA will be one of the first areas of development as part of the SZC construction project. The ACA will be temporary and operational for approximately ten years before it is decommissioned at which point the site will be returned to predevelopment condition.

A first issue of the basic drainage design note for the ACA was shared informally with stakeholders during 2020, including East Suffolk Council (ESC), Suffolk County Council (SCC), the Environment Agency (EA), East Suffolk Internal Drainage Board (ESIDB) and Natural England (NE). A meeting was held with stakeholders on 17th December 2020 and feedback gained. In addition, SCC as the Lead Local Flood Authority (LLFA) wrote a letter to SZC Co. dated 8th February 2021 (Appendix A1), setting out concerns around drainage design. Therefore, this document has been revised to address the feedback received.

The surface water drainage design has been progressed to a basic level of design, to demonstrate that the proposed strategy can sufficiently manage surface water runoff generated by the proposed development, within the Order Limits and whilst complying with current local and national guidance.

The revised document:

- Provides more information on historic infiltration data on the ACA,
- Updates the discharge strategy, and therefore Sustainable Drainage (SuDS) proposals,
- Removes below ground storage structures; and
- Provides assurance that the SuDS storage features have been designed in accordance with best practice guidance and shows there is space for these on site within the order limits.

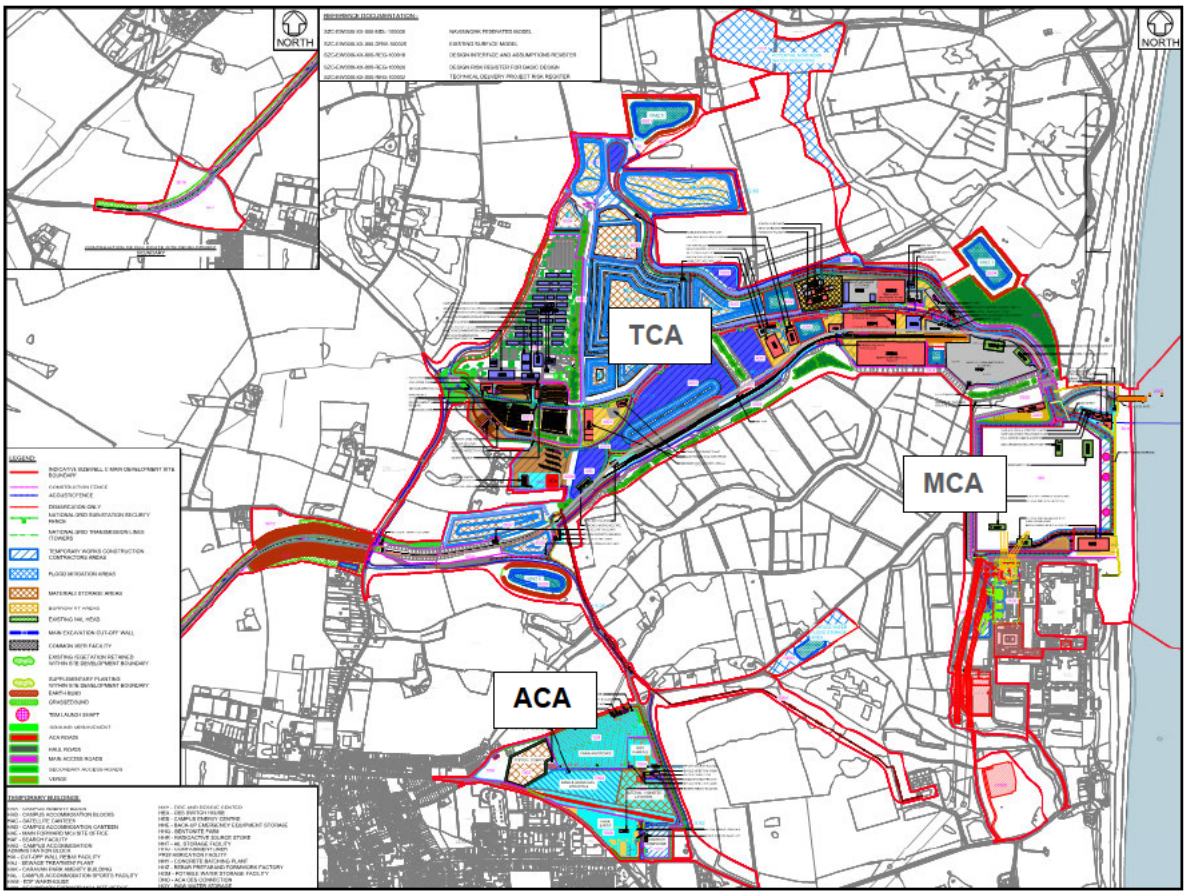
The design will be updated in the next design phase in conjunction with engagement with ESC, SCC, NE, EA and ESIDB.

1 INTRODUCTION

1.1 General

1.1.1 This technical note has been prepared to provide additional detail on the proposed Sizewell C (SZC) nuclear power station Enabling Works Basic Design (EWBD) surface water management proposals. This document primarily focuses on the Land East of the Eastlands Industrial Estate (LEEIE), as described in the Development Consent Order (DCO) submission, also known as the Ancillary Construction Area (ACA), the location of which is shown in Figure 1-1. Throughout this document, this area will be referred to as the ACA. SZC Co. acknowledge the design of surface water management will be updated and change throughout the next phases of design. SZC Co. will work collaboratively with Suffolk County Council (SCC) and other stakeholders throughout the detailed design phase.

Figure 1-1 - Sizewell C site, showing DCO boundary, ACA, MCA and TCA areas



1.1.2 Basic Design has been developed by SZC Co.

1.2 Project Background

1.2.1 The Sizewell C site is located on the Suffolk coast, approximately mid-way between Felixstowe and Lowestoft, to the north-east of the town of Leiston.

1.2.2 SZC Co. is applying for development consent to construct, operate and maintain Sizewell C nuclear power station. The project will take approximately 9-12 years to complete construction. The ACA will be required for the duration of this construction period to support the main construction works. After this point, the ACA will be returned to its existing state (i.e. a grassed field). This is summarised in the Development Consent Order (DCO) available publicly.

2 ACA CONSTRUCTION AREA

2.1 Existing ACA Site

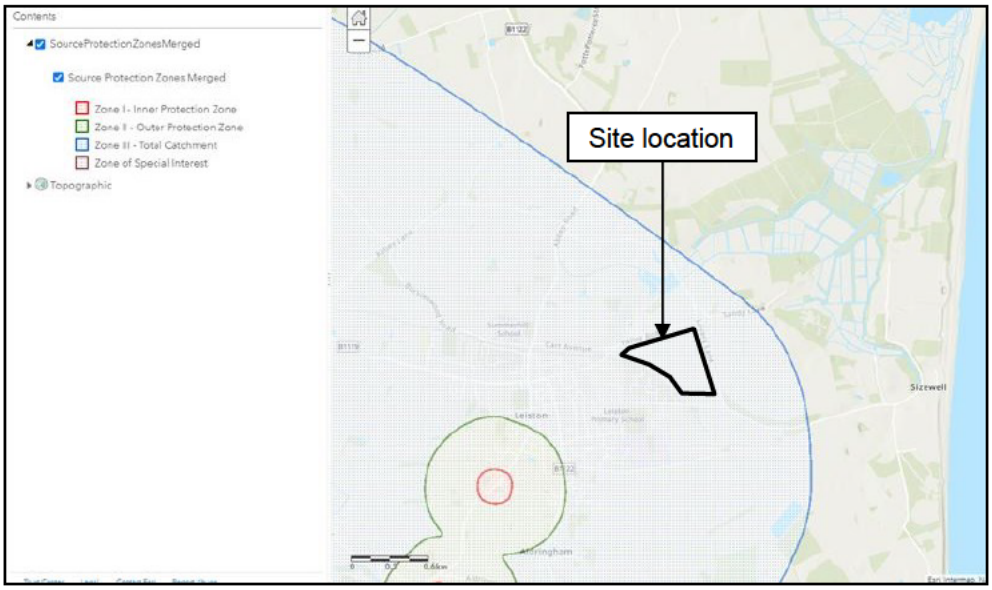
2.1.1 The ACA is currently an agricultural greenfield as shown in Figure 2-1 below, bounded by Valley Road, Lover's Lane, King George's Avenue and an existing railway line from Saxmundham. The site is approximately 30 hectares in area.

Figure 2-1 - Existing ACA greenfield

2.1.2 The whole of the proposed ACA is within Zone III of the Environment Agency (EA) groundwater source protection zone, shown in Figure 2-2. Although this does not mean a ban on discharge of surface water to groundwater at this site, it would need to be discussed with the EA should infiltration be considered in future on this site as a means of surface water disposal. However, as set out in Section 3 below, the potential for infiltration is extremely limited.

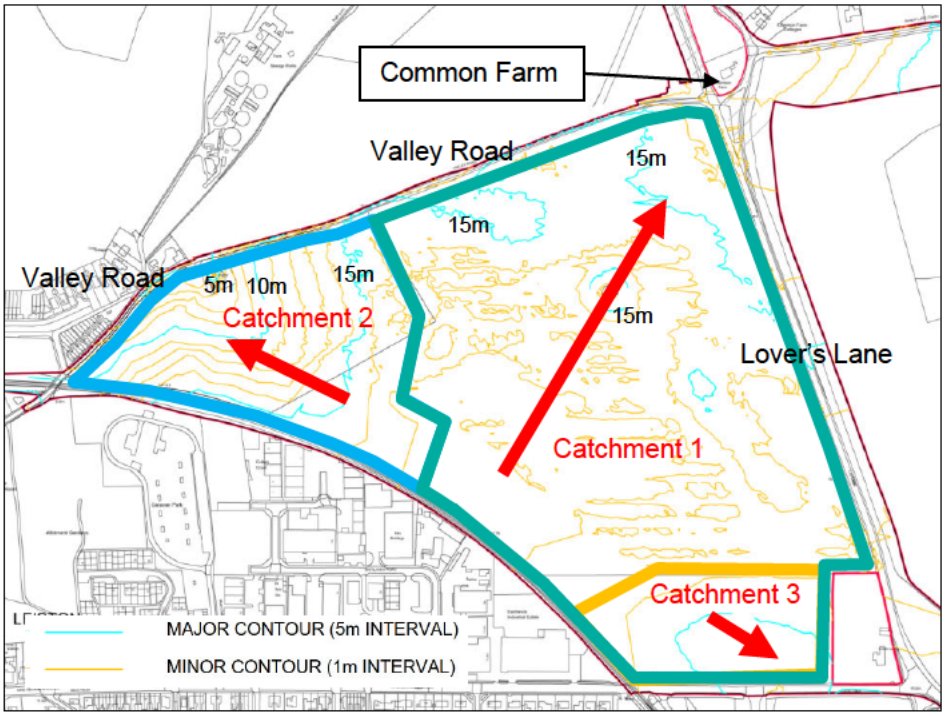
2.1.3 Groundwater levels in the ACA are shown to range between 1.6 mAOD and 2.1 mAOD (based on Environment Statement groundwater contours, presented here as Appendix B1).

Figure 2-2 - ACA groundwater source protection zone map



2.1.4 Figure 2-3 outlines the natural catchments based on the existing ground levels that were surveyed in 2019 using Lidar. The contours shown are at 1m intervals with the major (5m) contours highlighted in blue. The north-west section of the ACA is set lower than the remainder of the ACA and therefore does not contribute to the same catchment. Runoff from this area poses potential flood risk to the residential dwellings to the north of Valley Road. Catchment 2 encompasses approximately 4.4 ha of the ACA. Catchment 1 generally falls to the north-east to the junction of Valley Road with Lover's Lane at Common Farm which appears to generally travel towards the Leiston Drain. The southern part of the ACA falls south towards King George's Avenue, and is likely captured by an existing network within King George's Avenue, or infiltrates through roadside drainage systems. Catchment 3 currently includes an area of low-medium flood risk (i.e. between 1:30 and 1:1,000-year rainfall events). Flooding in this area will be alleviated as the site will capture surface water via permeable paving as well as a drainage network and discharged to the north.

Figure 2-3 - ACA site surface existing profile and surface water catchments (Waldeck Drone Survey 2019)



2.1.5 Further topographical surveys will be undertaken in 2021 to validate the existing data and inform the detailed design.

2.1.6 Greenfield runoff rates for the site have been calculated using UK SuDS guidance and are shown in Table 2-1 below. The output of the results from the UK SuDS calculation is attached in Appendix C1.

Table 2-1 - ACA greenfield runoff rates

Return Period (years)	Greenfield Rate (l/s)
1	61.3
Q_{BAR}	**70.4**
30	172.5
100	250.6

Q_{BAR} - peak rate of flow from a catchment for the mean annual flood - return period of approximately 1:2.3 years.

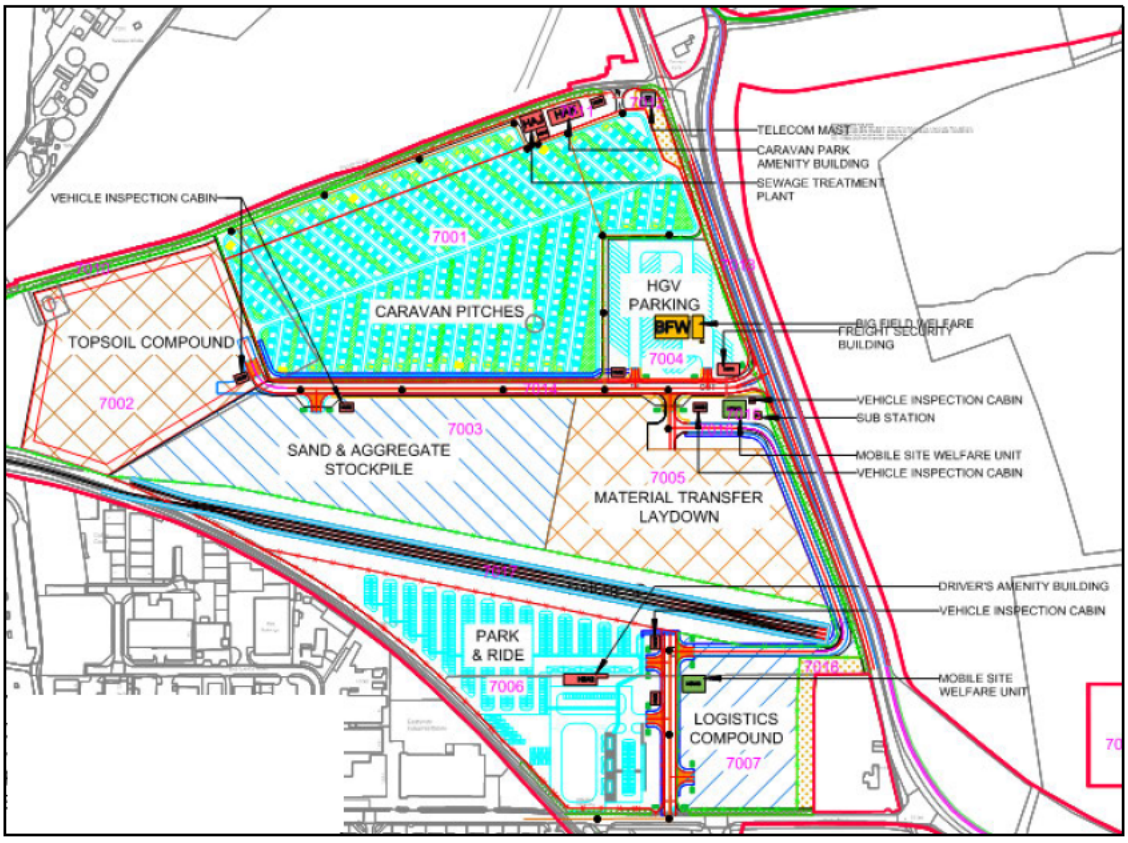
2.2 Proposal Overview

2.2.1 The ACA is proposed as a multi-purpose site with the following facilities:

- Caravan pitches to house approximately 400 caravans, providing temporary accommodation for some Contractors.
- Heavy Goods Vehicle (HGV) parking for Contractor vehicles required on site.
- Material stockpile areas – including a sand & aggregate stockpile area, a topsoil stockpile, and material transfer laydown area.
- Park and ride and logistics compounds to allow transport of staff to the main works areas.
- A rail-head central to the site to provide access for deliveries to site via rail.

These areas are shown in Figure 2-4.

Figure 2-4 - ACA areas



2.2.2 The ACA is isolated from the TCA and MCA, and therefore has an independent surface water drainage network to that serving the main construction site. With the above in mind, a drainage strategy has been developed for the ACA during the enabling works pre-detailed design stage,

building from the overall drainage strategy. This design will be updated and refined during detailed design and with continued engagement with stakeholders such as East Suffolk Council (ESC), SCC, Natural England, the EA, and East Suffolk Internal Drainage Board (IDB). The drainage design strategy is highlighted in the following section.

3 ACA DRAINAGE STRATEGY DEVELOPMENT

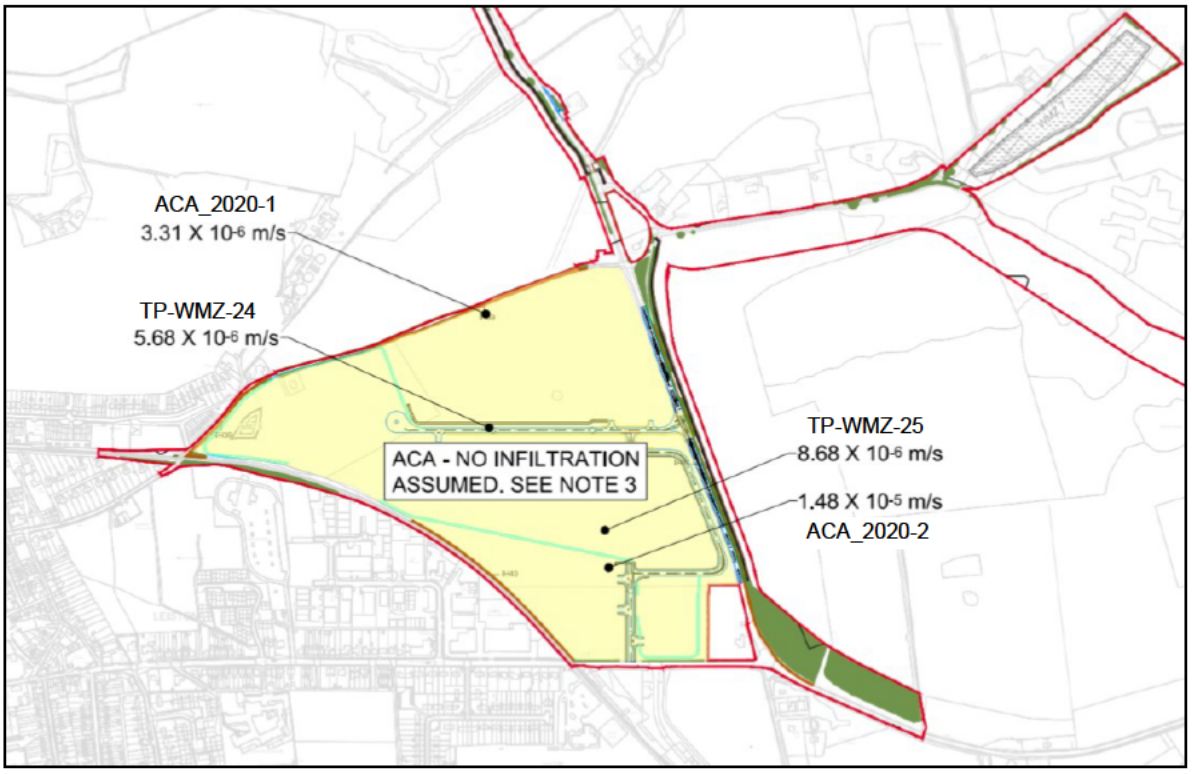
3.1 Background

3.1.1 The ACA drainage strategy has been informed by the site-wide Outline Drainage Strategy submitted with the DCO documentation (SZC Development Consent Order Outline Drainage Strategy EN010012-001802-SZC_Bk6_ES_V2_Ch2_Appx2A), as well as the proposed plot plan, described in Section 2.

3.1.2 As stated in the DCO drainage strategy, the ACA is known to have a low infiltration potential and therefore no infiltration has been conservatively assumed in Basic Design. The surface water runoff from this site would be managed on site, stored, and then discharged to a suitable nearby watercourse at an equivalent rate of Q_{BAR}, as agreed with external stakeholders on 17th December 2020 (see meeting minutes, item 4 in Appendix D1).

3.1.3 Figure 3-1 shows the historic infiltration rates recorded during ground investigation campaigns in 2016 by Structural Soils Limited (2016 Onshore Ground Investigation Campaign. Factual Report on Ground Investigation ref. SZC-SZC030-XX-000-REP-100000) and in 2020 by Fugro (Report on Ground Investigation without Geotechnical Evaluation. Sizewell Infiltration Testing ref G200003U_GIR Rev 02), within the ACA site. Infiltration test results from both reports are shown in Appendix E1. Whilst infiltration tests completed in April 2020 show improved infiltration rates and a potential opportunity to optimise the surface water drainage design, at this stage, no infiltration is assumed as a conservative measure to ensure that all surface water features are sized adequately. Further infiltration testing is planned in the ACA to confirm the infiltration potential and the design will be revised accordingly during Detailed Design. Infiltration has not been dismissed as an option for surface water disposal, and where permeable pavements are proposed, for example, it is expected that a percentage of surface water will infiltrate to ground. However, given previous history of ponding issues on the site, infiltration has not been relied upon in the design.

Figure 3-1 - ACA infiltration rate summary (results shown in Appendix E1)



3.1.4 The proposed drainage design will prioritise SuDS as a means of surface water treatment and discharge where practicable. The SuDS features currently proposed in the ACA include:

- Swales / Infiltration trenches (combined)
- Sediment ponds (2 no.)
- Permeable paving (where suitable) with filter drains

As well as the above, proprietary devices such as oil separators are also considered.

3.2 Design Strategy

3.2.1 The three existing catchments on site require different drainage strategies. As no infiltration is assumed, all surface water will be required to be discharged via watercourses adjacent to the site.

3.2.2 The original drainage strategy proposed in basic design aimed to mimic the existing site characteristics and predominantly discharge surface water runoff to the Leiston Drain at outfall O6, along Lover's Lane, at greenfield runoff rates. However, discussions with the EA, ESC, SCC and the IDB in

December 2020 concluded that there was a preference to make the primary surface water discharge from the ACA to the Sizewell Marshes instead (see Appendix D1 for meeting minutes, item 2).

3.2.3 To prevent altering the existing runoff characteristics, outfall O6 has been retained and is proposed to discharge flows from the Catchment 2 within the ACA only. This modification aims to improve water quality and quantity on site whilst providing an opportunity to recharge the Sizewell Marshes Site of Specific Scientific Interest (SSSI). It is important that the SSSI is neither overwhelmed with additional surface water runoff, nor starved of surface water during the construction and operation of SZC. Consequently, the approach adopted for the drainage of this site aims to maintain the existing drainage characteristics and forms the basis of the groundwater and surface water assessment in Volume 2, Chapter 19 of the Environmental Assessment. The importance of maintaining these drainage characteristics for the main development site has been reinforced in discussions with Natural England, the Suffolk Wildlife Trust, the Royal Society for the Protection of Birds (RSPB) and East Suffolk IDB.

3.2.4 Catchment 1 and 3 shown in Figure 2-3 are combined and make up 85% of the site. These catchments are proposed to be collected in gravity networks, either through permeable surfaces and filter drains where suitable, or gullies/channels with silt traps in hard surfaced areas. The surface water will then be conveyed towards a sediment pond east of the ACA, to provide attenuation and additional treatment, before discharging to the Sizewell Marshes.

3.2.5 Surface water runoff in Catchment 2 will be captured separately through swales and a sediment pond within the catchment, and then pumped east towards outfall O6 on Lover's Lane, discharging to the Leiston Drain. See Appendix F1 for the ACA surface water drainage general layout (SZC-EW0320-ATK-XX-000-XXXXXX-DRW-CCD-000004).

3.2.6 The outflow rate at both outfall locations will be restricted to the Q_{BAR} as agreed in the meeting quoted above.

3.2.7 Both sediment ponds (East ACA WMZ and West ACA WMZ) are be sized for a 1 in 100 year return period, including a 20% climate change allowance in accordance with the DCO outline drainage strategy.

3.2.8 A hydraulic model for the overall site has been constructed in Innovyze Microdrainage (2019) to size the networks and attenuation/infiltration features. The hydraulic model parameters used are summarised in Table 3-1.

Table 3-1 - ACA hydraulic model input parameters

	Parameter	Notes
Rainfall-Runoff method	Flood Studies Report (FSR), Flood Estimation Handbook (FEH) 1999 and 2013	All three models run to undertake sensitivity checks
Return Periods (years)	1, 30 and 100	As per DCO Outline Drainage Strategy [1]
Storm durations (min)	15 to 1440 (12 durations modelled)	As per DCO Outline Drainage Strategy [1]
Global time of entry (min)	15	Assumed site wide, however, to be refined (and likely increased) per catchment during detailed design
Volumetric Run-off Coefficient	0.761, 0.817 (summer, winter)	Wallingford Procedure Vol 1 Equation 7.3
Climate change (%)	20	As per DCO Outline Drainage Strategy [1] and EA guidance [2]
PIMP (%)	100	As per DCO Outline Drainage Strategy [1]

[1] Environmental Statement – 6.3 Volume 2 Main Development Site, Chapter 2 Description of the Permanent Development, Appendix 2A Outline Drainage Strategy (EN010012-001802-SZC_Bk6_ES_V2_Ch2_Appx2A)

[2] Environment Agency – Flood risk assessment: climate change allowances - Table 2: peak rainfall intensity allowance in small catchments (less than 5 km2) or urban drainage catchments (based on a 1961 to 1990 baseline)

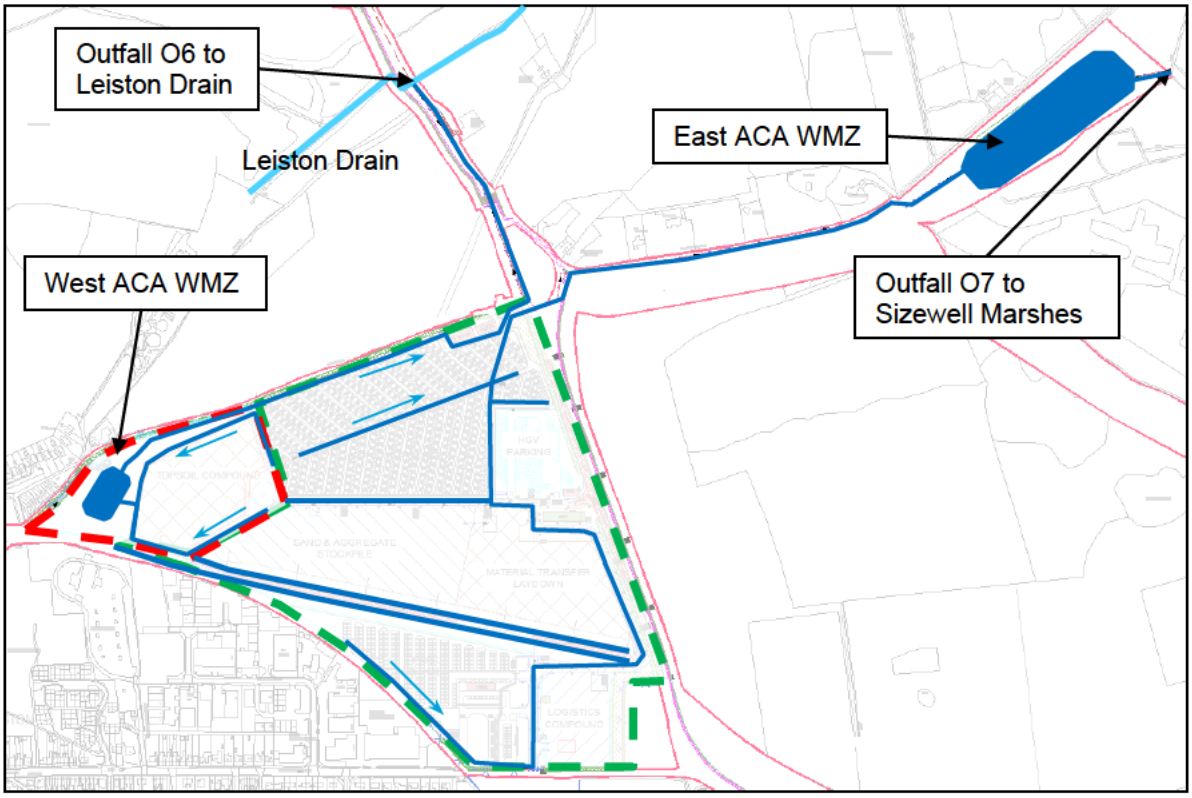
3.2.9 Main Catchment Overview (Catchment 1 & 3)

3.2.10 Catchments 1 & 3 are proposed to drain through a trunk network that runs from the park and ride area to the south, around the railhead, along the site access road, through the caravan pitches, to the north east of the main ACA site. This is shown indicatively in Figure 3-2 where catchments 1 & 3 are bound by the dashed-green line. From here, the surface water will be conveyed to an attenuation/infiltration basin (East ACA WMZ) east of the main ACA site, which will provide additional sediment treatment before discharging to the Sizewell Marshes at rate equivalent to Q_{BAR}.

3.2.11 Onsite attenuation will be provided in the subbase of the caravan pitches, logistics compound and materials transfer laydown areas, and is discussed further below. Groundwater levels in the ACA are shown to range between 1.6 mAOD and 2.1 mAOD (based on Environment Statement groundwater

contours in Appendix B1), much lower than the finished ground levels (average 15 mAOD).

Figure 3-2 - ACA discharge solution – overview



3.2.12 The outflow rate at the proposed outfall locations has been proportionally obtained from the calculated Q_{BAR} for the ACA site. Surface water will be restricted to 10.5 l/s and 59.9 l/s at outfall 06 and outfall 07, respectively.

3.2.13 An initial conservative storage estimate for the East ACA WMZ resulted in a storage requirement of 21700 m^3 as stated in the Water Management Zone Summary technical note (ref. SZC-EW0321-ATK-XX-000-XXXXXX-NOT-CCD-000001). The assessment allowed for a proposed outflow flowrate of 59.9 l/s, however excluded any allowance for storage upstream of the WMZ within the pipe network and any SuDS features, which will likely result in a lower attenuation volume.

3.2.14 Hydraulic modelling of the ACA has been progressed and the water volume produced during a 100-year rainfall event including 20% climate change is 15,600 m^3. The current proposed storage pond using a 59.9 l/s outflow rate is as per Table 3-2. Further work will be undertaken during Detailed Design to refine the hydraulic modelling and optimise the storage requirements.

3.2.15 It is acknowledged that the location of the East ACA WMZ is beside a low-lying area which has been identified as being susceptible to flooding in the latest Flood Risk Assessment (FRA). The East ACA WMZ has been positioned to be outside the flooding extent of a 1 in 100 year fluvial flood event + 25% climate change as well as the 1,000 year coastal inundation flood extent.

Table 3-2 - East ACA WMZ attenuation basin summary

	Pond / Water Management Zone
Pond volume (m^3)	15,650 (3D model volume, excluding freeboard)
Crest level (mAOD)	3.000
Invert level (mAOD)	1.600
Pond depth (m)	1.100 (excluding freeboard)
Pond side slopes (1:X)	3
Freeboard (mm)	300
Groundwater level (mAOD)	1.100

3.2.16 An indicative detail of what the WMZ storage pond may look like is shown in Figure 3-3 and Figure 3-4. The WMZs will be developed during Detailed Design stage and will include details of the sediment forebays, access ramps, inlet and outlet structures and maintenance regimes. The East ACA WMZ is not designed to infiltrate due to the proximity to ground water levels. Whilst it is expected that there could be some limited infiltration, the West ACA WMZ basin is not designed to infiltrate at this stage and is therefore sized conservatively.

Figure 3-3 - WMZ - indicative detail

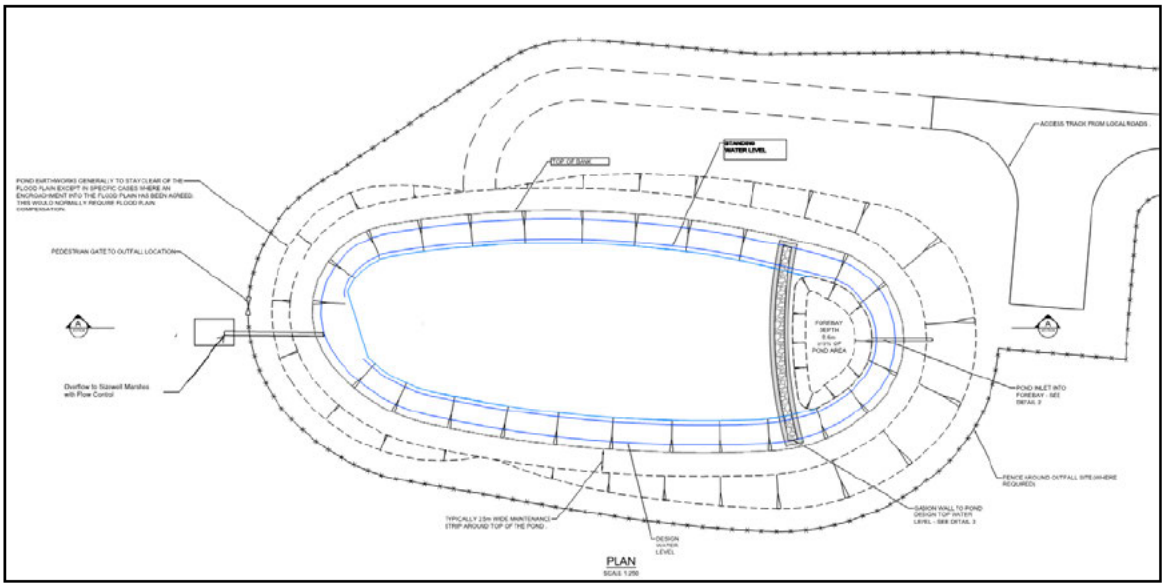
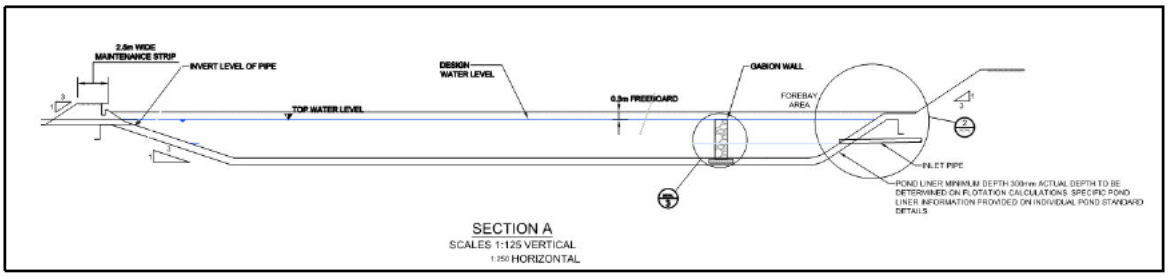


Figure 3-4 - WMZ - indicative section

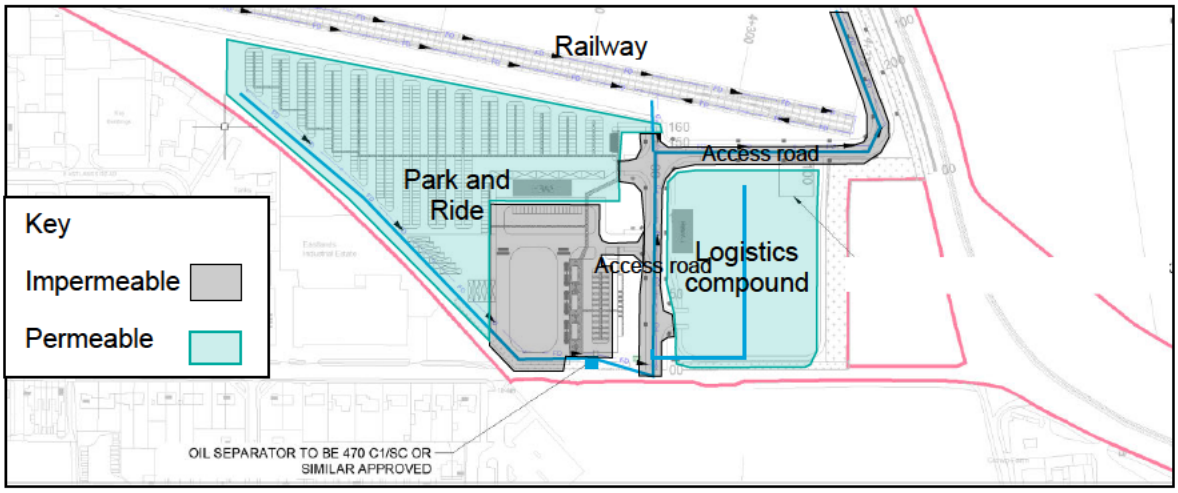


3.2.17 A high-level description of the drainage systems for each area within the main catchment are described in the sections below.

3.2.18 ***Park and Ride***

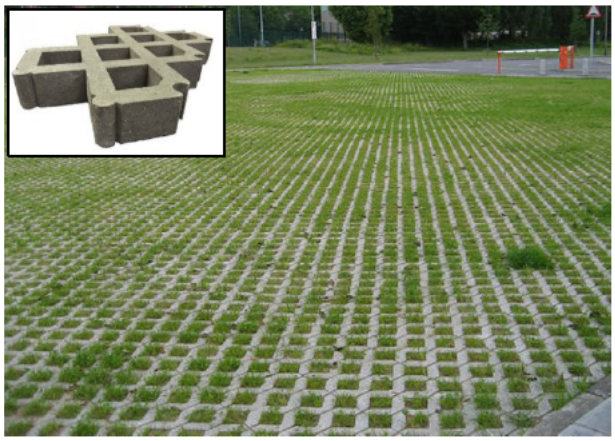
3.2.19 The park and ride area comprises two different surface types as shown in Figure 3-5.

Figure 3-5 - ACA discharge solution south of railway



3.2.20 The car parking area is proposed to generally have a permeable surface. This may be a truck-pave solution or similar, as shown in Figure 3-6.

Figure 3-6 - Truck-pave surface example



3.2.21 The area to the south-east of the park and ride is reserved for coaches and other large vehicle parking. At this stage, this area is proposed to be concrete pavement with channels and gullies to collect potential oil spills. This area may also be surfaced similarly to the park and ride area and use a permeable pavement but will be considered during Detailed Design.

3.2.22 ***Network Design***

3.2.23 Because the ACA is assumed to have no infiltration, from a hydraulic model perspective, all areas are considered to be 100% impermeable and all surface water runoff will be captured via their respective drainage systems.

3.2.24 The head of the trunk network at the park and ride begins with a 300mm dia. pipe, which increases to a 600mm dia. to drain the runoff from the park

and ride. The internal secondary and tertiary networks have not been modelled at this stage, however across the permeable surface, there will be a number of filter drains at the base of the Type 3 pavement build-up which will connect to the trunk main.

3.2.25 For the impermeable surface area in the park and ride, it is proposed to drain the internal areas by a combination of gullies and channels, which drain to the carrier drains. All channels and gullies are to contain silt traps to provide a primary level of treatment. At this stage, an oil separator is proposed to contain the potential risk of oil spillage from the car park where large vehicles are parked long-term in line with pollution prevention guidance. Consideration of an oil separator is based on a risk management approach to provide reliability and robustness in the design to ensure no oils/hydrocarbons enter the SSSI downstream. It is acknowledged that SCC prefers to not use oil separators to capture and treat oil spills and instead supports the use of a lined permeable pavement whereby oil spills can be treated through granular pavement layers. To provide further treatment and protection of the receiving watercourse, a hydrodynamic separator such as a Hydro Downstream Defender may also be utilised in conjunction with a permeable pavement. This approach will be considered at the next design stage and is further discussed in Section 4.4.8.

3.2.26 ***Access Road drainage***

3.2.27 The road surface will be standard asphalt pavement, and runoff is currently proposed to be collected using standard kerb gullies at standard spacing. The gully leads of approximately 150mm diameter shall be connected to the collector system beneath the road. Implementation of a SuDS system such as a filter/fin drain will be considered during detailed design as an alternative to provide surface water treatment at the source. Use of filter drains versus standard collection systems such as kerb and gullies will be considered on a risk-based approach in the next design phase.

3.2.28 Because of the types of vehicles using the roads, a wheel wash is proposed at the entrance to the site to remove sediment from earthworks vehicles before coming into the ACA and going out of the ACA onto the public road. Additional sweeper vehicles will be utilised to maintain the cleanliness of the road. This detail needs to be developed during the next design phase.

3.2.29 ***Logistics Compound***

3.2.30 Similar to the Park and Ride area, the logistics compound is proposed to have permeable surfacing. The pavement build-up beneath this is currently proposed to include a sub-base of Type 3 fill providing a minimum porosity of 30%. Internal secondary and tertiary networks have not been modelled,

however across the area, there will be a number of filter drains at the base of the Type 3 pavement layer which will connect to the trunk main.

3.2.31 ***Railway drainage***

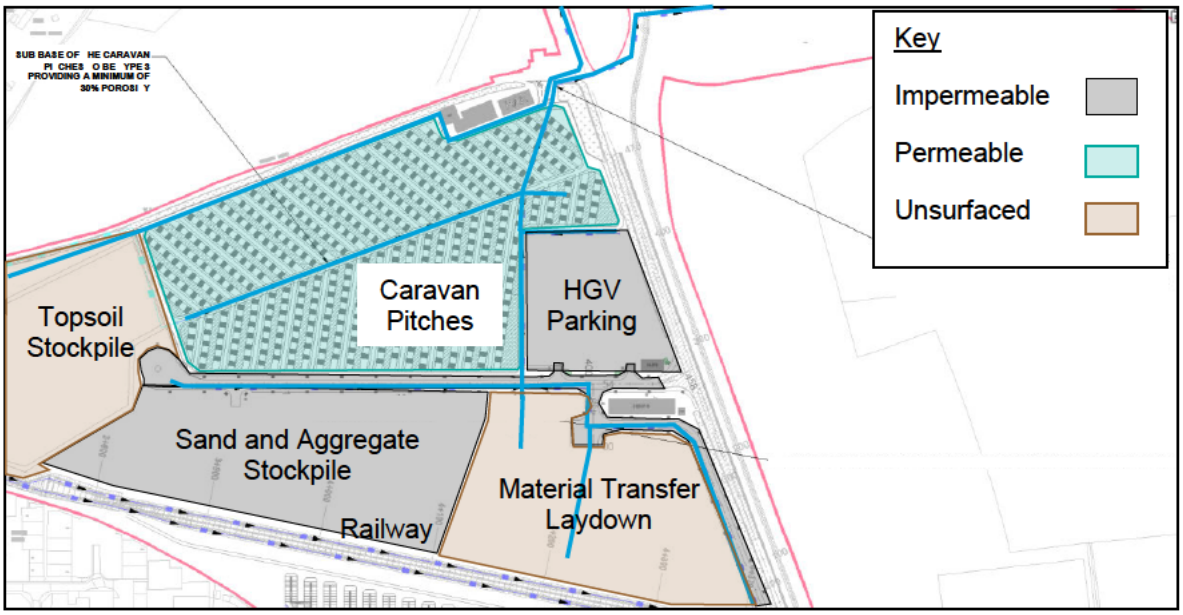
3.2.32 The runoff from the rail route is proposed to be collected by filter drains at a minimum crossfall of 1 in 30 draining on either side of the cutting, with catch pits proposed at 60m centres. The network discharges into the trunk main under the road via a sleeve through the rail retaining wall. Concrete perforated drainage channels will be considered as an alternative to filter drains to reduce the risk of blockages which are commonly experienced when using filter drains in railway applications. The trains will be diesel powered and will be able to park at this railhead. Refuelling will not be permitted on site, therefore the risk of oil spillages is lowered. A by-pass oil separator is proposed in this area to prevent oils and other hydrocarbons from entering the main network.

3.2.33 ***Sand & Aggregate Stockpiles***

3.2.34 The sand and aggregate stockpile areas will likely have a concrete base to allow materials to be constantly deposited in this location and moved around site via excavators and lorries. The surface water is currently proposed to be collected around the perimeter of the area via gullies and channels with silt traps to filter out the sediment. Further sediment settlement will be provided as the flows will convey to the East ACA WMZ. With increased engagement with logistic suppliers of sand and aggregate planned at the next design phase, discussions will consider the possibility to introduce swales in this area to capture and treat surface water runoff. Alternatively, implementation of an SDS Aqua-Xchange or equal filter drain network will be considered at the next design stage as opposed to conventional pipe/gully network to provide treatment opportunity.

3.2.35 It is understood SCC has concerns about blockages of silt traps and the lack of SuDS used in this part of the site. This needs further discussion and collaborative working with SCC and the EA to provide a suitable solution, however at this stage, standard collection methods with silt traps are proposed and maybe revised during Detailed Design. A maintenance management plan will be required and submitted prior to commencement of construction on the site.

Figure 3-7 - ACA discharge solution north of railway



3.2.36 ***Material Laydown Transfer***

3.2.37 The material transfer laydown area will likely be a gravelled surface, and therefore will allow surface water to infiltrate through granular materials, be naturally treated, and then be collected through filter drains within the sub-base build-up. A Type 3 granular fill providing a minimum porosity of 30% is proposed to provide storage across this area. Secondary and tertiary filter drains across the material transfer laydown area will convey flows to the trunk main.

3.2.38 ***HGV parking***

3.2.39 The surface of the HGV parking area is currently proposed to be a concreted heavy-duty pavement to allow for vehicle loads from HGVs. The concrete pavement will not allow infiltration, and therefore the surface water is currently proposed to be captured via gullies and channels with silt traps. The HGV area surface water network will be routed to a suitably sized oil separator to treat surface water for potential oil contamination prior to conveyance into the main network for the ACA.

3.2.40 This area will be revisited during Detailed Design to consider use of a permeable surface to filter contaminant naturally and use a SDS Aqua-Xchange or equal filter drain system, however at this stage, an oil separator is considered necessary given the pavement type and intended use.

3.2.41 ***Caravan Pitches***

3.2.42 The caravan pitch area has a permeable pavement surface which is proposed to be truck-pave (Figure 3-6) or similar. The pavement build-up beneath this is currently proposed to include a 200mm thick sub-base of Type 3 fill providing a minimum porosity of 30% this provides attenuation. The thickness of the sub-base has been based on the hydraulic performance and may be revised following structural design of the pavement. The flows will then convey to the trunk main and towards the East ACA WMZ.

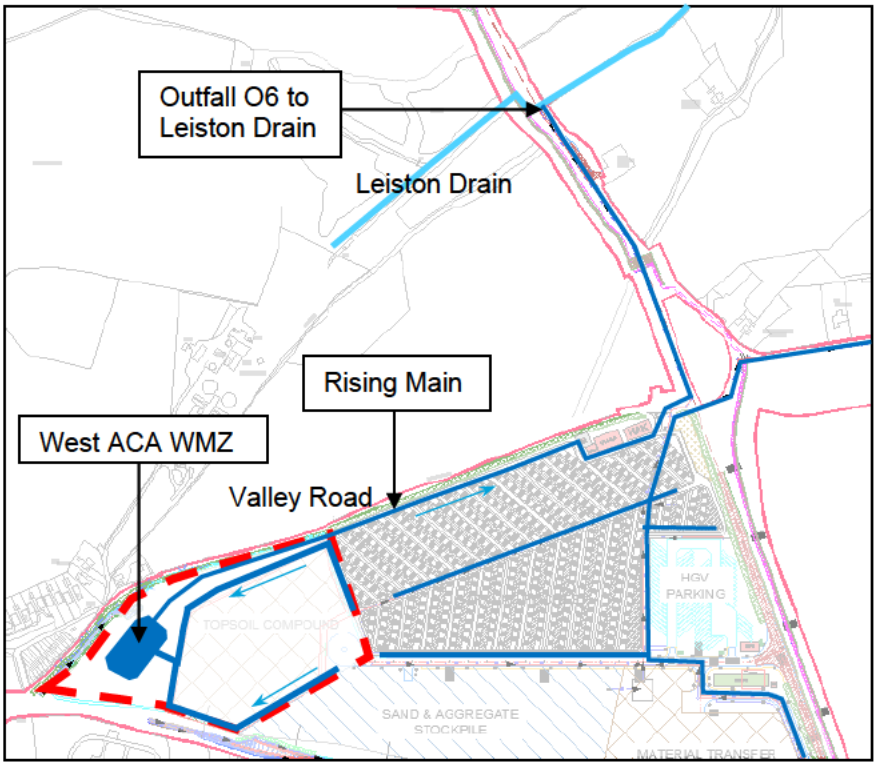
3.2.43 **Topsoil compound and area west of the topsoil compound (Catchment 2)**

3.2.44 This area of the site drains to the north-west towards Valley Road. There is an existing surface water network along Valley Road. SCC have indicated that the external network would require upgrade should a connection from the ACA be made to this asset due to capacity issues. Because of the uncertainty around this, at this stage the current solution will not discharge to the external network. This will be discussed with SCC to assess the possibility and the extent of upgrade to the existing network required.

3.2.45 Therefore, surface water runoff in Catchment 2, indicatively outlined by dashed-red line in Figure 3-8 is proposed to be captured separately through perimeter swales that convey to a sediment pond (West ACA WMZ) within the catchment and to stop any water running off site. As no infiltration is assumed, the attenuated runoff will require pumping from the low point of the site, east towards outfall O6 on Lover's Lane, discharging to the Leiston Drain.

3.2.46 The proposed swales and West ACA WMZ will be sized to accommodate the runoff volumes for a 100-year return period storm event. The swales will be designed in accordance with the CIRIA C753 SuDS Manual and check dams may be incorporated to the design to restrict the average velocity given that the existing ground levels fall steeply and to provide opportunity to treat captured runoff.

Figure 3-8 - ACA discharge solution – Topsoil Compound and area west of compound



3.2.47 An initial conservative storage estimate for the West ACA WMZ resulted in a storage requirement of 4000 m^3, with a proposed flowrate to the Leiston Drain of 10.5 l/s, as stated in the Water Management Zone Summary technical note (ref. SZC-EW0321-ATK-XX-000-XXXXXX-NOT-CCD-000001). The proposed rate is based on the calculated Q_{BAR} for the ACA site (Appendix C1). This assessment was undertaken using a source control calculation, which excluded any onsite storage upstream of the WMZ within the swale network.

3.2.48 Hydraulic modelling of the ACA has been progressed and the water volume produced during a 100-year rainfall event including 20% climate change is 1,900 m^3. Further work will be undertaken during Detailed Design to refine the hydraulic modelling and optimise the storage requirements. The current proposed storage pond using an outflow rate of 10.5 l/s is as per Table 3-3.

Table 3-3 - West ACA WMZ infiltration basin summary

	Pond / Water Management Zone
Pond volume (m^3)	2,100 (3D model volume, excluding freeboard)
Crest level (mAOD)	8.000
Invert level (mAOD)	5.700
Pond depth (m)	2.0 (excluding freeboard)
Pond side slopes (1:X)	3
Freeboard (mm)	300
Groundwater level (mAOD)	2.100

3.2.49 The attenuated volumes will be discharged to the Leiston Drain via a rising main of 100mm diameter at a rising gradient of 1:70 with a duty-assist pump capacity of 10.5l/s. The next stage of design for the West ACA WMZ sediment pond will include assessment for pump failure events to ensure that in the event of a pump failure, surface water runoff would not leave the site.

3.2.50 ***Topsoil Stockpile***

3.2.51 When the site is first occupied, the topsoil across the site will gradually be stripped and stockpiled in the north-west corner of the site as indicated on the general arrangement figures. The topsoil stockpile will be hydroseeded to minimise sediment runoff, however before the grass is established, the surface water will need to be captured and treated prior to discharge to the Leiston Drain. Furthermore, the topsoil stockpile will likely need to be churned approximately every two years to retain the nutrients and minerals in the soil, to allow it to be reused in the future. This will disturb the vegetated state of the topsoil stockpile and increase sediment runoff in the surface water.

3.2.52 The topsoil stockpile is proposed to be surrounded by a combination of hay bales and swales to remove the majority of the sediment in the surface water. The swales will convey surface water runoff towards the north west to the West ACA WMZ where further treatment can be undertaken. A typical detail of the swales and hay bales is shown in Figure 3-9 and Figure 3-10.

Figure 3-9 - Typical swale/infiltration trench detail

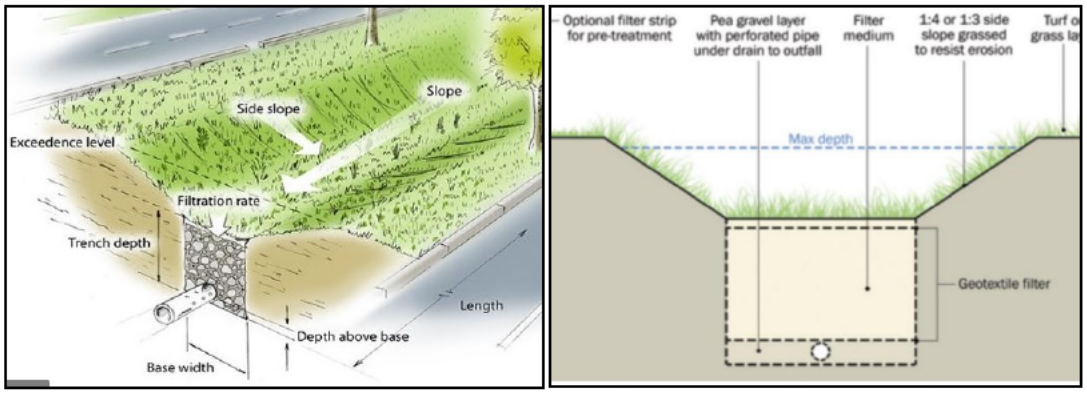
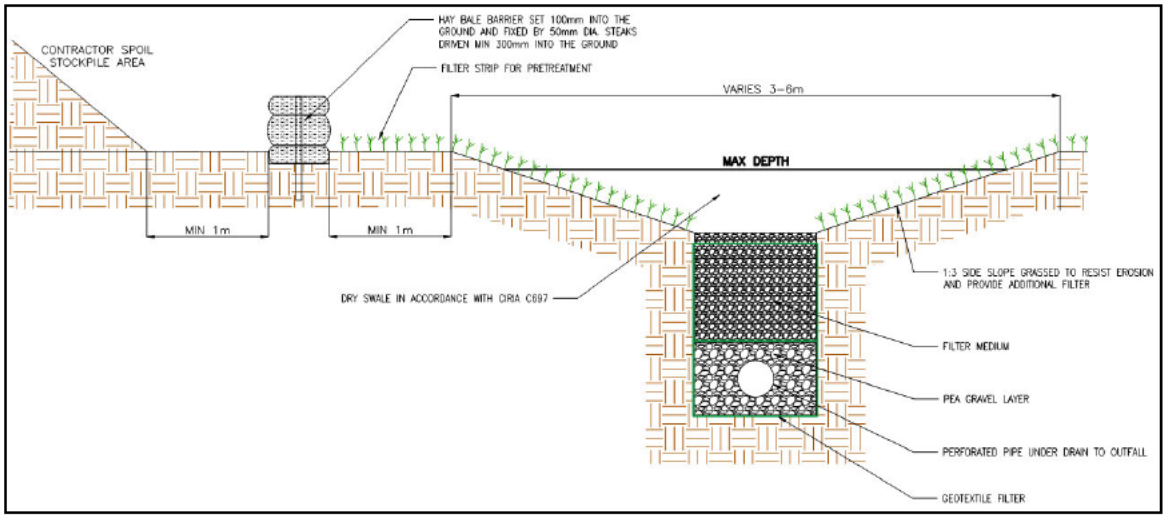


Figure 3-10 - Stockpile boundary treatment proposal



4 REVIEW OF ACA DRAINAGE STRATEGY THROUGH DETAILED DESIGN

4.1 Surface Water Catchment Methods

4.1.1 As the proposed ACA drainage strategy is developed through Detailed Design, it will be assessed to ensure it is the optimal solution to managing surface water on the site. This will include reviewing the design against opportunities where SuDS can be further utilised, with respect to practicality in each location of the ACA. During Detailed Design, the proposed surface water drainage infrastructure will consider failure scenarios to provide assurance that the proposed infrastructure is adequately sized to manage surface water runoff within the order limits, specifically targeted at what happens if the network becomes blocked.

4.1.2 SuDS and other design inputs

4.1.3 A priority in design was to use SuDS features where possible for the treatment, maintenance, and sustainability benefits. Table 4-1 shows an overview of the available SuDS techniques based on Table 7.1 of CIRIA. As stated in section 3.1, infiltration structures are not considered at this stage in the design. Living roofs will not be suitable on this industrial construction site either, with most buildings on site being prefabricated structures. Water will be reused as much as possible throughout the construction process. Rainwater harvesting tanks will be investigated in the next design phase, as well as the potential of reusing the WMZ water for construction activities where appropriate. This will also decrease the use of potable water on site.

Table 4-1 - Overview of SuDS techniques (based on Table 7.1 CIRIA C753)

SuDS Techniques	Flood Reduction	Pollution Reduction	Landscape & Wildlife Benefit
Re-use on site	✓	✓	✓
Living Roofs	✓	✓	✓
Basins & Ponds – Wetland – Balancing pond – Detention basin – Retention pond	✓	✓	✓
Filter strips and swales	✓	✓	✓
Infiltration – Soakaways – Infiltration trenches – Infiltration basin	✓	✓	✓
Permeable surface and filter drains – Gravelled areas – Paving blocks – Porous paving	✓	✓	
Tanked systems – Oversized pipes and box culverts	✓		

– Storm cells			
Proprietary treatment systems		✓	
– Oil separators			
– Settlement units			

4.1.4 The following SuDS techniques have been proposed in the design of the surface water drainage:

- Swales and a pond (West ACA WMZ) at the topsoil compound.
- A pond (East ACA WMZ) to the east of the site
- Permeable pavements and filter drains at the park and ride, material transfer laydown areas, the caravan pitches and logistics compound.
- Filter drains at the railway track drainage.

4.1.5 The following SuDS techniques will be considered in detailed design phase to further reduce runoff from the development and provide pollution reduction:

- Additional filter strips / filter drains along access roads
- Additional permeable paved areas
- Additional swales

4.2 Surface Water Storage Methods

4.2.1 As stated in Section 3.2.9 the ACA will discharge into the surface water network in the vicinity of the site, namely the Leiston Drain and the Sizewell Marshes. Discharge will be limited to a Q_{BAR}, therefore on-site attenuation will be required. The following attenuation methods will be utilised:

- Two ponds (WMZs) – west of the topsoil compound and east of ACA.
- Permeable pavements (Type 3 subbase minimum porosity of 30%) - Park and ride, caravan pitches, material transfer laydown areas and logistics compound.

4.3 Maintenance

4.3.1 The surface water design aims to minimise maintenance required on site by aiming to use gravity systems rather than pressurised systems as much

as possible. There will still be an element of maintenance required by the Contractor over time.

4.3.2 All surface water components are to be managed within the project by the Contractor. Regular maintenance of the surface water system will be undertaken throughout the lifecycle of the ACA. The Contractor will be required to submit a surface water operations and maintenance management plan that complies with the Code of Construction Practice (CoCP) prior to commencing construction on site.

4.3.3 The planned operational life of the ACA is expected to be approximately 10 years, after which it will be returned to its original greenfield condition. Swales and ponds will be maintained to ensure there is enough vegetation to operate as required for filtering runoff but kept cut to ensure the system is free flowing (in accordance with the CIRIA C753 SuDS Manual). Swales and ponds will be dredged of excess silt build up as required.

4.3.4 All below ground drainage will be designed in accordance with Sewers for Adoption (7th ed.) with all allowances for access and jetting. All filter drains with internal perforated pipes will be provided with rodding eyes on the ends.

4.3.5 A designated maintenance management plan will be in place for the life of the development, this will be used to ensure all aspects of the drainage system are regularly maintained as regularly as deemed necessary for each drainage element. The maintenance management plan will be submitted for approval prior to construction on site.

4.4 Surface Water Treatment

4.4.1 Pollution risk from runoff from the site has been managed through SuDS (assessed using the index approach) where possible. Where SuDS techniques are not currently proposed, other forms of sediment capture are provided. This is through the inclusion of silt traps, catch pits and oil separators within the traditional drainage systems.

4.4.2 **SuDS Index approach to water quality risk management**

4.4.3 As set out in Section 26.7.1 of the CIRIA C753 SuDS Manual, the simple index approach is used to assess water quality risk management and ultimately determine what SuDS measures are required to treat different types of developments. The steps are set out as:

Step 1 – Allocate suitable pollution hazard indices for the proposed land use

Step 2 – Select SuDS with a total pollution mitigation index that equals or exceeds the pollution hazard index

Step 3 – Where the discharge is to protected surface waters or groundwater, consider the need for a more precautionary approach

4.4.4 Given the general use of the ACA site we can allocate pollution indices (Table 26.2 CIRIA SuDS Manual) as one of the two categories, show in Table 4-2. The SuDS Manual does not provide a figure suitable for material stockpiles or loose topsoil, so a "medium" level pollution hazard level is assumed for these areas.

Table 4-2 - Pollution hazard indices for different land use classifications

Land Use	Pollution hazard levels	Total suspended solids (TSS)	Metals	Hydrocarbons
Commercial yard and delivery areas, non-residential car parking with frequent change (e.g. hospitals, retail), all roads except low traffic roads and trunk roads/motorways.	Medium	0.7	0.6	0.7
Sites with heavy pollution (e.g. haulage yards, lorry parks, highly frequented lorry approaches to industrial estates, waste sites), sites where chemicals and fuels (other than domestic fuel oil) are to be delivered, handled, stored, used or manufactured; industrial sites; trunk roads and motorways.	High	0.8	0.8	0.9

4.4.5 Table 4-3 summarises the intended use of each site within the ACA and the assigned pollution hazard level.

Table 4-3 - ACA pollution hazard indices assigned

ACA area	Description of proposed use	Assigned pollution hazard levels
Park and Ride area	Will be used for transporting site staff from the ACA to and from the TCA and MCA. Will constitute parking for site staff with a dedicated bus service	Medium

Logistics compound	Management depot for transport of staff and good around the sites	Medium
Railway	Railhead used for delivery of materials (sands, aggregates and other materials) to the ACA	Medium
Material Transfer Laydown	Laydown area for materials delivered to site from the train.	High
Sand & Aggregate Stockpile	Laydown area for the storage of sand and aggregates delivered to site from the train	High
Topsoil compound	Storage area for stripped topsoil	High
HGV parking	Parking area for contractors' HGVs and other plant	High
Caravan Pitches	For early contractors' accommodation and compounds	Medium

4.4.6 Indicative SuDS pollution mitigation indices are stated in Table 26.3 of the CIRIA SuDS Manual, copied into Table 4-4.

Table 4-4 - Indicative SuDS mitigation indices for discharges to surface waters

	Mitigation indices		
Land Use	**TSS**	**Metals**	**Hydrocarbons**
Filter strip	0.4	0.4	0.5
Filter drain	0.4	0.4	0.4
Swales	0.5	0.6	0.6
Bioretention system	0.8	0.8	0.8
Permeable pavement	0.7	0.6	0.7
Detention basin	0.5	0.5	0.6
Pond	0.7	0.7	0.5
Wetland	0.8	0.8	0.8

4.4.7 Assessing the proposed SuDS features for each of the ACA area we can determine a total pollution mitigation index (Table 26.3 CIRIA SuDS Manual) for each, see Table 4-5 below. This assessment is based on the current proposals and will be updated during the next design phase to reflect additional SuDS elements that are described in section 3.2.9 and

3.2.43. Where additional SuDS features are not considered appropriate at this design stage, proprietary, non-SuDS treatment are proposed in these areas. This is further discussed in section 4.4.8.

Table 4-5 - ACA SuDS mitigation indices for discharges to surface waters

ACA area	Assigned Pollution hazard levels	SuDS features proposed	Total SuDS mitigation Index		
			TSS	Metals	Hydrocarbons
Park and Ride area	Medium	- Permeable pavement - Pond	1.05 (>0.7)	0.95 (>0.6)	0.95 (>0.7)
Logistics compound	Medium	- Permeable Pavement - Pond	1.05 (>0.7)	0.95 (>0.6)	0.95 (>0.7)
Railway	Medium	- Filter drains - Pond	0.75 (>0.7)*	0.75 (>0.6)*	0.65 (<0.7)*
Material Transfer Laydown	High	- Permeable Pavement - Pond	1.05 (>0.8)	0.95 (>0.8)	0.95 (>0.9)
Sand & Aggregate Stockpile	High	- Pond	0.7 (<0.8)**	NA	NA
Topsoil compound	High	- Swale - Pond	0.85 (>0.8)	0.95 (>0.8)	0.85 (<0.9)
HGV parking	High	- Pond	0.7 (<0.8)*	0.7 (<0.8)*	0.5 (<0.9)*
Caravan Pitches	Medium	- Permeable Pavement - Pond	1.05 (>0.7)	0.95 (>0.6)	0.95 (>0.7)

** Drainage treatment to be supplemented by proprietary non-SuDS treatment, to be discussed and agreed with LLFA.*

*** Sand & Aggregate stockpile compound to be reviewed in next design phase to investigate the use of swales or filter drains around the perimeter of this compound.*

4.4.8 Proprietary drainage methods water quality risk management

4.4.9 As presented above, the current approach to manage surface water runoff along the access roads and sand/aggregate stockpile areas, is to use traditional drainage systems. For the railway and HGV areas supplementary treatment through traditional drainage will also be required. All proprietary drainage features will include silt traps and catch pits in all

gullies and manholes, where required separators will be implemented to manage water quality risks from TSS, metals and hydrocarbons.

4.4.10 The HGV parking area is currently proposed to drain through an oil separator to mitigate the risk of hydrocarbon spillage where large vehicles are parked long-term. The design will comply with the initiatives and best practice guidance for pollution prevention for impermeable areas. At this stage, this is deemed to be the most practicable solution. Similarly, the railway drainage will require a by-pass separator before connecting into the sitewide drainage network. The benefit of capturing potential oil spills and treating them in a proprietary device of specific performance specifications is that risk of pollution to downstream sensitive areas is greatly reduced. Proprietary drainage features also provide a level of certainty from past performance that is not immediately offered by vegetative solutions in the early months (sometimes 12 to 18 months) as they establish.

4.4.11 In places, such systems may be used a fail-safe method of treatment to supplement primary treatment observed using SuDS techniques and will be explored in future design stages.

5 CONCLUSION

5.1.1 The ACA drainage strategy has been informed by the DCO Outline Drainage Strategy. This includes not relying on infiltration as a means of surface water disposal, aiming to treat at source, and using suitable treatment methods where reasonable on site.

5.1.2 This note highlights that surface water on site will be collected primarily using SuDS techniques in combination with conventional drainage systems, and be stored, treated and discharged to nearby watercourses. There are several SuDS treatment mechanisms proposed on the site, as well as additional proprietary treatment systems. The surface water design prioritises SuDS features as a means of capture, treatment, and storage, and will be further considered in the next design stage.

5.1.3 The surface water design improves the existing flood risk of the site by allowing systems to capture surface water runoff and attenuate this up to the 1 in 100-year storm event, in accordance with national and local guidance. This is particularly shown in the north-west corner of the site, where swales will be installed to intercept overland flow that previously was directed to Valley Road. This area now captures and retains surface water on site and improves the flood risk to the properties downstream.

5.1.4 The surface water drainage design needs to be progressed further, in conjunction with external stakeholders such as ESC, SCC, Natural England, the EA, and East Suffolk IDB. Throughout the next design phase,

these stakeholders will be engaged with regularly to enable a suitable design that meets the needs of each party.

APPENDIX A:

A.1. Suffolk County Council Briefing Note

08 February 2021

The Sizewell C Project

Suffolk County Council briefing note to SZC Co. regarding its concerns on surface water drainage

Background

1. At the meeting between Suffolk County Council (the Council) and SZC Co. on 1 February 2021, the Council raised that it had concerns regarding the surface water drainage proposals not only for the Land East of Eastland Industrial Estate (LEEIE), but also for most of the other sites. This note set out the concerns and expectations of the Council as the Lead Local Flood Authority (referred to in the document as the LLFA) for these other sites.

Current progress

2. To date, good progress has been made on surface water drainage strategies for both the Two Village Bypass and the Sizewell Link Road. There are regular monthly meetings between the design team and key stakeholders to assess progress on multiple topics, determine potential solutions to any problems that have arisen and a good mechanism of feedback between meetings.
3. Whilst surface water drainage strategies are coming together for both schemes these are at quite a high level with no calculations or technical drawings provided to date.
4. The Land East of Eastlands Industrial Estate (LEEIE) is the only other site to have seen any progress with regards to surface water drainage strategies. The LLFA has significant concerns with the proposed approach to surface water management at this site.
5. No progress on surface water drainage strategies has been communicated to the Council for the other sites (Main Development Site, North & South Park & Rides, Freight Management Facility, Yoxford Roundabout). It is noted that the changes consultation includes a temporary outfall pipe from Main Development Site onto the beach. The need for this is a clear indication that more detailed work has been undertaken to assess surface water drainage strategies for this site that is yet to be communicated to the Council.

Specific concerns

6. Concerns regarding the approach taken for LEEIE have been made previously. This position remains unchanged. Two points worth highlighting from this site are;
    a. SZC Co.'s notion that there is 'insufficient space for SuDS'. This argument is not accepted by the LLFA on any of the proposed development sites. NPS EN-1 is clear that priority should be given to the use of SuDS.
    b. SZC Co.'s notion that the site is only temporary, and on that basis, local and national design guidance as usually applied, and thus a SuDS approach, is not necessarily applicable. This argument is not accepted by the LLFA on any of the proposed development sites. NPS EN-1 does not differentiate between temporary and permanent. The potential surface

water flood risk presented by a development is no less important just because it is temporary. If anything, temporary developments for construction purposes have the potential to further increase surface water flood risk compared to permanent development due to suspended sediments etc associated with construction works.

7. Due to the site's location within a sensitive environment, the Main Development Site (MDS) is of particular concern to the LLFA. This is all the more relevant given the proposed site uses. Very high-level details have been provided as part of the submission documentation, but no further information has been received to date.
8. Proposals for any site need to have a deliverable surface water drainage strategy. This infrastructure is essential to prevent an increase in flood risk and in this instance (MDS) to prevent any potential harm to the surrounding sensitive environment. The space required for SuDS should be assessed, determined, and allocated ***prior*** to space for other site uses being allocated; to ensure there is sufficient space for this essential infrastructure. The LLFA is concerned that this approach may not have been followed by SZC Co.
9. As previously stated, no information has been received for any site, with the exception of LEEIE, Two Village Bypass and Sizewell Link Road.
10. All the points raised in the Issues Tracker, shared in 2019 with the applicant, remain outstanding with little if any progress made on the vast majority of issues raised to date.

What we expect

11. The LLFA expect to see (ideally before, or at worst during, the Examination process) a deliverable surface water drainage strategy for each site of proposed development. Whilst the LLFA understand that at that stage detailed design is not essential, we do expect to see evidence that the strategy can be delivered, i.e. the measures can sufficiently manage surface water runoff generated by the proposed development, within the Order Limits and whilst complying with current local and national design guidance.
12. The LFFA understands that infiltration testing has been undertaken at all sites. However, the LLFA is yet to see the results of this testing in most instances. If a design is solely based on infiltration, SZC Co. needs to evidence that a suitable infiltration rate has been achieved. If a suitable infiltration rate has not been evidenced, an alternative method of surface water disposal (as per surface water disposal hierarchy) should be identified and an appropriate design developed on this basis.
13. If infiltration testing has not been undertaken for a particular site, then it must be demonstrated that;
    a. An infiltration strategy can be achieved with a minimum infiltration rate of 10mm/hr and an appropriate Factor of Safety; and
    b. An alternative method of surface water disposal is achievable (as per surface water drainage hierarchy).

    It must be demonstrated that both options are deliverable within the Order Limits if no infiltration testing is available.

14. Any drainage strategy must consider flood risk as identified in the relevant Flood Risk Assessments.

15. It is important that all design development considers maximum water levels, total basin depths, side slope gradients and the potential for each SuDS component to deliver surface water treatment. All these aspects will affect the sizing of SuDS components which ultimately impact land take and in turn, deliverability (especially on constrained sites).

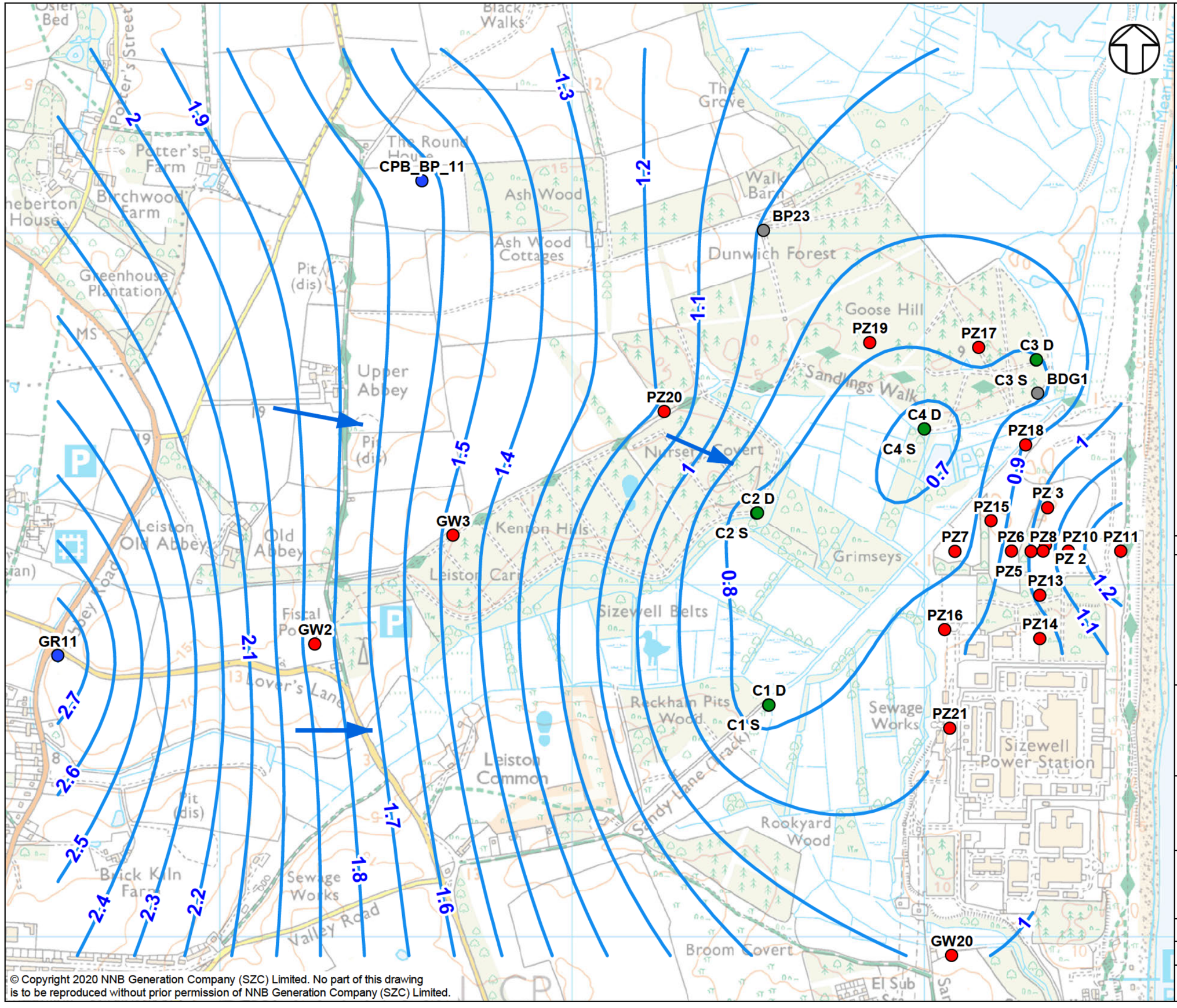
Recommended next Steps

16. The LLFA strongly recommends that the joint working approach with the LLFA taken for the design development of Two Village Bypass and Sizewell Link Road is replicated for each of the other development sites. This transparent and integrated approach has given the LLFA assurance that design is progressing in the right direction, even if more detailed information is not yet available for these two schemes.

17. As design development progresses further, additional details should be provided to the LLFA. This should include but is not limited to, results of ground investigation testing, dimensioned plans of proposed SUDS, design assumptions, results of rainfall simulations for proposed design and details of future maintenance arrangements.

APPENDIX B:

B.1. Groundwater Contour Drawing



NOTES

PEAT CONTOURS ARE CONSTRAINED TO THE EXTENT OF THE PEAT DEPOSITS

KEY

- 2010 BOREHOLES
- 2013 BOREHOLES
- 2014 BOREHOLES
- 2015 BOREHOLES
- GROUNDWATER CRAG CONTOURS (MAOD) - WINTER 2018
- GROUNDWATER FLOW DIRECTION

NOT PROTECTIVELY MARKED

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Project Title:
SIZEWELL C PROJECT
ENVIRONMENTAL STATEMENT
VOLUME 2
CHAPTER 19B1
GROUNDWATER AND SURFACE WATER APPENDIX B1

DRAWING TITLE:
GROUNDWATER CONTOURS IN CRAG AQUIFER DURING WINTER 20 8 (9 2 2018)

DRAWING NO:
FIGURE 19B 1.16

DATE:	DRAWN:	SCALE :
JAN 2020	S.R.H	1:10,103 @A3

SCALE BAR
0 0.1 0.2 0.3 0.4 0.5 KM

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APPENDIX C:

C.1. UK SuDS Greenfield Runoff Rate

HR Wallingford
Working with water

Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool

Calculated by:	Ka Po Leung
Site name:	Sizewell C
Site location:	ACA & WMZ7

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013) , the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be
the basis for setting consents for the drainage of surface water runoff from sites.

Site Details

Latitude:	52.20902° N
Longitude:	1.59176° E
Reference:	3647457570
Date:	Jan 20 2021 18:01

Runoff estimation approach IH124

Site characteristics

Total site area (ha): 50 (30.475)

Methodology

Q_{BAR} estimation method:	Calculate from SPR and SAAR
SPR estimation method:	Calculate from SOIL type

Soil characteristics

	Default	Edited
SOIL type:	3	3
HOST class:	N/A	N/A
SPR/SPRHOST:	0.37	0.37

Hydrological characteristics

	Default	Edited
SAAR (mm):	581	581
Hydrological region:	5	5
Growth curve factor 1 year:	0.87	0.87
Growth curve factor 30 years:	2.45	2.45
Growth curve factor 100 years:	3.56	3.56
Growth curve factor 200 years:	4.21	4.21

Notes

(1) Is Q_{BAR} < 2.0 l/s/ha?

When Q_{BAR} is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

(3) Is SPR/SPRHOST ≤ 0.3?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

Greenfield runoff rates

	Default	Edited	Interpolated
Q_{BAR} (l/s):	115.5	115.5	70.40
1 in 1 year (l/s):	100.49	100.49	61.25
1 in 30 years (l/s):	282.98	282.98	172.48
1 in 100 year (l/s):	411.19	411.19	250.62
1 in 200 years (l/s):	486.26	486.26	

Area Ratio: 0.60950

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement , which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

APPENDIX D:

D.1. EDF – LEEIE EWBD Drainage Design Feedback

PROTECTIVE MARKING

Minutes

SizewellC
Doing the power of good for Britain
EDF CGN

SZC Project - DCO

Meeting: EDF – LEEIE EWBD Basic Drainage Design Feedback

Attendees: [redacted] (EDF) JH, (Atkins) JJ, Atkins) NK, Atkins) ES, Wood) SDL, MM, EST, MW, M, S, GB, C

Meeting Type: MS Teams

Apologies: -

Meeting held on: 17 December 2020 1400-1530h

Meeting Agenda

1. Introductions
2. Review Objective(s) for the Meeting
3. Feedback on the enabling works basic design for drainage at LEEIE / ACA:
   a. WMA
   b. EA
   c. SCC
4. Was meeting objective(s) met?
5. AOB and next meeting date
6. Close

Meeting Minutes – 18/11/2020

Minute Ref	Actions/Comments	Who	By when
1.	**Introductions** Introductions and scene setting by [redacted] Objective 1 - Discussion around the feedback received from the EA, SCC and WMA on the technical information previously provided for the LEEIE (EW0302 ACA Drainage Strategy Technical Note), to understand concerns, points of clarity and area of common ground. Objective 2 – Time allowing, enable discussion on any other aspect of the change consultation pertaining to drainage e.g. the proposed temporary marine outfall.		
2.	YS: Questions on specific discharge rates and also queries as to why the discharge is currently proposed directly into Leiston Drain and not into the attenuation basin that would be preferable. BM: Agree – would be beneficial to go through a basin and provide improvements to the water quality. EDF should also seek to consult with Natural England for specific water quality requirements. ES: Happy to change the local strategy if all stakeholders agree it is the right approach. EST: Current EA position is that this site will not require permitting. ACTION: Potential design change - basin to be used prior to outfall to Leiston Drain. Subject to discussions with NE	JH	

edfenergy.com

25/01/2021 Minutes Page 1 of 1

PROTECTIVE MARKING

SZC Project - DCO

Minute Ref	Actions/Comments	Who	By when
3.	GB: Concern that pumping may be an issue under Land Drainage as downstream landowners do not have to consent to artificial flows. Something that will need to be considered. ES: Current intention is to pump internally and treat prior to discharge, so not going into third party land prior to discharge. GB: Chemistry is important and ecologists will seek reassurance that flows into Leiston Drain are of suitable quality. Also volume, given that Leiston is susceptible to flooding. MW: Modelling has shown that flood water will weir over Lovers Lane before backing up and causing any flooding in Leiston. Catchment 2 is the only area of LEEIE that flows towards Leiston.		
4	ES – Question: which green field runoff rate would be acceptable? MW: two options, preferably Q bar YS: Q bar Also seeking model outputs to understand storage. ES: Happy to provide. Will need to make some adjustments first before providing ACTION: Q bar to be used. ACTION: Model outputs to be provided once updated. And subject to discussions with NE.	 ES ES	
5.	BM: Questions over logistics compound uses. ES: Understand it will be an area that will be used for temporary storage of things - lower risk. BM: If low risk then no interceptor required. If that changes then it may be required. ES: Will seek further information on area usage. MW: Would need to understand how exceedance events are managed for the site as a whole. ACTION: Information on logistics compound to be provided.	 ES	
6.	BM: Concern over underground storage. Currently backing up. Can a pollution control device be used? ES: still under consideration but might be possible to incorporate in detailed design stage. BM: a pollution control device at the WMZ outlet may be a better option, although there are concerns over maintenance. JJ: Acknowledged that careful maintenance will be required but pointed out that operation and maintenance processes are taken very seriously on a nuclear power plant. ES: Likely to be considered further under detailed development, but concern noted.		
7.	BM: Question over the interceptor at HGV parking. ES: proposed oil intercept a at HGV parking MW: has to be a failsafe and not a primary.		
8.	BM: Question over the silt traps for stockpiles and how these will work. ES: Not yet fully considered - further information in detailed design stage		
9.	MW: question to the EA on pollution – would the EA require a permit to discharge into a main river? EST: No, it would not be required		
10.	MW: appears that treatment is not enough into a number of locations based on the index approach in the SuDS manual. MW: wants stockpiles area to be higher risk. Unclear how this is different to HGV parking. ES: vehicles will come in to remove and deposit materials. No long-term parking. Can discuss use further. MW: Not having enough space is not an excuse for not implementing SUDS JJ: SuDS Guidance principally developed for the likes of housing developments, not temporary structures likely lasting less than 10 years before being returned to existing state. Our approach has been to ensure SuDS are uppermost in the design thinking and to protect in particular the SSSI, so a balance across the site needs to be sought. We will look to enhance Amenity and BioDiversity within the LEEIE area as these are two of the four pillars of SuDS. Evidence has shown this helpful to residents mental health well-being		

PROTECTIVE MARKING

PROTECTIVE MARKING

SZC Project - DCO

Minute Ref	Actions/Comments	Who	By when
	MW: Acknowledges the point but the principles of SuDS must be observed. JJ: We will continue to work together to ensure the principles are observed.		
11.	MW: HGV parking – why different to the freight management facility which proposes permeable surfacing? ES: Little knowledge in this area. We'll need to look into before responding. **ACTION**: Review freight management facility proposals.	ES	
12.	MW: Question over storage under the caravan pitches. Over 12,000 cubic meters proposed where a two metre difference in ground level is shown on LIDAR. Does it back up and only use part of the storage or will it flood? ES: don't recall a two metre level difference. Storage would not necessarily follow the ground profile. It is likely that a changed approach at the outfall arrangement discussed in 2 above will reduce the need for this type of storage we will respond accordingly MW: If ground profile changes, drainage routes will also change, i.e. are catchments redefined.	ES	
13.	MW: For the stockpiles, agree with the hay bale approach to intercept runoff, but concern over the swale. Need more information on this. Suggested it won't work under certain circumstances. Where does it outfall to? ES: Need to come back after reviewing. **ACTION**: Review swale and provide further information.	ES	
14.	MW: Infiltration rates – needs to assume there is no infiltration. ES: Have assumed and there is no infiltration, although there will be some. MW: Would like to see output of GI / infiltration testing.		
15.	MW: Pond will not meet quality requirements for a pond so a basin will be better. ES: Comment noted MW: Note that there could be a legacy benefit.		
16.	SDL: detailed design will provide a more appropriate level of detail for permitting, if required.		
17.	MW: changes consultation wording suggests a temporary outfall up until the 1 in 30 year event. A 1 in 30 should be held above ground. Needs to understand the proposals. ES: We will come back with something more detailed. YS: Concerned if discharge into sea more frequently than 1 in 30. Would like to know criteria. JH: The intention of the 1 in 30 year value in the consultation was to provide an example of the likely exceedance event, rather than be definitive, since more work is required to match criteria to the construction phasing and activities. Agree that as the design evolves a more detailed description of deployment will be required, set in the context of the environmental sensitivities, i.e. seeking to provide outcome- rather than output-led approach. JJ: We are aware of sensitivities of the area and the need to keep water in the area. Intended to be used as a fail-safe as it is known that the drains in the area back up in winter months, and discharging may result in local flooding. GB: Water level management required. Standing water can be beneficial to the local ecology particularly in drought. JJ: Acknowledged, the use of source control elements throughout the site is predicated against the backdrop of maintaining ground water levels, the ecology and environment being uppermost in mind. MW: 1 in 30 to be contained **ACTION**: Provide further detail on temporary outfall proposals.	ES	
18.	Were objective(s) met? EST: a very productive meeting to be recorded as such on NSIP form. **ACTION**: JH to provide NSIP draft to EST	JH	
19.	**AOB and next meeting date** MW: Would like meetings for each AD site going forward		

PROTECTIVE MARKING

SZC Project - DCO

Minute Ref	Actions/Comments	Who	By when
	YS: Agree with MW JM: would like Natural England to be invited to future meetings No next meeting date set. **ACTION**: Invite NE to next meeting	JH	
20.	**Close**		

APPENDIX E:

E.1. Infiltration Rate Testing Results

TP-WMZ-24 & TP-WMZ-25 from Structural Soils Limited, July 2017 - 2016 Onshore Ground Investigation Campaign. Factual Report on Ground Investigation (SZC-SZC030-XX-000-REP-100000)

ACA_2020-1 & ACA_2020-2 from Fugro - Sizewell C Infiltration Testing Report on Ground Investigation without Geotechnical Evaluation (G200003U_GIR Rev 02)

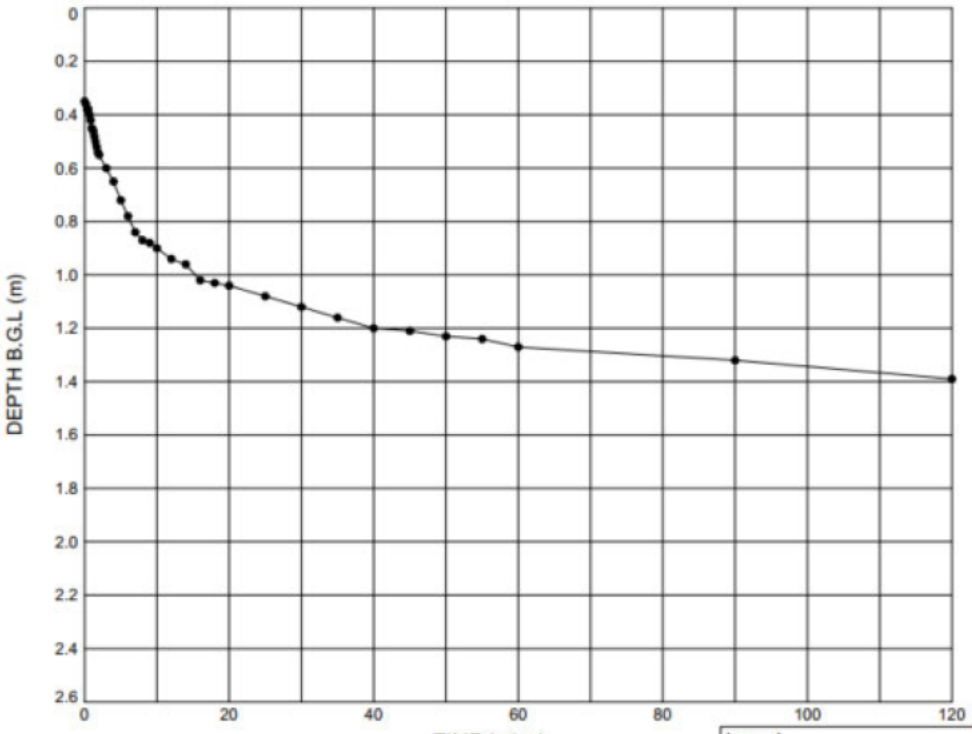
FULL SCALE SOAKAWAY TEST

Non-standard test

Soakaway Test - Position ID : **TP-WMZ-24**

Ground Level (m): **16.92** National Grid Co-ordinates: **E:645407.4 N:262892.8**

PLOT OF DEPTH OF WATER BELOW GROUND LEVEL AGAINST TIME



Test 1

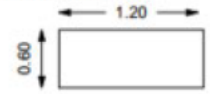
Pit start depth:	=	**3.00**	m
Pit final depth:	=	**3.00**	m
Effective depth, De	=	**2.65**	m
Effective storage volume, V_{p75-25}	=	**0.9540**	m³
Surface area, a_{p50}	=	**5.4900**	m²
Time, t_{p75-25}	=	**30619**	secs
Infiltration rate, f	=	**5.68×10^{-6}**	m/s

Please note test data was extrapolated to obtain tp75-tp25.

Legend

● Test 1 (14.3.17)

Plan (Not to scale)



No Bearing Taken

STRUCTURAL SOILS
The Potteries
Pottery Street
Castleford
W. Yorkshire WF10 1NJ

Compiled By	Date	Checked By	Date
[redacted]	14/6/17	[redacted]	14/6/17

Contract: **Sizewell Section 53 Land**

Contract Ref: **764156**

GINT_LIBRARY_V8_06.GLB | Version: v8_06_017 PrjVersion: v8_04 - Core+Logs - 002 | Graph I - TP SOAKAWAY - 2 - FINAL REPORT - AMP | 764156 - SIZEWELL SECTION 53 LAND.GPJ - v8_06 | 14/6/17 - 10:04 | AC7 |

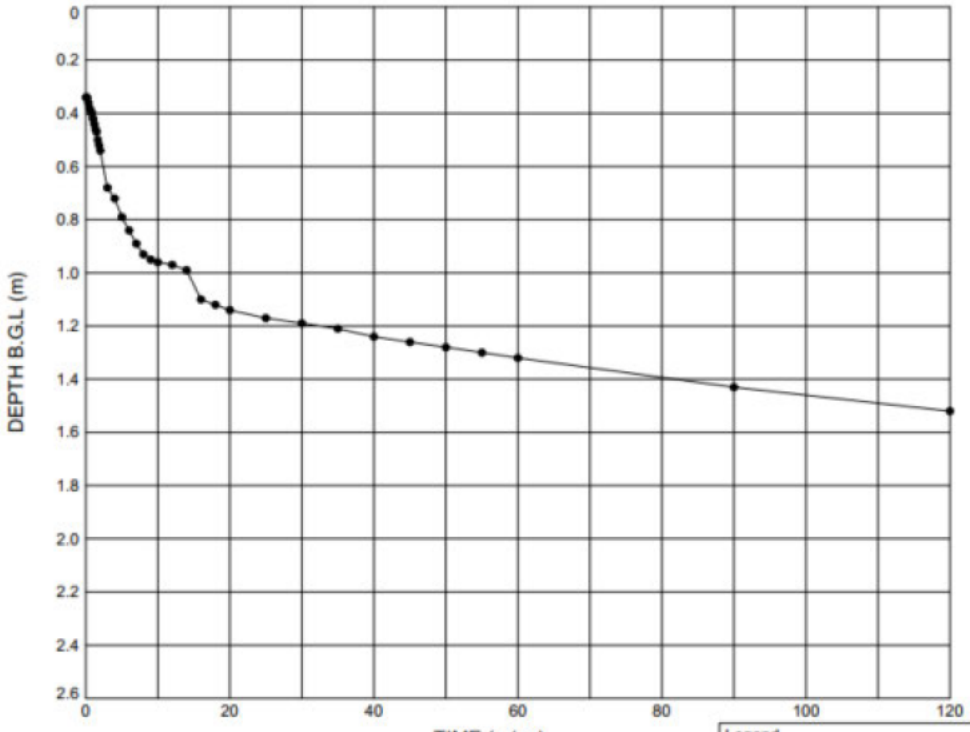
FULL SCALE SOAKAWAY TEST

Non-standard test

Soakaway Test - Position ID : **TP-WMZ-25**

Ground Level (m): **16.44** National Grid Co-ordinates: **E:645595.9 N:262725.8**

PLOT OF DEPTH OF WATER BELOW GROUND LEVEL AGAINST TIME



Test 1

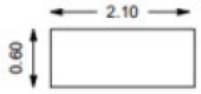
Pit start depth:	=	**3.00**	m
Pit final depth:	=	**3.00**	m
Effective depth, De	=	**2.66**	m
Effective storage volume, V_{p75-25}	=	**1.6758**	m^3
Surface area, a_{p50}	=	**8.4420**	m^2
Time, t_{p75-25}	=	**22861**	secs
Infiltration rate, f	=	**$8.68x10^{-6}$**	m/s

Please note test data was extrapolated to obtain tp75-tp25.

Legend

● Test 1 (14.3.17)

Plan (Not to scale)



No Bearing Taken

STRUCTURAL SOILS
The Potteries
Pottery Street
Castleford
W. Yorkshire WF10 1NJ

Compiled By	Date	Checked By	Date
[redacted]	14/6/17	[redacted]	14/6/17

Contract: **Sizewell Section 53 Land**

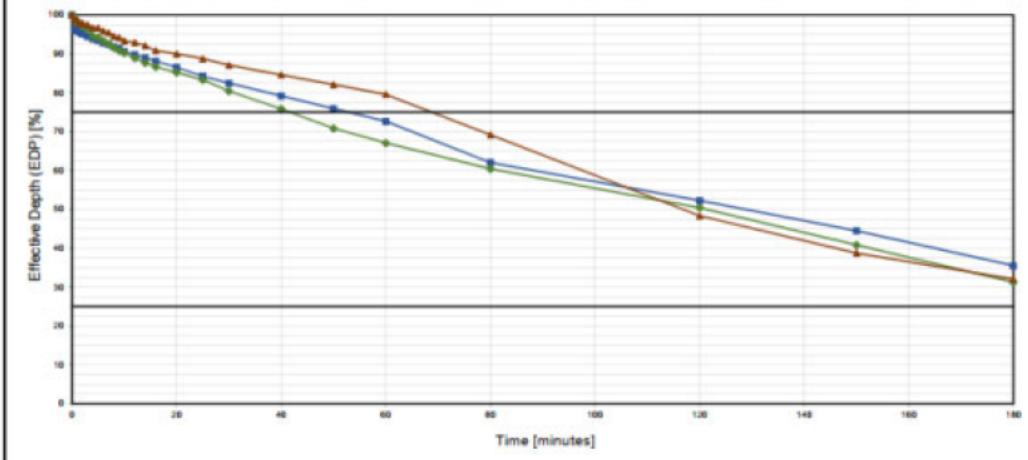
Contract Ref: **764156**

GINT_LIBRARY_V8_06.GLB Lib Version: v8_06_017 Prj Version: v8_06 - Core+Logs - 002 | Graph 1 - TP SOAKAWAY - 2 - FINAL REPORT - AMP | 764156 - SIZEWELL SECTION 53 LAND.GPJ - v8_06 | 14/6/17 - 10:05 | AC7 |

NNB GENERATION COMPANY (SZC)
SIZEWELL INFILTRATION TESTING

SOAKAWAY TEST RECORD

Date	06/03/2020	Operator	JJL	Hole Depth	3.50 m	Hole No.	ACA_2020-1



Test 1			Test 2			Test 3		
Start Time =	11:25		Start Time =	14:32		Start Time =	08:35	
Test Top =	0.45	m BGL	Test Top =	0.50	m BGL	Test Top =	0.50	m BGL
Test Base =	2.90	m BGL	Test Base =	2.90	m BGL	Test Base =	2.90	m BGL
75% EDP =	1.06	m BGL	75% EDP =	1.10	m BGL	75% EDP =	1.10	m BGL
50% EDP =	1.68	m BGL	50% EDP =	1.70	m BGL	50% EDP =	1.70	m BGL

Elapsed Time [hr:min:sec]	Water [m BDL]	Water [m BGL]	EDP [%]	Elapsed Time [hr:min:sec]	Water [m BDL]	Water [m BGL]	EDP [%]	Elapsed Time [hr:min:sec]	Water [m BDL]	Water [m BGL]	EDP [%]
00:00:00		0.45	100	00:00:00		0.50	100	00:00:00		0.50	100
00:00:30		0.54	96	00:00:30		0.54	98	00:00:30		0.53	99
00:01:00		0.55	96	00:01:00		0.54	98	00:01:00		0.53	99
00:01:30		0.56	96	00:01:30		0.56	98	00:01:30		0.55	98
00:02:00		0.57	95	00:02:00		0.57	97	00:02:00		0.55	98
00:03:00		0.59	94	00:03:00		0.59	96	00:03:00		0.56	98
00:04:00		0.60	94	00:04:00		0.63	95	00:04:00		0.58	97
00:05:00		0.61	93	00:05:00		0.64	94	00:05:00		0.58	97
00:06:00		0.63	93	00:06:00		0.66	93	00:06:00		0.60	96
00:07:00		0.64	92	00:07:00		0.68	93	00:07:00		0.61	95
00:08:00		0.65	92	00:08:00		0.70	92	00:08:00		0.63	95
00:09:00		0.66	91	00:09:00		0.72	91	00:09:00		0.64	94
00:10:00		0.68	91	00:10:00		0.74	90	00:10:00		0.66	93
00:12:00		0.70	90	00:12:00		0.77	89	00:12:00		0.67	93
00:14:00		0.72	89	00:14:00		0.80	88	00:14:00		0.69	92
00:16:00		0.74	88	00:16:00		0.82	87	00:16:00		0.72	91
00:20:00		0.78	87	00:20:00		0.86	85	00:20:00		0.74	90
00:25:00		0.84	84	00:25:00		0.90	83	00:25:00		0.77	89
00:30:00		0.88	82	00:30:00		0.97	80	00:30:00		0.81	87
00:40:00		0.96	79	00:40:00		1.08	76	00:40:00		0.87	85
00:50:00		1.04	76	00:50:00		1.20	71	00:50:00		0.93	82
01:00:00		1.12	73	01:00:00		1.29	67	01:00:00		0.99	80
01:20:00		1.38	62	01:20:00		1.45	60	01:20:00		1.24	69
02:00:00		1.62	52	02:00:00		1.69	50	02:00:00		1.74	48
02:30:00		1.81	44	02:30:00		1.92	41	02:30:00		1.97	39
03:00:00		2.03	36	03:00:00		2.15	31	03:00:00		2.13	32

Datum (-ve denotes AGL) = 0.00 m BGL
Ground Level taken as Datum.

Input by KB 09/03/2020 Checked by JJL 12/03/2020 Approved by NHA 05/06/2020

Contract No. G200003U Page 1 of 2

NNB GENERATION COMPANY (SZC)
SIZEWELL INFILTRATION TESTING

SOAKAWAY TEST RECORD							
Date	06/03/2020	Operator	JJL	Hole Depth	3.50 m	Hole No.	ACA_2020-1

Test Details

Datum (-ve denotes AGL) =	0.00 m BGL	Well Screen	
		External Diameter =	0.225 m
Hole Diameter =	0.30 m	Internal Diameter =	0.205 m
Hole Depth =	3.50 m BGL	Filter Material	
		Assumed Solid Fraction =	57.62 %
		Assumed Porosity =	42.38 %

Weather: Fine.

Geology: SAND and GRAVEL.

Remarks

Test 1 and Test 2 undertaken on 06/03/2020; Test 3 undertaken on 07/03/2020.
Test carried out inside 225mm well screen in gravel filled borehole. Volume of gravel fraction assumed to be 57.62% of the total volume of gravel filled space. Gravel filter commenced 0.50m BGL.
Standing water was noted at 2.90m BGL before test started; this standing water level is taken as the test base depth.
Water level did not reach 25% EPD for all Test 1, Test 2 and Test 3; infiltration rate based on data between 75% EPD and 50% EPD.

Calculation

	Test 1 ■		Test 2 ◆		Test 3 ▲	
Start Time =	11:25		14:32		08:35	
Test Top =	0.45	m BGL	0.50	m BGL	0.50	m BGL
Test Base =	2.90	m BGL	2.90	m BGL	2.90	m BGL
EDP =	2.45	m	2.40	m	2.40	m
75% EDP =	1.06	m BGL	1.10	m BGL	1.10	m BGL
50% EDP =	1.68	m BGL	1.70	m BGL	1.70	m BGL
V =	0.17	m^3	0.17	m^3	0.17	m^3
Vg =	0.04	m^3	0.04	m^3	0.04	m^3
Vp =	0.13	m^3	0.13	m^3	0.13	m^3
Vp75-50 =	0.03	m^3	0.03	m^3	0.03	m^3
ap =	2.08	m^2	2.05	m^2	2.05	m^2
Tp75 =	3142	s	2520	s	4124	s
Tp50 =	7800	s	7200	s	6971	s
Infiltration Rate, f =	3.34E-06	m/s	3.31E-06	m/s	5.43E-06	m/s

Notes

m AGL/BGL = metres above / below ground level;
m BDL = metres below datum level.

Effective depth of soakaway (EDP) is calculated from the initial water level to the base of hole.

V is the effective storage volume of water in the hole (ESV) when gravel fill not used; Vg is the effective volume taken up by the gravel;
Vp is the ESV, less the volume of the gravel fraction.
Vp75-50 is the ESV between 75% and 50% effective depth, less the volume of the gravel fraction.

ap is the average internal surface area of the hole between 75% and 50% effective depth including base area.

Tp75 is time at 75% EDP; Tp50 is time at 50% EDP.
Tp75-50 is the assessed time for water level to fall from 75% to 50% EDP.

$$Soil\ Infiltration\ rate, f = \frac{Vp_{75-50}}{ap \times Tp_{75-50}}$$

Input by KB 09/03/2020 Checked by JJL 12/03/2020 Approved by NHA 05/06/2020

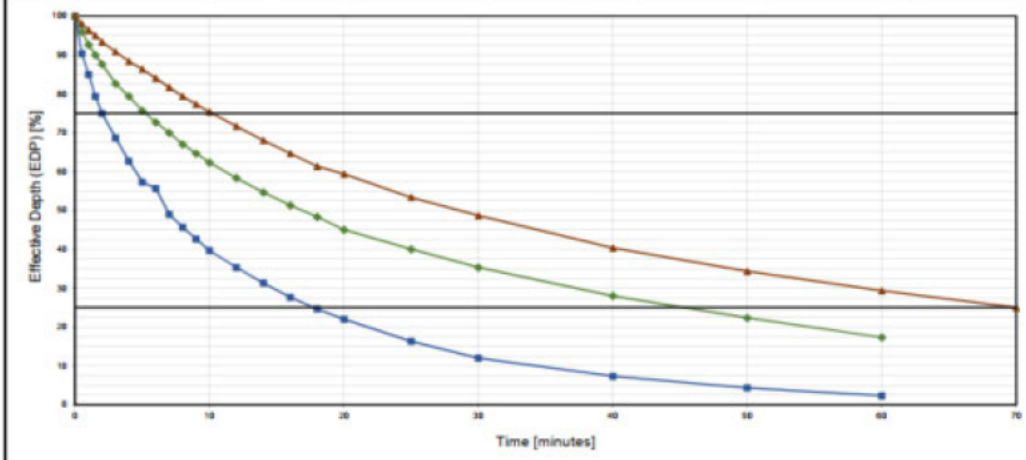
Contract No. G200003U

Page 2 of 2

NNB GENERATION COMPANY (SZC)
SIZEWELL INFILTRATION TESTING

SOAKAWAY TEST RECORD

Date	07/03/2020	Operator	JJL	Hole Depth	3.50 m	Hole No.	ACA_2020-2



	Test 1			Test 2			Test 3		
Start Time =	15:10			09:02			10:05		
Test Top =	0.50	m BGL		0.50	m BGL		0.50	m BGL	
Test Base =	3.50	m BGL		3.50	m BGL		3.50	m BGL	
75% EDP =	1.25	m BGL		1.25	m BGL		1.25	m BGL	
25% EDP =	2.75	m BGL		2.75	m BGL		2.75	m BGL	

Elapsed Time [hr:min:sec]	Water [m BDL]	Water [m BGL]	EDP [%]	Elapsed Time [hr:min:sec]	Water [m BDL]	Water [m BGL]	EDP [%]	Elapsed Time [hr:min:sec]	Water [m BDL]	Water [m BGL]	EDP [%]
00:00:00		0.50	100	00:00:00		0.50	100	00:00:00		0.50	100
00:00:30		0.79	90	00:00:30		0.62	96	00:00:30		0.56	98
00:01:00		0.95	85	00:01:00		0.72	93	00:01:00		0.61	96
00:01:30		1.12	79	00:01:30		0.80	90	00:01:30		0.65	95
00:02:00		1.25	75	00:02:00		0.87	88	00:02:00		0.70	93
00:03:00		1.44	69	00:03:00		1.02	83	00:03:00		0.78	91
00:04:00		1.62	63	00:04:00		1.12	79	00:04:00		0.85	88
00:05:00		1.78	57	00:05:00		1.23	76	00:05:00		0.91	86
00:06:00		1.83	56	00:06:00		1.32	73	00:06:00		0.98	84
00:07:00		2.03	49	00:07:00		1.40	70	00:07:00		1.05	82
00:08:00		2.13	46	00:08:00		1.49	67	00:08:00		1.12	79
00:09:00		2.22	43	00:09:00		1.56	65	00:09:00		1.18	77
00:10:00		2.31	40	00:10:00		1.63	62	00:10:00		1.24	75
00:12:00		2.44	35	00:12:00		1.75	58	00:12:00		1.35	72
00:14:00		2.56	31	00:14:00		1.86	55	00:14:00		1.46	68
00:16:00		2.67	28	00:16:00		1.96	51	00:16:00		1.56	65
00:18:00		2.76	25	00:18:00		2.05	48	00:18:00		1.66	61
00:20:00		2.84	22	00:20:00		2.15	45	00:20:00		1.72	59
00:25:00		3.01	16	00:25:00		2.30	40	00:25:00		1.90	53
00:30:00		3.14	12	00:30:00		2.44	35	00:30:00		2.04	49
00:40:00		3.28	7	00:40:00		2.66	28	00:40:00		2.29	40
00:50:00		3.37	4	00:50:00		2.83	22	00:50:00		2.47	34
01:00:00		3.43	2	01:00:00		2.98	17	01:00:00		2.62	29
								01:10:00		2.75	25

Datum (-ve denotes AGL) = 0.00 m BGL
Ground Level taken as Datum.

Input by KB 09/03/2020 Checked by JJL 12/03/2020 Approved by NHA 05/06/2020

Contract No. G200003U

Page 1 of 2

NNB GENERATION COMPANY (SZC)
SIZEWELL INFILTRATION TESTING

SOAKAWAY TEST RECORD

Date	07/03/2020	Operator	JJL	Hole Depth	3.50 m	Hole No.	ACA_2020-2

Test Details

Datum (-ve denotes AGL) =	0.00 m BGL	Well Screen	
		External Diameter =	0.225 m
Hole Diameter =	0.30 m	Internal Diameter =	0.205 m
Hole Depth =	3.50 m BGL	Filter Material	
		Assumed Solid Fraction =	57.62 %
		Assumed Porosity =	42.38 %

Weather: Cloudy.

Geology: Orangish brown SAND.

Remarks:
Test 1 undertaken on 07/03/2020; Test 2 and Test 3 undertaken on 08/03/2020.
Test carried out inside 225mm well screen in gravel filled borehole. Volume of gravel fraction assumed to be 57.62% of the total volume of gravel filled space. Gravel filter commences at 0.50m BGL.

Calculation

Test 1 ■			Test 2 ◆			Test 3 ▲		
Start Time =	15:10		Start Time =	09:02		Start Time =	10:05	
Test Top =	0.50	m BGL	Test Top =	0.50	m BGL	Test Top =	0.50	m BGL
Test Base =	3.50	m BGL	Test Base =	3.50	m BGL	Test Base =	3.50	m BGL
EDP =	3.00	m	EDP =	3.00	m	EDP =	3.00	m
75% EDP =	1.25	m BGL	75% EDP =	1.25	m BGL	75% EDP =	1.25	m BGL
25% EDP =	2.75	m BGL	25% EDP =	2.75	m BGL	25% EDP =	2.75	m BGL
V =	0.21	m^3	V =	0.21	m^3	V =	0.21	m^3
Vg =	0.05	m^3	Vg =	0.05	m^3	Vg =	0.05	m^3
Vp =	0.16	m^3	Vp =	0.16	m^3	Vp =	0.16	m^3
Vp75-25 =	0.08	m^3	Vp75-25 =	0.08	m^3	Vp75-25 =	0.08	m^3
ap50 =	1.48	m^2	ap50 =	1.48	m^2	ap50 =	1.48	m^2
Tp75 =	120	s	Tp75 =	321	s	Tp75 =	600	s
Tp25 =	1071	s	Tp25 =	2767	s	Tp25 =	4200	s
Infiltration Rate, f =	5.61E-05	m/s	Infiltration Rate, f =	2.18E-05	m/s	Infiltration Rate, f =	1.48E-05	m/s

Notes

m AGL/BGL = metres above / below ground level
m BDL = metres below datum level

Effective depth of soakaway (EDP) is calculated from the initial water level to the base of hole.

V is the effective storage volume of water in the hole (ESV) when gravel fill not used; Vg is the effective volume taken up by the gravel solid;
Vp is the ESV, less the volume of the gravel fraction.
Vp75-25 is the ESV between 75% and 25% effective depth, less the volume of the gravel fraction.

ap50 is the internal surface area of the hole up to 50% effective depth including base area.

Tp75 is time at 75% EDP; Tp25 is time at 25% EDP.
Tp75-25 is the assessed time for water level to fall from 75% to 25% EDP.

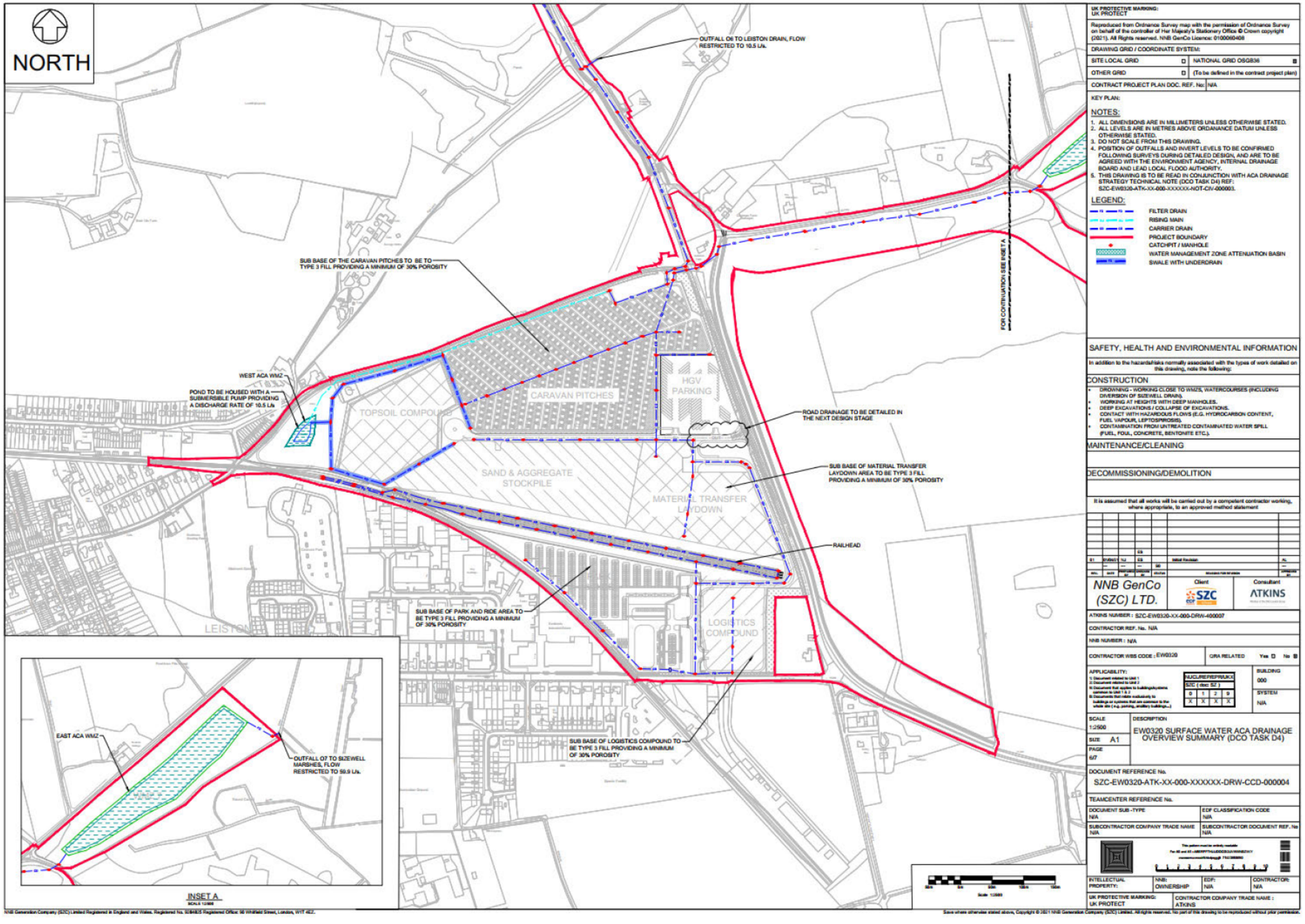
$$Soil\ Infiltration\ rate, f = \frac{Vp_{75-25}}{ap50 \times Tp_{75-25}}$$

Input by KB 09/03/2020 Checked by JJL 12/03/2020 Approved by NHA 05/06/2020

Contract No. G200003U Page 2 of 2

APPENDIX F:

F.1. ACA Surface Water Drainage Layout


NORTH
OUTFALL 06 TO LEISTON DRAIN, FLOW RESTRICTED TO 10.5 L/s.
SUB BASE OF THE CARAVAN PITCHES TO BE TO TYPE 3 FILL PROVIDING A MINIMUM OF 30% POROSITY
WEST ACA WMZ
POND TO BE HOUSED WITH A SUBMERSIBLE PUMP PROVIDING A DISCHARGE RATE OF 10.5 L/s
CARAVAN PITCHES
HGV PARKING
TOPSOIL COMPOUND
ROAD DRAINAGE TO BE DETAILED IN THE NEXT DESIGN STAGE
SAND & AGGREGATE STOCKPILE
MATERIAL TRANSFER LAYDOWN
SUB BASE OF MATERIAL TRANSFER LAYDOWN AREA TO BE TYPE 3 FILL PROVIDING A MINIMUM OF 30% POROSITY
RAILHEAD
SUB BASE OF PARK AND RIDE AREA TO BE TYPE 3 FILL PROVIDING A MINIMUM OF 30% POROSITY
LOGISTICS COMPOUND
SUB BASE OF LOGISTICS COMPOUND TO BE TYPE 3 FILL PROVIDING A MINIMUM OF 30% POROSITY
FOR CONTINUATION SEE INSET A
EAST ACA WMZ
OUTFALL 07 TO SIZEWELL MARSHES, FLOW RESTRICTED TO 59.9 L/s.
INSET A
UK PROTECTIVE MARKING: UK PROTECT
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DRAWING GRID / COORDINATE SYSTEM:
SITE LOCAL GRID
NATIONAL GRID OSGB36
OTHER GRID
(To be defined in the contract project plan)
CONTRACT PROJECT PLAN DOC. REF. No: N/A
KEY PLAN:
NOTES:
1. ALL DIMENSIONS ARE IN MILLIMETERS UNLESS OTHERWISE STATED.
2. ALL LEVELS AIRE IN METRES ABOVE ORDANANCE DATUM UNLESS OTHERWISE STATED.
3. DO NOT SCALE FROM THIS DRAWING.
4. POSITION OF OUTFALLS AND INVERT LEVELS TO BE CONFIRMED FOLLOWING SURVEYS DURING DETAILED DESIGN, AND ARE TO BE AGREED WITH THE ENVIRONMENT AGENCY, INTERNAL DRAINAGE BOARD AND LEAD LOCAL FLOOD AUTHORITY.
5. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ACA DRAINAGE STRATEGY TECHNICAL NOTE (DCO TASK D4) REF: SZC-EW0320-ATK-XX-000-XXXXXX-NOT-CIV-000003.
LEGEND:
FILTER DRAIN
RISING MAIN
CARRIER DRAIN
PROJECT BOUNDARY
CATCHPIT / MANHOLE
WATER MANAGEMENT ZONE ATTENUATION BASIN
SWALE WITH UNDERDRAIN
SAFETY, HEALTH AND ENVIRONMENTAL INFORMATION
In addition to the hazards/risks normally associated with the types of work detailed on this drawing, note the following:
CONSTRUCTION
DROWNING - WORKING CLOSE TO WMZS, WATERCOURSES (INCLUDING DIVERSION OF SIZEWELL DRAIN).
WORKING AT HEIGHTS WITH DEEP MANHOLES.
DEEP EXCAVATIONS / COLLAPSE OF EXCAVATIONS.
CONTACT WITH HAZARDOUS FLOWS (E.G. HYDROCARBON CONTENT, FUEL VAPOUR, LEPTOSPIROSIS).
CONTAMINATION FROM UNTREATED CONTAMINATED WATER SPILL (FUEL, FOUL, CONCRETE, BENTONITE ETC.).
MAINTENANCE/CLEANING
DECOMMISSIONING/DEMOLITION
It is assumed that all works will be carried out by a competent contractor working, where appropriate, to an approved method statement
NNB GenCo (SZC) LTD.
Client
Consultant
ATKINS
ATKINS NUMBER : SZC-EW0320-XX-000-DRW-400007
CONTRACTOR REF. No. N/A
NNB NUMBER : N/A
CONTRACTOR WBS CODE : EW0320
CDM RELATED Yes No
APPLICABILITY:
BUILDING 000
SYSTEM N/A
SCALE 1:2500
SIZE A1
PAGE 6/7
DESCRIPTION
EW0320 SURFACE WATER ACA DRAINAGE OVERVIEW SUMMARY (DCO TASK D4)
DOCUMENT REFERENCE No.
SZC-EW0320-ATK-XX-000-XXXXXX-DRW-CCD-000004
TEAMCENTER REFERENCE No.
DOCUMENT SUB -TYPE N/A
EDF CLASSIFICATION CODE N/A
SUBCONTRACTOR COMPANY TRADE NAME N/A
SUBCONTRACTOR DOCUMENT REF. No N/A
INTELLECTUAL PROPERTY:
NNB: OWNERSHIP
EDF: N/A
CONTRACTOR: N/A
UK PROTECTIVE MARKING: UK PROTECT
CONTRACTOR COMPANY TRADE NAME : ATKINS

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APPENDIX C

SIZEWELL DRAIN WATER MANAGEMENT CONTROL STRUCTURE (DCO TASK D5)

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1 INTRODUCTION

1.1.1 EDF Nuclear New Build Generation Company (SZC) Ltd. (NNB GenCo) are proposing to build Sizewell C (SZC) adjacent to the existing Sizewell A (SZA) and Sizewell B (SZB) Nuclear Power Station Sites, located on the east coast of Suffolk, bound by the North Sea to the east. The area belongs to the Suffolk Heritage Coast within the Suffolk Coast and Heaths Area of Outstanding Natural Beauty (AONB) and a small area of Sizewell Marshes Site of Special Scientific Interest (SSSI), the majority of which lies to the west of the site, is within the site boundary.

1.1.2 The Main Construction Area (MCA) is located in the east of the development site and comprises the proposed main power station platform which will house the UK EPR™ reactor units and associated facilities and building. The SZC development will require some limited land-take from the north-eastern part of Sizewell Marshes SSSI, in an area known as Goodram's Fen. This will include realignment of the watercourse commonly known as the Sizewell Drain around the western edge of the development to tie in with Leiston Drain which would be retained within a SSSI corridor. The realignment of Sizewell Drain is illustrated in Figure 19C.1 at Volume 2, Chapter 19, Appendix 19C of the Environment Statement [APP-309]. Sizewell Drain is managed by the East Suffolk Internal Drainage Board (IDB). The Leiston Drain is classified as a Main River and is managed by the Environment Agency.

1.1.3 The purpose of this document is to provide East Suffolk Internal Drainage Board and other stakeholders with outline design options for the proposed control structure on the realigned Sizewell Drain, in order to demonstrate the ability to enable fine tuning of water levels in the Sizewell Marshes SSSI, as described in Chapter 19, Volume 2 of the Environmental Statement. The choice and further design of the control structure would be undertaken in detailed design, in consultation with ESIDB, and subject to the required Land Drainage Consent.

2 WATER MANAGEMENT STRUCTURE

2.1 Purpose

2.1.1 The hydrological continuity between the floodplain and the Leiston Drain upstream is maintained by reintroducing a connection between Leiston Drain and the realigned Sizewell Drain. A water management structure will provide a means of implementing an adaptive water management regime across the eastern areas of Sizewell Marshes. This will encourage a movement of water through the marshes to maintain a healthy ecological

habitat. The structure is proposed to be set back from the confluence of Sizewell Drain and Leiston Drain by a short distance (ideally by 5 m to 10 m up Sizewell Drain) to create a backwater on the Sizewell Drain. The Sizewell Marshes can thus be kept at a higher water level than Leiston Drain and can be inundated seasonally allowing the marshes to dry out slowly as water levels in the Leiston Drain recede. An adjustable water management structure could provide further benefits to Sizewell Marshes, allowing the retained level to be dropped after a flood event to help drain the marshes more efficiently than would be possible from a fixed structure.

2.2 Structural Options

2.2.1 There are a number of water management structures that could be adopted for the connection between Leiston Drain and Sizewell Drain. Benefits and disadvantages of the various options are shown in Table 1.

Table 1 - Water Management Structure Options - Benefits and Disadvantages

Option	Photo	Description	Benefits	Disadvantages
Penstock Weir/ Sluice Gate		A penstock weir is in essence a sliding door which can be raised and lowered by using a turning wheel. A penstock door raises to open and allow the passage of water and lowers to isolate the flow. Traditionally made of wood, more recent types are constructed from stainless steel or High-Density Polyethylene (HDPE).	• Can allow for a continuous flow of water out of the Sizewell Marshes penned area and/or into the Leiston Drain. • Allows for an almost complete drawdown of water in Sizewell Marshes. • Large discharge capacity ensure excess water can be quickly discharged through the structure when penstock is raised.	• A desired water level cannot be set in the same way as alterative options because it is an undershot structure. • Once the gate is raised, regular checking is required to ascertain when required levels in the penned area have been reached. • Foundation for structure may require piles or ground improvement for stability due to the weak underlying peat and alluvium.
Overflow Weir		Combination of weir overflow plate, piped culvert, and earth bund. Penstock valve can be adopted as the weir overflow plate. The required water level is set by the height of weir overflow plate, which can be adjusted manually using a turning wheel.	• Allows fine control of water levels to be set. • Suitable for penning large volumes of water in Sizewell Marshes, when required. • Large discharge capacity ensure excess water can be quickly discharged through the structure when barrier is lowered.	• Not suitable for allowing complete drainage of the penned area as the weir plate (even when lowered to full intake) will be sitting proud of the ditch base by the height of the weir plate itself. • Would require the construction of a shallow slope and low permeability earth bund across the realigned Sizewell Drain. Foundation for structure may require piles or ground improvement for stability due to the weak underlying peat and alluvium.

Option	Photo	Description	Benefits	Disadvantages
Tilting Weir		Structure comprises of a weir plate fixed to two side cheeks that rotate through a 90-degree axis located into the base frame of the weir. The two side checks are driven by two gearboxes mounted into the cross beam. Manufactured in HDPE or stainless steel.	• Very fine control of water with variation of weir level. • Suitable for large river systems. • Large discharge capacity ensure excess water can be quickly discharged through the structure when tilted.	• Structure may require piles or ground improvement for foundation stability due to the weak underlying peat and alluvium.
Drop Board Sluice		Structure comprises metal sluice frame and softwood drop boards. Sluice boards are inserted to the required water height. Water may be either held back behind structure, or sluice boards used as a top height, above which water may 'overtop' in a controlled fashion.	• Can add or remove boards to adjust the penned water table in Sizewell Marshes. • Large discharge capacity ensure excess water can be quickly discharged through the structure when boards are lowered.	• Very fine control of water levels is not usually possible (i.e. in increments as per the height of each board). • Structure may require piles or ground improvement for foundation stability due to the weak underlying peat and alluvium.
Overflow Sluice		Structure comprises of 3no. prefabricated steel sections and a sluice barrier. The side plates of the structure are keyed back into each bank by approx. 2m and the ditch bottom by approx. 1m. Excess water above the required height set by the top of the barrier is able to overtop the sluice barrier and discharge from site.	• Robust, cost effective and long-lasting structure. • Allows fine control of water levels to be set. Required water level height can be set, and excess water allowed to overtop structure. • Large discharge capacity ensure excess water can be quickly discharged through the structure when barrier is lowered.	• Requires ratchet system to raise/lower barrier due to weight. • Bolts need to be adjusted to release and fix plates, which may be under water during periods of high flow and require care to locate and adjust. • Unit is heavy and requires machinery to lower in place/install. • Structure may require piles or ground improvement for foundation stability due to the weak underlying peat and alluvium.

3 EEL PASSAGE

3.1.1 The movement and natural migration of eels over and around water management structures can be mitigated using a range of products. Eel passes comprising climbing substrate can be fitted over weirs to allow eels to travel up stream. By simulating wet grass and providing an attractive flow, eels can find a safe route to continue their journey.

4 TIMELINE

4.1.1 It would be advantageous to install the water management structure connection between Leiston Drain and the realigned Sizewell Drain during the realignment of Sizewell Drain. This will make the structure among the earliest construction tasks for Sizewell C enabling works.

4.1.2 It is recommended that efforts should be made to carry out construction of this structure in the drier months of the year.

5 SUMMARY

5.1.1 This document has highlighted the requirement for the short-term and long-term requirements of a water-control structure prior to the connection between Leiston Drain and the realigned Sizewell Drain. This document outlines various water management structure options, noting some benefits and disadvantages of each, as well as outlining mitigations for eel movement.

5.1.2 As part of the DCO application the Environmental Statement (Book 6, Volume 2, Chapter 19 Groundwater and Surface Water) concluded at paragraph 19.6.104 the need for a water management structure with fine tuning capability:

5.1.3 “A key water management structure (pipe dam/tilting weir) is planned for the northern end of the Sizewell Drain as seen in Appendix 19C of this volume. The design of the structure considered the interfaces with other drains and ditches and would aim to ensure the existing water balance of the surrounding wetland areas was maintained. The enhanced water level control within the Sizewell Marshes SSSI would allow for fine tuning of the management regime over time. The specific position, nature and operational parameters of the control structures will be determined in conjunction with stakeholders.”

5.1.4 Correspondingly it is concluded that to meet the need to fine tune water levels, the following structures are preferred:

- Overflow weir
- Tilting weir
- Overflow sluice

APPENDIX D

MAIN DEVELOPMENT SITE WATER MANAGEMENT ZONE SUMMARY (DCO TASK D2)

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1 INTRODUCTION

1.1.1 This document has been prepared to provide further background to the surface water management proposals for Sizewell C (SZC) nuclear power station basic design. The surface water proposals prioritise Sustainable Drainage Systems (SuDS) which are incorporated across the site in the forms of swales, infiltration trenches, permeable pavements and infiltration basins. These have been provisioned for early in the project. This document provides an overview about the Main Development Site water management zone (WMZ) infiltration basins, identifying design parameters and providing assurance that there is adequate storage on site for various storm events throughout the power station construction duration. Infiltration basins are proposed across the site in the Temporary Construction Area (TCA), Ancillary Construction Area (ACA), and the Green Rail route. The ACA is also known as the Land East of Eastlands Industrial Estate (LEEIE). In this document this will be referred to as the ACA.

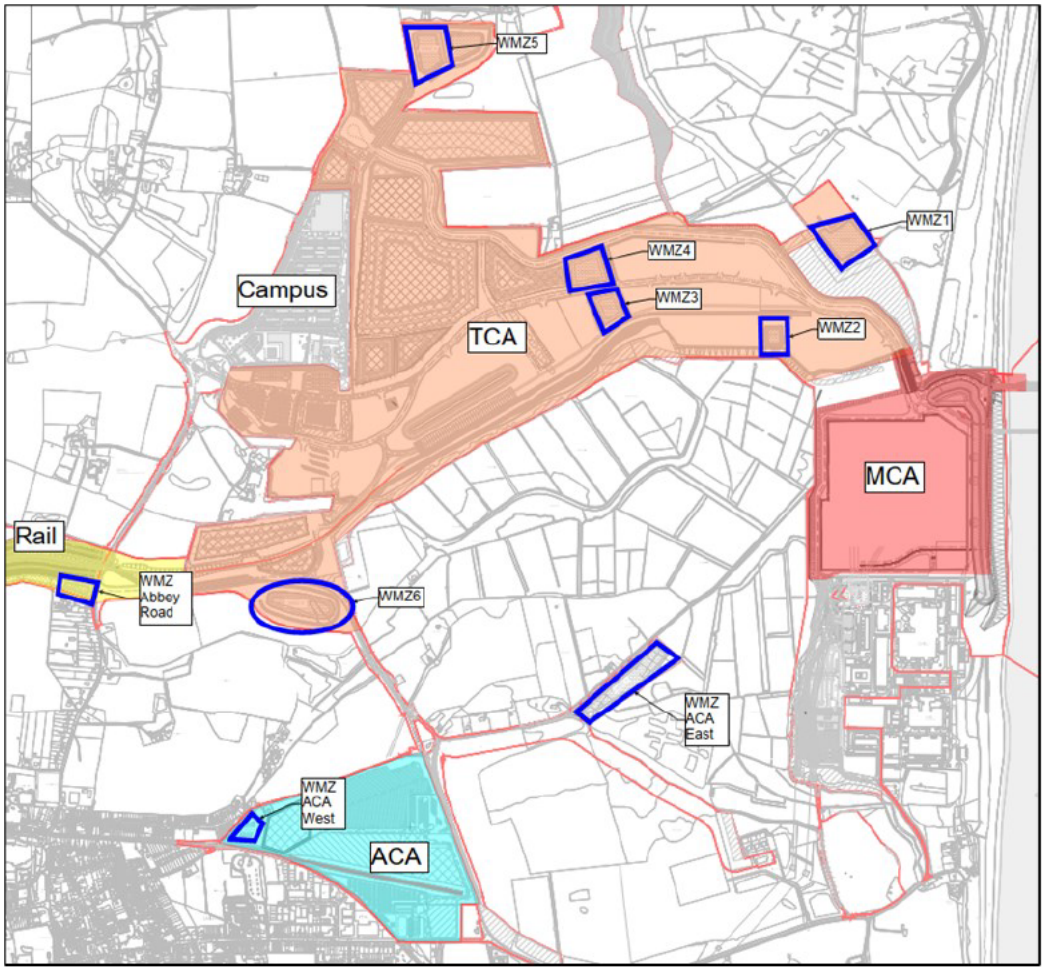
1.1.2 This note provides details of the WMZ infiltration basins for the established site. Temporary surface water control measures such as temporary sediment ponds will be required in areas prior to some of the WMZ infiltration basins are installed. The locations of the temporary surface water controls measures are to comply with the Code of Construction Practice (CoCP) and will be detailed alongside the construction sequencing with the Contractor.

1.1.3 The information presented in this report is in accordance with the overarching drainage principles that are documented in the SZC Development Consent Order (DCO) Outline Drainage Strategy at Volume 2, Chapter 2, Appendix 2A of the Environmental Statement [APP-181].

1.2 Background

1.2.1 The extent of the SZC Main Development Site (MDS) is set by the red line boundary shown in the Construction Site Plot Plan (CSPP). This incorporates the ACA, TCA, Main Construction Area (MCA), and Railway to the west. These areas are approximately outlined in Figure 1-1. Surface water drainage infrastructure will be required for all areas within the red line boundary and to ensure no surface water, other than at controlled greenfield runoff rates, will runoff the site up to a 1:100 year storm including climate change.

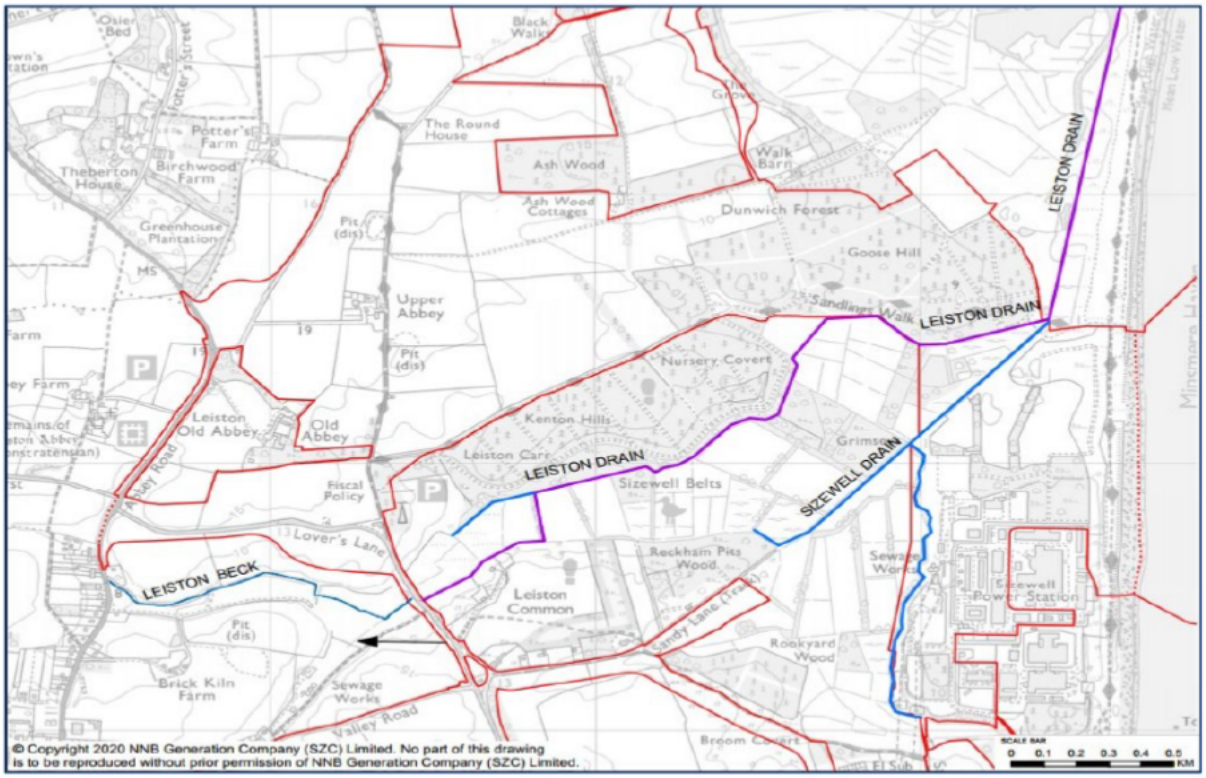
Figure 1-1 - Site plot plan with construction areas



1.2.2 Existing Site

1.2.3 The existing site is largely grassland across the TCA and the ACA. The MCA is also grassland with some ancillary Sizewell B buildings. The land to the south of the TCA is a Site of Special Scientific Interest (SSSI), which contains multiple watercourses, including two formal watercourses: the Leiston Drain and the Sizewell Drain. Surface water on the existing site currently infiltrates to ground and/or enters local watercourses which include the Leiston and Sizewell Drains and other minor tributaries – see Figure 1-2.

Figure 1-2 - Existing Surface Water Drains



1.2.4 Main Development Site Water Management Zones

1.2.5 The surface water drainage design is required to capture all surface water runoff from within the red line boundary, as defined in the Outline Drainage Strategy described in the Development Consent Order (DCO). To ensure that the construction site mimics the existing site surface water management, the runoff will be discharged through infiltration to ground where possible with some outfalls to existing watercourses or to the sea where necessary.

1.2.6 To manage the runoff across the MDS, catchments were identified across the TCA, ACA, MCA and Railway area. The following catchments were defined in the Outline Drainage Strategy:

- TCA – Catchments 1 to 6,
- ACA – Catchment ACA,
- MCA – Catchments 7 to 9,
- Railway

1.2.7 The surface water runoff within each catchment is proposed to infiltrate either directly through a permeable surface, or via a Sustainable Drainage System (SuDS) which will include:

- Swales;
- Infiltrations trenches; and,
- Infiltration basins (Water Management Zones).

1.2.8 Where suitable, the surfaces of the catchments are proposed to be permeable, so surface water will infiltrate to ground in the first instance. Any runoff that does not infiltrate directly will be captured through swales that border each catchment. The swales provide local source control to ensure the management of water returning to the ground to mimic the existing condition. The swales contain an infiltration trench beneath them which will encourage further infiltration, as well as provide additional storage. Any water that does not infiltrate through the infiltration trench into the surrounding ground will be captured by a perforated pipe within the trench, which will convey the flow to a Water Management Zone (WMZ) infiltration basin. This concept is shown in Figure 1-3 below. More frequent storm events will not need to overflow into the WMZ infiltration basins and surface water will be primarily discharged through infiltration at source. In less frequent storm events, the WMZ infiltration basins will be used to attenuate and infiltrate surface water and as such have been sized so they have capacity for a 1:100-year storm event including climate change.

1.2.9 Infiltration basins in catchments 1, 2, 3, and 6 have an outlet to nearby watercourses, restricted to greenfield runoff rates, and to be agreed with external stakeholders Suffolk County Council (SCC), Environment Agency (EA) and/or Internal Drainage Board (IDB) where applicable. As an additional backup measure, the WMZ infiltration basins for catchments 1-4 have an allowance for an overflow into a conventional drainage system (spine network) discharging to the combined drainage outfall (CDO) which discharges to the sea. Hydraulic modelling shows this network is not required; this spine network has only been included at this stage as a precaution.

Figure 1-3 - Surface water runoff capture and discharge process

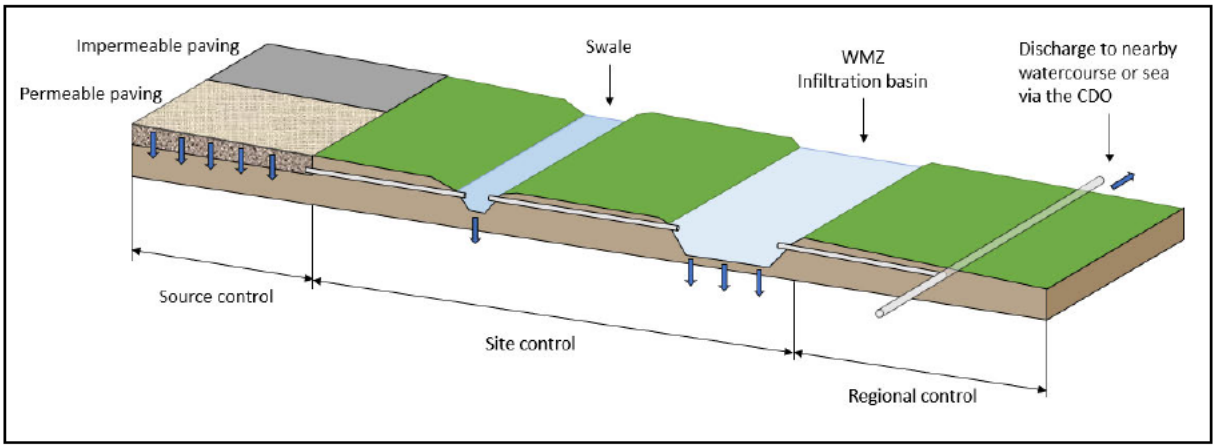
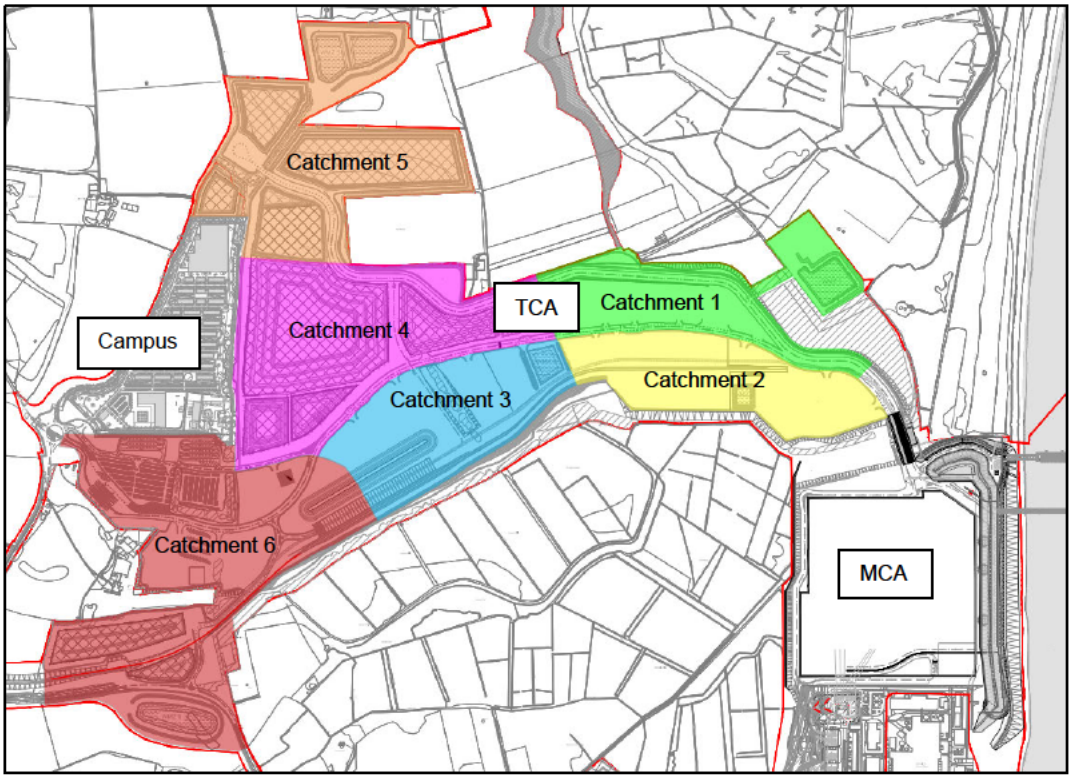


Figure 1-4 - TCA Enabling Works surface water drainage catchments



1.3 Scope

1.3.1 This document provides a summary of infiltration basins that are required to manage surface water runoff during the enabling works, in line with the Enabling Works surface water drainage strategy. The document presents the hydraulic assessment of the WMZs across the TCA, ACA and Railway area.

1.3.2 This document does not address the design of other minor SuDS features such as swales, infiltration trenches, and permeable paving. These features will be further detailed in future proposals, in conjunction with Contractor involvement.

2 DESIGN REQUIREMENTS

2.1.1 In accordance with the Outline Drainage Strategy, all infiltration basins within the MDS are designed to cater for a 100-year flood event plus a 20% allowance for climate change. This section summarises the design parameters used in the hydraulic assessment to determine the size of the WMZ infiltration basins. The volume assessment was conducted using MicroDrainage Source Control using the parameters and assumptions in the following sections. By sizing the infiltration basins using Source Control and not considering additional storage in the upstream network, the storage volumes calculated are conservative and will be able to be reduced in the next design phase.

2.2 General Parameters

2.2.1 The parameters in Table 2-1 were used to determine approximate storage volumes required for critical storm events for 100-year return period for a storm duration of up to 24 hours, including a 20% allowance for climate change in accordance with the Outline Drainage Strategy.

Table 2-1 - Input parameters for MicroDrainage Source Control storage volumes

	Parameter	Notes
Rainfall-Runoff method	Flood Studies Report (FSR), Flood Estimation Handbook (FEH) 1999 and 2013	Sensitivity check using FEH 1999 and 2013
Return Period (years)	100	As per DCO Outline Drainage Strategy [1]
Storm duration (minutes)	15 – 1440	As per DCO Outline Drainage Strategy [1]
Climate Change (%)	20	As per DCO Outline Drainage Strategy [1] and EA guidance [2]
Volumetric Runoff Coefficient	Varies per catchment	Wallingford Procedure Vol 1 Equation 7.3
Freeboard (mm)	300	CIRIA C753 – The SuDS Manual
Factor of Safety	1.5	[3]

[1] Environmental Statement – 6.3 Volume 2 Main Development Site, Chapter 2 Description of the Permanent Development, Appendix 2A Outline Drainage Strategy (EN010012-001802-SZC_Bk6_ES_V2_Ch2_Appx2A)

[2] Environment Agency – Flood risk assessment: climate change allowances - Table 2: peak rainfall intensity allowance in small catchments (less than 5 km^2) or urban drainage catchments (based on a 1961 to 1990 baseline)

[3] Table 25.2 in the CIRIA SuDS manual provides guidance on which Factor of Safety (FoS) to use given a range of areas and consequences of failure. Given this area is a temporary construction site for 10 years with infiltration basins designed for a 1:100 year return period, assuming only infiltration through the sides of the basin, and the selected infiltration rates are the worst case rates from a series of GI campaigns, it is proposed to use a FoS of 1.5 as opposed to 5 or 10. Use of a FoS of 5 or 10 would require even greater oversized infiltration basins which is not deemed necessary, especially where the basins have an overflow to the spine network.

2.2.2 All three rainfall-runoff methods were used to undertake sensitivity checks on the design volumes. It was noted that the FEH 2013 rainfall-runoff method generally provided more conservative values for greater return periods in comparison to FEH 1999 and FSR.

2.2.3 As the Sizewell development site is extensive, two FEH data sets were necessary to undertake the hydraulic modelling and are shown in Table 2-2 below. The rainfall data set used in the ACA drainage modelling was 'GB 647050, 262950', whereas all other areas used data set 'GB 647450, 264900'.

Table 2-2 - FEH 1999 rainfall parameters

FEH Site	C (1km)	D1 (1km)	D2 (1km)	D3 (1km)	E (1km)	F (1km)
GB 647050 262950	-0.019	0.298	0.279	0.207	0.309	2.506
GB 647450 264900	-0.02	0.299	0.272	0.215	0.311	2.506

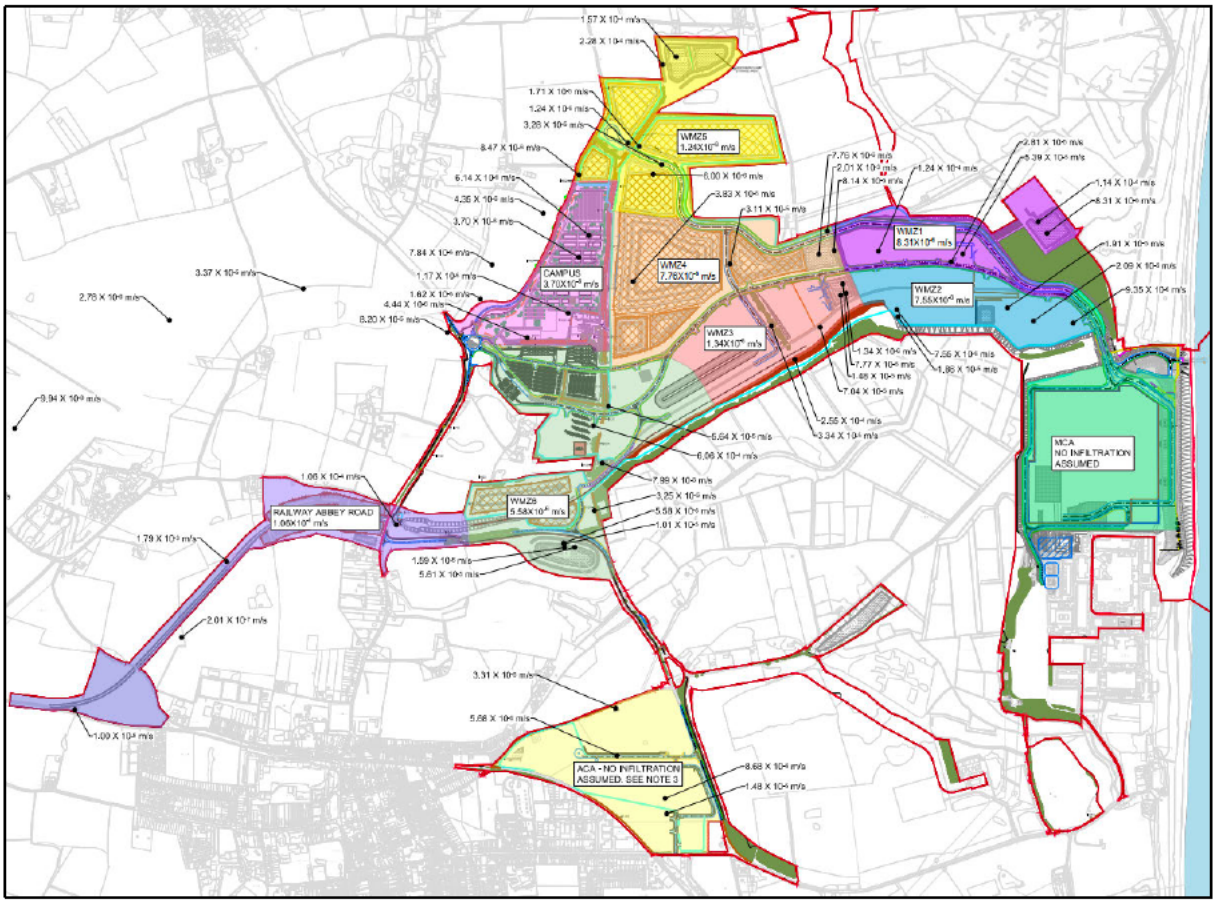
2.2.4 Using FSR, Sizewell, Suffolk was used as the location with M5-60 and 'r' ratio of 18.2 mm and 0.4 taken respectively. Storage estimates using all rainfall-runoff methods are included in this document.

2.2.5 Attenuation structures are modelled in Source Control to have side slopes of 1:3. The infiltration rate has been applied to the side walls of the attenuation structure only. No infiltration is applied to the base of the structure to account for any loss of efficiency over the design life.

2.3 Infiltration rates

2.3.1 Several ground investigation (GI) campaigns have been undertaken across the site to determine the infiltration potential across various catchment areas. The figure below summarises the range of infiltration rates recorded in four separate campaigns in 2014, 2015, 2017 and 2020. The lowest (worst-case) rate for each catchment has been used at this design stage for surface water calculations, specifically to calculate the storage volume required in infiltration basins. Further GI campaigns are planned, and results will be included during the next design stage. The geology across the site is largely sandy which provides confidence that the infiltration rates used in the surface water design are conservative.

Figure 2-1 - Infiltration rates (refer to drawing SZC-EW0320-ATK-XX-000-XXXXXX-DRW-CCD-000001 in Annex A)



2.3.2 In order to calculate the contributing areas to each of the water management zones, they have been assessed based on their land use with their appropriate percentage impermeable (PIMP) value for each area type:

- Roofed buildings: 100%
- Asphalt roads/pavements: 90%
- Gravel areas: 50%
- Road verges: 50%
- Stockpile area: 30%
- Grassed areas: 30%

2.3.3 Using the above PIMP values and known areas within each catchment, a source control model has been run to provide assurance that the design storage is able to be catered for within the WMZ infiltration basins.

2.4 Water Quality

2.4.1 The purpose of this document is to provide clarity around sizing of WMZ infiltration basins, however quality of surface water runoff from the site is also important and therefore is summarised in this section. Surface water discharges to, in order of preference, the ground, nearby watercourses, or the sea.

2.4.2 Discharges to nearby watercourses and the sea will be controlled through permit applications and ongoing monitoring to ensure the quality of the water meets the Environment Agency's (EA) criteria prior to discharge.

2.4.3 There are possible contaminants that need to be considered in surface water treatment design across the site. These are divided into:

- Sediment runoff
- Chemical spills, including concrete batching plant, waste consolidation centre and fuel farm.

2.4.4 Treatment of sediment runoff will be managed through the implementation of SuDS features on site, including:

- Swales
- Infiltration trenches
- Hay bales (around stockpiles)
- Silt fences (where suitable)
- WMZ infiltration basins

2.4.5 The positioning and location of these features will be further defined in the following design phases and will follow overarching principles in the CIRIA SuDS Manual (C753) as well as the Outline Drainage Strategy document.

2.4.6 Treatment of chemical spills will be required at source, by specific treatment systems. For example, around the fuel storage area the pavement will be impermeable to prevent fuel seeping into the groundwater. Any potential oil spills will be captured and treated via an oil interceptor sized and designed suitably for the potentially contaminated spill volumes.

2.4.7 The assessment of water quality risk management for each WMZ will be provided through the simple index approach as outlined in Section 26.7.1 of the CIRIA SuDS Manual (C753). This method will ultimately determine

what SuDS measures are required to treat different types of developments across the MDS. The steps are set out as:

Step 1 – Allocate suitable pollution hazard indices for the proposed land use
Step 2 – Select SuDS with a total pollution mitigation index that equals or exceeds the pollution hazard index
Step 3 – Where the discharge is to protected surface waters or groundwater, consider the need for a more precautionary approach

2.4.8 Proposed SuDS features within each catchment will be used to determine a total pollution mitigation index (Table 26.3 CIRIA SuDS Manual). Where additional SuDS features are not considered appropriate at this design stage, proprietary, non-SuDS treatment may be proposed. This assessment will be carried out for each WMZ in the next design phase.

2.5 Discharge Rates

2.5.1 Proposed discharge rates from infiltration basins to nearby watercourses have been defined following the Environment Agency guidance (Report SC030219 – Rainfall runoff management for developments). A Q_{bar} (peak rate of flow from a catchment for the mean annual flood - return period of approximately 1:2.3 years) greenfield runoff rate has been calculated for each catchment using UK SuDS guidance. In some cases (the ACA), this is the proposed restricting flow rate. Across the TCA however, it is noted that Q_{bar} is extremely small, and therefore the Environment Agency guidance is followed, whereby if Q_{bar} is less than 1 l/s/ha, the latter can be proposed as a limiting discharge rate. Where an outfall is proposed from an infiltration basin to nearby watercourses in the TCA and rail catchments, this is the proposed approach.

2.5.2 It is important that the SSSI is neither overwhelmed with additional surface water runoff, nor starved of surface water during the construction and operation of SZC. Maintaining the status quo of how the existing site drains is required to ensure the SSSI retains its current ecological and hydrological features. This has been reinforced by conversations with the EA and other stakeholders and is represented in both the groundwater/surface water modelling and flood risk modelling.

3 WATER MANAGEMENT ZONES

3.1.1 Generally, the surfaces of the catchments are largely permeable, so surface water will infiltrate to ground in the first instance. Any runoff that does not infiltrate directly or captured through swales with infiltration trenches will be captured by a perforated pipe within the trench, that will convey the flow to a Water Management Zone (WMZ) infiltration basin. The WMZs are

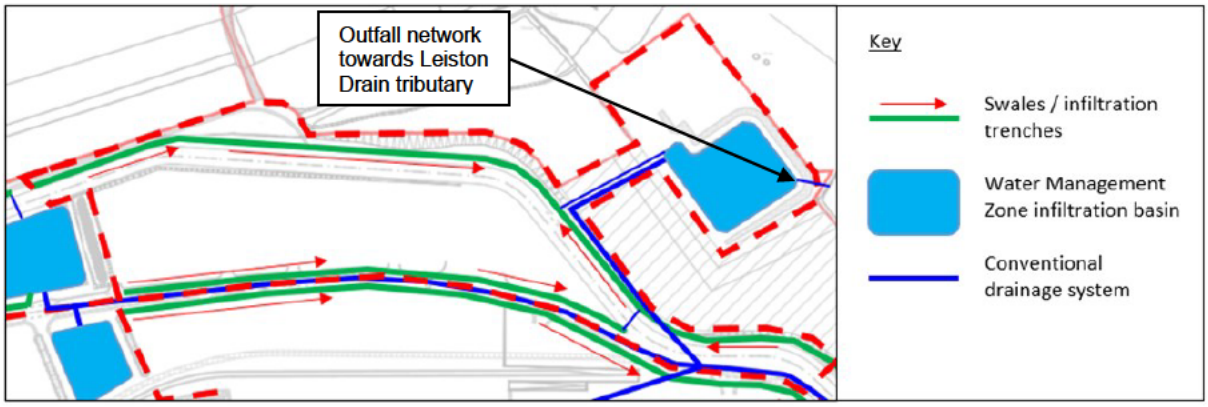
designed for 100-year return period rainfall events including climate change. In extreme rainfall events the WMZs for catchments 1-4 will overflow into a conventional drainage system (spine network) discharging to the CDO which outflows to the sea.

3.2 Catchment 1

3.2.1 Catchment 1 is located in the north eastern area of proposed TCA. This catchment houses plant and workshops such as joinery/metal workshops, a formwork factory and slurry treatment plants. It also houses the fire and rescue centre, Emergency response facility and fuel farm. The catchment encompasses sections of the site access road to the south, haul roads to north and east, and one of the Contractor's working compounds. Catchment 1 has a total area of 19.4 ha and will drain via combined swale and infiltration trenches with perforated pipes. Two main runs are proposed, north and south of the catchment, both running from the west to WMZ1 which is proposed in the east. An outfall from WMZ1 is proposed to discharge surface water to the Leiston Drain tributary east of WMZ1, at 19.4 l/s (equivalent to 1 l/s/ha). An overflow connection is also proposed from WMZ1 to the Construction Drainage Outfall (CDO).

3.2.2 Due to the nature of the use for this catchment and the risk of potential contamination, most of this area will require control and treatment of surface water runoff prior to discharge. For example, the fuel farm will be concreted, and other areas in the Contractor's compound will be hard standing if there is potential for chemical spills. A 90% PIMP factor is assumed for this catchment. The area of hardstanding may decrease in the future, however for this stage of design, a more conservative value is considered more suitable to space proof the infiltration basin.

Figure 3-1 - Catchment 1 proposed drainage



3.2.3 WMZ1

3.2.4 Alongside the general parameters stated in Section 2.2, the parameters in Table 3-1 were used to determine a conservative estimate for the required storage volume for WMZ1. The volume allocated for WMZ1 in the Civil 3D model exceeds this.

3.2.5 WMZ1 is proposed at a low point east of the TCA where the ground levels range between 2 and 3 mAOD. The groundwater contours from Winter 2018 included in the Environmental Statement showed the groundwater level is approximately 0.9 mAOD at the location of WMZ1 (see Annex B). Given the proximity to the groundwater table, infiltration from the basin is not considered feasible and the basin is assumed to be lined.

3.2.6 A more detailed figure showing the proposed arrangement of the WMZ1 basin is provided in Annex C.

Table 3-1 - Water Management Zone 1 - Infiltration Basin Summary

Design Input		**Comment**
Total catchment area	19.430 ha	
Percentage of runoff	90%	To be revised as design progresses
Volumetric runoff coefficient (Cv)	0.684, 0.746	Summer, winter respectively
Infiltration rate	0 m/s	
Overflow allowance to nearby watercourse	19.43 l/s	Assumed at 1 l/s/ha [1]
Overflow to spine network	Yes	Allowance for 200 l/s, not included in model
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	0.900 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	10770.1 m^3	1:100 year return period, 1440 winter storm
FEH 1999	13946.6 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**14690.4 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	1.200 mAOD	
Bottom of basin area	10579.2 m^2	

Top of basin area (excluding freeboard)	12618.8 m^2	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**17328 m^3**	(excluding 300mm freeboard)

[1] Based on Environment Agency guidance - Rainfall runoff management for developments ref. SC030219. Limiting discharge rates for sites should be set to Qbar or 1 l/s/ha, whichever is greater.

3.3 Catchment 2

3.3.1 Catchment 2 is south of catchment 1 and encompasses sections of the site access and haul roads at the point they converge and then cross the SSSI. It will contain Contractor compounds, including concrete batching plant, the railhead, a waste consolidation area, and several laydown areas. The catchment has a total area of approximately 17.4 ha. The majority of this area will be hardstanding and therefore a 90% PIMP factor has been assumed. The area of hardstanding may decrease in the future, however for this stage of design, a more conservative value is considered more suitable to space proof the infiltration basin.

3.3.2 The drainage in this catchment includes road edge swales to the south of the main access road collecting road runoff and runoff from the compound area north of the railhead. A separate network made up of filter drains is proposed at the compound perimeter to cater for the runoff immediately south of the railhead. The network discharges into WMZ2 to the south. An outfall from WMZ2 is proposed to discharge surface water to the Leiston Drain south of WMZ2, at 17.4 l/s (equivalent to 1 l/s/ha). An overflow connection is also proposed from WMZ2 to the Construction Drainage Outfall (CDO) via a spine network as a precaution.

Figure 3-2 - Catchment 2 proposed drainage

3.3.3 WMZ2

3.3.4 The parameters in Table 3-2 were used to determine a conservative estimate of the attenuation volume required to serve TCA Catchment 2.

Table 3-2 - Water Management Zone 2 - Infiltration Basin Summary

Design Input		**Comment**
Total catchment area	17.370 ha	
Percentage of runoff	90%	To be revised as design progresses
Volumetric runoff coefficient (Cv)	0.684, 0.746	Summer, winter respectively
Infiltration rate	7.55E-06 m/s	
Overflow allowance to nearby watercourse	17.37 l/s	Assumed at 1 l/s/ha [1]
Overflow to spine network	Yes	Allowance for 200 l/s, not included in model
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	0.800 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	9211.2 m^3	1:100 year return period, 1440 winter storm
FEH 1999	12005.4 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**12663.5 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	3.200 mAOD	
Bottom of basin area	3290.1 m^2	
Top of basin area (excluding freeboard)	6274.5 m^2	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**17694.5 m^3**	(excluding 300mm freeboard)

[1] Based on Environment Agency guidance - Rainfall runoff management for developments ref. SC030219. Limiting discharge rates for sites should be set to Qbar or 1 l/s/ha, whichever is greater.

3.4 Catchment 3

3.4.1 Catchment 3 is to the west of catchment 2 and is enclosed by roads on three sides and the rail to the south. It encompasses part of the combined site access road, a section of the railway and two Contractor's compounds. The catchment has a total area of approximately 21.0 ha. A 90% percentage of impermeable area has been allowed for in these areas conservatively, should the use of the Contractor compounds require hardstanding surfaces. This will likely be reduced in the future. A 50% PIMP has been applied to the railway sections.

3.4.2 The runoff is divided to drain into the road drainage swales proposed along the roads forming the perimeter drainage. A separate network has been designed to cater for the runoff from the unloading area platform and railway drainage. The perimeter drainage discharges to WMZ3 to the east of the catchment. An outfall from WMZ2 is proposed to discharge surface water to the Leiston Drain south of WMZ3, at 21.0 l/s (equivalent to 1 l/s/ha). An overflow connection is also proposed from WMZ3 to the Construction Drainage Outfall (CDO) via a spine network.

Figure 3-3 - Catchment 3 proposed drainage

3.4.3 **WMZ3**

3.4.4 Table 3-3 summarises the parameters used to determine a conservative estimate of the attenuation volume required and the volume space-proofed for WMZ3.

3.4.5 A more detailed figure showing the proposed arrangement of the WMZ3 basin is provided in Annex C.

Table 3-3 - Water Management Zone 3 - Infiltration Basin Summary

Design Input		Comment
Total catchment area	20.960 ha	
Percentage of runoff	90%	
Volumetric runoff coefficient (Cv)	0.684, 0.746	Summer, winter respectively
Infiltration rate	1.34E-06 m/s	
Overflow allowance to nearby watercourse	20.96 l/s	Assumed at 1 l/s/ha [1]
Overflow to spine network	Yes	Allowance for 200 l/s, not included in model
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	1.200 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	11458.8 m^3	1:100 year return period, 1440 winter storm
FEH 1999	14887.7 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**15685.8 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	5.000 mAOD	
Bottom of basin area	3346.8 m^2	
Top of basin area (excluding freeboard)	7162.9 m^2	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**17341.0 m^3**	(excluding 300mm freeboard)

[1] Based on Environment Agency guidance - Rainfall runoff management for developments ref. SC030219. Limiting discharge rates for sites should be set to Qbar or 1 l/s/ha, whichever is greater.

3.5 Catchment 4

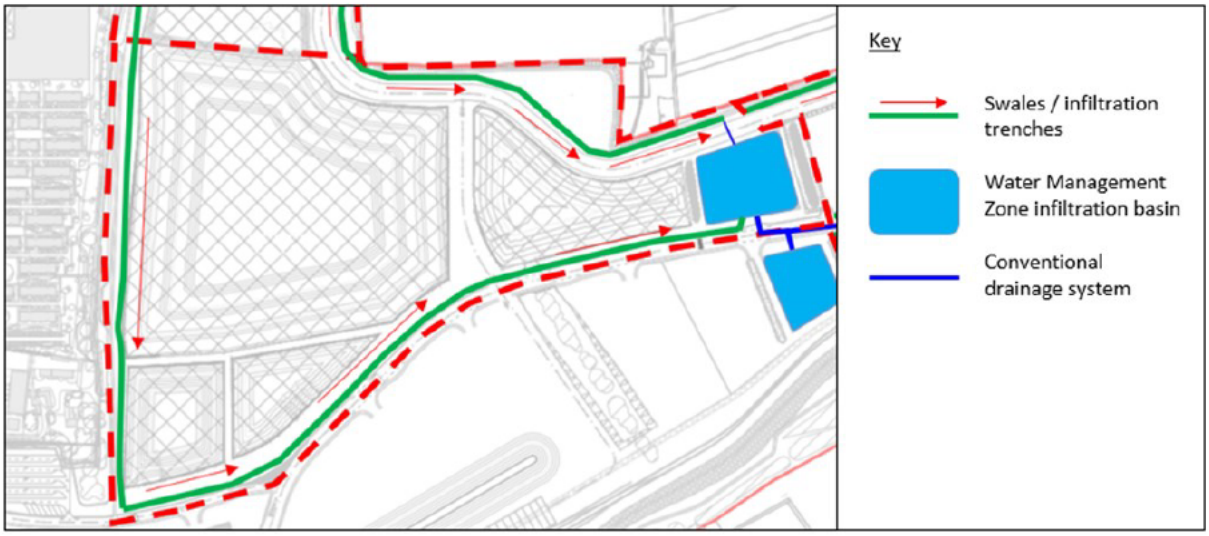
3.5.1 Catchment 4 is to the west of catchment 1. It encompasses part of the access and haul road but is predominantly material storage and stockpile area. The catchment has a total area of approximately 33.3 ha. This results

in a conservative percentage of impermeable area (PIMP) for the catchment to be 50%. As stockpiles are assigned a 30% PIMP, this figure may be reduced in the future, but for this design phase is considered conservative.

3.5.2 Perimeter road swales have been proposed along the roads to drain the runoff from the catchment. Two such networks, one from the north and the other from the south, discharge to WMZ4 located to the east of the catchment. An overflow connection is also proposed from WMZ4 to the Construction Drainage Outfall (CDO) via a spine network as a precaution.

3.5.3 A more detailed figure showing the proposed arrangement of the WMZ4 basin is provided in Annex C.

Figure 3-4 - Catchment 4 proposed drainage



3.5.4 **WMZ4**

3.5.5 Table 3-4 summarises the parameters used to determine a conservative estimate of the attenuation volume required and the volume space-proofed for WMZ4.

Table 3-4 - Water Management Zone 4 - Infiltration Basin Summary

Design Input		Comment
Total catchment area	33.320 ha	
Percentage of runoff	50%	
Volumetric runoff coefficient (Cv)	0.568, 0.680	Summer, winter respectively
Infiltration rate	7.76E-06 m/s	

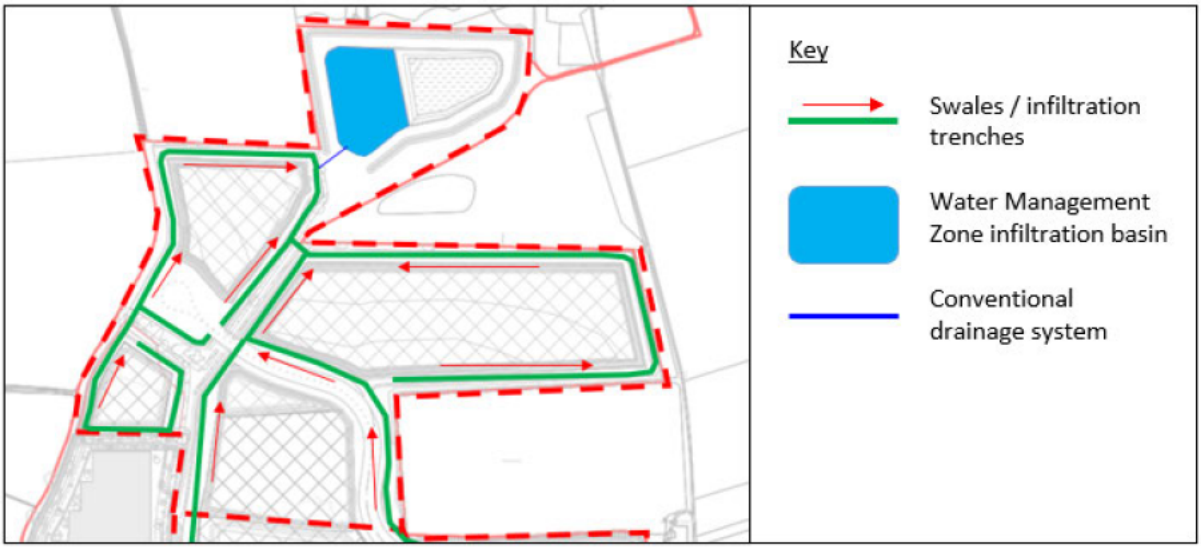
Overflow allowance to nearby watercourse	No	
Overflow to spine network	Yes	Allowance for 200 l/s, not included in model
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	1.200 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	10080.8 m^3	1:100 year return period, 1440 winter storm
FEH 1999	12795.4 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**13422.3 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	5.200 mAOD	
Bottom of basin area	4916.6 m^2	
Top of basin area (excluding freeboard)	9759.7 m^2	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**25688.8 m^3**	(excluding 300mm freeboard)

3.6 Catchment 5

3.6.1 Catchment 5 is to be north of catchment 4. It encompasses part of the haul road and is predominantly made up of proposed borrow pits and stockpile areas. The catchment has a total area of approximately 31.2 ha. A 50% PIMP factor has been applied to this area. As with catchment 4, this may be reduced in the future.

3.6.2 Two drainage networks along the site boundary have been designed as perimeter swales/infiltration trenches with perforated pipes, as well as a network surrounding the storage area. These networks discharge to WMZ5 located to the north of the catchment. No outfalls are proposed from WMZ5 at this stage.

Figure 3-5 - Catchment 5 proposed drainage



3.6.3 WMZ5

3.6.4 Table 3-5 summarises the parameters used to determine a conservative estimate of the attenuation volume required and the volume space-proofed for WMZ5.

Table 3-5 - Water Management Zone 5 - Infiltration Basin Summary

Design Input		Comment
Total catchment area	31.195 ha	
Percentage of runoff	50%	
Volumetric runoff coefficient (Cv)	0.568, 0.680	Summer, winter respectively
Infiltration rate	1.24E-06 m/s	
Overflow allowance to nearby watercourse	No	
Overflow to spine network	No	
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	1.400 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	9715.2 m^3	1:100 year return period, 1440 winter storm
FEH 1999	12296.3 m^3	1:100 year return period, 1440 winter storm

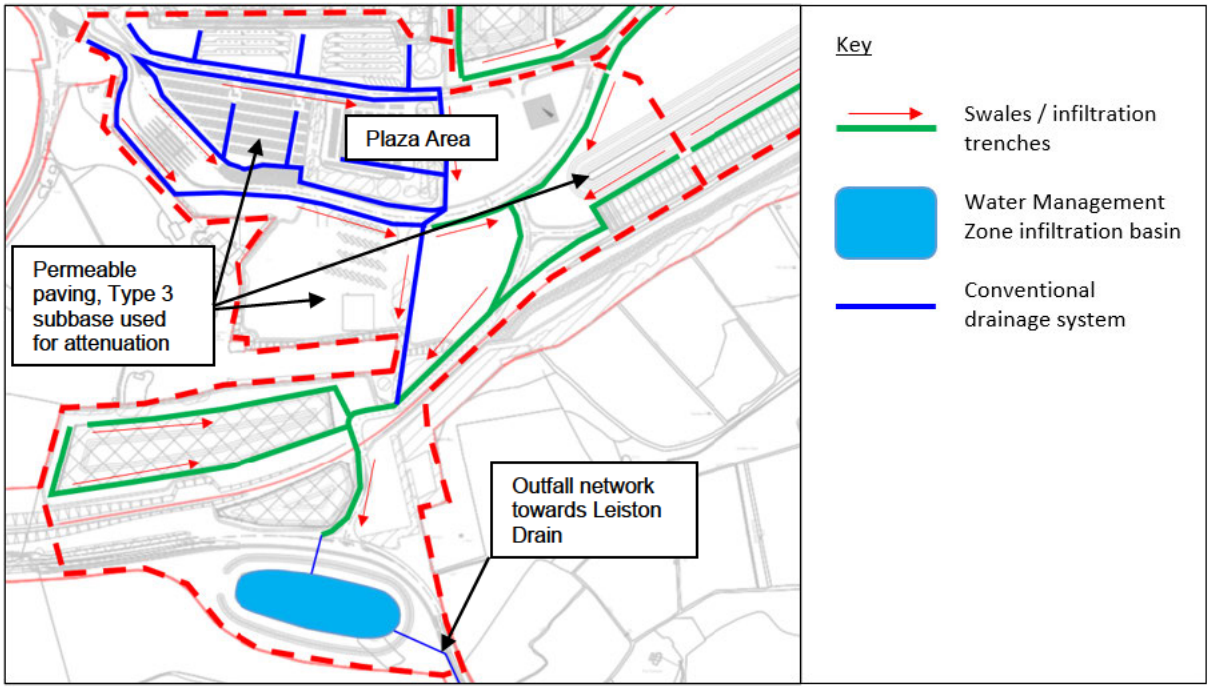
FEH 2013	12891.1 m^3	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	6.000 mAOD	
Bottom of basin area	7658.1 m^2	
Top of basin area (excluding freeboard)	9615.7 m^2	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**17223.8 m^3**	(excluding 300mm freeboard)

3.7 Catchment 6 & Plaza

3.7.1 Catchment 6 is located to the south-west of catchment 3 and encompasses site access roads, part of the railway, numerous site facilities, including rail and freight security buildings, vehicle inspection cabins, and the main TCA site offices. Catchment 6 also encompasses a sewage treatment plant, potable water storage facility and the Plaza area. The catchment has a total area of approximately 47.8 ha. A 58% PIMP has been applied to this catchment to account for stockpiles, soft landscaping and where TruckPave is proposed as hardstanding.

3.7.2 The rail drainage consists of filter drains adjacent to the track, cut off drains at the top of the cutting, and toe ditches at the bottom of the embankment. The Plaza drainage consists of filter drains along the road verges. Perimeter swales are proposed around the storage areas and adjacent to the access roads. All drainage networks discharge to WMZ6 located to the south of the catchment. An overflow is proposed to discharge runoff to the Leiston Drain near Lover's Lane.

Figure 3-6 - Catchment 6 proposed drainage



3.7.3 WMZ6

3.7.4 Table 3-6 summarises the parameters used to determine a conservative estimate of the attenuation volume required and the volume space-proofed for WMZ6.

Table 3-6 - Water Management Zone 6 - Infiltration Basin Summary

Design Input		Comment
Total catchment area	47.770 ha	
Percentage of runoff	58%	
Volumetric runoff coefficient (Cv)	0.604, 0.701	Summer, winter respectively
Infiltration rate	5.58E-06 m/s	
Overflow allowance to nearby watercourse	47.77 l/s	Assumed at 1 l/s/ha [1]
Overflow to spine network	No	
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	2.100 mAOD	Based on Environment Statement groundwater contours (Annex B)

MicroDrainage Source Control Summary		
FSR	14418.3 m^3	1:100 year return period, 1440 winter storm
FEH 1999	19117.2 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**20216.7 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	8.000 mAOD	
Bottom of basin area	7165.8 m^2	
Top of basin area (excluding freeboard)	11287.5 m^2	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**19376.0 m^3**	(excluding 300mm freeboard)

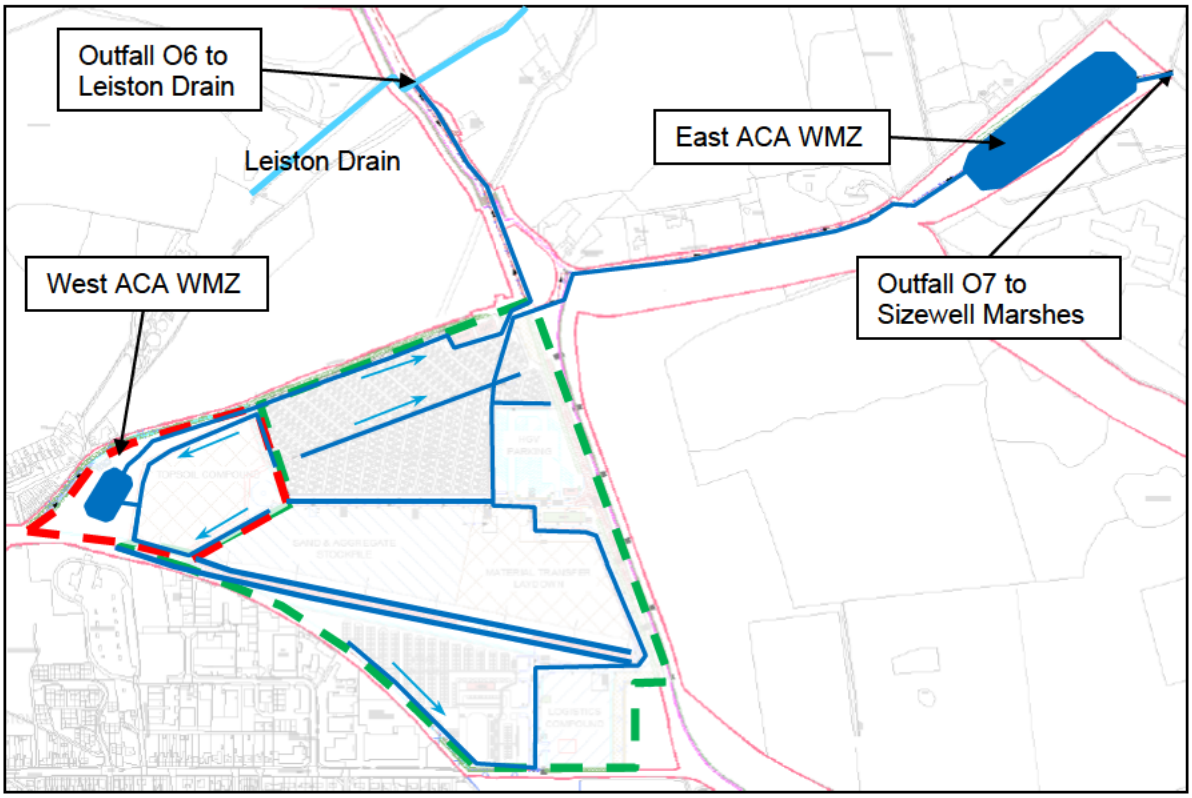
[1] Based on Environment Agency guidance - Rainfall runoff management for developments ref. SC030219. Limiting discharge rates for sites should be set to Qbar or 1 l/s/ha, whichever is greater.

3.8 Ancillary Construction Area (ACA)

3.8.1 The ACA is isolated from the TCA and MCA, and therefore has an independent surface water drainage network to that serving the main construction site. The ACA has an area of approximately 29.7 ha and encompasses caravan pitches, HGV parking, topsoil compound, sand and aggregate stockpile, material transfer laydown, park and ride and logistics compound. No infiltration is assumed within the ACA as per the DCO Outline Drainage Strategy, and runoff will be collected by a variety of features including swales, permeable paving with filter drains and conventional drainage elements.

3.8.2 Two water management zone attenuation features are proposed to store runoff prior to discharge. Runoff from the topsoil compound area and the area west of this compound (dashed red line in Figure 3-7) will be captured in swales and attenuated in the West ACA WMZ, before discharging to the Leiston Drain near Lover's Lane. Surface water runoff from all other areas (dashed green line in Figure 3-7) within the ACA will be conveyed to the East ACA WMZ, before discharging to the Sizewell Marshes. The outflows will be limited to greenfield runoff rates (Q_{bar}).

Figure 3-7 - ACA proposed drainage



3.8.3 East ACA WMZ

3.8.4 The drainage strategy within the ACA has been modified since Basic Design following agreement with the Environment Agency and Suffolk County Council to allow more runoff to be attenuated in the East WMZ and discharge to the Sizewell Marshes. Therefore, the area currently designated for the East WMZ in the construction site plot plan is being increased to meet the required volume calculated in Table 3-7.

3.8.5 The required attenuation volume for the East ACA WMZ is conservatively estimated as 21700 m^3. Further work will be undertaken during Detailed Design to determine the actual volume required, allowing for storage in the pipe network and infiltration within the WMZ.

Table 3-7 - ACA East - Infiltration Basin Summary

Design Input		Comment
Total catchment area	25.222 ha	
Percentage of runoff	100%	
Volumetric runoff coefficient (Cv)	0.761, 0.817	Summer, winter respectively
Infiltration rate	0 m/s	

Overflow allowance to nearby watercourse	59.87 l/s	Q_{bar}
Overflow to spine network	No	
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	1.000 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	15381.1 m^3	1:100 year return period, 1440 winter storm
FEH 1999	20579.7 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**21641.3 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	2.450 mAOD	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**22000 m^3**	(excluding 300mm freeboard)

3.8.6 West ACA WMZ

3.8.7 As stated above, the ACA drainage strategy is under development and the required attenuation volume for the West ACA WMZ is conservatively estimated as 3850 m^3. The current CSPP and Civil3D model includes a significantly smaller volume based on the previous ACA drainage strategy. Further modelling will be undertaken during Detailed Design to verify the size of the attenuation basin, including allowance for storage in the pipe network. Following this, the CSPP and Civil3D model will be updated accordingly.

Table 3-8 - ACA West - Infiltration Basin Summary

Design Input		Comment
Total catchment area	4.438 ha	
Percentage of runoff	100%	
Volumetric runoff coefficient (Cv)	0.761, 0.817	Summer, winter respectively
Infiltration rate	0 m/s	

Overflow allowance to nearby watercourse	10.53 l/s	Q_{bar}
Overflow to spine network	Yes	Allowance for 200 l/s, not included in model
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	2.100 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	2698.8 m^3	1:100 year return period, 1440 winter storm
FEH 1999	3623.2 m^3	1:100 year return period, 1440 winter storm
FEH 2013	**3812.3 m^3**	1:100 year return period, 1440 winter storm
Civil 3D Model Summary		
Invert level of basin	2.500 mAOD	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**4000 m^3**	Still to be modelled, but this area has been space-proofed for this size basin

3.9 West Railway Catchment 3 - Abbey Road

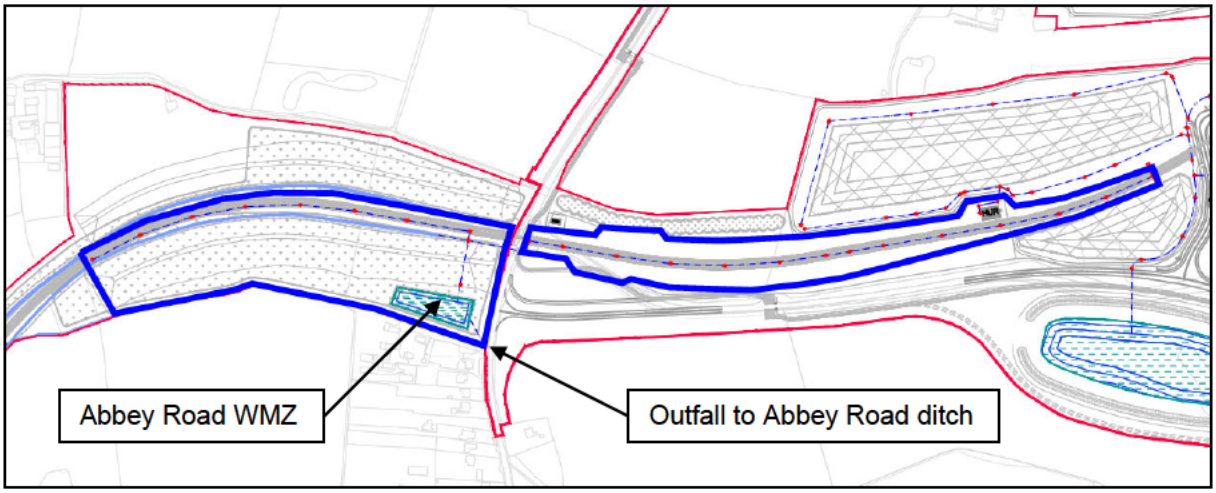
3.9.1 The West Railway Catchment 3 is one of five catchments serving the proposed Green Rail Route, which is located with the Main Development Site. The railway drainage largely relies on infiltration trenches and swales to drain the proposed track in addition to allowing continuity of existing ditches and watercourses.

3.9.2 West Railways Catchment 3 is approximately 6.5 ha and is in cutting with a level crossing at Abbey Road. Cut-off ditches are proposed on both the side of the rail cutting in order to capture the runoff from the landscape bund. A filter drain is proposed at the downside of the embankment to drain the railway runoff. A WMZ basin coupled with hydro-brake is proposed to limit the discharge as required. Runoff that does not infiltrate at source will convey to a WMZ infiltration basin and overflow to the Abbey Road ditch.

3.9.3 Figure 3-8 shows the currently proposed Abbey Road WMZ basin location. This location may be updated in the future to account for emerging flood

modelling information and existing known flooding issues in the vicinity of the current proposed WMZ basin.

Figure 3-8 - West Railway Catchment 3 – Abbey Road WMZ



3.9.4 Abbey Road WMZ

3.9.5 Table 3-9 summarises the parameters used to determine a conservative estimate of the attenuation volume required and the volume space-proofed for the Abbey Road WMZ.

Table 3-9 - Abbey Road WMZ - Infiltration Basin Summary

Design Input		Comment
Total catchment area	6.478 ha	
Percentage of runoff	50%	
Volumetric runoff coefficient (Cv)	0.568, 0.680	Summer, winter respectively
Infiltration rate	1.06E-04 m/s	
Overflow allowance to nearby watercourse	6.50 l/s	Assumed at 1 l/s/ha [1]
Overflow to spine network	No	
Sediment forebay	Included	To be detailed in next design phase
Access ramp	Included	To be detailed in next design phase
Groundwater level	3.000 mAOD	Based on Environment Statement groundwater contours (Annex B)
MicroDrainage Source Control Summary		
FSR	1048.1 m^3	1:100 year return period, 240 winter storm

FEH 1999	**1413.5 m³**	1:100 year return period, 240 winter storm
FEH 2013	1338.8 m³	1:100 year return period, 600 winter storm
Civil 3D Model Summary		
Invert level of basin	6.742 mAOD	
Bottom of basin area	1268.6 m²	
Top of basin area (excluding freeboard)	1964.5 m²	
Freeboard allowance	300mm	
Side slopes	1:3	
Total volume provided	**1872.0 m³**	(excluding 300mm freeboard)

[1] Based on Environment Agency guidance - Rainfall runoff management for developments ref. SC030219. Limiting discharge rates for sites should be set to Qbar or 1 l/s/ha, whichever is greater.

4 SUMMARY

4.1.1 This technical note summarises the required storage volumes for each WMZ attenuation basin across the SZC enabling works site. The volumes calculated are conservative and based on several assumptions. Further hydraulic modelling will be undertaken during Detailed Design which will decrease the required storage volumes. Table 4-1 provides a summary of the worst-case hydraulic model required storage volumes against the volumes currently provided for on the CSPP.

Table 4-1 - Water Management Zone - Infiltration Basin Summary

Design Input	Design Volume (m³) (worst case)	CAD Modelled Volume (m³)	Comment
WMZ1	14690.4	17328	Sufficient volume provided
WMZ2	12663.5	17694.5	Sufficient volume provided
WMZ3	15685.8	17341	Sufficient volume provided
WMZ4	13422.3	25688.8	Sufficient volume provided
WMZ5	12891.1	17223.8	Sufficient volume provided
WMZ6	20216.7	19376	Sufficient volume provided [3]
WMZ – ACA west	3812.3	4000	[1],[2] Sufficient volume provided

WMZ – ACA east	21641.3	22000	[1],[2] Sufficient volume provided
WMZ – Abbey Road	1413.5	1872	Sufficient volume provided

[1] Construction site plot plan is being updated to include additional volume as necessary to account for updated discharge strategy at the ACA in accordance with recent discussions with the EA and SCC.

[2] All WMZ infiltration basins have been sized based on source control models which do not consider additional storage volume in the network. Sizing the basins in this way allows space allocation on the plot plan, so that basin volumes and footprints can likely be downsized in the next design phase.

[3] Additional storage is provided in the Type 3 subbase of the permeable paving within the carpark of the plaza to provide the required design volume.

REFERENCES

1. Outline Drainage Strategy at Volume 2, Chapter 2, Appendix 2A of the Environmental Statement [APP-181]

2. Environment Agency – Climate change allowances, Table 2. Flood risk assessments: climate change allowances - GOV.UK (www.gov.uk)

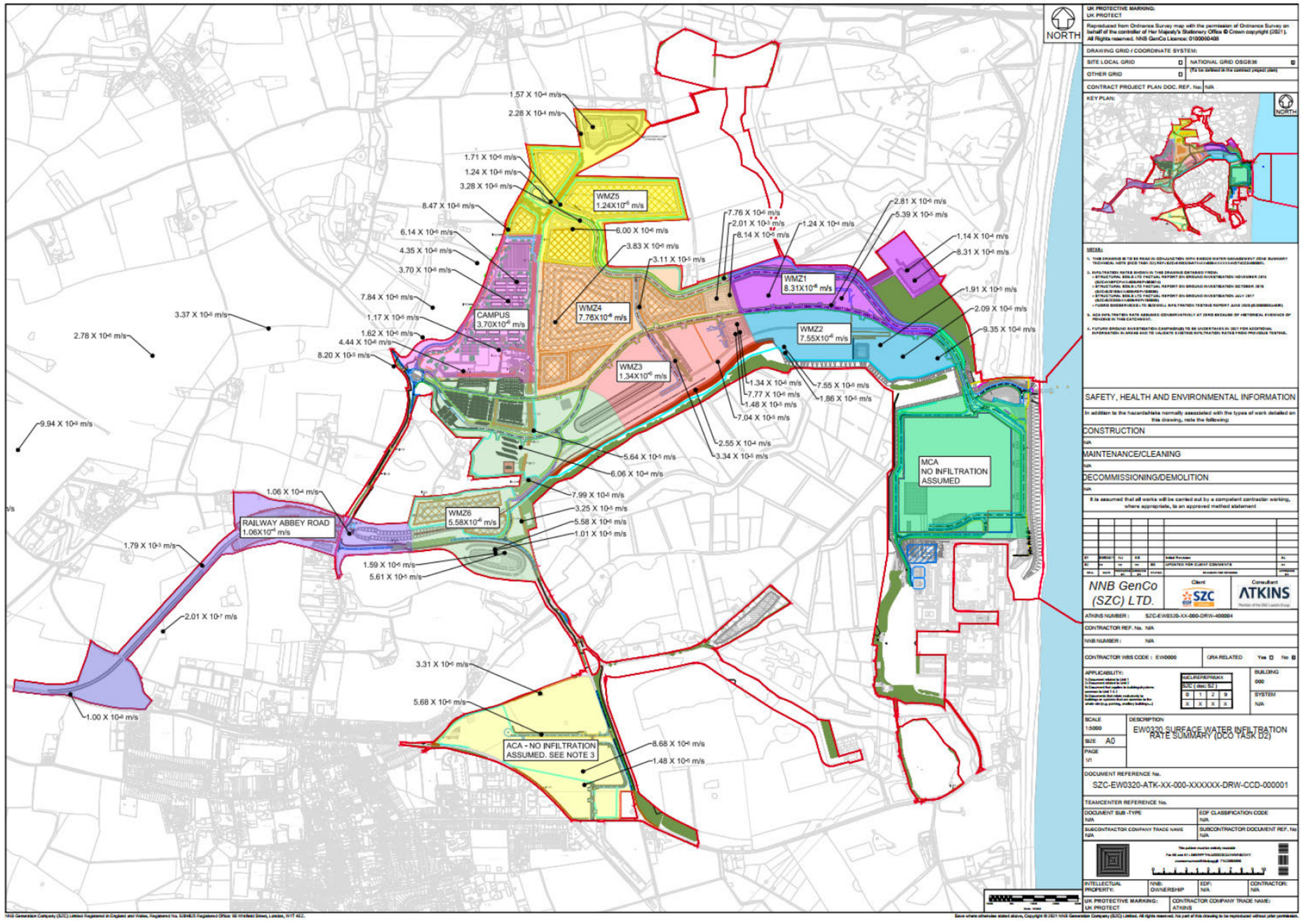
3. CIRIA - The SuDS Manual 2015. CIRIA C753

4. Fugro - Sizewell C Infiltration Testing Report on Ground Investigation without Geotechnical Evaluation. G200003U_GIR Rev 02

5. Environment Agency - Rainfall Runoff Management for Development. SC030219

ANNEX A

Infiltration Tests Summary Drawing


NORTH
WMZ5
1.24X10⁻⁶ m/s
WMZ4
7.76X10⁻⁶ m/s
CAMPUS
3.70X10⁻⁶ m/s
WMZ3
1.34X10⁻⁶ m/s
WMZ2
7.55X10⁻⁶ m/s
WMZ1
8.31X10⁻⁶ m/s
WMZ6
5.58X10⁻⁶ m/s
RAILWAY ABBEY ROAD
1.06X10⁻⁴ m/s
MCA
NO INFILTRATION
ASSUMED
ACA - NO INFILTRATION
ASSUMED. SEE NOTE 3
1.57 X 10⁻⁴ m/s
2.28 X 10⁻⁴ m/s
1.71 X 10⁻⁶ m/s
1.24 X 10⁻⁶ m/s
3.28 X 10⁻⁶ m/s
8.47 X 10⁻⁶ m/s
6.14 X 10⁻⁶ m/s
4.35 X 10⁻⁶ m/s
3.70 X 10⁻⁶ m/s
6.00 X 10⁻⁶ m/s
3.83 X 10⁻⁶ m/s
3.11 X 10⁻⁵ m/s
7.84 X 10⁻⁶ m/s
1.17 X 10⁻⁵ m/s
1.62 X 10⁻⁵ m/s
4.44 X 10⁻⁴ m/s
8.20 X 10⁻⁵ m/s
3.37 X 10⁻⁵ m/s
2.78 X 10⁻⁶ m/s
9.94 X 10⁻⁹ m/s
7.76 X 10⁻⁶ m/s
2.01 X 10⁻⁵ m/s
8.14 X 10⁻⁶ m/s
1.24 X 10⁻⁴ m/s
2.81 X 10⁻⁶ m/s
5.39 X 10⁻⁵ m/s
1.14 X 10⁻⁴ m/s
8.31 X 10⁻⁵ m/s
1.91 X 10⁻⁵ m/s
2.09 X 10⁻⁵ m/s
9.35 X 10⁻⁶ m/s
1.34 X 10⁻⁵ m/s
7.77 X 10⁻⁶ m/s
1.48 X 10⁻⁵ m/s
7.04 X 10⁻⁵ m/s
7.55 X 10⁻⁶ m/s
1.86 X 10⁻⁵ m/s
2.55 X 10⁻⁴ m/s
3.34 X 10⁻⁵ m/s
5.64 X 10⁻⁵ m/s
6.06 X 10⁻⁴ m/s
7.99 X 10⁻⁵ m/s
3.25 X 10⁻⁵ m/s
5.58 X 10⁻⁶ m/s
1.01 X 10⁻⁵ m/s
1.06 X 10⁻⁴ m/s
1.79 X 10⁻³ m/s
2.01 X 10⁻⁷ m/s
1.00 X 10⁻⁸ m/s
1.59 X 10⁻⁵ m/s
5.61 X 10⁻⁵ m/s
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5.68 X 10⁻⁵ m/s
8.68 X 10⁻⁵ m/s
1.48 X 10⁻⁵ m/s
UK PROTECTIVE MARKING:
UK PROTECT
DRAWING GRID / COORDINATE SYSTEM:
SITE LOCAL GRID
NATIONAL GRID OSGB36
OTHER GRID
CONTRACT PROJECT PLAN DOC. REF. No: N/A
KEY PLAN:
NOTES:
SAFETY, HEALTH AND ENVIRONMENTAL INFORMATION
In addition to the hazards/risks normally associated with the types of work detailed on this drawing, note the following:
CONSTRUCTION
N/A
MAINTENANCE/CLEANING
N/A
DECOMMISSIONING/DEMOLITION
N/A
It is assumed that all works will be carried out by a competent contractor working, where appropriate, to an approved method statement
NNB GenCo (SZC) LTD.
Client
Consultant
ATKINS
ATKINS NUMBER : SZC-EW0320-XX-000-DRW-400004
CONTRACTOR REF. No. N/A
NNB NUMBER : N/A
CONTRACTOR WBS CODE : EW0000
CDM RELATED Yes No
APPLICABILITY:
SCALE 1:5000
SIZE A0
PAGE 1/1
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DOCUMENT REFERENCE No.
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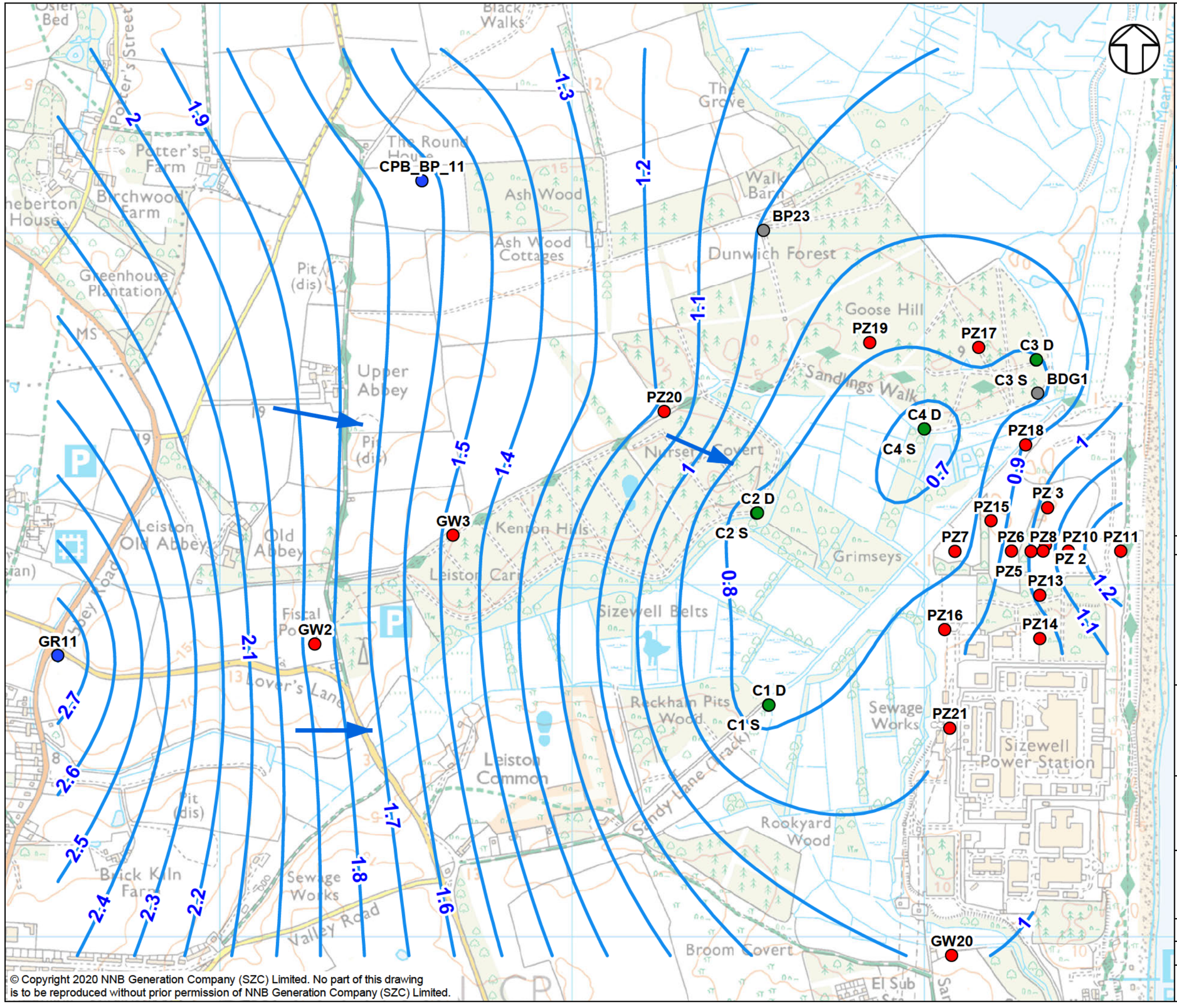
TEAMCENTER REFERENCE No.
DOCUMENT SUB -TYPE N/A
EDF CLASSIFICATION CODE N/A
SUBCONTRACTOR COMPANY TRADE NAME N/A
SUBCONTRACTOR DOCUMENT REF. No N/A
INTELLECTUAL PROPERTY:
NNB OWNERSHIP
EDF: N/A
CONTRACTOR: N/A
UK PROTECTIVE MARKING: UK PROTECT
CONTRACTOR COMPANY TRADE NAME: ATKINS

ANNEX B

Infiltration Tests Summary Drawing



NOTES

PEAT CONTOURS ARE CONSTRAINED TO THE EXTENT OF THE PEAT DEPOSITS

KEY

- 2010 BOREHOLES
- 2013 BOREHOLES
- 2014 BOREHOLES
- 2015 BOREHOLES
- GROUNDWATER CRAG CONTOURS (MAOD) - WINTER 2018
- GROUNDWATER FLOW DIRECTION

NOT PROTECTIVELY MARKED

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Project Title:
SIZEWELL C PROJECT
ENVIRONMENTAL STATEMENT
VOLUME 2
CHAPTER 19B1
GROUNDWATER AND SURFACE WATER APPENDIX B1

DRAWING TITLE:
GROUNDWATER CONTOURS IN CRAG AQUIFER DURING WINTER 20 8 (9 2 2018)

DRAWING NO:
FIGURE 19B 1.16

DATE:	DRAWN:	SCALE :
JAN 2020	S.R.H	1:10,103 @A3

SCALE BAR
0 0.1 0.2 0.3 0.4 0.5 KM

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ANNEX C

Figure 1 – Water Management Zone 1 Basin

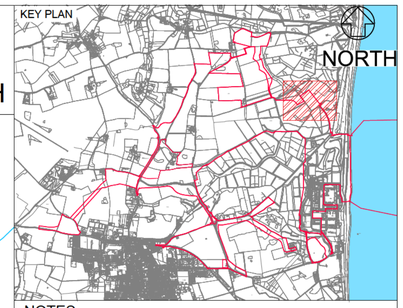
Figure 2 – Water Management Zones 3 and 4 Basins

LEGEND:

- PROJECT BOUNDARY
- WATER MANAGEMENT ZONE BASIN
- RETAINED VEGETATION
- MAJOR CONTOUR
- MINOR CONTOUR
- PIPE NETWORK
- POND TOP
- ORIGINAL WMZ BASIN BOUNDARY
- NATTERJACK TOADS
- 10 METER BUFFER
- EXISTING NATTERJACK TOAD PONDS
- APPROXIMATE EXTENT OF RABBIT WARREN BOUNDARY
- NATTERJACK TOAD HIBERNATION PERIMETER FENCELINE
- EXISTING GROUND
- MAXIMUM WATER LEVEL
- PROPOSED GROUND
- PERMEABLE GEOTEXTILE
- GRANULAR FILL
- COMPACTED SITE WON FILL

NORTH

KEY PLAN



NOTES:

1. ALL DIMENSIONS ARE IN MILLIMETRES UNLESS OTHERWISE STATED.

REFERENCES:

1. SZC_MDS_RABBIT WARREN INFO

NATTERJACK TOAD HIBERNATION PERIMETER FENCELINE

ORIGINAL WMZ1 BASIN BOUNDARY

HAY BALE BARRIER STRUCTURE AND SILT FENCE TO BE LOCATED AT BASE OF SLOPE

WMZ1 BASIN RESHAPED TO ALIGN WITH ENVIRONMENTAL / ECOLOGICAL ASSESSMENT

EXISTING GROUND TO BE BUILT UP TO ALLOW FALL INTO WMZ1 BASIN

MAINTENANCE ACCESS ROAD

BUND WITH CREST LEVEL AT 4.0m AOD

OVERFLOW PIPE DISCHARGING TO NEARBY LOCAL WATERCOURSE AT GREENFIELD RUNOFF RATES

WMZ 1 BASIN

Ponds

Drain

Pond

FB

Goose Hill

REVISION	DATE	DRAWN	CHECKED	REASONS FOR REVISION / COMMENTS	APPROVED
01	JULY 2021	SN	RV	DCO SUBMISSION	SZC Co

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PROJECT:
SIZEWELL C

DOCUMENT:
MAIN DEVELOPMENT SITE
WATER MANAGEMENT ZONE SUMMARY
ANNEX C
DEADLINE 5 SUBMISSION JULY 2021

DRAWING TITLE:
WATER MANAGEMENT ZONE 1
DESIGN UPDATE - PLAN

FIGURE NO:	REVISION:
FIGURE 1	01

DATE:	DRAWN:	SCALE:
JULY 2021	SN	1:1000

SCALE BAR:

10m 0m 10m 20m 30m 40m 50m 60m 70m

Scale 1:1000

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NORTH

Track

Ash Wood Cottages

Ash Wood Cottages

MAINTENANCE ACCESS ROAD

RETAINED VEGETATION

WMZ4 BASIN RESHAPED TO ALIGN WITH ENVIRONMENTAL / ECOLOGICAL ASSESSMENT

WMZ 4 BASIN

WMZ3 BASIN RESHAPED TO ALIGN WITH ENVIRONMENTAL / ECOLOGICAL ASSESSMENT

ORIGINAL WMZ4 BASIN BOUNDARY

ORIGINAL WMZ3 BASIN BOUNDARY

PROPOSED VEGETATION

FENCE

REFER NOTE 2 FOR COMPOUND ACCESS POINTS

WMZ 3 BASIN

Turn Pits

LEGEND:

- PROJECT BOUNDARY
- WATER MANAGEMENT ZONE BASIN
- EXISTING VEGETATION
- PROPOSED VEGETATION
- PROPOSED BUILDINGS
- PIPE NETWORK
- POND TOP
- ORIGINAL WMZ BASIN BOUNDARY
- PROPOSED STOCKPILE
- ACOUSTIC FENCE
- FENCE
- BUND

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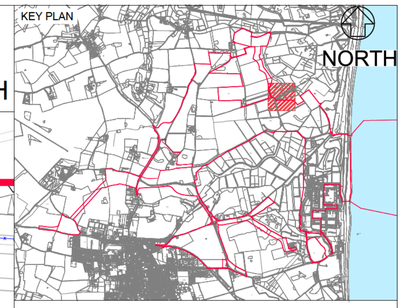
KEY PLAN



NOTES:

1. ALL DIMENSIONS ARE IN MILLIMETRES UNLESS OTHERWISE STATED.
2. COMPOUND ACCESS POINTS TO BE UPDATED IN THE NEXT DESIGN PHASE.

REVISION	DATE	DRAWN	CHECKED	REASONS FOR REVISION / COMMENTS	APPROVED
01	JULY 2021	SN	RV	DCO SUBMISSION	SZC Co

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PROJECT:
SIZEWELL C

DOCUMENT:
MAIN DEVELOPMENT SITE
WATER MANAGEMENT ZONE SUMMARY
ANNEX C
DEADLINE 5 SUBMISSION JULY 2021

DRAWING TITLE:
WATER MANAGEMENT ZONE 3 &4
DESIGN UPDATE PLAN LAYOUT

FIGURE NO:	REVISION:
FIGURE 2	01

DATE:	DRAWN:	SCALE:
JULY 2021	SN	1:1000

SCALE BAR:

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Scale 1:1000

APPENDIX E

TEMPORARY MARINE OUTFALL OPERATION SUMMARY (DCO TASK D3)

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1 INTRODUCTION 3
1.2 Background 3
1.3 Existing Site 5
2 SURFACE WATER MANAGEMENT 8
2.1 Overview 8
2.2 Surface Water Discharge 9
2.3 Temporary Marine Outfall 11
3 SUMMARY 13

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Figure 1-3 - Existing Site (left) with transparent construction site overlay (right) 6
Figure 1-4 - Existing Site Contours 7
Figure 2-1 - Approximate surface water catchment area 8
Figure 2-2 - Schematic showing proposed discharges 10
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Figure 2-5 - Indicative section discharge pipe from MCA to outfall 13

1 INTRODUCTION

1.1.1 This document provides a summary of the proposal to discharge surface water as a precautionary principle via a temporary outfall to the sea prior to the completion of the Sizewell C (SZC) Combined Drainage Outfall (CDO). The temporary outfall will be used as a redundancy feature as a back up to the surface water proposals that follow standard sustainable drainage (SuDS) guidance. This note describes why the temporary marine outfall is required and under what circumstances it will be used.

1.2 Background

1.2.1 The Sizewell C Main Development Site (MDS) contains the Sizewell Marshes Site of Special Scientific Interest (SSSI), which is an environmentally sensitive marshland and contains a watercourse known as the Leiston Drain and the Sizewell Drain. The Sizewell Drain runs diagonally across the north-west corner of the Sizewell C Main Construction Area (MCA), before joining the Leiston Drain (shown in Figure 1-1). The watercourse heads north approximately 1.7km towards the Minsmere Sluice before discharging to the sea via a level controlling structure.

1.2.2 The Sizewell Drain needs to be realigned to pass along the western edge of the proposed MCA and connect to the Leiston Drain. Figure 1-2 shows the indicative alignment of the realigned Sizewell Drain. During construction of the MDS and prior to the completion of the CDO, management of surface water run-off and discharge is required to prevent flooding of the site and any adverse effects on the nearby ecology.

Figure 1-1- Existing Leiston and Sizewell Drains – Extract from SZC Water Framework Directive Compliance Assessment Report Part 2 Figure 2.7

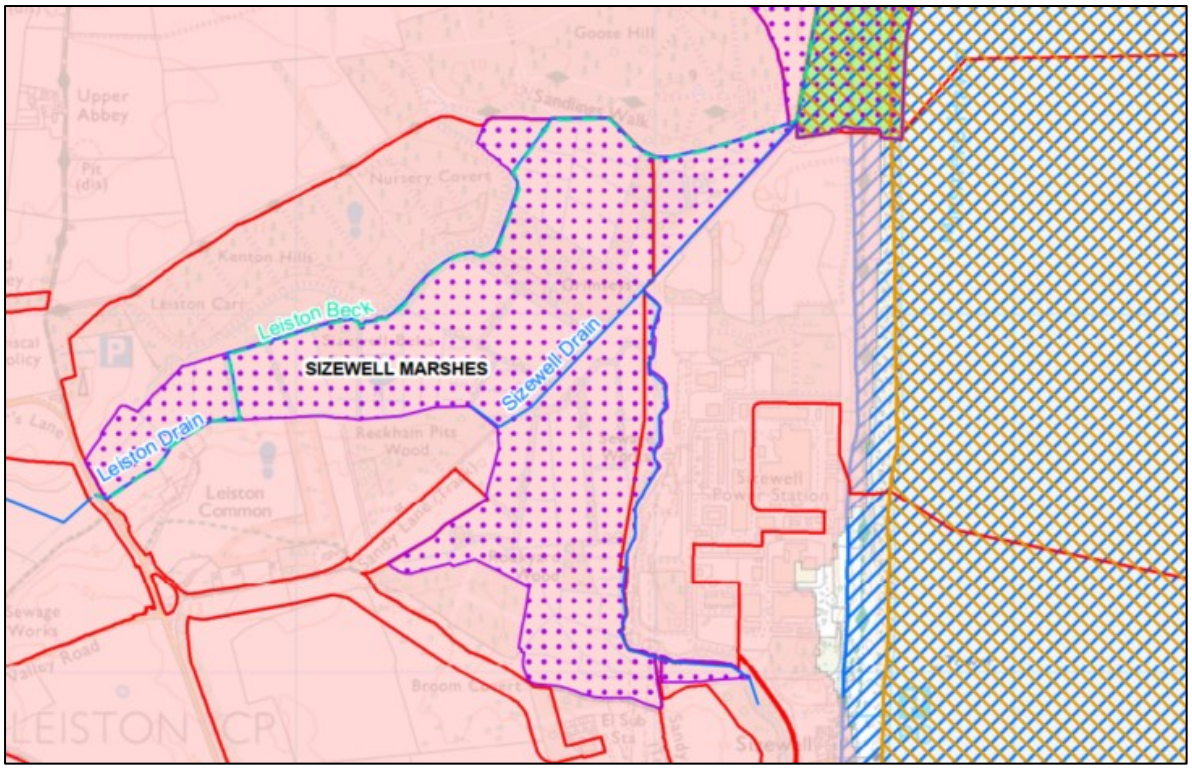
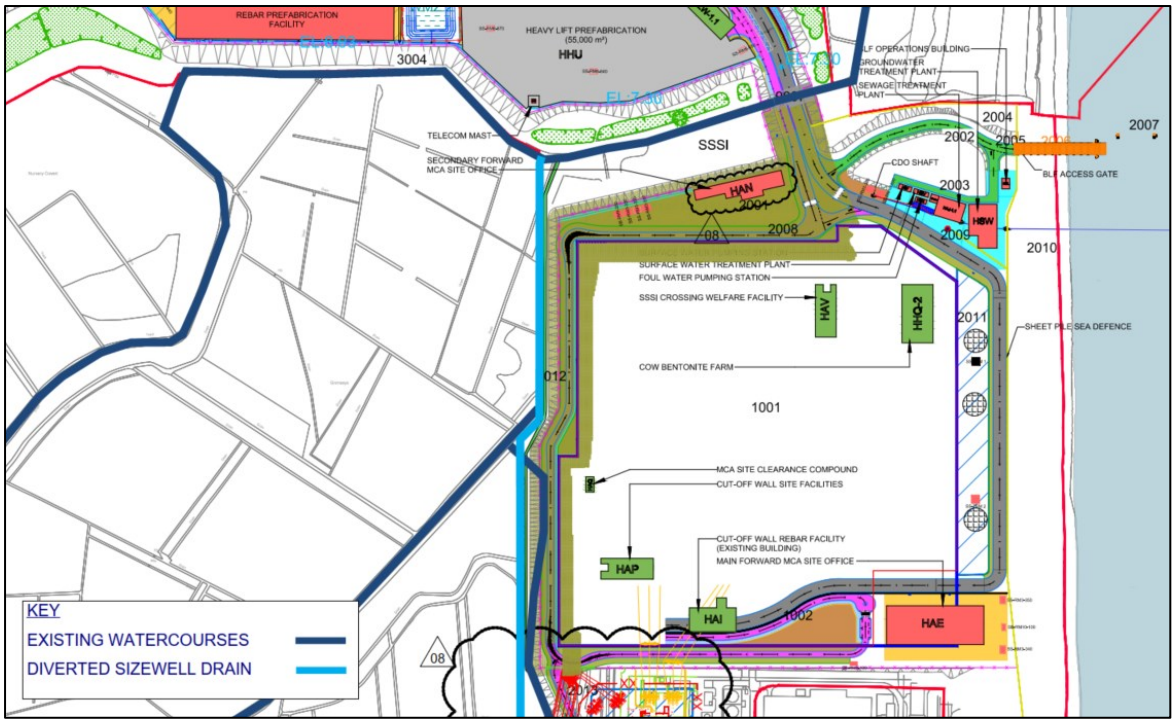


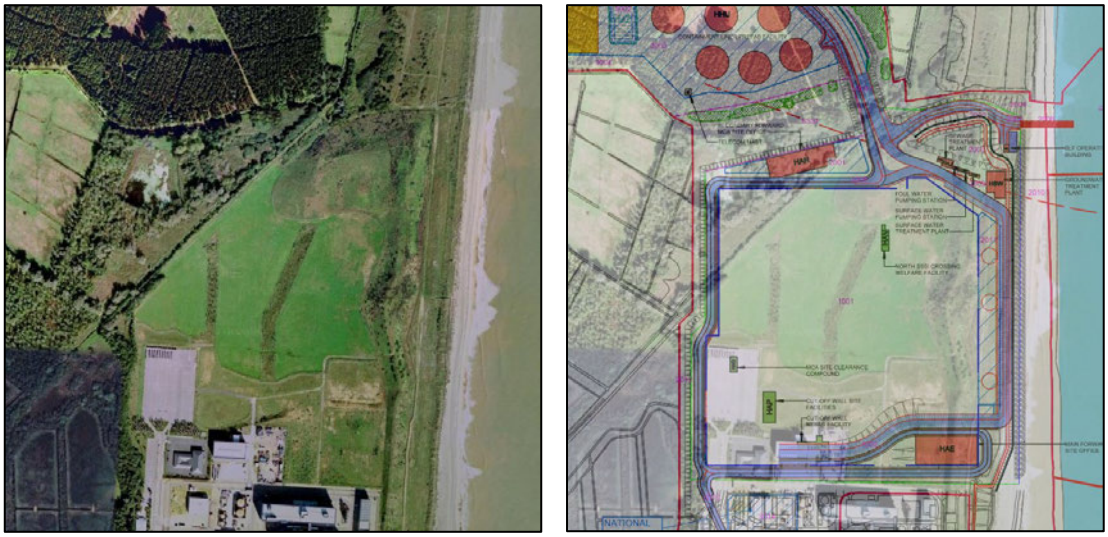
Figure 1-2 - Indicative Surface Watercourses – Existing and Diverted Sizewell Drain



1.3 Existing Site

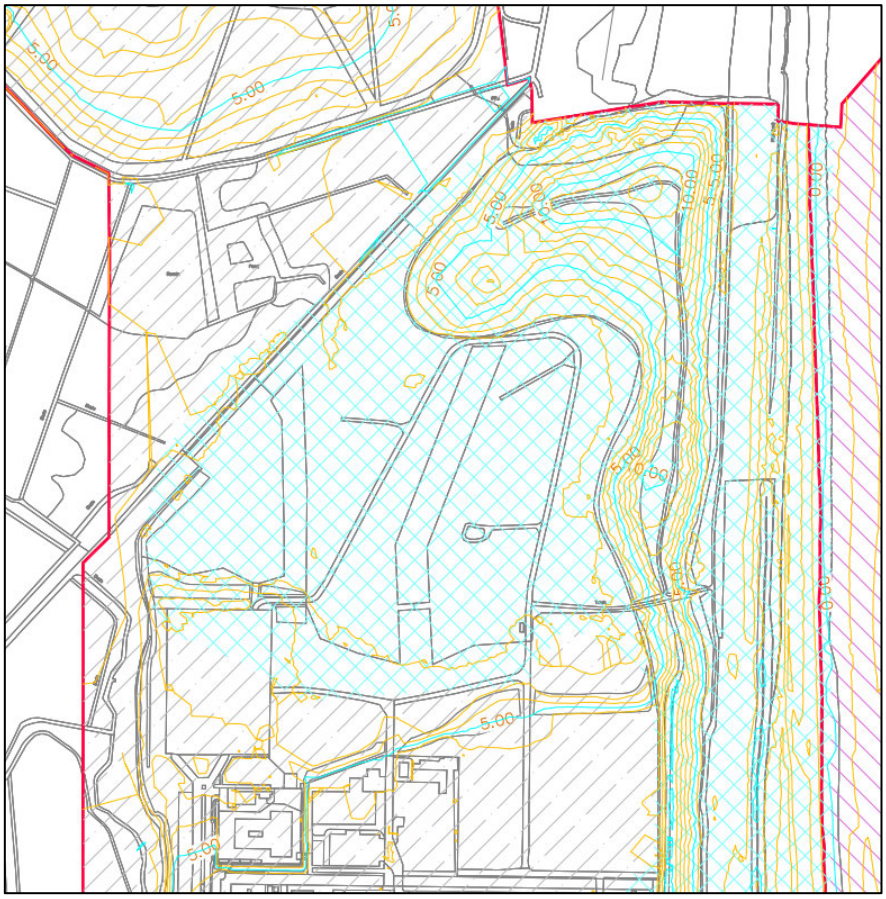
1.3.1 The existing site is largely grassland. The section of the MCA to the north-west of the Sizewell Drain makes up part of the SSSI. The area to the south and east of the Sizewell Drain includes grassland as well as some buildings and hardstanding. Figure 1-3 shows an aerial photograph of the existing site as well as a proposed construction site overlay.

Figure 1-3 - Existing Site (left) with transparent construction site overlay (right)



1.3.2 All levels given in this Technical note are designed finished levels including the existing site drains by a combination of infiltration as well as overland flow towards the Sizewell Drain. The existing site contours are shown in Figure 1-4.

Figure 1-4 - Existing Site Contours



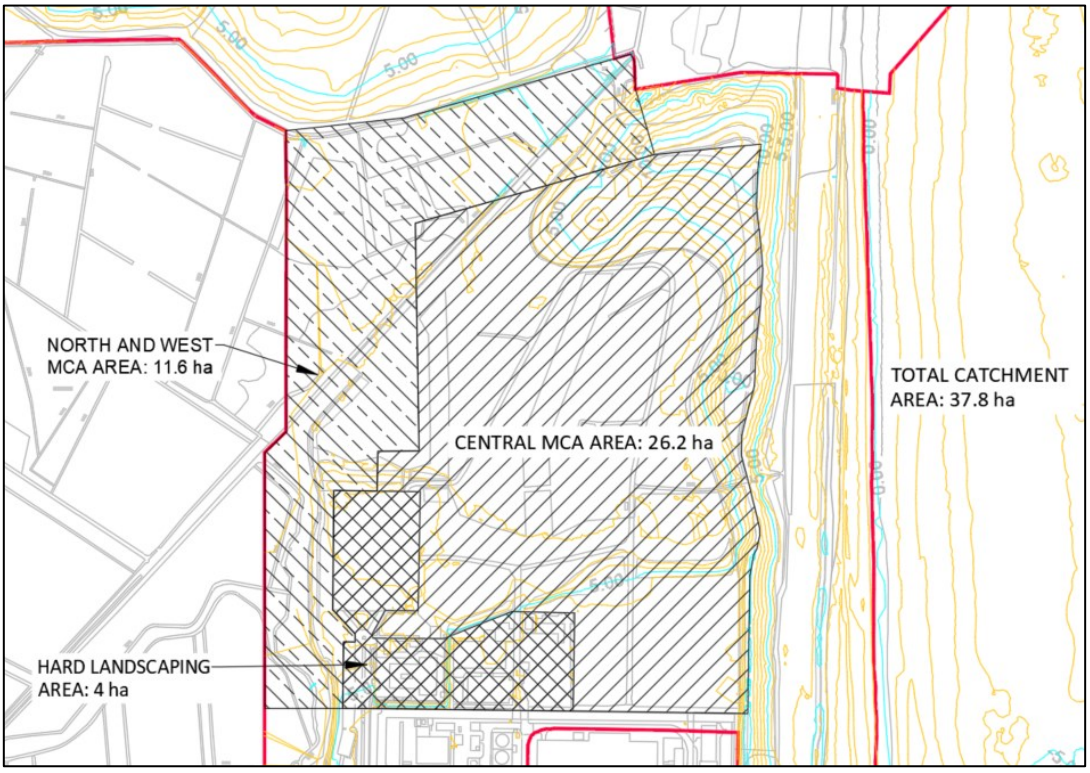
2 SURFACE WATER MANAGEMENT

2.1 Overview

2.1.1 When construction commences on the MDS, surface water must be managed so that a storm event with a return period of 1:100 years including an allowance for 20% climate change does not leave the site. Surface water will be captured and retained on site so that it can be treated and then discharged either through infiltration or to a suitable location at pre-agreed flow rates.

2.1.2 The approximate catchment shown in Figure 2-1 needs to be allowed for in the early surface water management proposals for the MCA when earthworks commence on site.

Figure 2-1 - Approximate surface water catchment area



2.1.3 The collection of surface water across the MCA will be designed to suit the sequence of construction events. Surface water will be collected and held in temporary attenuation ponds within the MCA, before being treated using proprietary devices if required.

2.1.4 Similarly, surface water runoff within the Temporary Construction Area (TCA), north of the Sizewell Marshes SSSI, will be collected, attenuated,

treated, and discharged to ground or local watercourses under normal conditions.

2.2 Surface Water Discharge

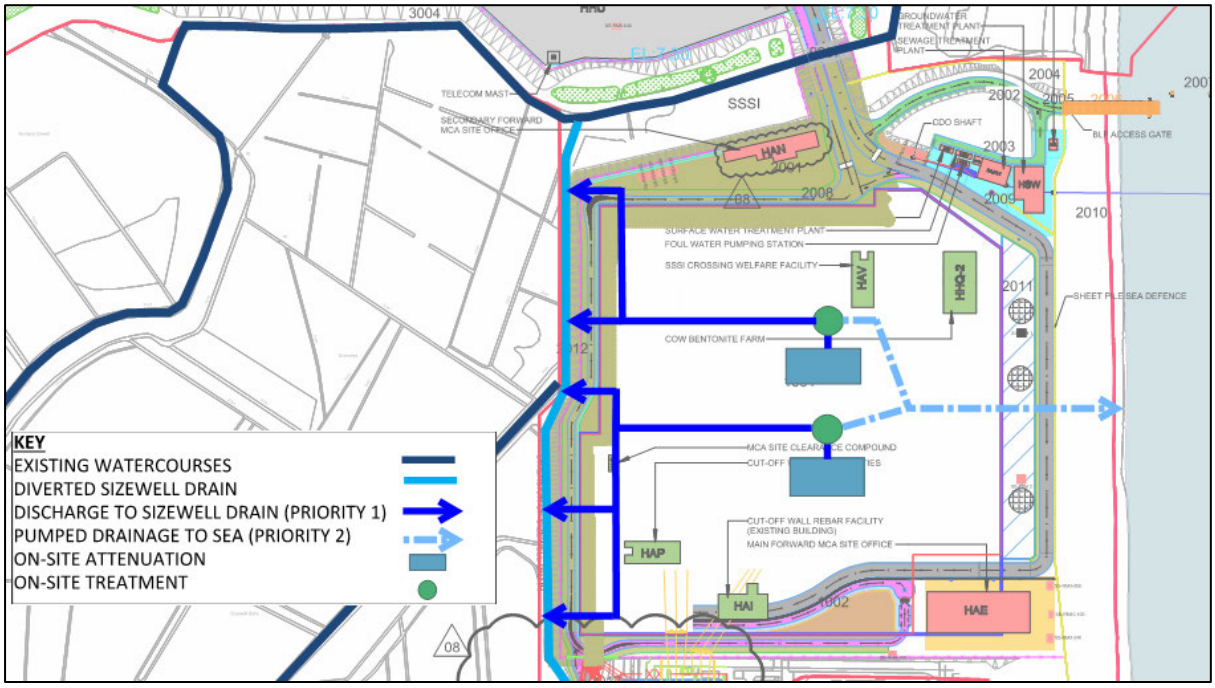
2.2.1 It is important to mimic existing conditions on the site to ensure the SSSI water levels, including ground water, are not affected by the construction works. This means surface water will discharge primarily via infiltration, using temporary infiltration ponds and other Sustainable Drainage (SuDS) features where possible.

2.2.2 Temporary infiltration ponds within the MCA will have outfalls discharging to the Sizewell Drain if infiltration alone is not sufficient to discharge surface water. The outfall locations are yet to be confirmed with the Internal Drainage Board (IDB), who are being engaged with to ensure that a discharge regime as close to existing conditions as possible is constructed. This may mean multiple discharges along the length of the existing Sizewell Drain, or on the new alignment once it has been realigned.

2.2.3 The surface water discharges to the Sizewell Drain will be restricted to greenfield runoff rates in accordance with Environment Agency (EA) guidance. The discharges will need to be permitted through a land drainage consent, with continuous monitoring to ensure flow rates do not exceed the permitted rates, and water quality meets the required treatment levels.

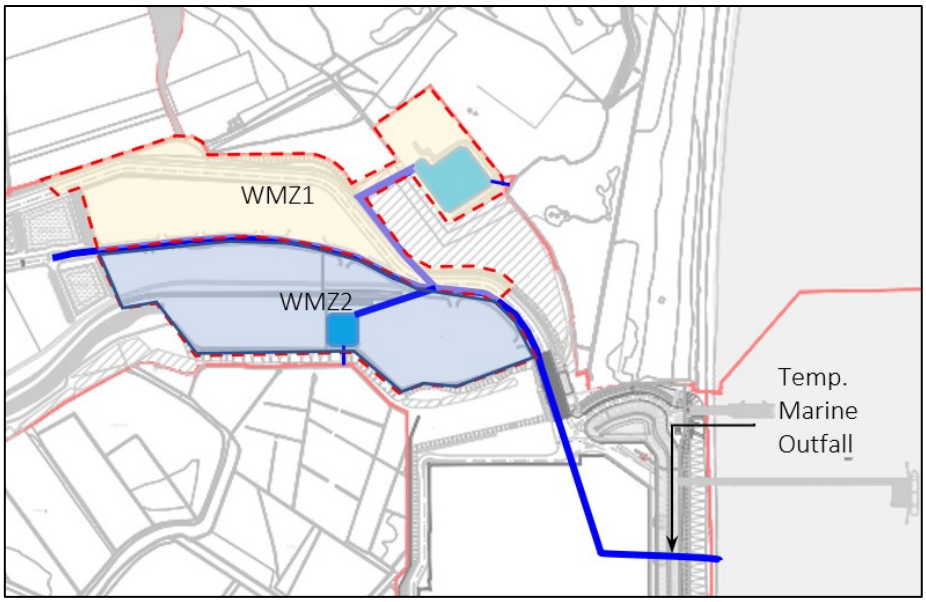
2.2.4 The Sizewell Marshes (including the Sizewell Drain) are known to flood occasionally due to either extreme rainfall events or other external factors, such as the Leiston Drain downstream being blocked or the Minsmere sluice inhibiting surface water flow to sea. In these scenarios, the Sizewell drain overtops and the low-lying areas in the SSSI become inundated with surface water. If a rainfall event occurs on the MDS while the SSSI is inundated with water, surface water runoff will be captured and attenuated in temporary infiltration ponds. However, discharging to the backed-up Sizewell Drain in these conditions is not considered suitable, even if restricted to greenfield runoff rates. In this scenario, another option for discharging surface water should be considered, and therefore a temporary marine outfall has been proposed which would discharge to sea, acting as a ‘release valve’. An indication of how surface water will be discharged from the MCA is shown in Figure 2-2. The temporary marine outfall is further described in the following section.

Figure 2-2 - Schematic showing proposed discharges



2.2.5 Attenuated surface water runoff from catchments within the TCA will be discharged to the Leiston Drain at various locations if infiltration alone is not sufficient to discharge surface water. However, during the early months of site establishment of Water Management Zone (WMZ) 1 and WMZ2 when the CDO is under construction, if the site is subject to an extreme storm or inundated locally with surface water, the temporary marine outfall will be used to discharge surface water to sea. An above ground pumped network would convey surface water towards the MCA, across the SSSI and out to the sea via the temporary marine outfall, as indicated in Figure 2-3.

Figure 2-3 - Possible TCA Catchments Discharging via the Temporary Marine Outfall



2.3 Temporary Marine Outfall

2.3.1 The temporary marine outfall is proposed to be installed early in the construction programme, as a redundancy measure or a precautionary principle for discharging surface water to sea, prior to the CDO being installed. The CDO is programmed to be commissioned by 19 April 2023 as per SZC-IWS Enabling Works Construction Schedule, after which the temporary marine outfall will be removed. For a 15 month period, the temporary marine outfall would principally be used where factors external to the MDS that are out of the control of SZC result in the Sizewell Drain being unsuitable to discharge to, for example, flooding on site caused by offsite flood conditions.

2.3.2 **Permitting, Operation, and Usage**

2.3.3 All outfalls to the SSSI as well as the sea will be controlled through conditions imposed through the permit application procedure with the EA. This permit will be applied for in the future through the EA. The conditions from the EA may stipulate a suitable water level within the SSSI that must be reached before the temporary marine outfall can be used. Similarly, there may be a level defined by the permit conditions where the marine outfall must be switched off and discharge is returned to the SSSI for recharge of surface and groundwater. The pump may also need to be used in other exceptional events such as if water level in and around the site present a risk to health and safety.

2.3.4 Further to the above, water quality levels will be stipulated in the permitting conditions that must be met prior to discharge to sea.

2.3.5 **Proposed Arrangement**

2.3.6 The temporary marine outfall would include a pump, or series of pumps, from the MDS and discharge to a gravity pipe that would discharge to sea at mean high water springs (MHWS) level. The pressurised pipework would be installed above ground where possible however it may need to be laid below ground in places, for example, across the Suffolk Coast Path. The pipework may be restrained using hoop rings or similar, and consideration will be made to ensure the Suffolk Coastal Path remains unobstructed.

2.3.7 The proposed outfall location is shown indicatively in Figure 2-4 and Figure 2-5. It is likely the shoreline will require local erosion protection measures in the form of sandbags or other suitable protection and need to be monitored for scour issues.

Figure 2-4 - Proposed outfall location

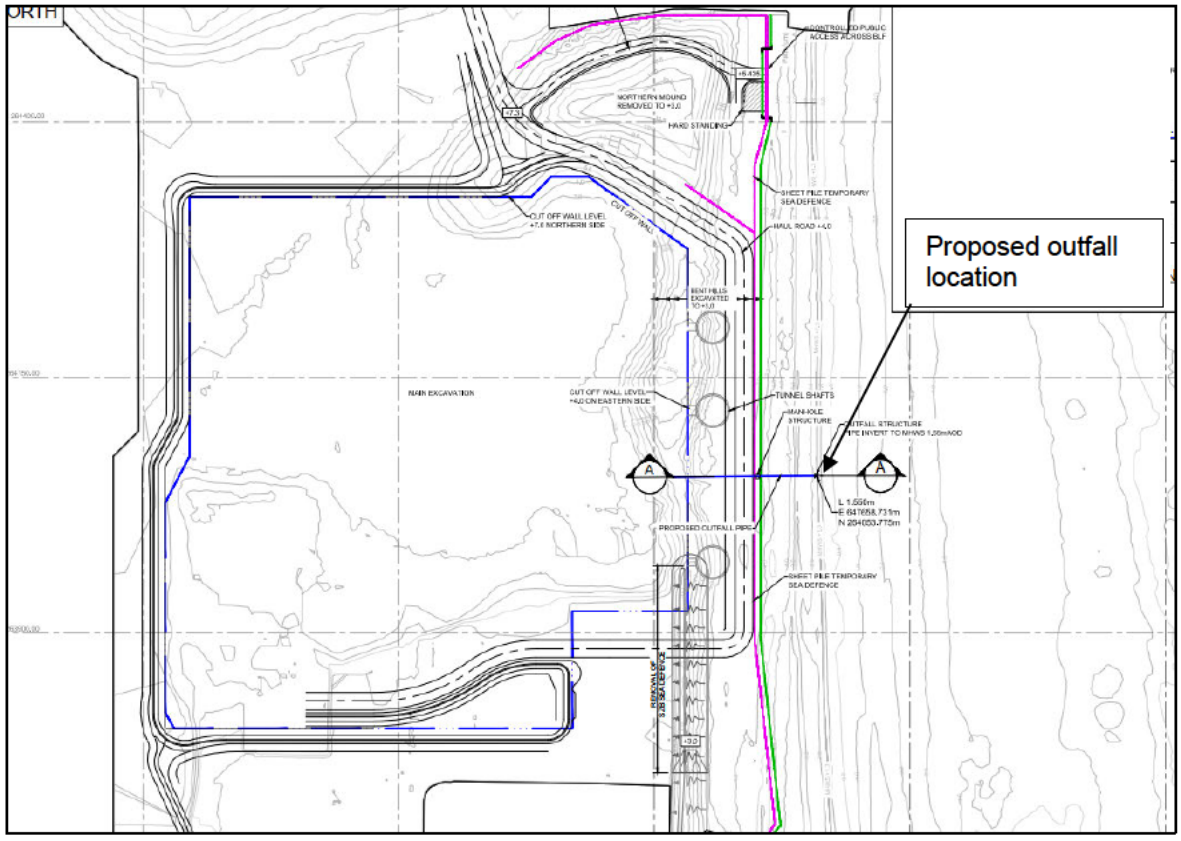
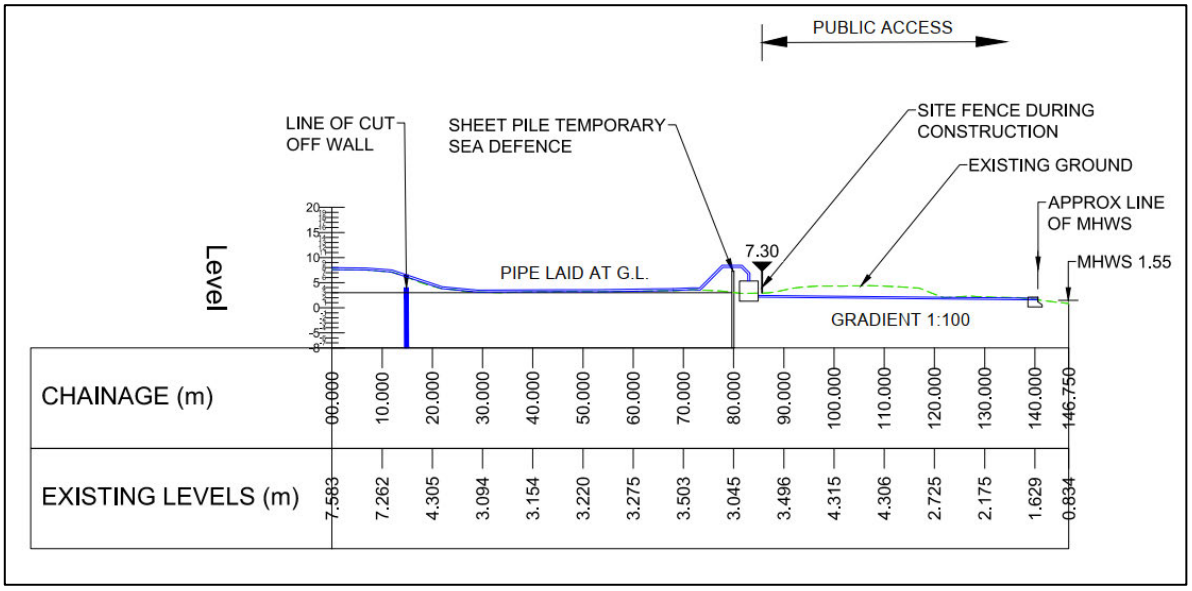


Figure 2-5 - Indicative section discharge pipe from MCA to outfall



3 SUMMARY

3.1.1 A temporary marine outfall is required prior to the installation of the CDO, to provide redundancy as a precautionary principle for discharging surface water from the MDS, if external factors mean that the Sizewell Drain is not suitable to discharge to. The outfall will be available to use for approximately 15 months, after which will be removed once the CDO is commissioned. The frequency of use depends on how these external factors coincide with rainfall events on the MDS. Further factors that may influence the use include maintenance of the Leiston Drain downstream, or surface water flooding in and around the site resulting in health and safety issues.

3.1.2 The use of the outfall would not have a significant impact on the input for surface water into the Sizewell Marshes SSSI as it would be used only when there was excess water in the SSSI. The outfall may never be used and will only be installed as a precautionary measure, to ensure that the SSSI is protected and that the construction site is still able to be operational in situations where external uncontrollable factors impact on the MDS.

3.1.3 The outfall will be controlled through conditions set by the EA under a construction water discharge activity permit.

APPENDIX F

SIZEWELL LINK ROAD PRELIMINARY DRAINAGE DESIGN NOTE

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3 DESCRIPTION OF DCO DRAINAGE CONCEPT DESIGN 3

4 ADDITIONAL INPUT DATA 8

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FIGURES

None provided.

APPENDICES

None provided.

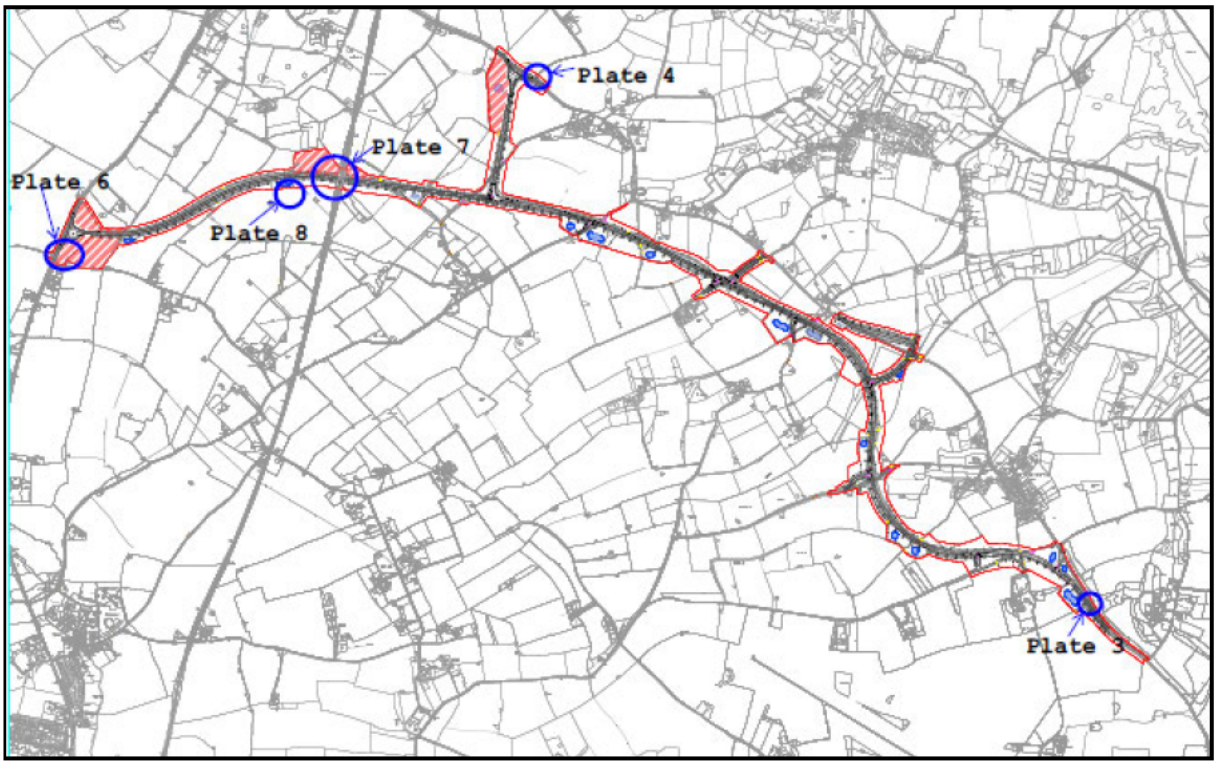
1 INTRODUCTION

1.1.1 NNB Generation Company (SZC) Limited (SZC Co.) submitted an application for a Development Consent Order (DCO) to the Planning Inspectorate under the Planning Act 2008 for the Sizewell C Project (referred to as the 'Application') in May 2020. The Application was accepted for examination in June 2020.

1.1.2 SZC Co. has undertaken work to validate and develop the design of the Sizewell link road that was originally submitted as part of the DCO application. This document forms one of a series of design validation and evolution documents being provided to the Examining Authority in support of the **Outline Drainage Strategy** [REP2-033].

1.1.3 The proposed development is one of the Sizewell C Project's associated development sites; a permanent single carriageway road that would run 6.8km from the A12 just south of Yoxford in an easterly direction, joining the B1122 south of the town of Theberton. A large-scale plan showing the route of Sizewell link road is shown in **Plate 1.** The specific locations shown in subsequent plates are identified for convenience.

Plate 1: Sizewell link road location and route



1.1.4 The Sizewell link road would create a new route around the south of the villages of Yoxford, Middleton Moor and Theberton, helping to reduce the amount of traffic on the B1122 during the peak construction phase of the Sizewell C Project.

1.1.5 The Sizewell link road will be designed to Suffolk County Council's (SCC) adoptable standards (Ref. 1).

1.1.6 The Sizewell link road will generate highway surface water runoff which will require to be removed, treated as necessary and disposed at a controlled rate of discharge.

1.1.7 The Sizewell link road will cross six watercourses at seven locations. Three local field ditch crossings have also been identified following a site visit in January 2021.

2 PURPOSE

2.1.1 The **Outline Drainage Strategy** [REP2-033] identified at concept level the proposed drainage approach required for:

- The effective removal of runoff from the proposed Sizewell link road highway and its disposal;
- The crossing of watercourses along the line of the Sizewell link road.

2.1.2 This strategy was developed in consultation with drainage regulators and local authorities, including SCC and the Environment Agency (EA). A number of workshops were held and the observations/requirements of drainage regulators were incorporated in the strategy.

2.1.3 The proposed drainage infrastructure was described in the concept drainage design submitted as part of the DCO application. This concept design was based on data and information available at that time. The design was supported by the submission of the **Sizewell Link Road Flood Risk Assessment** (FRA) [APP-136].

2.1.4 SZC Co. has subsequently developed the concept design to preliminary design stage. SZC Co. has also developed and updated the FRA with the submission of the **Sizewell Link Road FRA Addendum** [REP2-026].

2.1.5 The purpose of this technical note is to provide details of how the concept design has been modified in response to the new data, such that it continues to provide for the effective and satisfactory drainage of Sizewell link road, without unacceptable adverse impact on the water environment, both in terms of flood risk and pollution.

2.1.6 The content of this technical note summarises the design details and approach already shared in a series of design review meetings held with key stakeholders, including the EA and SCC.

3 DESCRIPTION OF DCO DRAINAGE CONCEPT DESIGN

3.1.1 The basic proposals for watercourse crossings were tested by hydraulic modelling as part of the Sizewell link road FRA and modified to mitigate any increase in flood risk due to the construction of the Sizewell link road and its associated side roads.

3.1.2 Based on available data at that stage, the concept design for the disposal of highway runoff was by infiltration to ground. However, it was not possible to undertake geotechnical investigation to confirm actual infiltration rates at that stage.

3.1.3 The concept design provided for traditional drainage at the A12 and B1122 Middleton Link roundabouts with a combination of highway gullies and combined kerb drains (CKDs) collecting runoff and discharging via carrier drains to infiltration basins where runoff would infiltrate to ground.

3.1.4 The required size of infiltration basins required for the roundabout runoff could not be accurately determined without validated infiltration rates. As a result, they were shown schematically and sufficient space within the red line boundary was provided.

3.1.5 Elsewhere on the main line of Sizewell link road and side roads drainage would be by “over the edge” with runoff flowing from the carriageway to be collected in swales. The swales were proposed to be 1 m wide, 0.5 m deep and have side slopes of 1 in 3.

3.1.6 Given the lack of validated infiltration rates the design included for the potential need for filter trenches in the base of the swale.

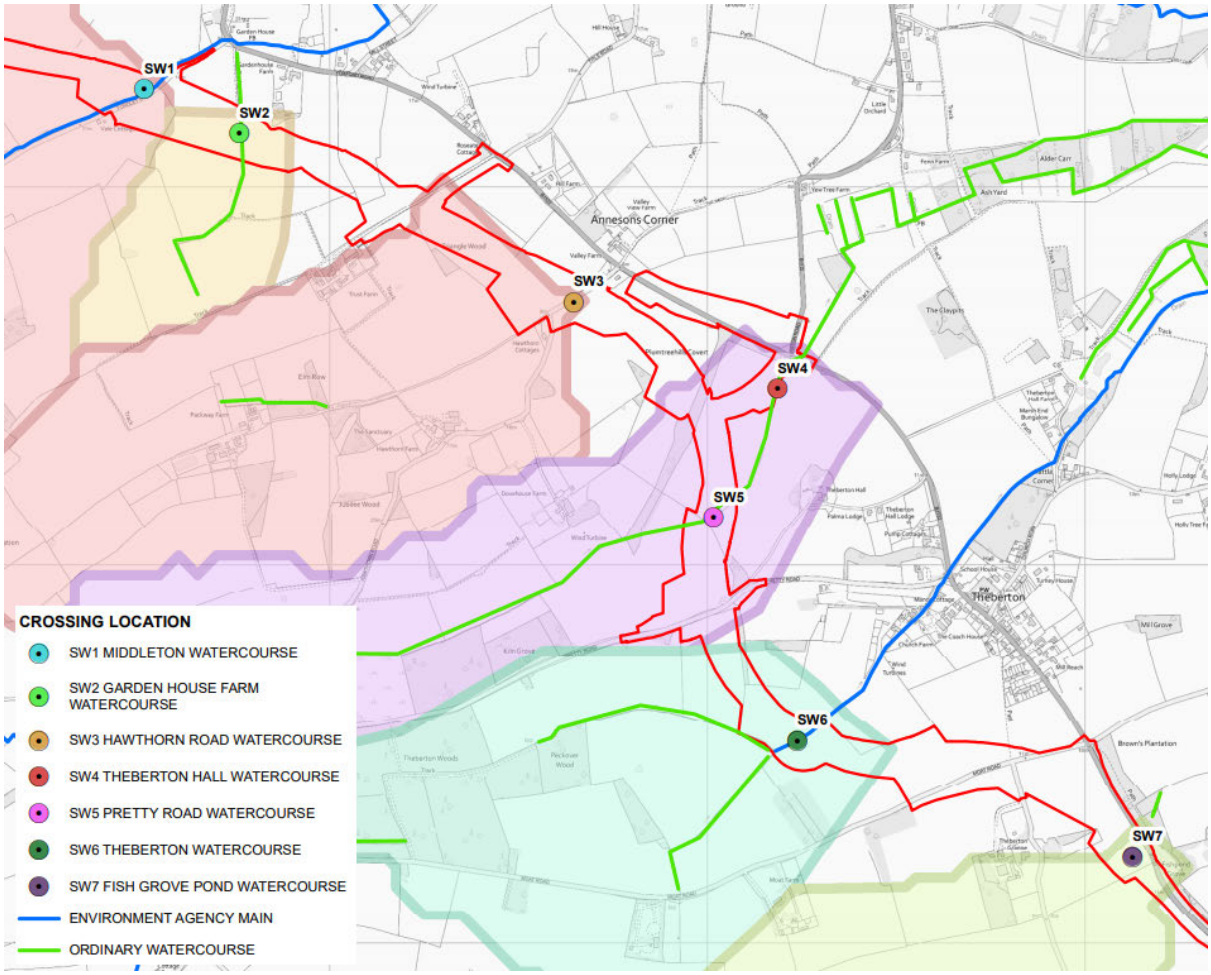
3.1.7 In addition, as back up to the swale/filter drain arrangement, a further allowance was made for 15 infiltration basins located along the line of Sizewell link road which would collect runoff not removed by the swale/filter drains.

3.1.8 Seven watercourse crossings were identified along the line of the Sizewell link road, numbered and named in the FRA as shown in **Table 1**. The location of these watercourses is shown in **Plate 2**.

Table 1: FRA referenced DCO Concept Drainage Watercourse Crossings

Crossing Number	Watercourse Number	Watercourse Name	Legal Status/Regulator
1	1	Middleton Drain	Main River EA
2	2	Garden House Farm Drain	Ordinary Watercourse SCC
3	3	Hawthorn Road Drain	Ordinary Watercourse SCC
4	5	Pretty Road Drain Leiston Road Crossing	Ordinary Watercourse SCC
5	5	Pretty Road Drain	Ordinary Watercourse SCC
6	6	Theberton Watercourse	Main River EA
7	7	Fishpond Grove Drain	Ordinary Watercourse SCC

Plate 2: Watercourse crossing locations (from Sizewell Link Road FRA [APP-136])



3.1.9 During development of concept design, it was established that there would be no change in road level or width required at crossing 4, the Pretty Road Drain beneath the B1122 near to the junction with the B1125 and link to Sizewell link road.

3.1.10 It was also determined that side road diversions for Fordley Road and Hawthorn Road would require to cross watercourse 1 – Middleton Drain and watercourse 3 Hawthorn Road Drain.

3.1.11 At its eastern end the Sizewell link road ties into the existing B1122 at the point where watercourse 7 – Fishpond Grove Drain crosses beneath the road in a 450 mm culvert. Since there was no open space between the

existing road and Sizewell link road the need to extend the existing culvert rather than construct a new culvert was confirmed.

3.1.12 With the exception of watercourse 7 crossing, all other crossings were proposed to be formed by use of portal culverts. Portal culverts have no base and can be installed such that the watercourse channel and immediate banks can be left in a natural state.

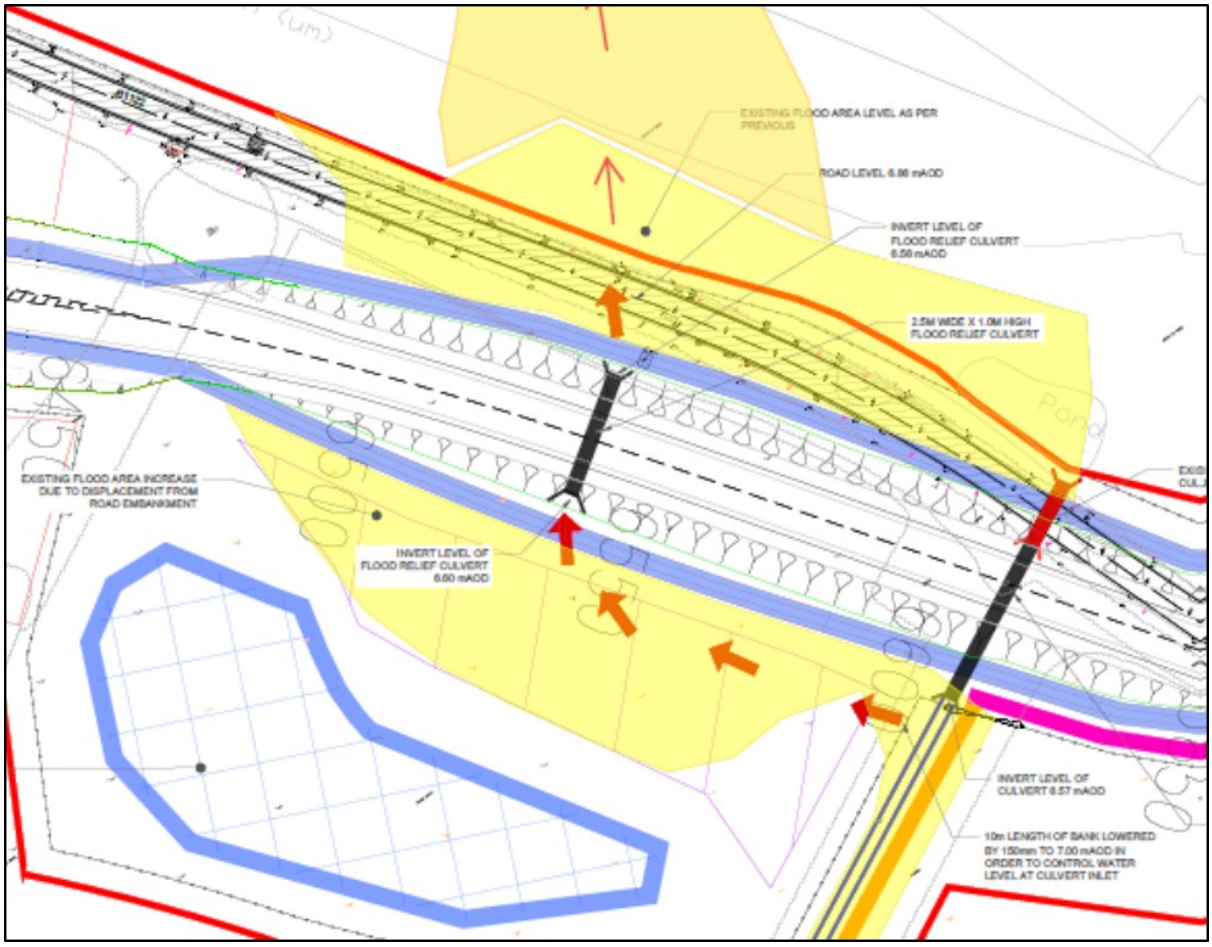
3.1.13 Portal culverts of maximum available width of 5.5 m were tested for watercourse crossings 1, 2, 3, 5 and 6 by hydraulic modelling to confirm whether their size would be sufficient to ensure no unacceptable increase in flood risk to the watercourses and any adjacent property.

3.1.14 Watercourse crossings 2, 5 and 6 were predicted to create no adverse impact but watercourse crossings 1 and 3 were predicted to cause unacceptable increase in flood levels. Since the portal culvert width could not be increased, additional adjacent flood relief box culverts were proposed. These would be 2.4 m wide and 1.0 m high.

3.1.15 In the case of watercourse crossing 1 it was not possible to install a portal culvert under the side road due to levels and so following discussion with regulators, it was proposed that the watercourse be diverted to avoid the side road thus eliminating the need for the crossing.

3.1.16 Due to lack for level data it was not possible to undertake hydraulic modelling of the watercourse crossing 7 existing baseline situation or with the extended length of culvert. However, it is apparent from the EA surface water flood map that an overland flow path routes water which overflows the bank to the west and then across the B1122. This is shown in **Plate 3**.

Plate 3: Crossing 7 overland flow path



3.1.17 The flow path is show by red arrows with predicted extent shaded yellow. Since the line of Sizewell link road would block this flow path a flood relief culvert, 2.4 m wide and 1.0 m high, was proposed to pass through the Sizewell link road in order to allow the flow path to remain.

3.1.18 Based on available desktop information it was noted that local field boundary ditches may exist at three locations. These were shown on DCO drawings as requiring possible ditch culverts.

4 ADDITIONAL INPUT DATA

4.1.1 The preliminary drainage design has been developed based on the concept design but modified to take account of data which has become available since DCO submission.

4.1.2 The new data which informs the design is listed below:

- Drone topographic survey of Sizewell link road route
- Topographic survey of watercourses within and adjacent to red line boundary
- Aerial view from drone flyover
- Ground investigation and infiltration testing
- Ground penetrating radar (GPR) survey
- Additional traditional topographic survey of critical locations
- Site visit and inspection of parts of Sizewell link road route where land access was available on 13 January 2021
- Site visit and inspection of parts of Sizewell link road route where land access was available on 24 February 2021
- Sizewell Link Road FRA Addendum (Draft)
- Highways England Water Risk Assessment Tool (HEWRAT)
- Hawthorn Road side road design change

4.1.3 The site visit covering the Sizewell link road extent between the A12 and the East Suffolk railway line was undertaken jointly with SCC.

4.1.4 The design development has also evolved through the Design Review meetings held with SCC and the EA. Comments and requirements confirmed by SCC and the EA have been recorded in minutes of the review meetings and taken into account.

4.1.5 The final draft preliminary design will be submitted to SCC as the intended adopting Highway Authority, to SCC as Lead Local Flood Authority and the EA. Any final comments can be addressed in the preliminary design drawings and reports, prior to issue as final design.

5 PRELIMINARY DRAINAGE DESIGN – HIGHWAY DRAINAGE EAST OF THE RAILWAY

5.1.1 The results of geotechnical investigation demonstrate that it is not possible to remove highway runoff by infiltration to ground. The infiltration rate data has been shared with SCC who have agreed that infiltration is not achievable. Accordingly, it is proposed that highway runoff is removed and disposed by discharge to existing watercourses.

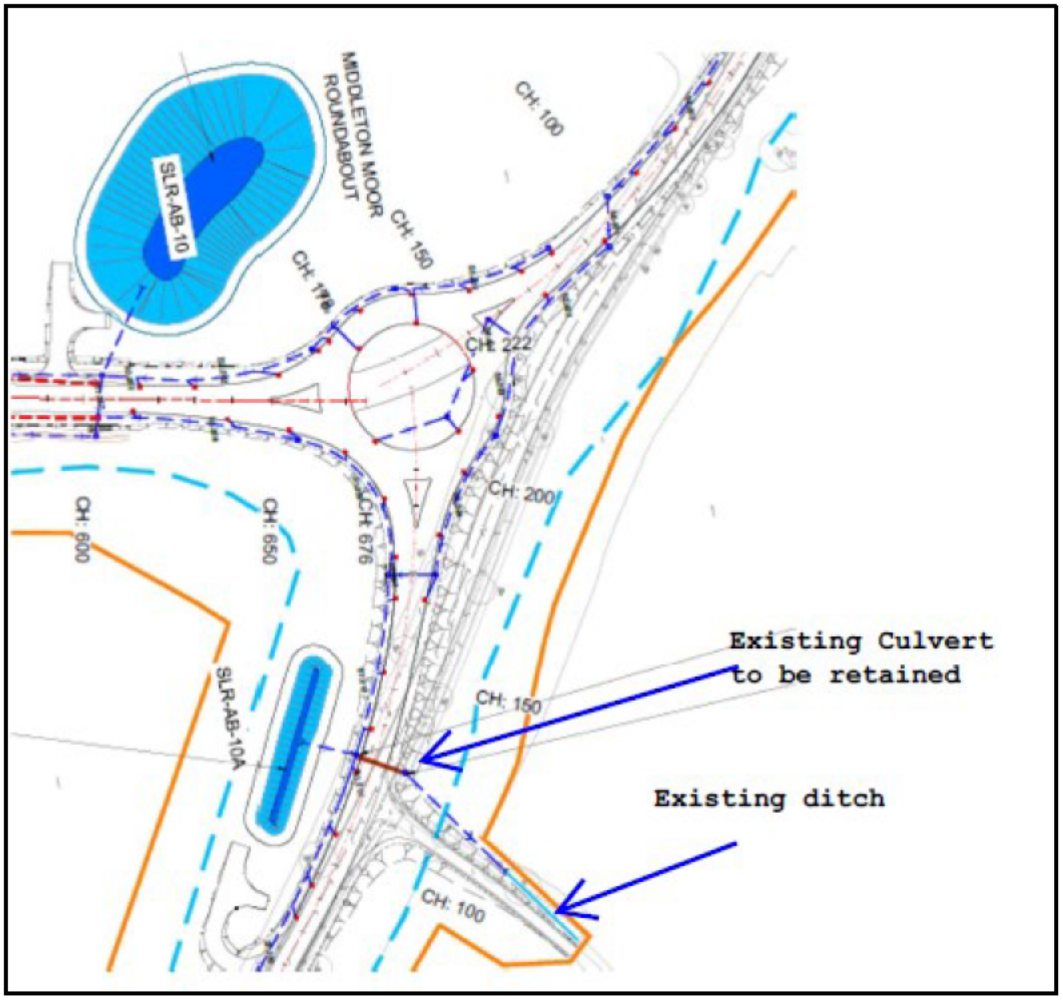
5.1.2 For the Sizewell link road and its side roads located to the east of the East Suffolk railway line there are watercourses to which discharge by gravity can be made. The watercourses are identified in **Table 1** / **Plate 2**.

5.1.3 In the case of the Middleton Link roundabout on the B1122, there is no watercourse shown on available OS based plans. However, the EA Surface Water Flood Map shows a flow path across the B1122 in proximity to the proposed roundabout. A 750 mm culvert was found at this location crossing below the B1122 road during a site visit. This culvert discharges into a deep ditch to the north which discharges into a tributary of the Minsmere River. The culvert is at a low point on the B1122 and drains the carriageway via a grip. A significant field land drainage network also discharges upstream of the culvert.

5.1.4 Given the extent of flows that currently discharge into the culvert, it is assumed that since the Sizewell link road drainage will replace the existing respective part of the B1122 runoff and the land drainage network, discharge to the existing culvert and ditch at an attenuated flow rate is acceptable.

5.1.5 The proposed drainage arrangement at the Middleton Link roundabout is shown in **Plate 4.** The proposed highway drainage for Middleton Link roundabout will remain unchanged with discharge to attenuation basin SLR-AB-10. The basin will also receive highway runoff from swales located on either side of the road, to the north of the link road crest point.

Plate 4: Middleton link roundabout drainage outfall



5.1.6 For Sizewell link road and all other side roads, the swale drainage and filter drains proposed will remain broadly as shown in DCO drawings. However, these will now provide a continuous outfall route to a watercourse.

5.1.7 Although in reality some removal of runoff will occur through limited infiltration, adsorption by vegetation and evaporation, as agreed with SCC, all drainage networks are designed and sized on the basis of no loss such that all highway runoff reaches and discharges into a watercourse.

5.1.8 In accordance with the hierarchy for disposal of highway runoff and to limit discharge so as not to increase flood risk, the discharge rate needs to be limited by flow control. This results in a requirement to provide temporary storage of runoff in the form of an attenuation basin adjacent to the watercourse.

5.1.9 In order to limit the size of these outfall attenuation basins and their inflow rate, upstream flow control points and offline attenuation basins are proposed along the line of the swales.

5.1.10 The number of basins required to attenuate the surface water runoff from the Sizewell link road will be reviewed further at the detail design stage and rationalised where possible.

5.1.11 Since the swales are no longer designed to infiltrate runoff, taking into account highway safety issues, their dimensions have been altered. When located in cutting or at level grade the depth of swale is reduced to 200 mm and the side slopes slackened to 1 in 5. This enables the requirement for the provision of vehicle restraint systems (VRS) to be avoided.

5.1.12 Swales at the toe of embankment will remain as proposed in the DCO design, at 0.5 m deep.

5.1.13 SCC guidance document "Sustainable Drainage Systems (SuDS) Appendix A" (Ref. 2) states that where discharge to watercourse is accepted, flow rate should be limited to either QBar or 2 l/s/ha whichever is the greater. However, since some Sizewell link road catchments are small this would result in a low permitted flow rate. Since the SCC guidance also requires a minimum flow control device opening of 100 mm, there is potential conflict between these requirements. Following liaison, SCC has agreed that a minimum controlled flow rate of 5 l/s could be accepted subject to evidence that it does not cause unacceptable increase in flood risk from the receiving watercourse.

5.1.14 Details of individual catchments, their gross areas and their flow rates set at 5 l/s flow rates for rainfall return periods of up to and including 1 in 100 years plus climate change are shown in Table 2 below.

Table 2: Highway discharge points to watercourse

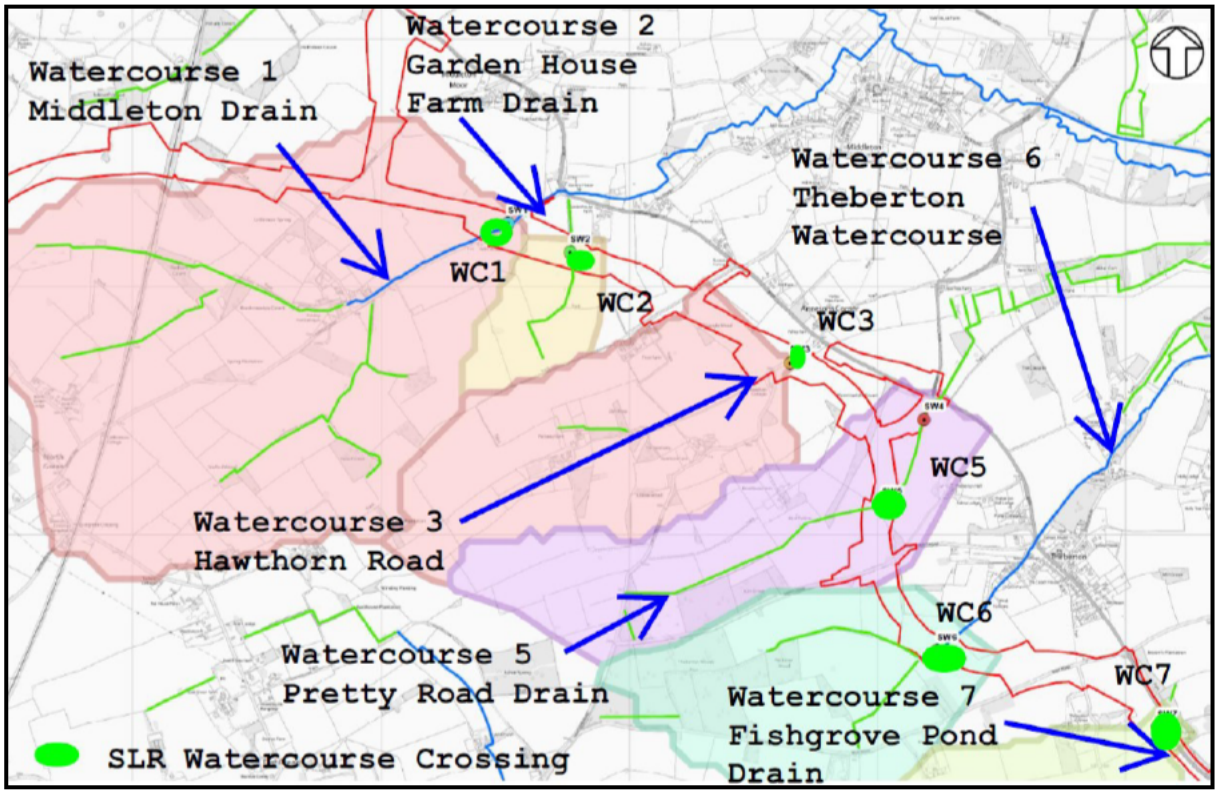
Receiving Watercourse	Outfall Basin ref	Catchment area gross (Ha)	Flow Rate @ 2 l/s/Ha	Proposed Flow Rate (l/s)
Unnamed watercourse west of A12 road	None	0.184	0.4	5.0
Unnamed watercourse north of B1122	SLR-AB-10	1.629	3.3	5.0

Middleton Moor				
Watercourse 1 Middleton Drain	AB-13 west	14.809	29.6	5.0
Watercourse 1 Middleton Drain	SLR-AB-15 east	0.947	1.9	5.0
Watercourse 2 Garden House Farm Drain	SLR-AB-16 east	3.075	6.2	5.0
Watercourse 3Hawthorn Road Drain SLR west	SLR-AB-20	2.888	5.8	5.0
Watercourse3 Hawthorn Road Drain B1122 east	SLR-AB-21	3.885	7.8	5.0
Watercourse 5 Pretty Road Drain B1125 west	SLR-AB-25	2.299	4.6	5.0
Watercourse 5 Pretty Road Drain B1125 east	SLR-AB-26	1.027	2.1	5.0
Watercourse 5 Pretty Road Drain SLR west	SLR-AB-27	0.558	1.1	5.0
Watercourse 5 Pretty Road Drain SLR east	SLR-AB-30	1.834	3.7	5.0
Watercourse 6 Theberton Watercourse west	SLR-AB-32	2.605	5.2	5.0

Watercourse 6 Theberton Watercourse east	SLR-AB-33	1.772	3.5	5.0
Watercourse 7 Fish Grove Pond Drain	SLR-AB-37	4.651	9.3	5.0

5.1.15 The catchment extents determined as part of the FRA study are shown in **Plate 5**.

Plate 5: Sizewell link road impacted local watercourse catchment extents [APP-138 Figure 4]



5.1.16 Details of flow rates derived from the 2 l/s/ha criteria are included for information. Of the 13 outfalls, 7 would be required to attenuate to less than the 5 l/s. Although 6 outfalls could discharge at greater rate with the exception of the catchment discharging from the west into Middleton Drain, the difference is limited. Accordingly, the design provides for a controlled flow rate of 5 l/s at each outfall.

5.1.17 In the case of the Middleton Drain catchment west, it is noted that the catchment includes for a pumped discharge for the Sizewell link road A12 roundabout and mainline across the railway at a flow rate of 5 l/s and thus the calculated 2 l/s/ha flow rate of 29.6 l/s is not applicable. As described in Section 7 below, subject to further investigation the transfer of flow from the west of the railway may not be taken forward to detailed design if a subsequent gravity solution can be substantiated.

5.1.18 The impact of discharging each catchment into its respective watercourse has been accessed using the FRA Addendum individual watercourse hydraulic models, including for watercourse 7 (not previously modelled as part of the Sizewell link road FRA). As confirmed in the Addendum report there is no adverse impact of these flows on the watercourse's capacity nor unacceptable increase in flood risk.

5.1.19 As agreed with SCC and the EA prior to DCO submission, the environmental impact of discharging highway runoff is to be assessed using the Highways England Water Risk Assessment Tool (HEWRAT) (Ref. 3) methodology. The assessment results confirm that a SuDS management train with the combination of swales, filter drains and attenuation basins, for Sizewell link road discharges to watercourses are low risk and therefore acceptable. SCC has indicated that they will wish to review the management train at detailed design stage and may wish to see provision of additional treatment stages.

5.1.20 To undertake an assessment of the hydraulic or environmental impact of discharge into the deep ditch north of the B1122 at Middleton Link further survey work would be required during the detailed design stage.

6 PRELIMINARY DRAINAGE DESIGN – HIGHWAY DRAINAGE WEST OF THE RAILWAY

6.1.1 Desktop study identified no watercourse crossings by the Sizewell link road between the A12 roundabout and the East Suffolk railway line. As a result, the FRA does not include any hydraulic models for watercourse crossings between the A12 roundabout and East Suffolk railway line. The FRA does confirm that this area forms part of the Middleton Drain catchment.

6.1.2 Following confirmation that infiltration is not possible the following options for removal of highway runoff have been considered:

- Swales and filter drains with additional oversized basins to contain the 1 in 100 year return period runoff volume plus follow on rainfall events

- Discharge to remote watercourses shown on OS maps either by gravity or pumping
- Discharge over the East Suffolk railway line to the catchment discharging to Middleton Drain
- Discharge to ground via deep boreholes into permeable strata

6.1.3 The options have been discussed with SCC as Highway Authority and LLFA.

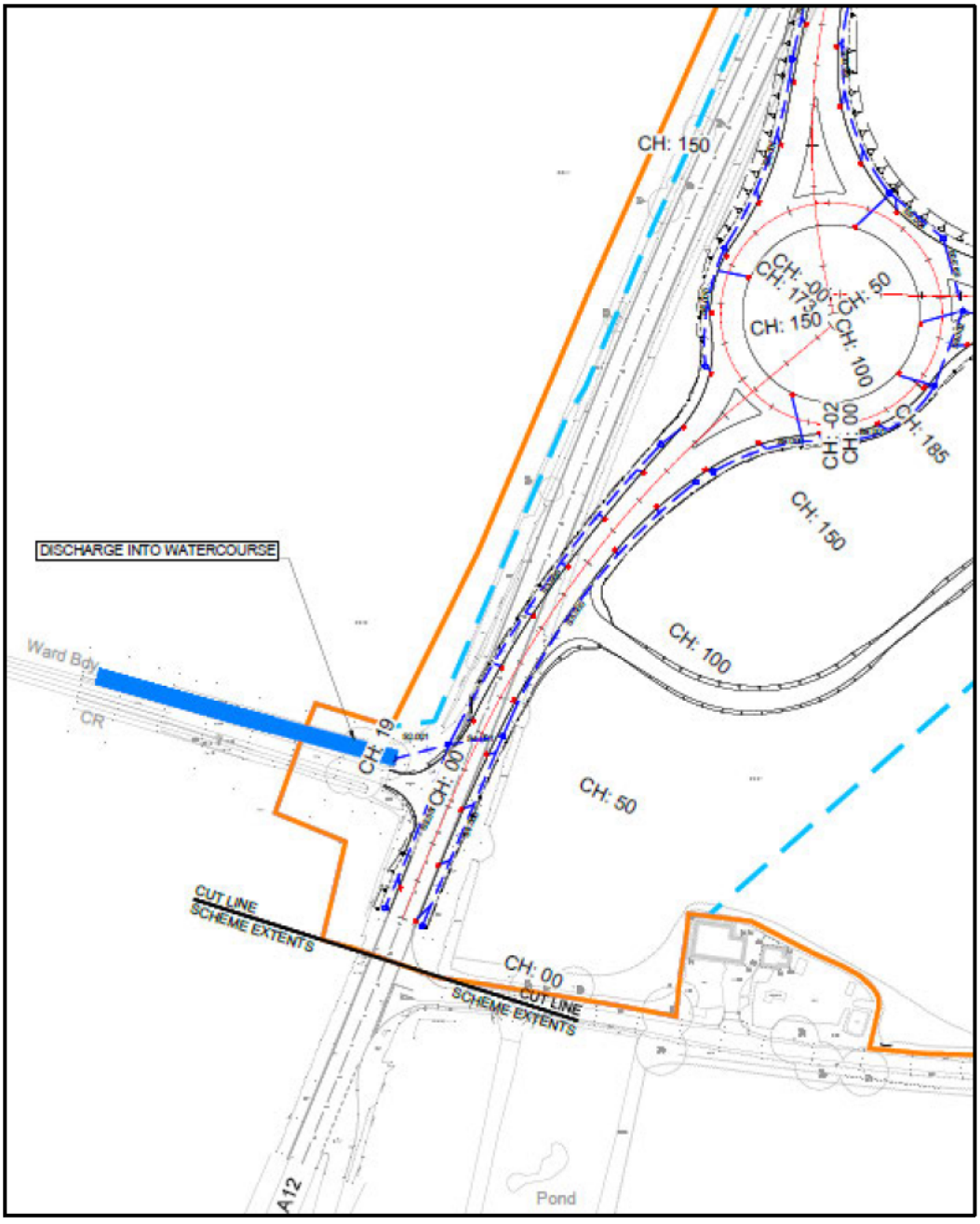
6.1.4 After consideration of the alternatives SCC has advised that the provision of oversized basins is not acceptable and that all drainage networks must have a positive outfall, to limit flood risk.

6.1.5 Following the joint SCC/WSP site visit on 13 January 2021 it is agreed that discharge west of the railway to the remote watercourses (within the red line boundary) to the north or south by gravity is not achievable. Since the alternative would be pumping, it is considered to be less disruptive to pump to the east of the railway and into the Middleton Drain west catchment compared to pumping to the remote watercourses.

6.1.6 SCC guidance document "Sustainable Drainage Systems (SuDS) Appendix A" states that deep borehole soakaways with depth greater than 2 m are considered not viable and will only be accepted as a last resort. Based on available geotechnical information the required depth of boreholes would be around 13 m and with uncertainty that suitable infiltration rates can be achieved this option has been discounted.

6.1.7 During the site visit and subsequently confirmed by the GPR survey, a small section of the existing A12 to the south of the roundabout was found to discharge to a deep ditch to the west of the road. It is proposed that the southern arm of the roundabout will be drained to this ditch using the same outfall point. The arrangement is shown in **Plate 6**. As shown in Table 2, the discharge rate will be controlled to 5 l/s.

Plate 6: Proposed highway drainage A12 roundabout southern arm



6.1.8 Based on the above considerations, the drainage of the A12 roundabout, its northern arm and the first portion of Sizewell link road arm will remain as a combination of highway gullies and combined kerb drains (CKDs) collecting runoff and discharging via carrier drains but the receiving infiltration basin changes to an attenuation basin SLR-AB-01.

6.1.9 In order to provide basin SLR-AB-01 an outfall as required by SCC, a small pumping station will be provided. This will pump at a rate of 5 l/s via a rising main which will discharge to a gravity network to the east of the Sizewell link road crest point at chainage 488 m.

6.1.10 The length of Sizewell link road from the A12 to chainage 488 m will drain in the same way as for the east of the railway with swale/filter drains and 2 supporting attenuation basins.

6.1.11 The length of Sizewell link road from chainage 488 m to the East Suffolk railway bridge will drain via swale/filter drains and discharge into a single attenuation basin SLR-AB-05 at chainage 1200 m. The attenuation basin SLR-AB-05 will discharge into a pumping station which will pump at a rate of 5 l/s via a rising main discharging into a gravity network to the east of the railway bridge and ultimately to Middleton Drain.

6.1.12 The rising main will be attached to the bridge structure when crossing the railway.

6.1.13 The Sizewell link road will have longfall and crossfall gradients as it crosses the railway bridge from east to west. Deck CKDs will be provided to remove runoff and they will outfall into the swales to the west.

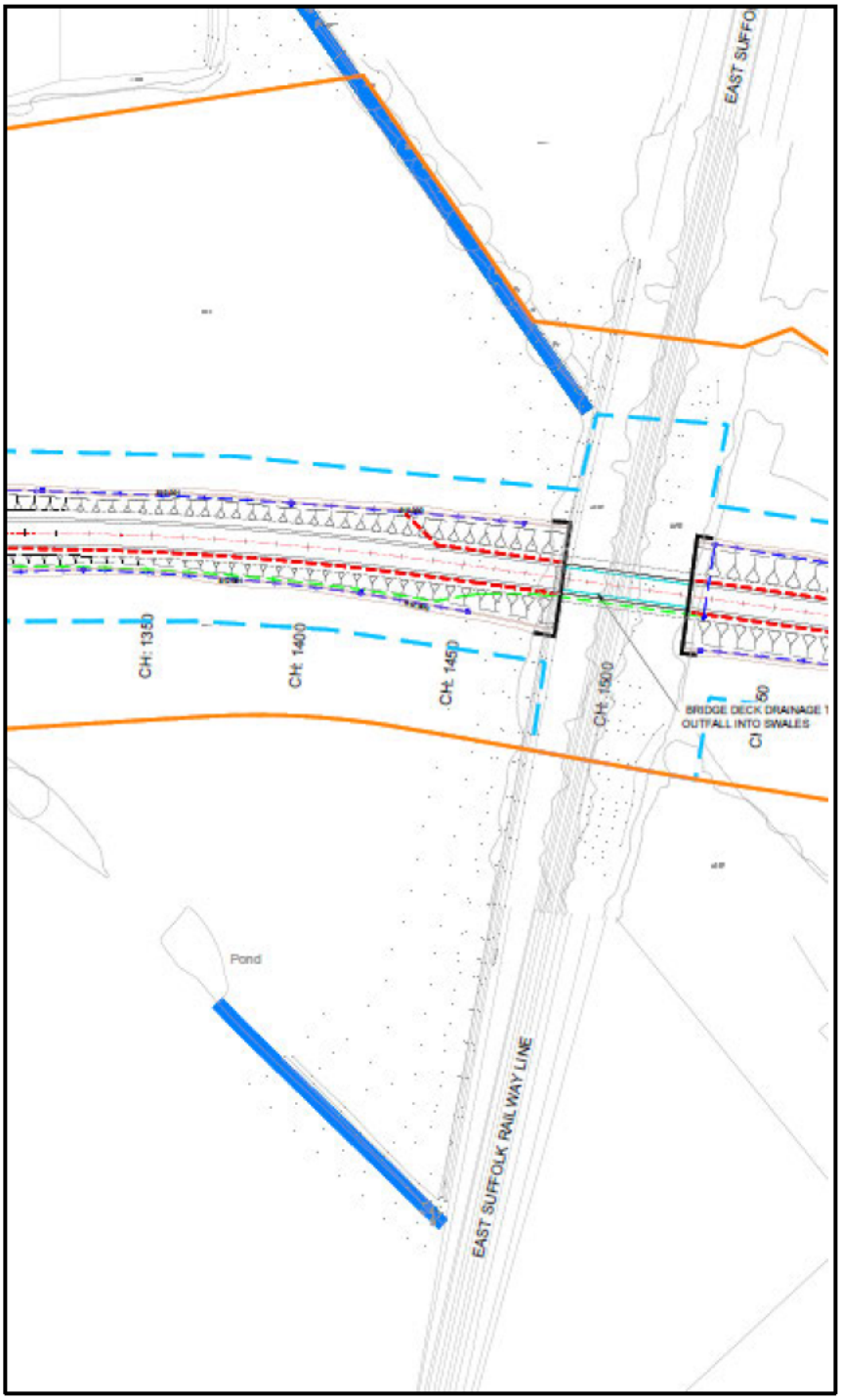
6.1.14 During the site visit the presence of two field boundary ditches was confirmed. These ditches are heavily silted and in poor state of maintenance. It is not clear as to whether they drain effectively or if they have a formal outfall. However, as confirmed with SCC where such ditches exist, they will be culverted beneath Sizewell link road such that their function remains intact. The ditches LDC1 and LDC2 are located at chainage 250 m and 750 m.

7 PRELIMINARY DRAINAGE DESIGN – WEST OF THE RAILWAY (GRAVITY OPTION ALTERNATIVE)

7.1.1 During the site visit on 13 January 2021, the presence of a shallow local ditch was discovered approximately 40 m to the north of Sizewell link road, adjacent to the East Suffolk railway boundary. This ditch follows a field boundary running north west and is shown blue in **Plate 7**. It is in a state of dereliction and would not be suitable as an outfall for Sizewell link road drainage. However, it does discharge into a watercourse, not shown on OS mapping, approximately 250 m north of Sizewell link road which runs north and which subject to confirmation of levels could be a suitable gravity outfall.

7.1.2 Similarly, to the south of the proposed Sizewell link road route a deep excavated field boundary ditch was discovered, approximately 200 m south, continuing in a southeast direction to a headwall with a 600mm outfall pipe. This ditch is also shown blue in **Plate 7**. Unverified plans provided by the landowner, show the 600mm pipe continues southwards within the railway at the base of the cutting before discharging into the Middleton Drain.

Plate 7: Local watercourses to north and south of Sizewell link road adjacent to East Suffolk Railway



7.1.3 Based on site observation it appeared that there are general falls in land from Sizewell link road towards these watercourses. It was agreed that

subject to confirmation of ground levels that it may be possible to connect to either the watercourse or ditch and obtain a gravity outfall.

7.1.4 As can be seen in **Plate 7** both the watercourses and ditch are located outside of the DCO boundary limits shown orange. Although connection to the watercourses would not be within the DCO limits, in accordance with the SCC required hierarchical approach, before SCC acceptance of a pumped outfall, it is to be established first whether a gravity connection is achievable.

7.1.5 A topographic survey of the area along the potential outfall route has been undertaken. This confirms that the bed level of the watercourse to the north is at a level of 33.66 mAOD. The invert level of the 750 mm outfall drain to the south is at a level of 34.84 mAOD. Sizewell link road is on an embankment above existing ground level which is at level of 37.8 mAOD in proximity to the railway boundary. As observed during the site visit these levels do confirm a fall in ground level both to the north and to the south.

7.1.6 Given that infiltration of highway runoff to ground is not possible, it is necessary for the filter drain pipe to have a falling gradient in order to remove runoff to an outfall point for removal, whether by gravity or pumping. The distance from the crest point at chainage 488 m to the railway boundary at chainage 1480 m is 992 m. Attenuation basin SLR-AB-05 which receives runoff from this section of Sizewell link road is located at chainage 1200 and collects runoff from both east and west. It is kept clear of the railway which is in cutting.

7.1.7 In order to provide the required continuous falling gradient, the basin bed level is fixed at 36.329 mAOD.

7.1.8 If an outfall is provided to the northern watercourse following Sizewell link road and field boundaries, its distance would be approximately 510 m. Given a need for a falling gradient and for the drain to have self-cleansing velocity a gradient of 1 in 150 is assumed. This would result in a fall of 3.4 m with an outfall level of 32.929 mAOD approximately 0.73 m lower than the watercourse.

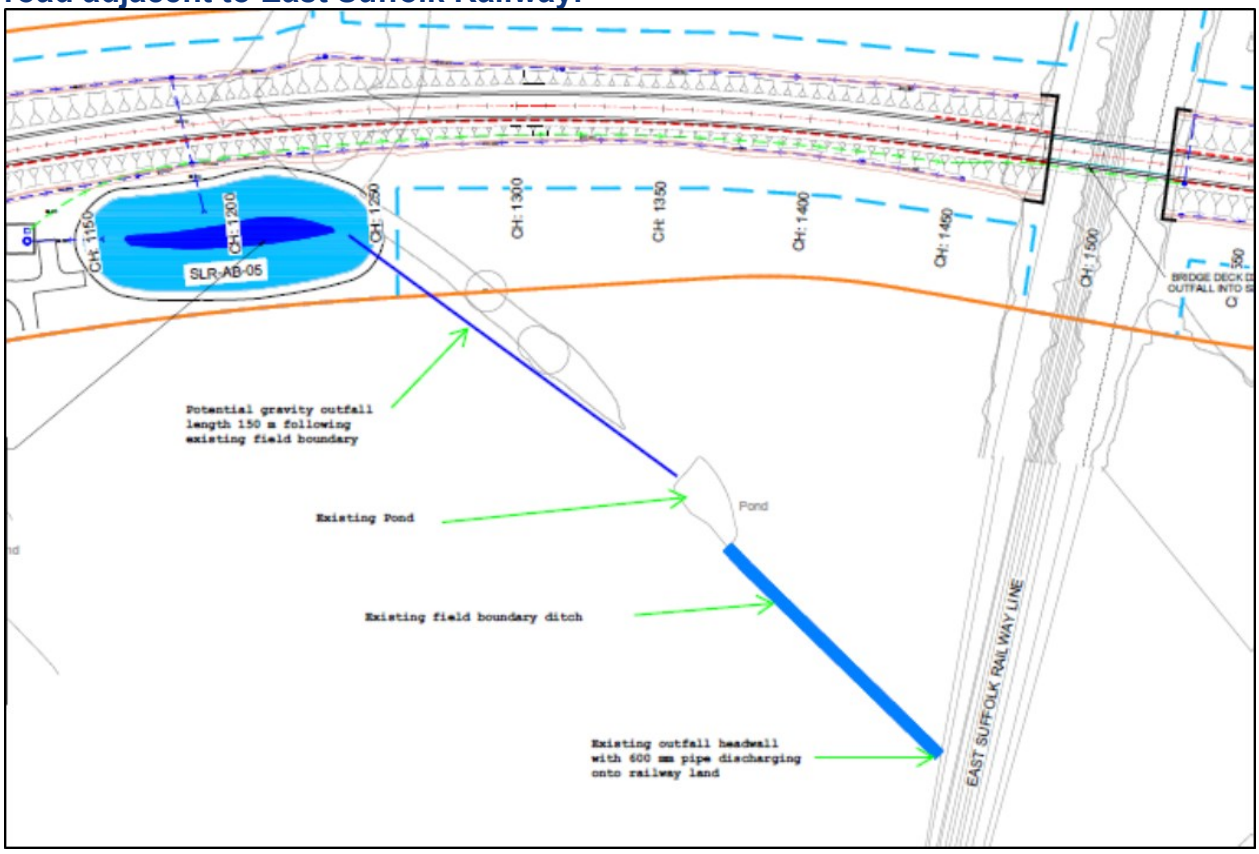
7.1.9 If an outfall is provided directly from the basin to the northern watercourse, the distance reduces to 300 m. This would result in an outfall level of 34.329 mAOD which is 0.67 m above the watercourse.

7.1.10 If an outfall is provided to the southern ditch following Sizewell link road and field boundaries, its distance would be approximately 460 m. This would result in a fall of 3.4 m with an outfall level of 33.262 mAOD approximately 1.58 m lower than the ditch.

7.1.11 If an outfall is provided directly from the basin to the southern ditch outfall, the distance reduces to 300 m. This would result in an outfall level of 34.329 mAOD which is 0.51 m below the ditch.

7.1.12 However, in reviewing a direct route, it is noted that the southern outfall would be able to discharge into an existing pond rather than extend to the 600 mm outfall drain. With discharge into the pond the invert level at outfall would be 35.329 mAOD, approximately 0.49 m above the outfall drain. The pond is at the upstream end of the ditch. This arrangement is shown in **Plate 8.**

Plate 8: Proposed gravity outfall to local pond and ditch south of Sizewell link road adjacent to East Suffolk Railway.



7.1.13 Of all of the alternatives, discharge via an outfall from the basin to the existing pond would have the minimum impact on land use since it would follow a field boundary and be the shortest distance. Whilst no levels are available for the pond, it was noted to be fairly deep during the site visit.

7.1.14 During liaison, SCC has confirmed that subject to the Sizewell link road being adopted as public highway, they would if necessary, accept the use of pumping stations provided that it can be demonstrated that no practical

gravity solution is available. On the basis that all attenuation basis and highway networks must have an outfall, it is necessary to provide a pumping station at the A12 roundabout from basin SLR-AB-01. However, if an outfall can be provided from attenuation basin SLR-AB-05 discharging via the pond and ditch, this would eliminate the need for a second pumping station and rising main across the railway discharging into the Middleton Drain west catchment.

7.1.15 SCC has advised that for any discharge to watercourse to be accepted, it is necessary to demonstrate that:

- the proposed rate of discharge to the watercourse will not result in increased flood risk
- the proposed discharge will not adversely impact on water quality
- there is continuity of downstream discharge route providing a guaranteed outfall

7.1.16 On the basis of currently available data, it is believed that that the SCC stated requirements can be met, whilst acknowledging that further data will be required to confirm this position.

7.1.17 The preliminary design solution proposed was completed subsequent to the finalisation of the **Sizewell Link Road FRA Addendum** [REP2-026]. The flood risk impact of the proposed discharge rate at this location requires to be confirmed formally in a future update to the FRA, but sensitivity testing in the hydraulic model has demonstrated that there is no resulting impact on properties.

7.1.18 Accordingly, whilst continuing to propose a drainage solution with a pumping station for the catchment to the west of the railway to ensure a reliable solution for the DCO application, with discharge to the east of the railway, the solutions to connect to the local watercourses will continue to be progressed through the design stages following further surveys such that if it can be demonstrated a gravity outfall option can be substantiated it will be substituted in preference of a pumped solution in accordance with the hierarchical approach required by SCC.

7.1.19 The proposed outfall is not located within the DCO red line boundary. Accordingly, SZC Co. has submitted a DCO red line boundary amendment into consultation which incorporates the land required for this outfall.

8 VALIDATION OF OUTLINE DRAINAGE STRATEGY

8.1.1 In accordance with the drainage hierarchy, the **Outline Drainage Strategy** [REP2-033] proposed the primary use of infiltration, with additional use of attenuation techniques (e.g. ponds and swales) to manage water quality and to further promote infiltration. The strategy acknowledged the need for discharge to watercourse where infiltration rates were insufficient to support a primarily infiltration-led approach.

8.1.2 The approach in the **Outline Drainage Strategy** [REP2-033] is validated by the completed preliminary design, which has demonstrated that infiltration is not applicable and proposes the attenuated discharge of water to watercourses.

8.1.3 The preliminary design documents will be made available for review and acceptance by SCC and the EA with respect to potential adoption of the Sizewell link road by SCC and for required regulatory consents.

9 SUMMARY AND CONCLUSION

9.1.1 The purpose of this technical note is to provide details of how the design has needed to evolve and develop as a result of provision of new information. The primary cause of change has been that following the completion of ground investigation works, the assumption that the primary means of removal and disposal of highway surface water runoff by infiltration to ground has been discounted. The alternative of discharge at controlled rates to watercourse, as an alternative has been discussed with SCC and the EA in liaison and through design review meetings.

9.1.2 The primary reason for updating the original DCO submitted FRA was to address the concerns expressed by the EA with regard to the extent of hydraulic modelling of the Sizewell link road culvert crossings. The extent and accuracy of modelling has been enhanced following the obtainment of watercourse surveys both upstream and downstream of crossing points.

9.1.3 Following the change with discharge of highway runoff to watercourse at a flow rate of 5 l/s per outfall, the FRA hydraulic modelling was used to test and demonstrate the insignificant impact of these direct flows on flood risk in the watercourses.

9.1.4 The highway drainage has been designed in accordance with Design Manual for Roads and Bridges, the CIRIA SuDS Manual C753 (Ref. 4) and to comply with stated requirements of SCC contained in their SuDS Local Design Guide Appendix A.

9.1.5 At this preliminary design stage, it is considered that the design provides for the effective removal, treatment and disposal of highway surface water runoff without adversely increasing flood risk to or from watercourses, or impacting on third parties. Discharge to watercourse would not adversely impact on water quality. The flood risk performance of the highway is as specified in DMRB and SCC guidance.

REFERENCES

1. Design Guide, Suffolk County Council, 2000, https://www.suffolk.gov.uk/planning-waste-and-environment/planning-and-development-advice/suffolk-design-guide-for-residential-areas/

2. Sustainable Drainage Systems (SuDS) a Local Design Guide Appendix A to the Suffolk Flood Risk Management Strategy, Suffolk County Council, May 2018 https://www.greensuffolk.org/app/uploads/2021/05/2018-10-01-SFRMS-SuDS-Guidance-Appendix-A-.pdf

3. Highways Agency et al. (2009). Volume 11, Section 3, Part 10: Road Drainage and the Water Environment, HD45/09. http://www.standardsforhighways.co.uk/ha/standards/dmrb/vol11/section3/hd4509.pdf

4. The SUDs Manual (C753), CIRIA, 2015, ISBN 978-0-86017-760-9.

APPENDIX G

TWO VILLAGE BYPASS PRELIMINARY DRAINAGE DESIGN NOTE

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None provided.

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None provided.

1 INTRODUCTION

1.1.1 NNB Generation Company (SZC) Limited (SZC Co.) submitted an application for a Development Consent Order (DCO) to the Planning Inspectorate under the Planning Act 2008 for the Sizewell C Project (referred to as the 'Application') in May 2020. The Application was accepted for examination in June 2020.

1.1.2 SZC Co. has undertaken work to validate and develop the design of the Sizewell link road that was originally submitted as part of the DCO application. This document forms one of a series of design validation and evolution documents being provided to the Examining Authority in support of the **Outline Drainage Strategy** [REP2-033].

1.1.3 The two village bypass forms one of the Associated Developments (AD) which are required to mitigate traffic impacts arising from the main development site. The two village bypass consists of a new 2.4 km long single carriageway road bypassing the villages of Stratford St Andrew and Farnham. The new bypass will connect to the existing A12 via at grade roundabouts at both the western and eastern ends of the scheme. The roundabout at the western end ties in with the existing A12 Main Road and the roundabout at the eastern end ties in with Friday Street.

1.1.4 The two village bypass will be designed to Suffolk County Council's (SCC) adoptable standards (Ref. 1).

1.1.5 The two village bypass will generate highway surface water runoff which will require to be removed, treated as necessary and disposed by infiltration to ground.

1.1.6 The two village bypass will cross the River Alde, its associated flood plain and two minor watercourses which need to be accommodated.

2 PURPOSE

2.1.1 The **Outline Drainage Strategy** [REP2-033] identified at concept level the proposed drainage approach required for:

- The effective removal of runoff from the proposed two village bypass highway and its disposal
- The crossing of the River Alde and its associated floodplain and watercourses along the line of the two village bypass

2.1.2 This strategy was developed in consultation with drainage regulators and local authorities, including SCC and the Environment Agency (EA). A number of workshops were held and the observations/requirements of drainage regulators were incorporated in the strategy.

2.1.3 The proposed drainage infrastructure was described in the concept drainage design submitted as part of the DCO application. This concept design was based on data and information available at that time. The design was supported by the submission of the **Two Village Bypass Flood Risk Assessment** (FRA) [APP-119].

2.1.4 Following the provision of new data, and subsequent to the DCO submission, SZC Co. has developed the concept level design to preliminary design stage.

2.1.5 The purpose of this technical note is to provide details of how the concept design has been modified in response to the new data, such that it continues to provide for the effective and satisfactory drainage of the two village bypass, without unacceptable adverse impact on the water environment, both in terms of flood risk and pollution.

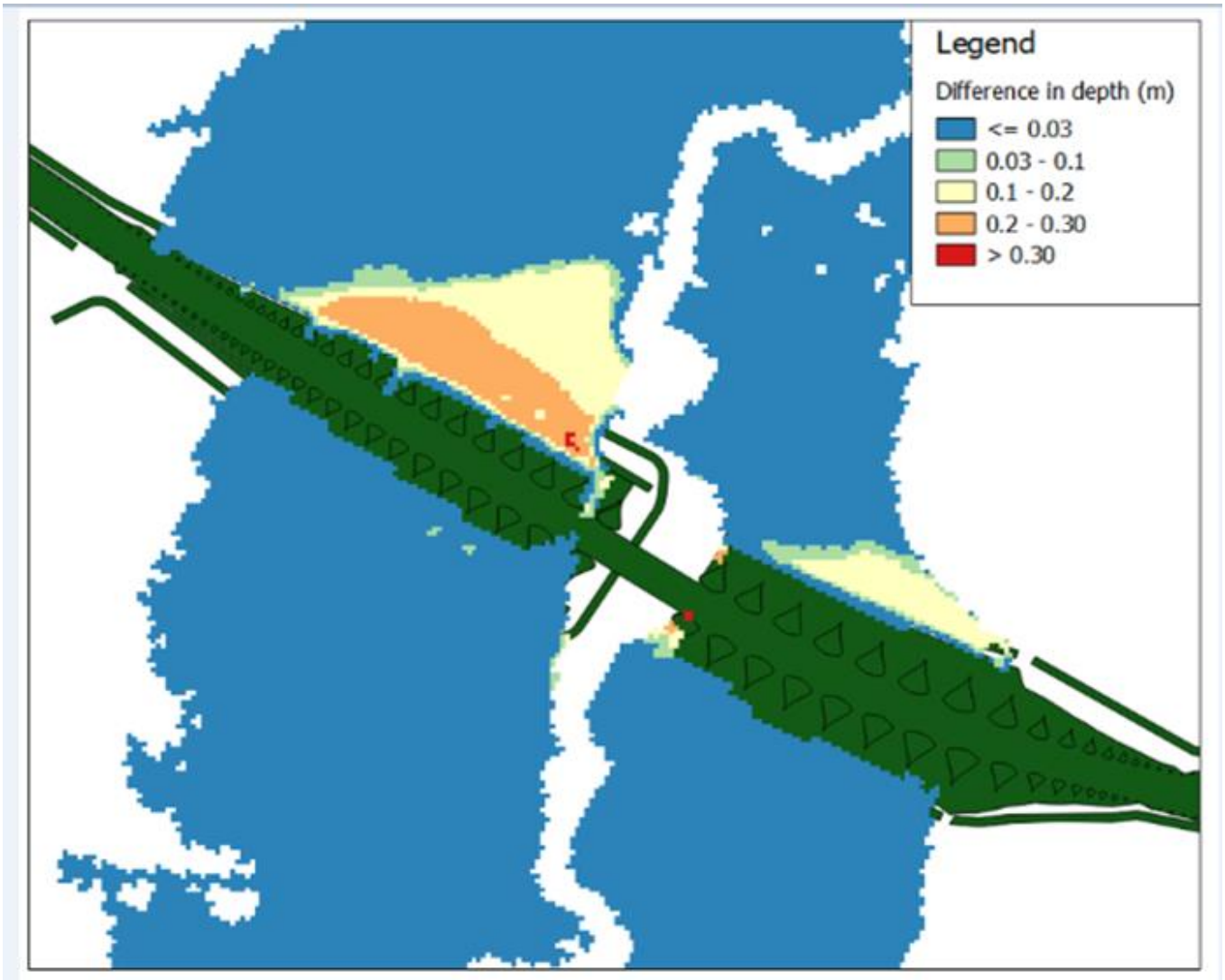
2.1.6 The content of this technical note summarises the design details and approach already shared in a series of design review meetings held with key stakeholders, including the EA and SCC.

3 DESCRIPTION OF DCO DRAINAGE CONCEPT DESIGN

3.1.1 The concept design proposal for the road crossing of the River Alde, its floodplain, and two adjacent local watercourses is with an embankment, wide bridge and flood relief culverts. The proposals were tested by hydraulic modelling undertaken as part of the **Two Village Bypass FRA** [APP-119]. This enabled the arrangements to be modified to optimise hydraulic performance and mitigate any increase in flood risk due to the construction of the two village bypass.

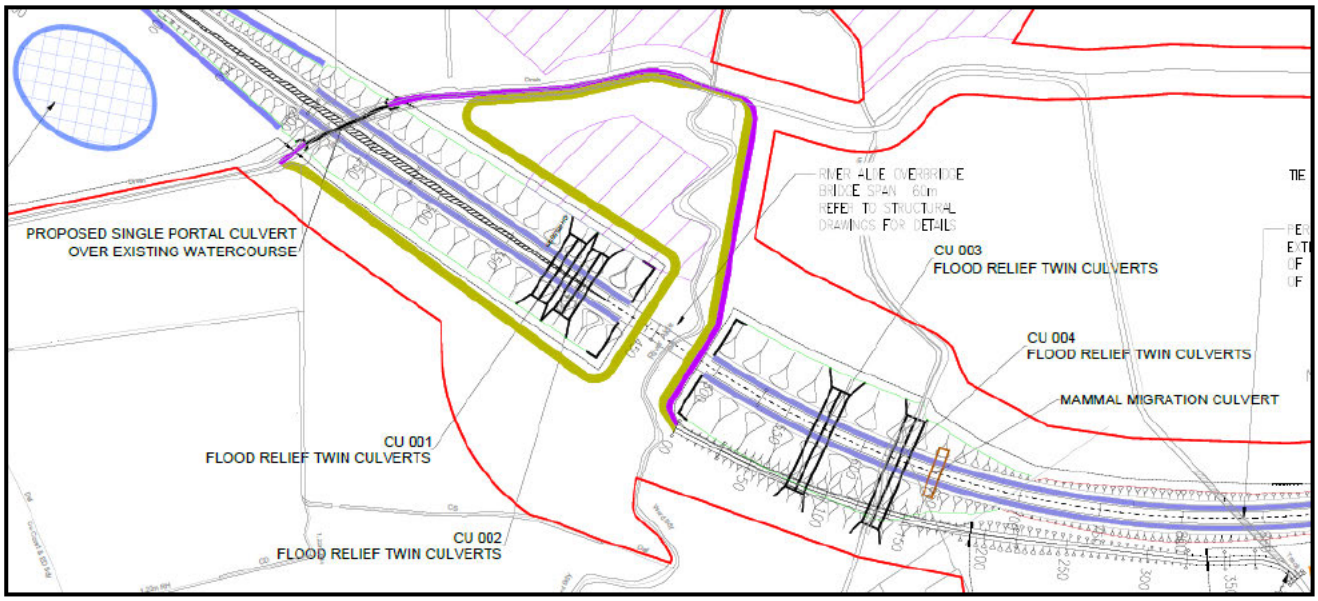
3.1.2 The final layout hydraulic modelling results predicted a limited increase in flood levels at the bridge of approximately 14 mm due to a 1 in 100 year rainfall event plus 35% climate change. Higher increases of up to 320 mm were predicted immediately upstream of the embankment but over a limited area and for a limited period. The results are shown in **Plate 1**.

Plate 1: River Alde crossing - predicted increase in flood depth for proposed bridge and embankment



3.1.3 The proposed final layout submitted for DCO is shown in **Plate 2**.

Plate 2: River Alde crossing - ridge and flood relief culvert locations



3.1.4 The concept drainage design provided for traditional drainage at the A12 roundabouts located at either end of the bypass with a combination of highway gullies and combined kerb drains (CKDs) collecting runoff and discharging via carrier drains to infiltration basins where runoff would infiltrate to ground.

3.1.5 The required size of infiltration basins required for the roundabout runoff could not, at that time, be accurately determined without validated infiltration rates. As a result, the basins were shown schematically and sufficient space within the red line boundary was provided.

3.1.6 Elsewhere on the main line of two village bypass and Hill Farm Lane side road, drainage would be by "over the edge" with runoff flowing from the carriageway to be collected in the adjacent swales. The swales were proposed to be 1 m wide, 0.5 m deep and have side slopes of 1 in 3. The location and extent of swales are shown indicatively on the DCO drawings.

3.1.7 Given the lack of validated infiltration rates the design included for the potential need for filter trenches in the base of the swale

3.1.8 In addition, as back up to the swale/filter drain arrangement, a further allowance was made for an infiltration basin located immediately east of the proposed embankment crossing of the River Alde floodplain. This basin has the twin purpose of collecting runoff not removed by the swale/filter drains but also prevents runoff flowing onto the embankment.

3.1.9 During liaison, SCC confirmed that removal of highway runoff from the River Alde embankment via infiltration within the floodplain would not be acceptable.

3.1.10 The DCO proposed the section of road between the eastern end of the embankment and the River Alde bridge would be drained either by underground drainage or drainage channel towards the bridge and then outfall with discharge into the river. Both the EA and SCC did not want highway runoff discharging directly to the river therefore in response to their concerns it was proposed that the highway on the embankment would therefore be drained either by underground drainage or a drainage channel, over the bridge, and discharge to the west and into the infiltration basin adjacent to the A12 roundabout.

3.1.11 A pipe would be provided within the bridge structure to pass forward the runoff to the west of the bridge.

3.1.12 The section of road between the River Alde bridge and the western end of the embankment would be drained either by underground drainage or drainage channel to the west and then discharge into the infiltration basin adjacent the A12 roundabout.

4 ADDITIONAL INPUT DATA

4.1.1 The preliminary drainage design has been developed based on the concept design but modified to take account of data which has become available since DCO submission.

4.1.2 The new data which informs the design is listed below:

- Drone topographic survey of the two village bypass route
- Topographic survey of watercourses within and adjacent to red line boundary
- Aerial view from drone flyover
- Ground investigation and infiltration testing
- Ground penetrating radar (GPR) survey
- Additional traditional topographic survey of critical locations
- Site visit and inspection of the full length of the two village bypass route on 12 January 2021

- Highways England Water Risk Assessment Tool (HEWRAT) (Ref. 2)

4.1.3 The January 2021 site visit was undertaken jointly with SCC.

4.1.4 The design development has also evolved through the design review meetings held with SCC and the EA. Comments and requirements confirmed by SCC and the EA have been recorded in minutes of the review meetings and taken into account.

4.1.5 The final draft preliminary design will be submitted to SCC as the intended adopting Highway Authority, to SCC as Lead Local Flood Authority and the EA. Any final comments can be addressed in the preliminary design drawings and reports, prior to issue as final design.

5 EXISTING HIGHWAY DRAINAGE ARRANGEMENTS

5.1.1 Following the site visit and review of survey data, details of existing highway drainage arrangements have been determined and are described below. The existing arrangements have been taken into account as part of preliminary design.

5.1.2 The existing section of the A12 south of Stratford St Andrew which will be modified with the construction of the two village bypass western roundabout and shown in **Plate 3** does have some limited formal surface drainage outlets in the form of 5 gullies and 4 kerb gullies.

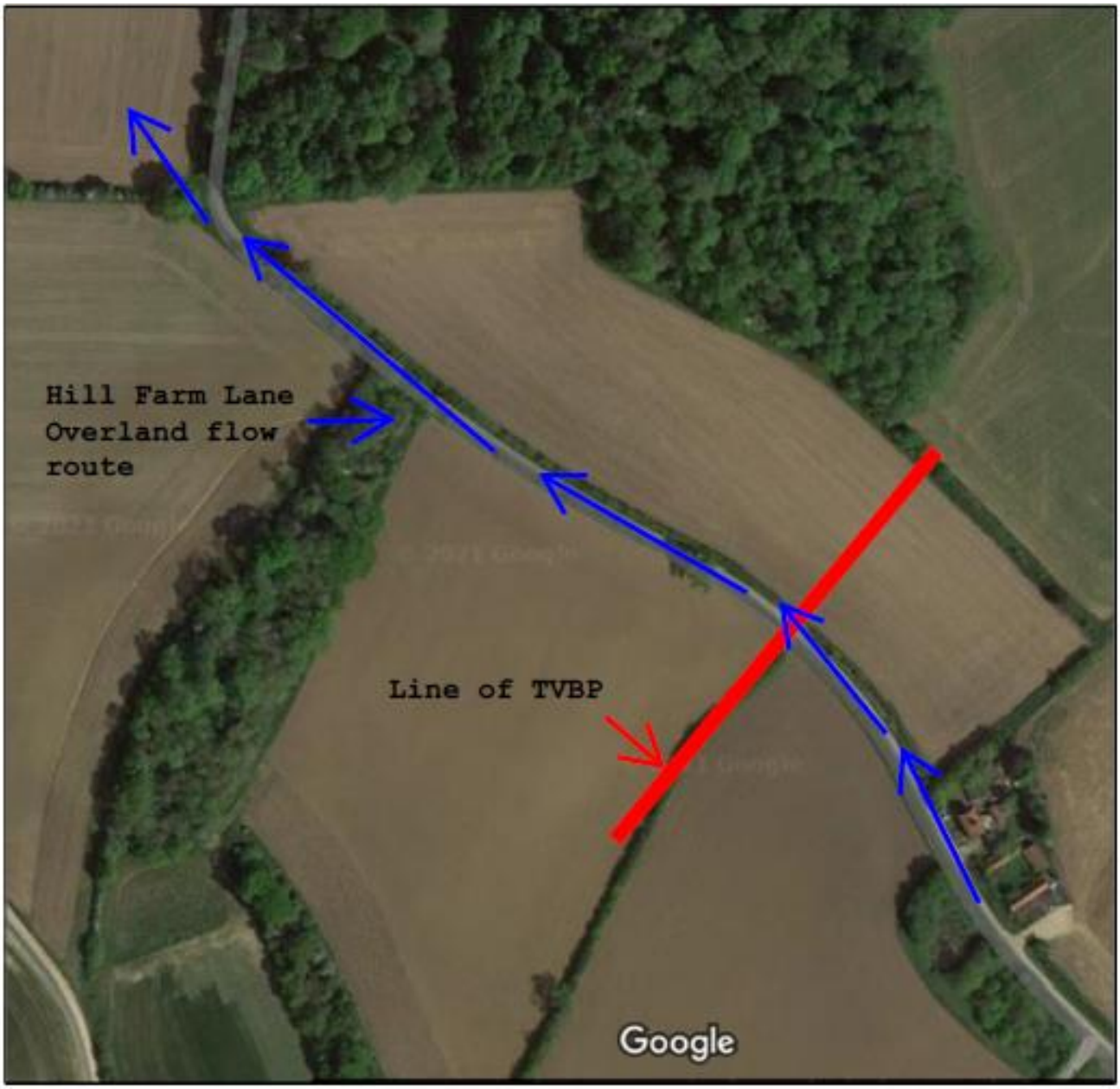
Plate 3: Existing A12 at the location of two village bypass western roundabout

5.1.3 For part of the southbound carriageway where there is no kerb, runoff is over the edge and onto the verge.

5.1.4 During the GPR utility survey the gullies and kerb gullies were inspected and all found to be silted up to an extent which prevented survey to establish the outfall routes. No surface water manholes were identified. As a result, it is assumed that all of the gullies and kerb gullies discharge to soakaway.

5.1.5 Further to the east the proposed two village bypass route cuts across the line of Hill Farm Lane and connectivity is retained through the provision of offset staggered T junctions. The current layout of Hill Farm Lane is shown in **Plate 4**.

Plate 4: Hill Farm Lane showing line of two village bypass and overland flow path



5.1.6 From survey data it can be seen that there is steep fall in level along Hill Farm Lane from Pond Barn Cottages, south of the line of two village bypass, to the north. This fall was noted during the site visit. No surface drainage outlets or formal infrastructure exists. As shown in **Plate 5** there are high banks on either side of the road. These contain runoff within the

road and this flows downhill to a bend in the road where it runs off into a field to the north west.

Plate 5: Hill Farm Lane showing high banks

5.1.7 The existing section of the A12 to the east of Farnham will be modified with the construction of the two village bypass eastern roundabout is shown in **Plate 6**. It does have a formal drainage network which has been identified and recorded as part of the GPR utility survey. The GRP survey traced the line of some highway drains but no outfall has been identified.

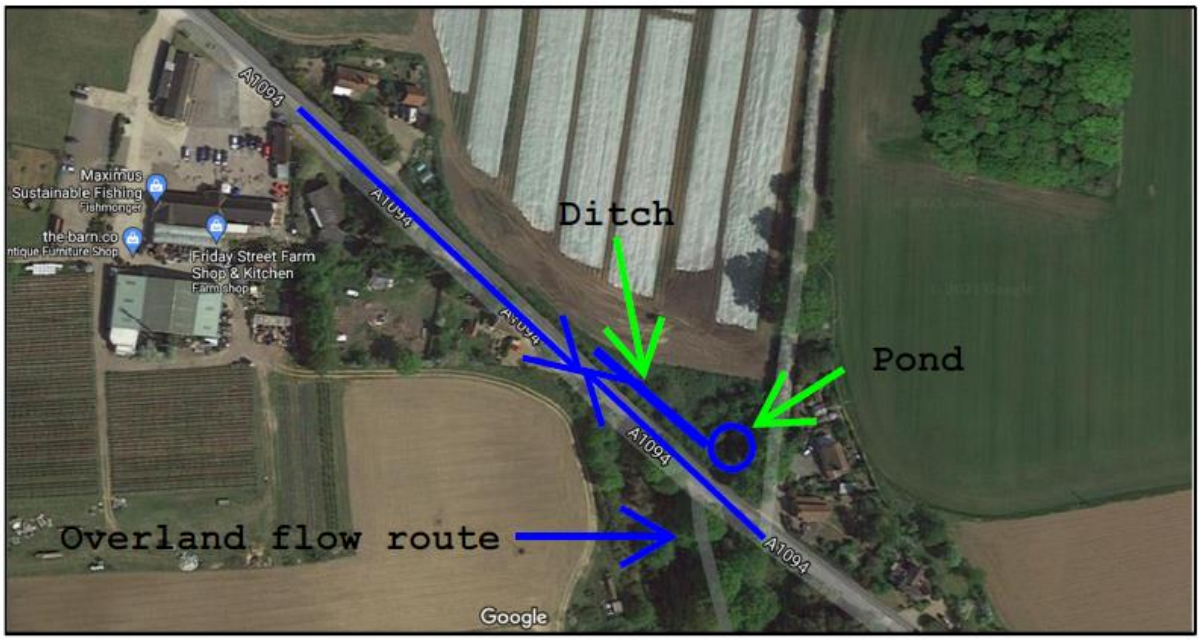
Plate 6: Existing A12 and A1094 junction at the location of two village bypass eastern roundabout

5.1.8 During the GPR utility survey a large number of gullies and kerb gullies were inspected and all found to be silted up to an extent which prevented survey to establish their outfall routes.

5.1.9 The junction of A12 and A1094 forms a local low point. The eastbound carriageway is lower than the westbound carriageway. The westbound carriageway has a crossfall to the centre reserve. Any runoff that does not get removed via gullies and kerb gullies flows through the gap created by the junction turning lanes and ultimately reaches the eastbound carriageway channel line.

5.1.10 The A1094 from its junction with the A12 crest point, has a steep fall to the south east to a low point. Surface water overland flow passes from the crest point to the local low point where it is removed by a highway grip and discharges into an existing ditch. The ditch runs south east behind the highway boundary hedge and terminates in an existing pond as shown in **Plate 7**.

Plate 7: Existing A12 and A1094 junction at the location of two village bypass eastern roundabout



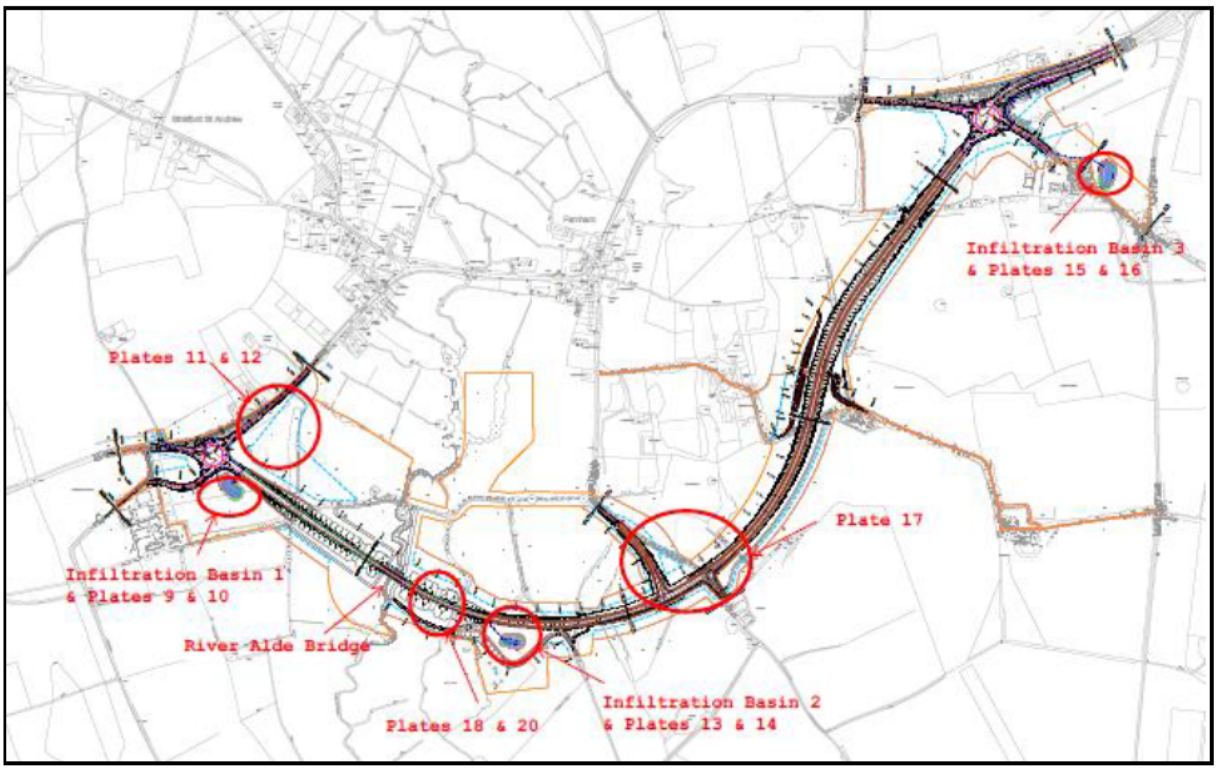
6 PRELIMINARY DRAINAGE DESIGN – HIGHWAY DRAINAGE

6.1.1 The results of geotechnical investigation infiltration testing undertaken at the proposed location of the three infiltration basins and at locations along the line of two village bypass demonstrate that it is possible to remove highway runoff by infiltration to ground. The infiltration rate data has been shared with SCC who have agreed that infiltration is achievable. Accordingly, the concept design proposal that highway runoff is removed and disposed by infiltration to ground remains broadly unchanged.

6.1.2 As agreed with SCC and the EA prior to DCO submission, the environmental impact of discharging highway runoff is to be assessed using the Highways England Water Risk Assessment Tool (HEWRAT) (Ref. 4) methodology. The assessment results confirm that a SuDS management train with the combination of swales, filter drains and infiltration basins, for the two village bypass discharges are low risk and therefore acceptable. SCC has indicated that they will wish to review the management train at detailed design stage and may wish to see provision of additional treatment stages.

6.1.3 A large-scale plan showing the route of the two village bypass is shown in **Plate 8.** The specific locations shown in subsequent Plates are identified for convenience.

Plate 8: Two village bypass location, route and features



6.1.4 The 3 proposed infiltration basins were shown schematically in the DCO drawings. As part of preliminary design, the highway drainage network has been developed using hydraulic modelling. This has enabled the required size of the basins to be determined and space has been allocated.

6.1.5 The location and performance of the A12 West Roundabout infiltration basin 1 is shown in **Plate 9** and the current dimensions hydraulic performance is shown in **Plate 10**.

Plate 9: A12 west roundabout with infiltration basin 1

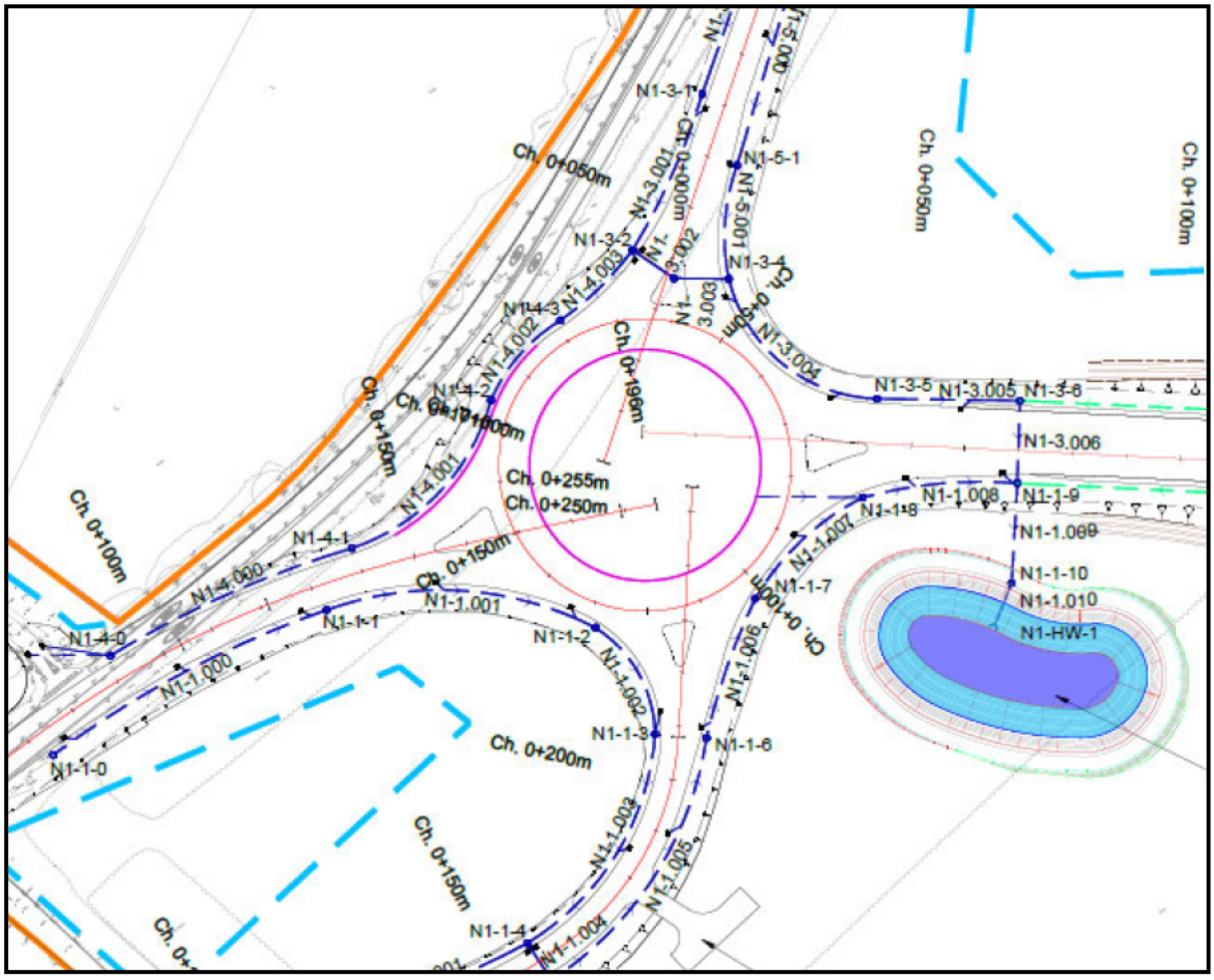


Plate 10: Two village bypass infiltration basin 1 approximate size and hydraulic performance

INFILTRATION BASIN 1 PRELIMINARY DESIGN

BASIN INVERT LEVEL - 7.130 m

TOP OF BASIN LEVEL - 9.119 m

STORAGE VOLUME - 1527 m^3

STORAGE DEPTH - 1.989 m

FREEBOARD - 300 mm

INFILTRATION RATE - 0.11239 m/hr

PREDICTED MAXIMUM WATER LEVEL IN 1 YEAR RETURN PERIOD - 7.391 m AOD

PREDICTED MAXIMUM WATER LEVEL IN 5 YEAR RETURN PERIOD - 7.576 m AOD

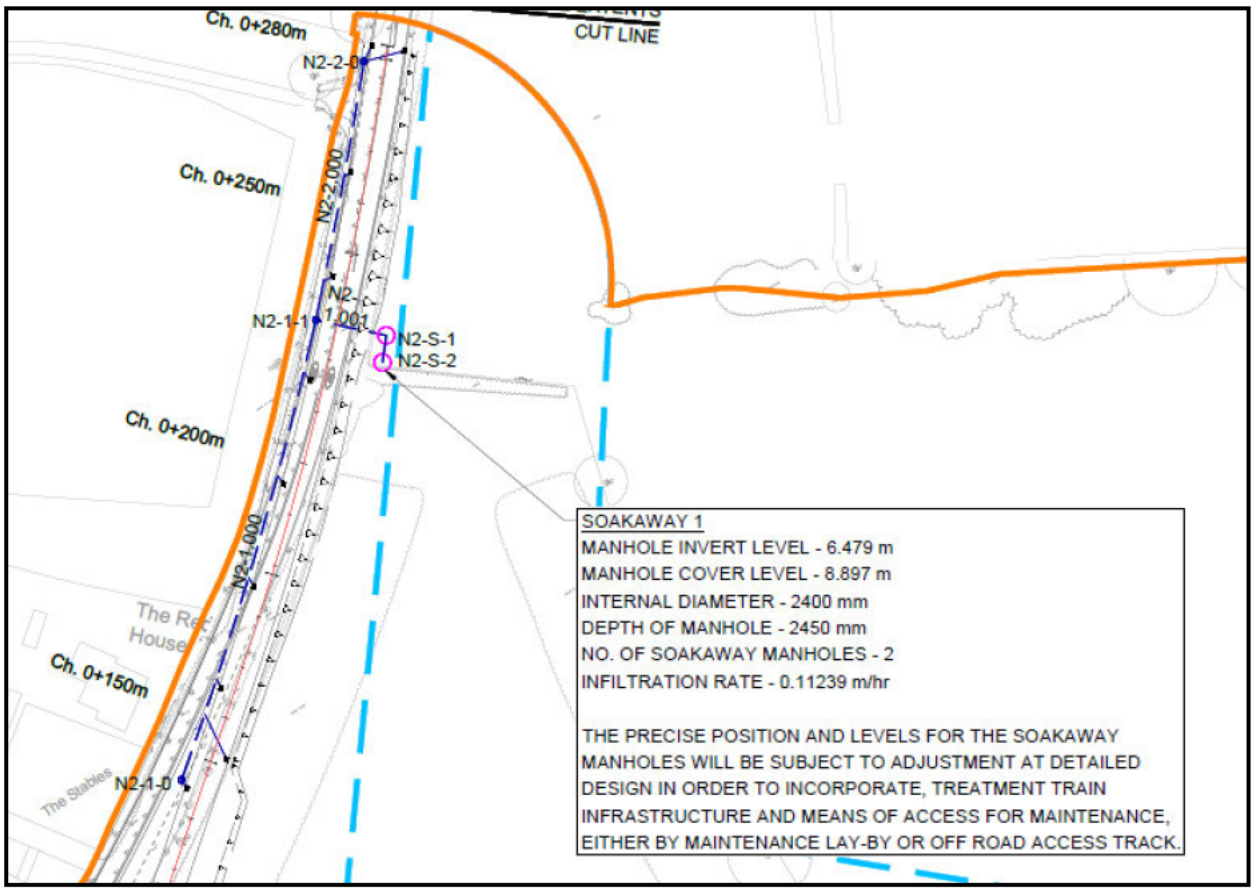
PREDICTED MAXIMUM WATER LEVEL IN 100 YEAR +40 % CC RETURN PERIOD - 8.326 m AOD

THE PRECISE POSITION, SHAPE AND LEVELS FOR THE BASIN WILL BE SUBJECT TO ADJUSTMENT AT DETAILED DESIGN IN ORDER TO INCORPORATE, TREATMENT TRAIN INFRASTRUCTURE, POTENTIAL ECOLOGICAL ENHANCEMENT AND OPTIMISE EARTHWORKS.

6.1.6 In addition to the majority of the A12 Roundabout, the infiltration basin will also provide an outfall for highway runoff from the two village bypass embankment crossing of the River Alde floodplain.

6.1.7 As a result of receiving detailed topographic levels and development of highway gradients, it has become apparent that it is not practical to drain the full length of the roundabout northern arm, back to the infiltration basin as it would require the basin to be approximately 4 m deep and with potential interaction with groundwater. Accordingly, whilst the first 150 m of the northern arm does drain back to the infiltration basin, the remaining 130 m where the proposed road alignment ties into the existing A12 drains to the north and would discharge into proposed soakaway manholes which enable infiltration. The northern roundabout tie-in drainage arrangement, based on assumed performance using the same infiltration rate as infiltration basin 1, is shown in **Plate 11**.

Plate 11: A12 west roundabout northern arm with soakaway manhole location



6.1.8 Given its proximity to the infiltration basin and the fact that the existing highway appears to drain via local kerb drains or over the edge, infiltrating runoff to ground, it was reasonable to assume that the soakaways would work. The hydraulic modelling of the catchment used the infiltration rates applicable to the infiltration basin. However, it was agreed with SCC and as a reasonable precaution, that infiltration testing at the soakaway manhole location should be undertaken prior to commencing detailed design.

6.1.9 Field log sheets for infiltration testing have been received in May 2021. They indicate that infiltration rates are not sufficient at the proposed soakaway manhole location for the western roundabout northern arm. In consequence the layout contained in the preliminary design will not be acceptable. Further site investigation and consideration of alternative outfall arrangements will be required either in advance of or at the start of detailed design stage.

6.1.10 Potential options have been identified which provide for an outfall arrangement located entirely within the permanent land take areas. These include:

i. possible connection to the proposed infiltration basin with increased depth;

ii. moving the soakaway closer to the roundabout; or

iii. an outfall route along the line of the two village bypass embankment discharging into the local watercourse.

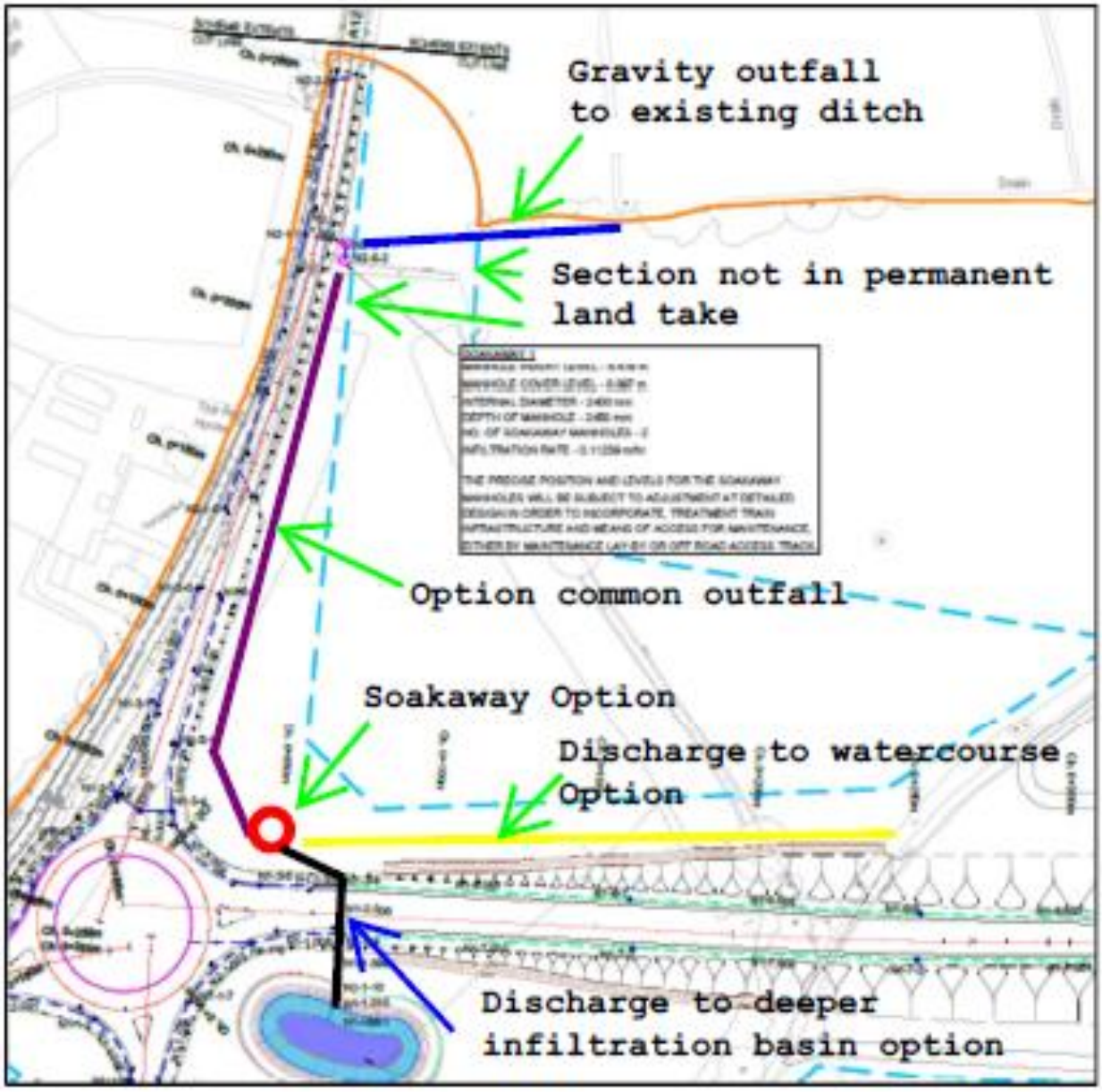
6.1.11 A further alternative option would be to

iv. discharge into a local ditch located within 100 m of the soakaway manhole.

6.1.12 The route would be located entirely within the red line boundary. However, it crosses land that is not retained and which will be transferred back to the landowner. SCC has confirmed that as a general position they do not require outfall highway drains to be located in land under their ownership. If this option was pursued, SCC would require a legal agreement in the form of an easement or wayleave providing a right to have the drain located in the land (not within their ownership) and a right of access for maintenance

6.1.13 The potential options are shown in **Plate 12**.

Plate 12: A12 west roundabout northern arm showing soakaway alternative options



6.1.14 Infiltration basin 2, east of the River Alde, remains in the same area indicated at DCO. It receives runoff from the two village bypass swales to the east. All runoff flowing along the swales and associated filter drains which does not infiltrate to ground is intercepted and diverted to the basin. This prevents the runoff overrunning onto the River Alde embankment.

6.1.15 Hydraulic modelling has been undertaken to determine the required location, size, depth and volume of the infiltration basin. Details are

provided in the first issue of the preliminary design drawings. Subsequent to issue it has been necessary to move the position of the basin to coordinate with the revised position and levels of the accommodation access track. The revised location of the infiltration basin will be shown either on an updated preliminary design drawing or in first revision of detailed design.

6.1.16 The DCO schematic location of infiltration basin 2 is shown in **Plate 13** and the current dimensions hydraulic performance is shown in **Plate 14**. The movement of the basin will nominally change the data in **Plate 14,** but it is included to demonstrate the technical feasibility of the design.

Plate 13: Two village bypass infiltration basin 2 location

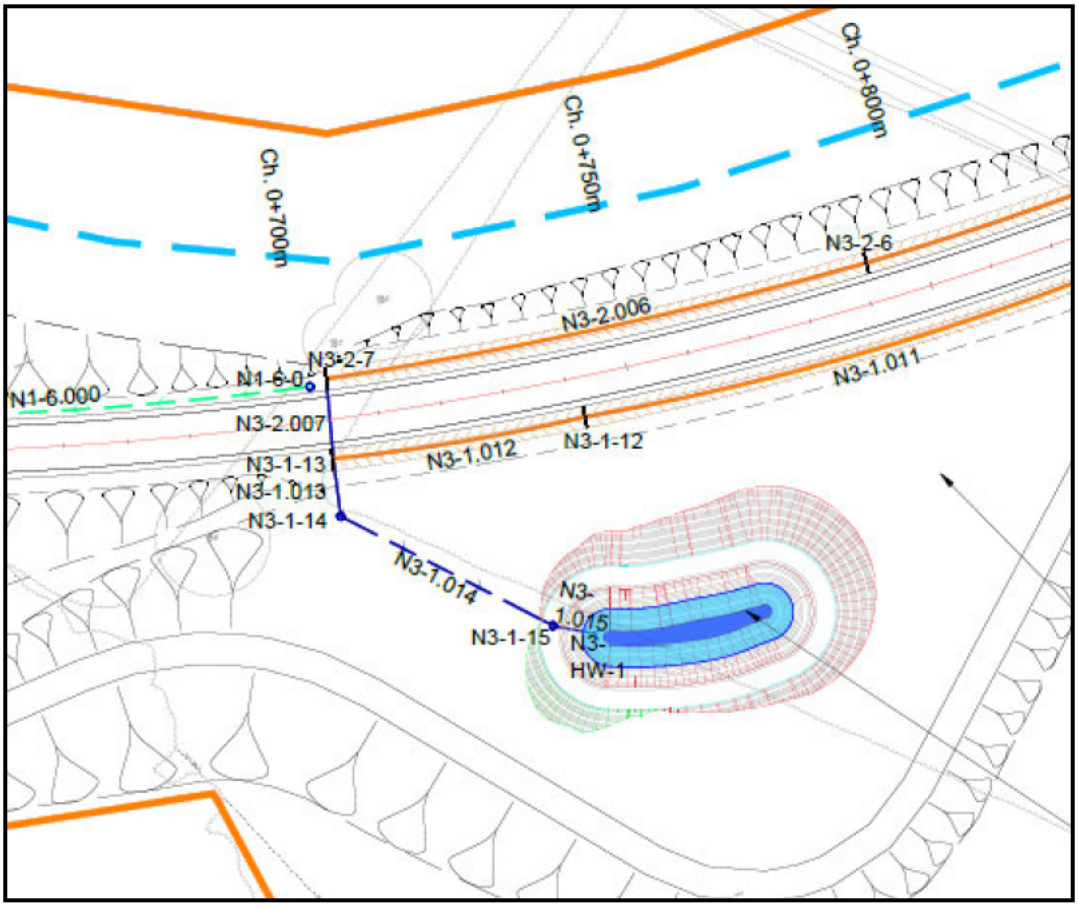


Plate 14: Two village bypass infiltration basin 2 approximate size and hydraulic performance

INFILTRATION BASIN 2 PRELIMINARY DESIGN
BASIN INVERT LEVEL - 12.124 m
TOP OF BASIN LEVEL - 13.810 m
STORAGE VOLUME - 611 m^3
STORAGE DEPTH - 1.686 m
FREEBOARD - 300 mm
INFILTRATION RATE - 0.82005 m/hr
PREDICTED MAXIMUM WATER LEVEL IN 1 YEAR RETURN PERIOD - 12.267 m AOD
PREDICTED MAXIMUM WATER LEVEL IN 5 YEAR RETURN PERIOD - 12.287 m AOD
PREDICTED MAXIMUM WATER LEVEL IN 100 YEAR +40 % CC RETURN PERIOD - 12.771 m AOD
THE PRECISE POSITION, SHAPE AND LEVELS FOR THE BASIN WILL BE SUBJECT TO ADJUSTMENT AT DETAILED DESIGN IN ORDER TO INCORPORATE, TREATMENT TRAIN INFRASTRUCTURE, POTENTIAL ECOLOGICAL ENHANCEMENT AND OPTIMISE EARTHWORKS.

6.1.17 The location and performance of the A12 East Roundabout infiltration basin 3 is shown in **Plate 15**. and the current dimensions hydraulic performance is shown in **Plate 16.**

Plate 15: A12 east roundabout infiltration basin 3 location

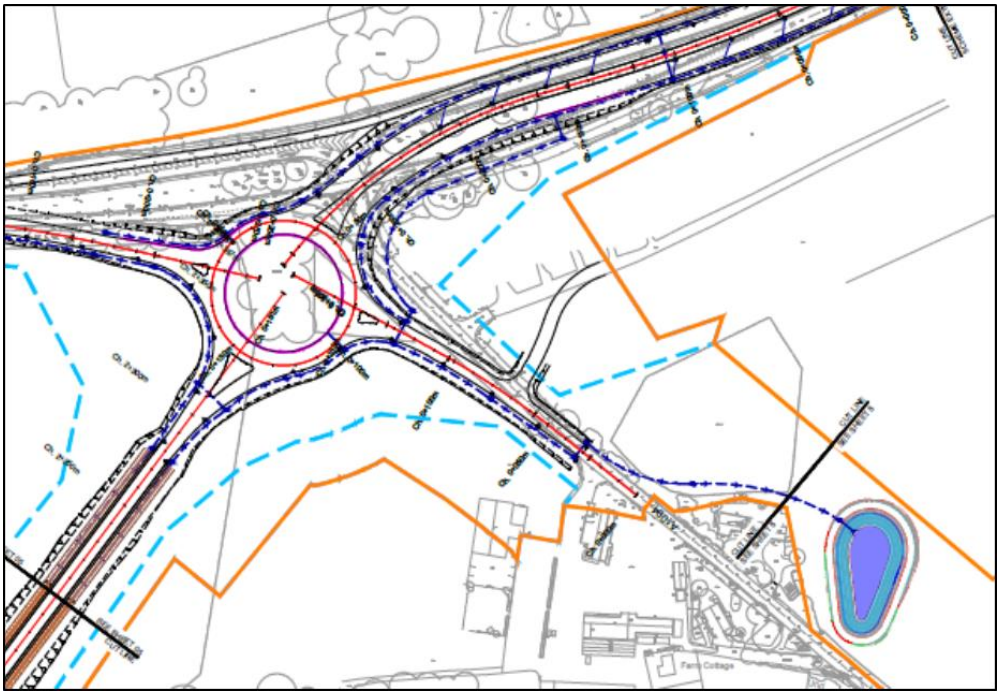


Plate 16: Two village bypass infiltration basin 3 approximate size and hydraulic performance

INFILTRATION BASIN 3 PRELIMINARY DESIGN
BASIN INVERT LEVEL - 9.914 m
TOP OF BASIN LEVEL - 11.700 m
STORAGE VOLUME - 1512 m^3
STORAGE DEPTH - 1.786 m
FREEBOARD - 300 mm
INFILTRATION RATE - 0.12611 m/hr
PREDICTED MAXIMUM WATER LEVEL IN 1 YEAR RETURN PERIOD - 10.511 m AOD
PREDICTED MAXIMUM WATER LEVEL IN 5 YEAR RETURN PERIOD - 10.631 m AOD
PREDICTED MAXIMUM WATER LEVEL IN 100 YEAR +40 % CC RETURN PERIOD - 11.269 m AOD

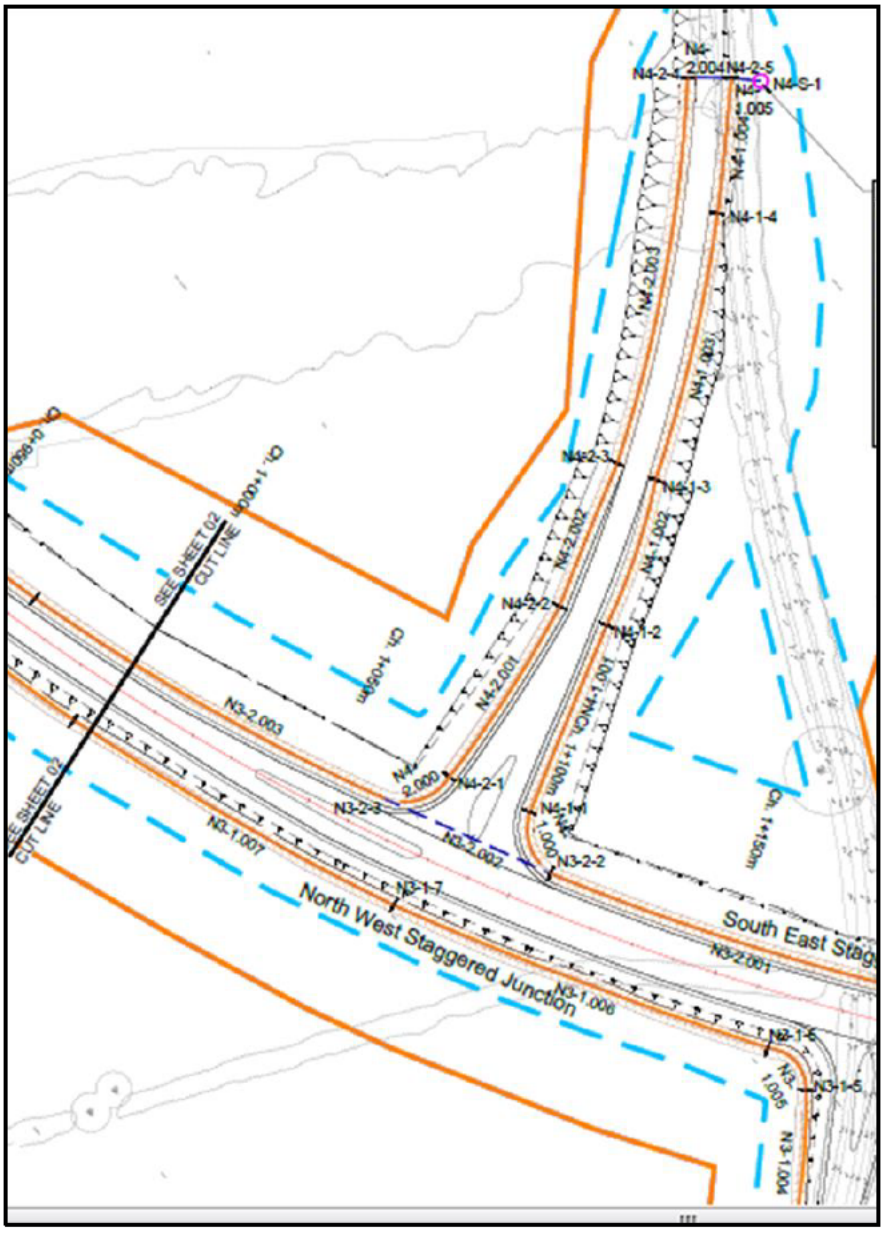
THE PRECISE POSITION, SHAPE AND LEVELS FOR THE BASIN WILL BE SUBJECT TO ADJUSTMENT AT DETAILED DESIGN IN ORDER TO INCORPORATE, TREATMENT TRAIN INFRASTRUCTURE, POTENTIAL ECOLOGICAL ENHANCEMENT AND OPTIMISE EARTHWORKS.

6.1.18 The infiltration basin receives all the runoff from the A12 East Roundabout and its arms. It also receives some runoff from the northern part of the two village bypass that has not fully infiltrated via the swales and filter drains.

6.1.19 The infiltration basin remains located in the same field adjacent to the A1094 but has been moved further north. This change has been made following the discovery of the ditch and pond described in section 5.1.10 and shown in **Plate 7**. If the infiltration were to be located in proximity to the pond the efficiency of infiltration could be reduced because the additional infiltration could cause local rising of groundwater.

6.1.20 As described in section 5.1.5, and shown in **Plate 17**, Hill Farm Lane is severed by the proposed two village bypass route with a proposed staggered junction arrangement being provided for connectivity.

Plate 17: Two village bypass Hill Farm Lane junction with soakaway manhole location



6.1.21 The DCO Drainage Strategy assumed that runoff from Hill Farm Lane would discharge to swales and filter drains allowing infiltration to ground.

6.1.22 The section of Hill Farm Lane to the south, which is at a higher level than two village bypass, has swale/filter drains which discharge into those proposed alongside the two village bypass, and for which Infiltration testing achieves satisfactory results.

6.1.23 The section of Hill Farm Lane to the north is at a lower level that two village bypass. A borehole excavated next to this side road found cohesive material which typically has poor infiltration rates and therefore would suggest that infiltration would not be viable. Based on available data it was considered that granular material would be found at a deeper depth below the cohesive material at a depth of around 5 m.

6.1.24 Discussions have taken place with SCC. Since it is agreed that there are no watercourses to which discharge can be made, it has been agreed that subject to detail, in principle a deep borehole soakaway could be permitted, providing evidence of the underlying granular material at reasonable depth is proven.

6.1.25 Results of a borehole excavation have been received in May 2021 and confirm the presence of the granular material at depth of 3.2 m bgl, adjacent to Hill Farm Lane. Infiltration testing results demonstrate that flow passes through into the permeable strata and that hence infiltration will be suitable. As agreed with SCC, when construction takes place, excavation will be made down into the granular material and an infiltration test to an appropriate standard (e.g. BRE Digest Soakaway design: DG 365 – 2016 (Ref. 3)) will be undertaken. The required size of soakaway manholes will be determined by the results.

7 REVISED DRAINAGE DESIGN STRATEGY – RIVER ALDE CROSSING

7.1.1 The position of the embankment with its flood relief culverts and the 60 m wide bridge remain as shown in the DCO drawings and as hydraulically modelled, with only minor changes which do not change hydraulic performance as reported in the **Two Village Bypass FRA**.

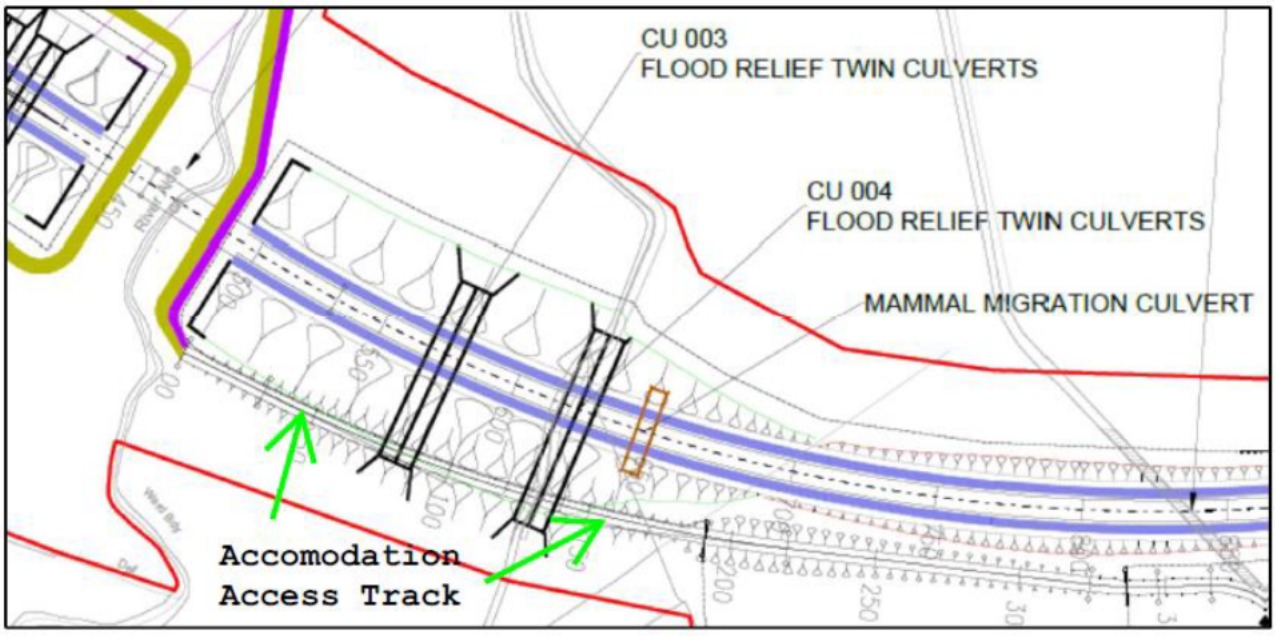
7.1.2 Following review of the topographic survey the central piers of the bridge have been moved to create greater distance from the proven position of the River Alde and its banks. The central span is increased to a width of 30 m and the side spans reduced to 15 m. The change is made to reduce the risk of scour should the river move its position and to provide a better width between top of bank and pier for maintenance. The reduction in side span widths does not adversely impact on the access track which is provided.

7.1.3 It is confirmed that this modification of piers does not cause any change to the hydraulic modelling results.

7.1.4 The change to the bridge pier positions has been notified to and discussed with SCC and the EA in design review meetings and no objection was raised.

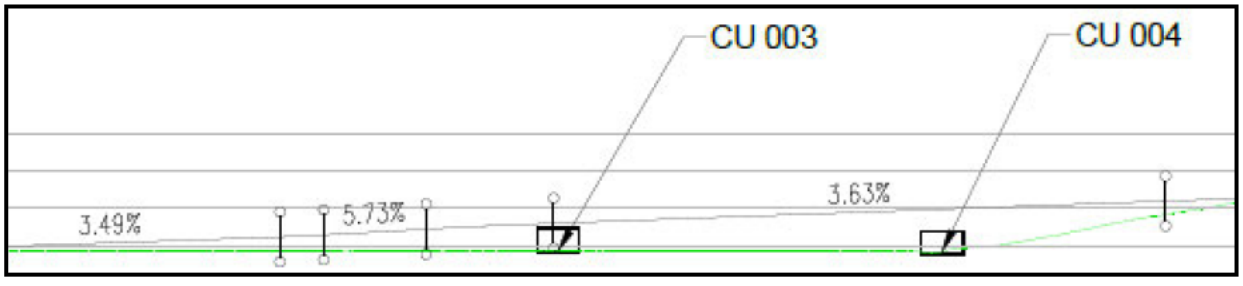
7.1.5 An accommodation access track is shown on the DCO drawing extract in **Plate 18**. This passes under the bridge on the east side of the River Alde and then follows in parallel alongside the downstream side of the proposed embankment and over the flood relief culverts as shown in **Plate 19**.

Plate 18: Two village bypass accommodation track east of the River Alde at DCO Submission



7.1.6 The culvert lengths were reviewed to meet an EA request to achieve a maximum length of 50m. The flood relief culverts CU003 and CU004 have a length of 65 m, and the flood relief culverts to the west have a length of 40m.

Plate 19: two village bypass accommodation track east of the River Alde – long section



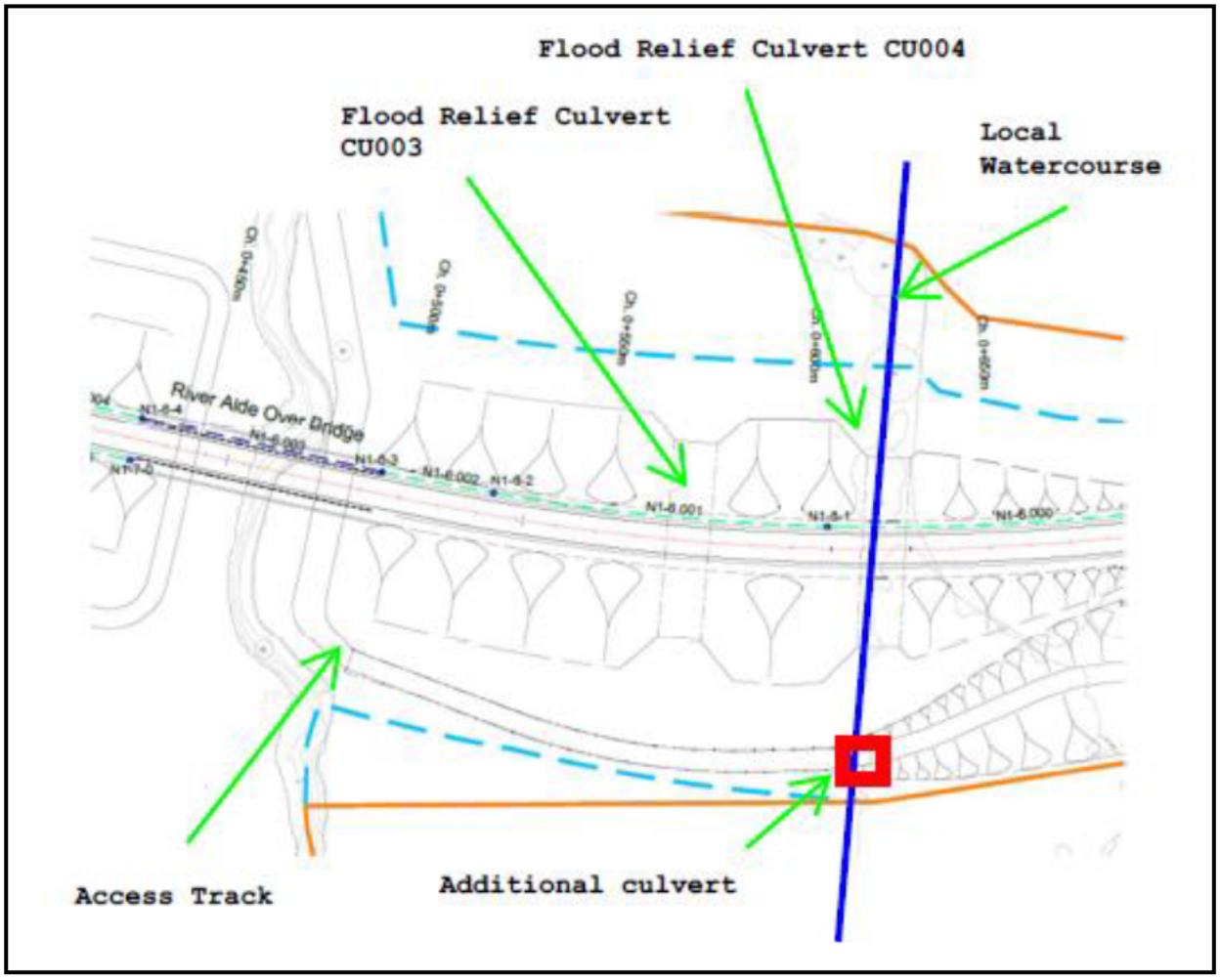
7.1.7 In order to reduce the length of culverts CU003 and CU004, it has been proposed that the accommodation track be laid at existing ground levels in

front of the toe of the embankment but with a steeper section to the east to achieve the higher tie-in levels at Hill Farm Road.

7.1.8 A residual impact of the accommodation track amendment is that, for the watercourse which passes through flood relief culvert CU004, there is a requirement for a new downstream culvert where the proposed track crosses.

7.1.9 The accommodation track amendment and associated alterations has been notified to and discussed with SCC and the EA in Design Review Meetings and no objection in principle was raised. The shortening for the length of the flood relief culverts albeit with the new downstream culvert crossing is the preferred solution. The revised arrangement is shown in **Plate 20.** Accordingly, SZC Co. has submitted a design amendment into consultation.

Plate 20: Two village bypass accommodation track and flood relief culverts east of the River Alde – revised arrangement



7.1.10 As part of structural design, the form of the flood relief culverts has been considered. Whilst the cross-sectional dimensions of the culverts remain unchanged, it has been decided that portal culvert structures will be proposed. The advantage of this is that the portal culvert better allows for the watercourse to pass through culvert CU004.

7.1.11 The same portal form of culvert is proposed for the watercourse and track which passes under the embankment to the west of the River Alde at chainage 210 m. This culvert is located just clear of the River Alde floodplain extent also provides a mammal crossing point beneath the embankment.

7.1.12 The DCO design included for the provision of a dedicated mammal crossing culvert to the east of culvert CU004 at chainage 650 m but this is some distance clear of the flood plain. As discussed with the EA it is acceptable to delete this culvert and replace it with a mammal ledge in culvert CU004 to better follow the flood plain extent and existing watercourse route. The mammal ledge is to be installed above the 1 in 100 year plus 40% climate change flood level.

7.1.13 During the joint site inspection with SCC which took place on 12 January 2021 it was confirmed that swales at the toe of embankment within the River Alde flood plain would not serve useful purpose as they will be regularly flooded.

7.1.14 The EA confirmed that the predicted limited increase in flood levels adjacent to the upstream side of the embankment is acceptable subject to agreement with the landowner.

7.1.15 SZC Co. has reached agreement with the landowner in a form that satisfies the EA. Accordingly, the provision of flood compensation areas (within the concept design) is deleted from the preliminary design.

7.1.16 During liaison SCC confirmed that there must be no infiltration directly adjacent the carriageway for highway runoff where drainage is located on top of the road embankment as SCC were concerned of erosion within the embankment layers. It was suggested to SCC that the section highway on the embankment could drain to either a linear channel drain or surface V channel and be removed by an underground drain discharging to the infiltration basin to the west and adjacent to the A12 roundabout. SCC stated that a linear channel drain would not be acceptable due to maintenance concerns. For the preliminary design the indicative proposed swales are replaced by options of either: surface V channel and gully; or kerb and gully infrastructure. The drainage options have been discussed with SCC in design review meetings and the preliminary design currently

proposes the use of concrete surface V channels and gullies. However, following recent review and consideration of integration with landscaping, SZC Co. is exploring a design alternative which provides for a vegetated surface with filtration layer and impermeable membrane below to ensure no infiltration to ground and this will be reviewed at the next design stage. Any proposed alternative would be discussed with and approved by SCC.

8 VALIDATION OF OUTLINE DRAINAGE STRATEGY

8.1.1 In accordance with the drainage hierarchy, the **Outline Drainage Strategy** [REP2-033] proposed the primary use of infiltration, with additional use of attenuation techniques (e.g. basins and swales) to manage water quality and to further promote infiltration. The **Outline Drainage Strategy** is validated by the completed preliminary design.

8.1.2 The preliminary design documents will be made available for review and acceptance by SCC and the EA with respect to potential adoption of the two village bypass by SCC and for required regulatory consents.

9 SUMMARY AND CONCLUSION

9.1.1 The purpose of this technical note is to provide details of how the concept design has needed to evolve and develop as a result of provision of new information. The proposed developments have been discussed with SCC and the EA in liaison and through design review meetings.

9.1.2 The highway drainage has been designed in accordance with Design Manual for Roads and Bridges, the CIRIA SUDs Manual C753 (Ref. 4) and to comply with stated requirements of SCC contained in their SUDs Local Design Guide Appendix A (Ref. 5).

9.1.3 At this preliminary design stage, it is considered that the design provides for the effective removal, treatment and disposal of highway runoff without adversely increasing flood risk to or from watercourses, impacting on third parties. The flood risk performance of the highway is as specified in DMRB and SCC guidance.

REFERENCES

1. Design Guide, Suffolk County Council, 2000, https://www.suffolk.gov.uk/planning-waste-and-environment/planning-and-development-advice/suffolk-design-guide-for-residential-areas/

2. Highways Agency et al. (2009). Volume 11, Section 3, Part 10: Road Drainage and the Water Environment, HD45/09. http://www.standardsforhighways.co.uk/ha/standards/dmrb/vol11/section3/hd4509.pdf

3. BRE Digest Soakaway design: DG 365 – 2016, BRE, 2016 https://www.brebookshop.com/details.jsp?id=327592

4. The SUDs Manual (C753), CIRIA, 2015, ISBN 978-0-86017-760-9.

5. Sustainable Drainage Systems (SuDS) a Local Design Guide Appendix A to the Suffolk Flood Risk Management Strategy, Suffolk County Council, May 2018 https://www.greensuffolk.org/app/uploads/2021/05/2018-10-01-SFRMS-SuDS-Guidance-Appendix-A-.pdf

APPENDIX H

YOXFORD ROUNDABOUT UPDATED DRAINAGE STRATEGY

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FIGURES

None provided.

APPENDICES

None provided.

1 INTRODUCTION

1.1.1 NNB Generation Company (SZC) Limited (SZC Co.) submitted an application for a Development Consent Order (DCO) to the Planning Inspectorate under the Planning Act 2008 for the Sizewell C Project (referred to as the 'Application') in May 2020. The Application was accepted for examination in June 2020.

1.1.2 SZC Co. has undertaken work to validate and develop the design of the Yoxford roundabout that was originally submitted as part of the DCO application. This document forms one of a series of design validation and evolution documents being provided to the Examining Authority in support of the **Outline Drainage Strategy** [REP2-033].

1.1.3 The Yoxford roundabout forms one of the Associated Developments (AD) which are required to mitigate traffic impacts arising from the main development site. The Yoxford roundabout consists of a new three arm roundabout, which includes the realignment of the existing A12 and B1122 Middleton Road, and the removal of the existing A12 and B1122 ghost island junction.

1.1.4 Yoxford roundabout modifies the existing public highway and as such will continue to form part of the highway network maintained by Suffolk County Council (SCC). As a result, it will require to be designed to meet SCC adoptable standards (Ref. 1).

1.1.5 Yoxford roundabout highway modifications will continue to generate surface water highway runoff which will require to be removed, treated as necessary and disposed.

2 PURPOSE

2.1.1 The **Outline Drainage Strategy** [REP2-033] identified at concept level the proposed drainage approach for the effective removal of runoff from the proposed Yoxford roundabout highway and its disposal.

2.1.2 This drainage strategy was developed in consultation with drainage regulators and local authorities, including SCC and the Environment Agency (EA). A number of workshops were held and the observations/requirements of drainage regulators were incorporated in the strategy.

2.1.3 The proposed drainage infrastructure was included in the concept design submitted as part of the DCO application. This concept design was based on data and information available at that time.

2.1.4 Following the provision of new data, and subsequent to the DCO submission, SZC Co. has developed the concept level design to preliminary design stage.

2.1.5 The purpose of this technical note is to provide details of how the concept design has been modified in response to the new data, such that it continues to provide for the effective and satisfactory drainage of Yoxford roundabout, without unacceptable adverse impact on the water environment, both in terms of flood risk and pollution.

2.1.6 The content of this technical note summarises the design details and approach already shared in a series of design review meetings held with key stakeholders, including the EA and SCC.

3 DESCRIPTION OF DCO DRAINAGE DESIGN STRATEGY

3.1.1 Based on available data at that stage, the concept design for the disposal of highway runoff was by infiltration to ground. However, it was not possible to undertake geotechnical investigation to confirm actual infiltration rates at that stage.

3.1.2 The drainage strategy provided for traditional drainage at the A12/B1122 roundabout and its east, north and southwest arms with a combination of highway gullies and combined kerb drains (CKDs) collecting runoff and discharging via carrier drains to an infiltration basin where runoff would infiltrate to ground.

3.1.3 The required size of the infiltration basin required for the roundabout runoff could not be accurately determined without validated infiltration rates. As a result, it was shown schematically and sufficient space within the red line boundary was provided. The position of the infiltration basin is to the south of the roundabout as shown in **Plate 1**, shaded blue. It is intended that the basin be integrated within a landscaped area shaded green.

Plate 1: Proposed location of infiltration basin at concept design stage

3.1.4 At concept design stage it was not clear as to whether the full extent of the modified highway B1122 Eastern Arm and A12 Northern Arm would be able to drain by gravity to the infiltration basin. However, the extent of carriageway discharging to the north and east would be reduced.

3.1.5 Similarly, and in accordance with SCC aspirations, the extent of carriageway draining via the highway drainage network into Yoxford would be substantially reduced.

4 ADDITIONAL INPUT DATA

4.1.1 The preliminary drainage design has been developed based on the concept design but modified to take account of data which has become available since DCO submission.

4.1.2 The new data which informs the design is listed below

- Drone topographic survey
- Aerial view from drone flyover
- Ground investigation and infiltration testing
- Ground penetrating radar (GPR) survey
- Additional traditional topographic survey of critical locations
- Site visits and inspection of Yoxford roundabout on 12 January 2021 and 24 February 2021
- Highways England Water Risk Assessment Tool (HEWRAT) (Ref. 2)

4.1.3 The design development has also evolved through the design review meetings held with SCC and between SZC Co. and SCC's Lead Local Flood Authority (LLFA) officer. Comments and requirements confirmed by SCC have been recorded in minutes of the review meetings and taken into account.

4.1.4 The final draft preliminary design has been submitted to SCC as the Highway Authority, to SCC as LLFA, and the EA. Any final comments can be addressed in the preliminary design drawings and reports, prior to issue as final design.

5 EXISTING HIGHWAY DRAINAGE ARRANGEMENTS

5.1.1 Since Yoxford roundabout replaces the existing T-junction of the A12 and B1122 highways and ties back into them to the east, north and southwest, it is necessary to take account of existing highway drainage and catchment areas in the design of drainage required for Yoxford roundabout.

5.1.2 The existing highway drainage is owned and maintained by SCC as Highway Authority. Liaison has taken place with SCC and although there are currently no formal plans showing the existing highway drainage infrastructure, SCC has been able to describe the drainage from the

junction of the A12/B1122 into Yoxford village and separately the B1122 to the east. The accuracy of these descriptions has been validated by site inspection.

5.1.3 During liaison SCC confirmed that the downstream drainage network in Yoxford has no spare capacity and there are existing flooding problems. As a result, no additional highway paved area can be connected to the highway drainage network that outfalls into Yoxford.

5.1.4 SCC has no knowledge of any flooding issues with the local highway drainage network which drains the B1122 to the east of Yoxford and outfalls via the track leading to the sewage treatment works.

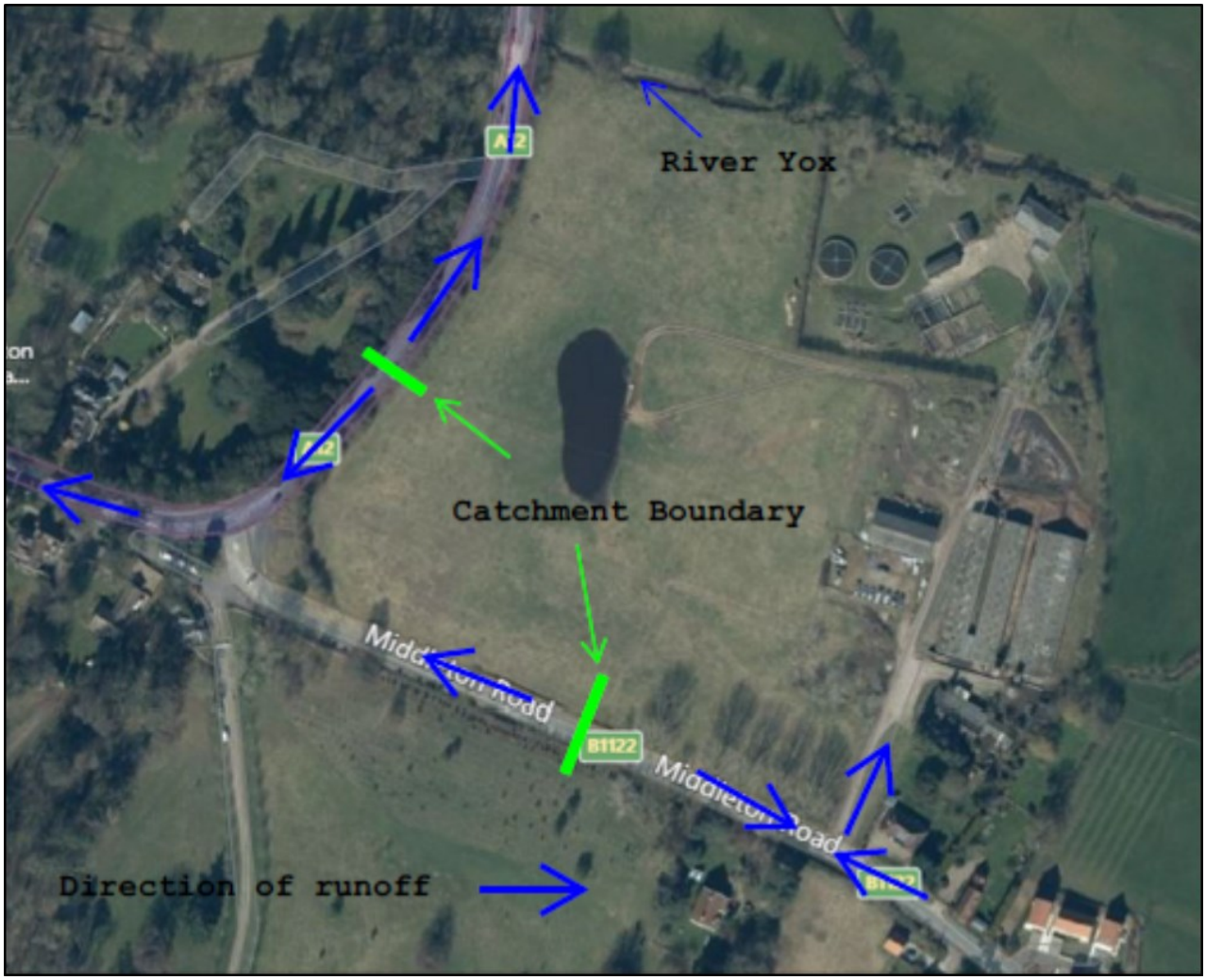
5.1.5 SCC was not able to confirm details of highway drainage on the A12 to the north of the road high point which falls towards the River Yox. Following site inspection, the presence of 2 gullies was noted on the northbound carriageway next to the Satis House entrance. However, there is no evidence of any highway drain or outfall into the River Yox for either northbound or southbound carriageways. Highway runoff is removed by overland flow across the River Yox bridge and then by a series of gullies which appear to outfall into drainage ditches which in turn discharge into the River Yox.

5.1.6 In summary it can be confirmed that there are 3 existing catchments within the extent of the Yoxford roundabout scheme:

- A12/B1122 outfalling southwest into Yoxford
- A12 outfalling north to the River Yox
- B1122 outfalling north

5.1.7 The extent of these catchments is shown in **Plate 2**.

Plate 2: Existing highway layout showing catchment boundaries and overland flow paths



6 PRELIMINARY DRAINAGE DESIGN

6.1.1 The results of Geotechnical Investigation with infiltration rate testing at the site of the infiltration basin demonstrate that it is possible to remove highway runoff by infiltration to ground. The infiltration rate data has been shared with SCC who has agreed that infiltration is achievable. Accordingly, it is proposed that highway runoff is removed and disposed by infiltration to ground to the extent possible.

6.1.2 In order to drain the maximum area into the infiltration basin located south of the roundabout the base level for the basin has been set at 10.5 mAOD. Side slopes for the basin have been set at 1 in 4 which is in accordance with SCC guidance. Hydraulic modelling demonstrates that the basin does fit within available space as shown in **Plate 3** with a maximum depth of water predicted to be 0.857 m during a 1 in 100 year return period rainfall event plus 40% allowance for climate change. The calculated maximum depth of attenuated water is on the basis that the base of the basin is lined and that infiltration is through the basin sides. This arrangement is required following completion of the HEWRAT assessment.

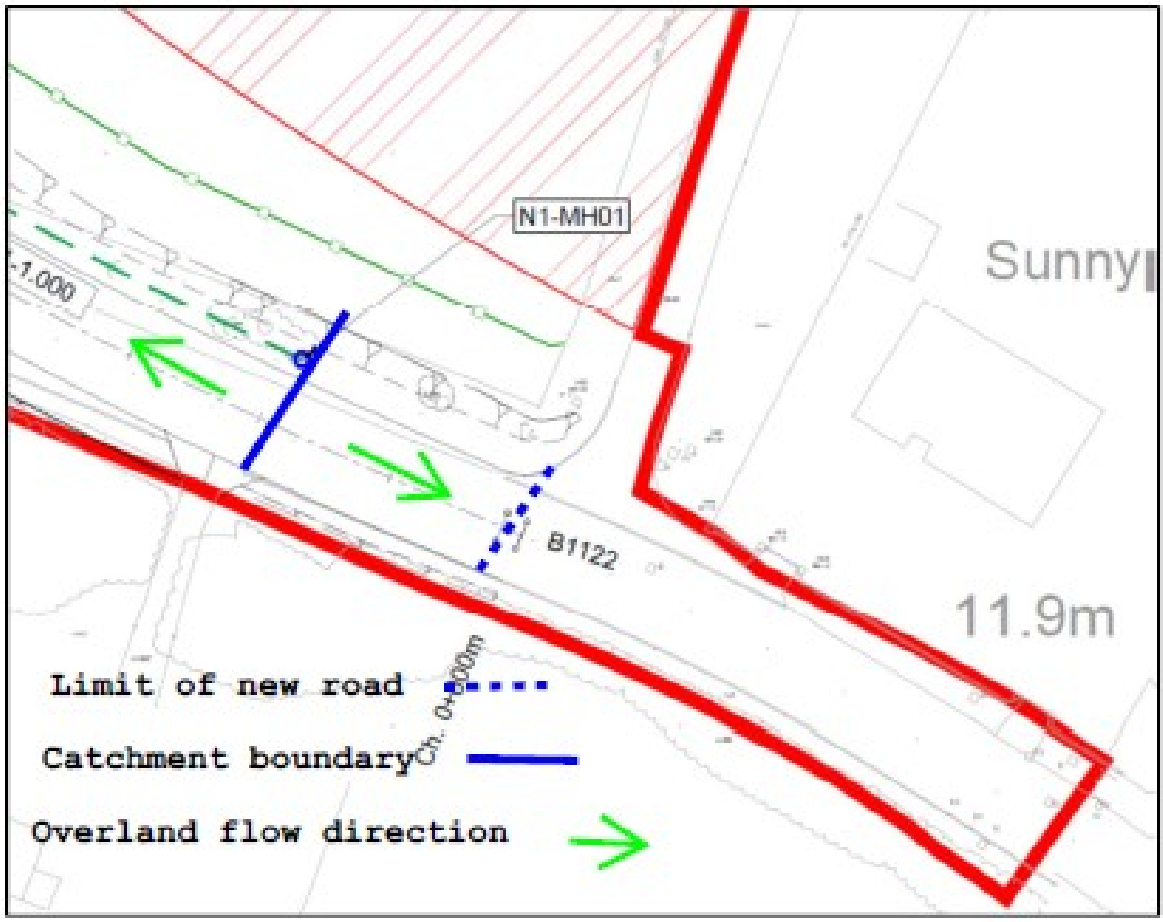
Plate 3: Infiltration basin footprint

6.1.3 The DCO drainage strategy allowed for removal of surface water highway runoff by use of gullies and combined kerb drains (CKDs). This strategy continues to apply for the roundabout and A12 southern arm. However, as part of design development, clear of the roundabout the southbound carriageway of the A12 northern arm and the eastbound carriageway of the

B1122 will discharge “over the edge” and into filter drains. The filter drain arrangement will also ensure that any runoff from the cutting adjacent the road is collected and does not flow onto the road.

6.1.4 A short 20 m section of the B1122 at the tie into existing road is not able to drain back against the road longfall and to the infiltration basin. The existing road has no formal drainage and overland flow follows the falling gradient to the east of the junction with the sewage treatment works access track at which point it is collected in existing gullies. The area is shown in **Plate 4** and as can be seen by reference to **Plate 2** the length of road discharging runoff by overland flow is reduced by approximately 80 m. Given this reduction and no evidence of flooding issues, it is not intended to provide any new formal surface drainage for removal of runoff on this section.

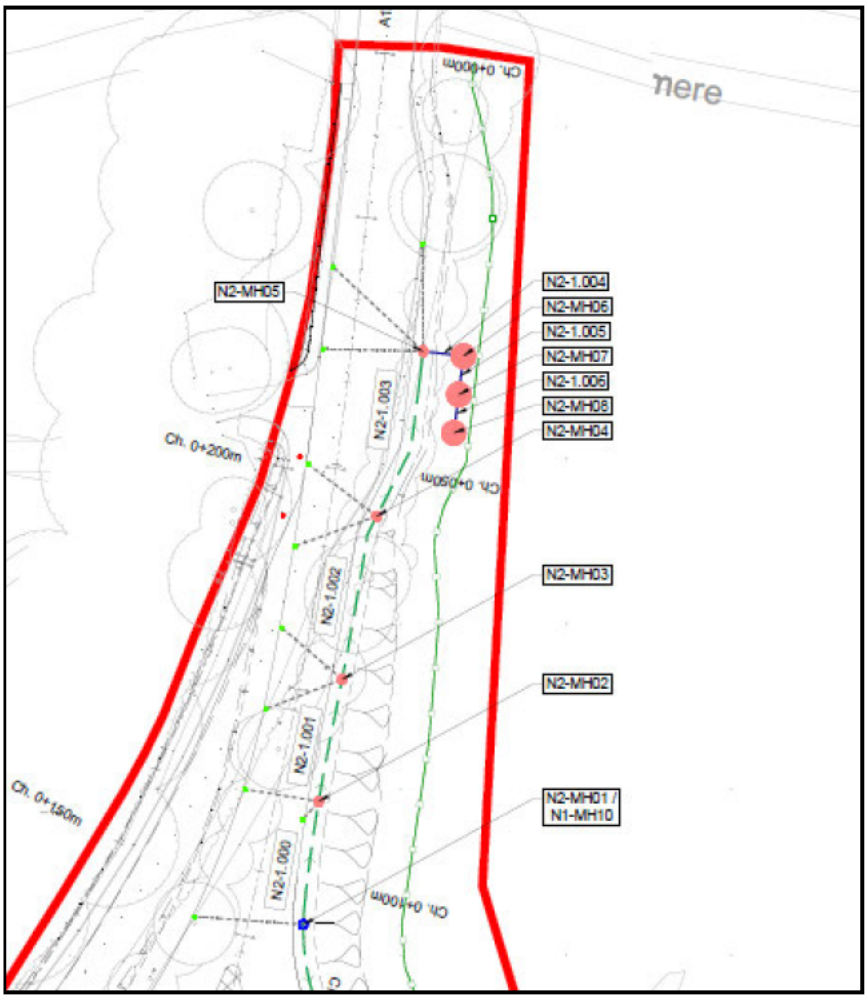
Plate 4: 20 m length of B1122 with no formal drainage



6.1.5 Most of the northern arm of the roundabout cannot drain back against the road longfall and to the infiltration basin by gravity. The length of this section of the A12 is approximately 100 m to the crossing of the River Yox. Given

its length, road modification, and long overland flow path to the north of the river, a local drainage network is proposed, separate to the infiltration basin catchment. As the northbound carriageway has a footpath and kerb, a series of gullies are proposed. The proposed gullies discharge across the road to a filter drain/carrier drain which in turn discharges north to proposed soakaways at the rear of the layby adjacent to the River Yox bridge. The southbound carriageway drains "over the edge" into the filter drain which also collects runoff from the adjacent cutting side. The arrangement is shown in **Plate 5** with the proposed soakaways shown by the three larger red circles.

Plate 5: A12/B1122 roundabout northern arm drainage



6.1.6 The HEWRAT assessment was completed following the design of northern arm with soakaway outfall. This indicated that due to assumed groundwater levels there would be a medium risk of pollution to groundwaters due to the short transit time for highway runoff to percolate through the strata. In the

case of the main infiltration basin this issue can be addressed by installing an impermeable base such that infiltration takes place through the sides of the basin, increasing transit time. An impermeable base soakaway option is not available for the northern arm soakaways.

6.1.7 The northern arm drainage strategy was discussed with SCC and draining the northern arm with discharge to the River Yox has been proposed as an alternative. The location of the required discharge point was inspected at the second site visit confirming the feasibility of an outfall route to the rear of the bridge parapet wall. SCC has confirmed that given the relative pollution risk to groundwater and the fact that existing highway runoff does discharge indirectly to the river, a discharge to the river from northern arm will be acceptable, subject to provision of effective treatment trains. However, since the River Yox is classified as main river the discharge and outfall headwall will require to be consented by the EA. Given that this section of A12 currently drains indirectly via a local ditch to the River Yox, with no provision of treatment, the proposed outfall will provide an improvement to the existing situation.

6.1.8 It is agreed that the design of the northern arm drainage outfall will be changed from soakaway to discharge to the River Yox at detailed design stage.

7 VALIDATION OF OUTLINE DRAINAGE STRATEGY

7.1.1 In accordance with the drainage hierarchy, the **Outline Drainage Strategy** [REP2-033] proposed the primary use of infiltration, with additional use of attenuation techniques (e.g. ponds and swales) to manage water quality and to further promote infiltration, and disposal to watercourse where necessary. The **Outline Drainage Strategy** is validated by the completed preliminary design.

7.1.2 The preliminary design documents will be made available for review and acceptance by SCC and the EA with respect to obtaining SCC consent to construct the road works and EA consent to discharge to main river.

8 SUMMARY AND CONCLUSION

8.1.1 The purpose of this technical note is to provide details of how the concept design has needed to evolve and develop as a result of provision of new information. The only significant change is that the A12 northern arm between Yoxford roundabout and the River Yox bridge will now discharge to the River Yox instead of to ground by infiltration.

8.1.2 The highway drainage has been designed in accordance with Design Manual for Roads and Bridges, the CIRIA SUDs Manual C753 (Ref. 3) and to comply with stated requirements of SCC contained in their SUDs Local Design Guide Appendix A (Ref. 4).

8.1.3 At this preliminary design stage, it is considered that the design provides for the effective removal, treatment and disposal of highway runoff. It reduces current level of flood risk within Yoxford and to the B1122 to the east providing a flood risk legacy benefit. The flood risk performance of the highway is as specified in DMRB and SCC guidance.

REFERENCES

1. Design Manual for Roads and Bridges and Manual of Contract Documents for Highway Works Series 500 Highways England 2000, http://www.standardsforhighways.co.uk/ha/standards/dmrb

2. The SUDs Manual (C753), CIRIA, 2015, ISBN 978-0-86017-760-9.

3. Sustainable Drainage Systems (SuDS) a Local Design Guide Appendix A to the Suffolk Flood Risk Management Strategy, Suffolk County Council, May 2018 https://www.greensuffolk.org/app/uploads/2021/05/2018-10-01-SFRMS-SuDS-Guidance-Appendix-A-.pdf

4. Highways Agency et al. (2009). Volume 11, Section 3, Part 10: Road Drainage and the Water Environment, LA 113 http://www.standardsforhighways.co.uk/ha/standards/dmrb/vol11/section3/LA 113.pdf

APPENDIX I

SIZEWELL C MAIN DEVELOPMENT SITE FLOOD RISK ASSESSMENT: ADDITIONAL HYDROLOGICAL REVIEW

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1 INTRODUCTION

1.1.1 As part of the Sizewell C Project Development Consent Order (DCO) application ('the Application') submitted in May 2020 a **Main Development Site (MDS) Flood Risk Assessment** (Doc Ref. 5.2) [APP-093] was prepared. The **MDS Flood Risk Assessment** describes flood risk from all sources of flooding, to the proposed main development site and the predicted impact of the development on flood risk elsewhere.

1.1.2 To inform the **MDS Flood Risk Assessment**, hydraulic modelling for fluvial, coastal inundation and tidal breach flooding was undertaken to assess flood risk for a range of return period events and climate change scenarios. Subsequently, further fluvial modelling and hydrology was undertaken to provide clarification to regulators and stakeholders and the results of the assessment were provided in **Appendix C** of the **Main Development Site (MDS) Flood Risk Assessment (FRA) Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161], hereafter referred to as the **MDS FRA Addendum**.

1.1.3 Following their review of the **MDS FRA Addendum** and the accompanying modelling data files, the Environment Agency provided clarification on their outstanding comments in relation to the hydraulic modelling, which included queries on the hydrological assessment. Responses to the comments collated in **Appendix B** of the **MDS FRA Addendum** (Doc. Ref. 5.2(A)Ad) [AS-161] were provided and considered alongside additional comments recorded in a meeting held on 22nd April 2021 with the Environment Agency. Following on from the meeting the proposed way forward was summarised and provided by the Environment Agency in a note 'Sizewell C MDS: Outstanding hydrology comments' dated 12th May 2021, provided in **APPENDIX A:** .

1.1.4 Further hydrological assessment and review has been carried out in response to the Environment Agency's comments based on the proposed way forward. The details and outcomes of this assessment are presented in this report.

2 BACKGROUND

2.1.1 The hydrological assessment for the Sizewell C project has been developed over a number of years, with the main analysis undertaken in 2015 prior to commencement of the hydraulic modelling. Since then, the Environment Agency has raised a series of comments and provided suggestions to undertake sensitivity testing. The majority of the comments were addressed or clarified within the Hydrology Report for the Application, as explained in **Appendix 3** of the **MDS Flood Risk Assessment** (Doc Ref. 5.2) [APP-

099] and **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161].

2.1.2 This report focuses on the additional assessment carried out to address the outstanding comments raised by the Environment Agency during the ongoing engagement, as collated in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] and the 'Sizewell C MDS: Outstanding hydrology comments' note provided by the Environment Agency on 12th May 2021.

2.1.3 The following sections discuss the specific comments and present the outcomes of any related checks or additional analysis, as required. Where there is overlap in the comments provided, then multiple comments have been addressed together for ease of review.

3 PERCENTAGE RUNOFF

3.1.1 In comment 2.1 in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] the Environment Agency raised concerns that less than the minimum number of events have been used to inform rainfall runoff parameters, i.e. only 3 events have been used in the study, when the FEH Volume 4 (Ref. 1) states that "At least five events should be analysed successfully for confidence in the results, the larger the number of events analysed, the greater the reliability of the derived unit hydrograph and losses model parameters (NERC, 1975, Mawdsley and Tagg, 1981)".

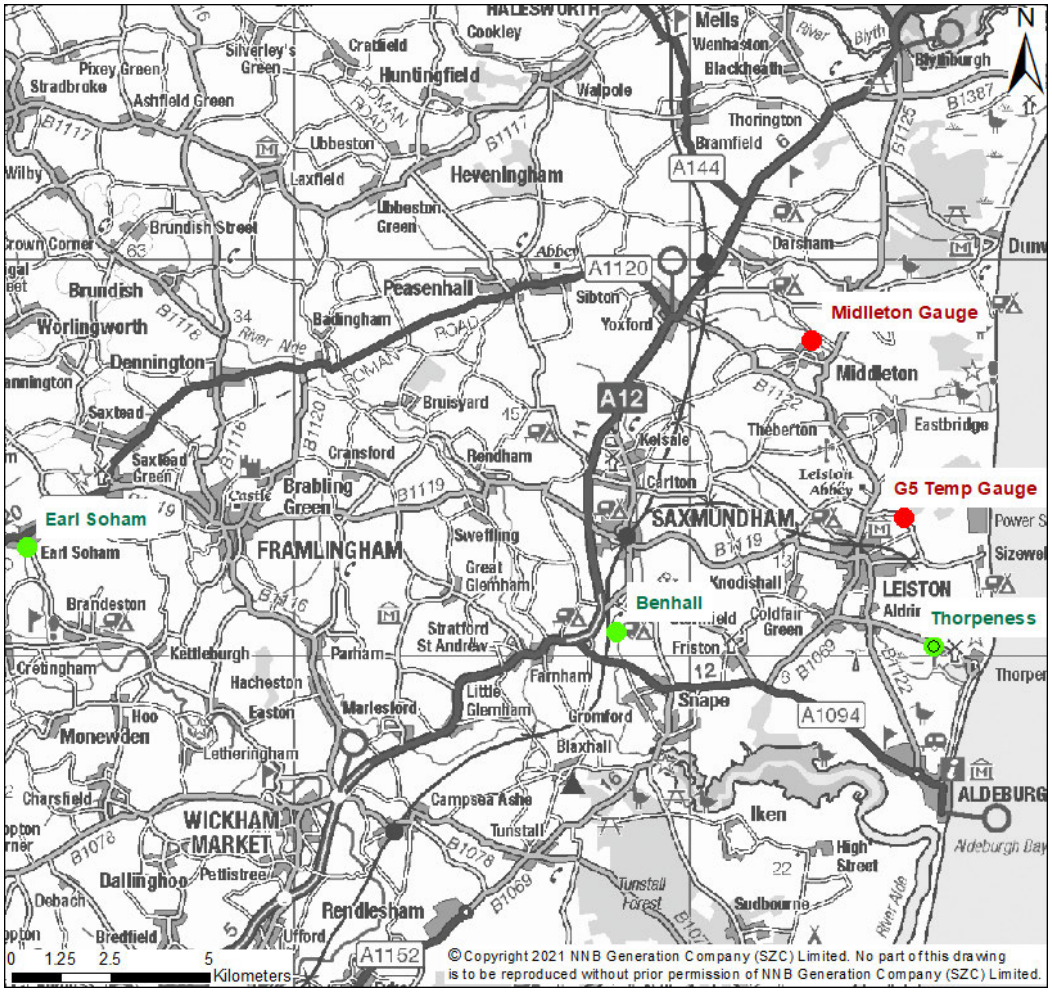
3.1.2 Section 3.1.3 of the Hydrology Report (**Appendix 3** of the **MDS Flood Risk Assessment** (Doc Ref. 5.2) [APP-099]) discusses the PR value adopted in the assessment and acknowledges that only 3 events were used to determine the PR values for the analysis. At the time of the report, this was due to the very limited availability of observable reliable data (especially for G5 temporary gauge where only 18 months of data was available at the time).

3.1.3 The Fluvial Modelling Report Addendum (**Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161]) does include a qualitative assessment of 3 additional events identified post January 2016 (i.e. the last event used in the original assessment). However, no additional calculations were undertaken at the time, although a qualitative comparison showed that the hydrograph shape and peak for these additional events were similar to the other events used in the analysis of percentage runoff. In their latest comments, the Environment Agency requested that a minimum of 5 events should be used in the assessment, as this would add confidence to the estimates.

3.1.4 To address these comments, percentage runoff calculations were carried out based on the recorded water level / flow at the Middleton gauging station for the main Minsmere catchment, where in absence of flow records the rating curve was used to calculate the flow based on recorded water levels. In addition, the G5 temporary gauging station was used for the Leiston catchment and as a donor for all other sub-catchments. This is the same approach as adopted for the original hydrological assessment.

3.1.5 The percentage runoff (PR) calculations were performed based on a simple formula, where the 'PR = cumulative flow / cumulative rainfall'. Similarly, to the original hydrological assessment for these calculations, recorded rainfall events at Benhall and Thorpeness rainfall gauges were reviewed and used for the Middleton and G5 gauge calculations respectively. Where not available, records from the Earl Soham rainfall gauge were used. The location of the flow and rainfall gauges is presented in **Plate 3.1**.

Plate 3.1: Location of the flow and rainfall gauging stations

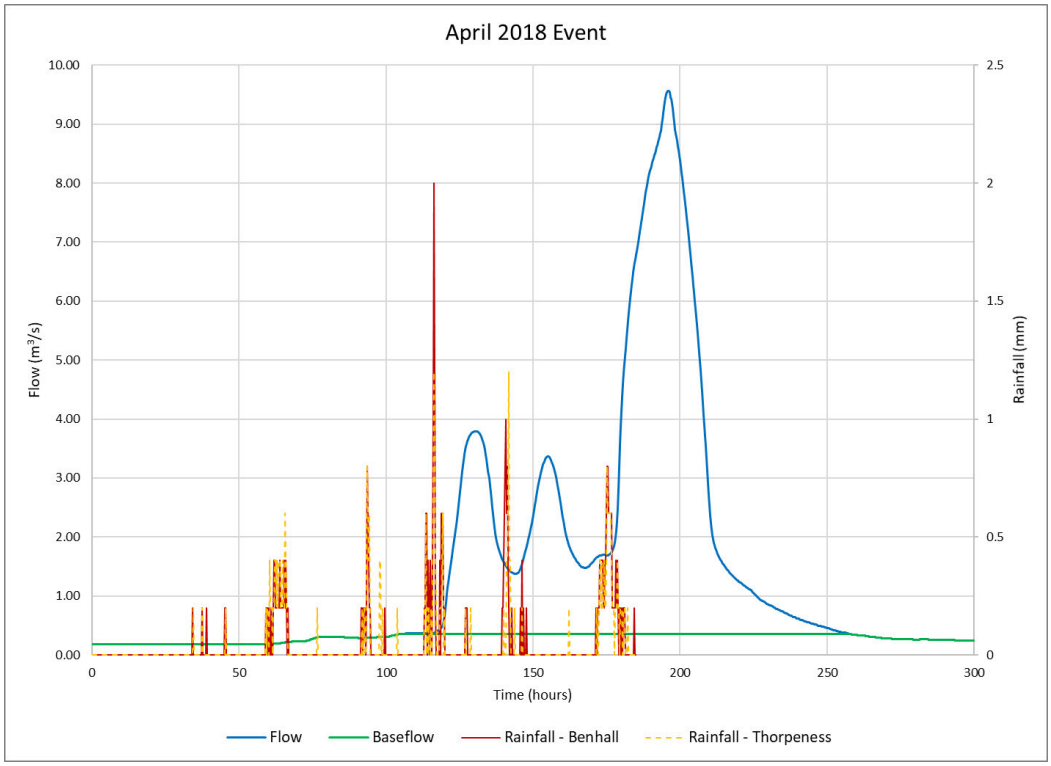


3.1 Middleton gauge

3.1.1 Section 3.3 of the Fluvial Modelling Report Addendum (**Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161]) discusses the qualitative analysis of the extended stage / flow dataset. Three high flow events have been identified, these being April 2018, November 2019 and December 2019, in addition to the three high flow events considered in the original hydrological assessment, namely January 2003, March 2010 and January 2016.

3.1.2 The percentage runoff calculations were carried out for all six events to derive an average PR value and to enable comparison of these with the values adopted in the estimation of design events. **Plate 3.2** presents the flow hydrograph and recorded rainfall for the April 2018 event and additional plots of all considered events are provided in **Figure 1** – **Figure 6** attached to this report.

Plate 3.2: April 2018 high flow (Middleton) and rainfall event



3.1.3 For the purpose of the percentage runoff calculations, only the antecedent rainfall conditions were considered, as shown in **Plate 3.2**. For events where multiple peaks were identified, the PR values were calculated for each peak flow separately by applying the cumulative rainfall only to that particular peak event. For example, the January 2003 event has four peak flow events (**Figure 1**), however between each of the peaks the flow returns

to baseflow. As such for each of the four peaks an individual PR value was derived, and then the average value determined for the entire event.

3.1.4 A catchment area of 50.16 km^2 was used in the calculations, in line with the adjusted area presented in Table 3.1 of the Hydrology Report (**Appendix 3** of the **MDS Flood Risk Assessment** (Doc Ref. 5.2) [APP-099]).

3.1.5 The time interval for both the flow and rainfall records was 15min. Rainfall was recorded in mm, whereas flow in m^3/s. As such, an appropriate unit conversion has been applied in the calculations.

3.1.6 **Table 3.1** provides a summary of the time period for the flow and rainfall records used for each of the events to derive the respective PR values. Where data was available, the PR values were calculated based on the data from two rainfall gauges for comparison.

3.1.7 The overall average PR value derived from the results presented in **Table 3.1** is 67%, taking an average event value for each of the high flow events. This is higher than the 50% PR value used in the original hydrological assessment, however it is noted that a sensitivity test has also previously been undertaken with a conservative PR value of 75%, as presented in section 3.6 of the Fluvial Modelling Report Addendum (**Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161]). Results from this sensitivity test showed that, for an extreme 1 in 100-year return period event at 2190 epoch (80% allowance for climate change), the 25% increase in PR values results only in a 5%-9% increase in peak flood depth across the catchment.

3.1.8 It is noted that this sensitivity test assumed a 75% PR value for all inflow boundaries (subcatchments) not only the main Minsmere River upstream, where the Middleton gauge is used, and therefore the results are likely to be conservative.

3.1.9 Furthermore, were the revised inflows to apply the 67% PR value in both the baseline and with scheme model simulations, it is anticipated that the difference in peak flood levels due to the increased PR values would be similar to that presented in the Application and is likely to be less influential for the more extreme events and those with the climate change scenarios.

3.1.10 The closest rainfall gauges have been used in the assessment. However, the available Benhall and Thorpeness rainfall gauges are located approximately 9 km and 8.5 km away (in a straight line) from the Middleton gauge. It is therefore possible that the amount of rainfall captured at those gauges does not accurately represent the amount of rainfall over the upper Minsmere catchment, upstream of the Middleton gauge.

Table 3.1: Summary of adopted flow and rainfall data timeframes and derived PR values for Middleton

High flow event		Flow records		Rainfall records		Baseflow (m^3/s)	PR value	
		From	To	From	To		Benhall	Thorpeness
January 2003	Peak 1	21/12/2002 19:15	25/12/2002 10:15	21/12/2002 21:15	22/12/2002 14:15	=<0.89	*89%	N/A
	Peak 2	25/12/2002 10:30	29/12/2002 10:15	25/12/2002 05:45	27/12/2002 04:30		*69%	N/A
	Peak 3	29/12/2002 10:30	01/01/2003 07:00	29/12/2002 08:00	29/12/2002 20:30		*70%	N/A
	Peak 4	01/01/2003 07:15	05/01/2003 11:15	01/01/2003 05:15	03/01/2003 16:30		*102%	N/A
March 2010		21/02/2010 00:00	03/03/2010 23:45	21/02/2010 09:45	28/02/2010 22:45	=<0.69	58%	N/A
January 2016	Peak 1	01/01/2016 02:00	07/01/2016 06:30	01/01/2016 09:45	05/01/2016 11:30	=<0.74	55%	N/A
	Peak 2	07/01/2016 06:45	09/01/2016 23:00	07/01/2016 02:30	09/01/2016 23:00		73%	N/A
April 2018		25/03/2018 21:00	07/04/2018 08:45	25/03/2018 21:15	25/03/2018 13:30	=<0.35	61%	70%
November 2019		10/11/2019 11:30	24/11/2019 10:00	11/11/2019 04:30	15/11/2019 05:00	=<0.22	65%	71%
December 2019		06/12/2019 06:00	02/01/2020 00:45	06/12/2019 07:15	26/12/2019 22:45	=<0.22	66%	49%

*Note: Benhall rain gauge data was not available for this event, therefore data from Earl Soham gauge was used as the closest available.

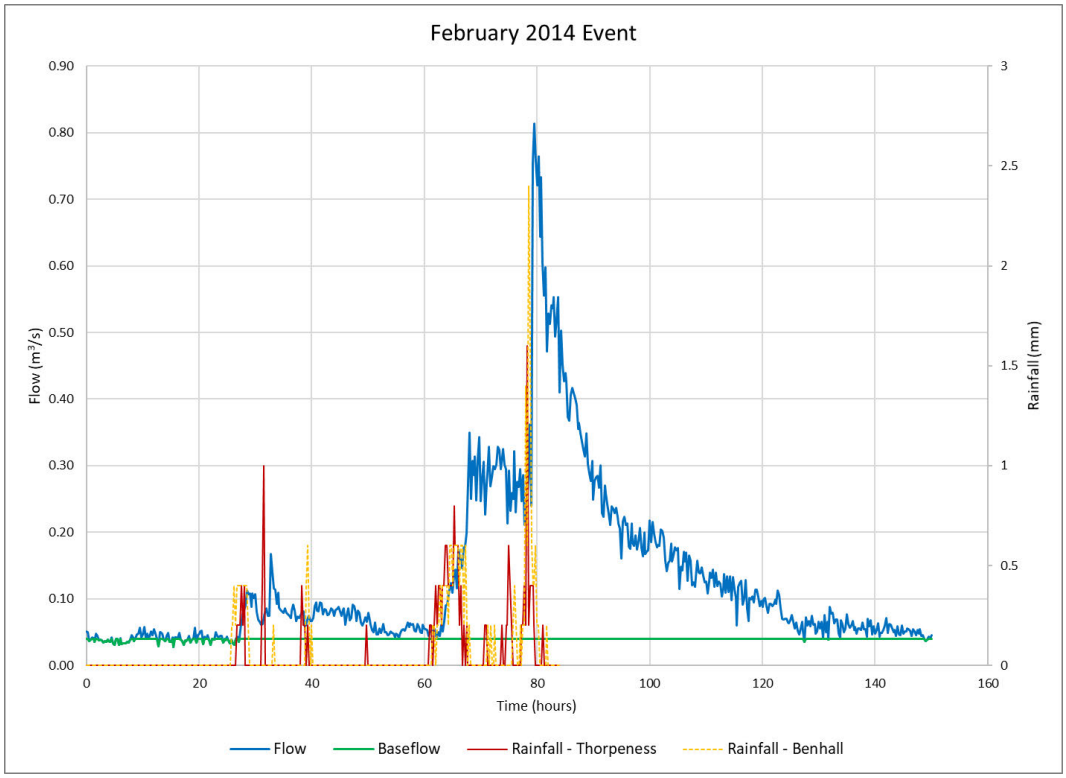
3.2 G5 temporary gauge

3.2.1 Percentage runoff calculation for the G5 temporary gauging station were also carried out for 6 identified high flow events, however the events used are different to those used in the Middleton gauge calculations. This variation in the events is based on there being no data from the G5 gauge available for those events (e.g. November and December 2019) as the dataset does not extend this far, or the recorded flow at the G5 gauge did not indicate a significant event suitable for the PR calculations. The review of events at the Middleton gauge and the G5 gauge has confirmed that where flow events are recorded at one site these are not necessarily reflected in significant events at the other location.

3.2.2 Furthermore, the time-series plot of the recorded flow at the G5 gauge presented in **Figure 7**, shows there are significant gaps in the recorded data from 2016 onwards and that where records are available there are no events with sufficient peak flow within that period. There are two moderately high peak flow events, one in June and the second in August 2016, however the rainfall record from the Thorpeness rainfall gauging station (closest to the G5 gauge as shown in **Plate 3.1**) does not have records of an antecedent rainfall event and therefore, percentage runoff values derived using this event data would not be representative.

3.2.3 On that basis, five events identified in 2014 and one in 2015 were used in the PR calculations for the G5 gauge. **Plate 3.3** presents the flow hydrograph (G5 gauge) and recorded rainfall (Benhall and Thorpeness) for the February 2014 event. Plots of all considered events are provided in **Figure 8** – **Figure 13**.

Plate 3.3: February 2014 high flow (G5) and rainfall event



3.2.4 For the purposes of the percentage runoff calculations, only the antecedent rainfall was applied from both, Thorpeness and Benhall rain gauges. A catchment area of 5.04 km^2 was taken based on a combined area of the LEIS_ABBEY and LEIS_LEISTON subcatchments (Table 3.1 of **Appendix 3** of the **MDS Flood Risk Assessment** (Doc Ref. 5.2) [APP-099]).

3.2.5 As with the Middleton gauge PR calculations, appropriate unit conversion was applied in the G5 PR calculations considering rainfall was provided in mm and flow in m^3/s with time interval of 15min.

3.2.6 **Table 3.2** provides a summary of the time period for the flow and rainfall records used for each of the events to derive the respective PR values for G5 based on the data from the two rainfall gauges at Thorpeness and Benhall for comparison.

3.2.7 The overall average PR value for the G5 gauge derived from the results presented in **Table 3.2** is 33%, taking into account data from both of the rainfall gauges. This is much lower than the average value of 50% used in the estimation of design flow events for all the sub-catchments. Therefore, the PR value applied in the hydraulic modelling for the Application is considered to be conservative.

Table 3.2: Summary of adopted flow and rainfall data timeframes and derived PR values for G5

High flow event	Flow records		Rainfall records		Baseflow (m^3/s)	PR value	
	From	To	From	To		Thorpeness	Benhall
February 2014	04/02/2014 00:00	10/02/2014 06:00	05/02/2014 01:45	07/02/2014 09:45	=<0.04	48%	36%
July 2014	07/07/2014 08:45	16/07/2014 05:00	08/07/2014 13:30	13/07/2014 20:00	=<0.03	13%	19%
October 2014	02/10/2014 05:30	11/10/2014 08:45	03/10/2014 07:15	08/10/2014 12:30	=<0.02	20%	17%
November 2014 – Event 1	30/10/2014 08:45	11/11/2014 08:00	30/10/2014 14:15	09/11/2014 10:15	=<0.02	40%	40%
November 2014 – Event 2	15/11/2014 09:00	26/11/2014 01:30	15/11/2014 16:45	23/11/2014 20:45	=<0.02	43%	37%
July 2015	23/07/2015 13:00	29/07/2015 08:30	24/07/2015 00:00	25/07/2015 08:15	=<0.02	24%	57%

3.3 Conclusions

3.3.1 Percentage runoff values for the Middleton gauge and the G5 temporary gauge were calculated based on six identified high flow events to derive an average PR value for each location and compare with those used in the hydraulic modelling carried out for the Application.

3.3.2 The derived average PR value for Middleton is 67%, which is higher than the 50% adopted in the modelling, although this would only apply to the upper Minsmere subcatchment as G5 gauge was used as donor site for all other sub-catchments, not Middleton.

3.3.3 In addition, sensitivity testing was carried out with a 75% PR value adopted for all subcatchments (not only upper Minsmere) with results showing relatively limited difference in peak flood levels. Also, the revised inflow would be applied to both the baseline and with scheme model schematisations and therefore it is anticipated that the relative difference in flood levels as a result of the proposed development would be similar to that reported in the Application.

3.3.4 For the G5 temporary gauge, the derived average PR value is 33%, which is significantly less than the 50% used in modelling. As such, the value applied in the modelling is considered conservative.

3.3.5 Overall, noting that the impact on flood risk to off-site receptors presented in the **Main Development Site (MDS) Flood Risk Assessment** (Doc Ref. 5.2) [APP-093] and subsequently in the **MDS FRA Addendum** (Doc. Ref. 5.2(A)Ad) [AS-157] was considered not significant, conclusions of the FRA in the Application would not be affected by the revised PR values.

3.3.6 The spreadsheets setting out the derivation of the PR calculations for the Middleton gauge and G5 gauge are provided as **APPENDIX A:** .

4 STANDARD PERCENTAGE RUNOFF

4.1.1 In comment 2.0 provided in **Appendix B** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161], the Environment Agency raised a concern that the best practice approach of deriving Standard Percentage Runoff (SPR) values based on soil properties and geology specific to each sub-catchment was not applied in the hydrological assessment for use in hydraulic modelling for the Application.

4.1.2 Section 3.1.2 of the Hydrology Report (**Appendix 3** of the **MDS Flood Risk Assessment** (Doc Ref. 5.2) [APP-099]) discusses the FEH catchment descriptors adopted in the assessment and acknowledges BFIHOST and SPRHOST should be checked taking into consideration the potential

variation in soil characteristics between the different sub-catchments. Although soil type and geology were considered at the time, detailed checks were not carried out at that stage of the study and as summarised in the preceding section a 50% PR value was adopted for the design flow estimates in the hydraulic modelling for all of the sub-catchments.

4.1.3 To address comments raised by the Environment Agency, additional calculations have been undertaken to derive SPR values for each of the sub-catchments based on the methodology set out in the FEH Volume 4 (Ref. 1). For this assessment, the approach proposed by the Environment Agency was used as outlined in the note 'Sizewell C MDS: Outstanding hydrology comments' dated 12th May 2021, which was provided following the discussions with the Environment Agency on 22nd April 2021.

4.1.4 A summary of the adopted approach is provided in **section 4.2**, details on the calculations of the SPR for the identified events for the Middleton gauge and the G5 temporary gauge are presented in **section 4.2** and **section 4.4** respectively. The SPR values for all other inflow sub-catchments were derived using a donor transfer approach in conjunction with SPRHOST based on the G5 temporary gauge with the results presented in **section 4.5** and conclusions are summarised in **section 4.6**.

4.2 Summary of Approach

4.2.1 In accordance with the approach recommended by the Environment Agency in the note 'Sizewell C MDS: Outstanding hydrology comments' dated 12th May 2021 appropriate Standard Percentage Runoff (SPR) values have been calculated in accordance with FEH Volume 4 (Ref. 1).

4.2.2 In addition to the observed flow / level data available from the Middleton gauge and G5 gauge, as is the case for this study where local observed SMD data is not available the Met Office Rainfall and Evaporation Calculation System (MORECS) records can be used.

4.2.3 MORECS data was obtained from the Met. Office for a number of data periods to match the events identified at the Middleton gauge and the G5 gauge to understand the catchment conditions leading up to each event.

4.2.4 The data was obtained for Grid Number 142, comprising a 40km by 40km square grid, at a weekly resolution for the week preceding the event. This supplies the user with weekly averages calculated at the end of the monitoring week and extends over the dates of the storm events identified. MORECS data runs from Wednesday to Tuesday, therefore where there was not a full 7 day period in a single week prior to the event, the MORECS data for the two weeks preceding the event was obtained.

4.2.5 As noted above, based on the Flood Studies Report (FSSR16) it is advisable to calculate the SPR for a subject catchment based on observed flow data.

4.2.6 The initial step in the procedure is to calculate the Percentage Runoff (PR) from the volume of rainfall and volume of runoff generated by an observed storm event. The PR values presented in this section may differ slightly from those presented in **section 2.1.3** due to the approach required in the assessment of SPR.

4.2.7 Prior to the calculation of SPR the hydrological conditions at the onset of a storm event must be determined. This involves calculation of the 5-day antecedent rainfall (API5) and catchment wetness index (CWI) parameters, both are measured in units of millimetres.

4.2.8 API5 was calculated using 15-minute time series rainfall data retrieved from the Benhall and Thorpeness Tipping Bucket Raingauges (TBR).

4.2.9 CWI is calculated using the five-day antecedent rainfall (API5) values and Soil Moisture Deficit (SMD) values prior to the onset of a storm event.

4.2.10 SPR is then calculated using the following equation:

$$SPR = PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}$$

where: SPR = Standard Percentage Runoff;

PRRURAL = Percentage Rural Runoff;

DPRCWI = Dynamic Percentage Runoff attributable to Catchment Wetness Index (CWI); and

DPRRAIN = Dynamic Percentage Runoff attributable to catchment rainfall.

4.2.11 This equation has been adopted for both the Middleton gauge and the G5 gauge as set out in the following sections.

4.3 Middleton gauge

4.3.1 The Middleton gauge represents the upper Minsmere catchment. Standard percentage runoff calculations were carried out for five high-flow events which were identified from a review of the Middleton gauge flow record. This was to ensure that the review was carried out in accordance with the best practice guidance set out in the FEH Volume 4 (Ref. 1) as requested by the Environment Agency.

4.3.2 These include the three events from January 2003, March 2010 and January 2016 which were considered in the original hydrological assessment as well as two additional, more recent, events identified from April 2018 and November 2019. The calculations for the SPR are provided in a spreadsheet accompanying this report as **APPENDIX C:** .

4.3.3 A summary of the main values identified within this calculation are summarised in **Table 4.1**.

Table 4.1: Parameters within the calculation of SPR for each of the high flow events at the Middleton gauge

Event Date	API5 (mm)	SMD (mm)	CWI (mm)	PR_{RURAL}	DPR_{RAIN}	SPR
01/01/2003	6.1	0.0	131.1	70.0	0.0	68.5
01/03/2010	6.1	1.3	129.8	58.0	0.0	56.8
08/01/2016	5.0	0.0	130.0	73.0	0.0	71.8
03/04/2018	5.2	1.4	128.8	55.0	0.0	54.0
28/11/2019	0.7	0.0	125.7	96.1	0.0	95.9

4.3.4 The SPR calculations from the five high-flow events summarised in **Table 4.1** were used to derive a mean SPR value for comparison with the SPRHOST value from the FEH catchment descriptors for the catchment.

4.3.5 The SPR calculations for each of the high flow events results in a mean SPR value of 69.4% for the Middleton gauge, as summarised in **Table 4.2**.

Table 4.2: SPR and PR comparison for each of the high flow events

Event Date	Peak Flow (m^3/s)	PR	SPR
01/01/2003	14.3	70.0	68.5
01/03/2010	9.0	58.0	56.8
08/01/2016	11.4	73.0	71.8
03/04/2018	9.6	59.0	54.0
28/11/2019	10.5	96.0	95.9
Mean		**71.2**	**69.4**

4.3.6 The detailed calculations and equations used in the derivation of SPR for the Middleton gauge are provided in **APPENDIX C:** .

4.4 G5 temporary gauge

4.4.1 The G5 temporary gauge represents the Leiston catchment that drains the area to the west of Sizewell. As noted in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] the G5 temporary gauge has been identified as the most appropriate in terms of hydrological similarity and also availability of the most comprehensive dataset, compared with the other temporary gauges.

4.4.2 Standard percentage runoff calculations have also been undertaken for the G5 gauge. However, similarly to the differences between the events identified in **section 3.2** the events used for the G5 gauge are different to those identified for the Middleton gauge.

4.4.3 Following a review of the data record collected from the G5 gauge between 2013 to 2019, a total of six high-flow events were identified for use in the SPR analysis, of which five were recorded within the 2014 calendar year.

Table 4.3: Parameters within the calculation of SPR for each of the high flow events at the G5 gauge

Event Date	API5 (mm)	SMD (mm)	CWI (mm)	PR_{RURAL}	DPR_{RAIN}	SPR
07/02/2014	2.7	0	127.7	35.9	0.00	35.2
12/07/2014	7.2	112.6	19.6	12.9	0.00	39.2
08/10/2014	4.4	103	26.4	19.9	0.00	44.5
05/11/2014	7.5	56.2	76.3	39.9	0.00	52.1
23/11/2014	1.3	24.8	101.5	39.9	0.00	45.8
25/07/2015	0.1	116.4	8.7	23.9	0.88	52.1

4.4.4 The SPR calculations from the six high-flow events summarised in **Table 4.3** were used to derive a mean SPR value for comparison with the SPRHOST value from the FEH catchment descriptors for the catchment.

4.4.5 The SPR calculations for each of the high flow events results in a mean SPR value of 44.8% for the G5 gauge, as summarised in **Table 4.4**. This is greater than the SPRHOST value derived from catchment descriptors.

Table 4.4: SPR and PR comparison for each of the high flow events

Event Date	Peak Flow (m^3/s)	PR	SPR
07/02/2014	0.8	36.0	35.2
12/07/2014	1.0	13.0	39.2
08/10/2014	1.1	20.0	44.5

05/11/2014	1.6	40.0	52.1
23/11/2014	1.1	40.0	45.8
25/07/2015	1.4	24.0	52.1
Mean		**28.8**	**44.8**

4.4.6 The detailed calculations and equations used in the derivation of SPR for the G5 gauge are provided in **APPENDIX C:** .

4.5 Sub-catchments

4.5.1 The catchment descriptors for the G5 gauge were found to have similar hydrological characteristics to the other upland sub-catchments. As such it was considered appropriate to use the G5 gauge as a donor catchment for the donor data transfer procedure.

4.5.2 The SPRHOST value assigned to the G5 gauge catchment is the average of the SPRHOST values for the Leiston and Leiston Abbey sub-catchments.

4.5.3 The SPR for the other upland sub-catchments using the G5 gauge as a donor catchment were subsequently calculated using a donor adjustment factor. In line with the guidance set out in the FEH Volume 4 (Ref. 1) this is calculated by dividing the observed SPR from the G5 gauged catchment by the SPR obtained from catchment descriptors at the G5 catchment.

4.5.4 This adjustment factor is then multiplied by the SPR from catchment descriptors for each of the sub-catchments that use the G5 catchment as a donor. The equation has been reproduced below for reference:

$$SPR_{s,adj} = SPR_{s,cds} (SPR_{g,obs}/SPR_{g,cds})$$

Where:

$SPR_{s,cds}$ = subject site catchment descriptors value;

$SPR_{g,obs}$ = gauged site observed value;

$SPR_{g,cds}$ = gauged site catchment descriptors value

4.5.5 Adopting the G5 as a donor catchment and using the SPR transfer method and SPR donor adjustment results in higher SPR values for all upland sub-catchments, summarised in **Table 4.5** below.

Table 4.5: Summary of the SPR values from the SPR transfer method for each of the sub-catchments

Upland Inflow Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	24.3	44.8	27.8	51.4
Leiston	24.3	44.8	20.7	38.2
Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	24.3	44.8	25.3	46.8

4.5.6 The detailed calculations and equations used in the derivation of the SPR for each of the sub-catchments using the SPR transfer method from the G5 gauge are provided in **APPENDIX C:** .

4.6 Comparison of flow hydrographs

4.6.1 The calculated SPR values for each of the sub-catchment inflows along with the average CWI value of 60.0 (based on the events at G5) were input to the inflow boundary units in the Flood Modeller software to understand the potential impact on the 1 in 100-year hydrographs.

4.6.2 In section 3.2.4 of the FEH Volume 4 (Ref. 1) there is guidance on the likely range of CWI that may be experienced in a catchment. This indicates that CWI typically varies between 120mm and 130mm, except on low SAAR catchments where it may fall to around 60mm. On this basis, a sensitivity test comparing the flow hydrographs was undertaken, assuming that the catchment may have been subject to wetter antecedent conditions. In this sensitivity testing the highest CWI value of 127.7, based on the February 2014 event at the G5 gauge, was also considered to understand the implication this may have on the 1 in 100-year flow hydrograph.

4.6.3 These flow hydrographs were compared with the peak flow hydrographs which were previously derived for both the 50% PR and 75% PR model

runs for the LEIS_LEISTON (G5 gauge), Middleton gauge and each of the sub-catchments.

4.6.4 The full suite of comparison graphs are provided in **APPENDIX D:** ; however, the hydrographs for the LEIS_LEISTON (G5 gauge) and key sub-catchments have been provided in **Plates 4.1** to **4.3**.

Plate 4.1: Comparison of flow hydrographs for LEIS_LEISTON (G5 gauge) inflow

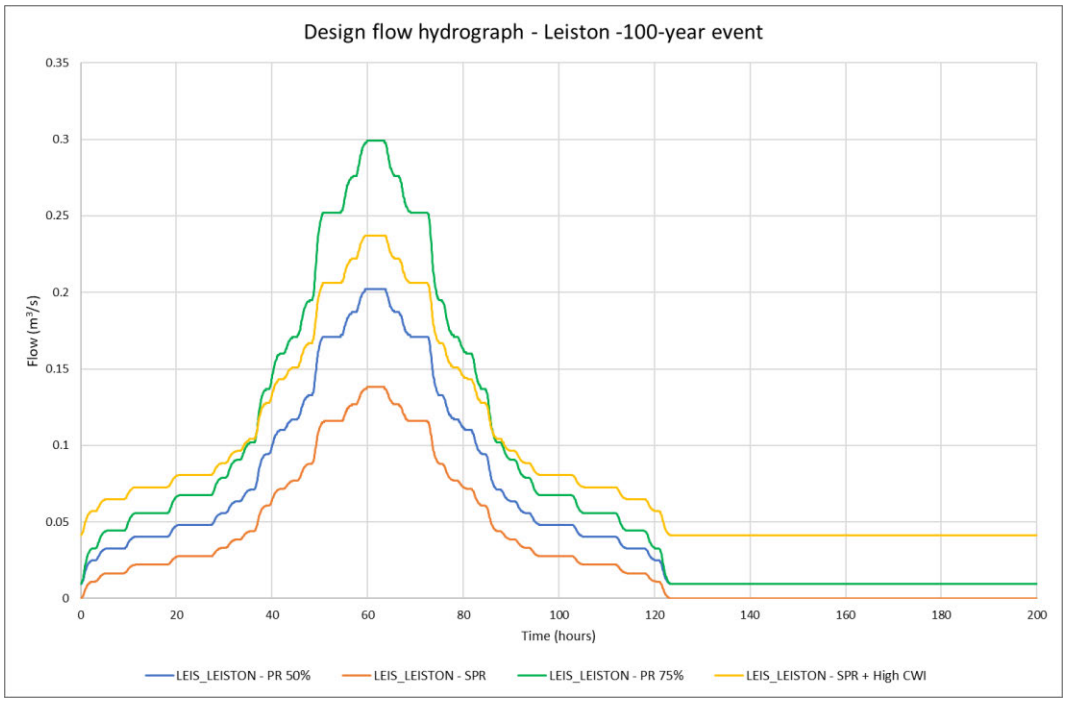


Plate 4.2: Comparison of flow hydrographs for LEIS_SIZEW inflow

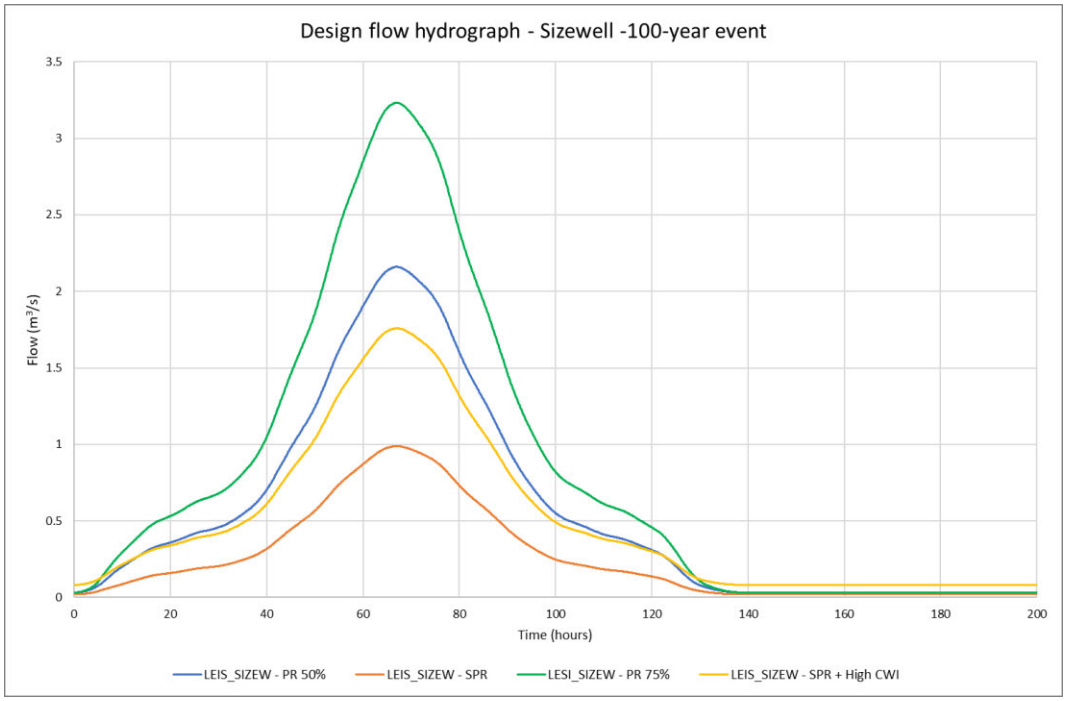
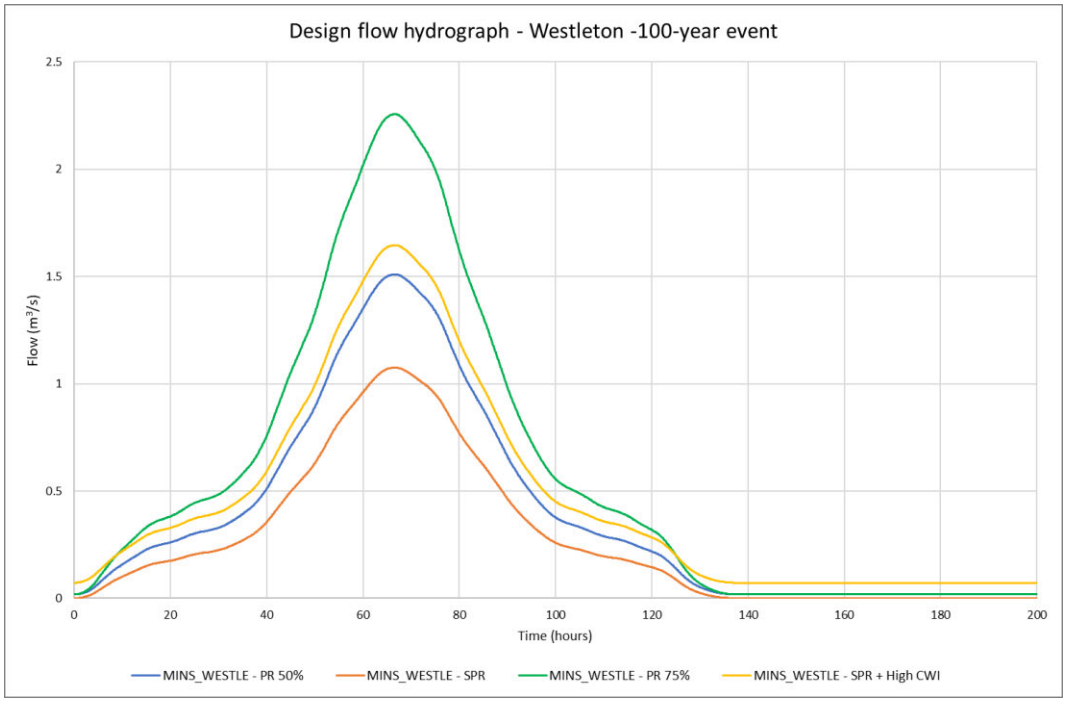


Plate 4.3: Comparison of flow hydrographs for MINS_WESTLE inflow



4.6.5 This comparison found that in the majority of the inflow locations i.e. for the LEIS_LEISTON (G5 gauge) and all the sub-catchments, for which G5 is the donor, the peak flow hydrograph for the SPR, based on the donor transfer approach, is close to or below the peak flow hydrograph for the 50% SPR scenario. In all of these inflow locations the peak flow hydrograph based on the calculated SPR is below the peak flow hydrograph for the 75% SPR scenario and in many of the sub-catchments it is significantly lower. Only, in the MINS_US is the SPR peak flow hydrograph greater than both the 50% PR and 75% PR peak flow hydrographs.

4.7 Sensitivity test

4.7.1 To assess the potential impact of the derived SPR and CWI values on the overall conclusions of the FRA, the sensitivity testing was also undertaken within the hydraulic model to confirm the relative increase in peak flood depth. For this sensitivity testing, the hydraulic model developed for the Project was simulated for both, the baseline and with scheme model schematisations.

4.7.2 Details of the hydraulic model development and boundary conditions are provided in **Appendix 2** of the **MDS Flood Risk Assessment** (Doc Ref. 5.2) [APP-094] and **Appendix C** of the **MDS FRA Addendum** (Doc. Ref. 5.2(A)Ad) [AS-161].

4.7.3 Both the baseline and with scheme models were run for the 1 in 100-year return period event present day scenario and for the future scenario i.e. including the allowance for climate change (65%) comprising a total of four model runs. For each of the model inflow boundaries, the respective FEH node was adjusted with the appropriate SPR and CWI values, as illustrated (inflow boundary MINS_EASTBR as an example) in **Plate 4.4**.

4.7.4 For the upstream Minsmere inflow, the average SPR and CWI was used based on the values derived for the Middleton gauge (adopted from **Table 4.1**). For the other sub-catchments, the derived donor SPR values were used (adopted from **Table 4.5**) with the highest (conservative approach) derived CWI value for the G5 temporary gauge (adopted from **Table 4.3**). For ease of reference the adopted SPR and CWI values for each sub-catchment are presented in **Table 4.6**.

Plate 4.4: Example of adjusted FEH inflow boundary

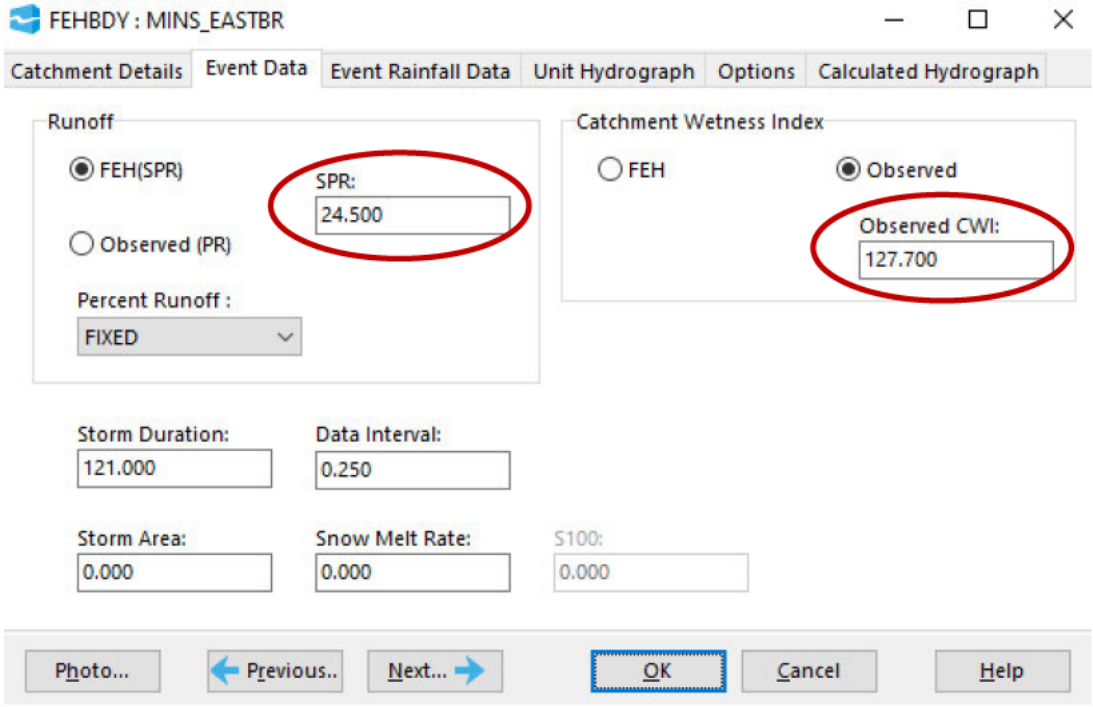
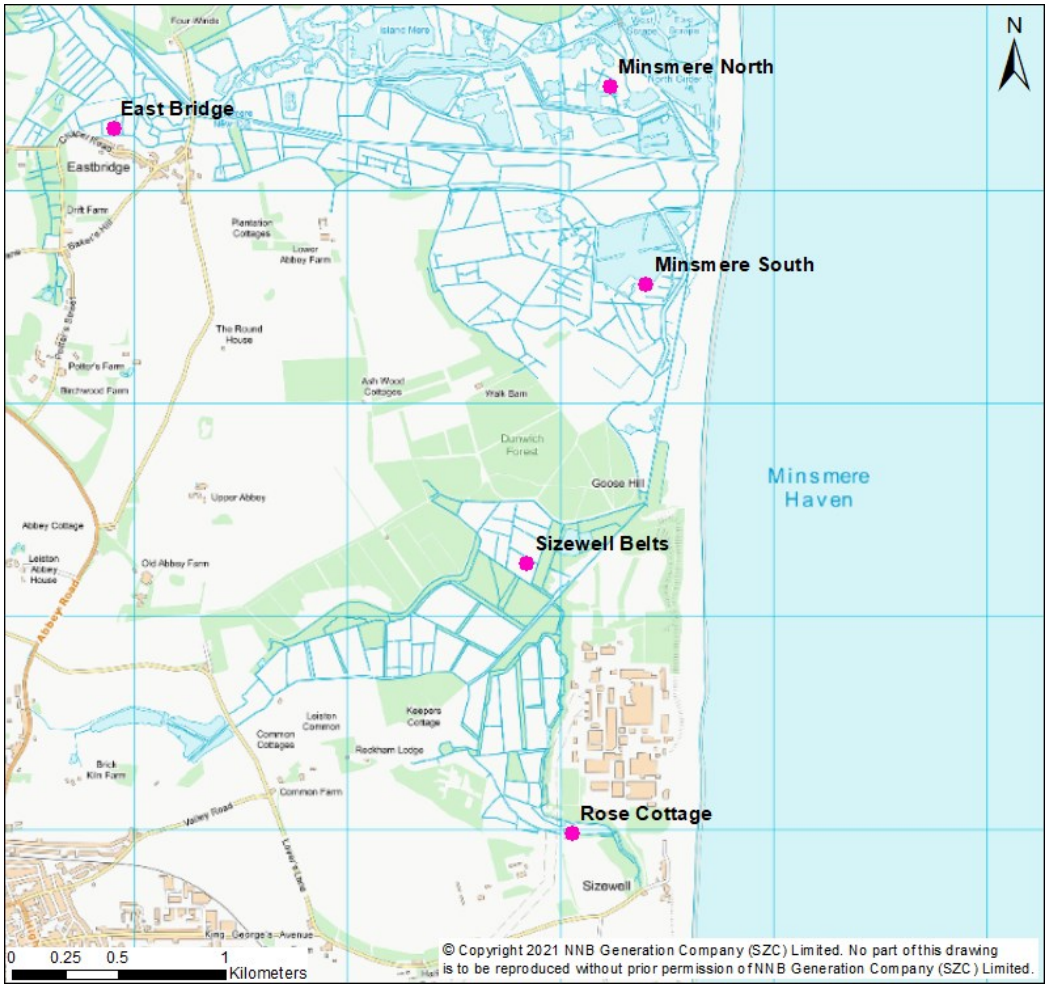


Table 4.6: Summary of the adopted SPR and CWI for each of the sub-catchments

Upland Inflow Sub-catchment	SPR	CWI
MINS_US	69.4	129.1
MINS_WESTLE	40.5	127.7
MINS_WARKBAR	25.9	127.7
MINS_WASH	59.9	127.7
MINS_THEBERT	54.5	127.7
MINS_POTTERS	46.8	127.7
MINS_SCOTT	25.0	127.7
MINS_DOCWRA	26.6	127.7
MINS_EASTBR	24.5	127.7
LEIS_UPPER	31.5	127.7
LEIS_LOVERS	33.6	127.7
LEIS_ABBEY	51.4	127.7
LEIS_LEISTON	38.2	127.7
SEIZEWELL	26.8	127.7

4.7.5 Results of the sensitivity tests were compared to determine the relative difference between the baseline and with scheme scenarios. The maximum flood depth was compared at five locations within the catchment, the locations of which are shown in **Plate 4.5**.

Plate 4.5: Selected model node points for results comparison



4.7.6 **Table 4.7** presents a comparison of the peak flood depths at the selected points between the baseline and with scheme scenarios, based on the adjusted SPR and CWI values. **Table 4.8** shows a comparison of the peak flood depth for the 1 in 100-year event at present day and future (with climate change allowance) for the two baseline scenarios, i.e. with PR (as presented in the Application) and SPR (as derived in this assessment) applied in the FEH inflow boundary.

Table 4.7: Peak fluvial flood depth comparison for the 1 in 100-year return period event with 65% climate change allowance

Comparison Point	Peak flood depth (m)		
Point Location	**Baseline**	**With Scheme**	**Difference**
East Bridge	1.48	1.49	0.01
Minsmere North	1.85	1.86	0.01
Minsmere South	2.28	2.29	0.01
Sizewell Belts	1.61	1.60	-0.01
Rose Cottage	1.31	1.30	-0.01

4.7.7 Results in **Table 4.7** show that the relative difference in flood depth between the baseline and with scheme scenarios with the adjusted SPR and CWI values is up to 0.01m for the 1 in 100-year event with 65% climate change allowance, which is in line with the relative impact of the Project reported in the **MDS FRA Addendum** (Doc. Ref. 5.2(A)Ad) [AS-157] submitted as part of the Application.

4.7.8 The **MDS FRA Addendum** (Doc. Ref. 5.2(A)Ad) [AS-157] shows that there is risk of flooding to a maximum of 6 residential and 6 non-residential properties and that the maximum increase in flood depth is up to 0.01m across all scenarios. The results from this SPR sensitivity test show that there are no additional residential or commercial properties affected to those already identified in the Application, and that the relative increase in flood depth to those properties remains no greater than 0.01m.

Table 4.8: Peak fluvial flood depth comparison for the baseline 1 in 100-year return period event present day and with 65% climate change allowance

Comparison Point	Baseline Peak flood depth (m)			
Point Location	**Present Day (PR)**	**Present Day (SPR)**	**65%CC (PR)**	**65%CC (SPR)**
East Bridge	0.79	1.17	1.31	1.48
Minsmere North	1.18	1.56	1.70	1.85
Minsmere South	1.61	1.99	2.13	2.28
Sizewell Belts	0.97	1.35	1.49	1.61
Rose Cottage	0.66	1.04	1.18	1.31

4.7.9 **Table 4.8** shows that for the 1 in 100-year baseline scenario, the adjusted SPR and CWI values result in an increase in peak flood depth by approximately 0.38m for the present day scenario and 0.17m for the future

scenario (with 65% climate change allowance). When compared with the post development scenario for the same event, the relative difference in flood depth as a result of the Project is up to 0.01m within the Minsmere area with a slight reduction in flood depth for the properties within the Sizewell Belts and Sizewell Gap area. This difference can be attributed to the adjusted SPR value which for most of the inflow boundaries within the Leiston catchment is less than the 50% adopted in the Application.

4.8 Conclusions

4.8.1 To address the comments raised by the Environment Agency in their note 'Sizewell C MDS: Outstanding hydrology comments' dated 12th May 2021 an assessment of appropriate SPR values has been undertaken for the Middleton gauge and G5 gauge using the approach set out in the FEH Volume 4 (Ref. 1). This approach is based on the use of observed high flow and rainfall events within the catchment and observed antecedent catchment conditions.

4.8.2 This assessment has found that the derived mean SPR value for Middleton is 69.6%, which is greater than that derived by catchment descriptors (SPRHOST).

4.8.3 The assessment has found that the derived mean SPR for the G5 gauge is 44.8%, which is greater than that derived by catchment descriptors (SPRHOST).

4.8.4 Furthermore, by adopting the G5 as a donor catchment and using the SPR by donor data transfer procedure and SPR adjustment this results in higher SPR values across all of the upland sub-catchments.

4.8.5 The calculated SPR values for each of the sub-catchment inflows along with the average CWI value of 60.0 (based on the events at G5) were input to the inflow boundary units in the Flood Modeller software to understand the potential impact on the 1 in 100-year hydrographs.

4.8.6 In section 3.2.4 of the FEH Volume 4 (Ref. 1) there is guidance on the likely range of CWI that may be experienced in a catchment. This indicates that CWI typically varies between 120mm and 130mm, except on low SAAR catchments where it may fall to around 60mm. On this basis, a comparison of the flow hydrographs was undertaken assuming that the catchment may have been subject to wetter antecedent conditions. In this sensitivity testing the highest CWI value of 127.7, based on the February 2014 event at the G5 gauge, was also considered to understand the implication this may have on the 1 in 100-year flow hydrograph.

4.8.7 These flow hydrographs were compared with the peak flow hydrographs which were previously derived for both the 50% PR and 75% PR model runs for the LEIS_LEISTON (G5 gauge), Middleton gauge and each of the sub-catchments.

4.8.8 This comparison found that in the majority of the inflow locations i.e. for the LEIS_LEISTON (G5 gauge) and all the sub-catchments, for which G5 is the donor, the peak flow hydrograph for the SPR, based on the donor transfer approach, is close to or below the peak flow hydrograph for the 50% SPR scenario. In all of these inflow locations the peak flow hydrograph based on the calculated SPR is below the peak flow hydrograph for the 75% SPR scenario and in many of the sub-catchments it is significantly lower. Only, in the MINS_US is the SPR peak flow hydrograph greater than both the 50% PR and 75% PR peak flow hydrographs.

4.8.9 Following the above checks, a sensitivity test was undertaken within the hydraulic model with the adjusted SPR and CWI values in the FEH inflow boundaries. The results of this sensitivity testing showed that, despite some increase in peak flood levels due to higher runoff, the relative difference between the baseline and with scheme scenarios remains no more than 0.01m, which is in line with the flood risk impact reported in the **MDS FRA Addendum** (Doc. Ref. 5.2(A)Ad) [AS-157]. Furthermore, there are no additional residential or commercial properties affected beyond those identified in the Application and the maximum increase in flood levels for those properties remains up to 0.01m, as set out in the Application.

4.8.10 The calculations and sensitivity testing show that, even with some changes to the derived flow hydrographs, the relative impact of the Project and flood risk to offsite receptors has not changed, and therefore the conclusions drawn in the Application remain valid.

5 REFH2 DESIGN RAINFALL

5.1.1 The Environment Agency noted in comment 1.8 in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] that if ReFH2 is not the preferred method for estimating river flows then a sensitivity test should be carried out given that the updated version of the software provided the opportunity to incorporate the FEH13 rainfall dataset.

5.1.2 As reported in the Fluvial Modelling Report in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161], a sensitivity test has been undertaken for the 1 in 100-year return period event with flows derived with the ReFH2 method. The estimates were derived using the FEH1999 (FEH99) data and the Environment Agency raised a further comment requesting that the FEH13 rainfall dataset also be considered.

5.1.3 To address this comment, further tests have been undertaken to compare the peak flow and total volume estimates from ReFH2 Flood Modeller units using the FEH99 and FEH13 design rainfall approaches.

5.1.4 Updated FEH catchment descriptors were obtained in May 2021 at the same key locations as those used in the previous hydrological assessment (shown in **Plate 5.1**) as follows:

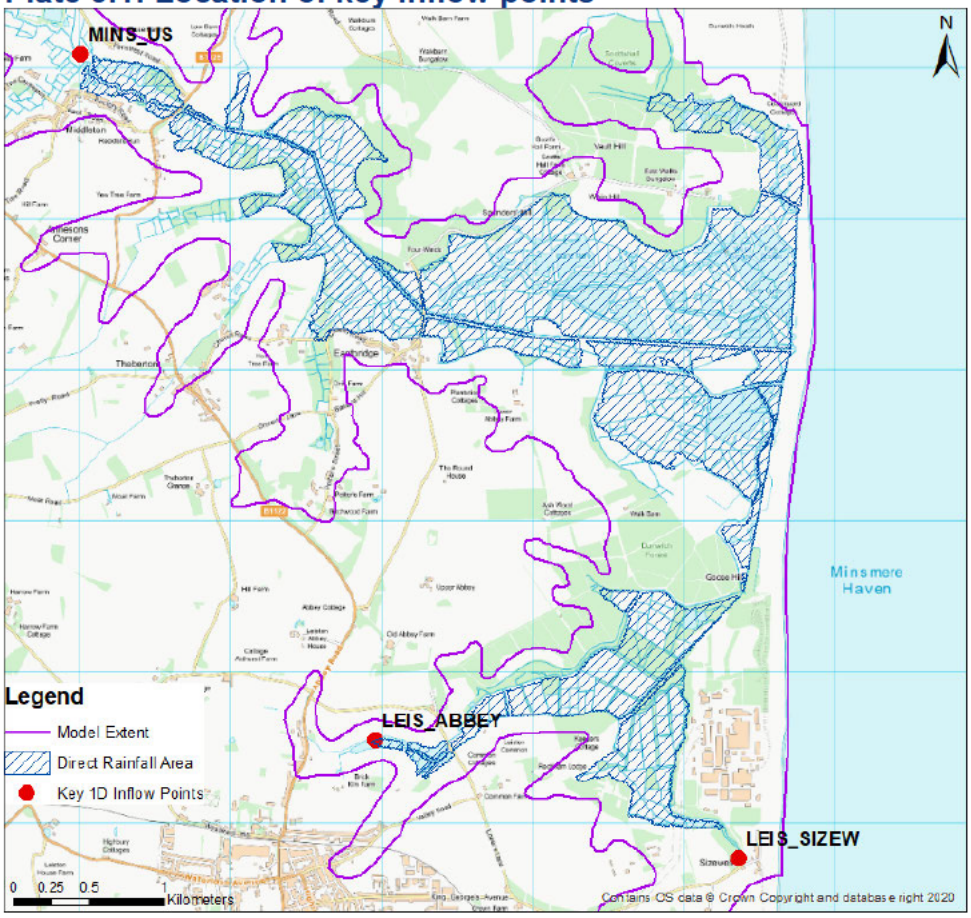
- 643000, 268100 = MINS_US
- 644950, 263550 = LEIS_ABBEY
- 647550, 262800 = LEIS_SIZEW

5.1.5 As part of the comparison exercise, the AREA parameter and the Minimum Flow values were set to be the same for the FEH13 analysis as those previously used for the FEH99 analysis.

5.1.6 The peak flow and total volume estimates for the 1 in 100-year event (121 hour critical storm duration) were subsequently compared for the listed Flood Modeller inflow units as summarised below:

- MINS_US
- LEIS_ABBEY
- LEIS_SIZEW1
- LEIS_SIZEW2
- LEIS_SIZEW3
- LEIS_SIZEW4

Plate 5.1: Location of key inflow points



5.1.7 The Total Flow determined in Flood Modeller using the FEH13 and FEH99 design rainfall approaches are presented and compared below in **Table 5.1**. The output reports from Flood Modeller for the ReFH2 FEH13 analysis are provided in **APPENDIX E:** .

Table 5.1: Comparison of the ReFH2 FEH99 and FEH13 peak flow estimates at key model inflow points for the 1 in 100-year event

Inflow Points	Peak Flow (m^3/s) (ReFH2 – FEH13)	Peak Flow (m^3/s) (ReFH2 – FEH99)	Difference (m3/s) (FEH13 – FEH99)
MINS_US	12.85	12.80	+0.05
LEIS_ABBEY	0.30	0.32	-0.02
LEIS_SIZEW1	0.06	0.05	+0.01
LEIS_SIZEW2	0.04	0.03	+0.01
LEIS_SIZEW3	0.03	0.03	0.00
LEIS_SIZEW4	0.01	0.01	0.00

5.1.8 The combination of FEH13 design rainfall calculations and updated catchment descriptors is shown to result in a minor increase in peak flows for the MINS_US and LEIS_SIZEW1 and LEIS_SIZEW2 locations. At LEIS_ABBEY the FEH13 design rainfall calculations are shown to be marginally lower than the FEH99 results.

5.1.9 The greatest increase in peak flow occurs at MINS_US, where there is an increase of 0.05m^3/s in peak flow. At LEIS_ABBEY, the FEH13 approach results in a reduction in the peak flow of 0.02m^3/s. Across the LEIS_SIZEW sub-catchments, there is a cumulative increase in peak flows of 0.02m^3/s. Subsequently, over the whole catchment there is a total increase in peak flow of 0.05m^3/s for the 1 in 100-year event.

5.1.10 In response to comment 1.9 raised by the Environment Agency and summarised in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161], the change in total volume that would be input into the model as a result of the different approaches (FEH13 vs FEH99) is displayed in **Table 5.2**.

Table 5.2: Comparison of ReFH2 FEH99 and FEH13 total volume estimates at key model inflow points for the 1 in 100-year event

Inflow Points	Total Volume (m^3) (ReFH2 – FEH13)	Total Volume (m^3) (ReFH2 – FEH99)	Difference (m^3) (FEH13 – FEH99)
MINS_US	674.37	672.11	+2.26
LEIS_ABBEY	14.61	15.48	-0.87
LEIS_SIZEW1	2.70	2.17	+0.53
LEIS_SIZEW2	1.90	1.53	+0.37
LEIS_SIZEW3	1.60	1.29	+0.31
LEIS_SIZEW4	0.59	0.47	+0.12

5.1.11 Given that there is an increase in peak flow estimated for the FEH13 approach at MINS_US and LEIS_SIZEW, there is also an increase in estimated total inflow volume at these locations. The total volumes have been calculated over the 121 hour critical storm duration for the 1 in 100-year event. It is predicted that there would be a total increase in volume of 2.26m^3 added to the model at MINS_US using the FEH13 design rainfall approach. A further 1.33m^3 would be added across the four LEIS_SIZEW sub-catchments.

5.1.12 At LEIS_ABBEY, were a reduction in peak flow was predicted using the FEH13 design rainfall approach, it is estimated that there would be a reduction in total volume into the system of 0.87m^3 at this location.

5.1.13 There will subsequently be a net increase of 2.72m^3 across the whole model through using the FEH13 design rainfall approach as opposed to the FEH99 approach.

5.2 Comparison of ReFH2 results with FEH results

5.2.1 As reported in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161], the ReFH2 method was tested in the hydraulic model compared with the results produced by the FEH method. To allow a direct comparison to be undertaken, the same catchment descriptors were used.

5.2.2 Again, this sensitivity test was carried out for the baseline 121-hour storm duration 1 in 100-year return period event.

5.2.3 Table 3.2 from **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] has been replicated below in **Table 5.3** with the results from the ReFH2 FEH13 design rainfall approach also added for comparison.

Table 5.3: Comparison of ReFH2 FEH99, ReFH2 FEH13 and FEH13 total volume estimates at key model inflow points for the 1 in 100-year event

Inflow Points	Peak Flow (m^3/s)			Total Volume (m^3)		
Model Node	**FEH**	**ReFH2 FEH99**	**ReFH2 FEH13**	**FEH**	**ReFH2 FEH99**	**ReFH2 FEH13**
MINS_US	18.64	12.80	12.85	974	672	674
LEIS_ABBEY	0.28	0.32	0.30	17	15	15
LEIS_SIZEW	0.18	0.12	0.14	9	5.5	6.8

5.3 Conclusions

5.3.1 In response to comment 1.8 in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] raised by the Environment Agency a review of the ReFH2 method was undertaken.

5.3.2 As reported in the Fluvial Modelling Report in **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161], a sensitivity test was undertaken for the 1 in 100-year return period event with flows derived with the ReFH2 method; however this was undertaken using the FEH99 rainfall dataset.

5.3.3 The Environment Agency raised a further comment requesting a review based on the FEH13 rainfall dataset and this has been adopted within the above assessment.

5.3.4 All catchment descriptors and parameters were adopted in accordance with those utilised in the original hydrological assessment other than the FEH13. Following comparison of the data in **Table 5.3** , it has been confirmed that although the analysis of the hydrology using the ReFH2 FEH13 rainfall dataset results in a small increase in peak flows, these are lower than those values produced by the FEH method and therefore the findings reported within **Appendix C** of the **MDS FRA Addendum** (Doc Ref. 5.2(A)Ad C) [AS-161] remain current.

5.3.5 As such, it is concluded that the FEH method continues to be considered as the more conservative in terms of its results than the ReFH2 method, and therefore can be continued to be considered as appropriate for adoption in the modelling analysis for the Sizewell C project.

REFERENCES

1. Centre for Ecology and Hydrology (CEH), Flood Estimation Handbook (FEH) – Volume 4: Rainfall-runoff method. 2008.

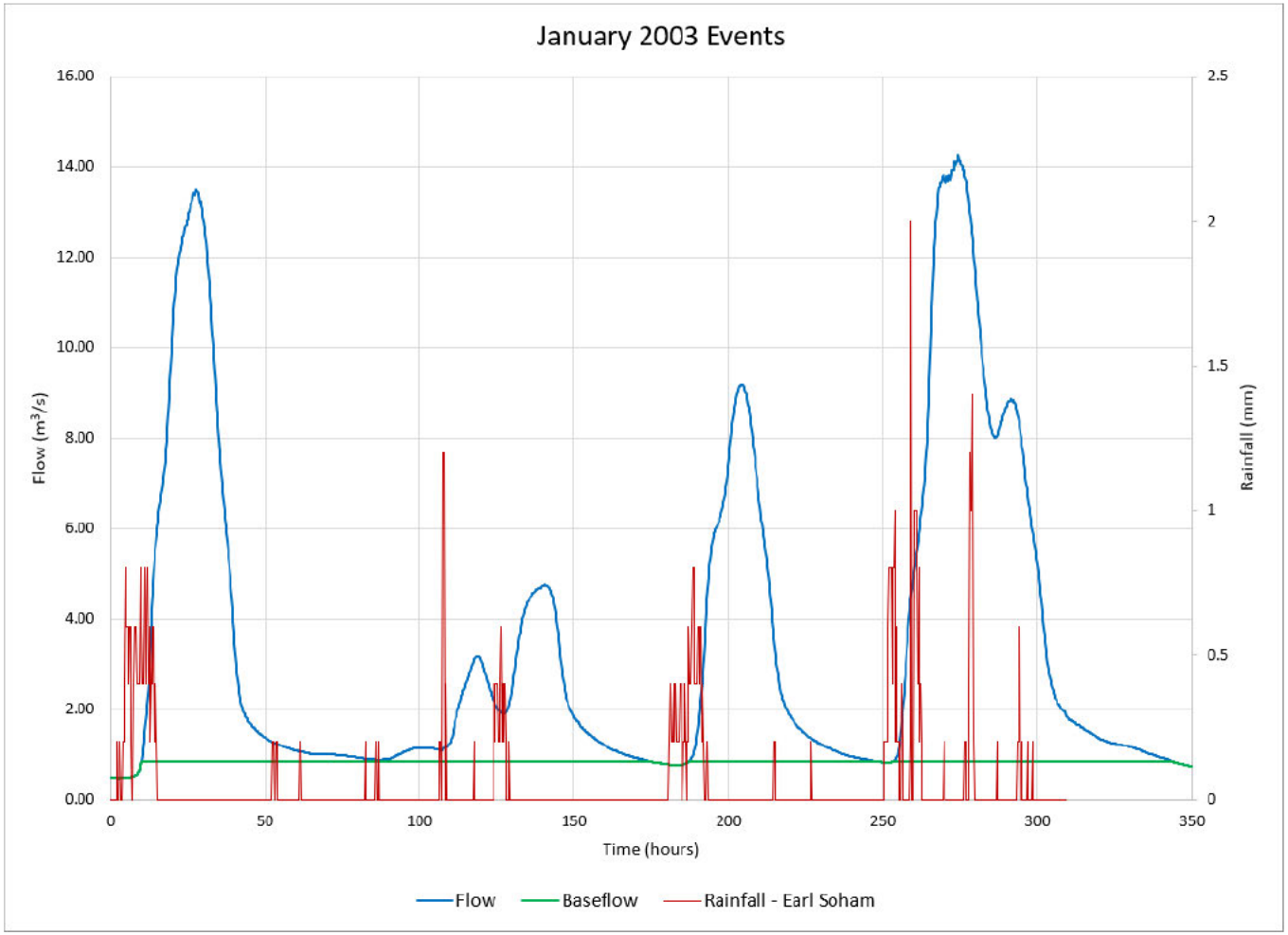


Figure 1: Recorded flow (Middleton) and rainfall (Earl Soham) – January 2003 event

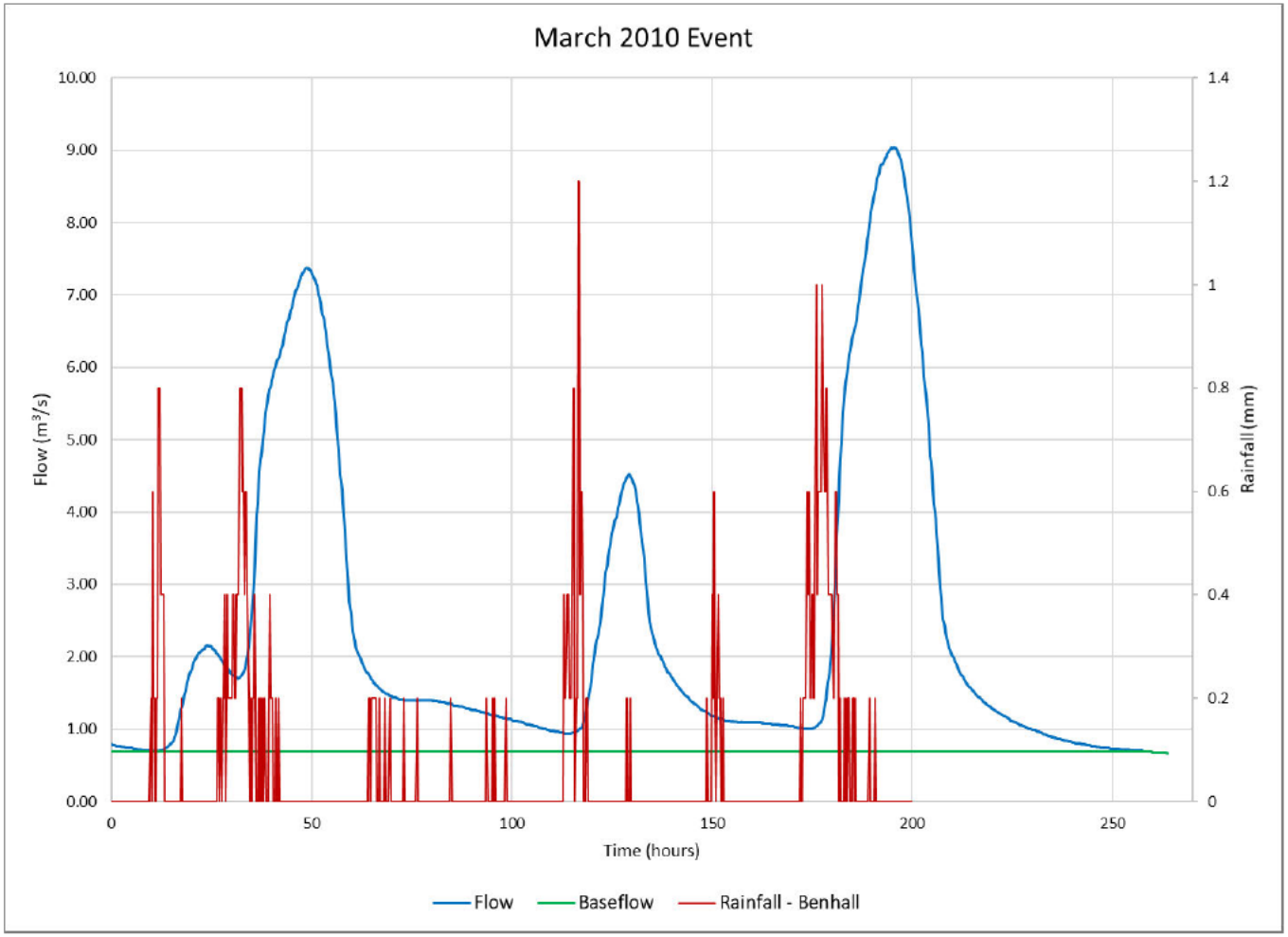


Figure 2: Recorded flow (Middleton) and rainfall (Benhall) – March 2010 event

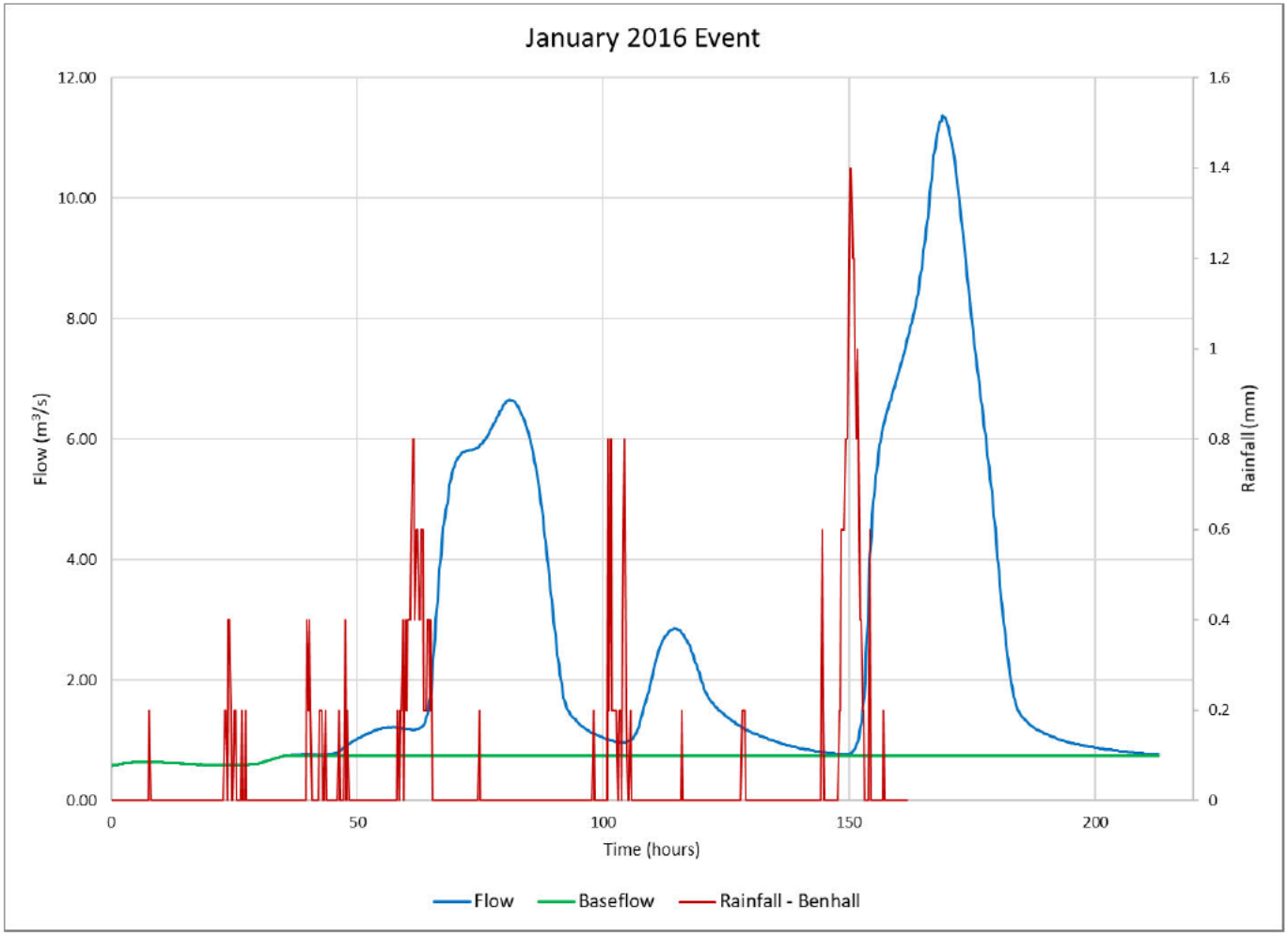


Figure 3: Recorded flow (Middleton) and rainfall (Benhall) – January 2016 event

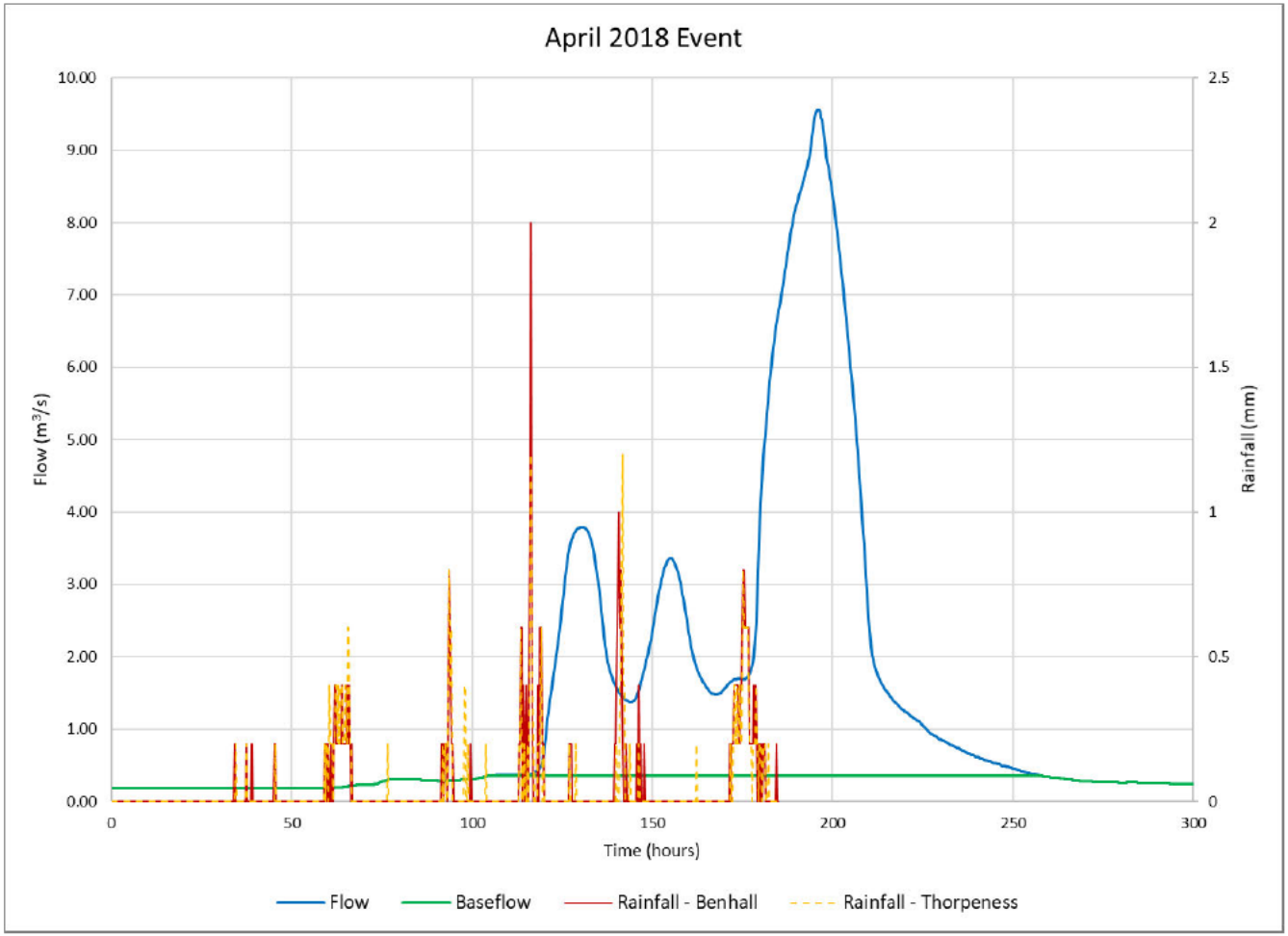


Figure 4: Recorded flow (Middleton) and rainfall (Benhall and Thorpeness) – April 2018 event

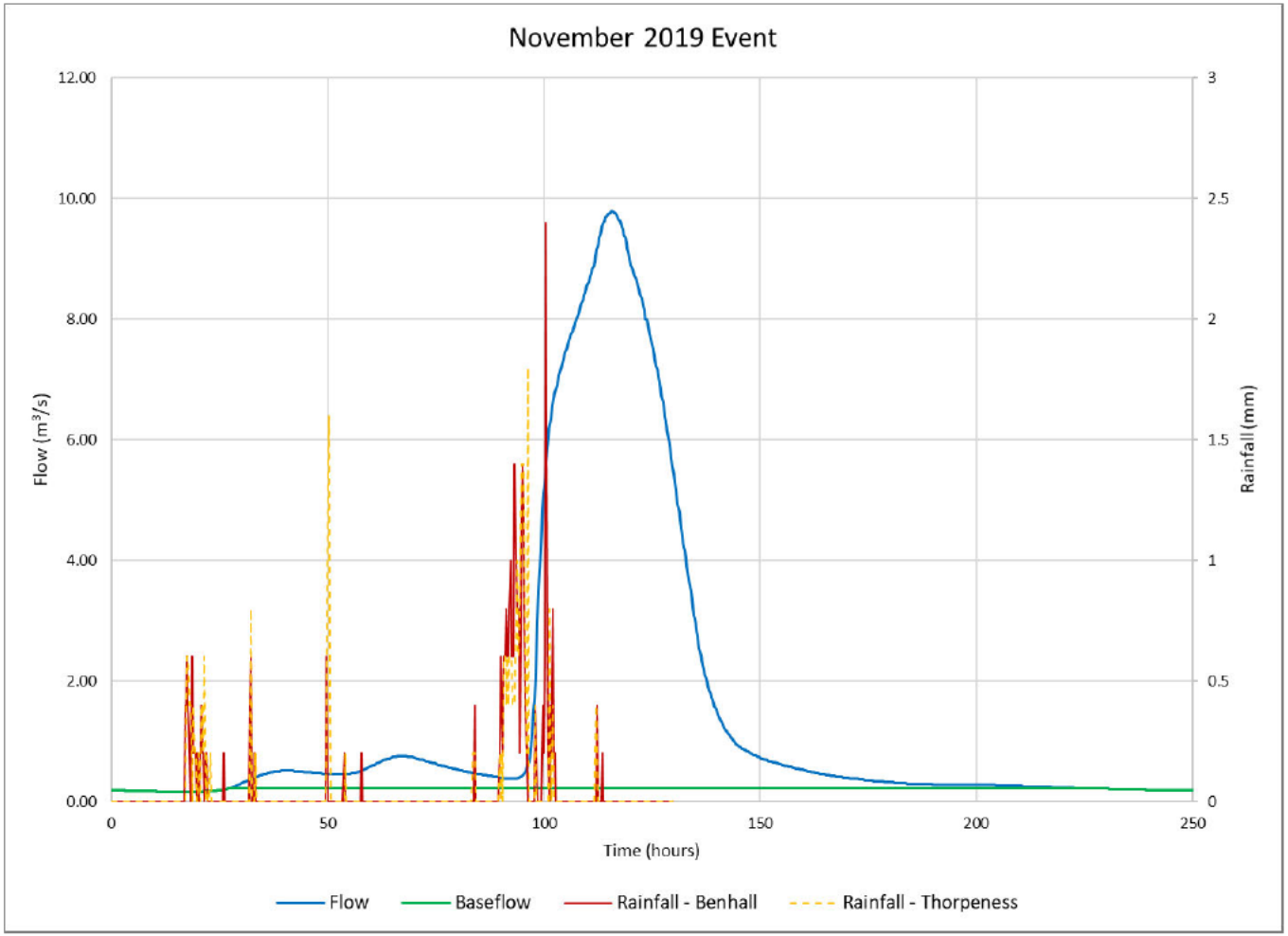


Figure 5: Recorded flow (Middleton) and rainfall (Benhall and Thorpeness) – November 2019 event

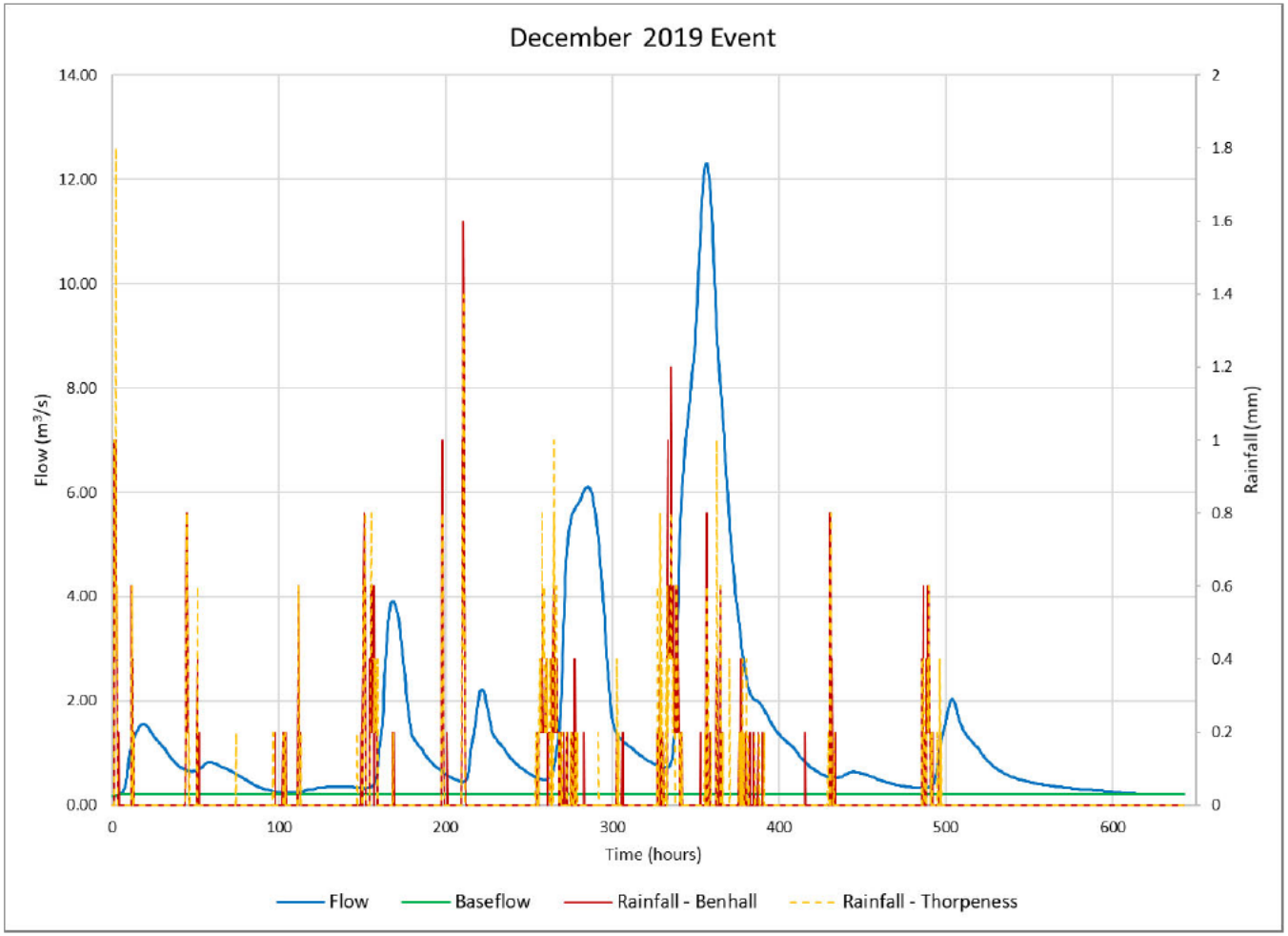


Figure 6: Recorded flow (Middleton) and rainfall (Benhall and Thorpeness) – December 2019 event

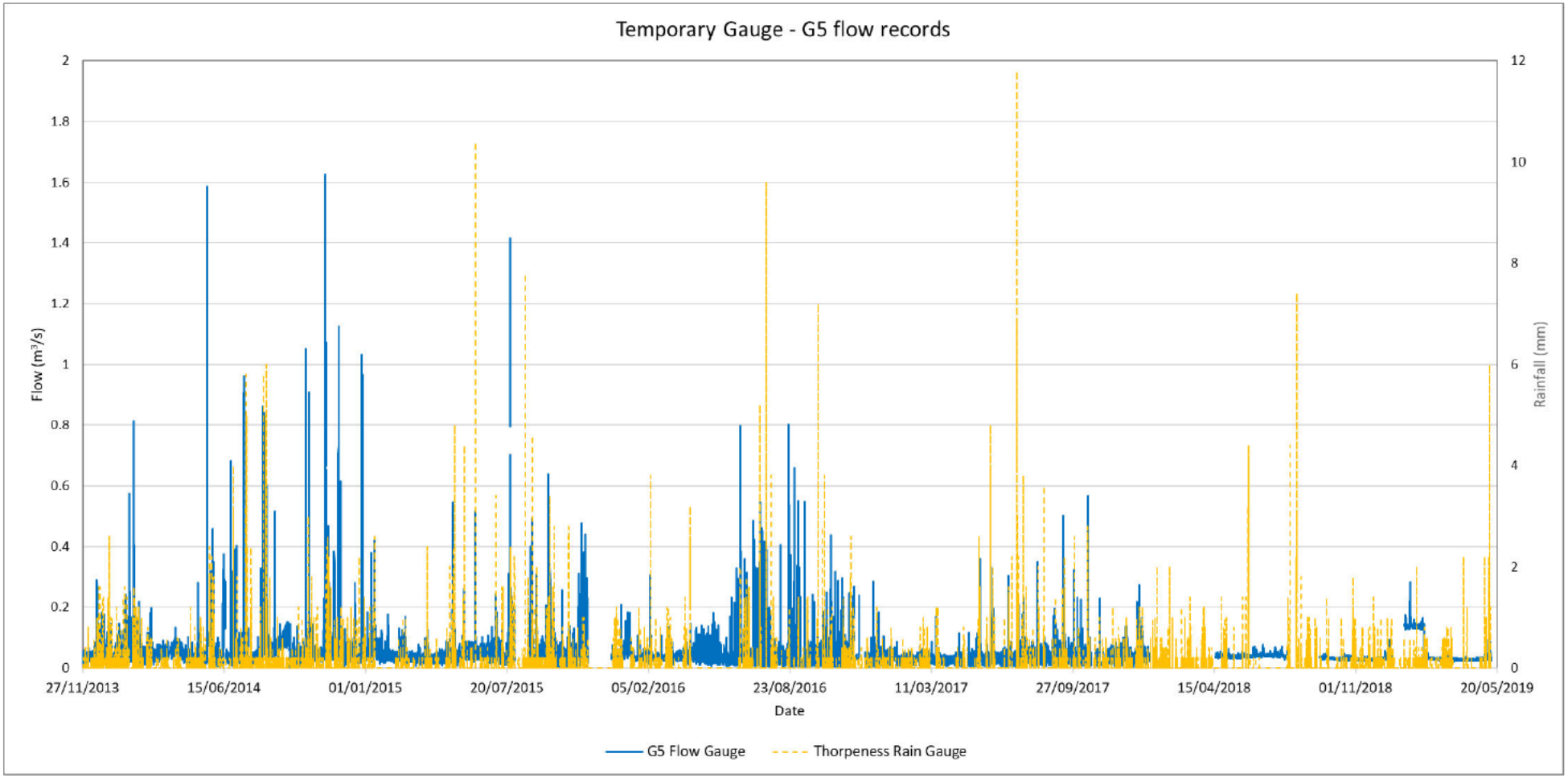


Figure 7: Recorded flow (G5) and rainfall (Thorpeness)

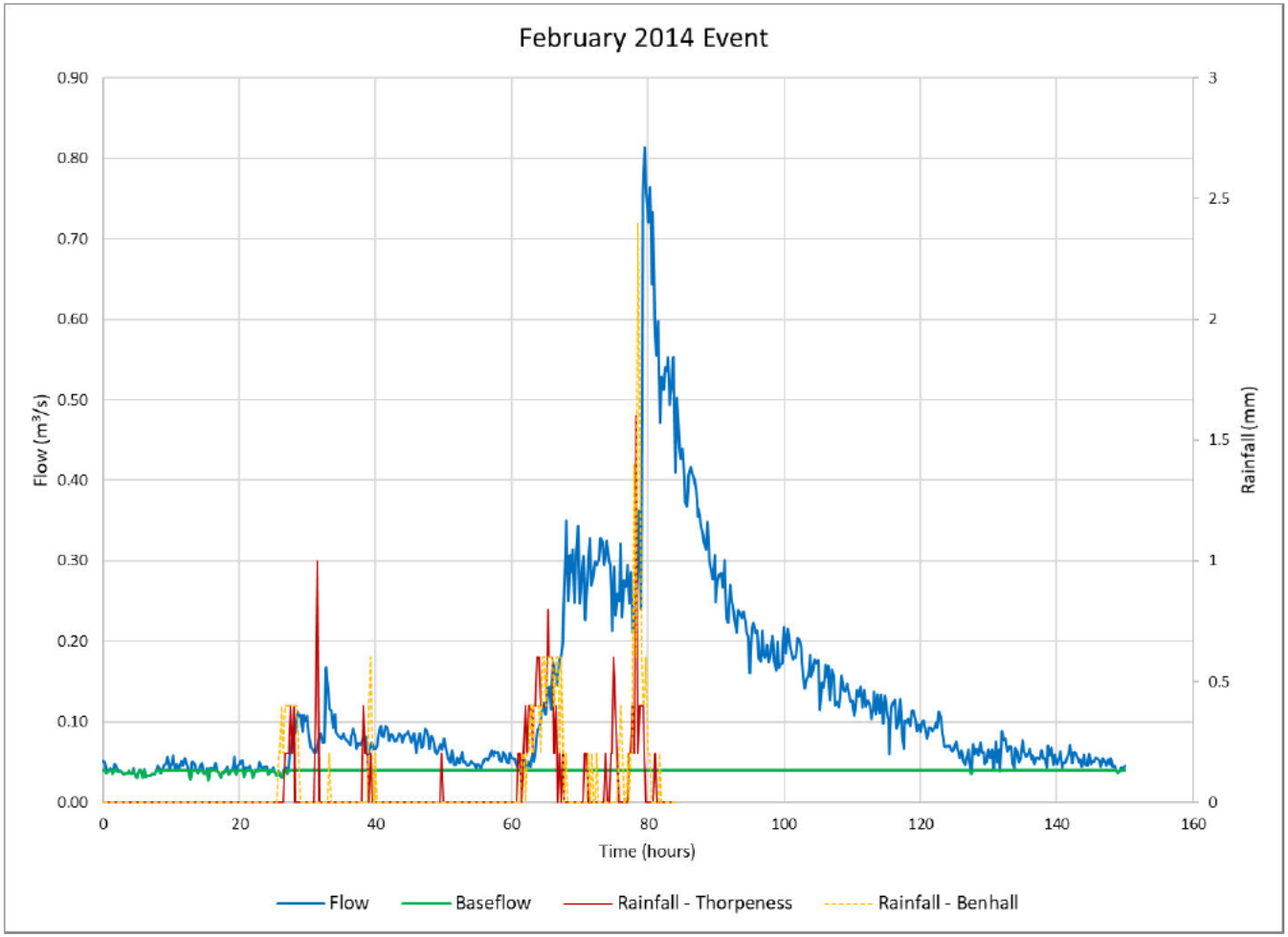


Figure 8: Recorded flow (G5) and rainfall (Benhall and Thorpeness) – February 2014 event

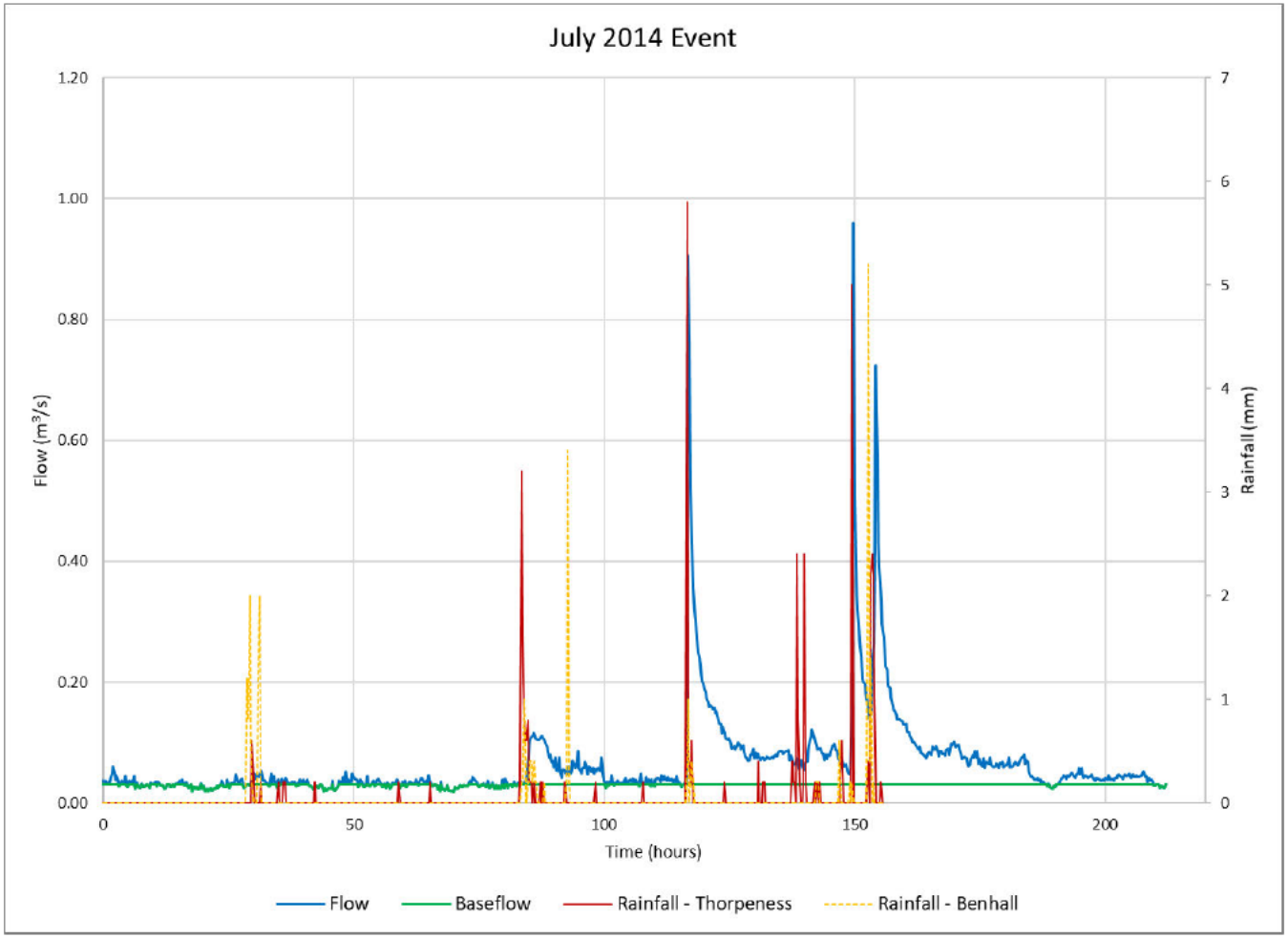


Figure 9: Recorded flow (G5) and rainfall (Benhall and Thorpeness) – July 2014 event

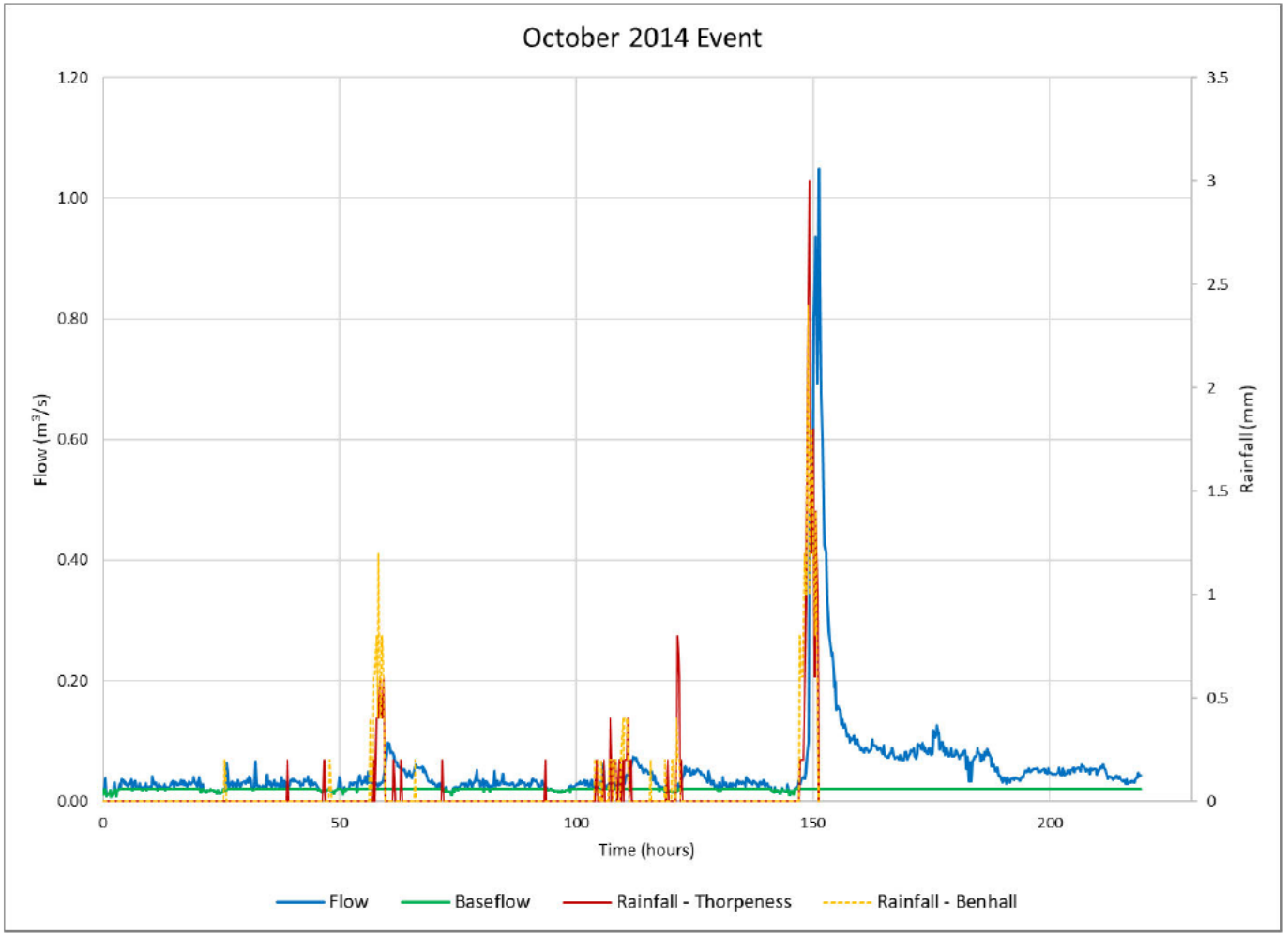


Figure 10: Recorded flow (G5) and rainfall (Benhall and Thorpeness) – October 2014 event

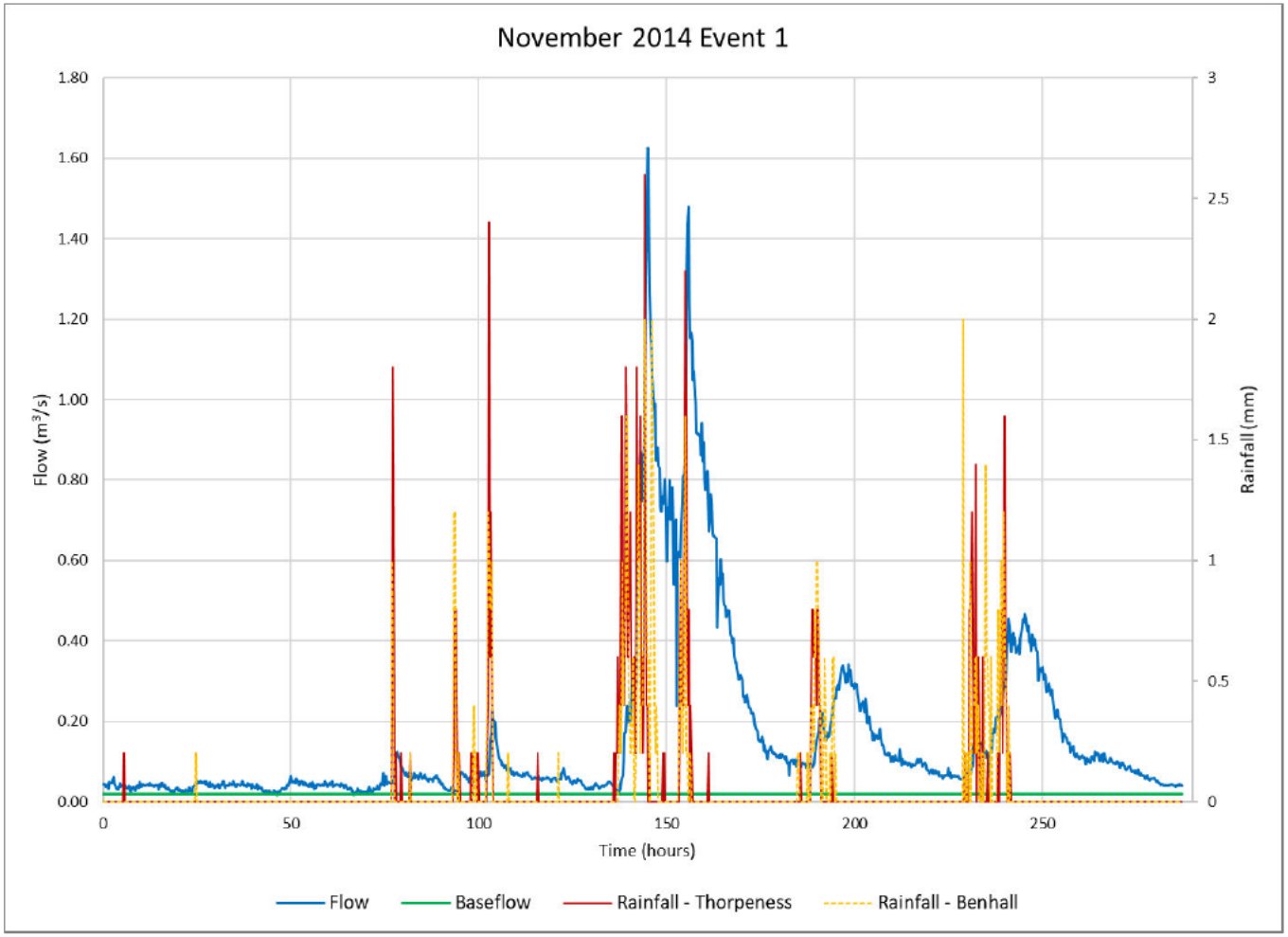


Figure 11: Recorded flow (G5) and rainfall (Benhall and Thorpeness) – November 2014 event 1

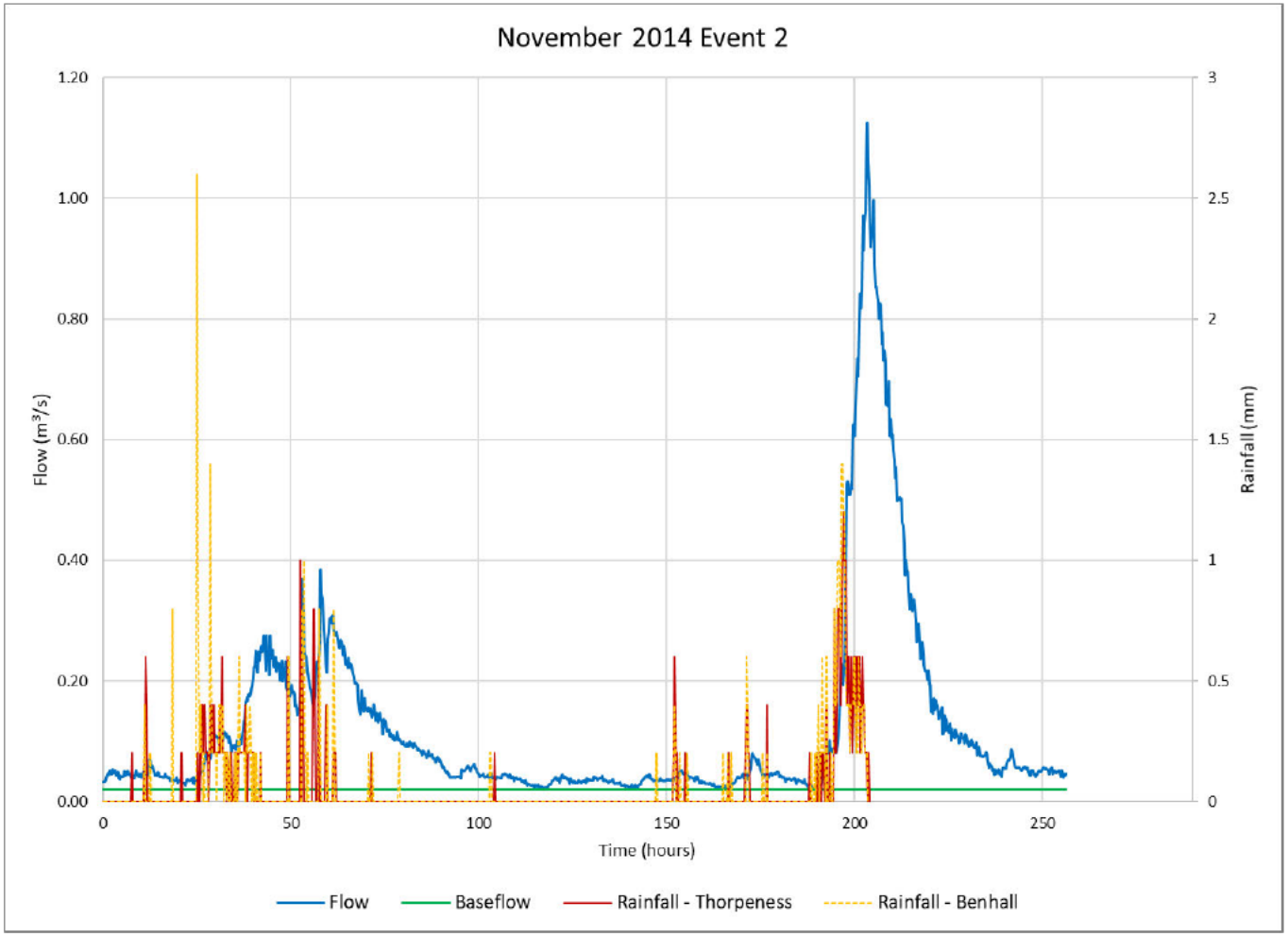


Figure 12: Recorded flow (G5) and rainfall (Benhall and Thorpeness) – November 2014 event 2

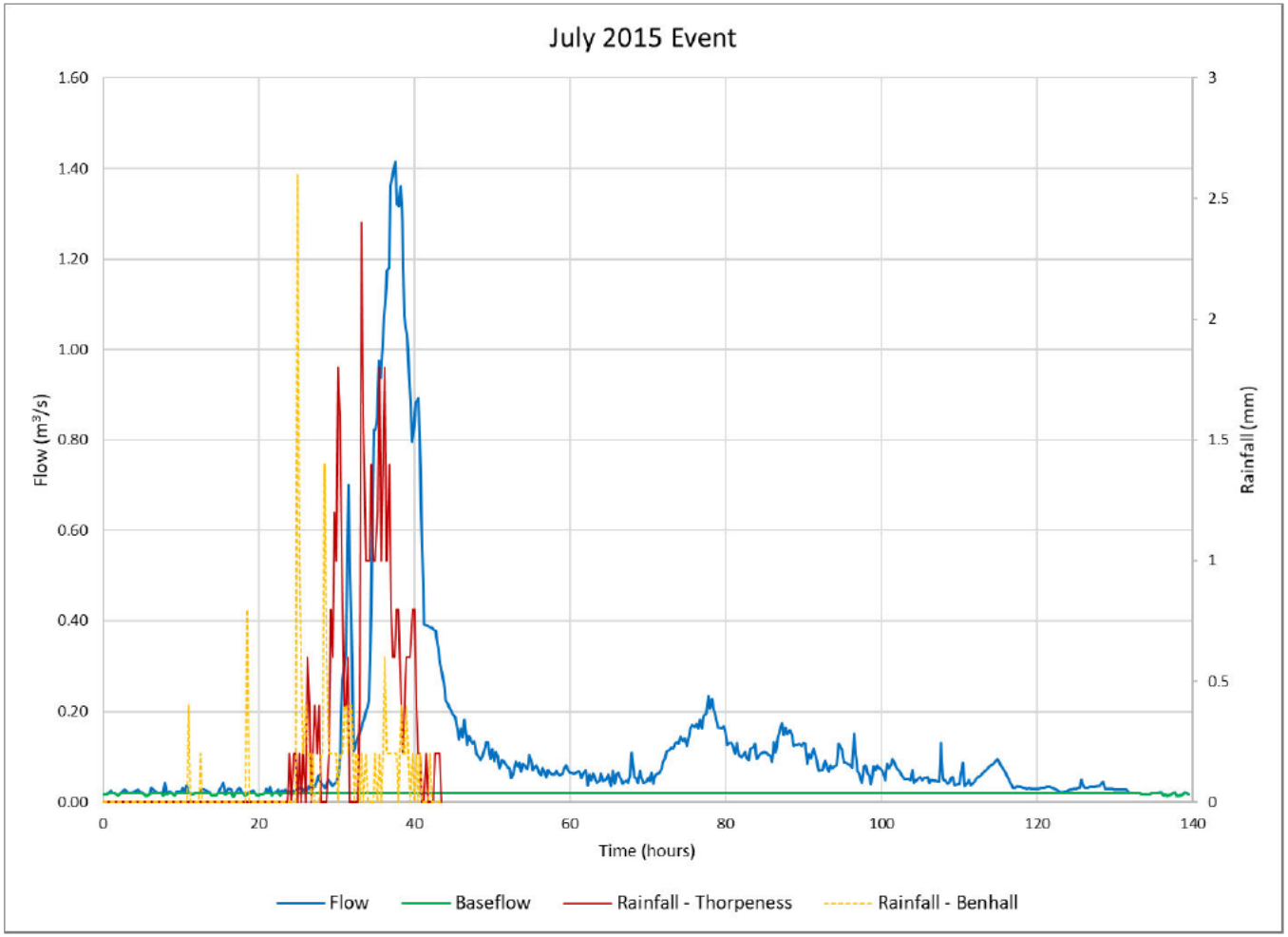


Figure 13: Recorded flow (G5) and rainfall (Benhall and Thorpeness) – July 2015 event

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APPENDIX A: ENVIRONMENT AGENCY NOTE 'SIZEWELL C MDS: OUTSTANDING HYDROLOGY COMMENTS' DATED 12TH MAY 2021

Following a meeting with Royal Haskoning on the 22nd April 2021 and the associated meeting minutes sent on the 30th April, 3 key points remain for the Environment Agency to action in relation to the fluvial hydrology. These are listed in points 1 to 3 below with a response provided under each heading.

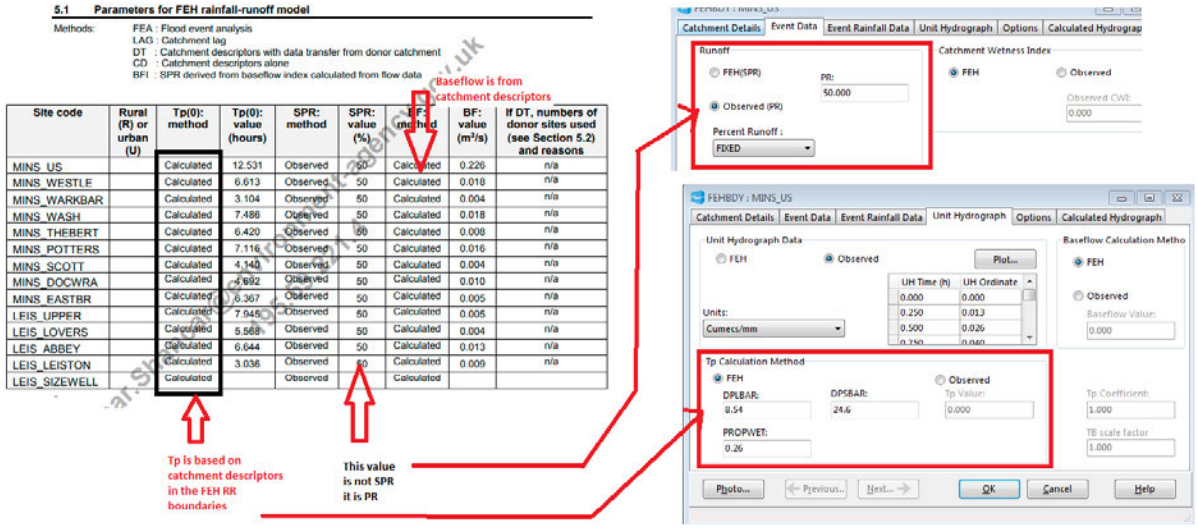
1. EA to provide a summary of the Environment Agency requirements to address and sign off the outstanding hydrological comments

The main outstanding issue is around the derivation of FEH rainfall-runoff parameters. The two key issues are listed below. I have provided the way forward in green text. I think the important thing to note here is that these are not new comments and have been reported in previous comment tracker spreadsheets.

1. Less than the minimum number of events have been used to inform rainfall runoff parameters. 3 events have been used in the study when the FEH Volume 4 states that "*At least five events should be analysed successfully for confidence in the results, the larger the number of events analysed, the greater the reliability of the derived unit hydrograph and losses model parameters* (NERC, 1975, Mawdsley and Tagg, 1981)". The Addendum report does include a qualitative assessment of 3 additional events, these being April 2018, November 2019, and December 2019 and the conclusion is that the hydrograph shape and peak "looks similar" to the other events used in the analysis of percentage runoff. Pointing out similarly in hydrograph shape between the original events and others isn't enough to convince that the parameter estimates are adequate The comment was about the large uncertainty associated with estimating parameters from fewer than the minimum number of events. As a minimum we would want to see 5 events used in the assessment (the additional events shown in the Addendum reporting would be perhaps a sensible choice - April 2018, November 2019, and December 2019). This would add confidence to the estimates. These revised estimates could be compared against those used in the modelling to demonstrate that the conclusions of the FRA would not be affected. In addition, this would add confidence to the estimates for the Nuclear Safety Case.

2. No table with flood event start and end times, antecedent rainfall (AP15), Soil Moisture Deficit (SMD), resulting Catchment Wetness Index (CWI), Percentage Runoff (PR), Dynamic Percentage Runoff (DPR), and Standard Percentage Runoff (SPR) has been provided (5 events minimum as stipulated in the FEH Vol 4) in the Addendum report as requested. Consequently it is difficult to properly scrutinise the calculations. Whilst the FEH calculation record suggests an SPR of 50% has been derived it appears as though SPR has not been calculated and only a fixed PR of 50% has been derived. This has been applied in the FEH RR boundaries as a fixed PR of 50% across all inflow boundaries. The FEH Calculation record erroneously states that SPR for all inflow catchments has been "calculated", that SPR is 50%, and that Time to Peak and Baseflow have been "calculated", this is not the case. Time to Peak and Baseflow appear to be from catchment descriptors, and the SPR value of 50% quoted in the FEH Calculation record is in fact PR (figure 1). This is not good practise. The correct approach would be to calculate SPR using PR, CWI and DPR and then use a donor transfer approach in conjunction with SPRHOST to estimate SPR for all other inflow catchments (e.g. SPRs.adj = SPRs.cds * (SPRg.obs/SPRg.cds)). Worked examples of how to do this and how to present the data are provided in Appendix A of the FEH Volume 4. An example from a modelling study for the River Leen and Day Brook (Black and Veatch, 2011) is also provided (see link below).

Figure 1: Values in the section 5.1 of the FEH calculation record which are not reported correctly. FEH RR parameters from the model hydrology files (ied) are also shown on the right of the image. The FEH calculation record implies that parameters have been calculated when in fact they are based on catchment descriptors or incorrectly quoted in the case of SPR



2. EA to provide example SPR derivation for an urbanised catchment as noted during the meeting

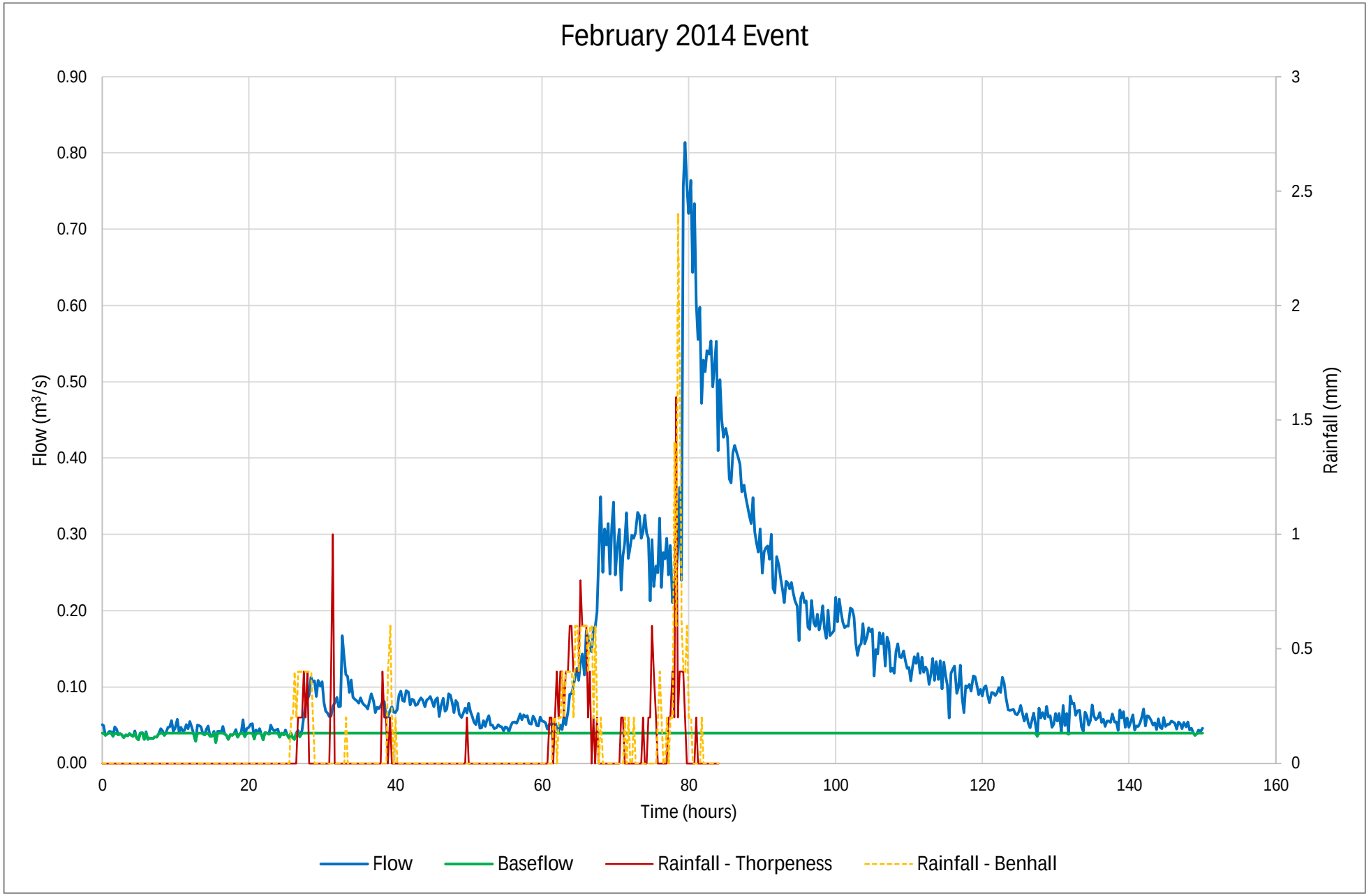
Please find the following link to the River Leen and Day Brook Modelling Study (Black and Veatch, 2011) which provides an example of how SPR has been calculated and how the data has been reported. Further worked examples are also included in Appendix A of the FEH Volume 4. Figure 2.2 of the FEH Volume 4 page 14 also provides a useful flow chart on the approach to parameter estimation based on data availability. When data is available at the subject site the approaches are estimating model parameters from flood event analysis as described in the comments above or to estimate model parameters from catchment LAG and BFI. For donor sites the recommended approach is to use the ratio of observed/estimated model parameters at the donor site to adjust the estimated parameters values at the subject site.

Link to hydrology calculations from the River Leen and Day Brook modelling study (Black and Veatch, 2011):
https://ea.sharefile.com/d-s5785aa00179749c287282d9f91d4149b

3. EA to discuss with internal Environment Agency colleagues data availability / approach in relation to defining the SMD and other parameters related to the derivation of SPR i.e. availability of MORECS or similar data

MORECS and MOSES data are the intellectual property of the Met Office and hence have to be requested from the Met Office for third party work. (https://www.metoffice.gov.uk/services/data/business-data). MORECS data is typically used for the derivation of SMD in studies which have improved the estimate of SMD using the FEH RR approach. The FEH Handbook Volume 4 page 160 states that "*SMD data are available in several forms for different periods. They can be obtained from the Met Office as daily estimated SMDs at synoptic weather stations using a modified Penman model. They can also be obtained as end of week or end of month areal averages over grass for 40km by 40km grid squares from the Met Office Rainfall and Evaporation Calculation System, MORECS which are usually adequate, unless the event is very localised*"

APPENDIX B: PERCENTAGE RUNOFF CALCULATION RECORDS


February 2014 Event
0.90
0.80
0.70
0.60
0.50
0.40
0.30
0.20
0.10
0.00
Flow (m³/s)
3
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
20
40
60
80
100
120
140
160
Time (hours)
Flow
Baseflow
Rainfall - Thorpeness
Rainfall - Benhall

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
04/02/2014 00 00	0.05	0.04	0.01	.	0	.
04/02/2014 00:15	0.05	0.04	0.01	.	0.25	.
04/02/2014 00:30	0.04	0.04	0.00	.	0.5	.
04/02/2014 00:45	0.04	0.04	0.00	.	0.75	.
04/02/2014 01 00	0.04	0.04	0.00	.	1	.
04/02/2014 01:15	0.04	0.04	0.00	.	1.25	.
04/02/2014 01:30	0.04	0.04	0.00	.	1.5	.
04/02/2014 01:45	0.05	0.04	0.01	.	1.75	.
04/02/2014 02 00	0.04	0.04	0.00	.	2	.
04/02/2014 02:15	0.04	0.04	0.00	.	2.25	.
04/02/2014 02:30	0.04	0.04	0.00	.	2.5	.
04/02/2014 02:45	0.04	0.04	0.00	.	2.75	.
04/02/2014 03 00	0.03	0.03	0.00	.	3	.
04/02/2014 03:15	0.04	0.04	0.00	.	3.25	.
04/02/2014 03:30	0.04	0.04	0.00	.	3.5	.
04/02/2014 03:45	0.04	0.04	0.00	.	3.75	.
04/02/2014 04 00	0.04	0.04	0.00	.	4	.
04/02/2014 04:15	0.04	0.04	0.00	.	4.25	.
04/02/2014 04:30	0.04	0.04	0.00	.	4.5	.
04/02/2014 04:45	0.03	0.03	0.00	.	4.75	.
04/02/2014 05 00	0.03	0.03	0.00	.	5	.
04/02/2014 05:15	0.04	0.04	0.00	.	5.25	.
04/02/2014 05:30	0.04	0.04	0.00	.	5.5	.
04/02/2014 05:45	0.03	0.03	0.00	.	5.75	.
04/02/2014 06 00	0.04	0.04	0.00	.	6	.
04/02/2014 06:15	0.03	0.03	0.00	.	6.25	.
04/02/2014 06:30	0.03	0.03	0.00	.	6.5	.
04/02/2014 06:45	0.03	0.03	0.00	.	6.75	.
04/02/2014 07 00	0.03	0.03	0.00	.	7	.
04/02/2014 07:15	0.03	0.03	0.00	.	7.25	.
04/02/2014 07:30	0.03	0.03	0.00	.	7.5	.
04/02/2014 07:45	0.04	0.04	0.00	.	7.75	.
04/02/2014 08 00	0.05	0.04	0.01	.	8	.
04/02/2014 08:15	0.04	0.04	0.00	.	8.25	.
04/02/2014 08:30	0.04	0.04	0.00	.	8.5	.
04/02/2014 08:45	0.04	0.04	0.00	.	8.75	.
04/02/2014 09 00	0.05	0.04	0.01	.	9	.
04/02/2014 09:15	0.05	0.04	0.01	.	9.25	.
04/02/2014 09:30	0.06	0.04	0.02	.	9.5	.
04/02/2014 09:45	0.04	0.04	0.00	.	9.75	.
04/02/2014 10 00	0.05	0.04	0.01	.	10	.
04/02/2014 10:15	0.06	0.04	0.02	.	10.25	.
04/02/2014 10:30	0.04	0.04	0.00	.	10.5	.
04/02/2014 10:45	0.05	0.04	0.01	.	10.75	.
04/02/2014 11 00	0.04	0.04	0.00	.	11	.
04/02/2014 11:15	0.04	0.04	0.00	.	11.25	.
04/02/2014 11:30	0.05	0.04	0.01	.	11.5	.
04/02/2014 11:45	0.05	0.04	0.01	.	11.75	.
04/02/2014 12 00	0.05	0.04	0.01	.	12	.
04/02/2014 12:15	0.05	0.04	0.01	.	12.25	.
04/02/2014 12:30	0.04	0.04	0.00	.	12.5	.
04/02/2014 12:45	0.03	0.03	0.00	.	12.75	.
04/02/2014 13 00	0.05	0.04	0.01	.	13	.
04/02/2014 13:15	0.05	0.04	0.01	.	13.25	.
04/02/2014 13:30	0.05	0.04	0.01	.	13.5	.
04/02/2014 13:45	0.04	0.04	0.00	.	13.75	.
04/02/2014 14 00	0.04	0.04	0.00	.	14	.
04/02/2014 14:15	0.04	0.04	0.00	.	14.25	.
04/02/2014 14:30	0.05	0.04	0.01	.	14.5	.
04/02/2014 14:45	0.04	0.04	0.00	.	14.75	.
04/02/2014 15 00	0.04	0.04	0.00	.	15	.
04/02/2014 15:15	0.04	0.04	0.00	.	15.25	.
04/02/2014 15:30	0.03	0.03	0.00	.	15.5	.
04/02/2014 15:45	0.04	0.04	0.00	.	15.75	.
04/02/2014 16 00	0.04	0.04	0.00	.	16	.
04/02/2014 16:15	0.04	0.04	0.00	.	16.25	.
04/02/2014 16:30	0.05	0.04	0.01	.	16.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Thorpeness	
Area (km^2)	5.04
Total Rain (P) mm	20.2
Time Interval (hour)	0.25
Percentage Runoff	48%

Benhall	
Area (km^2)	5.04
Total Rain (P) mm	26.6
Time Interval (hour)	0.25
Percentage Runoff	36%

Average PR	42%
Overall Average	33%

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
04/02/2014 16:45	0.04	0.04	0.00	.	16.75	.
04/02/2014 17 00	0.04	0.04	0.00	.	17	.
04/02/2014 17:15	0.03	0.03	0.00	.	17.25	.
04/02/2014 17:30	0.04	0.04	0.00	.	17.5	.
04/02/2014 17:45	0.04	0.04	0.00	.	17.75	.
04/02/2014 18 00	0.04	0.04	0.00	.	18	.
04/02/2014 18:15	0.04	0.04	0.00	.	18.25	.
04/02/2014 18:30	0.03	0.03	0.00	.	18.5	.
04/02/2014 18:45	0.04	0.04	0.00	.	18.75	.
04/02/2014 19 00	0.04	0.04	0.00	.	19	.
04/02/2014 19:15	0.06	0.04	0.02	.	19.25	.
04/02/2014 19:30	0.03	0.03	0.00	.	19.5	.
04/02/2014 19:45	0.05	0.04	0.01	.	19.75	.
04/02/2014 20 00	0.05	0.04	0.01	.	20	.
04/02/2014 20:15	0.05	0.04	0.01	.	20.25	.
04/02/2014 20:30	0.05	0.04	0.01	.	20.5	.
04/02/2014 20:45	0.03	0.03	0.00	.	20.75	.
04/02/2014 21 00	0.04	0.04	0.00	.	21	.
04/02/2014 21:15	0.04	0.04	0.00	.	21.25	.
04/02/2014 21:30	0.05	0.04	0.01	.	21.5	.
04/02/2014 21:45	0.04	0.04	0.00	.	21.75	.
04/02/2014 22 00	0.03	0.03	0.00	.	22	.
04/02/2014 22:15	0.04	0.04	0.00	.	22.25	.
04/02/2014 22:30	0.04	0.04	0.00	.	22.5	.
04/02/2014 22:45	0.04	0.04	0.00	.	22.75	.
04/02/2014 23 00	0.05	0.04	0.01	.	23	.
04/02/2014 23:15	0.04	0.04	0.00	.	23.25	.
04/02/2014 23:30	0.04	0.04	0.00	.	23.5	.
04/02/2014 23:45	0.04	0.04	0.00	.	23.75	.
05/02/2014 00 00	0.04	0.04	0.00	.	24	.
05/02/2014 00:15	0.03	0.03	0.00	.	24.25	.
05/02/2014 00:30	0.04	0.04	0.00	.	24.5	.
05/02/2014 00:45	0.04	0.04	0.00	.	24.75	.
05/02/2014 01 00	0.04	0.04	0.00	.	25	.
05/02/2014 01:15	0.04	0.04	0.00	.	25.25	.
05/02/2014 01:30	0.03	0.03	0.00	.	25.5	.
05/02/2014 01:45	0.04	0.04	0.00	.	25.75	0.2
05/02/2014 02 00	0.03	0.03	0.00	.	26	0.2
05/02/2014 02:15	0.03	0.03	0.00	.	26.25	0.4
05/02/2014 02:30	0.04	0.04	0.00	.	26.5	0.2
05/02/2014 02:45	0.04	0.04	0.00	0.2	26.75	0.4
05/02/2014 03 00	0.03	0.03	0.00	0.2	27	0.4
05/02/2014 03:15	0.04	0.04	0.00	0.2	27.25	0.4
05/02/2014 03:30	0.06	0.04	0.02	0.4	27.5	0.4
05/02/2014 03:45	0.08	0.04	0.04	0.2	27.75	0.4
05/02/2014 04 00	0.08	0.04	0.04	0.4	28	0.4
05/02/2014 04:15	0.09	0.04	0.05	.	28.25	0.4
05/02/2014 04:30	0.11	0.04	0.07	.	28.5	0.4
05/02/2014 04:45	0.11	0.04	0.07	.	28.75	0.2
05/02/2014 05 00	0.11	0.04	0.07	.	29	.
05/02/2014 05:15	0.09	0.04	0.05	.	29.25	.
05/02/2014 05:30	0.11	0.04	0.07	.	29.5	.
05/02/2014 05:45	0.10	0.04	0.06	.	29.75	.
05/02/2014 06 00	0.11	0.04	0.07	.	30	.
05/02/2014 06:15	0.08	0.04	0.04	.	30.25	.
05/02/2014 06:30	0.07	0.04	0.03	.	30.5	.
05/02/2014 06:45	0.07	0.04	0.03	.	30.75	.
05/02/2014 07 00	0.06	0.04	0.02	.	31	.
05/02/2014 07:15	0.06	0.04	0.02	0.4	31.25	.
05/02/2014 07:30	0.07	0.04	0.03	1	31.5	.
05/02/2014 07:45	0.08	0.04	0.04	.	31.75	.
05/02/2014 08 00	0.09	0.04	0.05	.	32	.
05/02/2014 08:15	0.07	0.04	0.03	.	32.25	.
05/02/2014 08:30	0.07	0.04	0.03	.	32.5	.
05/02/2014 08:45	0.17	0.04	0.13	.	32.75	.
05/02/2014 09 00	0.14	0.04	0.10	.	33	.
05/02/2014 09:15	0.12	0.04	0.08	.	33.25	0.2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
05/02/2014 09:30	0.11	0.04	0.07	.	33.5	.
05/02/2014 09:45	0.09	0.04	0.05	.	33.75	.
05/02/2014 10 00	0.11	0.04	0.07	.	34	.
05/02/2014 10:15	0.09	0.04	0.05	.	34.25	.
05/02/2014 10:30	0.08	0.04	0.04	.	34.5	.
05/02/2014 10:45	0.08	0.04	0.04	.	34.75	.
05/02/2014 11 00	0.08	0.04	0.04	.	35	.
05/02/2014 11:15	0.09	0.04	0.05	.	35.25	.
05/02/2014 11:30	0.08	0.04	0.04	.	35.5	.
05/02/2014 11:45	0.08	0.04	0.04	.	35.75	.
05/02/2014 12 00	0.07	0.04	0.03	.	36	.
05/02/2014 12:15	0.07	0.04	0.03	.	36.25	.
05/02/2014 12:30	0.08	0.04	0.04	.	36.5	.
05/02/2014 12:45	0.09	0.04	0.05	.	36.75	.
05/02/2014 13 00	0.08	0.04	0.04	.	37	.
05/02/2014 13:15	0.07	0.04	0.03	.	37.25	.
05/02/2014 13:30	0.07	0.04	0.03	.	37.5	.
05/02/2014 13:45	0.07	0.04	0.03	.	37.75	.
05/02/2014 14 00	0.08	0.04	0.04	.	38	.
05/02/2014 14:15	0.08	0.04	0.04	0.4	38.25	.
05/02/2014 14:30	0.08	0.04	0.04	0.2	38.5	.
05/02/2014 14:45	0.06	0.04	0.02	0.2	38.75	.
05/02/2014 15 00	0.06	0.04	0.02	.	39	0.4
05/02/2014 15:15	0.07	0.04	0.03	0.2	39.25	0.6
05/02/2014 15:30	0.07	0.04	0.03	.	39.5	0.2
05/02/2014 15:45	0.07	0.04	0.03	.	39.75	.
05/02/2014 16 00	0.07	0.04	0.03	.	40	0.2
05/02/2014 16:15	0.07	0.04	0.03	.	40.25	.
05/02/2014 16:30	0.09	0.04	0.05	.	40.5	.
05/02/2014 16:45	0.09	0.04	0.05	.	40.75	.
05/02/2014 17 00	0.08	0.04	0.04	.	41	.
05/02/2014 17:15	0.08	0.04	0.04	.	41.25	.
05/02/2014 17:30	0.09	0.04	0.05	.	41.5	.
05/02/2014 17:45	0.09	0.04	0.05	.	41.75	.
05/02/2014 18 00	0.08	0.04	0.04	.	42	.
05/02/2014 18:15	0.08	0.04	0.04	.	42.25	.
05/02/2014 18:30	0.08	0.04	0.04	.	42.5	.
05/02/2014 18:45	0.08	0.04	0.04	.	42.75	.
05/02/2014 19 00	0.08	0.04	0.04	.	43	.
05/02/2014 19:15	0.08	0.04	0.04	.	43.25	.
05/02/2014 19:30	0.09	0.04	0.05	.	43.5	.
05/02/2014 19:45	0.08	0.04	0.04	.	43.75	.
05/02/2014 20 00	0.07	0.04	0.03	.	44	.
05/02/2014 20:15	0.08	0.04	0.04	.	44.25	.
05/02/2014 20:30	0.08	0.04	0.04	.	44.5	.
05/02/2014 20:45	0.09	0.04	0.05	.	44.75	.
05/02/2014 21 00	0.08	0.04	0.04	.	45	.
05/02/2014 21:15	0.07	0.04	0.03	.	45.25	.
05/02/2014 21:30	0.08	0.04	0.04	.	45.5	.
05/02/2014 21:45	0.09	0.04	0.05	.	45.75	.
05/02/2014 22 00	0.06	0.04	0.02	.	46	.
05/02/2014 22:15	0.08	0.04	0.04	.	46.25	.
05/02/2014 22:30	0.09	0.04	0.05	.	46.5	.
05/02/2014 22:45	0.07	0.04	0.03	.	46.75	.
05/02/2014 23 00	0.07	0.04	0.03	.	47	.
05/02/2014 23:15	0.09	0.04	0.05	.	47.25	.
05/02/2014 23:30	0.09	0.04	0.05	.	47.5	.
05/02/2014 23:45	0.08	0.04	0.04	.	47.75	.
06/02/2014 00 00	0.07	0.04	0.03	.	48	.
06/02/2014 00:15	0.08	0.04	0.04	.	48.25	.
06/02/2014 00:30	0.08	0.04	0.04	.	48.5	.
06/02/2014 00:45	0.06	0.04	0.02	.	48.75	.
06/02/2014 01 00	0.06	0.04	0.02	.	49	.
06/02/2014 01:15	0.07	0.04	0.03	.	49.25	.
06/02/2014 01:30	0.07	0.04	0.03	.	49.5	.
06/02/2014 01:45	0.07	0.04	0.03	0.2	49.75	.
06/02/2014 02 00	0.08	0.04	0.04	.	50	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/02/2014 02:15	0.07	0.04	0.03	.	50.25	.
06/02/2014 02:30	0.06	0.04	0.02	.	50.5	.
06/02/2014 02:45	0.05	0.04	0.01	.	50.75	.
06/02/2014 03 00	0.05	0.04	0.01	.	51	.
06/02/2014 03:15	0.06	0.04	0.02	.	51.25	.
06/02/2014 03:30	0.05	0.04	0.01	.	51.5	.
06/02/2014 03:45	0.05	0.04	0.01	.	51.75	.
06/02/2014 04 00	0.06	0.04	0.02	.	52	.
06/02/2014 04:15	0.05	0.04	0.01	.	52.25	.
06/02/2014 04:30	0.06	0.04	0.02	.	52.5	.
06/02/2014 04:45	0.06	0.04	0.02	.	52.75	.
06/02/2014 05 00	0.05	0.04	0.01	.	53	.
06/02/2014 05:15	0.05	0.04	0.01	.	53.25	.
06/02/2014 05:30	0.05	0.04	0.01	.	53.5	.
06/02/2014 05:45	0.05	0.04	0.01	.	53.75	.
06/02/2014 06 00	0.05	0.04	0.01	.	54	.
06/02/2014 06:15	0.05	0.04	0.01	.	54.25	.
06/02/2014 06:30	0.05	0.04	0.01	.	54.5	.
06/02/2014 06:45	0.04	0.04	0.00	.	54.75	.
06/02/2014 07 00	0.05	0.04	0.01	.	55	.
06/02/2014 07:15	0.05	0.04	0.01	.	55.25	.
06/02/2014 07:30	0.04	0.04	0.00	.	55.5	.
06/02/2014 07:45	0.05	0.04	0.01	.	55.75	.
06/02/2014 08 00	0.05	0.04	0.01	.	56	.
06/02/2014 08:15	0.05	0.04	0.01	.	56.25	.
06/02/2014 08:30	0.05	0.04	0.01	.	56.5	.
06/02/2014 08:45	0.06	0.04	0.02	.	56.75	.
06/02/2014 09 00	0.06	0.04	0.02	.	57	.
06/02/2014 09:15	0.06	0.04	0.02	.	57.25	.
06/02/2014 09:30	0.06	0.04	0.02	.	57.5	.
06/02/2014 09:45	0.06	0.04	0.02	.	57.75	.
06/02/2014 10 00	0.06	0.04	0.02	.	58	.
06/02/2014 10:15	0.05	0.04	0.01	.	58.25	.
06/02/2014 10:30	0.05	0.04	0.01	.	58.5	.
06/02/2014 10:45	0.06	0.04	0.02	.	58.75	.
06/02/2014 11 00	0.06	0.04	0.02	.	59	.
06/02/2014 11:15	0.05	0.04	0.01	.	59.25	.
06/02/2014 11:30	0.05	0.04	0.01	.	59.5	.
06/02/2014 11:45	0.06	0.04	0.02	.	59.75	.
06/02/2014 12 00	0.06	0.04	0.02	.	60	.
06/02/2014 12:15	0.05	0.04	0.01	.	60.25	.
06/02/2014 12:30	0.05	0.04	0.01	.	60.5	.
06/02/2014 12:45	0.04	0.04	0.00	.	60.75	.
06/02/2014 13 00	0.05	0.04	0.01	0.2	61	.
06/02/2014 13:15	0.05	0.04	0.01	0.2	61.25	.
06/02/2014 13:30	0.05	0.04	0.01	.	61.5	0.2
06/02/2014 13:45	0.05	0.04	0.01	0.2	61.75	0.2
06/02/2014 14 00	0.05	0.04	0.01	0.4	62	.
06/02/2014 14:15	0.04	0.04	0.00	0.2	62.25	0.2
06/02/2014 14:30	0.05	0.04	0.01	0.4	62.5	0.2
06/02/2014 14:45	0.04	0.04	0.00	0.4	62.75	0.4
06/02/2014 15 00	0.06	0.04	0.02	0.2	63	0.2
06/02/2014 15:15	0.05	0.04	0.01	0.4	63.25	0.4
06/02/2014 15:30	0.07	0.04	0.03	0.4	63.5	0.4
06/02/2014 15:45	0.09	0.04	0.05	0.6	63.75	0.4
06/02/2014 16 00	0.09	0.04	0.05	0.6	64	0.4
06/02/2014 16:15	0.10	0.04	0.06	0.4	64.25	0.2
06/02/2014 16:30	0.11	0.04	0.07	0.4	64.5	0.6
06/02/2014 16:45	0.12	0.04	0.08	0.4	64.75	0.6
06/02/2014 17 00	0.11	0.04	0.07	0.4	65	0.4
06/02/2014 17:15	0.13	0.04	0.09	0.8	65.25	0.6
06/02/2014 17:30	0.14	0.04	0.10	0.6	65.5	0.6
06/02/2014 17:45	0.12	0.04	0.08	0.6	65.75	0.6
06/02/2014 18 00	0.17	0.04	0.13	0.6	66	0.6
06/02/2014 18:15	0.16	0.04	0.12	0.2	66.25	0.4
06/02/2014 18:30	0.16	0.04	0.12	0.4	66.5	0.6
06/02/2014 18:45	0.15	0.04	0.11	.	66.75	0.6

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/02/2014 19 00	0.18	0.04	0.14	0.2	67	0.2
06/02/2014 19:15	0.18	0.04	0.14	.	67.25	0.6
06/02/2014 19:30	0.20	0.04	0.16	0.2	67.5	0.2
06/02/2014 19:45	0.27	0.04	0.23	.	67.75	.
06/02/2014 20 00	0.35	0.04	0.31	.	68	0.2
06/02/2014 20:15	0.25	0.04	0.21	.	68.25	.
06/02/2014 20:30	0.31	0.04	0.27	.	68.5	.
06/02/2014 20:45	0.29	0.04	0.25	.	68.75	.
06/02/2014 21 00	0.31	0.04	0.27	.	69	.
06/02/2014 21:15	0.25	0.04	0.21	.	69.25	.
06/02/2014 21:30	0.31	0.04	0.27	.	69.5	.
06/02/2014 21:45	0.34	0.04	0.30	.	69.75	.
06/02/2014 22 00	0.25	0.04	0.21	.	70	.
06/02/2014 22:15	0.28	0.04	0.24	.	70.25	.
06/02/2014 22:30	0.31	0.04	0.27	.	70.5	.
06/02/2014 22:45	0.23	0.04	0.19	0.2	70.75	.
06/02/2014 23 00	0.27	0.04	0.23	0.2	71	.
06/02/2014 23:15	0.29	0.04	0.25	.	71.25	0.2
06/02/2014 23:30	0.33	0.04	0.29	.	71.5	.
06/02/2014 23:45	0.27	0.04	0.23	.	71.75	0.2
07/02/2014 00 00	0.28	0.04	0.24	.	72	.
07/02/2014 00:15	0.30	0.04	0.26	.	72.25	.
07/02/2014 00:30	0.29	0.04	0.25	.	72.5	0.2
07/02/2014 00:45	0.30	0.04	0.26	.	72.75	.
07/02/2014 01 00	0.33	0.04	0.29	.	73	.
07/02/2014 01:15	0.32	0.04	0.28	.	73.25	.
07/02/2014 01:30	0.29	0.04	0.25	.	73.5	.
07/02/2014 01:45	0.30	0.04	0.26	0.2	73.75	.
07/02/2014 02 00	0.33	0.04	0.29	.	74	.
07/02/2014 02:15	0.30	0.04	0.26	.	74.25	.
07/02/2014 02:30	0.29	0.04	0.25	0.2	74.5	.
07/02/2014 02:45	0.21	0.04	0.17	0.2	74.75	.
07/02/2014 03 00	0.29	0.04	0.25	0.6	75	.
07/02/2014 03:15	0.23	0.04	0.19	0.4	75.25	.
07/02/2014 03:30	0.26	0.04	0.22	0.2	75.5	.
07/02/2014 03:45	0.25	0.04	0.21	.	75.75	0.2
07/02/2014 04 00	0.32	0.04	0.28	.	76	0.4
07/02/2014 04:15	0.23	0.04	0.19	.	76.25	0.2
07/02/2014 04:30	0.28	0.04	0.24	.	76.5	.
07/02/2014 04:45	0.27	0.04	0.23	.	76.75	.
07/02/2014 05 00	0.30	0.04	0.26	.	77	0.2
07/02/2014 05:15	0.25	0.04	0.21	0.2	77.25	.
07/02/2014 05:30	0.29	0.04	0.25	0.2	77.5	0.2
07/02/2014 05:45	0.21	0.04	0.17	0.4	77.75	0.2
07/02/2014 06 00	0.24	0.04	0.20	0.2	78	1.4
07/02/2014 06:15	0.25	0.04	0.21	1.6	78.25	0.6
07/02/2014 06:30	0.28	0.04	0.24	0.2	78.5	2.4
07/02/2014 06:45	0.36	0.04	0.32	0.4	78.75	1.6
07/02/2014 07 00	0.24	0.04	0.20	0.4	79	0.6
07/02/2014 07:15	0.75	0.04	0.71	0.4	79.25	0.4
07/02/2014 07:30	0.81	0.04	0.77	0.2	79.5	0.4
07/02/2014 07:45	0.76	0.04	0.72	.	79.75	0.6
07/02/2014 08 00	0.72	0.04	0.68	.	80	0.2
07/02/2014 08:15	0.76	0.04	0.72	.	80.25	0.2
07/02/2014 08:30	0.64	0.04	0.60	.	80.5	.
07/02/2014 08:45	0.73	0.04	0.69	.	80.75	.
07/02/2014 09 00	0.60	0.04	0.56	0.2	81	.
07/02/2014 09:15	0.56	0.04	0.52	.	81.25	.
07/02/2014 09:30	0.60	0.04	0.56	.	81.5	.
07/02/2014 09:45	0.47	0.04	0.43	.	81.75	0.2
07/02/2014 10 00	0.53	0.04	0.49	.	82	.
07/02/2014 10:15	0.51	0.04	0.47	.	82.25	.
07/02/2014 10:30	0.54	0.04	0.50	.	82.5	.
07/02/2014 10:45	0.54	0.04	0.50	.	82.75	.
07/02/2014 11 00	0.55	0.04	0.51	.	83	.
07/02/2014 11:15	0.49	0.04	0.45	.	83.25	.
07/02/2014 11:30	0.52	0.04	0.48	.	83.5	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
07/02/2014 11:45	0.55	0.04	0.51	.	83.75	.
07/02/2014 12 00	0.41	0.04	0.37	.	84	.
07/02/2014 12:15	0.50	0.04	0.46	.	84.25	.
07/02/2014 12:30	0.45	0.04	0.41	.	84.5	.
07/02/2014 12:45	0.43	0.04	0.39	.	84.75	.
07/02/2014 13 00	0.44	0.04	0.40	.	85	.
07/02/2014 13:15	0.43	0.04	0.39	.	85.25	.
07/02/2014 13:30	0.37	0.04	0.33	.	85.5	.
07/02/2014 13:45	0.37	0.04	0.33	.	85.75	.
07/02/2014 14 00	0.41	0.04	0.37	.	86	.
07/02/2014 14:15	0.42	0.04	0.38	.	86.25	.
07/02/2014 14:30	0.41	0.04	0.37	.	86.5	.
07/02/2014 14:45	0.40	0.04	0.36	.	86.75	.
07/02/2014 15 00	0.39	0.04	0.35	.	87	.
07/02/2014 15:15	0.36	0.04	0.32	.	87.25	.
07/02/2014 15:30	0.36	0.04	0.32	.	87.5	.
07/02/2014 15:45	0.35	0.04	0.31	.	87.75	.
07/02/2014 16 00	0.34	0.04	0.30	.	88	.
07/02/2014 16:15	0.32	0.04	0.28	.	88.25	.
07/02/2014 16:30	0.31	0.04	0.27	.	88.5	.
07/02/2014 16:45	0.35	0.04	0.31	.	88.75	.
07/02/2014 17 00	0.30	0.04	0.26	.	89	.
07/02/2014 17:15	0.29	0.04	0.25	.	89.25	.
07/02/2014 17:30	0.28	0.04	0.24	.	89.5	.
07/02/2014 17:45	0.31	0.04	0.27	.	89.75	.
07/02/2014 18 00	0.25	0.04	0.21	.	90	.
07/02/2014 18:15	0.28	0.04	0.24	.	90.25	.
07/02/2014 18:30	0.28	0.04	0.24	.	90.5	.
07/02/2014 18:45	0.28	0.04	0.24	.	90.75	.
07/02/2014 19 00	0.27	0.04	0.23	.	91	.
07/02/2014 19:15	0.30	0.04	0.26	.	91.25	.
07/02/2014 19:30	0.23	0.04	0.19	.	91.5	.
07/02/2014 19:45	0.22	0.04	0.18	.	91.75	.
07/02/2014 20 00	0.27	0.04	0.23	.	92	.
07/02/2014 20:15	0.26	0.04	0.22	.	92.25	.
07/02/2014 20:30	0.24	0.04	0.20	.	92.5	.
07/02/2014 20:45	0.23	0.04	0.19	.	92.75	.
07/02/2014 21 00	0.21	0.04	0.17	.	93	.
07/02/2014 21:15	0.24	0.04	0.20	.	93.25	.
07/02/2014 21:30	0.24	0.04	0.20	.	93.5	.
07/02/2014 21:45	0.23	0.04	0.19	.	93.75	.
07/02/2014 22 00	0.24	0.04	0.20	.	94	.
07/02/2014 22:15	0.22	0.04	0.18	.	94.25	.
07/02/2014 22:30	0.21	0.04	0.17	.	94.5	.
07/02/2014 22:45	0.21	0.04	0.17	.	94.75	.
07/02/2014 23 00	0.16	0.04	0.12	.	95	.
07/02/2014 23:15	0.22	0.04	0.18	.	95.25	.
07/02/2014 23:30	0.22	0.04	0.18	.	95.5	.
07/02/2014 23:45	0.21	0.04	0.17	.	95.75	.
08/02/2014 00 00	0.21	0.04	0.17	.	96	.
08/02/2014 00:15	0.18	0.04	0.14	0.2	96.25	.
08/02/2014 00:30	0.18	0.04	0.14	.	96.5	.
08/02/2014 00:45	0.21	0.04	0.17	.	96.75	.
08/02/2014 01 00	0.18	0.04	0.14	.	97	0.2
08/02/2014 01:15	0.18	0.04	0.14	0.2	97.25	.
08/02/2014 01:30	0.20	0.04	0.16	.	97.5	.
08/02/2014 01:45	0.17	0.04	0.13	0.2	97.75	0.2
08/02/2014 02 00	0.19	0.04	0.15	0.2	98	.
08/02/2014 02:15	0.21	0.04	0.17	0.4	98.25	0.2
08/02/2014 02:30	0.18	0.04	0.14	0.4	98.5	0.2
08/02/2014 02:45	0.16	0.04	0.12	0.2	98.75	0.2
08/02/2014 03 00	0.20	0.04	0.16	.	99	0.4
08/02/2014 03:15	0.17	0.04	0.13	.	99.25	0.6
08/02/2014 03:30	0.17	0.04	0.13	.	99.5	.
08/02/2014 03:45	0.17	0.04	0.13	.	99.75	.
08/02/2014 04 00	0.22	0.04	0.18	0.2	100	0.2
08/02/2014 04:15	0.19	0.04	0.15	.	100.25	.

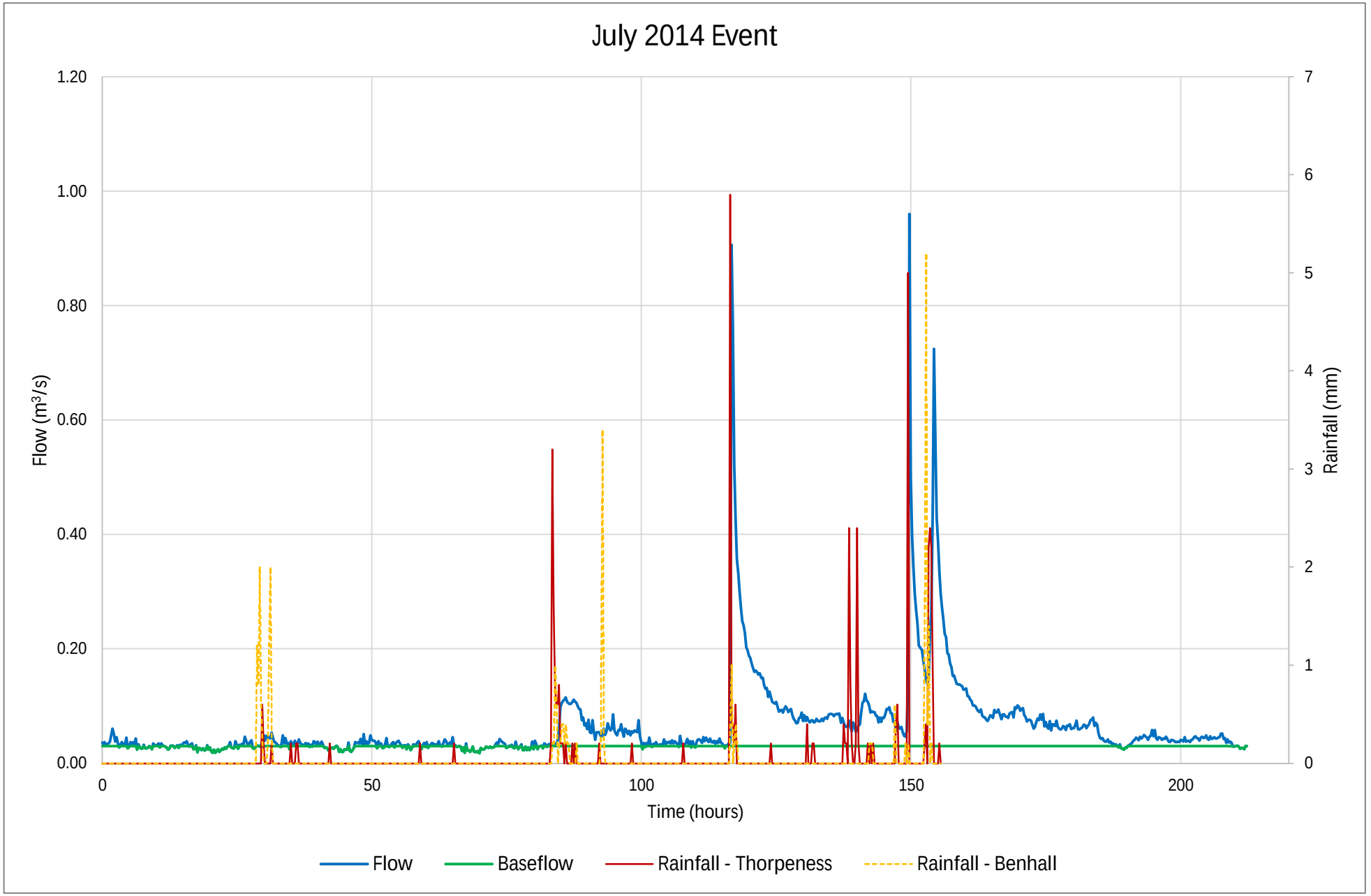
Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

		G5			Thorpeness		Benhall	Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)	Total Rain = rainfall only up to start of the event
08/02/2014 04:30	0.22	0.04	0.18		.	100.5	.	
08/02/2014 04:45	0.20	0.04	0.16		.	100.75	.	
08/02/2014 05 00	0.18	0.04	0.14		.	101	.	
08/02/2014 05:15	0.18	0.04	0.14		.	101.25	.	
08/02/2014 05:30	0.18	0.04	0.14		.	101.5	.	
08/02/2014 05:45	0.18	0.04	0.14		.	101.75	0.2	
08/02/2014 06 00	0.20	0.04	0.16		.	102	.	
08/02/2014 06:15	0.20	0.04	0.16		0.4	102.25	.	
08/02/2014 06:30	0.19	0.04	0.15		1.4	102.5	.	
08/02/2014 06:45	0.16	0.04	0.12		0.2	102.75	.	
08/02/2014 07 00	0.14	0.04	0.10		0.2	103	.	
08/02/2014 07:15	0.15	0.04	0.11		.	103.25	0.2	
08/02/2014 07:30	0.16	0.04	0.12		.	103.5	.	
08/02/2014 07:45	0.18	0.04	0.14		.	103.75	.	
08/02/2014 08 00	0.16	0.04	0.12		.	104	.	
08/02/2014 08:15	0.17	0.04	0.13		.	104.25	.	
08/02/2014 08:30	0.18	0.04	0.14		.	104.5	.	
08/02/2014 08:45	0.17	0.04	0.13		0.2	104.75	.	
08/02/2014 09 00	0.18	0.04	0.14		.	105	.	
08/02/2014 09:15	0.11	0.04	0.07		.	105.25	0.2	
08/02/2014 09:30	0.15	0.04	0.11		.	105.5	.	
08/02/2014 09:45	0.14	0.04	0.10		.	105.75	.	
08/02/2014 10 00	0.17	0.04	0.13		.	106	.	
08/02/2014 10:15	0.16	0.04	0.12		.	106.25	.	
08/02/2014 10:30	0.17	0.04	0.13		.	106.5	.	
08/02/2014 10:45	0.13	0.04	0.09		.	106.75	.	
08/02/2014 11 00	0.17	0.04	0.13		.	107	.	
08/02/2014 11:15	0.16	0.04	0.12		.	107.25	.	
08/02/2014 11:30	0.12	0.04	0.08		.	107.5	.	
08/02/2014 11:45	0.12	0.04	0.08		.	107.75	.	
08/02/2014 12 00	0.12	0.04	0.08		.	108	.	
08/02/2014 12:15	0.15	0.04	0.11		.	108.25	0.4	
08/02/2014 12:30	0.16	0.04	0.12		.	108.5	.	
08/02/2014 12:45	0.14	0.04	0.10		.	108.75	.	
08/02/2014 13 00	0.14	0.04	0.10		.	109	.	
08/02/2014 13:15	0.15	0.04	0.11		.	109.25	.	
08/02/2014 13:30	0.13	0.04	0.09		.	109.5	.	
08/02/2014 13:45	0.12	0.04	0.08		.	109.75	.	
08/02/2014 14 00	0.13	0.04	0.09		.	110	.	
08/02/2014 14:15	0.11	0.04	0.07		.	110.25	.	
08/02/2014 14:30	0.13	0.04	0.09		.	110.5	.	
08/02/2014 14:45	0.14	0.04	0.10		.	110.75	.	
08/02/2014 15 00	0.13	0.04	0.09		.	111	.	
08/02/2014 15:15	0.14	0.04	0.10		.	111.25	.	
08/02/2014 15:30	0.12	0.04	0.08		.	111.5	.	
08/02/2014 15:45	0.14	0.04	0.10		.	111.75	.	
08/02/2014 16 00	0.12	0.04	0.08		.	112	.	
08/02/2014 16:15	0.13	0.04	0.09		.	112.25	.	
08/02/2014 16:30	0.12	0.04	0.08		.	112.5	.	
08/02/2014 16:45	0.10	0.04	0.06		.	112.75	.	
08/02/2014 17 00	0.12	0.04	0.08		.	113	.	
08/02/2014 17:15	0.14	0.04	0.10		.	113.25	.	
08/02/2014 17:30	0.11	0.04	0.07		.	113.5	.	
08/02/2014 17:45	0.13	0.04	0.09		.	113.75	.	
08/02/2014 18 00	0.11	0.04	0.07		.	114	.	
08/02/2014 18:15	0.13	0.04	0.09		.	114.25	.	
08/02/2014 18:30	0.10	0.04	0.06		.	114.5	.	
08/02/2014 18:45	0.13	0.04	0.09		.	114.75	.	
08/02/2014 19 00	0.12	0.04	0.08		.	115	.	
08/02/2014 19:15	0.10	0.04	0.06		.	115.25	.	
08/02/2014 19:30	0.06	0.04	0.02		.	115.5	.	
08/02/2014 19:45	0.12	0.04	0.08		.	115.75	.	
08/02/2014 20 00	0.12	0.04	0.08		.	116	.	
08/02/2014 20:15	0.13	0.04	0.09		.	116.25	.	
08/02/2014 20:30	0.09	0.04	0.05		.	116.5	.	
08/02/2014 20:45	0.10	0.04	0.06		.	116.75	.	
08/02/2014 21 00	0.13	0.04	0.09		.	117	.	

	G5			Thorpeness		Benhall	Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Total Rain = rainfall only up to start of the event
08/02/2014 21:15	0.09	0.04	0.05	.	117.25	.	
08/02/2014 21:30	0.07	0.04	0.03	.	117.5	.	
08/02/2014 21:45	0.10	0.04	0.06	.	117.75	.	
08/02/2014 22 00	0.10	0.04	0.06	.	118	.	
08/02/2014 22:15	0.10	0.04	0.06	.	118.25	.	
08/02/2014 22:30	0.09	0.04	0.05	.	118.5	.	
08/02/2014 22:45	0.11	0.04	0.07	.	118.75	.	
08/02/2014 23 00	0.11	0.04	0.07	.	119	.	
08/02/2014 23:15	0.10	0.04	0.06	.	119.25	.	
08/02/2014 23:30	0.09	0.04	0.05	.	119.5	.	
08/02/2014 23:45	0.10	0.04	0.06	.	119.75	.	
09/02/2014 00 00	0.09	0.04	0.05	.	120	.	
09/02/2014 00:15	0.10	0.04	0.06	.	120.25	.	
09/02/2014 00:30	0.10	0.04	0.06	.	120.5	.	
09/02/2014 00:45	0.09	0.04	0.05	.	120.75	.	
09/02/2014 01 00	0.08	0.04	0.04	.	121	.	
09/02/2014 01:15	0.09	0.04	0.05	.	121.25	.	
09/02/2014 01:30	0.09	0.04	0.05	.	121.5	.	
09/02/2014 01:45	0.09	0.04	0.05	.	121.75	.	
09/02/2014 02 00	0.09	0.04	0.05	.	122	.	
09/02/2014 02:15	0.10	0.04	0.06	.	122.25	.	
09/02/2014 02:30	0.09	0.04	0.05	.	122.5	.	
09/02/2014 02:45	0.11	0.04	0.07	.	122.75	.	
09/02/2014 03 00	0.11	0.04	0.07	.	123	.	
09/02/2014 03:15	0.09	0.04	0.05	.	123.25	.	
09/02/2014 03:30	0.07	0.04	0.03	.	123.5	.	
09/02/2014 03:45	0.07	0.04	0.03	.	123.75	.	
09/02/2014 04 00	0.07	0.04	0.03	.	124	.	
09/02/2014 04:15	0.07	0.04	0.03	.	124.25	.	
09/02/2014 04:30	0.06	0.04	0.02	.	124.5	.	
09/02/2014 04:45	0.06	0.04	0.02	.	124.75	.	
09/02/2014 05 00	0.07	0.04	0.03	.	125	.	
09/02/2014 05:15	0.08	0.04	0.04	.	125.25	.	
09/02/2014 05:30	0.06	0.04	0.02	.	125.5	.	
09/02/2014 05:45	0.06	0.04	0.02	.	125.75	.	
09/02/2014 06 00	0.06	0.04	0.02	.	126	.	
09/02/2014 06:15	0.05	0.04	0.01	.	126.25	.	
09/02/2014 06:30	0.05	0.04	0.01	.	126.5	.	
09/02/2014 06:45	0.06	0.04	0.02	.	126.75	.	
09/02/2014 07 00	0.07	0.04	0.03	.	127	0.2	
09/02/2014 07:15	0.05	0.04	0.01	.	127.25	.	
09/02/2014 07:30	0.04	0.04	0.00	.	127.5	.	
09/02/2014 07:45	0.07	0.04	0.03	.	127.75	.	
09/02/2014 08 00	0.06	0.04	0.02	.	128	.	
09/02/2014 08:15	0.07	0.04	0.03	.	128.25	.	
09/02/2014 08:30	0.06	0.04	0.02	.	128.5	.	
09/02/2014 08:45	0.07	0.04	0.03	.	128.75	.	
09/02/2014 09 00	0.06	0.04	0.02	.	129	.	
09/02/2014 09:15	0.06	0.04	0.02	.	129.25	.	
09/02/2014 09:30	0.05	0.04	0.01	.	129.5	.	
09/02/2014 09:45	0.05	0.04	0.01	.	129.75	.	
09/02/2014 10 00	0.07	0.04	0.03	.	130	.	
09/02/2014 10:15	0.06	0.04	0.02	.	130.25	.	
09/02/2014 10:30	0.06	0.04	0.02	.	130.5	.	
09/02/2014 10:45	0.04	0.04	0.00	.	130.75	.	
09/02/2014 11 00	0.08	0.04	0.04	.	131	.	
09/02/2014 11:15	0.05	0.04	0.01	.	131.25	.	
09/02/2014 11:30	0.07	0.04	0.03	.	131.5	.	
09/02/2014 11:45	0.04	0.04	0.00	.	131.75	.	
09/02/2014 12 00	0.09	0.04	0.05	.	132	.	
09/02/2014 12:15	0.08	0.04	0.04	.	132.25	.	
09/02/2014 12:30	0.08	0.04	0.04	.	132.5	.	
09/02/2014 12:45	0.06	0.04	0.02	.	132.75	.	
09/02/2014 13 00	0.07	0.04	0.03	.	133	.	
09/02/2014 13:15	0.07	0.04	0.03	.	133.25	.	
09/02/2014 13:30	0.05	0.04	0.01	.	133.5	.	
09/02/2014 13:45	0.04	0.04	0.00	.	133.75	.	

		G5			Thorpeness		Benhall	Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)	Total Rain = rainfall only up to start of the event
09/02/2014 14 00		0.07	0.04	0.03	.	134	.	
09/02/2014 14:15		0.06	0.04	0.02	.	134.25	.	
09/02/2014 14:30		0.05	0.04	0.01	.	134.5	.	
09/02/2014 14:45		0.06	0.04	0.02	.	134.75	.	
09/02/2014 15 00		0.08	0.04	0.04	.	135	.	
09/02/2014 15:15		0.06	0.04	0.02	.	135.25	.	
09/02/2014 15:30		0.06	0.04	0.02	.	135.5	.	
09/02/2014 15:45		0.06	0.04	0.02	.	135.75	.	
09/02/2014 16 00		0.07	0.04	0.03	.	136	.	
09/02/2014 16:15		0.05	0.04	0.01	.	136.25	.	
09/02/2014 16:30		0.06	0.04	0.02	.	136.5	.	
09/02/2014 16:45		0.05	0.04	0.01	.	136.75	.	
09/02/2014 17 00		0.06	0.04	0.02	.	137	.	
09/02/2014 17:15		0.06	0.04	0.02	.	137.25	.	
09/02/2014 17:30		0.05	0.04	0.01	.	137.5	.	
09/02/2014 17:45		0.06	0.04	0.02	.	137.75	.	
09/02/2014 18 00		0.05	0.04	0.01	.	138	.	
09/02/2014 18:15		0.05	0.04	0.01	.	138.25	.	
09/02/2014 18:30		0.04	0.04	0.00	.	138.5	.	
09/02/2014 18:45		0.07	0.04	0.03	.	138.75	.	
09/02/2014 19 00		0.06	0.04	0.02	.	139	.	
09/02/2014 19:15		0.07	0.04	0.03	.	139.25	.	
09/02/2014 19:30		0.05	0.04	0.01	.	139.5	.	
09/02/2014 19:45		0.06	0.04	0.02	.	139.75	.	
09/02/2014 20 00		0.05	0.04	0.01	.	140	.	
09/02/2014 20:15		0.05	0.04	0.01	.	140.25	.	
09/02/2014 20:30		0.06	0.04	0.02	.	140.5	.	
09/02/2014 20:45		0.04	0.04	0.00	.	140.75	.	
09/02/2014 21 00		0.05	0.04	0.01	.	141	.	
09/02/2014 21:15		0.05	0.04	0.01	.	141.25	.	
09/02/2014 21:30		0.05	0.04	0.01	.	141.5	.	
09/02/2014 21:45		0.06	0.04	0.02	.	141.75	.	
09/02/2014 22 00		0.07	0.04	0.03	.	142	.	
09/02/2014 22:15		0.05	0.04	0.01	.	142.25	.	
09/02/2014 22:30		0.06	0.04	0.02	.	142.5	.	
09/02/2014 22:45		0.06	0.04	0.02	.	142.75	.	
09/02/2014 23 00		0.06	0.04	0.02	.	143	.	
09/02/2014 23:15		0.05	0.04	0.01	.	143.25	.	
09/02/2014 23:30		0.05	0.04	0.01	.	143.5	.	
09/02/2014 23:45		0.04	0.04	0.00	.	143.75	.	
10/02/2014 00 00		0.06	0.04	0.02	.	144	.	
10/02/2014 00:15		0.05	0.04	0.01	.	144.25	.	
10/02/2014 00:30		0.05	0.04	0.01	.	144.5	.	
10/02/2014 00:45		0.06	0.04	0.02	.	144.75	.	
10/02/2014 01 00		0.05	0.04	0.01	.	145	.	
10/02/2014 01:15		0.05	0.04	0.01	.	145.25	.	
10/02/2014 01:30		0.05	0.04	0.01	.	145.5	.	
10/02/2014 01:45		0.06	0.04	0.02	.	145.75	.	
10/02/2014 02 00		0.05	0.04	0.01	.	146	.	
10/02/2014 02:15		0.05	0.04	0.01	.	146.25	.	
10/02/2014 02:30		0.04	0.04	0.00	.	146.5	.	
10/02/2014 02:45		0.05	0.04	0.01	0.2	146.75	.	
10/02/2014 03 00		0.05	0.04	0.01	.	147	.	
10/02/2014 03:15		0.05	0.04	0.01	.	147.25	.	
10/02/2014 03:30		0.05	0.04	0.01	.	147.5	0.2	
10/02/2014 03:45		0.05	0.04	0.01	.	147.75	.	
10/02/2014 04 00		0.05	0.04	0.01	.	148	.	
10/02/2014 04:15		0.04	0.04	0.00	.	148.25	.	
10/02/2014 04:30		0.05	0.04	0.01	.	148.5	.	
10/02/2014 04:45		0.04	0.04	0.00	.	148.75	.	
10/02/2014 05 00		0.04	0.04	0.00	.	149	.	
10/02/2014 05:15		0.04	0.04	0.00	.	149.25	.	
10/02/2014 05:30		0.04	0.04	0.00	.	149.5	.	
10/02/2014 05:45		0.04	0.04	0.00	.	149.75	.	
10/02/2014 06 00		0.05	0.04	0.01	.	150	.	


July 2014 Event
1.20
1.00
0.80
0.60
0.40
0.20
0.00
Flow (m³/s)
7
6
5
4
3
2
1
0
Rainfall (mm)
0
50
100
150
200
Time (hours)
Flow
Baseflow
Rainfall - Thorpeness
Rainfall - Benhall

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
07/07/2014 08:45	0.04	0.03	0.01	.	0	.
07/07/2014 09 00	0.03	0.03	0.00	.	0.25	.
07/07/2014 09:15	0.04	0.03	0.01	.	0.5	.
07/07/2014 09:30	0.03	0.03	0.00	.	0.75	.
07/07/2014 09:45	0.03	0.03	0.00	.	1	.
07/07/2014 10 00	0.03	0.03	0.00	.	1.25	.
07/07/2014 10:15	0.04	0.03	0.01	.	1.5	.
07/07/2014 10:30	0.05	0.03	0.02	.	1.75	.
07/07/2014 10:45	0.06	0.03	0.03	.	2	.
07/07/2014 11 00	0.05	0.03	0.02	.	2.25	.
07/07/2014 11:15	0.04	0.03	0.01	.	2.5	.
07/07/2014 11:30	0.05	0.03	0.02	.	2.75	.
07/07/2014 11:45	0.03	0.03	0.00	.	3	.
07/07/2014 12 00	0.03	0.03	0.00	.	3.25	.
07/07/2014 12:15	0.03	0.03	0.00	.	3.5	.
07/07/2014 12:30	0.04	0.03	0.01	.	3.75	.
07/07/2014 12:45	0.03	0.03	0.00	.	4	.
07/07/2014 13 00	0.03	0.03	0.00	.	4.25	.
07/07/2014 13:15	0.04	0.03	0.01	.	4.5	.
07/07/2014 13:30	0.03	0.03	0.00	.	4.75	.
07/07/2014 13:45	0.03	0.03	0.00	.	5	.
07/07/2014 14 00	0.04	0.03	0.01	.	5.25	.
07/07/2014 14:15	0.03	0.03	0.00	.	5.5	.
07/07/2014 14:30	0.04	0.03	0.01	.	5.75	.
07/07/2014 14:45	0.03	0.03	0.00	.	6	.
07/07/2014 15 00	0.04	0.03	0.01	.	6.25	.
07/07/2014 15:15	0.02	0.02	0.00	.	6.5	.
07/07/2014 15:30	0.03	0.03	0.00	.	6.75	.
07/07/2014 15:45	0.03	0.03	0.00	.	7	.
07/07/2014 16 00	0.03	0.03	0.00	.	7.25	.
07/07/2014 16:15	0.03	0.03	0.00	.	7.5	.
07/07/2014 16:30	0.03	0.03	0.00	.	7.75	.
07/07/2014 16:45	0.03	0.03	0.00	.	8	.
07/07/2014 17 00	0.03	0.03	0.00	.	8.25	.
07/07/2014 17:15	0.03	0.03	0.00	.	8.5	.
07/07/2014 17:30	0.03	0.03	0.00	.	8.75	.
07/07/2014 17:45	0.03	0.03	0.00	.	9	.
07/07/2014 18 00	0.02	0.02	0.00	.	9.25	.
07/07/2014 18:15	0.03	0.03	0.00	.	9.5	.
07/07/2014 18:30	0.03	0.03	0.00	.	9.75	.
07/07/2014 18:45	0.03	0.03	0.00	.	10	.
07/07/2014 19 00	0.03	0.03	0.00	.	10.25	.
07/07/2014 19:15	0.03	0.03	0.00	.	10.5	.
07/07/2014 19:30	0.03	0.03	0.00	.	10.75	.
07/07/2014 19:45	0.03	0.03	0.00	.	11	.
07/07/2014 20 00	0.03	0.03	0.00	.	11.25	.
07/07/2014 20:15	0.03	0.03	0.00	.	11.5	.
07/07/2014 20:30	0.03	0.03	0.00	.	11.75	.
07/07/2014 20:45	0.03	0.03	0.00	.	12	.
07/07/2014 21 00	0.02	0.02	0.00	.	12.25	.
07/07/2014 21:15	0.03	0.03	0.00	.	12.5	.
07/07/2014 21:30	0.03	0.03	0.00	.	12.75	.
07/07/2014 21:45	0.03	0.03	0.00	.	13	.
07/07/2014 22 00	0.03	0.03	0.00	.	13.25	.
07/07/2014 22:15	0.03	0.03	0.00	.	13.5	.
07/07/2014 22:30	0.03	0.03	0.00	.	13.75	.
07/07/2014 22:45	0.03	0.03	0.00	.	14	.
07/07/2014 23 00	0.03	0.03	0.00	.	14.25	.
07/07/2014 23:15	0.03	0.03	0.00	.	14.5	.
07/07/2014 23:30	0.03	0.03	0.00	.	14.75	.
07/07/2014 23:45	0.03	0.03	0.00	.	15	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Thorpeness	
Area (km^2)	5.04
Total Rain (P) mm	42.4
Time Interval (hour)	0.25
Percentage Runoff	13%

Benhall	
Area (km^2)	5.04
Total Rain (P) mm	29.2
Time Interval (hour)	0.25
Percentage Runoff	19%

Average PR	16%

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/07/2014 00 00	0.04	0.03	0.01	.	15.25	.
08/07/2014 00:15	0.04	0.03	0.01	.	15.5	.
08/07/2014 00:30	0.04	0.03	0.01	.	15.75	.
08/07/2014 00:45	0.03	0.03	0.00	.	16	.
08/07/2014 01 00	0.03	0.03	0.00	.	16.25	.
08/07/2014 01:15	0.03	0.03	0.00	.	16.5	.
08/07/2014 01:30	0.03	0.03	0.00	.	16.75	.
08/07/2014 01:45	0.02	0.02	0.00	.	17	.
08/07/2014 02 00	0.03	0.03	0.00	.	17.25	.
08/07/2014 02:15	0.03	0.03	0.00	.	17.5	.
08/07/2014 02:30	0.02	0.02	0.00	.	17.75	.
08/07/2014 02:45	0.03	0.03	0.00	.	18	.
08/07/2014 03 00	0.03	0.03	0.00	.	18.25	.
08/07/2014 03:15	0.02	0.02	0.00	.	18.5	.
08/07/2014 03:30	0.03	0.03	0.00	.	18.75	.
08/07/2014 03:45	0.02	0.02	0.00	.	19	.
08/07/2014 04 00	0.02	0.02	0.00	.	19.25	.
08/07/2014 04:15	0.03	0.03	0.00	.	19.5	.
08/07/2014 04:30	0.02	0.02	0.00	.	19.75	.
08/07/2014 04:45	0.03	0.03	0.00	.	20	.
08/07/2014 05 00	0.02	0.02	0.00	.	20.25	.
08/07/2014 05:15	0.02	0.02	0.00	.	20.5	.
08/07/2014 05:30	0.02	0.02	0.00	.	20.75	.
08/07/2014 05:45	0.02	0.02	0.00	.	21	.
08/07/2014 06 00	0.02	0.02	0.00	.	21.25	.
08/07/2014 06:15	0.02	0.02	0.00	.	21.5	.
08/07/2014 06:30	0.02	0.02	0.00	.	21.75	.
08/07/2014 06:45	0.02	0.02	0.00	.	22	.
08/07/2014 07 00	0.03	0.03	0.00	.	22.25	.
08/07/2014 07:15	0.02	0.02	0.00	.	22.5	.
08/07/2014 07:30	0.03	0.03	0.00	.	22.75	.
08/07/2014 07:45	0.03	0.03	0.00	.	23	.
08/07/2014 08 00	0.03	0.03	0.00	.	23.25	.
08/07/2014 08:15	0.03	0.03	0.00	.	23.5	.
08/07/2014 08:30	0.04	0.03	0.01	.	23.75	.
08/07/2014 08:45	0.03	0.03	0.00	.	24	.
08/07/2014 09 00	0.03	0.03	0.00	.	24.25	.
08/07/2014 09:15	0.03	0.03	0.00	.	24.5	.
08/07/2014 09:30	0.04	0.03	0.01	.	24.75	.
08/07/2014 09:45	0.03	0.03	0.00	.	25	.
08/07/2014 10 00	0.03	0.03	0.00	.	25.25	.
08/07/2014 10:15	0.03	0.03	0.00	.	25.5	.
08/07/2014 10:30	0.03	0.03	0.00	.	25.75	.
08/07/2014 10:45	0.03	0.03	0.00	.	26	.
08/07/2014 11 00	0.03	0.03	0.00	.	26.25	.
08/07/2014 11:15	0.05	0.03	0.02	.	26.5	.
08/07/2014 11:30	0.04	0.03	0.01	.	26.75	.
08/07/2014 11:45	0.03	0.03	0.00	.	27	.
08/07/2014 12 00	0.03	0.03	0.00	.	27.25	.
08/07/2014 12:15	0.04	0.03	0.01	.	27.5	.
08/07/2014 12:30	0.04	0.03	0.01	.	27.75	.
08/07/2014 12:45	0.03	0.03	0.00	.	28	.
08/07/2014 13 00	0.03	0.03	0.00	.	28.25	.
08/07/2014 13:15	0.03	0.03	0.00	.	28.5	.
08/07/2014 13:30	0.03	0.03	0.00	.	28.75	1.2
08/07/2014 13:45	0.03	0.03	0.00	.	29	0.8
08/07/2014 14 00	0.03	0.03	0.00	.	29.25	2
08/07/2014 14:15	0.03	0.03	0.00	.	29.5	0.6
08/07/2014 14:30	0.04	0.03	0.01	0.6	29.75	0.2
08/07/2014 14:45	0.05	0.03	0.02	0.2	30	.
08/07/2014 15 00	0.04	0.03	0.01	.	30.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/07/2014 15:15	0.05	0.03	0.02	.	30.5	.
08/07/2014 15:30	0.04	0.03	0.01	.	30.75	0.2
08/07/2014 15:45	0.05	0.03	0.02	.	31	1.2
08/07/2014 16 00	0.04	0.03	0.01	.	31.25	2
08/07/2014 16:15	0.05	0.03	0.02	0.2	31.5	0.2
08/07/2014 16:30	0.04	0.03	0.01	.	31.75	.
08/07/2014 16:45	0.04	0.03	0.01	.	32	.
08/07/2014 17 00	0.04	0.03	0.01	.	32.25	.
08/07/2014 17:15	0.03	0.03	0.00	.	32.5	.
08/07/2014 17:30	0.03	0.03	0.00	.	32.75	.
08/07/2014 17:45	0.03	0.03	0.00	.	33	.
08/07/2014 18 00	0.03	0.03	0.00	.	33.25	.
08/07/2014 18:15	0.05	0.03	0.02	.	33.5	.
08/07/2014 18:30	0.03	0.03	0.00	.	33.75	.
08/07/2014 18:45	0.04	0.03	0.01	.	34	.
08/07/2014 19 00	0.03	0.03	0.00	.	34.25	.
08/07/2014 19:15	0.04	0.03	0.01	.	34.5	.
08/07/2014 19:30	0.02	0.02	0.00	.	34.75	.
08/07/2014 19:45	0.04	0.03	0.01	0.2	35	.
08/07/2014 20 00	0.03	0.03	0.00	.	35.25	.
08/07/2014 20:15	0.03	0.03	0.00	.	35.5	.
08/07/2014 20:30	0.04	0.03	0.01	.	35.75	.
08/07/2014 20:45	0.03	0.03	0.00	0.2	36	.
08/07/2014 21 00	0.03	0.03	0.00	0.2	36.25	.
08/07/2014 21:15	0.04	0.03	0.01	.	36.5	.
08/07/2014 21:30	0.04	0.03	0.01	.	36.75	.
08/07/2014 21:45	0.03	0.03	0.00	.	37	.
08/07/2014 22 00	0.03	0.03	0.00	.	37.25	.
08/07/2014 22:15	0.03	0.03	0.00	.	37.5	.
08/07/2014 22:30	0.04	0.03	0.01	.	37.75	.
08/07/2014 22:45	0.03	0.03	0.00	.	38	.
08/07/2014 23 00	0.03	0.03	0.00	.	38.25	.
08/07/2014 23:15	0.03	0.03	0.00	.	38.5	.
08/07/2014 23:30	0.03	0.03	0.00	.	38.75	.
08/07/2014 23:45	0.03	0.03	0.00	.	39	.
09/07/2014 00 00	0.04	0.03	0.01	.	39.25	.
09/07/2014 00:15	0.04	0.03	0.01	.	39.5	.
09/07/2014 00:30	0.03	0.03	0.00	.	39.75	.
09/07/2014 00:45	0.04	0.03	0.01	.	40	.
09/07/2014 01 00	0.03	0.03	0.00	.	40.25	.
09/07/2014 01:15	0.03	0.03	0.00	.	40.5	.
09/07/2014 01:30	0.04	0.03	0.01	.	40.75	.
09/07/2014 01:45	0.03	0.03	0.00	.	41	.
09/07/2014 02 00	0.03	0.03	0.00	.	41.25	.
09/07/2014 02:15	0.03	0.03	0.00	.	41.5	.
09/07/2014 02:30	0.03	0.03	0.00	.	41.75	.
09/07/2014 02:45	0.02	0.02	0.00	.	42	.
09/07/2014 03 00	0.02	0.02	0.00	0.2	42.25	.
09/07/2014 03:15	0.03	0.03	0.00	.	42.5	.
09/07/2014 03:30	0.03	0.03	0.00	.	42.75	.
09/07/2014 03:45	0.03	0.03	0.00	.	43	.
09/07/2014 04 00	0.03	0.03	0.00	.	43.25	.
09/07/2014 04:15	0.03	0.03	0.00	.	43.5	.
09/07/2014 04:30	0.03	0.03	0.00	.	43.75	.
09/07/2014 04:45	0.02	0.02	0.00	.	44	.
09/07/2014 05 00	0.02	0.02	0.00	.	44.25	.
09/07/2014 05:15	0.02	0.02	0.00	.	44.5	.
09/07/2014 05:30	0.02	0.02	0.00	.	44.75	.
09/07/2014 05:45	0.02	0.02	0.00	.	45	.
09/07/2014 06 00	0.02	0.02	0.00	.	45.25	.
09/07/2014 06:15	0.02	0.02	0.00	.	45.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

		G5		Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
09/07/2014 06:30	0.04	0.03	0.01	.	45.75	.
09/07/2014 06:45	0.02	0.02	0.00	.	46	.
09/07/2014 07 00	0.02	0.02	0.00	.	46.25	.
09/07/2014 07:15	0.02	0.02	0.00	.	46.5	.
09/07/2014 07:30	0.03	0.03	0.00	.	46.75	.
09/07/2014 07:45	0.04	0.03	0.01	.	47	.
09/07/2014 08 00	0.04	0.03	0.01	.	47.25	.
09/07/2014 08:15	0.04	0.03	0.01	.	47.5	.
09/07/2014 08:30	0.03	0.03	0.00	.	47.75	.
09/07/2014 08:45	0.04	0.03	0.01	.	48	.
09/07/2014 09 00	0.03	0.03	0.00	.	48.25	.
09/07/2014 09:15	0.05	0.03	0.02	.	48.5	.
09/07/2014 09:30	0.03	0.03	0.00	.	48.75	.
09/07/2014 09:45	0.04	0.03	0.01	.	49	.
09/07/2014 10 00	0.03	0.03	0.00	.	49.25	.
09/07/2014 10:15	0.04	0.03	0.01	.	49.5	.
09/07/2014 10:30	0.05	0.03	0.02	.	49.75	.
09/07/2014 10:45	0.04	0.03	0.01	.	50	.
09/07/2014 11 00	0.04	0.03	0.01	.	50.25	.
09/07/2014 11:15	0.04	0.03	0.01	.	50.5	.
09/07/2014 11:30	0.04	0.03	0.01	.	50.75	.
09/07/2014 11:45	0.03	0.03	0.00	.	51	.
09/07/2014 12 00	0.04	0.03	0.01	.	51.25	.
09/07/2014 12:15	0.03	0.03	0.00	.	51.5	.
09/07/2014 12:30	0.03	0.03	0.00	.	51.75	.
09/07/2014 12:45	0.03	0.03	0.00	.	52	.
09/07/2014 13 00	0.03	0.03	0.00	.	52.25	.
09/07/2014 13:15	0.03	0.03	0.00	.	52.5	.
09/07/2014 13:30	0.04	0.03	0.01	.	52.75	.
09/07/2014 13:45	0.03	0.03	0.00	.	53	.
09/07/2014 14 00	0.03	0.03	0.00	.	53.25	.
09/07/2014 14:15	0.03	0.03	0.00	.	53.5	.
09/07/2014 14:30	0.03	0.03	0.00	.	53.75	.
09/07/2014 14:45	0.04	0.03	0.01	.	54	.
09/07/2014 15 00	0.03	0.03	0.00	.	54.25	.
09/07/2014 15:15	0.04	0.03	0.01	.	54.5	.
09/07/2014 15:30	0.04	0.03	0.01	.	54.75	.
09/07/2014 15:45	0.04	0.03	0.01	.	55	.
09/07/2014 16 00	0.03	0.03	0.00	.	55.25	.
09/07/2014 16:15	0.03	0.03	0.00	.	55.5	.
09/07/2014 16:30	0.03	0.03	0.00	.	55.75	.
09/07/2014 16:45	0.03	0.03	0.00	.	56	.
09/07/2014 17 00	0.03	0.03	0.00	.	56.25	.
09/07/2014 17:15	0.02	0.02	0.00	.	56.5	.
09/07/2014 17:30	0.03	0.03	0.00	.	56.75	.
09/07/2014 17:45	0.03	0.03	0.00	.	57	.
09/07/2014 18 00	0.02	0.02	0.00	.	57.25	.
09/07/2014 18:15	0.03	0.03	0.00	.	57.5	.
09/07/2014 18:30	0.03	0.03	0.00	.	57.75	.
09/07/2014 18:45	0.03	0.03	0.00	.	58	.
09/07/2014 19 00	0.03	0.03	0.00	.	58.25	.
09/07/2014 19:15	0.04	0.03	0.01	.	58.5	.
09/07/2014 19:30	0.04	0.03	0.01	.	58.75	.
09/07/2014 19:45	0.03	0.03	0.00	0.2	59	.
09/07/2014 20 00	0.02	0.02	0.00	.	59.25	.
09/07/2014 20:15	0.03	0.03	0.00	.	59.5	.
09/07/2014 20:30	0.04	0.03	0.01	.	59.75	.
09/07/2014 20:45	0.03	0.03	0.00	.	60	.
09/07/2014 21 00	0.04	0.03	0.01	.	60.25	.
09/07/2014 21:15	0.03	0.03	0.00	.	60.5	.
09/07/2014 21:30	0.03	0.03	0.00	.	60.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
09/07/2014 21:45	0.03	0.03	0.00	.	61	.
09/07/2014 22 00	0.04	0.03	0.01	.	61.25	.
09/07/2014 22:15	0.03	0.03	0.00	.	61.5	.
09/07/2014 22:30	0.03	0.03	0.00	.	61.75	.
09/07/2014 22:45	0.03	0.03	0.00	.	62	.
09/07/2014 23 00	0.03	0.03	0.00	.	62.25	.
09/07/2014 23:15	0.04	0.03	0.01	.	62.5	.
09/07/2014 23:30	0.03	0.03	0.00	.	62.75	.
09/07/2014 23:45	0.03	0.03	0.00	.	63	.
10/07/2014 00 00	0.03	0.03	0.00	.	63.25	.
10/07/2014 00:15	0.04	0.03	0.01	.	63.5	.
10/07/2014 00:30	0.04	0.03	0.01	.	63.75	.
10/07/2014 00:45	0.03	0.03	0.00	.	64	.
10/07/2014 01 00	0.03	0.03	0.00	.	64.25	.
10/07/2014 01:15	0.04	0.03	0.01	.	64.5	.
10/07/2014 01:30	0.03	0.03	0.00	.	64.75	.
10/07/2014 01:45	0.05	0.03	0.02	.	65	.
10/07/2014 02 00	0.03	0.03	0.00	0.2	65.25	.
10/07/2014 02:15	0.03	0.03	0.00	.	65.5	.
10/07/2014 02:30	0.03	0.03	0.00	.	65.75	.
10/07/2014 02:45	0.03	0.03	0.00	.	66	.
10/07/2014 03 00	0.03	0.03	0.00	.	66.25	.
10/07/2014 03:15	0.03	0.03	0.00	.	66.5	.
10/07/2014 03:30	0.02	0.02	0.00	.	66.75	.
10/07/2014 03:45	0.03	0.03	0.00	.	67	.
10/07/2014 04 00	0.02	0.02	0.00	.	67.25	.
10/07/2014 04:15	0.03	0.03	0.00	.	67.5	.
10/07/2014 04:30	0.02	0.02	0.00	.	67.75	.
10/07/2014 04:45	0.02	0.02	0.00	.	68	.
10/07/2014 05 00	0.02	0.02	0.00	.	68.25	.
10/07/2014 05:15	0.02	0.02	0.00	.	68.5	.
10/07/2014 05:30	0.03	0.03	0.00	.	68.75	.
10/07/2014 05:45	0.02	0.02	0.00	.	69	.
10/07/2014 06 00	0.02	0.02	0.00	.	69.25	.
10/07/2014 06:15	0.02	0.02	0.00	.	69.5	.
10/07/2014 06:30	0.02	0.02	0.00	.	69.75	.
10/07/2014 06:45	0.02	0.02	0.00	.	70	.
10/07/2014 07 00	0.03	0.03	0.00	.	70.25	.
10/07/2014 07:15	0.02	0.02	0.00	.	70.5	.
10/07/2014 07:30	0.02	0.02	0.00	.	70.75	.
10/07/2014 07:45	0.03	0.03	0.00	.	71	.
10/07/2014 08 00	0.03	0.03	0.00	.	71.25	.
10/07/2014 08:15	0.03	0.03	0.00	.	71.5	.
10/07/2014 08:30	0.03	0.03	0.00	.	71.75	.
10/07/2014 08:45	0.03	0.03	0.00	.	72	.
10/07/2014 09 00	0.03	0.03	0.00	.	72.25	.
10/07/2014 09:15	0.03	0.03	0.00	.	72.5	.
10/07/2014 09:30	0.03	0.03	0.00	.	72.75	.
10/07/2014 09:45	0.03	0.03	0.00	.	73	.
10/07/2014 10 00	0.04	0.03	0.01	.	73.25	.
10/07/2014 10:15	0.03	0.03	0.00	.	73.5	.
10/07/2014 10:30	0.04	0.03	0.01	.	73.75	.
10/07/2014 10:45	0.04	0.03	0.01	.	74	.
10/07/2014 11 00	0.04	0.03	0.01	.	74.25	.
10/07/2014 11:15	0.04	0.03	0.01	.	74.5	.
10/07/2014 11:30	0.03	0.03	0.00	.	74.75	.
10/07/2014 11:45	0.03	0.03	0.00	.	75	.
10/07/2014 12 00	0.03	0.03	0.00	.	75.25	.
10/07/2014 12:15	0.03	0.03	0.00	.	75.5	.
10/07/2014 12:30	0.03	0.03	0.00	.	75.75	.
10/07/2014 12:45	0.03	0.03	0.00	.	76	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
10/07/2014 13 00	0.03	0.03	0.00	.	76.25	.
10/07/2014 13:15	0.03	0.03	0.00	.	76.5	.
10/07/2014 13:30	0.04	0.03	0.01	.	76.75	.
10/07/2014 13:45	0.03	0.03	0.00	.	77	.
10/07/2014 14 00	0.02	0.02	0.00	.	77.25	.
10/07/2014 14:15	0.03	0.03	0.00	.	77.5	.
10/07/2014 14:30	0.03	0.03	0.00	.	77.75	.
10/07/2014 14:45	0.02	0.02	0.00	.	78	.
10/07/2014 15 00	0.02	0.02	0.00	.	78.25	.
10/07/2014 15:15	0.03	0.03	0.00	.	78.5	.
10/07/2014 15:30	0.02	0.02	0.00	.	78.75	.
10/07/2014 15:45	0.03	0.03	0.00	.	79	.
10/07/2014 16 00	0.02	0.02	0.00	.	79.25	.
10/07/2014 16:15	0.03	0.03	0.00	.	79.5	.
10/07/2014 16:30	0.04	0.03	0.01	.	79.75	.
10/07/2014 16:45	0.02	0.02	0.00	.	80	.
10/07/2014 17 00	0.04	0.03	0.01	.	80.25	.
10/07/2014 17:15	0.03	0.03	0.00	.	80.5	.
10/07/2014 17:30	0.02	0.02	0.00	.	80.75	.
10/07/2014 17:45	0.03	0.03	0.00	.	81	.
10/07/2014 18 00	0.03	0.03	0.00	.	81.25	.
10/07/2014 18:15	0.03	0.03	0.00	.	81.5	.
10/07/2014 18:30	0.03	0.03	0.00	.	81.75	.
10/07/2014 18:45	0.03	0.03	0.00	.	82	.
10/07/2014 19 00	0.03	0.03	0.00	.	82.25	.
10/07/2014 19:15	0.03	0.03	0.00	.	82.5	.
10/07/2014 19:30	0.03	0.03	0.00	.	82.75	.
10/07/2014 19:45	0.03	0.03	0.00	.	83	.
10/07/2014 20 00	0.03	0.03	0.00	0.2	83.25	.
10/07/2014 20:15	0.03	0.03	0.00	3.2	83.5	0.2
10/07/2014 20:30	0.03	0.03	0.00	1.6	83.75	0.2
10/07/2014 20:45	0.03	0.03	0.00	0.8	84	1
10/07/2014 21 00	0.03	0.03	0.00	0.6	84.25	0.6
10/07/2014 21:15	0.04	0.03	0.01	0.6	84.5	.
10/07/2014 21:30	0.06	0.03	0.03	0.8	84.75	0.2
10/07/2014 21:45	0.10	0.03	0.07	0.2	85	0.2
10/07/2014 22 00	0.11	0.03	0.08	0.2	85.25	0.4
10/07/2014 22:15	0.11	0.03	0.08	0.2	85.5	0.4
10/07/2014 22:30	0.11	0.03	0.08	.	85.75	0.2
10/07/2014 22:45	0.12	0.03	0.09	0.2	86	0.4
10/07/2014 23 00	0.11	0.03	0.08	.	86.25	0.2
10/07/2014 23:15	0.10	0.03	0.07	.	86.5	0.2
10/07/2014 23:30	0.10	0.03	0.07	.	86.75	.
10/07/2014 23:45	0.10	0.03	0.07	.	87	.
11/07/2014 00 00	0.11	0.03	0.08	0.2	87.25	.
11/07/2014 00:15	0.11	0.03	0.08	.	87.5	.
11/07/2014 00:30	0.11	0.03	0.08	0.2	87.75	.
11/07/2014 00:45	0.11	0.03	0.08	.	88	0.2
11/07/2014 01 00	0.10	0.03	0.07	.	88.25	.
11/07/2014 01:15	0.10	0.03	0.07	.	88.5	.
11/07/2014 01:30	0.09	0.03	0.06	.	88.75	.
11/07/2014 01:45	0.08	0.03	0.05	.	89	.
11/07/2014 02 00	0.08	0.03	0.05	.	89.25	.
11/07/2014 02:15	0.07	0.03	0.04	.	89.5	.
11/07/2014 02:30	0.07	0.03	0.04	.	89.75	.
11/07/2014 02:45	0.06	0.03	0.03	.	90	.
11/07/2014 03 00	0.08	0.03	0.05	.	90.25	.
11/07/2014 03:15	0.05	0.03	0.02	.	90.5	.
11/07/2014 03:30	0.05	0.03	0.02	.	90.75	.
11/07/2014 03:45	0.08	0.03	0.05	.	91	.
11/07/2014 04 00	0.05	0.03	0.02	.	91.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

		G5		Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
11/07/2014 04:15	0.04	0.03	0.01	.	91.5	.
11/07/2014 04:30	0.05	0.03	0.02	.	91.75	.
11/07/2014 04:45	0.05	0.03	0.02	.	92	.
11/07/2014 05 00	0.05	0.03	0.02	0.2	92.25	.
11/07/2014 05:15	0.05	0.03	0.02	.	92.5	0.2
11/07/2014 05:30	0.05	0.03	0.02	.	92.75	3.4
11/07/2014 05:45	0.06	0.03	0.03	.	93	0.2
11/07/2014 06 00	0.05	0.03	0.02	.	93.25	.
11/07/2014 06:15	0.05	0.03	0.02	.	93.5	.
11/07/2014 06:30	0.07	0.03	0.04	.	93.75	.
11/07/2014 06:45	0.06	0.03	0.03	.	94	.
11/07/2014 07 00	0.06	0.03	0.03	.	94.25	.
11/07/2014 07:15	0.06	0.03	0.03	.	94.5	.
11/07/2014 07:30	0.09	0.03	0.06	.	94.75	.
11/07/2014 07:45	0.06	0.03	0.03	.	95	.
11/07/2014 08 00	0.05	0.03	0.02	.	95.25	.
11/07/2014 08:15	0.05	0.03	0.02	.	95.5	.
11/07/2014 08:30	0.06	0.03	0.03	.	95.75	.
11/07/2014 08:45	0.06	0.03	0.03	.	96	.
11/07/2014 09 00	0.07	0.03	0.04	.	96.25	.
11/07/2014 09:15	0.06	0.03	0.03	.	96.5	.
11/07/2014 09:30	0.05	0.03	0.02	.	96.75	.
11/07/2014 09:45	0.06	0.03	0.03	.	97	.
11/07/2014 10 00	0.06	0.03	0.03	.	97.25	.
11/07/2014 10:15	0.05	0.03	0.02	.	97.5	.
11/07/2014 10:30	0.06	0.03	0.03	.	97.75	.
11/07/2014 10:45	0.05	0.03	0.02	.	98	.
11/07/2014 11 00	0.06	0.03	0.03	0.2	98.25	.
11/07/2014 11:15	0.05	0.03	0.02	.	98.5	.
11/07/2014 11:30	0.06	0.03	0.03	.	98.75	.
11/07/2014 11:45	0.06	0.03	0.03	.	99	.
11/07/2014 12 00	0.05	0.03	0.02	.	99.25	.
11/07/2014 12:15	0.08	0.03	0.05	.	99.5	.
11/07/2014 12:30	0.05	0.03	0.02	.	99.75	.
11/07/2014 12:45	0.04	0.03	0.01	.	100	.
11/07/2014 13 00	0.02	0.02	0.00	.	100.25	.
11/07/2014 13:15	0.04	0.03	0.01	.	100.5	.
11/07/2014 13:30	0.03	0.03	0.00	.	100.75	.
11/07/2014 13:45	0.04	0.03	0.01	.	101	.
11/07/2014 14 00	0.03	0.03	0.00	.	101.25	.
11/07/2014 14:15	0.05	0.03	0.02	.	101.5	.
11/07/2014 14:30	0.03	0.03	0.00	.	101.75	.
11/07/2014 14:45	0.03	0.03	0.00	.	102	.
11/07/2014 15 00	0.03	0.03	0.00	.	102.25	.
11/07/2014 15:15	0.03	0.03	0.00	.	102.5	.
11/07/2014 15:30	0.04	0.03	0.01	.	102.75	.
11/07/2014 15:45	0.03	0.03	0.00	.	103	.
11/07/2014 16 00	0.03	0.03	0.00	.	103.25	.
11/07/2014 16:15	0.03	0.03	0.00	.	103.5	.
11/07/2014 16:30	0.03	0.03	0.00	.	103.75	.
11/07/2014 16:45	0.03	0.03	0.00	.	104	.
11/07/2014 17 00	0.04	0.03	0.01	.	104.25	.
11/07/2014 17:15	0.03	0.03	0.00	.	104.5	.
11/07/2014 17:30	0.04	0.03	0.01	.	104.75	.
11/07/2014 17:45	0.04	0.03	0.01	.	105	.
11/07/2014 18 00	0.04	0.03	0.01	.	105.25	.
11/07/2014 18:15	0.03	0.03	0.00	.	105.5	.
11/07/2014 18:30	0.04	0.03	0.01	.	105.75	.
11/07/2014 18:45	0.03	0.03	0.00	.	106	.
11/07/2014 19 00	0.04	0.03	0.01	.	106.25	.
11/07/2014 19:15	0.04	0.03	0.01	.	106.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
11/07/2014 19:30	0.03	0.03	0.00	.	106.75	.
11/07/2014 19:45	0.03	0.03	0.00	.	107	.
11/07/2014 20 00	0.05	0.03	0.02	.	107.25	.
11/07/2014 20:15	0.03	0.03	0.00	.	107.5	.
11/07/2014 20:30	0.03	0.03	0.00	0.2	107.75	.
11/07/2014 20:45	0.03	0.03	0.00	.	108	.
11/07/2014 21 00	0.04	0.03	0.01	.	108.25	.
11/07/2014 21:15	0.04	0.03	0.01	.	108.5	.
11/07/2014 21:30	0.03	0.03	0.00	.	108.75	.
11/07/2014 21:45	0.04	0.03	0.01	.	109	.
11/07/2014 22 00	0.03	0.03	0.00	.	109.25	.
11/07/2014 22:15	0.04	0.03	0.01	.	109.5	.
11/07/2014 22:30	0.03	0.03	0.00	.	109.75	.
11/07/2014 22:45	0.03	0.03	0.00	.	110	.
11/07/2014 23 00	0.04	0.03	0.01	.	110.25	.
11/07/2014 23:15	0.04	0.03	0.01	.	110.5	.
11/07/2014 23:30	0.04	0.03	0.01	.	110.75	.
11/07/2014 23:45	0.04	0.03	0.01	.	111	.
12/07/2014 00 00	0.04	0.03	0.01	.	111.25	.
12/07/2014 00:15	0.05	0.03	0.02	.	111.5	.
12/07/2014 00:30	0.04	0.03	0.01	.	111.75	.
12/07/2014 00:45	0.04	0.03	0.01	.	112	.
12/07/2014 01 00	0.04	0.03	0.01	.	112.25	.
12/07/2014 01:15	0.04	0.03	0.01	.	112.5	.
12/07/2014 01:30	0.04	0.03	0.01	.	112.75	.
12/07/2014 01:45	0.04	0.03	0.01	.	113	.
12/07/2014 02 00	0.04	0.03	0.01	.	113.25	.
12/07/2014 02:15	0.04	0.03	0.01	.	113.5	.
12/07/2014 02:30	0.03	0.03	0.00	.	113.75	.
12/07/2014 02:45	0.04	0.03	0.01	.	114	.
12/07/2014 03 00	0.04	0.03	0.01	.	114.25	.
12/07/2014 03:15	0.04	0.03	0.01	.	114.5	.
12/07/2014 03:30	0.04	0.03	0.01	.	114.75	.
12/07/2014 03:45	0.03	0.03	0.00	.	115	.
12/07/2014 04 00	0.03	0.03	0.00	.	115.25	.
12/07/2014 04:15	0.03	0.03	0.00	.	115.5	.
12/07/2014 04:30	0.03	0.03	0.00	.	115.75	.
12/07/2014 04:45	0.03	0.03	0.00	.	116	.
12/07/2014 05 00	0.04	0.03	0.01	.	116.25	.
12/07/2014 05:15	0.04	0.03	0.01	5.8	116.5	0.4
12/07/2014 05:30	0.91	0.03	0.88	0.4	116.75	1
12/07/2014 05:45	0.77	0.03	0.74	0.4	117	.
12/07/2014 06 00	0.52	0.03	0.49	0.2	117.25	0.2
12/07/2014 06:15	0.43	0.03	0.40	0.6	117.5	0.4
12/07/2014 06:30	0.36	0.03	0.33	.	117.75	0.2
12/07/2014 06:45	0.33	0.03	0.30	.	118	.
12/07/2014 07 00	0.30	0.03	0.27	.	118.25	.
12/07/2014 07:15	0.27	0.03	0.24	.	118.5	.
12/07/2014 07:30	0.25	0.03	0.22	.	118.75	.
12/07/2014 07:45	0.24	0.03	0.21	.	119	.
12/07/2014 08 00	0.23	0.03	0.20	.	119.25	.
12/07/2014 08:15	0.20	0.03	0.17	.	119.5	.
12/07/2014 08:30	0.20	0.03	0.17	.	119.75	.
12/07/2014 08:45	0.19	0.03	0.16	.	120	.
12/07/2014 09 00	0.18	0.03	0.15	.	120.25	.
12/07/2014 09:15	0.17	0.03	0.14	.	120.5	.
12/07/2014 09:30	0.17	0.03	0.14	.	120.75	.
12/07/2014 09:45	0.16	0.03	0.13	.	121	.
12/07/2014 10 00	0.16	0.03	0.13	.	121.25	.
12/07/2014 10:15	0.16	0.03	0.13	.	121.5	.
12/07/2014 10:30	0.15	0.03	0.12	.	121.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
12/07/2014 10:45	0.16	0.03	0.13	.	122	.
12/07/2014 11 00	0.15	0.03	0.12	.	122.25	.
12/07/2014 11:15	0.15	0.03	0.12	.	122.5	.
12/07/2014 11:30	0.14	0.03	0.11	.	122.75	.
12/07/2014 11:45	0.13	0.03	0.10	.	123	.
12/07/2014 12 00	0.13	0.03	0.10	.	123.25	.
12/07/2014 12:15	0.12	0.03	0.09	.	123.5	.
12/07/2014 12:30	0.12	0.03	0.09	.	123.75	.
12/07/2014 12:45	0.12	0.03	0.09	0.2	124	.
12/07/2014 13 00	0.11	0.03	0.08	.	124.25	.
12/07/2014 13:15	0.11	0.03	0.08	.	124.5	.
12/07/2014 13:30	0.10	0.03	0.07	.	124.75	.
12/07/2014 13:45	0.11	0.03	0.08	.	125	.
12/07/2014 14 00	0.10	0.03	0.07	.	125.25	.
12/07/2014 14:15	0.09	0.03	0.06	.	125.5	.
12/07/2014 14:30	0.09	0.03	0.06	.	125.75	.
12/07/2014 14:45	0.09	0.03	0.06	.	126	.
12/07/2014 15 00	0.09	0.03	0.06	.	126.25	.
12/07/2014 15:15	0.09	0.03	0.06	.	126.5	.
12/07/2014 15:30	0.10	0.03	0.07	.	126.75	.
12/07/2014 15:45	0.10	0.03	0.07	.	127	.
12/07/2014 16 00	0.09	0.03	0.06	.	127.25	.
12/07/2014 16:15	0.09	0.03	0.06	.	127.5	.
12/07/2014 16:30	0.09	0.03	0.06	.	127.75	.
12/07/2014 16:45	0.08	0.03	0.05	.	128	.
12/07/2014 17 00	0.08	0.03	0.05	.	128.25	.
12/07/2014 17:15	0.07	0.03	0.04	.	128.5	.
12/07/2014 17:30	0.07	0.03	0.04	.	128.75	.
12/07/2014 17:45	0.07	0.03	0.04	.	129	.
12/07/2014 18 00	0.08	0.03	0.05	.	129.25	.
12/07/2014 18:15	0.08	0.03	0.05	.	129.5	.
12/07/2014 18:30	0.09	0.03	0.06	.	129.75	.
12/07/2014 18:45	0.07	0.03	0.04	.	130	.
12/07/2014 19 00	0.08	0.03	0.05	.	130.25	.
12/07/2014 19:15	0.07	0.03	0.04	.	130.5	.
12/07/2014 19:30	0.08	0.03	0.05	0.4	130.75	.
12/07/2014 19:45	0.07	0.03	0.04	.	131	.
12/07/2014 20 00	0.07	0.03	0.04	.	131.25	.
12/07/2014 20:15	0.07	0.03	0.04	.	131.5	.
12/07/2014 20:30	0.08	0.03	0.05	0.2	131.75	.
12/07/2014 20:45	0.07	0.03	0.04	0.2	132	.
12/07/2014 21 00	0.07	0.03	0.04	.	132.25	.
12/07/2014 21:15	0.08	0.03	0.05	.	132.5	.
12/07/2014 21:30	0.07	0.03	0.04	.	132.75	.
12/07/2014 21:45	0.07	0.03	0.04	.	133	.
12/07/2014 22 00	0.07	0.03	0.04	.	133.25	.
12/07/2014 22:15	0.08	0.03	0.05	.	133.5	.
12/07/2014 22:30	0.07	0.03	0.04	.	133.75	.
12/07/2014 22:45	0.08	0.03	0.05	.	134	.
12/07/2014 23 00	0.08	0.03	0.05	.	134.25	.
12/07/2014 23:15	0.08	0.03	0.05	.	134.5	.
12/07/2014 23:30	0.08	0.03	0.05	.	134.75	.
12/07/2014 23:45	0.09	0.03	0.06	.	135	.
13/07/2014 00 00	0.09	0.03	0.06	.	135.25	.
13/07/2014 00:15	0.09	0.03	0.06	.	135.5	.
13/07/2014 00:30	0.08	0.03	0.05	.	135.75	.
13/07/2014 00:45	0.09	0.03	0.06	.	136	.
13/07/2014 01 00	0.09	0.03	0.06	.	136.25	.
13/07/2014 01:15	0.09	0.03	0.06	.	136.5	.
13/07/2014 01:30	0.09	0.03	0.06	.	136.75	.
13/07/2014 01:45	0.07	0.03	0.04	.	137	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
13/07/2014 02 00	0.08	0.03	0.05	.	137.25	.
13/07/2014 02:15	0.07	0.03	0.04	0.4	137.5	.
13/07/2014 02:30	0.06	0.03	0.03	0.2	137.75	.
13/07/2014 02:45	0.06	0.03	0.03	0.2	138	.
13/07/2014 03 00	0.06	0.03	0.03	.	138.25	.
13/07/2014 03:15	0.07	0.03	0.04	2.4	138.5	.
13/07/2014 03:30	0.06	0.03	0.03	0.8	138.75	.
13/07/2014 03:45	0.06	0.03	0.03	0.2	139	.
13/07/2014 04 00	0.07	0.03	0.04	.	139.25	.
13/07/2014 04:15	0.06	0.03	0.03	.	139.5	.
13/07/2014 04:30	0.06	0.03	0.03	0.2	139.75	.
13/07/2014 04:45	0.06	0.03	0.03	2.4	140	.
13/07/2014 05 00	0.07	0.03	0.04	0.2	140.25	.
13/07/2014 05:15	0.07	0.03	0.04	.	140.5	.
13/07/2014 05:30	0.09	0.03	0.06	.	140.75	.
13/07/2014 05:45	0.11	0.03	0.08	.	141	.
13/07/2014 06 00	0.11	0.03	0.08	.	141.25	.
13/07/2014 06:15	0.12	0.03	0.09	.	141.5	.
13/07/2014 06:30	0.11	0.03	0.08	.	141.75	.
13/07/2014 06:45	0.11	0.03	0.08	0.2	142	.
13/07/2014 07 00	0.10	0.03	0.07	.	142.25	0.2
13/07/2014 07:15	0.09	0.03	0.06	0.2	142.5	0.2
13/07/2014 07:30	0.09	0.03	0.06	.	142.75	0.2
13/07/2014 07:45	0.09	0.03	0.06	0.2	143	.
13/07/2014 08 00	0.09	0.03	0.06	.	143.25	.
13/07/2014 08:15	0.08	0.03	0.05	.	143.5	.
13/07/2014 08:30	0.08	0.03	0.05	.	143.75	.
13/07/2014 08:45	0.07	0.03	0.04	.	144	.
13/07/2014 09 00	0.08	0.03	0.05	.	144.25	.
13/07/2014 09:15	0.07	0.03	0.04	.	144.5	.
13/07/2014 09:30	0.08	0.03	0.05	.	144.75	.
13/07/2014 09:45	0.08	0.03	0.05	.	145	.
13/07/2014 10 00	0.09	0.03	0.06	.	145.25	.
13/07/2014 10:15	0.09	0.03	0.06	.	145.5	.
13/07/2014 10:30	0.09	0.03	0.06	.	145.75	.
13/07/2014 10:45	0.10	0.03	0.07	.	146	.
13/07/2014 11 00	0.09	0.03	0.06	.	146.25	.
13/07/2014 11:15	0.09	0.03	0.06	.	146.5	.
13/07/2014 11:30	0.07	0.03	0.04	.	146.75	.
13/07/2014 11:45	0.07	0.03	0.04	.	147	0.6
13/07/2014 12 00	0.06	0.03	0.03	0.4	147.25	.
13/07/2014 12:15	0.07	0.03	0.04	0.6	147.5	.
13/07/2014 12:30	0.06	0.03	0.03	.	147.75	.
13/07/2014 12:45	0.06	0.03	0.03	.	148	.
13/07/2014 13 00	0.06	0.03	0.03	.	148.25	.
13/07/2014 13:15	0.05	0.03	0.02	.	148.5	.
13/07/2014 13:30	0.05	0.03	0.02	.	148.75	.
13/07/2014 13:45	0.05	0.03	0.02	.	149	0.2
13/07/2014 14 00	0.06	0.03	0.03	.	149.25	.
13/07/2014 14:15	0.14	0.03	0.11	5	149.5	0.2
13/07/2014 14:30	0.96	0.03	0.93	.	149.75	.
13/07/2014 14:45	0.50	0.03	0.47	.	150	.
13/07/2014 15 00	0.40	0.03	0.37	.	150.25	.
13/07/2014 15:15	0.34	0.03	0.31	.	150.5	.
13/07/2014 15:30	0.30	0.03	0.27	.	150.75	.
13/07/2014 15:45	0.27	0.03	0.24	.	151	.
13/07/2014 16 00	0.24	0.03	0.21	.	151.25	.
13/07/2014 16:15	0.21	0.03	0.18	.	151.5	.
13/07/2014 16:30	0.20	0.03	0.17	.	151.75	.
13/07/2014 16:45	0.20	0.03	0.17	.	152	.
13/07/2014 17 00	0.18	0.03	0.15	.	152.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
13/07/2014 17:15	0.16	0.03	0.13	0.2	152.5	1.6
13/07/2014 17:30	0.15	0.03	0.12	0.4	152.75	5.2
13/07/2014 17:45	0.14	0.03	0.11	.	153	0.4
13/07/2014 18 00	0.15	0.03	0.12	2.2	153.25	1.4
13/07/2014 18:15	0.22	0.03	0.19	2.4	153.5	.
13/07/2014 18:30	0.26	0.03	0.23	2.2	153.75	0.2
13/07/2014 18:45	0.43	0.03	0.40	1	154	.
13/07/2014 19 00	0.72	0.03	0.69	.	154.25	.
13/07/2014 19:15	0.57	0.03	0.54	.	154.5	.
13/07/2014 19:30	0.43	0.03	0.40	.	154.75	.
13/07/2014 19:45	0.39	0.03	0.36	.	155	.
13/07/2014 20 00	0.34	0.03	0.31	0.2	155.25	.
13/07/2014 20:15	0.30	0.03	0.27	.	155.5	.
13/07/2014 20:30	0.27	0.03	0.24	.	155.75	.
13/07/2014 20:45	0.25	0.03	0.22	.	156	.
13/07/2014 21 00	0.23	0.03	0.20	.	156.25	.
13/07/2014 21:15	0.22	0.03	0.19	.	156.5	.
13/07/2014 21:30	0.19	0.03	0.16	.	156.75	.
13/07/2014 21:45	0.19	0.03	0.16	.	157	.
13/07/2014 22 00	0.17	0.03	0.14	.	157.25	.
13/07/2014 22:15	0.17	0.03	0.14	.	157.5	.
13/07/2014 22:30	0.15	0.03	0.12	.	157.75	.
13/07/2014 22:45	0.15	0.03	0.12	.	158	.
13/07/2014 23 00	0.15	0.03	0.12	.	158.25	.
13/07/2014 23:15	0.14	0.03	0.11	.	158.5	.
13/07/2014 23:30	0.14	0.03	0.11	.	158.75	.
13/07/2014 23:45	0.14	0.03	0.11	.	159	.
14/07/2014 00 00	0.14	0.03	0.11	.	159.25	.
14/07/2014 00:15	0.13	0.03	0.10	.	159.5	.
14/07/2014 00:30	0.13	0.03	0.10	.	159.75	.
14/07/2014 00:45	0.13	0.03	0.10	.	160	.
14/07/2014 01 00	0.13	0.03	0.10	.	160.25	.
14/07/2014 01:15	0.12	0.03	0.09	.	160.5	.
14/07/2014 01:30	0.12	0.03	0.09	.	160.75	.
14/07/2014 01:45	0.11	0.03	0.08	.	161	.
14/07/2014 02 00	0.11	0.03	0.08	.	161.25	.
14/07/2014 02:15	0.10	0.03	0.07	.	161.5	.
14/07/2014 02:30	0.10	0.03	0.07	.	161.75	.
14/07/2014 02:45	0.10	0.03	0.07	.	162	.
14/07/2014 03 00	0.09	0.03	0.06	.	162.25	.
14/07/2014 03:15	0.09	0.03	0.06	.	162.5	.
14/07/2014 03:30	0.09	0.03	0.06	.	162.75	.
14/07/2014 03:45	0.09	0.03	0.06	.	163	.
14/07/2014 04 00	0.08	0.03	0.05	0.2	163.25	.
14/07/2014 04:15	0.08	0.03	0.05	0.2	163.5	.
14/07/2014 04:30	0.08	0.03	0.05	.	163.75	.
14/07/2014 04:45	0.08	0.03	0.05	.	164	.
14/07/2014 05 00	0.07	0.03	0.04	.	164.25	.
14/07/2014 05:15	0.08	0.03	0.05	.	164.5	.
14/07/2014 05:30	0.08	0.03	0.05	.	164.75	.
14/07/2014 05:45	0.08	0.03	0.05	.	165	.
14/07/2014 06 00	0.08	0.03	0.05	.	165.25	.
14/07/2014 06:15	0.09	0.03	0.06	.	165.5	.
14/07/2014 06:30	0.09	0.03	0.06	.	165.75	.
14/07/2014 06:45	0.09	0.03	0.06	.	166	.
14/07/2014 07 00	0.09	0.03	0.06	.	166.25	.
14/07/2014 07:15	0.09	0.03	0.06	.	166.5	.
14/07/2014 07:30	0.08	0.03	0.05	.	166.75	.
14/07/2014 07:45	0.09	0.03	0.06	.	167	.
14/07/2014 08 00	0.09	0.03	0.06	.	167.25	.
14/07/2014 08:15	0.08	0.03	0.05	.	167.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
14/07/2014 08:30	0.08	0.03	0.05	.	167.75	.
14/07/2014 08:45	0.08	0.03	0.05	.	168	.
14/07/2014 09 00	0.09	0.03	0.06	.	168.25	.
14/07/2014 09:15	0.09	0.03	0.06	.	168.5	.
14/07/2014 09:30	0.09	0.03	0.06	.	168.75	.
14/07/2014 09:45	0.08	0.03	0.05	.	169	.
14/07/2014 10 00	0.10	0.03	0.07	.	169.25	.
14/07/2014 10:15	0.10	0.03	0.07	.	169.5	.
14/07/2014 10:30	0.10	0.03	0.07	.	169.75	.
14/07/2014 10:45	0.10	0.03	0.07	.	170	.
14/07/2014 11 00	0.09	0.03	0.06	.	170.25	.
14/07/2014 11:15	0.10	0.03	0.07	.	170.5	.
14/07/2014 11:30	0.10	0.03	0.07	.	170.75	.
14/07/2014 11:45	0.08	0.03	0.05	.	171	.
14/07/2014 12 00	0.08	0.03	0.05	.	171.25	.
14/07/2014 12:15	0.07	0.03	0.04	.	171.5	.
14/07/2014 12:30	0.08	0.03	0.05	.	171.75	.
14/07/2014 12:45	0.08	0.03	0.05	.	172	.
14/07/2014 13 00	0.07	0.03	0.04	.	172.25	.
14/07/2014 13:15	0.07	0.03	0.04	.	172.5	.
14/07/2014 13:30	0.06	0.03	0.03	.	172.75	.
14/07/2014 13:45	0.06	0.03	0.03	.	173	.
14/07/2014 14 00	0.07	0.03	0.04	.	173.25	.
14/07/2014 14:15	0.08	0.03	0.05	.	173.5	.
14/07/2014 14:30	0.07	0.03	0.04	.	173.75	.
14/07/2014 14:45	0.09	0.03	0.06	.	174	.
14/07/2014 15 00	0.08	0.03	0.05	.	174.25	.
14/07/2014 15:15	0.09	0.03	0.06	.	174.5	.
14/07/2014 15:30	0.06	0.03	0.03	.	174.75	.
14/07/2014 15:45	0.07	0.03	0.04	.	175	.
14/07/2014 16 00	0.06	0.03	0.03	.	175.25	.
14/07/2014 16:15	0.06	0.03	0.03	.	175.5	.
14/07/2014 16:30	0.07	0.03	0.04	.	175.75	.
14/07/2014 16:45	0.06	0.03	0.03	.	176	.
14/07/2014 17 00	0.07	0.03	0.04	.	176.25	.
14/07/2014 17:15	0.07	0.03	0.04	.	176.5	.
14/07/2014 17:30	0.07	0.03	0.04	.	176.75	.
14/07/2014 17:45	0.07	0.03	0.04	.	177	.
14/07/2014 18 00	0.06	0.03	0.03	.	177.25	.
14/07/2014 18:15	0.06	0.03	0.03	.	177.5	.
14/07/2014 18:30	0.06	0.03	0.03	.	177.75	.
14/07/2014 18:45	0.06	0.03	0.03	.	178	.
14/07/2014 19 00	0.07	0.03	0.04	.	178.25	.
14/07/2014 19:15	0.06	0.03	0.03	.	178.5	.
14/07/2014 19:30	0.06	0.03	0.03	.	178.75	.
14/07/2014 19:45	0.07	0.03	0.04	.	179	.
14/07/2014 20 00	0.07	0.03	0.04	.	179.25	.
14/07/2014 20:15	0.07	0.03	0.04	.	179.5	.
14/07/2014 20:30	0.06	0.03	0.03	.	179.75	.
14/07/2014 20:45	0.06	0.03	0.03	.	180	.
14/07/2014 21 00	0.06	0.03	0.03	.	180.25	.
14/07/2014 21:15	0.07	0.03	0.04	.	180.5	.
14/07/2014 21:30	0.07	0.03	0.04	.	180.75	.
14/07/2014 21:45	0.06	0.03	0.03	.	181	.
14/07/2014 22 00	0.06	0.03	0.03	.	181.25	.
14/07/2014 22:15	0.06	0.03	0.03	.	181.5	.
14/07/2014 22:30	0.06	0.03	0.03	.	181.75	.
14/07/2014 22:45	0.07	0.03	0.04	.	182	.
14/07/2014 23 00	0.07	0.03	0.04	.	182.25	.
14/07/2014 23:15	0.06	0.03	0.03	.	182.5	.
14/07/2014 23:30	0.07	0.03	0.04	.	182.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

		G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)
14/07/2014 23:45		0.07	0.03	0.04	.	183	.
15/07/2014 00 00		0.08	0.03	0.05	.	183.25	.
15/07/2014 00:15		0.08	0.03	0.05	.	183.5	.
15/07/2014 00:30		0.08	0.03	0.05	.	183.75	.
15/07/2014 00:45		0.07	0.03	0.04	.	184	.
15/07/2014 01 00		0.07	0.03	0.04	.	184.25	.
15/07/2014 01:15		0.07	0.03	0.04	.	184.5	.
15/07/2014 01:30		0.05	0.03	0.02	.	184.75	.
15/07/2014 01:45		0.04	0.03	0.01	.	185	.
15/07/2014 02 00		0.04	0.03	0.01	.	185.25	.
15/07/2014 02:15		0.04	0.03	0.01	.	185.5	.
15/07/2014 02:30		0.04	0.03	0.01	.	185.75	.
15/07/2014 02:45		0.04	0.03	0.01	0.2	186	.
15/07/2014 03 00		0.04	0.03	0.01	.	186.25	.
15/07/2014 03:15		0.04	0.03	0.01	.	186.5	.
15/07/2014 03:30		0.04	0.03	0.01	.	186.75	.
15/07/2014 03:45		0.04	0.03	0.01	.	187	.
15/07/2014 04 00		0.03	0.03	0.00	.	187.25	.
15/07/2014 04:15		0.03	0.03	0.00	.	187.5	.
15/07/2014 04:30		0.03	0.03	0.00	.	187.75	.
15/07/2014 04:45		0.03	0.03	0.00	.	188	.
15/07/2014 05 00		0.03	0.03	0.00	.	188.25	.
15/07/2014 05:15		0.03	0.03	0.00	.	188.5	.
15/07/2014 05:30		0.03	0.03	0.00	.	188.75	.
15/07/2014 05:45		0.03	0.03	0.00	.	189	.
15/07/2014 06 00		0.03	0.03	0.00	.	189.25	.
15/07/2014 06:15		0.02	0.02	0.00	.	189.5	.
15/07/2014 06:30		0.03	0.03	0.00	.	189.75	.
15/07/2014 06:45		0.03	0.03	0.00	.	190	.
15/07/2014 07 00		0.03	0.03	0.00	.	190.25	.
15/07/2014 07:15		0.03	0.03	0.00	.	190.5	.
15/07/2014 07:30		0.03	0.03	0.00	.	190.75	.
15/07/2014 07:45		0.04	0.03	0.01	.	191	.
15/07/2014 08 00		0.04	0.03	0.01	.	191.25	.
15/07/2014 08:15		0.04	0.03	0.01	.	191.5	.
15/07/2014 08:30		0.05	0.03	0.02	.	191.75	.
15/07/2014 08:45		0.04	0.03	0.01	.	192	.
15/07/2014 09 00		0.04	0.03	0.01	.	192.25	.
15/07/2014 09:15		0.05	0.03	0.02	.	192.5	.
15/07/2014 09:30		0.04	0.03	0.01	.	192.75	.
15/07/2014 09:45		0.05	0.03	0.02	.	193	.
15/07/2014 10 00		0.05	0.03	0.02	.	193.25	.
15/07/2014 10:15		0.05	0.03	0.02	.	193.5	.
15/07/2014 10:30		0.04	0.03	0.01	.	193.75	.
15/07/2014 10:45		0.04	0.03	0.01	.	194	.
15/07/2014 11 00		0.05	0.03	0.02	.	194.25	.
15/07/2014 11:15		0.05	0.03	0.02	.	194.5	.
15/07/2014 11:30		0.06	0.03	0.03	.	194.75	.
15/07/2014 11:45		0.05	0.03	0.02	.	195	.
15/07/2014 12 00		0.06	0.03	0.03	.	195.25	.
15/07/2014 12:15		0.04	0.03	0.01	.	195.5	.
15/07/2014 12:30		0.04	0.03	0.01	.	195.75	.
15/07/2014 12:45		0.05	0.03	0.02	.	196	.
15/07/2014 13 00		0.04	0.03	0.01	.	196.25	.
15/07/2014 13:15		0.04	0.03	0.01	.	196.5	.
15/07/2014 13:30		0.04	0.03	0.01	.	196.75	.
15/07/2014 13:45		0.04	0.03	0.01	.	197	.
15/07/2014 14 00		0.05	0.03	0.02	.	197.25	.
15/07/2014 14:15		0.04	0.03	0.01	.	197.5	.
15/07/2014 14:30		0.04	0.03	0.01	.	197.75	.
15/07/2014 14:45		0.04	0.03	0.01	.	198	.

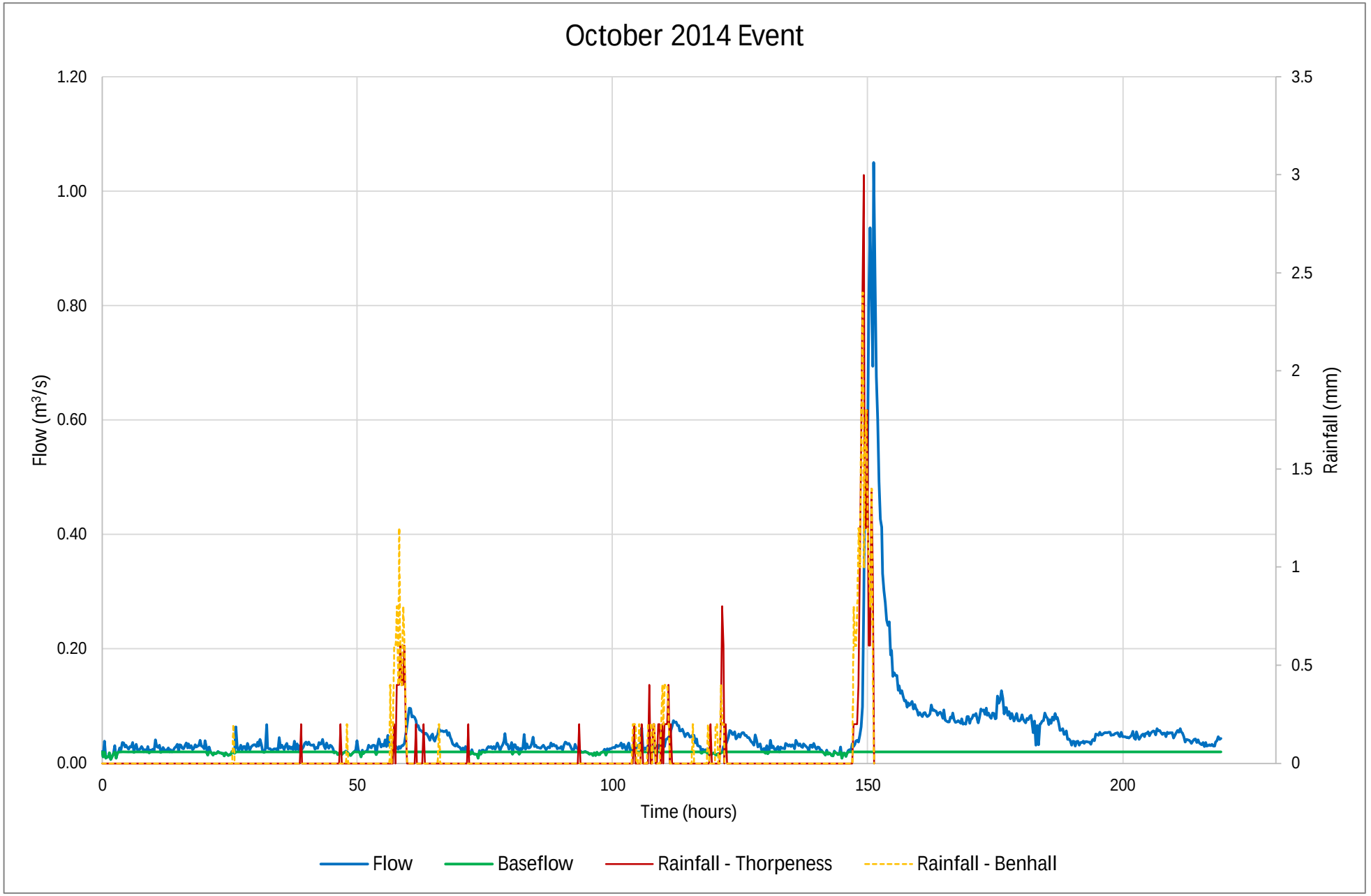
Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

		G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)
15/07/2014 15 00		0.04	0.03	0.01	.	198.25	.
15/07/2014 15:15		0.04	0.03	0.01	.	198.5	.
15/07/2014 15:30		0.04	0.03	0.01	.	198.75	.
15/07/2014 15:45		0.04	0.03	0.01	.	199	.
15/07/2014 16 00		0.04	0.03	0.01	.	199.25	.
15/07/2014 16:15		0.04	0.03	0.01	.	199.5	.
15/07/2014 16:30		0.04	0.03	0.01	.	199.75	.
15/07/2014 16:45		0.04	0.03	0.01	.	200	.
15/07/2014 17 00		0.04	0.03	0.01	.	200.25	.
15/07/2014 17:15		0.04	0.03	0.01	.	200.5	.
15/07/2014 17:30		0.05	0.03	0.02	.	200.75	.
15/07/2014 17:45		0.04	0.03	0.01	.	201	.
15/07/2014 18 00		0.04	0.03	0.01	.	201.25	.
15/07/2014 18:15		0.04	0.03	0.01	.	201.5	.
15/07/2014 18:30		0.04	0.03	0.01	.	201.75	.
15/07/2014 18:45		0.04	0.03	0.01	.	202	.
15/07/2014 19 00		0.04	0.03	0.01	.	202.25	.
15/07/2014 19:15		0.05	0.03	0.02	.	202.5	.
15/07/2014 19:30		0.05	0.03	0.02	.	202.75	.
15/07/2014 19:45		0.04	0.03	0.01	.	203	.
15/07/2014 20 00		0.04	0.03	0.01	.	203.25	.
15/07/2014 20:15		0.04	0.03	0.01	.	203.5	.
15/07/2014 20:30		0.04	0.03	0.01	.	203.75	.
15/07/2014 20:45		0.05	0.03	0.02	.	204	.
15/07/2014 21 00		0.04	0.03	0.01	.	204.25	.
15/07/2014 21:15		0.04	0.03	0.01	.	204.5	.
15/07/2014 21:30		0.05	0.03	0.02	.	204.75	.
15/07/2014 21:45		0.04	0.03	0.01	.	205	.
15/07/2014 22 00		0.04	0.03	0.01	.	205.25	.
15/07/2014 22:15		0.05	0.03	0.02	.	205.5	.
15/07/2014 22:30		0.04	0.03	0.01	.	205.75	.
15/07/2014 22:45		0.04	0.03	0.01	.	206	.
15/07/2014 23 00		0.05	0.03	0.02	0.4	206.25	.
15/07/2014 23:15		0.04	0.03	0.01	.	206.5	.
15/07/2014 23:30		0.04	0.03	0.01	.	206.75	.
15/07/2014 23:45		0.04	0.03	0.01	.	207	.
16/07/2014 00 00		0.05	0.03	0.02	.	207.25	.
16/07/2014 00:15		0.05	0.03	0.02	.	207.5	.
16/07/2014 00:30		0.05	0.03	0.02	.	207.75	.
16/07/2014 00:45		0.04	0.03	0.01	.	208	.
16/07/2014 01 00		0.04	0.03	0.01	.	208.25	.
16/07/2014 01:15		0.04	0.03	0.01	.	208.5	.
16/07/2014 01:30		0.04	0.03	0.01	.	208.75	.
16/07/2014 01:45		0.04	0.03	0.01	.	209	.
16/07/2014 02 00		0.04	0.03	0.01	0.2	209.25	.
16/07/2014 02:15		0.04	0.03	0.01	.	209.5	.
16/07/2014 02:30		0.03	0.03	0.00	.	209.75	.
16/07/2014 02:45		0.03	0.03	0.00	0.4	210	.
16/07/2014 03 00		0.03	0.03	0.00	.	210.25	.
16/07/2014 03:15		0.03	0.03	0.00	.	210.5	.
16/07/2014 03:30		0.03	0.03	0.00	0.2	210.75	.
16/07/2014 03:45		0.03	0.03	0.00	.	211	.
16/07/2014 04 00		0.03	0.03	0.00	.	211.25	.
16/07/2014 04:15		0.03	0.03	0.00	.	211.5	.
16/07/2014 04:30		0.02	0.02	0.00	.	211.75	.
16/07/2014 04:45		0.03	0.03	0.00	.	212	.
16/07/2014 05 00		0.03	0.03	0.00	.	212.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event


October 2014 Event
1.20
1.00
0.80
0.60
0.40
0.20
0.00
Flow (m³/s)
3.5
3
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
50
100
150
200
Time (hours)
Flow
Baseflow
Rainfall - Thorpeness
Rainfall - Benhall

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
02/10/2014 05:30	0.02	0.02	0.00	.	0	.
02/10/2014 05:45	0.01	0.01	0.00	.	0.25	.
02/10/2014 06:00	0.04	0.02	0.02	.	0.5	.
02/10/2014 06:15	0.01	0.01	0.00	.	0.75	.
02/10/2014 06:30	0.01	0.01	0.00	.	1	.
02/10/2014 06:45	0.01	0.01	0.00	.	1.25	.
02/10/2014 07:00	0.02	0.02	0.00	.	1.5	.
02/10/2014 07:15	0.01	0.01	0.00	.	1.75	.
02/10/2014 07:30	0.01	0.01	0.00	.	2	.
02/10/2014 07:45	0.02	0.02	0.00	.	2.25	.
02/10/2014 08:00	0.03	0.02	0.01	.	2.5	.
02/10/2014 08:15	0.01	0.01	0.00	.	2.75	.
02/10/2014 08:30	0.02	0.02	0.00	.	3	.
02/10/2014 08:45	0.02	0.02	0.00	.	3.25	.
02/10/2014 09:00	0.03	0.02	0.01	.	3.5	.
02/10/2014 09:15	0.02	0.02	0.00	.	3.75	.
02/10/2014 09:30	0.04	0.02	0.02	.	4	.
02/10/2014 09:45	0.04	0.02	0.02	.	4.25	.
02/10/2014 10:00	0.03	0.02	0.01	.	4.5	.
02/10/2014 10:15	0.03	0.02	0.01	.	4.75	.
02/10/2014 10:30	0.03	0.02	0.01	.	5	.
02/10/2014 10:45	0.02	0.02	0.00	.	5.25	.
02/10/2014 11:00	0.03	0.02	0.01	.	5.5	.
02/10/2014 11:15	0.03	0.02	0.01	.	5.75	.
02/10/2014 11:30	0.04	0.02	0.02	.	6	.
02/10/2014 11:45	0.02	0.02	0.00	.	6.25	.
02/10/2014 12:00	0.03	0.02	0.01	.	6.5	.
02/10/2014 12:15	0.03	0.02	0.01	.	6.75	.
02/10/2014 12:30	0.02	0.02	0.00	.	7	.
02/10/2014 12:45	0.02	0.02	0.00	.	7.25	.
02/10/2014 13:00	0.03	0.02	0.01	.	7.5	.
02/10/2014 13:15	0.03	0.02	0.01	.	7.75	.
02/10/2014 13:30	0.02	0.02	0.00	.	8	.
02/10/2014 13:45	0.02	0.02	0.00	.	8.25	.
02/10/2014 14:00	0.02	0.02	0.00	.	8.5	.
02/10/2014 14:15	0.02	0.02	0.00	.	8.75	.
02/10/2014 14:30	0.03	0.02	0.01	.	9	.
02/10/2014 14:45	0.02	0.02	0.00	.	9.25	.
02/10/2014 15:00	0.02	0.02	0.00	.	9.5	.
02/10/2014 15:15	0.02	0.02	0.00	.	9.75	.
02/10/2014 15:30	0.02	0.02	0.00	.	10	.
02/10/2014 15:45	0.02	0.02	0.00	.	10.25	.
02/10/2014 16:00	0.04	0.02	0.02	.	10.5	.
02/10/2014 16:15	0.03	0.02	0.01	.	10.75	.
02/10/2014 16:30	0.03	0.02	0.01	.	11	.
02/10/2014 16:45	0.03	0.02	0.01	.	11.25	.
02/10/2014 17:00	0.02	0.02	0.00	.	11.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Thorpeness	
Area (km^2)	5.04
Total Rain (P) mm	26 8
Time Interval (hour)	0.25
Percentage Runoff	20%

Benhall	
Area (km^2)	5.04
Total Rain (P) mm	31 2
Time Interval (hour)	0.25
Percentage Runoff	17%

Average PR	18%

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
02/10/2014 17:15	0.02	0.02	0.00	.	11.75	.
02/10/2014 17:30	0.03	0.02	0.01	.	12	.
02/10/2014 17:45	0.02	0.02	0.00	.	12.25	.
02/10/2014 18:00	0.02	0.02	0.00	.	12.5	.
02/10/2014 18:15	0.02	0.02	0.00	.	12.75	.
02/10/2014 18:30	0.03	0.02	0.01	.	13	.
02/10/2014 18:45	0.02	0.02	0.00	.	13.25	.
02/10/2014 19:00	0.02	0.02	0.00	.	13.5	.
02/10/2014 19:15	0.02	0.02	0.00	.	13.75	.
02/10/2014 19:30	0.02	0.02	0.00	.	14	.
02/10/2014 19:45	0.03	0.02	0.01	.	14.25	.
02/10/2014 20:00	0.03	0.02	0.01	.	14.5	.
02/10/2014 20:15	0.03	0.02	0.01	.	14.75	.
02/10/2014 20:30	0.02	0.02	0.00	.	15	.
02/10/2014 20:45	0.03	0.02	0.01	.	15.25	.
02/10/2014 21:00	0.03	0.02	0.01	.	15.5	.
02/10/2014 21:15	0.03	0.02	0.01	.	15.75	.
02/10/2014 21:30	0.03	0.02	0.01	.	16	.
02/10/2014 21:45	0.03	0.02	0.01	.	16.25	.
02/10/2014 22:00	0.04	0.02	0.02	.	16.5	.
02/10/2014 22:15	0.03	0.02	0.01	.	16.75	.
02/10/2014 22:30	0.03	0.02	0.01	.	17	.
02/10/2014 22:45	0.03	0.02	0.01	.	17.25	.
02/10/2014 23:00	0.03	0.02	0.01	.	17.5	.
02/10/2014 23:15	0.02	0.02	0.00	.	17.75	.
02/10/2014 23:30	0.03	0.02	0.01	.	18	.
02/10/2014 23:45	0.03	0.02	0.01	.	18.25	.
03/10/2014 00:00	0.03	0.02	0.01	.	18.5	.
03/10/2014 00:15	0.03	0.02	0.01	.	18.75	.
03/10/2014 00:30	0.03	0.02	0.01	.	19	.
03/10/2014 00:45	0.04	0.02	0.02	.	19.25	.
03/10/2014 01:00	0.03	0.02	0.01	.	19.5	.
03/10/2014 01:15	0.03	0.02	0.01	.	19.75	.
03/10/2014 01:30	0.03	0.02	0.01	.	20	.
03/10/2014 01:45	0.04	0.02	0.02	.	20.25	.
03/10/2014 02:00	0.03	0.02	0.01	.	20.5	.
03/10/2014 02:15	0.01	0.01	0.00	.	20.75	.
03/10/2014 02:30	0.03	0.02	0.01	.	21	.
03/10/2014 02:45	0.02	0.02	0.00	.	21.25	.
03/10/2014 03:00	0.02	0.02	0.00	.	21.5	.
03/10/2014 03:15	0.01	0.01	0.00	.	21.75	.
03/10/2014 03:30	0.02	0.02	0.00	.	22	.
03/10/2014 03:45	0.02	0.02	0.00	.	22.25	.
03/10/2014 04:00	0.02	0.02	0.00	.	22.5	.
03/10/2014 04:15	0.02	0.02	0.00	.	22.75	.
03/10/2014 04:30	0.02	0.02	0.00	.	23	.
03/10/2014 04:45	0.02	0.02	0.00	.	23.25	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
03/10/2014 05:00	0.02	0.02	0.00	.	23.5	.
03/10/2014 05:15	0.02	0.02	0.00	.	23.75	.
03/10/2014 05:30	0.01	0.01	0.00	.	24	.
03/10/2014 05:45	0.02	0.02	0.00	.	24.25	.
03/10/2014 06:00	0.02	0.02	0.00	.	24.5	.
03/10/2014 06:15	0.01	0.01	0.00	.	24.75	.
03/10/2014 06:30	0.01	0.01	0.00	.	25	.
03/10/2014 06:45	0.02	0.02	0.00	.	25.25	.
03/10/2014 07:00	0.02	0.02	0.00	.	25.5	.
03/10/2014 07:15	0.02	0.02	0.00	.	25.75	0.2
03/10/2014 07:30	0.02	0.02	0.00	.	26	.
03/10/2014 07:45	0.06	0.02	0.04	.	26.25	.
03/10/2014 08:00	0.03	0.02	0.01	.	26.5	.
03/10/2014 08:15	0.02	0.02	0.00	.	26.75	.
03/10/2014 08:30	0.03	0.02	0.01	.	27	.
03/10/2014 08:45	0.03	0.02	0.01	.	27.25	.
03/10/2014 09:00	0.02	0.02	0.00	.	27.5	.
03/10/2014 09:15	0.03	0.02	0.01	.	27.75	.
03/10/2014 09:30	0.03	0.02	0.01	.	28	.
03/10/2014 09:45	0.02	0.02	0.00	.	28.25	.
03/10/2014 10:00	0.03	0.02	0.01	.	28.5	.
03/10/2014 10:15	0.03	0.02	0.01	.	28.75	.
03/10/2014 10:30	0.02	0.02	0.00	.	29	.
03/10/2014 10:45	0.03	0.02	0.01	.	29.25	.
03/10/2014 11:00	0.03	0.02	0.01	.	29.5	.
03/10/2014 11:15	0.03	0.02	0.01	.	29.75	.
03/10/2014 11:30	0.03	0.02	0.01	.	30	.
03/10/2014 11:45	0.03	0.02	0.01	.	30.25	.
03/10/2014 12:00	0.04	0.02	0.02	.	30.5	.
03/10/2014 12:15	0.03	0.02	0.01	.	30.75	.
03/10/2014 12:30	0.04	0.02	0.02	.	31	.
03/10/2014 12:45	0.03	0.02	0.01	.	31.25	.
03/10/2014 13:00	0.02	0.02	0.00	.	31.5	.
03/10/2014 13:15	0.02	0.02	0.00	.	31.75	.
03/10/2014 13:30	0.03	0.02	0.01	.	32	.
03/10/2014 13:45	0.07	0.02	0.05	.	32.25	.
03/10/2014 14:00	0.03	0.02	0.01	.	32.5	.
03/10/2014 14:15	0.03	0.02	0.01	.	32.75	.
03/10/2014 14:30	0.03	0.02	0.01	.	33	.
03/10/2014 14:45	0.02	0.02	0.00	.	33.25	.
03/10/2014 15:00	0.02	0.02	0.00	.	33.5	.
03/10/2014 15:15	0.03	0.02	0.01	.	33.75	.
03/10/2014 15:30	0.02	0.02	0.00	.	34	.
03/10/2014 15:45	0.03	0.02	0.01	.	34.25	.
03/10/2014 16:00	0.02	0.02	0.00	.	34.5	.
03/10/2014 16:15	0.04	0.02	0.02	.	34.75	.
03/10/2014 16:30	0.03	0.02	0.01	.	35	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
03/10/2014 16:45	0.03	0.02	0.01	.	35.25	.
03/10/2014 17:00	0.03	0.02	0.01	.	35.5	.
03/10/2014 17:15	0.02	0.02	0.00	.	35.75	.
03/10/2014 17:30	0.03	0.02	0.01	.	36	.
03/10/2014 17:45	0.03	0.02	0.01	.	36.25	.
03/10/2014 18:00	0.02	0.02	0.00	.	36.5	.
03/10/2014 18:15	0.03	0.02	0.01	.	36.75	.
03/10/2014 18:30	0.03	0.02	0.01	.	37	.
03/10/2014 18:45	0.03	0.02	0.01	.	37.25	.
03/10/2014 19:00	0.02	0.02	0.00	.	37.5	.
03/10/2014 19:15	0.04	0.02	0.02	.	37.75	.
03/10/2014 19:30	0.02	0.02	0.00	.	38	.
03/10/2014 19:45	0.03	0.02	0.01	.	38.25	.
03/10/2014 20:00	0.02	0.02	0.00	.	38.5	.
03/10/2014 20:15	0.03	0.02	0.01	.	38.75	.
03/10/2014 20:30	0.03	0.02	0.01	0.2	39	.
03/10/2014 20:45	0.02	0.02	0.00	.	39.25	.
03/10/2014 21:00	0.03	0.02	0.01	.	39.5	.
03/10/2014 21:15	0.03	0.02	0.01	.	39.75	.
03/10/2014 21:30	0.04	0.02	0.02	.	40	.
03/10/2014 21:45	0.03	0.02	0.01	.	40.25	.
03/10/2014 22:00	0.04	0.02	0.02	.	40.5	.
03/10/2014 22:15	0.03	0.02	0.01	.	40.75	.
03/10/2014 22:30	0.03	0.02	0.01	.	41	.
03/10/2014 22:45	0.03	0.02	0.01	.	41.25	.
03/10/2014 23:00	0.03	0.02	0.01	.	41.5	.
03/10/2014 23:15	0.02	0.02	0.00	.	41.75	.
03/10/2014 23:30	0.03	0.02	0.01	.	42	.
03/10/2014 23:45	0.03	0.02	0.01	.	42.25	.
04/10/2014 00:00	0.04	0.02	0.02	.	42.5	.
04/10/2014 00:15	0.03	0.02	0.01	.	42.75	.
04/10/2014 00:30	0.03	0.02	0.01	.	43	.
04/10/2014 00:45	0.04	0.02	0.02	.	43.25	.
04/10/2014 01:00	0.03	0.02	0.01	.	43.5	.
04/10/2014 01:15	0.03	0.02	0.01	.	43.75	.
04/10/2014 01:30	0.04	0.02	0.02	.	44	.
04/10/2014 01:45	0.03	0.02	0.01	.	44.25	.
04/10/2014 02:00	0.03	0.02	0.01	.	44.5	.
04/10/2014 02:15	0.03	0.02	0.01	.	44.75	.
04/10/2014 02:30	0.03	0.02	0.01	.	45	.
04/10/2014 02:45	0.03	0.02	0.01	.	45.25	.
04/10/2014 03:00	0.02	0.02	0.00	.	45.5	.
04/10/2014 03:15	0.02	0.02	0.00	.	45.75	.
04/10/2014 03:30	0.02	0.02	0.00	.	46	.
04/10/2014 03:45	0.02	0.02	0.00	.	46.25	.
04/10/2014 04:00	0.02	0.02	0.00	.	46.5	.
04/10/2014 04:15	0.02	0.02	0.00	0.2	46.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
04/10/2014 04:30	0.02	0.02	0.00	.	47	.
04/10/2014 04:45	0.02	0.02	0.00	.	47.25	.
04/10/2014 05:00	0.02	0.02	0.00	.	47.5	.
04/10/2014 05:15	0.02	0.02	0.00	.	47.75	.
04/10/2014 05:30	0.02	0.02	0.00	.	48	0.2
04/10/2014 05:45	0.02	0.02	0.00	.	48.25	.
04/10/2014 06:00	0.02	0.02	0.00	.	48.5	.
04/10/2014 06:15	0.01	0.01	0.00	.	48.75	.
04/10/2014 06:30	0.02	0.02	0.00	.	49	.
04/10/2014 06:45	0.02	0.02	0.00	.	49.25	.
04/10/2014 07:00	0.02	0.02	0.00	.	49.5	.
04/10/2014 07:15	0.02	0.02	0.00	.	49.75	.
04/10/2014 07:30	0.04	0.02	0.02	.	50	.
04/10/2014 07:45	0.02	0.02	0.00	.	50.25	.
04/10/2014 08:00	0.02	0.02	0.00	.	50.5	.
04/10/2014 08:15	0.01	0.01	0.00	.	50.75	.
04/10/2014 08:30	0.02	0.02	0.00	.	51	.
04/10/2014 08:45	0.02	0.02	0.00	.	51.25	.
04/10/2014 09:00	0.02	0.02	0.00	.	51.5	.
04/10/2014 09:15	0.02	0.02	0.00	.	51.75	.
04/10/2014 09:30	0.02	0.02	0.00	.	52	.
04/10/2014 09:45	0.03	0.02	0.01	.	52.25	.
04/10/2014 10:00	0.03	0.02	0.01	.	52.5	.
04/10/2014 10:15	0.03	0.02	0.01	.	52.75	.
04/10/2014 10:30	0.03	0.02	0.01	.	53	.
04/10/2014 10:45	0.03	0.02	0.01	.	53.25	.
04/10/2014 11:00	0.03	0.02	0.01	.	53.5	.
04/10/2014 11:15	0.01	0.01	0.00	.	53.75	.
04/10/2014 11:30	0.03	0.02	0.01	.	54	.
04/10/2014 11:45	0.04	0.02	0.02	.	54.25	.
04/10/2014 12:00	0.03	0.02	0.01	.	54.5	.
04/10/2014 12:15	0.03	0.02	0.01	.	54.75	.
04/10/2014 12:30	0.03	0.02	0.01	.	55	.
04/10/2014 12:45	0.03	0.02	0.01	.	55.25	.
04/10/2014 13:00	0.04	0.02	0.02	.	55.5	.
04/10/2014 13:15	0.03	0.02	0.01	.	55.75	.
04/10/2014 13:30	0.05	0.02	0.03	.	56	.
04/10/2014 13:45	0.03	0.02	0.01	.	56.25	.
04/10/2014 14:00	0.03	0.02	0.01	.	56.5	0.4
04/10/2014 14:15	0.03	0.02	0.01	.	56.75	.
04/10/2014 14:30	0.03	0.02	0.01	.	57	0.2
04/10/2014 14:45	0.03	0.02	0.01	0.2	57.25	0.6
04/10/2014 15:00	0.03	0.02	0.01	.	57.5	0.6
04/10/2014 15:15	0.03	0.02	0.01	0.4	57.75	0.8
04/10/2014 15:30	0.02	0.02	0.00	0.4	58	0.4
04/10/2014 15:45	0.03	0.02	0.01	0.4	58.25	1.2
04/10/2014 16:00	0.03	0.02	0.01	0.6	58.5	0.4

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
04/10/2014 16:15	0.03	0.02	0.01	0.4	58.75	0.4
04/10/2014 16:30	0.03	0.02	0.01	0.4	59	0.8
04/10/2014 16:45	0.03	0.02	0.01	0.6	59.25	0.6
04/10/2014 17:00	0.05	0.02	0.03	0.2	59.5	0.2
04/10/2014 17:15	0.07	0.02	0.05	.	59.75	.
04/10/2014 17:30	0.08	0.02	0.06	.	60	.
04/10/2014 17:45	0.10	0.02	0.08	.	60.25	.
04/10/2014 18:00	0.10	0.02	0.08	.	60.5	.
04/10/2014 18:15	0.08	0.02	0.06	.	60.75	.
04/10/2014 18:30	0.08	0.02	0.06	.	61	.
04/10/2014 18:45	0.08	0.02	0.06	.	61.25	.
04/10/2014 19:00	0.07	0.02	0.05	0.2	61.5	.
04/10/2014 19:15	0.06	0.02	0.04	.	61.75	.
04/10/2014 19:30	0.07	0.02	0.05	.	62	.
04/10/2014 19:45	0.06	0.02	0.04	.	62.25	.
04/10/2014 20:00	0.06	0.02	0.04	.	62.5	.
04/10/2014 20:15	0.06	0.02	0.04	.	62.75	.
04/10/2014 20:30	0.05	0.02	0.03	0.2	63	.
04/10/2014 20:45	0.05	0.02	0.03	.	63.25	.
04/10/2014 21:00	0.05	0.02	0.03	.	63.5	.
04/10/2014 21:15	0.05	0.02	0.03	.	63.75	.
04/10/2014 21:30	0.05	0.02	0.03	.	64	.
04/10/2014 21:45	0.04	0.02	0.02	.	64.25	.
04/10/2014 22:00	0.05	0.02	0.03	.	64.5	.
04/10/2014 22:15	0.05	0.02	0.03	.	64.75	.
04/10/2014 22:30	0.04	0.02	0.02	.	65	.
04/10/2014 22:45	0.04	0.02	0.02	.	65.25	.
04/10/2014 23:00	0.05	0.02	0.03	.	65.5	.
04/10/2014 23:15	0.05	0.02	0.03	.	65.75	.
04/10/2014 23:30	0.06	0.02	0.04	.	66	0.2
04/10/2014 23:45	0.06	0.02	0.04	.	66.25	.
05/10/2014 00:00	0.06	0.02	0.04	.	66.5	.
05/10/2014 00:15	0.06	0.02	0.04	.	66.75	.
05/10/2014 00:30	0.06	0.02	0.04	.	67	.
05/10/2014 00:45	0.06	0.02	0.04	.	67.25	.
05/10/2014 01:00	0.06	0.02	0.04	.	67.5	.
05/10/2014 01:15	0.05	0.02	0.03	.	67.75	.
05/10/2014 01:30	0.05	0.02	0.03	.	68	.
05/10/2014 01:45	0.04	0.02	0.02	.	68.25	.
05/10/2014 02:00	0.04	0.02	0.02	.	68.5	.
05/10/2014 02:15	0.03	0.02	0.01	.	68.75	.
05/10/2014 02:30	0.03	0.02	0.01	.	69	.
05/10/2014 02:45	0.03	0.02	0.01	.	69.25	.
05/10/2014 03:00	0.03	0.02	0.01	.	69.5	.
05/10/2014 03:15	0.03	0.02	0.01	.	69.75	.
05/10/2014 03:30	0.03	0.02	0.01	.	70	.
05/10/2014 03:45	0.03	0.02	0.01	.	70.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
05/10/2014 04:00	0.02	0.02	0.00	.	70.5	.
05/10/2014 04:15	0.03	0.02	0.01	.	70.75	.
05/10/2014 04:30	0.02	0.02	0.00	.	71	.
05/10/2014 04:45	0.03	0.02	0.01	.	71.25	.
05/10/2014 05:00	0.02	0.02	0.00	.	71.5	.
05/10/2014 05:15	0.02	0.02	0.00	0.2	71.75	.
05/10/2014 05:30	0.02	0.02	0.00	.	72	.
05/10/2014 05:45	0.02	0.02	0.00	.	72.25	.
05/10/2014 06:00	0.02	0.02	0.00	.	72.5	.
05/10/2014 06:15	0.02	0.02	0.00	.	72.75	.
05/10/2014 06:30	0.02	0.02	0.00	.	73	.
05/10/2014 06:45	0.02	0.02	0.00	.	73.25	.
05/10/2014 07:00	0.01	0.01	0.00	.	73.5	.
05/10/2014 07:15	0.01	0.01	0.00	.	73.75	.
05/10/2014 07:30	0.02	0.02	0.00	.	74	.
05/10/2014 07:45	0.02	0.02	0.00	.	74.25	.
05/10/2014 08:00	0.02	0.02	0.00	.	74.5	.
05/10/2014 08:15	0.02	0.02	0.00	.	74.75	.
05/10/2014 08:30	0.02	0.02	0.00	.	75	.
05/10/2014 08:45	0.02	0.02	0.00	.	75.25	.
05/10/2014 09:00	0.03	0.02	0.01	.	75.5	.
05/10/2014 09:15	0.03	0.02	0.01	.	75.75	.
05/10/2014 09:30	0.03	0.02	0.01	.	76	.
05/10/2014 09:45	0.03	0.02	0.01	.	76.25	.
05/10/2014 10:00	0.03	0.02	0.01	.	76.5	.
05/10/2014 10:15	0.03	0.02	0.01	.	76.75	.
05/10/2014 10:30	0.02	0.02	0.00	.	77	.
05/10/2014 10:45	0.03	0.02	0.01	.	77.25	.
05/10/2014 11:00	0.04	0.02	0.02	.	77.5	.
05/10/2014 11:15	0.03	0.02	0.01	.	77.75	.
05/10/2014 11:30	0.02	0.02	0.00	.	78	.
05/10/2014 11:45	0.03	0.02	0.01	.	78.25	.
05/10/2014 12:00	0.03	0.02	0.01	.	78.5	.
05/10/2014 12:15	0.04	0.02	0.02	.	78.75	.
05/10/2014 12:30	0.05	0.02	0.03	.	79	.
05/10/2014 12:45	0.03	0.02	0.01	.	79.25	.
05/10/2014 13:00	0.03	0.02	0.01	.	79.5	.
05/10/2014 13:15	0.02	0.02	0.00	.	79.75	.
05/10/2014 13:30	0.03	0.02	0.01	.	80	.
05/10/2014 13:45	0.04	0.02	0.02	.	80.25	.
05/10/2014 14:00	0.02	0.02	0.00	.	80.5	.
05/10/2014 14:15	0.03	0.02	0.01	.	80.75	.
05/10/2014 14:30	0.03	0.02	0.01	.	81	.
05/10/2014 14:45	0.03	0.02	0.01	.	81.25	.
05/10/2014 15:00	0.03	0.02	0.01	.	81.5	.
05/10/2014 15:15	0.02	0.02	0.00	.	81.75	.
05/10/2014 15:30	0.03	0.02	0.01	.	82	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
05/10/2014 15:45	0.02	0.02	0.00	.	82.25	.
05/10/2014 16:00	0.03	0.02	0.01	.	82.5	.
05/10/2014 16:15	0.05	0.02	0.03	.	82.75	.
05/10/2014 16:30	0.02	0.02	0.00	.	83	.
05/10/2014 16:45	0.03	0.02	0.01	.	83.25	.
05/10/2014 17:00	0.03	0.02	0.01	.	83.5	.
05/10/2014 17:15	0.03	0.02	0.01	.	83.75	.
05/10/2014 17:30	0.03	0.02	0.01	.	84	.
05/10/2014 17:45	0.04	0.02	0.02	.	84.25	.
05/10/2014 18:00	0.05	0.02	0.03	.	84.5	.
05/10/2014 18:15	0.03	0.02	0.01	.	84.75	.
05/10/2014 18:30	0.03	0.02	0.01	.	85	.
05/10/2014 18:45	0.03	0.02	0.01	.	85.25	.
05/10/2014 19:00	0.03	0.02	0.01	.	85.5	.
05/10/2014 19:15	0.03	0.02	0.01	.	85.75	.
05/10/2014 19:30	0.03	0.02	0.01	.	86	.
05/10/2014 19:45	0.03	0.02	0.01	.	86.25	.
05/10/2014 20:00	0.03	0.02	0.01	.	86.5	.
05/10/2014 20:15	0.03	0.02	0.01	.	86.75	.
05/10/2014 20:30	0.02	0.02	0.00	.	87	.
05/10/2014 20:45	0.03	0.02	0.01	.	87.25	.
05/10/2014 21:00	0.03	0.02	0.01	.	87.5	.
05/10/2014 21:15	0.03	0.02	0.01	.	87.75	.
05/10/2014 21:30	0.04	0.02	0.02	.	88	.
05/10/2014 21:45	0.03	0.02	0.01	.	88.25	.
05/10/2014 22:00	0.03	0.02	0.01	.	88.5	.
05/10/2014 22:15	0.03	0.02	0.01	.	88.75	.
05/10/2014 22:30	0.03	0.02	0.01	.	89	.
05/10/2014 22:45	0.03	0.02	0.01	.	89.25	.
05/10/2014 23:00	0.03	0.02	0.01	.	89.5	.
05/10/2014 23:15	0.03	0.02	0.01	.	89.75	.
05/10/2014 23:30	0.03	0.02	0.01	.	90	.
05/10/2014 23:45	0.02	0.02	0.00	.	90.25	.
06/10/2014 00:00	0.03	0.02	0.01	.	90.5	.
06/10/2014 00:15	0.04	0.02	0.02	.	90.75	.
06/10/2014 00:30	0.04	0.02	0.02	.	91	.
06/10/2014 00:45	0.03	0.02	0.01	.	91.25	.
06/10/2014 01:00	0.03	0.02	0.01	.	91.5	.
06/10/2014 01:15	0.03	0.02	0.01	.	91.75	.
06/10/2014 01:30	0.03	0.02	0.01	.	92	.
06/10/2014 01:45	0.02	0.02	0.00	.	92.25	.
06/10/2014 02:00	0.03	0.02	0.01	.	92.5	.
06/10/2014 02:15	0.03	0.02	0.01	.	92.75	.
06/10/2014 02:30	0.03	0.02	0.01	.	93	.
06/10/2014 02:45	0.03	0.02	0.01	.	93.25	.
06/10/2014 03:00	0.02	0.02	0.00	0.2	93.5	.
06/10/2014 03:15	0.02	0.02	0.00	.	93.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/10/2014 03:30	0.02	0.02	0.00	.	94	.
06/10/2014 03:45	0.02	0.02	0.00	.	94.25	.
06/10/2014 04:00	0.02	0.02	0.00	.	94.5	.
06/10/2014 04:15	0.02	0.02	0.00	.	94.75	.
06/10/2014 04:30	0.02	0.02	0.00	.	95	.
06/10/2014 04:45	0.02	0.02	0.00	.	95.25	.
06/10/2014 05:00	0.02	0.02	0.00	.	95.5	.
06/10/2014 05:15	0.02	0.02	0.00	.	95.75	.
06/10/2014 05:30	0.02	0.02	0.00	.	96	.
06/10/2014 05:45	0.01	0.01	0.00	.	96.25	.
06/10/2014 06:00	0.02	0.02	0.00	.	96.5	.
06/10/2014 06:15	0.01	0.01	0.00	.	96.75	.
06/10/2014 06:30	0.02	0.02	0.00	.	97	.
06/10/2014 06:45	0.02	0.02	0.00	.	97.25	.
06/10/2014 07:00	0.02	0.02	0.00	.	97.5	.
06/10/2014 07:15	0.02	0.02	0.00	.	97.75	.
06/10/2014 07:30	0.02	0.02	0.00	.	98	.
06/10/2014 07:45	0.02	0.02	0.00	.	98.25	.
06/10/2014 08:00	0.02	0.02	0.00	.	98.5	.
06/10/2014 08:15	0.01	0.01	0.00	.	98.75	.
06/10/2014 08:30	0.03	0.02	0.01	.	99	.
06/10/2014 08:45	0.02	0.02	0.00	.	99.25	.
06/10/2014 09:00	0.03	0.02	0.01	.	99.5	.
06/10/2014 09:15	0.02	0.02	0.00	.	99.75	.
06/10/2014 09:30	0.03	0.02	0.01	.	100	.
06/10/2014 09:45	0.03	0.02	0.01	.	100.25	.
06/10/2014 10:00	0.03	0.02	0.01	.	100.5	.
06/10/2014 10:15	0.03	0.02	0.01	.	100.75	.
06/10/2014 10:30	0.03	0.02	0.01	.	101	.
06/10/2014 10:45	0.03	0.02	0.01	.	101.25	.
06/10/2014 11:00	0.03	0.02	0.01	.	101.5	.
06/10/2014 11:15	0.04	0.02	0.02	.	101.75	.
06/10/2014 11:30	0.03	0.02	0.01	.	102	.
06/10/2014 11:45	0.03	0.02	0.01	.	102.25	.
06/10/2014 12:00	0.03	0.02	0.01	.	102.5	.
06/10/2014 12:15	0.02	0.02	0.00	.	102.75	.
06/10/2014 12:30	0.03	0.02	0.01	.	103	.
06/10/2014 12:45	0.04	0.02	0.02	.	103.25	.
06/10/2014 13:00	0.02	0.02	0.00	.	103.5	.
06/10/2014 13:15	0.02	0.02	0.00	.	103.75	.
06/10/2014 13:30	0.03	0.02	0.01	.	104	0.2
06/10/2014 13:45	0.03	0.02	0.01	0.2	104.25	0.2
06/10/2014 14:00	0.02	0.02	0.00	.	104.5	0.2
06/10/2014 14:15	0.03	0.02	0.01	.	104.75	.
06/10/2014 14:30	0.03	0.02	0.01	.	105	.
06/10/2014 14:45	0.03	0.02	0.01	.	105.25	0.2
06/10/2014 15:00	0.03	0.02	0.01	.	105.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/10/2014 15:15	0.06	0.02	0.04	0.2	105.75	.
06/10/2014 15:30	0.02	0.02	0.00	.	106	.
06/10/2014 15:45	0.02	0.02	0.00	.	106.25	.
06/10/2014 16:00	0.03	0.02	0.01	.	106.5	.
06/10/2014 16:15	0.02	0.02	0.00	.	106.75	.
06/10/2014 16:30	0.03	0.02	0.01	.	107	0.2
06/10/2014 16:45	0.02	0.02	0.00	0.4	107.25	0.2
06/10/2014 17:00	0.02	0.02	0.00	.	107.5	0.2
06/10/2014 17:15	0.03	0.02	0.01	.	107.75	.
06/10/2014 17:30	0.03	0.02	0.01	0.2	108	0.2
06/10/2014 17:45	0.03	0.02	0.01	0.2	108.25	0.2
06/10/2014 18:00	0.03	0.02	0.01	.	108.5	.
06/10/2014 18:15	0.03	0.02	0.01	.	108.75	.
06/10/2014 18:30	0.03	0.02	0.01	0.2	109	.
06/10/2014 18:45	0.03	0.02	0.01	0.2	109.25	.
06/10/2014 19:00	0.04	0.02	0.02	.	109.5	0.2
06/10/2014 19:15	0.04	0.02	0.02	0.2	109.75	0.4
06/10/2014 19:30	0.04	0.02	0.02	.	110	0.2
06/10/2014 19:45	0.03	0.02	0.01	0.2	110.25	0.4
06/10/2014 20:00	0.04	0.02	0.02	0.2	110.5	0.4
06/10/2014 20:15	0.04	0.02	0.02	0.2	110.75	0.4
06/10/2014 20:30	0.05	0.02	0.03	0.4	111	0.2
06/10/2014 20:45	0.05	0.02	0.03	.	111.25	.
06/10/2014 21:00	0.06	0.02	0.04	0.2	111.5	.
06/10/2014 21:15	0.06	0.02	0.04	.	111.75	.
06/10/2014 21:30	0.07	0.02	0.05	.	112	.
06/10/2014 21:45	0.07	0.02	0.05	.	112.25	.
06/10/2014 22:00	0.07	0.02	0.05	.	112.5	.
06/10/2014 22:15	0.07	0.02	0.05	.	112.75	.
06/10/2014 22:30	0.07	0.02	0.05	.	113	.
06/10/2014 22:45	0.06	0.02	0.04	.	113.25	.
06/10/2014 23:00	0.06	0.02	0.04	.	113.5	.
06/10/2014 23:15	0.06	0.02	0.04	.	113.75	.
06/10/2014 23:30	0.05	0.02	0.03	.	114	.
06/10/2014 23:45	0.05	0.02	0.03	.	114.25	.
07/10/2014 00:00	0.05	0.02	0.03	.	114.5	.
07/10/2014 00:15	0.05	0.02	0.03	.	114.75	.
07/10/2014 00:30	0.05	0.02	0.03	.	115	.
07/10/2014 00:45	0.05	0.02	0.03	.	115.25	.
07/10/2014 01:00	0.05	0.02	0.03	.	115.5	.
07/10/2014 01:15	0.05	0.02	0.03	.	115.75	0.2
07/10/2014 01:30	0.05	0.02	0.03	.	116	.
07/10/2014 01:45	0.04	0.02	0.02	.	116.25	.
07/10/2014 02:00	0.04	0.02	0.02	.	116.5	.
07/10/2014 02:15	0.03	0.02	0.01	.	116.75	.
07/10/2014 02:30	0.03	0.02	0.01	.	117	.
07/10/2014 02:45	0.03	0.02	0.01	.	117.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
07/10/2014 03:00	0.02	0.02	0.00	.	117.5	.
07/10/2014 03:15	0.02	0.02	0.00	.	117.75	.
07/10/2014 03:30	0.02	0.02	0.00	.	118	.
07/10/2014 03:45	0.02	0.02	0.00	.	118.25	.
07/10/2014 04:00	0.02	0.02	0.00	.	118.5	.
07/10/2014 04:15	0.02	0.02	0.00	.	118.75	0.2
07/10/2014 04:30	0.03	0.02	0.01	.	119	.
07/10/2014 04:45	0.02	0.02	0.00	0.2	119.25	.
07/10/2014 05:00	0.02	0.02	0.00	.	119.5	.
07/10/2014 05:15	0.02	0.02	0.00	.	119.75	.
07/10/2014 05:30	0.02	0.02	0.00	.	120	.
07/10/2014 05:45	0.02	0.02	0.00	.	120.25	0.2
07/10/2014 06:00	0.01	0.01	0.00	.	120.5	0.2
07/10/2014 06:15	0.02	0.02	0.00	.	120.75	.
07/10/2014 06:30	0.02	0.02	0.00	.	121	.
07/10/2014 06:45	0.02	0.02	0.00	0.2	121.25	0.4
07/10/2014 07:00	0.02	0.02	0.00	0.8	121.5	0.2
07/10/2014 07:15	0.03	0.02	0.01	0.6	121.75	0.2
07/10/2014 07:30	0.03	0.02	0.01	.	122	.
07/10/2014 07:45	0.03	0.02	0.01	0.2	122.25	.
07/10/2014 08:00	0.04	0.02	0.02	.	122.5	.
07/10/2014 08:15	0.05	0.02	0.03	.	122.75	.
07/10/2014 08:30	0.06	0.02	0.04	.	123	.
07/10/2014 08:45	0.06	0.02	0.04	.	123.25	.
07/10/2014 09:00	0.05	0.02	0.03	.	123.5	.
07/10/2014 09:15	0.05	0.02	0.03	.	123.75	.
07/10/2014 09:30	0.05	0.02	0.03	.	124	.
07/10/2014 09:45	0.04	0.02	0.02	.	124.25	.
07/10/2014 10:00	0.05	0.02	0.03	.	124.5	.
07/10/2014 10:15	0.05	0.02	0.03	.	124.75	.
07/10/2014 10:30	0.05	0.02	0.03	.	125	.
07/10/2014 10:45	0.05	0.02	0.03	.	125.25	.
07/10/2014 11:00	0.05	0.02	0.03	.	125.5	.
07/10/2014 11:15	0.05	0.02	0.03	.	125.75	.
07/10/2014 11:30	0.05	0.02	0.03	.	126	.
07/10/2014 11:45	0.05	0.02	0.03	.	126.25	.
07/10/2014 12:00	0.04	0.02	0.02	.	126.5	.
07/10/2014 12:15	0.04	0.02	0.02	.	126.75	.
07/10/2014 12:30	0.04	0.02	0.02	.	127	.
07/10/2014 12:45	0.04	0.02	0.02	.	127.25	.
07/10/2014 13:00	0.04	0.02	0.02	.	127.5	.
07/10/2014 13:15	0.03	0.02	0.01	.	127.75	.
07/10/2014 13:30	0.05	0.02	0.03	.	128	.
07/10/2014 13:45	0.04	0.02	0.02	.	128.25	.
07/10/2014 14:00	0.03	0.02	0.01	.	128.5	.
07/10/2014 14:15	0.03	0.02	0.01	.	128.75	.
07/10/2014 14:30	0.03	0.02	0.01	.	129	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
07/10/2014 14:45	0.02	0.02	0.00	.	129.25	.
07/10/2014 15:00	0.02	0.02	0.00	.	129.5	.
07/10/2014 15:15	0.03	0.02	0.01	.	129.75	.
07/10/2014 15:30	0.02	0.02	0.00	.	130	.
07/10/2014 15:45	0.03	0.02	0.01	.	130.25	.
07/10/2014 16:00	0.02	0.02	0.00	.	130.5	.
07/10/2014 16:15	0.02	0.02	0.00	.	130.75	.
07/10/2014 16:30	0.04	0.02	0.02	.	131	.
07/10/2014 16:45	0.03	0.02	0.01	.	131.25	.
07/10/2014 17:00	0.03	0.02	0.01	.	131.5	.
07/10/2014 17:15	0.02	0.02	0.00	.	131.75	.
07/10/2014 17:30	0.02	0.02	0.00	.	132	.
07/10/2014 17:45	0.03	0.02	0.01	.	132.25	.
07/10/2014 18:00	0.03	0.02	0.01	.	132.5	.
07/10/2014 18:15	0.02	0.02	0.00	.	132.75	.
07/10/2014 18:30	0.03	0.02	0.01	.	133	.
07/10/2014 18:45	0.03	0.02	0.01	.	133.25	.
07/10/2014 19:00	0.03	0.02	0.01	.	133.5	.
07/10/2014 19:15	0.03	0.02	0.01	.	133.75	.
07/10/2014 19:30	0.03	0.02	0.01	.	134	.
07/10/2014 19:45	0.03	0.02	0.01	.	134.25	.
07/10/2014 20:00	0.03	0.02	0.01	.	134.5	.
07/10/2014 20:15	0.03	0.02	0.01	.	134.75	.
07/10/2014 20:30	0.03	0.02	0.01	.	135	.
07/10/2014 20:45	0.03	0.02	0.01	.	135.25	.
07/10/2014 21:00	0.03	0.02	0.01	.	135.5	.
07/10/2014 21:15	0.03	0.02	0.01	.	135.75	.
07/10/2014 21:30	0.04	0.02	0.02	.	136	.
07/10/2014 21:45	0.04	0.02	0.02	.	136.25	.
07/10/2014 22:00	0.03	0.02	0.01	.	136.5	.
07/10/2014 22:15	0.03	0.02	0.01	.	136.75	.
07/10/2014 22:30	0.03	0.02	0.01	.	137	.
07/10/2014 22:45	0.03	0.02	0.01	.	137.25	.
07/10/2014 23:00	0.03	0.02	0.01	.	137.5	.
07/10/2014 23:15	0.03	0.02	0.01	.	137.75	.
07/10/2014 23:30	0.03	0.02	0.01	.	138	.
07/10/2014 23:45	0.03	0.02	0.01	.	138.25	.
08/10/2014 00:00	0.02	0.02	0.00	.	138.5	.
08/10/2014 00:15	0.03	0.02	0.01	.	138.75	.
08/10/2014 00:30	0.03	0.02	0.01	.	139	.
08/10/2014 00:45	0.03	0.02	0.01	.	139.25	.
08/10/2014 01:00	0.03	0.02	0.01	.	139.5	.
08/10/2014 01:15	0.03	0.02	0.01	.	139.75	.
08/10/2014 01:30	0.02	0.02	0.00	.	140	.
08/10/2014 01:45	0.03	0.02	0.01	.	140.25	.
08/10/2014 02:00	0.03	0.02	0.01	.	140.5	.
08/10/2014 02:15	0.02	0.02	0.00	.	140.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/10/2014 02:30	0.02	0.02	0.00	.	141	.
08/10/2014 02:45	0.02	0.02	0.00	.	141.25	.
08/10/2014 03:00	0.02	0.02	0.00	.	141.5	.
08/10/2014 03:15	0.01	0.01	0.00	.	141.75	.
08/10/2014 03:30	0.02	0.02	0.00	.	142	.
08/10/2014 03:45	0.02	0.02	0.00	.	142.25	.
08/10/2014 04:00	0.02	0.02	0.00	.	142.5	.
08/10/2014 04:15	0.02	0.02	0.00	.	142.75	.
08/10/2014 04:30	0.01	0.01	0.00	.	143	.
08/10/2014 04:45	0.01	0.01	0.00	.	143.25	.
08/10/2014 05:00	0.02	0.02	0.00	.	143.5	.
08/10/2014 05:15	0.02	0.02	0.00	.	143.75	.
08/10/2014 05:30	0.02	0.02	0.00	.	144	.
08/10/2014 05:45	0.02	0.02	0.00	.	144.25	.
08/10/2014 06:00	0.02	0.02	0.00	.	144.5	.
08/10/2014 06:15	0.03	0.02	0.01	.	144.75	.
08/10/2014 06:30	0.01	0.01	0.00	.	145	.
08/10/2014 06:45	0.02	0.02	0.00	.	145.25	.
08/10/2014 07:00	0.02	0.02	0.00	.	145.5	.
08/10/2014 07:15	0.01	0.01	0.00	.	145.75	.
08/10/2014 07:30	0.02	0.02	0.00	.	146	.
08/10/2014 07:45	0.02	0.02	0.00	.	146.25	.
08/10/2014 08:00	0.02	0.02	0.00	.	146.5	.
08/10/2014 08:15	0.02	0.02	0.00	.	146.75	.
08/10/2014 08:30	0.03	0.02	0.01	.	147	.
08/10/2014 08:45	0.03	0.02	0.01	0.2	147.25	0.8
08/10/2014 09:00	0.03	0.02	0.01	0.2	147.5	0.6
08/10/2014 09:15	0.04	0.02	0.02	0.2	147.75	0.6
08/10/2014 09:30	0.04	0.02	0.02	0.2	148	0.8
08/10/2014 09:45	0.04	0.02	0.02	0.4	148.25	1.2
08/10/2014 10:00	0.05	0.02	0.03	1	148.5	1
08/10/2014 10:15	0.06	0.02	0.04	1.6	148.75	1.8
08/10/2014 10:30	0.10	0.02	0.08	2.4	149	2.4
08/10/2014 10:45	0.29	0.02	0.27	3	149.25	1
08/10/2014 11:00	0.48	0.02	0.46	1.2	149.5	1.6
08/10/2014 11:15	0.43	0.02	0.41	1.2	149.75	1.8
08/10/2014 11:30	0.49	0.02	0.47	1.8	150	1.2
08/10/2014 11:45	0.81	0.02	0.79	0.6	150.25	1
08/10/2014 12:00	0.94	0.02	0.92	0.6	150.5	0.8
08/10/2014 12:15	0.82	0.02	0.80	1.4	150.75	1.4
08/10/2014 12:30	0.69	0.02	0.67	1	151	0.4
08/10/2014 12:45	1.05	0.02	1.03	.	151.25	.
08/10/2014 13:00	0.86	0.02	0.84	.	151.5	.
08/10/2014 13:15	0.68	0.02	0.66	.	151.75	.
08/10/2014 13:30	0.60	0.02	0.58	.	152	.
08/10/2014 13:45	0.49	0.02	0.47	.	152.25	.
08/10/2014 14:00	0.43	0.02	0.41	.	152.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/10/2014 14:15	0.41	0.02	0.39	.	152.75	.
08/10/2014 14:30	0.33	0.02	0.31	.	153	.
08/10/2014 14:45	0.30	0.02	0.28	.	153.25	.
08/10/2014 15:00	0.28	0.02	0.26	.	153.5	.
08/10/2014 15:15	0.25	0.02	0.23	.	153.75	.
08/10/2014 15:30	0.24	0.02	0.22	.	154	.
08/10/2014 15:45	0.25	0.02	0.23	.	154.25	.
08/10/2014 16:00	0.19	0.02	0.17	.	154.5	.
08/10/2014 16:15	0.20	0.02	0.18	.	154.75	.
08/10/2014 16:30	0.15	0.02	0.13	.	155	.
08/10/2014 16:45	0.16	0.02	0.14	.	155.25	.
08/10/2014 17:00	0.15	0.02	0.13	0.2	155.5	.
08/10/2014 17:15	0.15	0.02	0.13	.	155.75	.
08/10/2014 17:30	0.13	0.02	0.11	.	156	.
08/10/2014 17:45	0.14	0.02	0.12	.	156.25	.
08/10/2014 18:00	0.12	0.02	0.10	.	156.5	.
08/10/2014 18:15	0.13	0.02	0.11	.	156.75	.
08/10/2014 18:30	0.12	0.02	0.10	.	157	.
08/10/2014 18:45	0.11	0.02	0.09	.	157.25	.
08/10/2014 19:00	0.11	0.02	0.09	.	157.5	.
08/10/2014 19:15	0.10	0.02	0.08	.	157.75	.
08/10/2014 19:30	0.11	0.02	0.09	.	158	.
08/10/2014 19:45	0.10	0.02	0.08	.	158.25	.
08/10/2014 20:00	0.10	0.02	0.08	.	158.5	.
08/10/2014 20:15	0.11	0.02	0.09	.	158.75	.
08/10/2014 20:30	0.09	0.02	0.07	.	159	.
08/10/2014 20:45	0.10	0.02	0.08	.	159.25	.
08/10/2014 21:00	0.09	0.02	0.07	.	159.5	.
08/10/2014 21:15	0.09	0.02	0.07	.	159.75	.
08/10/2014 21:30	0.08	0.02	0.06	.	160	.
08/10/2014 21:45	0.09	0.02	0.07	.	160.25	.
08/10/2014 22:00	0.08	0.02	0.06	.	160.5	.
08/10/2014 22:15	0.08	0.02	0.06	.	160.75	.
08/10/2014 22:30	0.09	0.02	0.07	.	161	.
08/10/2014 22:45	0.09	0.02	0.07	.	161.25	.
08/10/2014 23:00	0.08	0.02	0.06	.	161.5	.
08/10/2014 23:15	0.08	0.02	0.06	.	161.75	.
08/10/2014 23:30	0.08	0.02	0.06	.	162	.
08/10/2014 23:45	0.09	0.02	0.07	.	162.25	.
09/10/2014 00:00	0.10	0.02	0.08	.	162.5	.
09/10/2014 00:15	0.09	0.02	0.07	.	162.75	.
09/10/2014 00:30	0.09	0.02	0.07	.	163	.
09/10/2014 00:45	0.09	0.02	0.07	.	163.25	.
09/10/2014 01:00	0.09	0.02	0.07	.	163.5	.
09/10/2014 01:15	0.08	0.02	0.06	.	163.75	.
09/10/2014 01:30	0.09	0.02	0.07	.	164	.
09/10/2014 01:45	0.09	0.02	0.07	.	164.25	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
09/10/2014 02:00	0.09	0.02	0.07	.	164.5	.
09/10/2014 02:15	0.08	0.02	0.06	.	164.75	.
09/10/2014 02:30	0.09	0.02	0.07	.	165	.
09/10/2014 02:45	0.08	0.02	0.06	.	165.25	.
09/10/2014 03:00	0.07	0.02	0.05	.	165.5	.
09/10/2014 03:15	0.07	0.02	0.05	.	165.75	.
09/10/2014 03:30	0.07	0.02	0.05	.	166	.
09/10/2014 03:45	0.08	0.02	0.06	.	166.25	.
09/10/2014 04:00	0.08	0.02	0.06	.	166.5	.
09/10/2014 04:15	0.09	0.02	0.07	.	166.75	.
09/10/2014 04:30	0.08	0.02	0.06	.	167	.
09/10/2014 04:45	0.07	0.02	0.05	.	167.25	.
09/10/2014 05:00	0.07	0.02	0.05	.	167.5	.
09/10/2014 05:15	0.07	0.02	0.05	.	167.75	.
09/10/2014 05:30	0.07	0.02	0.05	.	168	.
09/10/2014 05:45	0.07	0.02	0.05	.	168.25	.
09/10/2014 06:00	0.08	0.02	0.06	.	168.5	.
09/10/2014 06:15	0.07	0.02	0.05	.	168.75	.
09/10/2014 06:30	0.07	0.02	0.05	.	169	.
09/10/2014 06:45	0.07	0.02	0.05	.	169.25	.
09/10/2014 07:00	0.08	0.02	0.06	.	169.5	.
09/10/2014 07:15	0.08	0.02	0.06	.	169.75	.
09/10/2014 07:30	0.07	0.02	0.05	.	170	.
09/10/2014 07:45	0.08	0.02	0.06	.	170.25	.
09/10/2014 08:00	0.08	0.02	0.06	.	170.5	.
09/10/2014 08:15	0.08	0.02	0.06	.	170.75	.
09/10/2014 08:30	0.08	0.02	0.06	.	171	.
09/10/2014 08:45	0.09	0.02	0.07	.	171.25	.
09/10/2014 09:00	0.08	0.02	0.06	.	171.5	.
09/10/2014 09:15	0.07	0.02	0.05	.	171.75	.
09/10/2014 09:30	0.08	0.02	0.06	.	172	.
09/10/2014 09:45	0.09	0.02	0.07	.	172.25	.
09/10/2014 10:00	0.09	0.02	0.07	.	172.5	.
09/10/2014 10:15	0.09	0.02	0.07	.	172.75	.
09/10/2014 10:30	0.09	0.02	0.07	.	173	.
09/10/2014 10:45	0.10	0.02	0.08	.	173.25	.
09/10/2014 11:00	0.08	0.02	0.06	.	173.5	.
09/10/2014 11:15	0.09	0.02	0.07	.	173.75	.
09/10/2014 11:30	0.08	0.02	0.06	.	174	.
09/10/2014 11:45	0.08	0.02	0.06	.	174.25	.
09/10/2014 12:00	0.09	0.02	0.07	.	174.5	.
09/10/2014 12:15	0.09	0.02	0.07	.	174.75	.
09/10/2014 12:30	0.08	0.02	0.06	0.6	175	0.4
09/10/2014 12:45	0.08	0.02	0.06	.	175.25	.
09/10/2014 13:00	0.12	0.02	0.10	.	175.5	.
09/10/2014 13:15	0.10	0.02	0.08	.	175.75	.
09/10/2014 13:30	0.11	0.02	0.09	.	176	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
09/10/2014 13:45	0.13	0.02	0.11	.	176.25	.
09/10/2014 14:00	0.11	0.02	0.09	.	176.5	.
09/10/2014 14:15	0.09	0.02	0.07	.	176.75	.
09/10/2014 14:30	0.10	0.02	0.08	.	177	.
09/10/2014 14:45	0.10	0.02	0.08	.	177.25	.
09/10/2014 15:00	0.08	0.02	0.06	.	177.5	.
09/10/2014 15:15	0.09	0.02	0.07	.	177.75	.
09/10/2014 15:30	0.08	0.02	0.06	.	178	.
09/10/2014 15:45	0.09	0.02	0.07	.	178.25	.
09/10/2014 16:00	0.08	0.02	0.06	.	178.5	0.2
09/10/2014 16:15	0.07	0.02	0.05	.	178.75	.
09/10/2014 16:30	0.08	0.02	0.06	.	179	.
09/10/2014 16:45	0.09	0.02	0.07	.	179.25	.
09/10/2014 17:00	0.07	0.02	0.05	.	179.5	.
09/10/2014 17:15	0.07	0.02	0.05	.	179.75	.
09/10/2014 17:30	0.08	0.02	0.06	.	180	.
09/10/2014 17:45	0.08	0.02	0.06	.	180.25	.
09/10/2014 18:00	0.08	0.02	0.06	.	180.5	.
09/10/2014 18:15	0.07	0.02	0.05	.	180.75	.
09/10/2014 18:30	0.07	0.02	0.05	.	181	.
09/10/2014 18:45	0.08	0.02	0.06	.	181.25	.
09/10/2014 19:00	0.08	0.02	0.06	.	181.5	.
09/10/2014 19:15	0.08	0.02	0.06	.	181.75	.
09/10/2014 19:30	0.08	0.02	0.06	.	182	.
09/10/2014 19:45	0.07	0.02	0.05	.	182.25	.
09/10/2014 20:00	0.05	0.02	0.03	.	182.5	.
09/10/2014 20:15	0.07	0.02	0.05	.	182.75	.
09/10/2014 20:30	0.03	0.02	0.01	.	183	.
09/10/2014 20:45	0.07	0.02	0.05	.	183.25	.
09/10/2014 21:00	0.03	0.02	0.01	.	183.5	.
09/10/2014 21:15	0.07	0.02	0.05	.	183.75	.
09/10/2014 21:30	0.07	0.02	0.05	.	184	.
09/10/2014 21:45	0.07	0.02	0.05	.	184.25	.
09/10/2014 22:00	0.07	0.02	0.05	.	184.5	.
09/10/2014 22:15	0.09	0.02	0.07	.	184.75	.
09/10/2014 22:30	0.08	0.02	0.06	.	185	.
09/10/2014 22:45	0.08	0.02	0.06	.	185.25	.
09/10/2014 23:00	0.07	0.02	0.05	.	185.5	.
09/10/2014 23:15	0.08	0.02	0.06	.	185.75	.
09/10/2014 23:30	0.07	0.02	0.05	.	186	.
09/10/2014 23:45	0.08	0.02	0.06	.	186.25	.
10/10/2014 00:00	0.08	0.02	0.06	.	186.5	.
10/10/2014 00:15	0.09	0.02	0.07	.	186.75	.
10/10/2014 00:30	0.08	0.02	0.06	.	187	.
10/10/2014 00:45	0.08	0.02	0.06	.	187.25	.
10/10/2014 01:00	0.07	0.02	0.05	.	187.5	.
10/10/2014 01:15	0.06	0.02	0.04	.	187.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
10/10/2014 01:30	0.06	0.02	0.04	.	188	.
10/10/2014 01:45	0.06	0.02	0.04	.	188.25	.
10/10/2014 02:00	0.05	0.02	0.03	.	188.5	.
10/10/2014 02:15	0.05	0.02	0.03	.	188.75	.
10/10/2014 02:30	0.06	0.02	0.04	.	189	.
10/10/2014 02:45	0.04	0.02	0.02	.	189.25	.
10/10/2014 03:00	0.04	0.02	0.02	.	189.5	.
10/10/2014 03:15	0.04	0.02	0.02	.	189.75	.
10/10/2014 03:30	0.03	0.02	0.01	.	190	.
10/10/2014 03:45	0.04	0.02	0.02	.	190.25	.
10/10/2014 04:00	0.04	0.02	0.02	.	190.5	.
10/10/2014 04:15	0.03	0.02	0.01	.	190.75	.
10/10/2014 04:30	0.04	0.02	0.02	.	191	.
10/10/2014 04:45	0.04	0.02	0.02	.	191.25	.
10/10/2014 05:00	0.03	0.02	0.01	.	191.5	.
10/10/2014 05:15	0.04	0.02	0.02	.	191.75	.
10/10/2014 05:30	0.04	0.02	0.02	.	192	.
10/10/2014 05:45	0.04	0.02	0.02	.	192.25	.
10/10/2014 06:00	0.03	0.02	0.01	.	192.5	.
10/10/2014 06:15	0.04	0.02	0.02	.	192.75	.
10/10/2014 06:30	0.04	0.02	0.02	.	193	.
10/10/2014 06:45	0.04	0.02	0.02	.	193.25	.
10/10/2014 07:00	0.04	0.02	0.02	.	193.5	.
10/10/2014 07:15	0.03	0.02	0.01	.	193.75	.
10/10/2014 07:30	0.04	0.02	0.02	.	194	.
10/10/2014 07:45	0.04	0.02	0.02	.	194.25	.
10/10/2014 08:00	0.04	0.02	0.02	.	194.5	.
10/10/2014 08:15	0.05	0.02	0.03	.	194.75	.
10/10/2014 08:30	0.05	0.02	0.03	.	195	.
10/10/2014 08:45	0.05	0.02	0.03	.	195.25	.
10/10/2014 09:00	0.05	0.02	0.03	.	195.5	.
10/10/2014 09:15	0.05	0.02	0.03	.	195.75	.
10/10/2014 09:30	0.05	0.02	0.03	.	196	.
10/10/2014 09:45	0.05	0.02	0.03	.	196.25	.
10/10/2014 10:00	0.05	0.02	0.03	.	196.5	.
10/10/2014 10:15	0.05	0.02	0.03	.	196.75	.
10/10/2014 10:30	0.05	0.02	0.03	.	197	.
10/10/2014 10:45	0.05	0.02	0.03	.	197.25	.
10/10/2014 11:00	0.05	0.02	0.03	.	197.5	.
10/10/2014 11:15	0.05	0.02	0.03	.	197.75	.
10/10/2014 11:30	0.05	0.02	0.03	.	198	.
10/10/2014 11:45	0.05	0.02	0.03	.	198.25	.
10/10/2014 12:00	0.05	0.02	0.03	.	198.5	.
10/10/2014 12:15	0.05	0.02	0.03	.	198.75	.
10/10/2014 12:30	0.05	0.02	0.03	.	199	.
10/10/2014 12:45	0.05	0.02	0.03	.	199.25	.
10/10/2014 13:00	0.05	0.02	0.03	.	199.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

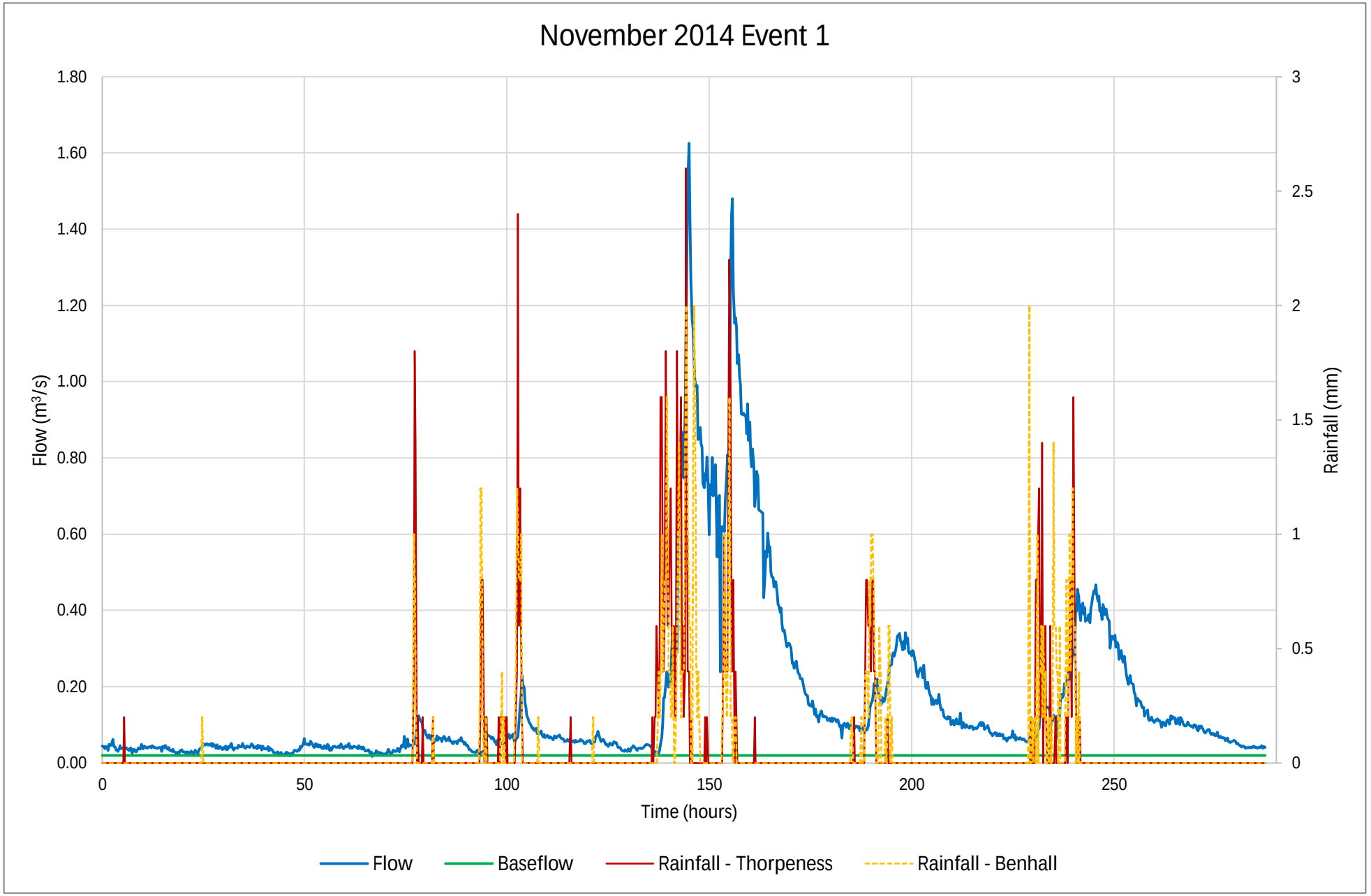
Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
10/10/2014 13:15	0.05	0.02	0.03	.	199.75	.
10/10/2014 13:30	0.05	0.02	0.03	.	200	.
10/10/2014 13:45	0.05	0.02	0.03	.	200.25	.
10/10/2014 14:00	0.05	0.02	0.03	.	200.5	.
10/10/2014 14:15	0.04	0.02	0.02	.	200.75	.
10/10/2014 14:30	0.05	0.02	0.03	.	201	.
10/10/2014 14:45	0.04	0.02	0.02	.	201.25	.
10/10/2014 15:00	0.05	0.02	0.03	.	201.5	.
10/10/2014 15:15	0.05	0.02	0.03	0.2	201.75	.
10/10/2014 15:30	0.06	0.02	0.04	.	202	.
10/10/2014 15:45	0.04	0.02	0.02	.	202.25	.
10/10/2014 16:00	0.04	0.02	0.02	.	202.5	.
10/10/2014 16:15	0.05	0.02	0.03	.	202.75	.
10/10/2014 16:30	0.05	0.02	0.03	.	203	.
10/10/2014 16:45	0.04	0.02	0.02	.	203.25	.
10/10/2014 17:00	0.05	0.02	0.03	.	203.5	.
10/10/2014 17:15	0.05	0.02	0.03	.	203.75	.
10/10/2014 17:30	0.05	0.02	0.03	.	204	.
10/10/2014 17:45	0.05	0.02	0.03	.	204.25	.
10/10/2014 18:00	0.05	0.02	0.03	.	204.5	.
10/10/2014 18:15	0.05	0.02	0.03	.	204.75	.
10/10/2014 18:30	0.06	0.02	0.04	.	205	.
10/10/2014 18:45	0.05	0.02	0.03	.	205.25	.
10/10/2014 19:00	0.05	0.02	0.03	.	205.5	.
10/10/2014 19:15	0.06	0.02	0.04	0.2	205.75	.
10/10/2014 19:30	0.06	0.02	0.04	.	206	.
10/10/2014 19:45	0.06	0.02	0.04	.	206.25	.
10/10/2014 20:00	0.05	0.02	0.03	.	206.5	.
10/10/2014 20:15	0.06	0.02	0.04	.	206.75	.
10/10/2014 20:30	0.06	0.02	0.04	.	207	.
10/10/2014 20:45	0.06	0.02	0.04	.	207.25	.
10/10/2014 21:00	0.05	0.02	0.03	.	207.5	.
10/10/2014 21:15	0.05	0.02	0.03	.	207.75	.
10/10/2014 21:30	0.05	0.02	0.03	.	208	.
10/10/2014 21:45	0.05	0.02	0.03	.	208.25	.
10/10/2014 22:00	0.05	0.02	0.03	.	208.5	.
10/10/2014 22:15	0.05	0.02	0.03	.	208.75	.
10/10/2014 22:30	0.05	0.02	0.03	.	209	.
10/10/2014 22:45	0.05	0.02	0.03	.	209.25	.
10/10/2014 23:00	0.05	0.02	0.03	.	209.5	.
10/10/2014 23:15	0.05	0.02	0.03	.	209.75	.
10/10/2014 23:30	0.04	0.02	0.02	.	210	.
10/10/2014 23:45	0.05	0.02	0.03	.	210.25	.
11/10/2014 00:00	0.05	0.02	0.03	.	210.5	.
11/10/2014 00:15	0.06	0.02	0.04	.	210.75	.
11/10/2014 00:30	0.05	0.02	0.03	.	211	.
11/10/2014 00:45	0.06	0.02	0.04	.	211.25	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
11/10/2014 01:00	0.05	0.02	0.03	.	211.5	.
11/10/2014 01:15	0.05	0.02	0.03	.	211.75	.
11/10/2014 01:30	0.05	0.02	0.03	.	212	.
11/10/2014 01:45	0.04	0.02	0.02	.	212.25	.
11/10/2014 02:00	0.04	0.02	0.02	.	212.5	.
11/10/2014 02:15	0.04	0.02	0.02	.	212.75	.
11/10/2014 02:30	0.04	0.02	0.02	.	213	.
11/10/2014 02:45	0.04	0.02	0.02	.	213.25	.
11/10/2014 03:00	0.03	0.02	0.01	.	213.5	.
11/10/2014 03:15	0.04	0.02	0.02	.	213.75	.
11/10/2014 03:30	0.04	0.02	0.02	.	214	.
11/10/2014 03:45	0.04	0.02	0.02	.	214.25	.
11/10/2014 04:00	0.04	0.02	0.02	.	214.5	.
11/10/2014 04:15	0.04	0.02	0.02	.	214.75	.
11/10/2014 04:30	0.04	0.02	0.02	.	215	.
11/10/2014 04:45	0.03	0.02	0.01	.	215.25	.
11/10/2014 05:00	0.03	0.02	0.01	.	215.5	.
11/10/2014 05:15	0.04	0.02	0.02	.	215.75	.
11/10/2014 05:30	0.03	0.02	0.01	.	216	.
11/10/2014 05:45	0.04	0.02	0.02	.	216.25	.
11/10/2014 06:00	0.03	0.02	0.01	.	216.5	.
11/10/2014 06:15	0.03	0.02	0.01	.	216.75	.
11/10/2014 06:30	0.03	0.02	0.01	.	217	.
11/10/2014 06:45	0.03	0.02	0.01	.	217.25	.
11/10/2014 07:00	0.03	0.02	0.01	.	217.5	.
11/10/2014 07:15	0.03	0.02	0.01	.	217.75	.
11/10/2014 07:30	0.03	0.02	0.01	.	218	.
11/10/2014 07:45	0.04	0.02	0.02	.	218.25	.
11/10/2014 08:00	0.04	0.02	0.02	.	218.5	.
11/10/2014 08:15	0.05	0.02	0.03	.	218.75	.
11/10/2014 08:30	0.04	0.02	0.02	.	219	.
11/10/2014 08:45	0.04	0.02	0.02	.	219.25	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event


November 2014 Event 1
1.80
1.60
1.40
1.20
1.00
0.80
0.60
0.40
0.20
0.00
Flow (m³/s)
3
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
50
100
150
200
250
Time (hours)
Flow
Baseflow
Rainfall - Thorpeness
Rainfall - Benhall

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
30/10/2014 08:45	0.04	0.02	0.02	.	0	.
30/10/2014 09:00	0.04	0.02	0.02	.	0.25	.
30/10/2014 09:15	0.04	0.02	0.02	.	0.5	.
30/10/2014 09:30	0.04	0.02	0.02	.	0.75	.
30/10/2014 09:45	0.04	0.02	0.02	.	1	.
30/10/2014 10:00	0.04	0.02	0.02	.	1.25	.
30/10/2014 10:15	0.03	0.02	0.01	.	1.5	.
30/10/2014 10:30	0.05	0.02	0.03	.	1.75	.
30/10/2014 10:45	0.05	0.02	0.03	.	2	.
30/10/2014 11:00	0.05	0.02	0.03	.	2.25	.
30/10/2014 11:15	0.06	0.02	0.04	.	2.5	.
30/10/2014 11:30	0.06	0.02	0.04	.	2.75	.
30/10/2014 11:45	0.04	0.02	0.02	.	3	.
30/10/2014 12:00	0.04	0.02	0.02	.	3.25	.
30/10/2014 12:15	0.03	0.02	0.01	.	3.5	.
30/10/2014 12:30	0.03	0.02	0.01	.	3.75	.
30/10/2014 12:45	0.03	0.02	0.01	.	4	.
30/10/2014 13:00	0.04	0.02	0.02	.	4.25	.
30/10/2014 13:15	0.05	0.02	0.03	.	4.5	.
30/10/2014 13:30	0.04	0.02	0.02	.	4.75	.
30/10/2014 13:45	0.04	0.02	0.02	.	5	.
30/10/2014 14:00	0.04	0.02	0.02	.	5.25	.
30/10/2014 14:15	0.04	0.02	0.02	0.2	5.5	.
30/10/2014 14:30	0.04	0.02	0.02	.	5.75	.
30/10/2014 14:45	0.04	0.02	0.02	.	6	.
30/10/2014 15:00	0.04	0.02	0.02	.	6.25	.
30/10/2014 15:15	0.04	0.02	0.02	.	6.5	.
30/10/2014 15:30	0.03	0.02	0.01	.	6.75	.
30/10/2014 15:45	0.04	0.02	0.02	.	7	.
30/10/2014 16:00	0.04	0.02	0.02	.	7.25	.
30/10/2014 16:15	0.03	0.02	0.01	.	7.5	.
30/10/2014 16:30	0.03	0.02	0.01	.	7.75	.
30/10/2014 16:45	0.04	0.02	0.02	.	8	.
30/10/2014 17:00	0.03	0.02	0.01	.	8.25	.
30/10/2014 17:15	0.03	0.02	0.01	.	8.5	.
30/10/2014 17:30	0.04	0.02	0.02	.	8.75	.
30/10/2014 17:45	0.04	0.02	0.02	.	9	.
30/10/2014 18:00	0.04	0.02	0.02	.	9.25	.
30/10/2014 18:15	0.04	0.02	0.02	.	9.5	.
30/10/2014 18:30	0.05	0.02	0.03	.	9.75	.
30/10/2014 18:45	0.04	0.02	0.02	.	10	.
30/10/2014 19:00	0.04	0.02	0.02	.	10.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

Thorpeness	
Area (km^2)	5.04
Total Rain (P) mm	74.8
Time Interval (hour)	0.25
Percentage Runoff	40%

Benhall	
Area (km^2)	5.04
Total Rain (P) mm	74.2
Time Interval (hour)	0.25
Percentage Runoff	40%
Average PR	40%

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
30/10/2014 19:15	0.04	0.02	0.02	.	10.5	.
30/10/2014 19:30	0.04	0.02	0.02	.	10.75	.
30/10/2014 19:45	0.04	0.02	0.02	.	11	.
30/10/2014 20:00	0.04	0.02	0.02	.	11.25	.
30/10/2014 20:15	0.04	0.02	0.02	.	11.5	.
30/10/2014 20:30	0.04	0.02	0.02	.	11.75	.
30/10/2014 20:45	0.04	0.02	0.02	.	12	.
30/10/2014 21:00	0.04	0.02	0.02	.	12.25	.
30/10/2014 21:15	0.05	0.02	0.03	.	12.5	.
30/10/2014 21:30	0.04	0.02	0.02	.	12.75	.
30/10/2014 21:45	0.04	0.02	0.02	.	13	.
30/10/2014 22:00	0.04	0.02	0.02	.	13.25	.
30/10/2014 22:15	0.04	0.02	0.02	.	13.5	.
30/10/2014 22:30	0.04	0.02	0.02	.	13.75	.
30/10/2014 22:45	0.04	0.02	0.02	.	14	.
30/10/2014 23:00	0.04	0.02	0.02	.	14.25	.
30/10/2014 23:15	0.04	0.02	0.02	.	14.5	.
30/10/2014 23:30	0.03	0.02	0.01	.	14.75	.
30/10/2014 23:45	0.04	0.02	0.02	.	15	.
31/10/2014 00:00	0.04	0.02	0.02	.	15.25	.
31/10/2014 00:15	0.05	0.02	0.03	.	15.5	.
31/10/2014 00:30	0.05	0.02	0.03	.	15.75	.
31/10/2014 00:45	0.04	0.02	0.02	.	16	.
31/10/2014 01:00	0.04	0.02	0.02	.	16.25	.
31/10/2014 01:15	0.04	0.02	0.02	.	16.5	.
31/10/2014 01:30	0.03	0.02	0.01	.	16.75	.
31/10/2014 01:45	0.03	0.02	0.01	.	17	.
31/10/2014 02:00	0.03	0.02	0.01	.	17.25	.
31/10/2014 02:15	0.04	0.02	0.02	.	17.5	.
31/10/2014 02:30	0.03	0.02	0.01	.	17.75	.
31/10/2014 02:45	0.03	0.02	0.01	.	18	.
31/10/2014 03:00	0.03	0.02	0.01	.	18.25	.
31/10/2014 03:15	0.03	0.02	0.01	.	18.5	.
31/10/2014 03:30	0.03	0.02	0.01	.	18.75	.
31/10/2014 03:45	0.02	0.02	0.00	.	19	.
31/10/2014 04:00	0.03	0.02	0.01	.	19.25	.
31/10/2014 04:15	0.03	0.02	0.01	.	19.5	.
31/10/2014 04:30	0.03	0.02	0.01	.	19.75	.
31/10/2014 04:45	0.03	0.02	0.01	.	20	.
31/10/2014 05:00	0.03	0.02	0.01	.	20.25	.
31/10/2014 05:15	0.03	0.02	0.01	.	20.5	.
31/10/2014 05:30	0.03	0.02	0.01	.	20.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
31/10/2014 05:45	0.03	0.02	0.01	.	21	.
31/10/2014 06:00	0.03	0.02	0.01	.	21.25	.
31/10/2014 06:15	0.02	0.02	0.00	.	21.5	.
31/10/2014 06:30	0.03	0.02	0.01	.	21.75	.
31/10/2014 06:45	0.03	0.02	0.01	.	22	.
31/10/2014 07:00	0.03	0.02	0.01	.	22.25	.
31/10/2014 07:15	0.03	0.02	0.01	.	22.5	.
31/10/2014 07:30	0.03	0.02	0.01	.	22.75	.
31/10/2014 07:45	0.03	0.02	0.01	.	23	.
31/10/2014 08:00	0.03	0.02	0.01	.	23.25	.
31/10/2014 08:15	0.03	0.02	0.01	.	23.5	.
31/10/2014 08:30	0.03	0.02	0.01	.	23.75	.
31/10/2014 08:45	0.04	0.02	0.02	.	24	.
31/10/2014 09:00	0.04	0.02	0.02	.	24.25	.
31/10/2014 09:15	0.04	0.02	0.02	.	24.5	.
31/10/2014 09:30	0.04	0.02	0.02	.	24.75	0.2
31/10/2014 09:45	0.05	0.02	0.03	.	25	.
31/10/2014 10:00	0.05	0.02	0.03	.	25.25	.
31/10/2014 10:15	0.05	0.02	0.03	.	25.5	.
31/10/2014 10:30	0.05	0.02	0.03	.	25.75	.
31/10/2014 10:45	0.05	0.02	0.03	.	26	.
31/10/2014 11:00	0.05	0.02	0.03	.	26.25	.
31/10/2014 11:15	0.05	0.02	0.03	.	26.5	.
31/10/2014 11:30	0.05	0.02	0.03	.	26.75	.
31/10/2014 11:45	0.05	0.02	0.03	.	27	.
31/10/2014 12:00	0.04	0.02	0.02	.	27.25	.
31/10/2014 12:15	0.05	0.02	0.03	.	27.5	.
31/10/2014 12:30	0.05	0.02	0.03	.	27.75	.
31/10/2014 12:45	0.04	0.02	0.02	.	28	.
31/10/2014 13:00	0.04	0.02	0.02	.	28.25	.
31/10/2014 13:15	0.05	0.02	0.03	.	28.5	.
31/10/2014 13:30	0.04	0.02	0.02	.	28.75	.
31/10/2014 13:45	0.04	0.02	0.02	.	29	.
31/10/2014 14:00	0.04	0.02	0.02	.	29.25	.
31/10/2014 14:15	0.04	0.02	0.02	.	29.5	.
31/10/2014 14:30	0.04	0.02	0.02	.	29.75	.
31/10/2014 14:45	0.04	0.02	0.02	.	30	.
31/10/2014 15:00	0.04	0.02	0.02	.	30.25	.
31/10/2014 15:15	0.04	0.02	0.02	.	30.5	.
31/10/2014 15:30	0.04	0.02	0.02	.	30.75	.
31/10/2014 15:45	0.03	0.02	0.01	.	31	.
31/10/2014 16:00	0.04	0.02	0.02	.	31.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
31/10/2014 16:15	0.04	0.02	0.02	.	31.5	.
31/10/2014 16:30	0.05	0.02	0.03	.	31.75	.
31/10/2014 16:45	0.05	0.02	0.03	.	32	.
31/10/2014 17:00	0.04	0.02	0.02	.	32.25	.
31/10/2014 17:15	0.03	0.02	0.01	.	32.5	.
31/10/2014 17:30	0.04	0.02	0.02	.	32.75	.
31/10/2014 17:45	0.04	0.02	0.02	.	33	.
31/10/2014 18:00	0.04	0.02	0.02	.	33.25	.
31/10/2014 18:15	0.04	0.02	0.02	.	33.5	.
31/10/2014 18:30	0.05	0.02	0.03	.	33.75	.
31/10/2014 18:45	0.04	0.02	0.02	.	34	.
31/10/2014 19:00	0.04	0.02	0.02	.	34.25	.
31/10/2014 19:15	0.04	0.02	0.02	.	34.5	.
31/10/2014 19:30	0.05	0.02	0.03	.	34.75	.
31/10/2014 19:45	0.05	0.02	0.03	.	35	.
31/10/2014 20:00	0.04	0.02	0.02	.	35.25	.
31/10/2014 20:15	0.04	0.02	0.02	.	35.5	.
31/10/2014 20:30	0.04	0.02	0.02	.	35.75	.
31/10/2014 20:45	0.04	0.02	0.02	.	36	.
31/10/2014 21:00	0.04	0.02	0.02	.	36.25	.
31/10/2014 21:15	0.04	0.02	0.02	.	36.5	.
31/10/2014 21:30	0.04	0.02	0.02	.	36.75	.
31/10/2014 21:45	0.05	0.02	0.03	.	37	.
31/10/2014 22:00	0.05	0.02	0.03	.	37.25	.
31/10/2014 22:15	0.04	0.02	0.02	.	37.5	.
31/10/2014 22:30	0.04	0.02	0.02	.	37.75	.
31/10/2014 22:45	0.04	0.02	0.02	.	38	.
31/10/2014 23:00	0.04	0.02	0.02	.	38.25	.
31/10/2014 23:15	0.05	0.02	0.03	.	38.5	.
31/10/2014 23:30	0.04	0.02	0.02	.	38.75	.
31/10/2014 23:45	0.04	0.02	0.02	.	39	.
01/11/2014 00:00	0.04	0.02	0.02	.	39.25	.
01/11/2014 00:15	0.03	0.02	0.01	.	39.5	.
01/11/2014 00:30	0.04	0.02	0.02	.	39.75	.
01/11/2014 00:45	0.04	0.02	0.02	.	40	.
01/11/2014 01:00	0.04	0.02	0.02	.	40.25	.
01/11/2014 01:15	0.04	0.02	0.02	.	40.5	.
01/11/2014 01:30	0.04	0.02	0.02	.	40.75	.
01/11/2014 01:45	0.04	0.02	0.02	.	41	.
01/11/2014 02:00	0.03	0.02	0.01	.	41.25	.
01/11/2014 02:15	0.04	0.02	0.02	.	41.5	.
01/11/2014 02:30	0.04	0.02	0.02	.	41.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
01/11/2014 02:45	0.03	0.02	0.01	.	42	.
01/11/2014 03:00	0.03	0.02	0.01	.	42.25	.
01/11/2014 03:15	0.03	0.02	0.01	.	42.5	.
01/11/2014 03:30	0.03	0.02	0.01	.	42.75	.
01/11/2014 03:45	0.03	0.02	0.01	.	43	.
01/11/2014 04:00	0.03	0.02	0.01	.	43.25	.
01/11/2014 04:15	0.03	0.02	0.01	.	43.5	.
01/11/2014 04:30	0.02	0.02	0.00	.	43.75	.
01/11/2014 04:45	0.02	0.02	0.00	.	44	.
01/11/2014 05:00	0.03	0.02	0.01	.	44.25	.
01/11/2014 05:15	0.02	0.02	0.00	.	44.5	.
01/11/2014 05:30	0.02	0.02	0.00	.	44.75	.
01/11/2014 05:45	0.02	0.02	0.00	.	45	.
01/11/2014 06:00	0.02	0.02	0.00	.	45.25	.
01/11/2014 06:15	0.03	0.02	0.01	.	45.5	.
01/11/2014 06:30	0.03	0.02	0.01	.	45.75	.
01/11/2014 06:45	0.02	0.02	0.00	.	46	.
01/11/2014 07:00	0.02	0.02	0.00	.	46.25	.
01/11/2014 07:15	0.02	0.02	0.00	.	46.5	.
01/11/2014 07:30	0.03	0.02	0.01	.	46.75	.
01/11/2014 07:45	0.02	0.02	0.00	.	47	.
01/11/2014 08:00	0.02	0.02	0.00	.	47.25	.
01/11/2014 08:15	0.03	0.02	0.01	.	47.5	.
01/11/2014 08:30	0.03	0.02	0.01	.	47.75	.
01/11/2014 08:45	0.03	0.02	0.01	.	48	.
01/11/2014 09:00	0.03	0.02	0.01	.	48.25	.
01/11/2014 09:15	0.04	0.02	0.02	.	48.5	.
01/11/2014 09:30	0.03	0.02	0.01	.	48.75	.
01/11/2014 09:45	0.04	0.02	0.02	.	49	.
01/11/2014 10:00	0.04	0.02	0.02	.	49.25	.
01/11/2014 10:15	0.05	0.02	0.03	.	49.5	.
01/11/2014 10:30	0.05	0.02	0.03	.	49.75	.
01/11/2014 10:45	0.06	0.02	0.04	.	50	.
01/11/2014 11:00	0.05	0.02	0.03	.	50.25	.
01/11/2014 11:15	0.05	0.02	0.03	.	50.5	.
01/11/2014 11:30	0.05	0.02	0.03	.	50.75	.
01/11/2014 11:45	0.05	0.02	0.03	.	51	.
01/11/2014 12:00	0.05	0.02	0.03	.	51.25	.
01/11/2014 12:15	0.06	0.02	0.04	.	51.5	.
01/11/2014 12:30	0.05	0.02	0.03	.	51.75	.
01/11/2014 12:45	0.05	0.02	0.03	.	52	.
01/11/2014 13:00	0.04	0.02	0.02	.	52.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
01/11/2014 13:15	0.04	0.02	0.02	.	52.5	.
01/11/2014 13:30	0.05	0.02	0.03	.	52.75	.
01/11/2014 13:45	0.05	0.02	0.03	.	53	.
01/11/2014 14:00	0.04	0.02	0.02	.	53.25	.
01/11/2014 14:15	0.05	0.02	0.03	.	53.5	.
01/11/2014 14:30	0.04	0.02	0.02	.	53.75	.
01/11/2014 14:45	0.05	0.02	0.03	.	54	.
01/11/2014 15:00	0.04	0.02	0.02	.	54.25	.
01/11/2014 15:15	0.04	0.02	0.02	.	54.5	.
01/11/2014 15:30	0.04	0.02	0.02	.	54.75	.
01/11/2014 15:45	0.05	0.02	0.03	.	55	.
01/11/2014 16:00	0.04	0.02	0.02	.	55.25	.
01/11/2014 16:15	0.04	0.02	0.02	.	55.5	.
01/11/2014 16:30	0.05	0.02	0.03	.	55.75	.
01/11/2014 16:45	0.04	0.02	0.02	.	56	.
01/11/2014 17:00	0.03	0.02	0.01	.	56.25	.
01/11/2014 17:15	0.04	0.02	0.02	.	56.5	.
01/11/2014 17:30	0.03	0.02	0.01	.	56.75	.
01/11/2014 17:45	0.04	0.02	0.02	.	57	.
01/11/2014 18:00	0.04	0.02	0.02	.	57.25	.
01/11/2014 18:15	0.04	0.02	0.02	.	57.5	.
01/11/2014 18:30	0.04	0.02	0.02	.	57.75	.
01/11/2014 18:45	0.04	0.02	0.02	.	58	.
01/11/2014 19:00	0.04	0.02	0.02	.	58.25	.
01/11/2014 19:15	0.04	0.02	0.02	.	58.5	.
01/11/2014 19:30	0.04	0.02	0.02	.	58.75	.
01/11/2014 19:45	0.05	0.02	0.03	.	59	.
01/11/2014 20:00	0.05	0.02	0.03	.	59.25	.
01/11/2014 20:15	0.04	0.02	0.02	.	59.5	.
01/11/2014 20:30	0.04	0.02	0.02	.	59.75	.
01/11/2014 20:45	0.04	0.02	0.02	.	60	.
01/11/2014 21:00	0.05	0.02	0.03	.	60.25	.
01/11/2014 21:15	0.04	0.02	0.02	.	60.5	.
01/11/2014 21:30	0.05	0.02	0.03	.	60.75	.
01/11/2014 21:45	0.05	0.02	0.03	.	61	.
01/11/2014 22:00	0.04	0.02	0.02	.	61.25	.
01/11/2014 22:15	0.04	0.02	0.02	.	61.5	.
01/11/2014 22:30	0.04	0.02	0.02	.	61.75	.
01/11/2014 22:45	0.04	0.02	0.02	.	62	.
01/11/2014 23:00	0.04	0.02	0.02	.	62.25	.
01/11/2014 23:15	0.04	0.02	0.02	.	62.5	.
01/11/2014 23:30	0.04	0.02	0.02	.	62.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
01/11/2014 23:45	0.04	0.02	0.02	.	63	.
02/11/2014 00:00	0.04	0.02	0.02	.	63.25	.
02/11/2014 00:15	0.05	0.02	0.03	.	63.5	.
02/11/2014 00:30	0.04	0.02	0.02	.	63.75	.
02/11/2014 00:45	0.04	0.02	0.02	.	64	.
02/11/2014 01:00	0.04	0.02	0.02	.	64.25	.
02/11/2014 01:15	0.04	0.02	0.02	.	64.5	.
02/11/2014 01:30	0.04	0.02	0.02	.	64.75	.
02/11/2014 01:45	0.03	0.02	0.01	.	65	.
02/11/2014 02:00	0.03	0.02	0.01	.	65.25	.
02/11/2014 02:15	0.03	0.02	0.01	.	65.5	.
02/11/2014 02:30	0.03	0.02	0.01	.	65.75	.
02/11/2014 02:45	0.03	0.02	0.01	.	66	.
02/11/2014 03:00	0.03	0.02	0.01	.	66.25	.
02/11/2014 03:15	0.03	0.02	0.01	.	66.5	.
02/11/2014 03:30	0.02	0.02	0.00	.	66.75	.
02/11/2014 03:45	0.02	0.02	0.00	.	67	.
02/11/2014 04:00	0.02	0.02	0.00	.	67.25	.
02/11/2014 04:15	0.02	0.02	0.00	.	67.5	.
02/11/2014 04:30	0.03	0.02	0.01	.	67.75	.
02/11/2014 04:45	0.03	0.02	0.01	.	68	.
02/11/2014 05:00	0.03	0.02	0.01	.	68.25	.
02/11/2014 05:15	0.03	0.02	0.01	.	68.5	.
02/11/2014 05:30	0.02	0.02	0.00	.	68.75	.
02/11/2014 05:45	0.03	0.02	0.01	.	69	.
02/11/2014 06:00	0.02	0.02	0.00	.	69.25	.
02/11/2014 06:15	0.02	0.02	0.00	.	69.5	.
02/11/2014 06:30	0.02	0.02	0.00	.	69.75	.
02/11/2014 06:45	0.02	0.02	0.00	.	70	.
02/11/2014 07:00	0.02	0.02	0.00	.	70.25	.
02/11/2014 07:15	0.03	0.02	0.01	.	70.5	.
02/11/2014 07:30	0.04	0.02	0.02	.	70.75	.
02/11/2014 07:45	0.03	0.02	0.01	.	71	.
02/11/2014 08:00	0.02	0.02	0.00	.	71.25	.
02/11/2014 08:15	0.03	0.02	0.01	.	71.5	.
02/11/2014 08:30	0.03	0.02	0.01	.	71.75	.
02/11/2014 08:45	0.03	0.02	0.01	.	72	.
02/11/2014 09:00	0.03	0.02	0.01	.	72.25	.
02/11/2014 09:15	0.03	0.02	0.01	.	72.5	.
02/11/2014 09:30	0.03	0.02	0.01	.	72.75	.
02/11/2014 09:45	0.04	0.02	0.02	.	73	.
02/11/2014 10:00	0.03	0.02	0.01	.	73.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
02/11/2014 10:15	0.03	0.02	0.01	.	73.5	.
02/11/2014 10:30	0.04	0.02	0.02	.	73.75	.
02/11/2014 10:45	0.05	0.02	0.03	.	74	.
02/11/2014 11:00	0.04	0.02	0.02	.	74.25	.
02/11/2014 11:15	0.05	0.02	0.03	.	74.5	.
02/11/2014 11:30	0.07	0.02	0.05	.	74.75	.
02/11/2014 11:45	0.04	0.02	0.02	.	75	.
02/11/2014 12:00	0.06	0.02	0.04	.	75.25	.
02/11/2014 12:15	0.06	0.02	0.04	.	75.5	.
02/11/2014 12:30	0.04	0.02	0.02	.	75.75	.
02/11/2014 12:45	0.05	0.02	0.03	.	76	.
02/11/2014 13:00	0.05	0.02	0.03	.	76.25	.
02/11/2014 13:15	0.05	0.02	0.03	.	76.5	.
02/11/2014 13:30	0.05	0.02	0.03	.	76.75	.
02/11/2014 13:45	0.05	0.02	0.03	0.4	77	1
02/11/2014 14:00	0.05	0.02	0.03	1.8	77.25	0.8
02/11/2014 14:15	0.06	0.02	0.04	1.4	77.5	0.2
02/11/2014 14:30	0.11	0.02	0.09	.	77.75	.
02/11/2014 14:45	0.11	0.02	0.09	0.2	78	.
02/11/2014 15:00	0.12	0.02	0.10	.	78.25	.
02/11/2014 15:15	0.12	0.02	0.10	.	78.5	.
02/11/2014 15:30	0.11	0.02	0.09	.	78.75	.
02/11/2014 15:45	0.11	0.02	0.09	.	79	.
02/11/2014 16:00	0.09	0.02	0.07	0.2	79.25	.
02/11/2014 16:15	0.08	0.02	0.06	.	79.5	.
02/11/2014 16:30	0.08	0.02	0.06	.	79.75	.
02/11/2014 16:45	0.08	0.02	0.06	.	80	.
02/11/2014 17:00	0.07	0.02	0.05	.	80.25	.
02/11/2014 17:15	0.07	0.02	0.05	.	80.5	.
02/11/2014 17:30	0.07	0.02	0.05	.	80.75	.
02/11/2014 17:45	0.07	0.02	0.05	.	81	.
02/11/2014 18:00	0.06	0.02	0.04	.	81.25	.
02/11/2014 18:15	0.07	0.02	0.05	.	81.5	.
02/11/2014 18:30	0.06	0.02	0.04	0.2	81.75	0.2
02/11/2014 18:45	0.05	0.02	0.03	.	82	.
02/11/2014 19:00	0.06	0.02	0.04	.	82.25	.
02/11/2014 19:15	0.06	0.02	0.04	.	82.5	.
02/11/2014 19:30	0.07	0.02	0.05	.	82.75	.
02/11/2014 19:45	0.06	0.02	0.04	.	83	.
02/11/2014 20:00	0.07	0.02	0.05	.	83.25	.
02/11/2014 20:15	0.07	0.02	0.05	.	83.5	.
02/11/2014 20:30	0.06	0.02	0.04	.	83.75	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
02/11/2014 20:45	0.06	0.02	0.04	.	84	.
02/11/2014 21:00	0.07	0.02	0.05	.	84.25	.
02/11/2014 21:15	0.07	0.02	0.05	.	84.5	.
02/11/2014 21:30	0.06	0.02	0.04	.	84.75	.
02/11/2014 21:45	0.06	0.02	0.04	.	85	.
02/11/2014 22:00	0.06	0.02	0.04	.	85.25	.
02/11/2014 22:15	0.06	0.02	0.04	.	85.5	.
02/11/2014 22:30	0.07	0.02	0.05	.	85.75	.
02/11/2014 22:45	0.06	0.02	0.04	.	86	.
02/11/2014 23:00	0.06	0.02	0.04	.	86.25	.
02/11/2014 23:15	0.05	0.02	0.03	.	86.5	.
02/11/2014 23:30	0.05	0.02	0.03	.	86.75	.
02/11/2014 23:45	0.06	0.02	0.04	.	87	.
03/11/2014 00:00	0.05	0.02	0.03	.	87.25	.
03/11/2014 00:15	0.06	0.02	0.04	.	87.5	.
03/11/2014 00:30	0.05	0.02	0.03	.	87.75	.
03/11/2014 00:45	0.06	0.02	0.04	.	88	.
03/11/2014 01:00	0.06	0.02	0.04	.	88.25	.
03/11/2014 01:15	0.06	0.02	0.04	.	88.5	.
03/11/2014 01:30	0.07	0.02	0.05	.	88.75	.
03/11/2014 01:45	0.06	0.02	0.04	.	89	.
03/11/2014 02:00	0.06	0.02	0.04	.	89.25	.
03/11/2014 02:15	0.05	0.02	0.03	.	89.5	.
03/11/2014 02:30	0.05	0.02	0.03	.	89.75	.
03/11/2014 02:45	0.04	0.02	0.02	.	90	.
03/11/2014 03:00	0.05	0.02	0.03	.	90.25	.
03/11/2014 03:15	0.04	0.02	0.02	.	90.5	.
03/11/2014 03:30	0.03	0.02	0.01	.	90.75	.
03/11/2014 03:45	0.04	0.02	0.02	.	91	.
03/11/2014 04:00	0.03	0.02	0.01	.	91.25	.
03/11/2014 04:15	0.03	0.02	0.01	.	91.5	.
03/11/2014 04:30	0.03	0.02	0.01	.	91.75	.
03/11/2014 04:45	0.03	0.02	0.01	.	92	.
03/11/2014 05:00	0.03	0.02	0.01	.	92.25	.
03/11/2014 05:15	0.03	0.02	0.01	.	92.5	.
03/11/2014 05:30	0.03	0.02	0.01	.	92.75	.
03/11/2014 05:45	0.03	0.02	0.01	.	93	.
03/11/2014 06:00	0.03	0.02	0.01	.	93.25	0.2
03/11/2014 06:15	0.03	0.02	0.01	0.2	93.5	1.2
03/11/2014 06:30	0.03	0.02	0.01	0.8	93.75	1.2
03/11/2014 06:45	0.03	0.02	0.01	0.8	94	0.2
03/11/2014 07:00	0.03	0.02	0.01	0.4	94.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
03/11/2014 07:15	0.03	0.02	0.01	.	94.5	.
03/11/2014 07:30	0.05	0.02	0.03	0.2	94.75	0.2
03/11/2014 07:45	0.07	0.02	0.05	0.2	95	.
03/11/2014 08:00	0.07	0.02	0.05	.	95.25	.
03/11/2014 08:15	0.07	0.02	0.05	.	95.5	.
03/11/2014 08:30	0.07	0.02	0.05	.	95.75	.
03/11/2014 08:45	0.07	0.02	0.05	.	96	.
03/11/2014 09:00	0.06	0.02	0.04	.	96.25	.
03/11/2014 09:15	0.07	0.02	0.05	.	96.5	.
03/11/2014 09:30	0.06	0.02	0.04	.	96.75	.
03/11/2014 09:45	0.05	0.02	0.03	.	97	.
03/11/2014 10:00	0.06	0.02	0.04	.	97.25	.
03/11/2014 10:15	0.05	0.02	0.03	.	97.5	.
03/11/2014 10:30	0.06	0.02	0.04	.	97.75	.
03/11/2014 10:45	0.05	0.02	0.03	0.2	98	.
03/11/2014 11:00	0.05	0.02	0.03	.	98.25	.
03/11/2014 11:15	0.05	0.02	0.03	0.2	98.5	0.2
03/11/2014 11:30	0.05	0.02	0.03	0.2	98.75	0.4
03/11/2014 11:45	0.05	0.02	0.03	0.2	99	.
03/11/2014 12:00	0.05	0.02	0.03	0.2	99.25	0.2
03/11/2014 12:15	0.05	0.02	0.03	0.2	99.5	.
03/11/2014 12:30	0.07	0.02	0.05	.	99.75	.
03/11/2014 12:45	0.06	0.02	0.04	0.2	100	.
03/11/2014 13:00	0.07	0.02	0.05	.	100.25	.
03/11/2014 13:15	0.07	0.02	0.05	.	100.5	.
03/11/2014 13:30	0.06	0.02	0.04	.	100.75	.
03/11/2014 13:45	0.07	0.02	0.05	.	101	.
03/11/2014 14:00	0.07	0.02	0.05	.	101.25	.
03/11/2014 14:15	0.08	0.02	0.06	.	101.5	.
03/11/2014 14:30	0.06	0.02	0.04	.	101.75	.
03/11/2014 14:45	0.05	0.02	0.03	.	102	0.2
03/11/2014 15:00	0.06	0.02	0.04	0.2	102.25	0.4
03/11/2014 15:15	0.07	0.02	0.05	0.4	102.5	1.2
03/11/2014 15:30	0.07	0.02	0.05	2.4	102.75	1
03/11/2014 15:45	0.10	0.02	0.08	0.6	103	0.8
03/11/2014 16:00	0.15	0.02	0.13	1.2	103.25	0.8
03/11/2014 16:15	0.17	0.02	0.15	0.6	103.5	1
03/11/2014 16:30	0.23	0.02	0.21	0.2	103.75	.
03/11/2014 16:45	0.20	0.02	0.18	.	104	.
03/11/2014 17:00	0.20	0.02	0.18	.	104.25	.
03/11/2014 17:15	0.16	0.02	0.14	.	104.5	.
03/11/2014 17:30	0.14	0.02	0.12	.	104.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
03/11/2014 17:45	0.12	0.02	0.10	.	105	.
03/11/2014 18:00	0.12	0.02	0.10	.	105.25	.
03/11/2014 18:15	0.11	0.02	0.09	.	105.5	.
03/11/2014 18:30	0.10	0.02	0.08	.	105.75	.
03/11/2014 18:45	0.10	0.02	0.08	.	106	.
03/11/2014 19:00	0.09	0.02	0.07	.	106.25	.
03/11/2014 19:15	0.09	0.02	0.07	.	106.5	.
03/11/2014 19:30	0.08	0.02	0.06	.	106.75	.
03/11/2014 19:45	0.09	0.02	0.07	.	107	.
03/11/2014 20:00	0.09	0.02	0.07	.	107.25	.
03/11/2014 20:15	0.08	0.02	0.06	.	107.5	.
03/11/2014 20:30	0.08	0.02	0.06	.	107.75	0.2
03/11/2014 20:45	0.08	0.02	0.06	.	108	.
03/11/2014 21:00	0.08	0.02	0.06	.	108.25	.
03/11/2014 21:15	0.08	0.02	0.06	.	108.5	.
03/11/2014 21:30	0.07	0.02	0.05	.	108.75	.
03/11/2014 21:45	0.07	0.02	0.05	.	109	.
03/11/2014 22:00	0.07	0.02	0.05	.	109.25	.
03/11/2014 22:15	0.07	0.02	0.05	.	109.5	.
03/11/2014 22:30	0.07	0.02	0.05	.	109.75	.
03/11/2014 22:45	0.07	0.02	0.05	.	110	.
03/11/2014 23:00	0.07	0.02	0.05	.	110.25	.
03/11/2014 23:15	0.07	0.02	0.05	.	110.5	.
03/11/2014 23:30	0.07	0.02	0.05	.	110.75	.
03/11/2014 23:45	0.07	0.02	0.05	.	111	.
04/11/2014 00:00	0.06	0.02	0.04	.	111.25	.
04/11/2014 00:15	0.06	0.02	0.04	.	111.5	.
04/11/2014 00:30	0.07	0.02	0.05	.	111.75	.
04/11/2014 00:45	0.07	0.02	0.05	.	112	.
04/11/2014 01:00	0.07	0.02	0.05	.	112.25	.
04/11/2014 01:15	0.07	0.02	0.05	.	112.5	.
04/11/2014 01:30	0.07	0.02	0.05	.	112.75	.
04/11/2014 01:45	0.07	0.02	0.05	.	113	.
04/11/2014 02:00	0.07	0.02	0.05	.	113.25	.
04/11/2014 02:15	0.06	0.02	0.04	.	113.5	.
04/11/2014 02:30	0.06	0.02	0.04	.	113.75	.
04/11/2014 02:45	0.06	0.02	0.04	.	114	.
04/11/2014 03:00	0.06	0.02	0.04	.	114.25	.
04/11/2014 03:15	0.06	0.02	0.04	.	114.5	.
04/11/2014 03:30	0.06	0.02	0.04	.	114.75	.
04/11/2014 03:45	0.06	0.02	0.04	.	115	.
04/11/2014 04:00	0.06	0.02	0.04	.	115.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
04/11/2014 04:15	0.06	0.02	0.04	.	115.5	.
04/11/2014 04:30	0.06	0.02	0.04	0.2	115.75	.
04/11/2014 04:45	0.05	0.02	0.03	.	116	.
04/11/2014 05:00	0.06	0.02	0.04	.	116.25	.
04/11/2014 05:15	0.06	0.02	0.04	.	116.5	.
04/11/2014 05:30	0.05	0.02	0.03	.	116.75	.
04/11/2014 05:45	0.06	0.02	0.04	.	117	.
04/11/2014 06:00	0.05	0.02	0.03	.	117.25	.
04/11/2014 06:15	0.06	0.02	0.04	.	117.5	.
04/11/2014 06:30	0.06	0.02	0.04	.	117.75	.
04/11/2014 06:45	0.06	0.02	0.04	.	118	.
04/11/2014 07:00	0.06	0.02	0.04	.	118.25	.
04/11/2014 07:15	0.06	0.02	0.04	.	118.5	.
04/11/2014 07:30	0.06	0.02	0.04	.	118.75	.
04/11/2014 07:45	0.05	0.02	0.03	.	119	.
04/11/2014 08:00	0.05	0.02	0.03	.	119.25	.
04/11/2014 08:15	0.05	0.02	0.03	.	119.5	.
04/11/2014 08:30	0.06	0.02	0.04	.	119.75	.
04/11/2014 08:45	0.06	0.02	0.04	.	120	.
04/11/2014 09:00	0.06	0.02	0.04	.	120.25	.
04/11/2014 09:15	0.06	0.02	0.04	.	120.5	.
04/11/2014 09:30	0.05	0.02	0.03	.	120.75	.
04/11/2014 09:45	0.05	0.02	0.03	.	121	.
04/11/2014 10:00	0.06	0.02	0.04	.	121.25	0.2
04/11/2014 10:15	0.06	0.02	0.04	.	121.5	.
04/11/2014 10:30	0.05	0.02	0.03	.	121.75	.
04/11/2014 10:45	0.07	0.02	0.05	.	122	.
04/11/2014 11:00	0.07	0.02	0.05	.	122.25	.
04/11/2014 11:15	0.08	0.02	0.06	.	122.5	.
04/11/2014 11:30	0.07	0.02	0.05	.	122.75	.
04/11/2014 11:45	0.07	0.02	0.05	.	123	.
04/11/2014 12:00	0.06	0.02	0.04	.	123.25	.
04/11/2014 12:15	0.06	0.02	0.04	.	123.5	.
04/11/2014 12:30	0.06	0.02	0.04	.	123.75	.
04/11/2014 12:45	0.06	0.02	0.04	.	124	.
04/11/2014 13:00	0.05	0.02	0.03	.	124.25	.
04/11/2014 13:15	0.05	0.02	0.03	.	124.5	.
04/11/2014 13:30	0.05	0.02	0.03	.	124.75	.
04/11/2014 13:45	0.04	0.02	0.02	.	125	.
04/11/2014 14:00	0.05	0.02	0.03	.	125.25	.
04/11/2014 14:15	0.05	0.02	0.03	.	125.5	.
04/11/2014 14:30	0.05	0.02	0.03	.	125.75	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
04/11/2014 14:45	0.05	0.02	0.03	.	126	.
04/11/2014 15:00	0.05	0.02	0.03	.	126.25	.
04/11/2014 15:15	0.06	0.02	0.04	.	126.5	.
04/11/2014 15:30	0.05	0.02	0.03	.	126.75	.
04/11/2014 15:45	0.05	0.02	0.03	.	127	.
04/11/2014 16:00	0.05	0.02	0.03	.	127.25	.
04/11/2014 16:15	0.04	0.02	0.02	.	127.5	.
04/11/2014 16:30	0.04	0.02	0.02	.	127.75	.
04/11/2014 16:45	0.04	0.02	0.02	.	128	.
04/11/2014 17:00	0.03	0.02	0.01	.	128.25	.
04/11/2014 17:15	0.03	0.02	0.01	.	128.5	.
04/11/2014 17:30	0.03	0.02	0.01	.	128.75	.
04/11/2014 17:45	0.03	0.02	0.01	.	129	.
04/11/2014 18:00	0.03	0.02	0.01	.	129.25	.
04/11/2014 18:15	0.03	0.02	0.01	.	129.5	.
04/11/2014 18:30	0.03	0.02	0.01	.	129.75	.
04/11/2014 18:45	0.04	0.02	0.02	.	130	.
04/11/2014 19:00	0.03	0.02	0.01	.	130.25	.
04/11/2014 19:15	0.03	0.02	0.01	.	130.5	.
04/11/2014 19:30	0.04	0.02	0.02	.	130.75	.
04/11/2014 19:45	0.04	0.02	0.02	.	131	.
04/11/2014 20:00	0.05	0.02	0.03	.	131.25	.
04/11/2014 20:15	0.04	0.02	0.02	.	131.5	.
04/11/2014 20:30	0.04	0.02	0.02	.	131.75	.
04/11/2014 20:45	0.04	0.02	0.02	.	132	.
04/11/2014 21:00	0.03	0.02	0.01	.	132.25	.
04/11/2014 21:15	0.04	0.02	0.02	.	132.5	.
04/11/2014 21:30	0.04	0.02	0.02	.	132.75	.
04/11/2014 21:45	0.04	0.02	0.02	.	133	.
04/11/2014 22:00	0.04	0.02	0.02	.	133.25	.
04/11/2014 22:15	0.04	0.02	0.02	.	133.5	.
04/11/2014 22:30	0.04	0.02	0.02	.	133.75	.
04/11/2014 22:45	0.04	0.02	0.02	.	134	.
04/11/2014 23:00	0.05	0.02	0.03	.	134.25	.
04/11/2014 23:15	0.05	0.02	0.03	.	134.5	.
04/11/2014 23:30	0.05	0.02	0.03	.	134.75	.
04/11/2014 23:45	0.05	0.02	0.03	.	135	.
05/11/2014 00:00	0.05	0.02	0.03	.	135.25	.
05/11/2014 00:15	0.04	0.02	0.02	.	135.5	.
05/11/2014 00:30	0.04	0.02	0.02	.	135.75	.
05/11/2014 00:45	0.04	0.02	0.02	0.2	136	.
05/11/2014 01:00	0.03	0.02	0.01	.	136.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
05/11/2014 01:15	0.03	0.02	0.01	0.2	136.5	.
05/11/2014 01:30	0.03	0.02	0.01	0.2	136.75	.
05/11/2014 01:45	0.03	0.02	0.01	0.6	137	.
05/11/2014 02:00	0.03	0.02	0.01	0.4	137.25	0.2
05/11/2014 02:15	0.03	0.02	0.01	0.2	137.5	0.4
05/11/2014 02:30	0.03	0.02	0.01	0.4	137.75	0.2
05/11/2014 02:45	0.05	0.02	0.03	1.6	138	0.4
05/11/2014 03:00	0.07	0.02	0.05	1.6	138.25	1
05/11/2014 03:15	0.10	0.02	0.08	0.8	138.5	0.4
05/11/2014 03:30	0.17	0.02	0.15	0.4	138.75	0.6
05/11/2014 03:45	0.17	0.02	0.15	0.6	139	0.8
05/11/2014 04:00	0.21	0.02	0.19	1.8	139.25	0.8
05/11/2014 04:15	0.24	0.02	0.22	1.2	139.5	1.6
05/11/2014 04:30	0.23	0.02	0.21	0.6	139.75	1
05/11/2014 04:45	0.20	0.02	0.18	0.6	140	0.4
05/11/2014 05:00	0.20	0.02	0.18	1	140.25	0.4
05/11/2014 05:15	0.21	0.02	0.19	1.2	140.5	0.2
05/11/2014 05:30	0.29	0.02	0.27	0.6	140.75	0.2
05/11/2014 05:45	0.34	0.02	0.32	0.4	141	0.6
05/11/2014 06:00	0.35	0.02	0.33	0.6	141.25	.
05/11/2014 06:15	0.34	0.02	0.32	0.2	141.5	.
05/11/2014 06:30	0.29	0.02	0.27	0.2	141.75	0.2
05/11/2014 06:45	0.29	0.02	0.27	1.8	142	0.6
05/11/2014 07:00	0.59	0.02	0.57	1	142.25	1
05/11/2014 07:15	0.76	0.02	0.74	1	142.5	1.4
05/11/2014 07:30	0.82	0.02	0.80	1.2	142.75	0.8
05/11/2014 07:45	0.83	0.02	0.81	1.6	143	0.2
05/11/2014 08:00	0.87	0.02	0.85	0.4	143.25	0.4
05/11/2014 08:15	0.86	0.02	0.84	0.6	143.5	0.4
05/11/2014 08:30	0.75	0.02	0.73	0.2	143.75	0.4
05/11/2014 08:45	0.91	0.02	0.89	0.4	144	1.4
05/11/2014 09:00	1.11	0.02	1.09	2.6	144.25	2
05/11/2014 09:15	1.31	0.02	1.29	1.4	144.5	1.6
05/11/2014 09:30	1.52	0.02	1.50	0.4	144.75	1
05/11/2014 09:45	1.63	0.02	1.61	0.4	145	0.6
05/11/2014 10:00	1.43	0.02	1.41	.	145.25	0.6
05/11/2014 10:15	1.27	0.02	1.25	0.2	145.5	.
05/11/2014 10:30	1.16	0.02	1.14	.	145.75	.
05/11/2014 10:45	1.14	0.02	1.12	.	146	1.4
05/11/2014 11:00	1.06	0.02	1.04	.	146.25	2
05/11/2014 11:15	1.00	0.02	0.98	.	146.5	1.6
05/11/2014 11:30	0.98	0.02	0.96	.	146.75	0.4

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
05/11/2014 11:45	0.99	0.02	0.97	.	147	0.2
05/11/2014 12:00	0.85	0.02	0.83	.	147.25	0.4
05/11/2014 12:15	0.85	0.02	0.83	.	147.5	0.2
05/11/2014 12:30	0.88	0.02	0.86	.	147.75	.
05/11/2014 12:45	0.84	0.02	0.82	.	148	.
05/11/2014 13:00	0.83	0.02	0.81	.	148.25	.
05/11/2014 13:15	0.73	0.02	0.71	.	148.5	.
05/11/2014 13:30	0.72	0.02	0.70	.	148.75	.
05/11/2014 13:45	0.76	0.02	0.74	0.2	149	.
05/11/2014 14:00	0.74	0.02	0.72	.	149.25	.
05/11/2014 14:15	0.80	0.02	0.78	0.2	149.5	.
05/11/2014 14:30	0.71	0.02	0.69	.	149.75	.
05/11/2014 14:45	0.60	0.02	0.58	.	150	.
05/11/2014 15:00	0.73	0.02	0.71	.	150.25	.
05/11/2014 15:15	0.70	0.02	0.68	.	150.5	.
05/11/2014 15:30	0.80	0.02	0.78	.	150.75	.
05/11/2014 15:45	0.70	0.02	0.68	.	151	.
05/11/2014 16:00	0.75	0.02	0.73	.	151.25	.
05/11/2014 16:15	0.78	0.02	0.76	.	151.5	.
05/11/2014 16:30	0.66	0.02	0.64	.	151.75	.
05/11/2014 16:45	0.54	0.02	0.52	.	152	.
05/11/2014 17:00	0.69	0.02	0.67	.	152.25	.
05/11/2014 17:15	0.70	0.02	0.68	.	152.5	.
05/11/2014 17:30	0.24	0.02	0.22	.	152.75	.
05/11/2014 17:45	0.60	0.02	0.58	.	153	.
05/11/2014 18:00	0.62	0.02	0.60	.	153.25	0.2
05/11/2014 18:15	0.62	0.02	0.60	0.6	153.5	0.4
05/11/2014 18:30	0.61	0.02	0.59	1	153.75	1
05/11/2014 18:45	0.69	0.02	0.67	0.4	154	0.4
05/11/2014 19:00	0.75	0.02	0.73	0.4	154.25	0.2
05/11/2014 19:15	0.81	0.02	0.79	0.4	154.5	0.4
05/11/2014 19:30	0.78	0.02	0.76	1.4	154.75	1
05/11/2014 19:45	0.85	0.02	0.83	2.2	155	1.6
05/11/2014 20:00	1.28	0.02	1.26	1.6	155.25	0.2
05/11/2014 20:15	1.44	0.02	1.42	0.6	155.5	0.2
05/11/2014 20:30	1.48	0.02	1.46	0.4	155.75	.
05/11/2014 20:45	1.24	0.02	1.22	0.8	156	.
05/11/2014 21:00	1.15	0.02	1.13	.	156.25	0.2
05/11/2014 21:15	1.17	0.02	1.15	0.4	156.5	0.2
05/11/2014 21:30	1.15	0.02	1.13	0.2	156.75	.
05/11/2014 21:45	1.05	0.02	1.03	.	157	.
05/11/2014 22:00	1.07	0.02	1.05	.	157.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
05/11/2014 22:15	1.01	0.02	0.99	.	157.5	.
05/11/2014 22:30	0.99	0.02	0.97	.	157.75	.
05/11/2014 22:45	0.92	0.02	0.90	.	158	.
05/11/2014 23:00	0.91	0.02	0.89	.	158.25	.
05/11/2014 23:15	0.92	0.02	0.90	.	158.5	.
05/11/2014 23:30	0.91	0.02	0.89	.	158.75	.
05/11/2014 23:45	0.91	0.02	0.89	.	159	.
06/11/2014 00:00	0.86	0.02	0.84	.	159.25	.
06/11/2014 00:15	0.94	0.02	0.92	.	159.5	.
06/11/2014 00:30	0.85	0.02	0.83	.	159.75	.
06/11/2014 00:45	0.89	0.02	0.87	.	160	.
06/11/2014 01:00	0.80	0.02	0.78	.	160.25	.
06/11/2014 01:15	0.78	0.02	0.76	.	160.5	.
06/11/2014 01:30	0.82	0.02	0.80	.	160.75	.
06/11/2014 01:45	0.78	0.02	0.76	.	161	.
06/11/2014 02:00	0.67	0.02	0.65	0.2	161.25	.
06/11/2014 02:15	0.71	0.02	0.69	.	161.5	.
06/11/2014 02:30	0.76	0.02	0.74	.	161.75	.
06/11/2014 02:45	0.75	0.02	0.73	.	162	.
06/11/2014 03:00	0.66	0.02	0.64	.	162.25	.
06/11/2014 03:15	0.66	0.02	0.64	.	162.5	.
06/11/2014 03:30	0.66	0.02	0.64	.	162.75	.
06/11/2014 03:45	0.66	0.02	0.64	.	163	.
06/11/2014 04:00	0.65	0.02	0.63	.	163.25	.
06/11/2014 04:15	0.43	0.02	0.41	.	163.5	.
06/11/2014 04:30	0.50	0.02	0.48	.	163.75	.
06/11/2014 04:45	0.56	0.02	0.54	.	164	.
06/11/2014 05:00	0.54	0.02	0.52	.	164.25	.
06/11/2014 05:15	0.60	0.02	0.58	.	164.5	.
06/11/2014 05:30	0.55	0.02	0.53	.	164.75	.
06/11/2014 05:45	0.57	0.02	0.55	.	165	.
06/11/2014 06:00	0.50	0.02	0.48	.	165.25	.
06/11/2014 06:15	0.49	0.02	0.47	.	165.5	.
06/11/2014 06:30	0.49	0.02	0.47	.	165.75	.
06/11/2014 06:45	0.46	0.02	0.44	.	166	.
06/11/2014 07:00	0.48	0.02	0.46	.	166.25	.
06/11/2014 07:15	0.48	0.02	0.46	.	166.5	.
06/11/2014 07:30	0.45	0.02	0.43	.	166.75	.
06/11/2014 07:45	0.42	0.02	0.40	.	167	.
06/11/2014 08:00	0.41	0.02	0.39	.	167.25	.
06/11/2014 08:15	0.39	0.02	0.37	.	167.5	.
06/11/2014 08:30	0.41	0.02	0.39	.	167.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/11/2014 08:45	0.36	0.02	0.34	.	168	.
06/11/2014 09:00	0.35	0.02	0.33	.	168.25	.
06/11/2014 09:15	0.35	0.02	0.33	.	168.5	.
06/11/2014 09:30	0.33	0.02	0.31	.	168.75	.
06/11/2014 09:45	0.32	0.02	0.30	.	169	.
06/11/2014 10:00	0.30	0.02	0.28	.	169.25	.
06/11/2014 10:15	0.31	0.02	0.29	.	169.5	.
06/11/2014 10:30	0.31	0.02	0.29	.	169.75	.
06/11/2014 10:45	0.31	0.02	0.29	.	170	.
06/11/2014 11:00	0.30	0.02	0.28	.	170.25	.
06/11/2014 11:15	0.26	0.02	0.24	.	170.5	.
06/11/2014 11:30	0.26	0.02	0.24	.	170.75	.
06/11/2014 11:45	0.25	0.02	0.23	.	171	.
06/11/2014 12:00	0.26	0.02	0.24	.	171.25	.
06/11/2014 12:15	0.27	0.02	0.25	.	171.5	.
06/11/2014 12:30	0.25	0.02	0.23	.	171.75	.
06/11/2014 12:45	0.24	0.02	0.22	.	172	.
06/11/2014 13:00	0.23	0.02	0.21	.	172.25	.
06/11/2014 13:15	0.22	0.02	0.20	.	172.5	.
06/11/2014 13:30	0.22	0.02	0.20	.	172.75	.
06/11/2014 13:45	0.22	0.02	0.20	.	173	.
06/11/2014 14:00	0.20	0.02	0.18	.	173.25	.
06/11/2014 14:15	0.19	0.02	0.17	.	173.5	.
06/11/2014 14:30	0.18	0.02	0.16	.	173.75	.
06/11/2014 14:45	0.18	0.02	0.16	.	174	.
06/11/2014 15:00	0.18	0.02	0.16	.	174.25	.
06/11/2014 15:15	0.15	0.02	0.13	.	174.5	.
06/11/2014 15:30	0.15	0.02	0.13	.	174.75	.
06/11/2014 15:45	0.15	0.02	0.13	.	175	.
06/11/2014 16:00	0.15	0.02	0.13	.	175.25	.
06/11/2014 16:15	0.16	0.02	0.14	.	175.5	.
06/11/2014 16:30	0.15	0.02	0.13	.	175.75	.
06/11/2014 16:45	0.13	0.02	0.11	.	176	.
06/11/2014 17:00	0.14	0.02	0.12	.	176.25	.
06/11/2014 17:15	0.12	0.02	0.10	.	176.5	.
06/11/2014 17:30	0.12	0.02	0.10	.	176.75	.
06/11/2014 17:45	0.11	0.02	0.09	.	177	.
06/11/2014 18:00	0.13	0.02	0.11	.	177.25	.
06/11/2014 18:15	0.13	0.02	0.11	.	177.5	.
06/11/2014 18:30	0.14	0.02	0.12	.	177.75	.
06/11/2014 18:45	0.12	0.02	0.10	.	178	.
06/11/2014 19:00	0.12	0.02	0.10	.	178.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/11/2014 19:15	0.12	0.02	0.10	.	178.5	.
06/11/2014 19:30	0.12	0.02	0.10	.	178.75	.
06/11/2014 19:45	0.12	0.02	0.10	.	179	.
06/11/2014 20:00	0.11	0.02	0.09	.	179.25	.
06/11/2014 20:15	0.11	0.02	0.09	.	179.5	.
06/11/2014 20:30	0.12	0.02	0.10	.	179.75	.
06/11/2014 20:45	0.11	0.02	0.09	.	180	.
06/11/2014 21:00	0.12	0.02	0.10	.	180.25	.
06/11/2014 21:15	0.11	0.02	0.09	.	180.5	.
06/11/2014 21:30	0.12	0.02	0.10	.	180.75	.
06/11/2014 21:45	0.11	0.02	0.09	.	181	.
06/11/2014 22:00	0.11	0.02	0.09	.	181.25	.
06/11/2014 22:15	0.11	0.02	0.09	.	181.5	.
06/11/2014 22:30	0.11	0.02	0.09	.	181.75	.
06/11/2014 22:45	0.10	0.02	0.08	.	182	.
06/11/2014 23:00	0.10	0.02	0.08	.	182.25	.
06/11/2014 23:15	0.10	0.02	0.08	.	182.5	.
06/11/2014 23:30	0.07	0.02	0.05	.	182.75	.
06/11/2014 23:45	0.10	0.02	0.08	.	183	.
07/11/2014 00:00	0.10	0.02	0.08	.	183.25	.
07/11/2014 00:15	0.10	0.02	0.08	.	183.5	.
07/11/2014 00:30	0.09	0.02	0.07	.	183.75	.
07/11/2014 00:45	0.10	0.02	0.08	.	184	.
07/11/2014 01:00	0.10	0.02	0.08	.	184.25	.
07/11/2014 01:15	0.09	0.02	0.07	.	184.5	.
07/11/2014 01:30	0.09	0.02	0.07	.	184.75	.
07/11/2014 01:45	0.10	0.02	0.08	.	185	0.2
07/11/2014 02:00	0.10	0.02	0.08	.	185.25	0.2
07/11/2014 02:15	0.10	0.02	0.08	.	185.5	.
07/11/2014 02:30	0.09	0.02	0.07	0.2	185.75	.
07/11/2014 02:45	0.09	0.02	0.07	.	186	.
07/11/2014 03:00	0.10	0.02	0.08	.	186.25	.
07/11/2014 03:15	0.10	0.02	0.08	.	186.5	.
07/11/2014 03:30	0.09	0.02	0.07	.	186.75	.
07/11/2014 03:45	0.10	0.02	0.08	.	187	.
07/11/2014 04:00	0.08	0.02	0.06	.	187.25	.
07/11/2014 04:15	0.09	0.02	0.07	.	187.5	0.2
07/11/2014 04:30	0.09	0.02	0.07	.	187.75	.
07/11/2014 04:45	0.09	0.02	0.07	.	188	.
07/11/2014 05:00	0.09	0.02	0.07	.	188.25	.
07/11/2014 05:15	0.09	0.02	0.07	0.4	188.5	0.4
07/11/2014 05:30	0.09	0.02	0.07	0.8	188.75	0.4

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
07/11/2014 05:45	0.09	0.02	0.07	0.8	189	0.4
07/11/2014 06:00	0.10	0.02	0.08	0.6	189.25	0.2
07/11/2014 06:15	0.12	0.02	0.10	0.6	189.5	0.8
07/11/2014 06:30	0.15	0.02	0.13	0.6	189.75	0.6
07/11/2014 06:45	0.16	0.02	0.14	0.4	190	1
07/11/2014 07:00	0.16	0.02	0.14	0.8	190.25	1
07/11/2014 07:15	0.18	0.02	0.16	0.8	190.5	0.8
07/11/2014 07:30	0.21	0.02	0.19	0.4	190.75	0.6
07/11/2014 07:45	0.19	0.02	0.17	0.4	191	0.4
07/11/2014 08:00	0.20	0.02	0.18	.	191.25	.
07/11/2014 08:15	0.22	0.02	0.20	.	191.5	.
07/11/2014 08:30	0.19	0.02	0.17	.	191.75	.
07/11/2014 08:45	0.18	0.02	0.16	.	192	0.6
07/11/2014 09:00	0.17	0.02	0.15	.	192.25	0.4
07/11/2014 09:15	0.15	0.02	0.13	.	192.5	.
07/11/2014 09:30	0.17	0.02	0.15	.	192.75	.
07/11/2014 09:45	0.16	0.02	0.14	.	193	.
07/11/2014 10:00	0.16	0.02	0.14	.	193.25	.
07/11/2014 10:15	0.17	0.02	0.15	.	193.5	0.2
07/11/2014 10:30	0.19	0.02	0.17	.	193.75	.
07/11/2014 10:45	0.21	0.02	0.19	0.2	194	0.2
07/11/2014 11:00	0.22	0.02	0.20	.	194.25	0.6
07/11/2014 11:15	0.24	0.02	0.22	.	194.5	0.6
07/11/2014 11:30	0.26	0.02	0.24	.	194.75	.
07/11/2014 11:45	0.26	0.02	0.24	.	195	0.2
07/11/2014 12:00	0.28	0.02	0.26	.	195.25	.
07/11/2014 12:15	0.29	0.02	0.27	.	195.5	.
07/11/2014 12:30	0.28	0.02	0.26	.	195.75	.
07/11/2014 12:45	0.29	0.02	0.27	.	196	.
07/11/2014 13:00	0.31	0.02	0.29	.	196.25	.
07/11/2014 13:15	0.33	0.02	0.31	.	196.5	.
07/11/2014 13:30	0.34	0.02	0.32	.	196.75	.
07/11/2014 13:45	0.34	0.02	0.32	.	197	.
07/11/2014 14:00	0.32	0.02	0.30	.	197.25	.
07/11/2014 14:15	0.32	0.02	0.30	.	197.5	.
07/11/2014 14:30	0.30	0.02	0.28	.	197.75	.
07/11/2014 14:45	0.32	0.02	0.30	.	198	.
07/11/2014 15:00	0.30	0.02	0.28	.	198.25	.
07/11/2014 15:15	0.34	0.02	0.32	.	198.5	.
07/11/2014 15:30	0.31	0.02	0.29	.	198.75	.
07/11/2014 15:45	0.33	0.02	0.31	.	199	.
07/11/2014 16:00	0.29	0.02	0.27	.	199.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
07/11/2014 16:15	0.29	0.02	0.27	.	199.5	.
07/11/2014 16:30	0.29	0.02	0.27	.	199.75	.
07/11/2014 16:45	0.28	0.02	0.26	.	200	.
07/11/2014 17:00	0.30	0.02	0.28	.	200.25	.
07/11/2014 17:15	0.29	0.02	0.27	.	200.5	.
07/11/2014 17:30	0.27	0.02	0.25	.	200.75	.
07/11/2014 17:45	0.26	0.02	0.24	.	201	.
07/11/2014 18:00	0.24	0.02	0.22	.	201.25	.
07/11/2014 18:15	0.23	0.02	0.21	.	201.5	.
07/11/2014 18:30	0.24	0.02	0.22	.	201.75	.
07/11/2014 18:45	0.24	0.02	0.22	.	202	.
07/11/2014 19:00	0.25	0.02	0.23	.	202.25	.
07/11/2014 19:15	0.24	0.02	0.22	.	202.5	.
07/11/2014 19:30	0.22	0.02	0.20	.	202.75	.
07/11/2014 19:45	0.26	0.02	0.24	.	203	.
07/11/2014 20:00	0.23	0.02	0.21	.	203.25	.
07/11/2014 20:15	0.20	0.02	0.18	.	203.5	.
07/11/2014 20:30	0.20	0.02	0.18	.	203.75	.
07/11/2014 20:45	0.21	0.02	0.19	.	204	.
07/11/2014 21:00	0.19	0.02	0.17	.	204.25	.
07/11/2014 21:15	0.18	0.02	0.16	.	204.5	.
07/11/2014 21:30	0.18	0.02	0.16	.	204.75	.
07/11/2014 21:45	0.15	0.02	0.13	.	205	.
07/11/2014 22:00	0.17	0.02	0.15	.	205.25	.
07/11/2014 22:15	0.15	0.02	0.13	.	205.5	.
07/11/2014 22:30	0.16	0.02	0.14	.	205.75	.
07/11/2014 22:45	0.16	0.02	0.14	.	206	.
07/11/2014 23:00	0.16	0.02	0.14	.	206.25	.
07/11/2014 23:15	0.16	0.02	0.14	.	206.5	.
07/11/2014 23:30	0.18	0.02	0.16	.	206.75	.
07/11/2014 23:45	0.16	0.02	0.14	.	207	.
08/11/2014 00:00	0.14	0.02	0.12	.	207.25	.
08/11/2014 00:15	0.14	0.02	0.12	.	207.5	.
08/11/2014 00:30	0.14	0.02	0.12	.	207.75	.
08/11/2014 00:45	0.12	0.02	0.10	.	208	.
08/11/2014 01:00	0.12	0.02	0.10	.	208.25	.
08/11/2014 01:15	0.12	0.02	0.10	.	208.5	.
08/11/2014 01:30	0.11	0.02	0.09	.	208.75	.
08/11/2014 01:45	0.12	0.02	0.10	.	209	.
08/11/2014 02:00	0.12	0.02	0.10	.	209.25	.
08/11/2014 02:15	0.12	0.02	0.10	.	209.5	.
08/11/2014 02:30	0.10	0.02	0.08	.	209.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/11/2014 02:45	0.10	0.02	0.08	.	210	.
08/11/2014 03:00	0.11	0.02	0.09	.	210.25	.
08/11/2014 03:15	0.10	0.02	0.08	.	210.5	.
08/11/2014 03:30	0.10	0.02	0.08	.	210.75	.
08/11/2014 03:45	0.12	0.02	0.10	.	211	.
08/11/2014 04:00	0.10	0.02	0.08	.	211.25	.
08/11/2014 04:15	0.10	0.02	0.08	.	211.5	.
08/11/2014 04:30	0.10	0.02	0.08	.	211.75	.
08/11/2014 04:45	0.13	0.02	0.11	.	212	.
08/11/2014 05:00	0.10	0.02	0.08	.	212.25	.
08/11/2014 05:15	0.09	0.02	0.07	.	212.5	.
08/11/2014 05:30	0.11	0.02	0.09	.	212.75	.
08/11/2014 05:45	0.10	0.02	0.08	.	213	.
08/11/2014 06:00	0.09	0.02	0.07	.	213.25	.
08/11/2014 06:15	0.10	0.02	0.08	.	213.5	.
08/11/2014 06:30	0.10	0.02	0.08	.	213.75	.
08/11/2014 06:45	0.09	0.02	0.07	.	214	.
08/11/2014 07:00	0.09	0.02	0.07	.	214.25	.
08/11/2014 07:15	0.10	0.02	0.08	.	214.5	.
08/11/2014 07:30	0.09	0.02	0.07	.	214.75	.
08/11/2014 07:45	0.10	0.02	0.08	.	215	.
08/11/2014 08:00	0.09	0.02	0.07	.	215.25	.
08/11/2014 08:15	0.09	0.02	0.07	.	215.5	.
08/11/2014 08:30	0.09	0.02	0.07	.	215.75	.
08/11/2014 08:45	0.09	0.02	0.07	.	216	.
08/11/2014 09:00	0.09	0.02	0.07	.	216.25	.
08/11/2014 09:15	0.10	0.02	0.08	.	216.5	.
08/11/2014 09:30	0.10	0.02	0.08	.	216.75	.
08/11/2014 09:45	0.11	0.02	0.09	.	217	.
08/11/2014 10:00	0.10	0.02	0.08	.	217.25	.
08/11/2014 10:15	0.11	0.02	0.09	.	217.5	.
08/11/2014 10:30	0.10	0.02	0.08	.	217.75	.
08/11/2014 10:45	0.09	0.02	0.07	.	218	.
08/11/2014 11:00	0.09	0.02	0.07	.	218.25	.
08/11/2014 11:15	0.09	0.02	0.07	.	218.5	.
08/11/2014 11:30	0.10	0.02	0.08	.	218.75	.
08/11/2014 11:45	0.09	0.02	0.07	.	219	.
08/11/2014 12:00	0.08	0.02	0.06	.	219.25	.
08/11/2014 12:15	0.08	0.02	0.06	.	219.5	.
08/11/2014 12:30	0.08	0.02	0.06	.	219.75	.
08/11/2014 12:45	0.07	0.02	0.05	.	220	.
08/11/2014 13:00	0.08	0.02	0.06	.	220.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/11/2014 13:15	0.08	0.02	0.06	.	220.5	.
08/11/2014 13:30	0.08	0.02	0.06	.	220.75	.
08/11/2014 13:45	0.07	0.02	0.05	.	221	.
08/11/2014 14:00	0.08	0.02	0.06	.	221.25	.
08/11/2014 14:15	0.07	0.02	0.05	.	221.5	.
08/11/2014 14:30	0.08	0.02	0.06	.	221.75	.
08/11/2014 14:45	0.07	0.02	0.05	.	222	.
08/11/2014 15:00	0.07	0.02	0.05	.	222.25	.
08/11/2014 15:15	0.07	0.02	0.05	.	222.5	.
08/11/2014 15:30	0.06	0.02	0.04	.	222.75	.
08/11/2014 15:45	0.06	0.02	0.04	.	223	.
08/11/2014 16:00	0.07	0.02	0.05	.	223.25	.
08/11/2014 16:15	0.06	0.02	0.04	.	223.5	.
08/11/2014 16:30	0.06	0.02	0.04	.	223.75	.
08/11/2014 16:45	0.07	0.02	0.05	.	224	.
08/11/2014 17:00	0.07	0.02	0.05	.	224.25	.
08/11/2014 17:15	0.07	0.02	0.05	.	224.5	.
08/11/2014 17:30	0.07	0.02	0.05	.	224.75	.
08/11/2014 17:45	0.08	0.02	0.06	.	225	.
08/11/2014 18:00	0.06	0.02	0.04	.	225.25	.
08/11/2014 18:15	0.07	0.02	0.05	.	225.5	.
08/11/2014 18:30	0.06	0.02	0.04	.	225.75	.
08/11/2014 18:45	0.07	0.02	0.05	.	226	.
08/11/2014 19:00	0.06	0.02	0.04	.	226.25	.
08/11/2014 19:15	0.06	0.02	0.04	.	226.5	.
08/11/2014 19:30	0.07	0.02	0.05	.	226.75	.
08/11/2014 19:45	0.06	0.02	0.04	.	227	.
08/11/2014 20:00	0.06	0.02	0.04	.	227.25	.
08/11/2014 20:15	0.06	0.02	0.04	.	227.5	.
08/11/2014 20:30	0.06	0.02	0.04	.	227.75	.
08/11/2014 20:45	0.06	0.02	0.04	.	228	.
08/11/2014 21:00	0.06	0.02	0.04	.	228.25	.
08/11/2014 21:15	0.05	0.02	0.03	.	228.5	.
08/11/2014 21:30	0.06	0.02	0.04	.	228.75	.
08/11/2014 21:45	0.06	0.02	0.04	.	229	2
08/11/2014 22:00	0.07	0.02	0.05	.	229.25	.
08/11/2014 22:15	0.07	0.02	0.05	0.2	229.5	.
08/11/2014 22:30	0.06	0.02	0.04	.	229.75	0.2
08/11/2014 22:45	0.06	0.02	0.04	.	230	.
08/11/2014 23:00	0.07	0.02	0.05	.	230.25	0.2
08/11/2014 23:15	0.07	0.02	0.05	0.2	230.5	0.2
08/11/2014 23:30	0.07	0.02	0.05	0.8	230.75	.

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
08/11/2014 23:45	0.07	0.02	0.05	0.8	231	1
09/11/2014 00:00	0.09	0.02	0.07	1	231.25	.
09/11/2014 00:15	0.09	0.02	0.07	1.2	231.5	0.4
09/11/2014 00:30	0.14	0.02	0.12	0.2	231.75	0.4
09/11/2014 00:45	0.15	0.02	0.13	0.2	232	0.6
09/11/2014 01:00	0.15	0.02	0.13	1.4	232.25	0.2
09/11/2014 01:15	0.13	0.02	0.11	.	232.5	0.6
09/11/2014 01:30	0.15	0.02	0.13	0.4	232.75	0.2
09/11/2014 01:45	0.16	0.02	0.14	0.6	233	0.4
09/11/2014 02:00	0.14	0.02	0.12	0.2	233.25	.
09/11/2014 02:15	0.15	0.02	0.13	.	233.5	.
09/11/2014 02:30	0.14	0.02	0.12	.	233.75	0.2
09/11/2014 02:45	0.15	0.02	0.13	.	234	.
09/11/2014 03:00	0.13	0.02	0.11	0.6	234.25	0.2
09/11/2014 03:15	0.12	0.02	0.10	.	234.5	.
09/11/2014 03:30	0.11	0.02	0.09	.	234.75	0.2
09/11/2014 03:45	0.13	0.02	0.11	.	235	1.4
09/11/2014 04:00	0.12	0.02	0.10	.	235.25	0.6
09/11/2014 04:15	0.12	0.02	0.10	0.2	235.5	0.6
09/11/2014 04:30	0.06	0.02	0.04	.	235.75	0.4
09/11/2014 04:45	0.12	0.02	0.10	.	236	0.4
09/11/2014 05:00	0.12	0.02	0.10	.	236.25	.
09/11/2014 05:15	0.12	0.02	0.10	.	236.5	0.6
09/11/2014 05:30	0.17	0.02	0.15	.	236.75	.
09/11/2014 05:45	0.18	0.02	0.16	.	237	.
09/11/2014 06:00	0.17	0.02	0.15	.	237.25	.
09/11/2014 06:15	0.18	0.02	0.16	.	237.5	.
09/11/2014 06:30	0.21	0.02	0.19	.	237.75	.
09/11/2014 06:45	0.21	0.02	0.19	.	238	0.4
09/11/2014 07:00	0.20	0.02	0.18	0.2	238.25	0.8
09/11/2014 07:15	0.23	0.02	0.21	.	238.5	0.2
09/11/2014 07:30	0.24	0.02	0.22	0.4	238.75	0.6
09/11/2014 07:45	0.22	0.02	0.20	0.4	239	1
09/11/2014 08:00	0.23	0.02	0.21	0.8	239.25	0.4
09/11/2014 08:15	0.26	0.02	0.24	0.2	239.5	0.8
09/11/2014 08:30	0.30	0.02	0.28	0.8	239.75	1.2
09/11/2014 08:45	0.28	0.02	0.26	1.6	240	0.6
09/11/2014 09:00	0.30	0.02	0.28	0.6	240.25	0.6
09/11/2014 09:15	0.41	0.02	0.39	0.4	240.5	.
09/11/2014 09:30	0.40	0.02	0.38	.	240.75	0.2
09/11/2014 09:45	0.46	0.02	0.44	.	241	.
09/11/2014 10:00	0.44	0.02	0.42	0.2	241.25	0.4

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
09/11/2014 10:15	0.39	0.02	0.37	0.2	241.5	.
09/11/2014 10:30	0.37	0.02	0.35	.	241.75	.
09/11/2014 10:45	0.41	0.02	0.39	.	242	.
09/11/2014 11:00	0.42	0.02	0.40	.	242.25	.
09/11/2014 11:15	0.39	0.02	0.37	.	242.5	.
09/11/2014 11:30	0.41	0.02	0.39	.	242.75	.
09/11/2014 11:45	0.37	0.02	0.35	.	243	.
09/11/2014 12:00	0.38	0.02	0.36	.	243.25	.
09/11/2014 12:15	0.37	0.02	0.35	.	243.5	.
09/11/2014 12:30	0.39	0.02	0.37	.	243.75	.
09/11/2014 12:45	0.37	0.02	0.35	.	244	.
09/11/2014 13:00	0.41	0.02	0.39	.	244.25	.
09/11/2014 13:15	0.42	0.02	0.40	.	244.5	.
09/11/2014 13:30	0.44	0.02	0.42	.	244.75	.
09/11/2014 13:45	0.45	0.02	0.43	.	245	.
09/11/2014 14:00	0.45	0.02	0.43	.	245.25	.
09/11/2014 14:15	0.47	0.02	0.45	.	245.5	.
09/11/2014 14:30	0.44	0.02	0.42	.	245.75	.
09/11/2014 14:45	0.42	0.02	0.40	.	246	.
09/11/2014 15:00	0.44	0.02	0.42	.	246.25	.
09/11/2014 15:15	0.40	0.02	0.38	.	246.5	.
09/11/2014 15:30	0.40	0.02	0.38	.	246.75	.
09/11/2014 15:45	0.38	0.02	0.36	.	247	.
09/11/2014 16:00	0.42	0.02	0.40	.	247.25	.
09/11/2014 16:15	0.41	0.02	0.39	.	247.5	.
09/11/2014 16:30	0.39	0.02	0.37	.	247.75	.
09/11/2014 16:45	0.40	0.02	0.38	.	248	.
09/11/2014 17:00	0.39	0.02	0.37	.	248.25	.
09/11/2014 17:15	0.38	0.02	0.36	.	248.5	.
09/11/2014 17:30	0.37	0.02	0.35	.	248.75	.
09/11/2014 17:45	0.30	0.02	0.28	.	249	.
09/11/2014 18:00	0.32	0.02	0.30	.	249.25	.
09/11/2014 18:15	0.33	0.02	0.31	.	249.5	.
09/11/2014 18:30	0.33	0.02	0.31	.	249.75	.
09/11/2014 18:45	0.32	0.02	0.30	.	250	.
09/11/2014 19:00	0.34	0.02	0.32	.	250.25	.
09/11/2014 19:15	0.30	0.02	0.28	.	250.5	.
09/11/2014 19:30	0.32	0.02	0.30	.	250.75	.
09/11/2014 19:45	0.31	0.02	0.29	.	251	.
09/11/2014 20:00	0.27	0.02	0.25	.	251.25	.
09/11/2014 20:15	0.28	0.02	0.26	.	251.5	.
09/11/2014 20:30	0.29	0.02	0.27	.	251.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
09/11/2014 20:45	0.28	0.02	0.26	.	252	.
09/11/2014 21:00	0.26	0.02	0.24	.	252.25	.
09/11/2014 21:15	0.28	0.02	0.26	.	252.5	.
09/11/2014 21:30	0.26	0.02	0.24	.	252.75	.
09/11/2014 21:45	0.23	0.02	0.21	.	253	.
09/11/2014 22:00	0.22	0.02	0.20	.	253.25	.
09/11/2014 22:15	0.21	0.02	0.19	.	253.5	.
09/11/2014 22:30	0.22	0.02	0.20	.	253.75	.
09/11/2014 22:45	0.23	0.02	0.21	.	254	.
09/11/2014 23:00	0.21	0.02	0.19	.	254.25	.
09/11/2014 23:15	0.21	0.02	0.19	.	254.5	.
09/11/2014 23:30	0.21	0.02	0.19	.	254.75	.
09/11/2014 23:45	0.18	0.02	0.16	.	255	.
10/11/2014 00:00	0.18	0.02	0.16	.	255.25	.
10/11/2014 00:15	0.15	0.02	0.13	.	255.5	.
10/11/2014 00:30	0.17	0.02	0.15	.	255.75	.
10/11/2014 00:45	0.17	0.02	0.15	.	256	.
10/11/2014 01:00	0.16	0.02	0.14	.	256.25	.
10/11/2014 01:15	0.16	0.02	0.14	.	256.5	.
10/11/2014 01:30	0.15	0.02	0.13	.	256.75	.
10/11/2014 01:45	0.15	0.02	0.13	.	257	.
10/11/2014 02:00	0.15	0.02	0.13	.	257.25	.
10/11/2014 02:15	0.12	0.02	0.10	.	257.5	.
10/11/2014 02:30	0.13	0.02	0.11	.	257.75	.
10/11/2014 02:45	0.13	0.02	0.11	.	258	.
10/11/2014 03:00	0.14	0.02	0.12	.	258.25	.
10/11/2014 03:15	0.12	0.02	0.10	.	258.5	.
10/11/2014 03:30	0.11	0.02	0.09	.	258.75	.
10/11/2014 03:45	0.11	0.02	0.09	.	259	.
10/11/2014 04:00	0.12	0.02	0.10	.	259.25	.
10/11/2014 04:15	0.11	0.02	0.09	.	259.5	.
10/11/2014 04:30	0.11	0.02	0.09	.	259.75	.
10/11/2014 04:45	0.11	0.02	0.09	.	260	.
10/11/2014 05:00	0.11	0.02	0.09	.	260.25	.
10/11/2014 05:15	0.11	0.02	0.09	.	260.5	.
10/11/2014 05:30	0.12	0.02	0.10	.	260.75	.
10/11/2014 05:45	0.11	0.02	0.09	.	261	.
10/11/2014 06:00	0.11	0.02	0.09	.	261.25	.
10/11/2014 06:15	0.10	0.02	0.08	.	261.5	.
10/11/2014 06:30	0.09	0.02	0.07	.	261.75	.
10/11/2014 06:45	0.11	0.02	0.09	.	262	.
10/11/2014 07:00	0.11	0.02	0.09	.	262.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
10/11/2014 07:15	0.10	0.02	0.08	.	262.5	.
10/11/2014 07:30	0.10	0.02	0.08	.	262.75	.
10/11/2014 07:45	0.11	0.02	0.09	.	263	.
10/11/2014 08:00	0.11	0.02	0.09	.	263.25	.
10/11/2014 08:15	0.11	0.02	0.09	.	263.5	.
10/11/2014 08:30	0.10	0.02	0.08	.	263.75	.
10/11/2014 08:45	0.12	0.02	0.10	.	264	.
10/11/2014 09:00	0.12	0.02	0.10	.	264.25	.
10/11/2014 09:15	0.12	0.02	0.10	.	264.5	.
10/11/2014 09:30	0.12	0.02	0.10	.	264.75	.
10/11/2014 09:45	0.12	0.02	0.10	.	265	.
10/11/2014 10:00	0.10	0.02	0.08	.	265.25	.
10/11/2014 10:15	0.10	0.02	0.08	.	265.5	.
10/11/2014 10:30	0.12	0.02	0.10	.	265.75	.
10/11/2014 10:45	0.12	0.02	0.10	.	266	.
10/11/2014 11:00	0.10	0.02	0.08	.	266.25	.
10/11/2014 11:15	0.12	0.02	0.10	.	266.5	.
10/11/2014 11:30	0.11	0.02	0.09	.	266.75	.
10/11/2014 11:45	0.11	0.02	0.09	.	267	.
10/11/2014 12:00	0.10	0.02	0.08	.	267.25	.
10/11/2014 12:15	0.10	0.02	0.08	.	267.5	.
10/11/2014 12:30	0.10	0.02	0.08	.	267.75	.
10/11/2014 12:45	0.10	0.02	0.08	.	268	.
10/11/2014 13:00	0.11	0.02	0.09	.	268.25	.
10/11/2014 13:15	0.10	0.02	0.08	.	268.5	.
10/11/2014 13:30	0.10	0.02	0.08	.	268.75	.
10/11/2014 13:45	0.10	0.02	0.08	.	269	.
10/11/2014 14:00	0.10	0.02	0.08	.	269.25	.
10/11/2014 14:15	0.09	0.02	0.07	.	269.5	.
10/11/2014 14:30	0.10	0.02	0.08	.	269.75	.
10/11/2014 14:45	0.10	0.02	0.08	.	270	.
10/11/2014 15:00	0.10	0.02	0.08	.	270.25	.
10/11/2014 15:15	0.09	0.02	0.07	.	270.5	.
10/11/2014 15:30	0.08	0.02	0.06	.	270.75	.
10/11/2014 15:45	0.10	0.02	0.08	.	271	.
10/11/2014 16:00	0.09	0.02	0.07	.	271.25	.
10/11/2014 16:15	0.10	0.02	0.08	.	271.5	.
10/11/2014 16:30	0.09	0.02	0.07	.	271.75	.
10/11/2014 16:45	0.09	0.02	0.07	.	272	.
10/11/2014 17:00	0.08	0.02	0.06	.	272.25	.
10/11/2014 17:15	0.08	0.02	0.06	.	272.5	.
10/11/2014 17:30	0.08	0.02	0.06	.	272.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
10/11/2014 17:45	0.09	0.02	0.07	.	273	.
10/11/2014 18:00	0.09	0.02	0.07	.	273.25	.
10/11/2014 18:15	0.09	0.02	0.07	.	273.5	.
10/11/2014 18:30	0.08	0.02	0.06	.	273.75	.
10/11/2014 18:45	0.08	0.02	0.06	.	274	.
10/11/2014 19:00	0.08	0.02	0.06	.	274.25	.
10/11/2014 19:15	0.07	0.02	0.05	.	274.5	.
10/11/2014 19:30	0.08	0.02	0.06	.	274.75	.
10/11/2014 19:45	0.07	0.02	0.05	.	275	.
10/11/2014 20:00	0.07	0.02	0.05	.	275.25	.
10/11/2014 20:15	0.08	0.02	0.06	.	275.5	.
10/11/2014 20:30	0.07	0.02	0.05	.	275.75	.
10/11/2014 20:45	0.07	0.02	0.05	.	276	.
10/11/2014 21:00	0.07	0.02	0.05	.	276.25	.
10/11/2014 21:15	0.07	0.02	0.05	.	276.5	.
10/11/2014 21:30	0.07	0.02	0.05	.	276.75	.
10/11/2014 21:45	0.07	0.02	0.05	.	277	.
10/11/2014 22:00	0.06	0.02	0.04	.	277.25	.
10/11/2014 22:15	0.06	0.02	0.04	.	277.5	.
10/11/2014 22:30	0.06	0.02	0.04	.	277.75	.
10/11/2014 22:45	0.07	0.02	0.05	.	278	.
10/11/2014 23:00	0.06	0.02	0.04	.	278.25	.
10/11/2014 23:15	0.05	0.02	0.03	.	278.5	.
10/11/2014 23:30	0.05	0.02	0.03	.	278.75	.
10/11/2014 23:45	0.06	0.02	0.04	.	279	.
11/11/2014 00:00	0.06	0.02	0.04	.	279.25	.
11/11/2014 00:15	0.06	0.02	0.04	.	279.5	.
11/11/2014 00:30	0.06	0.02	0.04	.	279.75	.
11/11/2014 00:45	0.06	0.02	0.04	.	280	.
11/11/2014 01:00	0.05	0.02	0.03	.	280.25	.
11/11/2014 01:15	0.05	0.02	0.03	.	280.5	.
11/11/2014 01:30	0.05	0.02	0.03	.	280.75	.
11/11/2014 01:45	0.05	0.02	0.03	.	281	.
11/11/2014 02:00	0.05	0.02	0.03	.	281.25	.
11/11/2014 02:15	0.04	0.02	0.02	.	281.5	.
11/11/2014 02:30	0.04	0.02	0.02	.	281.75	.
11/11/2014 02:45	0.04	0.02	0.02	.	282	.
11/11/2014 03:00	0.04	0.02	0.02	.	282.25	.
11/11/2014 03:15	0.04	0.02	0.02	.	282.5	.
11/11/2014 03:30	0.04	0.02	0.02	.	282.75	.
11/11/2014 03:45	0.04	0.02	0.02	.	283	.
11/11/2014 04:00	0.04	0.02	0.02	.	283.25	.

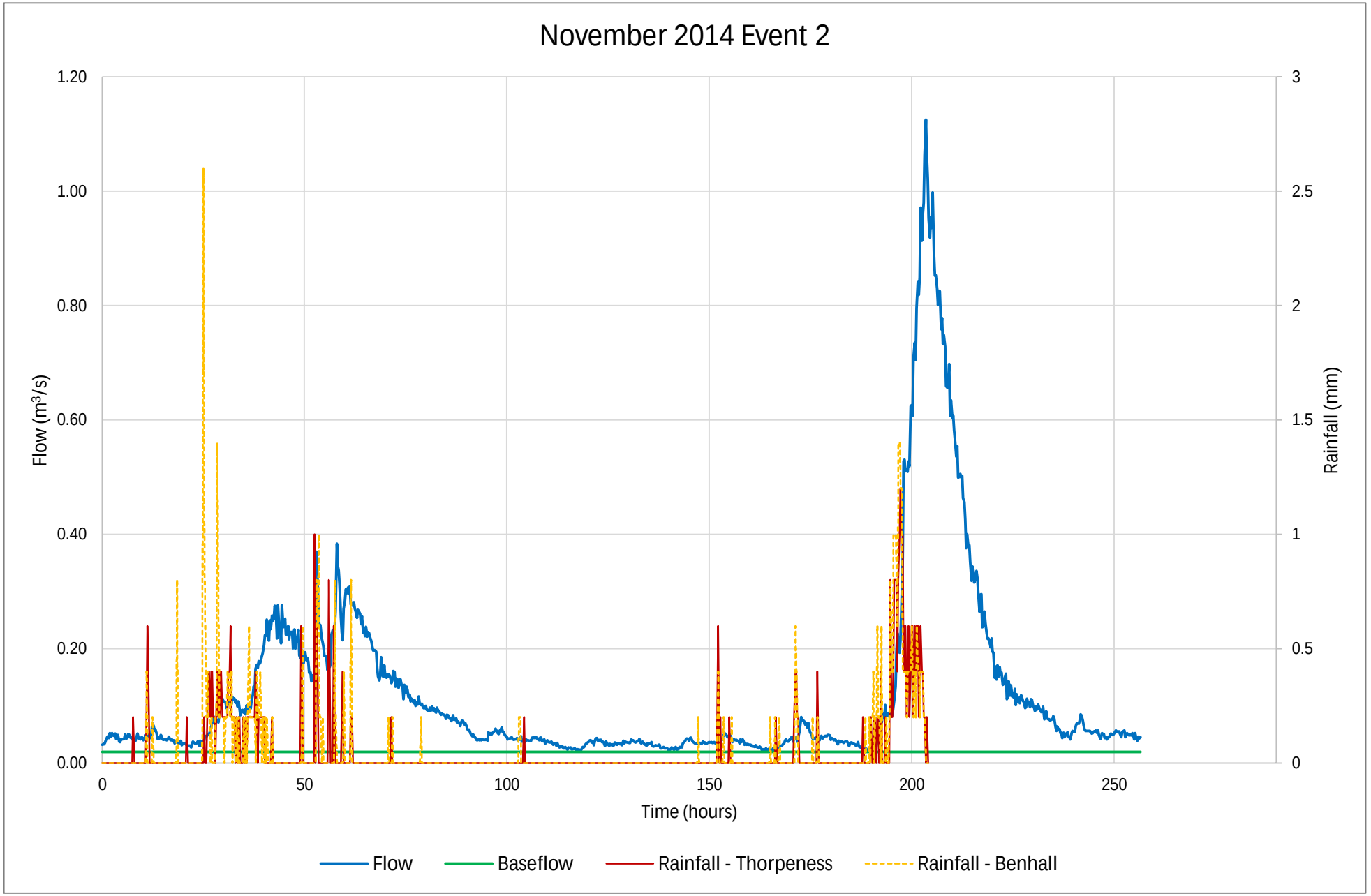
Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
11/11/2014 04:15	0.04	0.02	0.02	.	283.5	.
11/11/2014 04:30	0.04	0.02	0.02	.	283.75	.
11/11/2014 04:45	0.04	0.02	0.02	.	284	.
11/11/2014 05:00	0.04	0.02	0.02	.	284.25	.
11/11/2014 05:15	0.04	0.02	0.02	.	284.5	.
11/11/2014 05:30	0.04	0.02	0.02	.	284.75	.
11/11/2014 05:45	0.04	0.02	0.02	.	285	.
11/11/2014 06:00	0.04	0.02	0.02	.	285.25	.
11/11/2014 06:15	0.04	0.02	0.02	.	285.5	.
11/11/2014 06:30	0.04	0.02	0.02	.	285.75	.
11/11/2014 06:45	0.04	0.02	0.02	.	286	.
11/11/2014 07:00	0.04	0.02	0.02	.	286.25	.
11/11/2014 07:15	0.04	0.02	0.02	.	286.5	.
11/11/2014 07:30	0.04	0.02	0.02	.	286.75	.
11/11/2014 07:45	0.04	0.02	0.02	.	287	.
11/11/2014 08:00	0.04	0.02	0.02	.	287.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event


November 2014 Event 2
1.20
1.00
0.80
0.60
0.40
0.20
0.00
Flow (m³/s)
3
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
50
100
150
200
250
Time (hours)
Flow
Baseflow
Rainfall - Thorpeness
Rainfall - Benhall

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
15/11/2014 09:00	0.03	0.02	0.01	.	0	.
15/11/2014 09:15	0.03	0.02	0.01	.	0.25	.
15/11/2014 09:30	0.03	0.02	0.01	.	0.5	.
15/11/2014 09:45	0.03	0.02	0.01	.	0.75	.
15/11/2014 10:00	0.04	0.02	0.02	.	1	.
15/11/2014 10:15	0.04	0.02	0.02	.	1.25	.
15/11/2014 10:30	0.05	0.02	0.03	.	1.5	.
15/11/2014 10:45	0.04	0.02	0.02	.	1.75	.
15/11/2014 11:00	0.05	0.02	0.03	.	2	.
15/11/2014 11:15	0.05	0.02	0.03	.	2.25	.
15/11/2014 11:30	0.05	0.02	0.03	.	2.5	.
15/11/2014 11:45	0.05	0.02	0.03	.	2.75	.
15/11/2014 12:00	0.05	0.02	0.03	.	3	.
15/11/2014 12:15	0.05	0.02	0.03	.	3.25	.
15/11/2014 12:30	0.04	0.02	0.02	.	3.5	.
15/11/2014 12:45	0.05	0.02	0.03	.	3.75	.
15/11/2014 13:00	0.05	0.02	0.03	.	4	.
15/11/2014 13:15	0.04	0.02	0.02	.	4.25	.
15/11/2014 13:30	0.04	0.02	0.02	.	4.5	.
15/11/2014 13:45	0.04	0.02	0.02	.	4.75	.
15/11/2014 14:00	0.04	0.02	0.02	.	5	.
15/11/2014 14:15	0.04	0.02	0.02	.	5.25	.
15/11/2014 14:30	0.04	0.02	0.02	.	5.5	.
15/11/2014 14:45	0.05	0.02	0.03	.	5.75	.
15/11/2014 15:00	0.04	0.02	0.02	.	6	.
15/11/2014 15:15	0.04	0.02	0.02	.	6.25	.
15/11/2014 15:30	0.05	0.02	0.03	.	6.5	.
15/11/2014 15:45	0.05	0.02	0.03	.	6.75	.
15/11/2014 16:00	0.04	0.02	0.02	.	7	.
15/11/2014 16:15	0.04	0.02	0.02	.	7.25	.
15/11/2014 16:30	0.05	0.02	0.03	.	7.5	.
15/11/2014 16:45	0.04	0.02	0.02	0.2	7.75	.
15/11/2014 17:00	0.04	0.02	0.02	.	8	.
15/11/2014 17:15	0.04	0.02	0.02	.	8.25	.
15/11/2014 17:30	0.04	0.02	0.02	.	8.5	.
15/11/2014 17:45	0.05	0.02	0.03	.	8.75	.
15/11/2014 18:00	0.04	0.02	0.02	.	9	.
15/11/2014 18:15	0.04	0.02	0.02	.	9.25	.
15/11/2014 18:30	0.04	0.02	0.02	.	9.5	.
15/11/2014 18:45	0.04	0.02	0.02	.	9.75	.
15/11/2014 19:00	0.04	0.02	0.02	.	10	.
15/11/2014 19:15	0.04	0.02	0.02	.	10.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

Thorpeness	
Area (km^2)	5.04
Total Rain (P) mm	44.4
Time Interval (hour)	0.25
Percentage Runoff	43%

Benhall	
Area (km^2)	5.04
Total Rain (P) mm	51.2
Time Interval (hour)	0.25
Percentage Runoff	37%

Average PR	40%

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
15/11/2014 19:30	0.04	0.02	0.02	.	10.5	.
15/11/2014 19:45	0.05	0.02	0.03	.	10.75	.
15/11/2014 20:00	0.05	0.02	0.03	0.2	11	0.4
15/11/2014 20:15	0.04	0.02	0.02	0.6	11.25	.
15/11/2014 20:30	0.05	0.02	0.03	0.4	11.5	.
15/11/2014 20:45	0.05	0.02	0.03	.	11.75	.
15/11/2014 21:00	0.04	0.02	0.02	.	12	.
15/11/2014 21:15	0.05	0.02	0.03	.	12.25	.
15/11/2014 21:30	0.07	0.02	0.05	.	12.5	0.2
15/11/2014 21:45	0.06	0.02	0.04	.	12.75	.
15/11/2014 22:00	0.06	0.02	0.04	.	13	.
15/11/2014 22:15	0.06	0.02	0.04	.	13.25	.
15/11/2014 22:30	0.05	0.02	0.03	.	13.5	.
15/11/2014 22:45	0.04	0.02	0.02	.	13.75	.
15/11/2014 23:00	0.04	0.02	0.02	.	14	.
15/11/2014 23:15	0.04	0.02	0.02	.	14.25	.
15/11/2014 23:30	0.05	0.02	0.03	.	14.5	.
15/11/2014 23:45	0.05	0.02	0.03	.	14.75	.
16/11/2014 00:00	0.04	0.02	0.02	.	15	.
16/11/2014 00:15	0.04	0.02	0.02	.	15.25	.
16/11/2014 00:30	0.04	0.02	0.02	.	15.5	.
16/11/2014 00:45	0.04	0.02	0.02	.	15.75	.
16/11/2014 01:00	0.04	0.02	0.02	.	16	.
16/11/2014 01:15	0.04	0.02	0.02	.	16.25	.
16/11/2014 01:30	0.05	0.02	0.03	.	16.5	.
16/11/2014 01:45	0.04	0.02	0.02	.	16.75	.
16/11/2014 02:00	0.04	0.02	0.02	.	17	.
16/11/2014 02:15	0.04	0.02	0.02	.	17.25	.
16/11/2014 02:30	0.04	0.02	0.02	.	17.5	.
16/11/2014 02:45	0.04	0.02	0.02	.	17.75	.
16/11/2014 03:00	0.03	0.02	0.01	.	18	.
16/11/2014 03:15	0.04	0.02	0.02	.	18.25	.
16/11/2014 03:30	0.04	0.02	0.02	.	18.5	0.8
16/11/2014 03:45	0.04	0.02	0.02	.	18.75	.
16/11/2014 04:00	0.03	0.02	0.01	.	19	.
16/11/2014 04:15	0.03	0.02	0.01	.	19.25	.
16/11/2014 04:30	0.04	0.02	0.02	.	19.5	.
16/11/2014 04:45	0.03	0.02	0.01	.	19.75	.
16/11/2014 05:00	0.03	0.02	0.01	.	20	.
16/11/2014 05:15	0.04	0.02	0.02	.	20.25	.
16/11/2014 05:30	0.03	0.02	0.01	.	20.5	.
16/11/2014 05:45	0.03	0.02	0.01	.	20.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
16/11/2014 06:00	0.03	0.02	0.01	0.2	21	.
16/11/2014 06:15	0.03	0.02	0.01	.	21.25	.
16/11/2014 06:30	0.03	0.02	0.01	.	21.5	.
16/11/2014 06:45	0.03	0.02	0.01	.	21.75	.
16/11/2014 07:00	0.03	0.02	0.01	.	22	.
16/11/2014 07:15	0.04	0.02	0.02	.	22.25	.
16/11/2014 07:30	0.04	0.02	0.02	.	22.5	.
16/11/2014 07:45	0.04	0.02	0.02	.	22.75	.
16/11/2014 08:00	0.03	0.02	0.01	.	23	.
16/11/2014 08:15	0.03	0.02	0.01	.	23.25	.
16/11/2014 08:30	0.04	0.02	0.02	.	23.5	.
16/11/2014 08:45	0.04	0.02	0.02	.	23.75	.
16/11/2014 09:00	0.03	0.02	0.01	.	24	.
16/11/2014 09:15	0.04	0.02	0.02	.	24.25	.
16/11/2014 09:30	0.03	0.02	0.01	.	24.5	.
16/11/2014 09:45	0.04	0.02	0.02	.	24.75	.
16/11/2014 10:00	0.04	0.02	0.02	.	25	2.6
16/11/2014 10:15	0.04	0.02	0.02	0.2	25.25	1
16/11/2014 10:30	0.05	0.02	0.03	.	25.5	0.6
16/11/2014 10:45	0.05	0.02	0.03	.	25.75	0.2
16/11/2014 11:00	0.05	0.02	0.03	0.2	26	0.4
16/11/2014 11:15	0.05	0.02	0.03	0.4	26.25	0.2
16/11/2014 11:30	0.05	0.02	0.03	0.4	26.5	0.2
16/11/2014 11:45	0.06	0.02	0.04	0.2	26.75	.
16/11/2014 12:00	0.06	0.02	0.04	0.4	27	0.2
16/11/2014 12:15	0.07	0.02	0.05	0.4	27.25	.
16/11/2014 12:30	0.08	0.02	0.06	0.2	27.5	.
16/11/2014 12:45	0.07	0.02	0.05	0.2	27.75	.
16/11/2014 13:00	0.07	0.02	0.05	.	28	0.2
16/11/2014 13:15	0.07	0.02	0.05	0.2	28.25	0.2
16/11/2014 13:30	0.07	0.02	0.05	0.4	28.5	1.4
16/11/2014 13:45	0.07	0.02	0.05	0.2	28.75	0.6
16/11/2014 14:00	0.09	0.02	0.07	0.4	29	0.2
16/11/2014 14:15	0.09	0.02	0.07	0.2	29.25	0.2
16/11/2014 14:30	0.11	0.02	0.09	0.4	29.5	0.2
16/11/2014 14:45	0.11	0.02	0.09	0.2	29.75	0.2
16/11/2014 15:00	0.11	0.02	0.09	0.2	30	0.2
16/11/2014 15:15	0.11	0.02	0.09	0.2	30.25	.
16/11/2014 15:30	0.11	0.02	0.09	0.2	30.5	0.2
16/11/2014 15:45	0.10	0.02	0.08	0.2	30.75	0.2
16/11/2014 16:00	0.10	0.02	0.08	0.2	31	0.4
16/11/2014 16:15	0.10	0.02	0.08	0.4	31.25	0.4

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
16/11/2014 16:30	0.11	0.02	0.09	0.4	31.5	0.2
16/11/2014 16:45	0.11	0.02	0.09	0.6	31.75	0.4
16/11/2014 17:00	0.10	0.02	0.08	0.2	32	0.4
16/11/2014 17:15	0.12	0.02	0.10	0.2	32.25	.
16/11/2014 17:30	0.11	0.02	0.09	0.2	32.5	0.2
16/11/2014 17:45	0.11	0.02	0.09	0.2	32.75	0.2
16/11/2014 18:00	0.11	0.02	0.09	.	33	.
16/11/2014 18:15	0.11	0.02	0.09	0.2	33.25	0.2
16/11/2014 18:30	0.10	0.02	0.08	.	33.5	.
16/11/2014 18:45	0.11	0.02	0.09	0.2	33.75	0.2
16/11/2014 19:00	0.10	0.02	0.08	0.2	34	.
16/11/2014 19:15	0.08	0.02	0.06	.	34.25	.
16/11/2014 19:30	0.09	0.02	0.07	.	34.5	.
16/11/2014 19:45	0.09	0.02	0.07	.	34.75	.
16/11/2014 20:00	0.09	0.02	0.07	0.2	35	0.2
16/11/2014 20:15	0.09	0.02	0.07	.	35.25	.
16/11/2014 20:30	0.09	0.02	0.07	0.2	35.5	0.2
16/11/2014 20:45	0.10	0.02	0.08	.	35.75	.
16/11/2014 21:00	0.09	0.02	0.07	0.2	36	0.2
16/11/2014 21:15	0.09	0.02	0.07	0.2	36.25	0.6
16/11/2014 21:30	0.10	0.02	0.08	0.2	36.5	0.2
16/11/2014 21:45	0.09	0.02	0.07	0.2	36.75	0.2
16/11/2014 22:00	0.11	0.02	0.09	0.2	37	0.2
16/11/2014 22:15	0.12	0.02	0.10	0.2	37.25	0.2
16/11/2014 22:30	0.13	0.02	0.11	0.2	37.5	0.2
16/11/2014 22:45	0.12	0.02	0.10	0.2	37.75	0.2
16/11/2014 23:00	0.16	0.02	0.14	0.4	38	.
16/11/2014 23:15	0.17	0.02	0.15	0.2	38.25	0.4
16/11/2014 23:30	0.17	0.02	0.15	.	38.5	0.2
16/11/2014 23:45	0.18	0.02	0.16	0.2	38.75	0.2
17/11/2014 00:00	0.17	0.02	0.15	0.2	39	0.4
17/11/2014 00:15	0.18	0.02	0.16	0.2	39.25	0.2
17/11/2014 00:30	0.19	0.02	0.17	0.2	39.5	.
17/11/2014 00:45	0.19	0.02	0.17	0.2	39.75	0.2
17/11/2014 01:00	0.21	0.02	0.19	0.2	40	.
17/11/2014 01:15	0.22	0.02	0.20	.	40.25	0.2
17/11/2014 01:30	0.22	0.02	0.20	.	40.5	.
17/11/2014 01:45	0.25	0.02	0.23	.	40.75	0.2
17/11/2014 02:00	0.23	0.02	0.21	.	41	.
17/11/2014 02:15	0.21	0.02	0.19	.	41.25	.
17/11/2014 02:30	0.25	0.02	0.23	.	41.5	.
17/11/2014 02:45	0.23	0.02	0.21	.	41.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
17/11/2014 03:00	0.26	0.02	0.24	0.2	42	0.2
17/11/2014 03:15	0.25	0.02	0.23	.	42.25	.
17/11/2014 03:30	0.25	0.02	0.23	.	42.5	.
17/11/2014 03:45	0.28	0.02	0.26	.	42.75	.
17/11/2014 04:00	0.26	0.02	0.24	.	43	.
17/11/2014 04:15	0.22	0.02	0.20	.	43.25	.
17/11/2014 04:30	0.28	0.02	0.26	.	43.5	.
17/11/2014 04:45	0.23	0.02	0.21	.	43.75	.
17/11/2014 05:00	0.24	0.02	0.22	.	44	.
17/11/2014 05:15	0.21	0.02	0.19	.	44.25	.
17/11/2014 05:30	0.28	0.02	0.26	.	44.5	.
17/11/2014 05:45	0.24	0.02	0.22	.	44.75	.
17/11/2014 06:00	0.24	0.02	0.22	.	45	.
17/11/2014 06:15	0.25	0.02	0.23	.	45.25	.
17/11/2014 06:30	0.22	0.02	0.20	.	45.5	.
17/11/2014 06:45	0.22	0.02	0.20	.	45.75	.
17/11/2014 07:00	0.24	0.02	0.22	.	46	.
17/11/2014 07:15	0.22	0.02	0.20	.	46.25	.
17/11/2014 07:30	0.23	0.02	0.21	.	46.5	.
17/11/2014 07:45	0.23	0.02	0.21	.	46.75	.
17/11/2014 08:00	0.23	0.02	0.21	.	47	.
17/11/2014 08:15	0.20	0.02	0.18	.	47.25	.
17/11/2014 08:30	0.23	0.02	0.21	.	47.5	.
17/11/2014 08:45	0.20	0.02	0.18	.	47.75	.
17/11/2014 09:00	0.21	0.02	0.19	.	48	.
17/11/2014 09:15	0.22	0.02	0.20	.	48.25	.
17/11/2014 09:30	0.23	0.02	0.21	.	48.5	.
17/11/2014 09:45	0.19	0.02	0.17	.	48.75	.
17/11/2014 10:00	0.18	0.02	0.16	.	49	.
17/11/2014 10:15	0.20	0.02	0.18	0.6	49.25	.
17/11/2014 10:30	0.19	0.02	0.17	0.2	49.5	0.6
17/11/2014 10:45	0.17	0.02	0.15	.	49.75	.
17/11/2014 11:00	0.18	0.02	0.16	.	50	.
17/11/2014 11:15	0.19	0.02	0.17	.	50.25	.
17/11/2014 11:30	0.18	0.02	0.16	.	50.5	.
17/11/2014 11:45	0.18	0.02	0.16	.	50.75	.
17/11/2014 12:00	0.18	0.02	0.16	.	51	.
17/11/2014 12:15	0.16	0.02	0.14	.	51.25	.
17/11/2014 12:30	0.16	0.02	0.14	.	51.5	.
17/11/2014 12:45	0.14	0.02	0.12	.	51.75	.
17/11/2014 13:00	0.15	0.02	0.13	.	52	.
17/11/2014 13:15	0.15	0.02	0.13	.	52.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
17/11/2014 13:30	0.17	0.02	0.15	1	52.5	.
17/11/2014 13:45	0.19	0.02	0.17	.	52.75	.
17/11/2014 14:00	0.37	0.02	0.35	0.6	53	0.8
17/11/2014 14:15	0.31	0.02	0.29	0.4	53.25	0.6
17/11/2014 14:30	0.25	0.02	0.23	.	53.5	1
17/11/2014 14:45	0.24	0.02	0.22	.	53.75	0.2
17/11/2014 15:00	0.24	0.02	0.22	.	54	0.2
17/11/2014 15:15	0.22	0.02	0.20	.	54.25	.
17/11/2014 15:30	0.21	0.02	0.19	.	54.5	0.2
17/11/2014 15:45	0.20	0.02	0.18	.	54.75	.
17/11/2014 16:00	0.19	0.02	0.17	.	55	.
17/11/2014 16:15	0.19	0.02	0.17	.	55.25	.
17/11/2014 16:30	0.18	0.02	0.16	.	55.5	.
17/11/2014 16:45	0.16	0.02	0.14	.	55.75	.
17/11/2014 17:00	0.17	0.02	0.15	0.8	56	.
17/11/2014 17:15	0.17	0.02	0.15	0.4	56.25	.
17/11/2014 17:30	0.17	0.02	0.15	.	56.5	.
17/11/2014 17:45	0.23	0.02	0.21	.	56.75	.
17/11/2014 18:00	0.23	0.02	0.21	.	57	.
17/11/2014 18:15	0.23	0.02	0.21	0.6	57.25	.
17/11/2014 18:30	0.24	0.02	0.22	0.2	57.5	0.8
17/11/2014 18:45	0.27	0.02	0.25	.	57.75	0.2
17/11/2014 19:00	0.38	0.02	0.36	.	58	.
17/11/2014 19:15	0.34	0.02	0.32	.	58.25	.
17/11/2014 19:30	0.34	0.02	0.32	.	58.5	.
17/11/2014 19:45	0.31	0.02	0.29	.	58.75	.
17/11/2014 20:00	0.25	0.02	0.23	.	59	.
17/11/2014 20:15	0.23	0.02	0.21	0.2	59.25	.
17/11/2014 20:30	0.21	0.02	0.19	0.4	59.5	.
17/11/2014 20:45	0.27	0.02	0.25	.	59.75	0.4
17/11/2014 21:00	0.28	0.02	0.26	.	60	.
17/11/2014 21:15	0.30	0.02	0.28	.	60.25	.
17/11/2014 21:30	0.30	0.02	0.28	.	60.5	.
17/11/2014 21:45	0.31	0.02	0.29	.	60.75	.
17/11/2014 22:00	0.30	0.02	0.28	.	61	.
17/11/2014 22:15	0.31	0.02	0.29	.	61.25	.
17/11/2014 22:30	0.28	0.02	0.26	0.2	61.5	0.8
17/11/2014 22:45	0.28	0.02	0.26	0.2	61.75	.
17/11/2014 23:00	0.27	0.02	0.25	.	62	.
17/11/2014 23:15	0.28	0.02	0.26	.	62.25	.
17/11/2014 23:30	0.27	0.02	0.25	.	62.5	.
17/11/2014 23:45	0.26	0.02	0.24	.	62.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
18/11/2014 00:00	0.25	0.02	0.23	.	63	.
18/11/2014 00:15	0.27	0.02	0.25	.	63.25	.
18/11/2014 00:30	0.27	0.02	0.25	.	63.5	.
18/11/2014 00:45	0.26	0.02	0.24	.	63.75	.
18/11/2014 01:00	0.24	0.02	0.22	.	64	.
18/11/2014 01:15	0.26	0.02	0.24	.	64.25	.
18/11/2014 01:30	0.23	0.02	0.21	.	64.5	.
18/11/2014 01:45	0.23	0.02	0.21	.	64.75	.
18/11/2014 02:00	0.22	0.02	0.20	.	65	.
18/11/2014 02:15	0.24	0.02	0.22	.	65.25	.
18/11/2014 02:30	0.22	0.02	0.20	.	65.5	.
18/11/2014 02:45	0.23	0.02	0.21	.	65.75	.
18/11/2014 03:00	0.23	0.02	0.21	.	66	.
18/11/2014 03:15	0.22	0.02	0.20	.	66.25	.
18/11/2014 03:30	0.21	0.02	0.19	.	66.5	.
18/11/2014 03:45	0.20	0.02	0.18	.	66.75	.
18/11/2014 04:00	0.20	0.02	0.18	.	67	.
18/11/2014 04:15	0.20	0.02	0.18	.	67.25	.
18/11/2014 04:30	0.20	0.02	0.18	.	67.5	.
18/11/2014 04:45	0.19	0.02	0.17	.	67.75	.
18/11/2014 05:00	0.17	0.02	0.15	.	68	.
18/11/2014 05:15	0.15	0.02	0.13	.	68.25	.
18/11/2014 05:30	0.14	0.02	0.12	.	68.5	.
18/11/2014 05:45	0.15	0.02	0.13	.	68.75	.
18/11/2014 06:00	0.19	0.02	0.17	.	69	.
18/11/2014 06:15	0.15	0.02	0.13	.	69.25	.
18/11/2014 06:30	0.15	0.02	0.13	.	69.5	.
18/11/2014 06:45	0.17	0.02	0.15	.	69.75	.
18/11/2014 07:00	0.15	0.02	0.13	.	70	.
18/11/2014 07:15	0.15	0.02	0.13	.	70.25	.
18/11/2014 07:30	0.16	0.02	0.14	.	70.5	.
18/11/2014 07:45	0.15	0.02	0.13	.	70.75	0.2
18/11/2014 08:00	0.15	0.02	0.13	.	71	.
18/11/2014 08:15	0.15	0.02	0.13	.	71.25	.
18/11/2014 08:30	0.14	0.02	0.12	0.2	71.5	.
18/11/2014 08:45	0.14	0.02	0.12	.	71.75	0.2
18/11/2014 09:00	0.16	0.02	0.14	.	72	.
18/11/2014 09:15	0.16	0.02	0.14	.	72.25	.
18/11/2014 09:30	0.13	0.02	0.11	.	72.5	.
18/11/2014 09:45	0.15	0.02	0.13	.	72.75	.
18/11/2014 10:00	0.15	0.02	0.13	.	73	.
18/11/2014 10:15	0.13	0.02	0.11	.	73.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
18/11/2014 10:30	0.14	0.02	0.12	.	73.5	.
18/11/2014 10:45	0.15	0.02	0.13	.	73.75	.
18/11/2014 11:00	0.14	0.02	0.12	.	74	.
18/11/2014 11:15	0.13	0.02	0.11	.	74.25	.
18/11/2014 11:30	0.11	0.02	0.09	.	74.5	.
18/11/2014 11:45	0.14	0.02	0.12	.	74.75	.
18/11/2014 12:00	0.12	0.02	0.10	.	75	.
18/11/2014 12:15	0.13	0.02	0.11	.	75.25	.
18/11/2014 12:30	0.13	0.02	0.11	.	75.5	.
18/11/2014 12:45	0.12	0.02	0.10	.	75.75	.
18/11/2014 13:00	0.12	0.02	0.10	.	76	.
18/11/2014 13:15	0.11	0.02	0.09	.	76.25	.
18/11/2014 13:30	0.11	0.02	0.09	.	76.5	.
18/11/2014 13:45	0.11	0.02	0.09	.	76.75	.
18/11/2014 14:00	0.10	0.02	0.08	.	77	.
18/11/2014 14:15	0.11	0.02	0.09	.	77.25	.
18/11/2014 14:30	0.10	0.02	0.08	.	77.5	.
18/11/2014 14:45	0.11	0.02	0.09	.	77.75	.
18/11/2014 15:00	0.10	0.02	0.08	.	78	.
18/11/2014 15:15	0.12	0.02	0.10	.	78.25	.
18/11/2014 15:30	0.10	0.02	0.08	.	78.5	.
18/11/2014 15:45	0.10	0.02	0.08	.	78.75	0.2
18/11/2014 16:00	0.10	0.02	0.08	.	79	.
18/11/2014 16:15	0.10	0.02	0.08	.	79.25	.
18/11/2014 16:30	0.10	0.02	0.08	.	79.5	.
18/11/2014 16:45	0.10	0.02	0.08	.	79.75	.
18/11/2014 17:00	0.10	0.02	0.08	.	80	.
18/11/2014 17:15	0.09	0.02	0.07	.	80.25	.
18/11/2014 17:30	0.09	0.02	0.07	.	80.5	.
18/11/2014 17:45	0.09	0.02	0.07	.	80.75	.
18/11/2014 18:00	0.10	0.02	0.08	.	81	.
18/11/2014 18:15	0.09	0.02	0.07	.	81.25	.
18/11/2014 18:30	0.10	0.02	0.08	.	81.5	.
18/11/2014 18:45	0.09	0.02	0.07	.	81.75	.
18/11/2014 19:00	0.10	0.02	0.08	.	82	.
18/11/2014 19:15	0.09	0.02	0.07	.	82.25	.
18/11/2014 19:30	0.09	0.02	0.07	.	82.5	.
18/11/2014 19:45	0.10	0.02	0.08	.	82.75	.
18/11/2014 20:00	0.09	0.02	0.07	.	83	.
18/11/2014 20:15	0.09	0.02	0.07	.	83.25	.
18/11/2014 20:30	0.09	0.02	0.07	.	83.5	.
18/11/2014 20:45	0.08	0.02	0.06	.	83.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
18/11/2014 21:00	0.09	0.02	0.07	.	84	.
18/11/2014 21:15	0.08	0.02	0.06	.	84.25	.
18/11/2014 21:30	0.08	0.02	0.06	.	84.5	.
18/11/2014 21:45	0.08	0.02	0.06	.	84.75	.
18/11/2014 22:00	0.08	0.02	0.06	.	85	.
18/11/2014 22:15	0.08	0.02	0.06	.	85.25	.
18/11/2014 22:30	0.08	0.02	0.06	.	85.5	.
18/11/2014 22:45	0.08	0.02	0.06	.	85.75	.
18/11/2014 23:00	0.08	0.02	0.06	.	86	.
18/11/2014 23:15	0.07	0.02	0.05	.	86.25	.
18/11/2014 23:30	0.08	0.02	0.06	.	86.5	.
18/11/2014 23:45	0.08	0.02	0.06	.	86.75	.
19/11/2014 00:00	0.08	0.02	0.06	.	87	.
19/11/2014 00:15	0.08	0.02	0.06	.	87.25	.
19/11/2014 00:30	0.08	0.02	0.06	.	87.5	.
19/11/2014 00:45	0.07	0.02	0.05	.	87.75	.
19/11/2014 01:00	0.07	0.02	0.05	.	88	.
19/11/2014 01:15	0.07	0.02	0.05	.	88.25	.
19/11/2014 01:30	0.06	0.02	0.04	.	88.5	.
19/11/2014 01:45	0.07	0.02	0.05	.	88.75	.
19/11/2014 02:00	0.07	0.02	0.05	.	89	.
19/11/2014 02:15	0.07	0.02	0.05	.	89.25	.
19/11/2014 02:30	0.07	0.02	0.05	.	89.5	.
19/11/2014 02:45	0.07	0.02	0.05	.	89.75	.
19/11/2014 03:00	0.06	0.02	0.04	.	90	.
19/11/2014 03:15	0.06	0.02	0.04	.	90.25	.
19/11/2014 03:30	0.06	0.02	0.04	.	90.5	.
19/11/2014 03:45	0.06	0.02	0.04	.	90.75	.
19/11/2014 04:00	0.05	0.02	0.03	.	91	.
19/11/2014 04:15	0.05	0.02	0.03	.	91.25	.
19/11/2014 04:30	0.05	0.02	0.03	.	91.5	.
19/11/2014 04:45	0.05	0.02	0.03	.	91.75	.
19/11/2014 05:00	0.05	0.02	0.03	.	92	.
19/11/2014 05:15	0.04	0.02	0.02	.	92.25	.
19/11/2014 05:30	0.04	0.02	0.02	.	92.5	.
19/11/2014 05:45	0.04	0.02	0.02	.	92.75	.
19/11/2014 06:00	0.04	0.02	0.02	.	93	.
19/11/2014 06:15	0.04	0.02	0.02	.	93.25	.
19/11/2014 06:30	0.04	0.02	0.02	.	93.5	.
19/11/2014 06:45	0.04	0.02	0.02	.	93.75	.
19/11/2014 07:00	0.04	0.02	0.02	.	94	.
19/11/2014 07:15	0.04	0.02	0.02	.	94.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
19/11/2014 07:30	0.04	0.02	0.02	.	94.5	.
19/11/2014 07:45	0.04	0.02	0.02	.	94.75	.
19/11/2014 08:00	0.04	0.02	0.02	.	95	.
19/11/2014 08:15	0.04	0.02	0.02	.	95.25	.
19/11/2014 08:30	0.05	0.02	0.03	.	95.5	.
19/11/2014 08:45	0.05	0.02	0.03	.	95.75	.
19/11/2014 09:00	0.05	0.02	0.03	.	96	.
19/11/2014 09:15	0.05	0.02	0.03	.	96.25	.
19/11/2014 09:30	0.05	0.02	0.03	.	96.5	.
19/11/2014 09:45	0.05	0.02	0.03	.	96.75	.
19/11/2014 10:00	0.06	0.02	0.04	.	97	.
19/11/2014 10:15	0.06	0.02	0.04	.	97.25	.
19/11/2014 10:30	0.06	0.02	0.04	.	97.5	.
19/11/2014 10:45	0.05	0.02	0.03	.	97.75	.
19/11/2014 11:00	0.05	0.02	0.03	.	98	.
19/11/2014 11:15	0.06	0.02	0.04	.	98.25	.
19/11/2014 11:30	0.06	0.02	0.04	.	98.5	.
19/11/2014 11:45	0.06	0.02	0.04	.	98.75	.
19/11/2014 12:00	0.05	0.02	0.03	.	99	.
19/11/2014 12:15	0.05	0.02	0.03	.	99.25	.
19/11/2014 12:30	0.05	0.02	0.03	.	99.5	.
19/11/2014 12:45	0.05	0.02	0.03	.	99.75	.
19/11/2014 13:00	0.05	0.02	0.03	.	100	.
19/11/2014 13:15	0.04	0.02	0.02	.	100.25	.
19/11/2014 13:30	0.04	0.02	0.02	.	100.5	.
19/11/2014 13:45	0.04	0.02	0.02	.	100.75	.
19/11/2014 14:00	0.04	0.02	0.02	.	101	.
19/11/2014 14:15	0.05	0.02	0.03	.	101.25	.
19/11/2014 14:30	0.04	0.02	0.02	.	101.5	.
19/11/2014 14:45	0.04	0.02	0.02	.	101.75	.
19/11/2014 15:00	0.04	0.02	0.02	.	102	.
19/11/2014 15:15	0.04	0.02	0.02	.	102.25	.
19/11/2014 15:30	0.04	0.02	0.02	.	102.5	.
19/11/2014 15:45	0.04	0.02	0.02	.	102.75	.
19/11/2014 16:00	0.04	0.02	0.02	.	103	0.2
19/11/2014 16:15	0.04	0.02	0.02	.	103.25	0.2
19/11/2014 16:30	0.05	0.02	0.03	.	103.5	.
19/11/2014 16:45	0.04	0.02	0.02	.	103.75	.
19/11/2014 17:00	0.04	0.02	0.02	.	104	.
19/11/2014 17:15	0.04	0.02	0.02	0.2	104.25	.
19/11/2014 17:30	0.04	0.02	0.02	.	104.5	.
19/11/2014 17:45	0.04	0.02	0.02	.	104.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
19/11/2014 18:00	0.04	0.02	0.02	.	105	.
19/11/2014 18:15	0.04	0.02	0.02	.	105.25	.
19/11/2014 18:30	0.04	0.02	0.02	.	105.5	.
19/11/2014 18:45	0.04	0.02	0.02	.	105.75	.
19/11/2014 19:00	0.04	0.02	0.02	.	106	.
19/11/2014 19:15	0.04	0.02	0.02	.	106.25	.
19/11/2014 19:30	0.04	0.02	0.02	.	106.5	.
19/11/2014 19:45	0.04	0.02	0.02	.	106.75	.
19/11/2014 20:00	0.05	0.02	0.03	.	107	.
19/11/2014 20:15	0.04	0.02	0.02	.	107.25	.
19/11/2014 20:30	0.04	0.02	0.02	.	107.5	.
19/11/2014 20:45	0.04	0.02	0.02	.	107.75	.
19/11/2014 21:00	0.04	0.02	0.02	.	108	.
19/11/2014 21:15	0.04	0.02	0.02	.	108.25	.
19/11/2014 21:30	0.04	0.02	0.02	.	108.5	.
19/11/2014 21:45	0.04	0.02	0.02	.	108.75	.
19/11/2014 22:00	0.04	0.02	0.02	.	109	.
19/11/2014 22:15	0.04	0.02	0.02	.	109.25	.
19/11/2014 22:30	0.03	0.02	0.01	.	109.5	.
19/11/2014 22:45	0.04	0.02	0.02	.	109.75	.
19/11/2014 23:00	0.04	0.02	0.02	.	110	.
19/11/2014 23:15	0.04	0.02	0.02	.	110.25	.
19/11/2014 23:30	0.04	0.02	0.02	.	110.5	.
19/11/2014 23:45	0.04	0.02	0.02	.	110.75	.
20/11/2014 00:00	0.04	0.02	0.02	.	111	.
20/11/2014 00:15	0.03	0.02	0.01	.	111.25	.
20/11/2014 00:30	0.03	0.02	0.01	.	111.5	.
20/11/2014 00:45	0.03	0.02	0.01	.	111.75	.
20/11/2014 01:00	0.03	0.02	0.01	.	112	.
20/11/2014 01:15	0.03	0.02	0.01	.	112.25	.
20/11/2014 01:30	0.03	0.02	0.01	.	112.5	.
20/11/2014 01:45	0.03	0.02	0.01	.	112.75	.
20/11/2014 02:00	0.03	0.02	0.01	.	113	.
20/11/2014 02:15	0.03	0.02	0.01	.	113.25	.
20/11/2014 02:30	0.03	0.02	0.01	.	113.5	.
20/11/2014 02:45	0.03	0.02	0.01	.	113.75	.
20/11/2014 03:00	0.03	0.02	0.01	.	114	.
20/11/2014 03:15	0.03	0.02	0.01	.	114.25	.
20/11/2014 03:30	0.03	0.02	0.01	.	114.5	.
20/11/2014 03:45	0.03	0.02	0.01	.	114.75	.
20/11/2014 04:00	0.02	0.02	0.00	.	115	.
20/11/2014 04:15	0.03	0.02	0.01	.	115.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
20/11/2014 04:30	0.03	0.02	0.01	.	115.5	.
20/11/2014 04:45	0.03	0.02	0.01	.	115.75	.
20/11/2014 05:00	0.02	0.02	0.00	.	116	.
20/11/2014 05:15	0.02	0.02	0.00	.	116.25	.
20/11/2014 05:30	0.03	0.02	0.01	.	116.5	.
20/11/2014 05:45	0.03	0.02	0.01	.	116.75	.
20/11/2014 06:00	0.02	0.02	0.00	.	117	.
20/11/2014 06:15	0.02	0.02	0.00	.	117.25	.
20/11/2014 06:30	0.02	0.02	0.00	.	117.5	.
20/11/2014 06:45	0.02	0.02	0.00	.	117.75	.
20/11/2014 07:00	0.02	0.02	0.00	.	118	.
20/11/2014 07:15	0.02	0.02	0.00	.	118.25	.
20/11/2014 07:30	0.02	0.02	0.00	.	118.5	.
20/11/2014 07:45	0.03	0.02	0.01	.	118.75	.
20/11/2014 08:00	0.03	0.02	0.01	.	119	.
20/11/2014 08:15	0.03	0.02	0.01	.	119.25	.
20/11/2014 08:30	0.03	0.02	0.01	.	119.5	.
20/11/2014 08:45	0.03	0.02	0.01	.	119.75	.
20/11/2014 09:00	0.04	0.02	0.02	.	120	.
20/11/2014 09:15	0.04	0.02	0.02	.	120.25	.
20/11/2014 09:30	0.04	0.02	0.02	.	120.5	.
20/11/2014 09:45	0.04	0.02	0.02	.	120.75	.
20/11/2014 10:00	0.04	0.02	0.02	.	121	.
20/11/2014 10:15	0.04	0.02	0.02	.	121.25	.
20/11/2014 10:30	0.03	0.02	0.01	.	121.5	.
20/11/2014 10:45	0.04	0.02	0.02	.	121.75	.
20/11/2014 11:00	0.04	0.02	0.02	.	122	.
20/11/2014 11:15	0.04	0.02	0.02	.	122.25	.
20/11/2014 11:30	0.04	0.02	0.02	.	122.5	.
20/11/2014 11:45	0.04	0.02	0.02	.	122.75	.
20/11/2014 12:00	0.04	0.02	0.02	.	123	.
20/11/2014 12:15	0.04	0.02	0.02	.	123.25	.
20/11/2014 12:30	0.04	0.02	0.02	.	123.5	.
20/11/2014 12:45	0.04	0.02	0.02	.	123.75	.
20/11/2014 13:00	0.04	0.02	0.02	.	124	.
20/11/2014 13:15	0.03	0.02	0.01	.	124.25	.
20/11/2014 13:30	0.04	0.02	0.02	.	124.5	.
20/11/2014 13:45	0.04	0.02	0.02	.	124.75	.
20/11/2014 14:00	0.03	0.02	0.01	.	125	.
20/11/2014 14:15	0.03	0.02	0.01	.	125.25	.
20/11/2014 14:30	0.03	0.02	0.01	.	125.5	.
20/11/2014 14:45	0.03	0.02	0.01	.	125.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
20/11/2014 15:00	0.03	0.02	0.01	.	126	.
20/11/2014 15:15	0.03	0.02	0.01	.	126.25	.
20/11/2014 15:30	0.03	0.02	0.01	.	126.5	.
20/11/2014 15:45	0.04	0.02	0.02	.	126.75	.
20/11/2014 16:00	0.03	0.02	0.01	.	127	.
20/11/2014 16:15	0.03	0.02	0.01	.	127.25	.
20/11/2014 16:30	0.03	0.02	0.01	.	127.5	.
20/11/2014 16:45	0.03	0.02	0.01	.	127.75	.
20/11/2014 17:00	0.03	0.02	0.01	.	128	.
20/11/2014 17:15	0.03	0.02	0.01	.	128.25	.
20/11/2014 17:30	0.03	0.02	0.01	.	128.5	.
20/11/2014 17:45	0.04	0.02	0.02	.	128.75	.
20/11/2014 18:00	0.03	0.02	0.01	.	129	.
20/11/2014 18:15	0.04	0.02	0.02	.	129.25	.
20/11/2014 18:30	0.04	0.02	0.02	.	129.5	.
20/11/2014 18:45	0.04	0.02	0.02	.	129.75	.
20/11/2014 19:00	0.04	0.02	0.02	.	130	.
20/11/2014 19:15	0.03	0.02	0.01	.	130.25	.
20/11/2014 19:30	0.03	0.02	0.01	.	130.5	.
20/11/2014 19:45	0.04	0.02	0.02	.	130.75	.
20/11/2014 20:00	0.04	0.02	0.02	.	131	.
20/11/2014 20:15	0.04	0.02	0.02	.	131.25	.
20/11/2014 20:30	0.04	0.02	0.02	.	131.5	.
20/11/2014 20:45	0.04	0.02	0.02	.	131.75	.
20/11/2014 21:00	0.04	0.02	0.02	.	132	.
20/11/2014 21:15	0.04	0.02	0.02	.	132.25	.
20/11/2014 21:30	0.04	0.02	0.02	.	132.5	.
20/11/2014 21:45	0.04	0.02	0.02	.	132.75	.
20/11/2014 22:00	0.04	0.02	0.02	.	133	.
20/11/2014 22:15	0.03	0.02	0.01	.	133.25	.
20/11/2014 22:30	0.04	0.02	0.02	.	133.5	.
20/11/2014 22:45	0.03	0.02	0.01	.	133.75	.
20/11/2014 23:00	0.03	0.02	0.01	.	134	.
20/11/2014 23:15	0.03	0.02	0.01	.	134.25	.
20/11/2014 23:30	0.03	0.02	0.01	.	134.5	.
20/11/2014 23:45	0.03	0.02	0.01	.	134.75	.
21/11/2014 00:00	0.03	0.02	0.01	.	135	.
21/11/2014 00:15	0.03	0.02	0.01	.	135.25	.
21/11/2014 00:30	0.03	0.02	0.01	.	135.5	.
21/11/2014 00:45	0.04	0.02	0.02	.	135.75	.
21/11/2014 01:00	0.03	0.02	0.01	.	136	.
21/11/2014 01:15	0.03	0.02	0.01	.	136.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
21/11/2014 01:30	0.03	0.02	0.01	.	136.5	.
21/11/2014 01:45	0.03	0.02	0.01	.	136.75	.
21/11/2014 02:00	0.03	0.02	0.01	.	137	.
21/11/2014 02:15	0.03	0.02	0.01	.	137.25	.
21/11/2014 02:30	0.03	0.02	0.01	.	137.5	.
21/11/2014 02:45	0.03	0.02	0.01	.	137.75	.
21/11/2014 03:00	0.03	0.02	0.01	.	138	.
21/11/2014 03:15	0.03	0.02	0.01	.	138.25	.
21/11/2014 03:30	0.03	0.02	0.01	.	138.5	.
21/11/2014 03:45	0.03	0.02	0.01	.	138.75	.
21/11/2014 04:00	0.03	0.02	0.01	.	139	.
21/11/2014 04:15	0.03	0.02	0.01	.	139.25	.
21/11/2014 04:30	0.03	0.02	0.01	.	139.5	.
21/11/2014 04:45	0.02	0.02	0.00	.	139.75	.
21/11/2014 05:00	0.02	0.02	0.00	.	140	.
21/11/2014 05:15	0.02	0.02	0.00	.	140.25	.
21/11/2014 05:30	0.02	0.02	0.00	.	140.5	.
21/11/2014 05:45	0.03	0.02	0.01	.	140.75	.
21/11/2014 06:00	0.03	0.02	0.01	.	141	.
21/11/2014 06:15	0.02	0.02	0.00	.	141.25	.
21/11/2014 06:30	0.02	0.02	0.00	.	141.5	.
21/11/2014 06:45	0.03	0.02	0.01	.	141.75	.
21/11/2014 07:00	0.02	0.02	0.00	.	142	.
21/11/2014 07:15	0.03	0.02	0.01	.	142.25	.
21/11/2014 07:30	0.02	0.02	0.00	.	142.5	.
21/11/2014 07:45	0.03	0.02	0.01	.	142.75	.
21/11/2014 08:00	0.03	0.02	0.01	.	143	.
21/11/2014 08:15	0.03	0.02	0.01	.	143.25	.
21/11/2014 08:30	0.03	0.02	0.01	.	143.5	.
21/11/2014 08:45	0.04	0.02	0.02	.	143.75	.
21/11/2014 09:00	0.04	0.02	0.02	.	144	.
21/11/2014 09:15	0.04	0.02	0.02	.	144.25	.
21/11/2014 09:30	0.04	0.02	0.02	.	144.5	.
21/11/2014 09:45	0.04	0.02	0.02	.	144.75	.
21/11/2014 10:00	0.04	0.02	0.02	.	145	.
21/11/2014 10:15	0.04	0.02	0.02	.	145.25	.
21/11/2014 10:30	0.04	0.02	0.02	.	145.5	.
21/11/2014 10:45	0.04	0.02	0.02	.	145.75	.
21/11/2014 11:00	0.04	0.02	0.02	.	146	.
21/11/2014 11:15	0.04	0.02	0.02	.	146.25	.
21/11/2014 11:30	0.03	0.02	0.01	.	146.5	.
21/11/2014 11:45	0.03	0.02	0.01	.	146.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
21/11/2014 12:00	0.03	0.02	0.01	.	147	.
21/11/2014 12:15	0.03	0.02	0.01	.	147.25	0.2
21/11/2014 12:30	0.03	0.02	0.01	.	147.5	.
21/11/2014 12:45	0.03	0.02	0.01	.	147.75	.
21/11/2014 13:00	0.03	0.02	0.01	.	148	.
21/11/2014 13:15	0.03	0.02	0.01	.	148.25	.
21/11/2014 13:30	0.04	0.02	0.02	.	148.5	.
21/11/2014 13:45	0.03	0.02	0.01	.	148.75	.
21/11/2014 14:00	0.04	0.02	0.02	.	149	.
21/11/2014 14:15	0.03	0.02	0.01	.	149.25	.
21/11/2014 14:30	0.03	0.02	0.01	.	149.5	.
21/11/2014 14:45	0.04	0.02	0.02	.	149.75	.
21/11/2014 15:00	0.04	0.02	0.02	.	150	.
21/11/2014 15:15	0.04	0.02	0.02	.	150.25	.
21/11/2014 15:30	0.04	0.02	0.02	.	150.5	.
21/11/2014 15:45	0.03	0.02	0.01	.	150.75	.
21/11/2014 16:00	0.04	0.02	0.02	.	151	.
21/11/2014 16:15	0.04	0.02	0.02	.	151.25	.
21/11/2014 16:30	0.03	0.02	0.01	.	151.5	.
21/11/2014 16:45	0.03	0.02	0.01	.	151.75	.
21/11/2014 17:00	0.04	0.02	0.02	0.2	152	0.2
21/11/2014 17:15	0.04	0.02	0.02	0.6	152.25	0.4
21/11/2014 17:30	0.04	0.02	0.02	.	152.5	.
21/11/2014 17:45	0.04	0.02	0.02	0.2	152.75	.
21/11/2014 18:00	0.04	0.02	0.02	.	153	.
21/11/2014 18:15	0.04	0.02	0.02	.	153.25	.
21/11/2014 18:30	0.05	0.02	0.03	.	153.5	0.2
21/11/2014 18:45	0.05	0.02	0.03	.	153.75	.
21/11/2014 19:00	0.05	0.02	0.03	.	154	.
21/11/2014 19:15	0.05	0.02	0.03	.	154.25	.
21/11/2014 19:30	0.05	0.02	0.03	.	154.5	.
21/11/2014 19:45	0.05	0.02	0.03	.	154.75	.
21/11/2014 20:00	0.04	0.02	0.02	0.2	155	.
21/11/2014 20:15	0.05	0.02	0.03	.	155.25	.
21/11/2014 20:30	0.04	0.02	0.02	.	155.5	0.2
21/11/2014 20:45	0.04	0.02	0.02	.	155.75	.
21/11/2014 21:00	0.04	0.02	0.02	.	156	.
21/11/2014 21:15	0.04	0.02	0.02	.	156.25	.
21/11/2014 21:30	0.04	0.02	0.02	.	156.5	.
21/11/2014 21:45	0.04	0.02	0.02	.	156.75	.
21/11/2014 22:00	0.04	0.02	0.02	.	157	.
21/11/2014 22:15	0.04	0.02	0.02	.	157.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
21/11/2014 22:30	0.03	0.02	0.01	.	157.5	.
21/11/2014 22:45	0.04	0.02	0.02	.	157.75	.
21/11/2014 23:00	0.04	0.02	0.02	.	158	.
21/11/2014 23:15	0.04	0.02	0.02	.	158.25	.
21/11/2014 23:30	0.04	0.02	0.02	.	158.5	.
21/11/2014 23:45	0.03	0.02	0.01	.	158.75	.
22/11/2014 00:00	0.03	0.02	0.01	.	159	.
22/11/2014 00:15	0.03	0.02	0.01	.	159.25	.
22/11/2014 00:30	0.03	0.02	0.01	.	159.5	.
22/11/2014 00:45	0.03	0.02	0.01	.	159.75	.
22/11/2014 01:00	0.03	0.02	0.01	.	160	.
22/11/2014 01:15	0.03	0.02	0.01	.	160.25	.
22/11/2014 01:30	0.03	0.02	0.01	.	160.5	.
22/11/2014 01:45	0.03	0.02	0.01	.	160.75	.
22/11/2014 02:00	0.03	0.02	0.01	.	161	.
22/11/2014 02:15	0.03	0.02	0.01	.	161.25	.
22/11/2014 02:30	0.03	0.02	0.01	.	161.5	.
22/11/2014 02:45	0.03	0.02	0.01	.	161.75	.
22/11/2014 03:00	0.03	0.02	0.01	.	162	.
22/11/2014 03:15	0.03	0.02	0.01	.	162.25	.
22/11/2014 03:30	0.03	0.02	0.01	.	162.5	.
22/11/2014 03:45	0.03	0.02	0.01	.	162.75	.
22/11/2014 04:00	0.02	0.02	0.00	.	163	.
22/11/2014 04:15	0.02	0.02	0.00	.	163.25	.
22/11/2014 04:30	0.02	0.02	0.00	.	163.5	.
22/11/2014 04:45	0.02	0.02	0.00	.	163.75	.
22/11/2014 05:00	0.03	0.02	0.01	.	164	.
22/11/2014 05:15	0.02	0.02	0.00	.	164.25	.
22/11/2014 05:30	0.02	0.02	0.00	.	164.5	.
22/11/2014 05:45	0.02	0.02	0.00	.	164.75	.
22/11/2014 06:00	0.02	0.02	0.00	.	165	0.2
22/11/2014 06:15	0.02	0.02	0.00	.	165.25	.
22/11/2014 06:30	0.02	0.02	0.00	.	165.5	.
22/11/2014 06:45	0.03	0.02	0.01	.	165.75	.
22/11/2014 07:00	0.02	0.02	0.00	.	166	.
22/11/2014 07:15	0.03	0.02	0.01	.	166.25	0.2
22/11/2014 07:30	0.02	0.02	0.00	0.2	166.5	.
22/11/2014 07:45	0.02	0.02	0.00	.	166.75	.
22/11/2014 08:00	0.02	0.02	0.00	.	167	.
22/11/2014 08:15	0.03	0.02	0.01	.	167.25	0.2
22/11/2014 08:30	0.03	0.02	0.01	.	167.5	.
22/11/2014 08:45	0.03	0.02	0.01	.	167.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
22/11/2014 09:00	0.03	0.02	0.01	.	168	.
22/11/2014 09:15	0.03	0.02	0.01	.	168.25	.
22/11/2014 09:30	0.03	0.02	0.01	.	168.5	.
22/11/2014 09:45	0.04	0.02	0.02	.	168.75	.
22/11/2014 10:00	0.04	0.02	0.02	.	169	.
22/11/2014 10:15	0.04	0.02	0.02	.	169.25	.
22/11/2014 10:30	0.04	0.02	0.02	.	169.5	.
22/11/2014 10:45	0.04	0.02	0.02	.	169.75	.
22/11/2014 11:00	0.04	0.02	0.02	.	170	.
22/11/2014 11:15	0.04	0.02	0.02	.	170.25	.
22/11/2014 11:30	0.05	0.02	0.03	.	170.5	.
22/11/2014 11:45	0.04	0.02	0.02	.	170.75	.
22/11/2014 12:00	0.04	0.02	0.02	0.2	171	.
22/11/2014 12:15	0.04	0.02	0.02	0.4	171.25	0.6
22/11/2014 12:30	0.05	0.02	0.03	0.4	171.5	0.4
22/11/2014 12:45	0.04	0.02	0.02	0.2	171.75	0.2
22/11/2014 13:00	0.04	0.02	0.02	0.2	172	.
22/11/2014 13:15	0.05	0.02	0.03	.	172.25	.
22/11/2014 13:30	0.07	0.02	0.05	.	172.5	.
22/11/2014 13:45	0.08	0.02	0.06	.	172.75	.
22/11/2014 14:00	0.07	0.02	0.05	.	173	.
22/11/2014 14:15	0.07	0.02	0.05	.	173.25	.
22/11/2014 14:30	0.07	0.02	0.05	.	173.5	.
22/11/2014 14:45	0.07	0.02	0.05	.	173.75	.
22/11/2014 15:00	0.07	0.02	0.05	.	174	.
22/11/2014 15:15	0.06	0.02	0.04	.	174.25	.
22/11/2014 15:30	0.07	0.02	0.05	.	174.5	.
22/11/2014 15:45	0.06	0.02	0.04	.	174.75	.
22/11/2014 16:00	0.05	0.02	0.03	.	175	.
22/11/2014 16:15	0.05	0.02	0.03	.	175.25	.
22/11/2014 16:30	0.04	0.02	0.02	.	175.5	0.2
22/11/2014 16:45	0.04	0.02	0.02	.	175.75	.
22/11/2014 17:00	0.04	0.02	0.02	.	176	.
22/11/2014 17:15	0.04	0.02	0.02	.	176.25	.
22/11/2014 17:30	0.04	0.02	0.02	.	176.5	.
22/11/2014 17:45	0.04	0.02	0.02	0.4	176.75	0.2
22/11/2014 18:00	0.04	0.02	0.02	.	177	.
22/11/2014 18:15	0.04	0.02	0.02	.	177.25	.
22/11/2014 18:30	0.04	0.02	0.02	.	177.5	.
22/11/2014 18:45	0.05	0.02	0.03	.	177.75	.
22/11/2014 19:00	0.04	0.02	0.02	.	178	.
22/11/2014 19:15	0.05	0.02	0.03	.	178.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
22/11/2014 19:30	0.05	0.02	0.03	.	178.5	.
22/11/2014 19:45	0.05	0.02	0.03	.	178.75	.
22/11/2014 20:00	0.05	0.02	0.03	.	179	.
22/11/2014 20:15	0.05	0.02	0.03	.	179.25	.
22/11/2014 20:30	0.05	0.02	0.03	.	179.5	.
22/11/2014 20:45	0.05	0.02	0.03	.	179.75	.
22/11/2014 21:00	0.04	0.02	0.02	.	180	.
22/11/2014 21:15	0.04	0.02	0.02	.	180.25	.
22/11/2014 21:30	0.04	0.02	0.02	.	180.5	.
22/11/2014 21:45	0.04	0.02	0.02	.	180.75	.
22/11/2014 22:00	0.04	0.02	0.02	.	181	.
22/11/2014 22:15	0.04	0.02	0.02	.	181.25	.
22/11/2014 22:30	0.04	0.02	0.02	.	181.5	.
22/11/2014 22:45	0.03	0.02	0.01	.	181.75	.
22/11/2014 23:00	0.04	0.02	0.02	.	182	.
22/11/2014 23:15	0.04	0.02	0.02	.	182.25	.
22/11/2014 23:30	0.04	0.02	0.02	.	182.5	.
22/11/2014 23:45	0.04	0.02	0.02	.	182.75	.
23/11/2014 00:00	0.04	0.02	0.02	.	183	.
23/11/2014 00:15	0.04	0.02	0.02	.	183.25	.
23/11/2014 00:30	0.04	0.02	0.02	.	183.5	.
23/11/2014 00:45	0.04	0.02	0.02	.	183.75	.
23/11/2014 01:00	0.04	0.02	0.02	.	184	.
23/11/2014 01:15	0.04	0.02	0.02	.	184.25	.
23/11/2014 01:30	0.03	0.02	0.01	.	184.5	.
23/11/2014 01:45	0.03	0.02	0.01	.	184.75	.
23/11/2014 02:00	0.04	0.02	0.02	.	185	.
23/11/2014 02:15	0.04	0.02	0.02	.	185.25	.
23/11/2014 02:30	0.03	0.02	0.01	.	185.5	.
23/11/2014 02:45	0.03	0.02	0.01	.	185.75	.
23/11/2014 03:00	0.03	0.02	0.01	.	186	.
23/11/2014 03:15	0.03	0.02	0.01	.	186.25	.
23/11/2014 03:30	0.03	0.02	0.01	.	186.5	.
23/11/2014 03:45	0.04	0.02	0.02	.	186.75	.
23/11/2014 04:00	0.03	0.02	0.01	.	187	.
23/11/2014 04:15	0.03	0.02	0.01	.	187.25	.
23/11/2014 04:30	0.03	0.02	0.01	.	187.5	.
23/11/2014 04:45	0.03	0.02	0.01	.	187.75	.
23/11/2014 05:00	0.02	0.02	0.00	0.2	188	.
23/11/2014 05:15	0.02	0.02	0.00	.	188.25	.
23/11/2014 05:30	0.02	0.02	0.00	.	188.5	0.2
23/11/2014 05:45	0.03	0.02	0.01	.	188.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
23/11/2014 06:00	0.02	0.02	0.00	.	189	.
23/11/2014 06:15	0.02	0.02	0.00	.	189.25	.
23/11/2014 06:30	0.02	0.02	0.00	.	189.5	0.2
23/11/2014 06:45	0.02	0.02	0.00	.	189.75	.
23/11/2014 07:00	0.02	0.02	0.00	0.2	190	0.2
23/11/2014 07:15	0.03	0.02	0.01	.	190.25	0.2
23/11/2014 07:30	0.03	0.02	0.01	.	190.5	0.4
23/11/2014 07:45	0.03	0.02	0.01	0.2	190.75	.
23/11/2014 08:00	0.03	0.02	0.01	0.2	191	0.2
23/11/2014 08:15	0.03	0.02	0.01	.	191.25	0.2
23/11/2014 08:30	0.04	0.02	0.02	0.2	191.5	0.6
23/11/2014 08:45	0.05	0.02	0.03	0.2	191.75	0.2
23/11/2014 09:00	0.07	0.02	0.05	.	192	0.2
23/11/2014 09:15	0.07	0.02	0.05	0.2	192.25	.
23/11/2014 09:30	0.07	0.02	0.05	0.4	192.5	0.6
23/11/2014 09:45	0.08	0.02	0.06	.	192.75	.
23/11/2014 10:00	0.09	0.02	0.07	.	193	.
23/11/2014 10:15	0.08	0.02	0.06	.	193.25	.
23/11/2014 10:30	0.10	0.02	0.08	0.2	193.5	.
23/11/2014 10:45	0.08	0.02	0.06	.	193.75	0.2
23/11/2014 11:00	0.09	0.02	0.07	.	194	.
23/11/2014 11:15	0.08	0.02	0.06	.	194.25	.
23/11/2014 11:30	0.08	0.02	0.06	.	194.5	0.2
23/11/2014 11:45	0.09	0.02	0.07	0.8	194.75	0.8
23/11/2014 12:00	0.08	0.02	0.06	0.2	195	0.4
23/11/2014 12:15	0.08	0.02	0.06	0.2	195.25	0.4
23/11/2014 12:30	0.10	0.02	0.08	0.4	195.5	1
23/11/2014 12:45	0.11	0.02	0.09	0.8	195.75	1
23/11/2014 13:00	0.13	0.02	0.11	0.8	196	1
23/11/2014 13:15	0.19	0.02	0.17	0.8	196.25	0.8
23/11/2014 13:30	0.23	0.02	0.21	0.4	196.5	0.6
23/11/2014 13:45	0.22	0.02	0.20	0.8	196.75	1.4
23/11/2014 14:00	0.19	0.02	0.17	1	197	1.4
23/11/2014 14:15	0.22	0.02	0.20	1.2	197.25	1.2
23/11/2014 14:30	0.27	0.02	0.25	1	197.5	1.2
23/11/2014 14:45	0.36	0.02	0.34	1	197.75	0.4
23/11/2014 15:00	0.53	0.02	0.51	0.4	198	0.4
23/11/2014 15:15	0.53	0.02	0.51	0.6	198.25	0.4
23/11/2014 15:30	0.51	0.02	0.49	0.6	198.5	0.4
23/11/2014 15:45	0.51	0.02	0.49	0.2	198.75	0.2
23/11/2014 16:00	0.51	0.02	0.49	0.4	199	0.4
23/11/2014 16:15	0.53	0.02	0.51	0.6	199.25	0.4

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
23/11/2014 16:30	0.52	0.02	0.50	0.2	199.5	0.4
23/11/2014 16:45	0.62	0.02	0.60	0.4	199.75	0.4
23/11/2014 17:00	0.63	0.02	0.61	0.6	200	0.6
23/11/2014 17:15	0.61	0.02	0.59	0.6	200.25	0.4
23/11/2014 17:30	0.71	0.02	0.69	0.2	200.5	0.2
23/11/2014 17:45	0.74	0.02	0.72	0.6	200.75	0.4
23/11/2014 18:00	0.70	0.02	0.68	0.4	201	0.2
23/11/2014 18:15	0.80	0.02	0.78	0.6	201.25	0.6
23/11/2014 18:30	0.84	0.02	0.82	0.6	201.5	0.4
23/11/2014 18:45	0.82	0.02	0.80	0.2	201.75	0.4
23/11/2014 19:00	0.85	0.02	0.83	0.4	202	0.2
23/11/2014 19:15	0.97	0.02	0.95	0.6	202.25	0.4
23/11/2014 19:30	0.91	0.02	0.89	0.4	202.5	0.4
23/11/2014 19:45	0.96	0.02	0.94	0.4	202.75	0.4
23/11/2014 20:00	0.98	0.02	0.96	0.2	203	0.2
23/11/2014 20:15	1.06	0.02	1.04	0.2	203.25	0.2
23/11/2014 20:30	1.13	0.02	1.11	.	203.5	.
23/11/2014 20:45	1.06	0.02	1.04	0.2	203.75	.
23/11/2014 21:00	1.02	0.02	1.00	.	204	.
23/11/2014 21:15	0.95	0.02	0.93	.	204.25	.
23/11/2014 21:30	0.92	0.02	0.90	.	204.5	.
23/11/2014 21:45	0.95	0.02	0.93	.	204.75	.
23/11/2014 22:00	0.94	0.02	0.92	.	205	.
23/11/2014 22:15	1.00	0.02	0.98	.	205.25	.
23/11/2014 22:30	0.89	0.02	0.87	.	205.5	.
23/11/2014 22:45	0.85	0.02	0.83	.	205.75	.
23/11/2014 23:00	0.85	0.02	0.83	.	206	.
23/11/2014 23:15	0.83	0.02	0.81	.	206.25	.
23/11/2014 23:30	0.80	0.02	0.78	.	206.5	.
23/11/2014 23:45	0.83	0.02	0.81	.	206.75	0.2
24/11/2014 00:00	0.82	0.02	0.80	.	207	.
24/11/2014 00:15	0.76	0.02	0.74	.	207.25	.
24/11/2014 00:30	0.78	0.02	0.76	.	207.5	.
24/11/2014 00:45	0.73	0.02	0.71	.	207.75	.
24/11/2014 01:00	0.75	0.02	0.73	.	208	.
24/11/2014 01:15	0.73	0.02	0.71	.	208.25	.
24/11/2014 01:30	0.66	0.02	0.64	.	208.5	.
24/11/2014 01:45	0.66	0.02	0.64	.	208.75	.
24/11/2014 02:00	0.66	0.02	0.64	.	209	.
24/11/2014 02:15	0.70	0.02	0.68	.	209.25	.
24/11/2014 02:30	0.61	0.02	0.59	.	209.5	.
24/11/2014 02:45	0.63	0.02	0.61	.	209.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
24/11/2014 03:00	0.60	0.02	0.58	.	210	.
24/11/2014 03:15	0.61	0.02	0.59	.	210.25	.
24/11/2014 03:30	0.58	0.02	0.56	.	210.5	.
24/11/2014 03:45	0.56	0.02	0.54	.	210.75	.
24/11/2014 04:00	0.54	0.02	0.52	.	211	.
24/11/2014 04:15	0.55	0.02	0.53	.	211.25	.
24/11/2014 04:30	0.50	0.02	0.48	.	211.5	.
24/11/2014 04:45	0.50	0.02	0.48	.	211.75	.
24/11/2014 05:00	0.51	0.02	0.49	.	212	.
24/11/2014 05:15	0.50	0.02	0.48	0.2	212.25	.
24/11/2014 05:30	0.50	0.02	0.48	.	212.5	.
24/11/2014 05:45	0.46	0.02	0.44	.	212.75	.
24/11/2014 06:00	0.46	0.02	0.44	.	213	.
24/11/2014 06:15	0.43	0.02	0.41	.	213.25	.
24/11/2014 06:30	0.38	0.02	0.36	.	213.5	.
24/11/2014 06:45	0.40	0.02	0.38	.	213.75	.
24/11/2014 07:00	0.38	0.02	0.36	.	214	.
24/11/2014 07:15	0.38	0.02	0.36	.	214.25	.
24/11/2014 07:30	0.35	0.02	0.33	.	214.5	.
24/11/2014 07:45	0.32	0.02	0.30	.	214.75	.
24/11/2014 08:00	0.34	0.02	0.32	.	215	.
24/11/2014 08:15	0.34	0.02	0.32	.	215.25	.
24/11/2014 08:30	0.32	0.02	0.30	.	215.5	.
24/11/2014 08:45	0.32	0.02	0.30	.	215.75	.
24/11/2014 09:00	0.34	0.02	0.32	.	216	.
24/11/2014 09:15	0.32	0.02	0.30	.	216.25	.
24/11/2014 09:30	0.30	0.02	0.28	.	216.5	.
24/11/2014 09:45	0.26	0.02	0.24	.	216.75	.
24/11/2014 10:00	0.29	0.02	0.27	.	217	.
24/11/2014 10:15	0.29	0.02	0.27	.	217.25	.
24/11/2014 10:30	0.24	0.02	0.22	.	217.5	.
24/11/2014 10:45	0.24	0.02	0.22	.	217.75	.
24/11/2014 11:00	0.26	0.02	0.24	.	218	.
24/11/2014 11:15	0.25	0.02	0.23	.	218.25	.
24/11/2014 11:30	0.23	0.02	0.21	.	218.5	.
24/11/2014 11:45	0.22	0.02	0.20	.	218.75	.
24/11/2014 12:00	0.22	0.02	0.20	.	219	.
24/11/2014 12:15	0.21	0.02	0.19	.	219.25	.
24/11/2014 12:30	0.20	0.02	0.18	.	219.5	.
24/11/2014 12:45	0.22	0.02	0.20	.	219.75	.
24/11/2014 13:00	0.19	0.02	0.17	.	220	.
24/11/2014 13:15	0.19	0.02	0.17	.	220.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
24/11/2014 13:30	0.15	0.02	0.13	.	220.5	.
24/11/2014 13:45	0.17	0.02	0.15	.	220.75	.
24/11/2014 14:00	0.15	0.02	0.13	.	221	.
24/11/2014 14:15	0.17	0.02	0.15	.	221.25	.
24/11/2014 14:30	0.15	0.02	0.13	.	221.5	.
24/11/2014 14:45	0.17	0.02	0.15	.	221.75	.
24/11/2014 15:00	0.15	0.02	0.13	.	222	.
24/11/2014 15:15	0.16	0.02	0.14	.	222.25	.
24/11/2014 15:30	0.14	0.02	0.12	.	222.5	.
24/11/2014 15:45	0.14	0.02	0.12	.	222.75	.
24/11/2014 16:00	0.15	0.02	0.13	.	223	.
24/11/2014 16:15	0.16	0.02	0.14	.	223.25	.
24/11/2014 16:30	0.11	0.02	0.09	.	223.5	.
24/11/2014 16:45	0.11	0.02	0.09	.	223.75	.
24/11/2014 17:00	0.14	0.02	0.12	.	224	.
24/11/2014 17:15	0.12	0.02	0.10	.	224.25	.
24/11/2014 17:30	0.14	0.02	0.12	.	224.5	.
24/11/2014 17:45	0.12	0.02	0.10	.	224.75	.
24/11/2014 18:00	0.12	0.02	0.10	.	225	.
24/11/2014 18:15	0.11	0.02	0.09	.	225.25	.
24/11/2014 18:30	0.13	0.02	0.11	.	225.5	.
24/11/2014 18:45	0.10	0.02	0.08	.	225.75	.
24/11/2014 19:00	0.12	0.02	0.10	.	226	.
24/11/2014 19:15	0.11	0.02	0.09	.	226.25	.
24/11/2014 19:30	0.11	0.02	0.09	.	226.5	.
24/11/2014 19:45	0.10	0.02	0.08	.	226.75	.
24/11/2014 20:00	0.12	0.02	0.10	.	227	.
24/11/2014 20:15	0.11	0.02	0.09	.	227.25	.
24/11/2014 20:30	0.11	0.02	0.09	.	227.5	.
24/11/2014 20:45	0.11	0.02	0.09	.	227.75	.
24/11/2014 21:00	0.10	0.02	0.08	.	228	.
24/11/2014 21:15	0.10	0.02	0.08	.	228.25	.
24/11/2014 21:30	0.11	0.02	0.09	.	228.5	.
24/11/2014 21:45	0.11	0.02	0.09	.	228.75	.
24/11/2014 22:00	0.10	0.02	0.08	.	229	.
24/11/2014 22:15	0.10	0.02	0.08	.	229.25	.
24/11/2014 22:30	0.11	0.02	0.09	.	229.5	.
24/11/2014 22:45	0.11	0.02	0.09	.	229.75	.
24/11/2014 23:00	0.10	0.02	0.08	.	230	.
24/11/2014 23:15	0.10	0.02	0.08	.	230.25	.
24/11/2014 23:30	0.09	0.02	0.07	.	230.5	.
24/11/2014 23:45	0.10	0.02	0.08	.	230.75	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
25/11/2014 00:00	0.09	0.02	0.07	.	231	.
25/11/2014 00:15	0.10	0.02	0.08	.	231.25	.
25/11/2014 00:30	0.10	0.02	0.08	.	231.5	.
25/11/2014 00:45	0.09	0.02	0.07	.	231.75	.
25/11/2014 01:00	0.09	0.02	0.07	.	232	.
25/11/2014 01:15	0.09	0.02	0.07	.	232.25	.
25/11/2014 01:30	0.10	0.02	0.08	.	232.5	.
25/11/2014 01:45	0.08	0.02	0.06	.	232.75	.
25/11/2014 02:00	0.08	0.02	0.06	.	233	.
25/11/2014 02:15	0.09	0.02	0.07	.	233.25	.
25/11/2014 02:30	0.08	0.02	0.06	.	233.5	.
25/11/2014 02:45	0.08	0.02	0.06	.	233.75	.
25/11/2014 03:00	0.08	0.02	0.06	.	234	.
25/11/2014 03:15	0.07	0.02	0.05	.	234.25	.
25/11/2014 03:30	0.08	0.02	0.06	.	234.5	.
25/11/2014 03:45	0.08	0.02	0.06	.	234.75	.
25/11/2014 04:00	0.08	0.02	0.06	.	235	.
25/11/2014 04:15	0.08	0.02	0.06	.	235.25	.
25/11/2014 04:30	0.06	0.02	0.04	.	235.5	.
25/11/2014 04:45	0.06	0.02	0.04	.	235.75	.
25/11/2014 05:00	0.06	0.02	0.04	.	236	.
25/11/2014 05:15	0.06	0.02	0.04	.	236.25	.
25/11/2014 05:30	0.06	0.02	0.04	.	236.5	.
25/11/2014 05:45	0.05	0.02	0.03	.	236.75	.
25/11/2014 06:00	0.05	0.02	0.03	.	237	.
25/11/2014 06:15	0.04	0.02	0.02	.	237.25	.
25/11/2014 06:30	0.05	0.02	0.03	.	237.5	.
25/11/2014 06:45	0.05	0.02	0.03	.	237.75	0.2
25/11/2014 07:00	0.05	0.02	0.03	.	238	.
25/11/2014 07:15	0.05	0.02	0.03	.	238.25	.
25/11/2014 07:30	0.05	0.02	0.03	.	238.5	.
25/11/2014 07:45	0.05	0.02	0.03	.	238.75	.
25/11/2014 08:00	0.04	0.02	0.02	.	239	.
25/11/2014 08:15	0.04	0.02	0.02	.	239.25	.
25/11/2014 08:30	0.05	0.02	0.03	.	239.5	.
25/11/2014 08:45	0.06	0.02	0.04	.	239.75	.
25/11/2014 09:00	0.05	0.02	0.03	.	240	.
25/11/2014 09:15	0.05	0.02	0.03	.	240.25	.
25/11/2014 09:30	0.06	0.02	0.04	.	240.5	.
25/11/2014 09:45	0.07	0.02	0.05	.	240.75	.
25/11/2014 10:00	0.07	0.02	0.05	.	241	.
25/11/2014 10:15	0.07	0.02	0.05	.	241.25	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
25/11/2014 10:30	0.07	0.02	0.05	.	241.5	.
25/11/2014 10:45	0.09	0.02	0.07	.	241.75	.
25/11/2014 11:00	0.08	0.02	0.06	.	242	.
25/11/2014 11:15	0.07	0.02	0.05	.	242.25	.
25/11/2014 11:30	0.07	0.02	0.05	.	242.5	.
25/11/2014 11:45	0.06	0.02	0.04	.	242.75	.
25/11/2014 12:00	0.06	0.02	0.04	.	243	.
25/11/2014 12:15	0.06	0.02	0.04	.	243.25	.
25/11/2014 12:30	0.06	0.02	0.04	.	243.5	.
25/11/2014 12:45	0.06	0.02	0.04	.	243.75	.
25/11/2014 13:00	0.06	0.02	0.04	.	244	.
25/11/2014 13:15	0.05	0.02	0.03	.	244.25	.
25/11/2014 13:30	0.05	0.02	0.03	.	244.5	.
25/11/2014 13:45	0.05	0.02	0.03	.	244.75	.
25/11/2014 14:00	0.06	0.02	0.04	.	245	.
25/11/2014 14:15	0.05	0.02	0.03	.	245.25	.
25/11/2014 14:30	0.06	0.02	0.04	.	245.5	.
25/11/2014 14:45	0.05	0.02	0.03	.	245.75	.
25/11/2014 15:00	0.06	0.02	0.04	.	246	.
25/11/2014 15:15	0.05	0.02	0.03	.	246.25	.
25/11/2014 15:30	0.04	0.02	0.02	.	246.5	.
25/11/2014 15:45	0.04	0.02	0.02	.	246.75	.
25/11/2014 16:00	0.05	0.02	0.03	.	247	.
25/11/2014 16:15	0.05	0.02	0.03	.	247.25	.
25/11/2014 16:30	0.05	0.02	0.03	.	247.5	.
25/11/2014 16:45	0.04	0.02	0.02	.	247.75	.
25/11/2014 17:00	0.05	0.02	0.03	.	248	.
25/11/2014 17:15	0.04	0.02	0.02	.	248.25	.
25/11/2014 17:30	0.04	0.02	0.02	.	248.5	.
25/11/2014 17:45	0.05	0.02	0.03	.	248.75	.
25/11/2014 18:00	0.05	0.02	0.03	.	249	.
25/11/2014 18:15	0.05	0.02	0.03	.	249.25	.
25/11/2014 18:30	0.05	0.02	0.03	.	249.5	.
25/11/2014 18:45	0.05	0.02	0.03	.	249.75	.
25/11/2014 19:00	0.05	0.02	0.03	.	250	.
25/11/2014 19:15	0.05	0.02	0.03	.	250.25	.
25/11/2014 19:30	0.06	0.02	0.04	.	250.5	.
25/11/2014 19:45	0.05	0.02	0.03	.	250.75	.
25/11/2014 20:00	0.05	0.02	0.03	.	251	.
25/11/2014 20:15	0.06	0.02	0.04	.	251.25	.
25/11/2014 20:30	0.05	0.02	0.03	.	251.5	.
25/11/2014 20:45	0.05	0.02	0.03	.	251.75	.

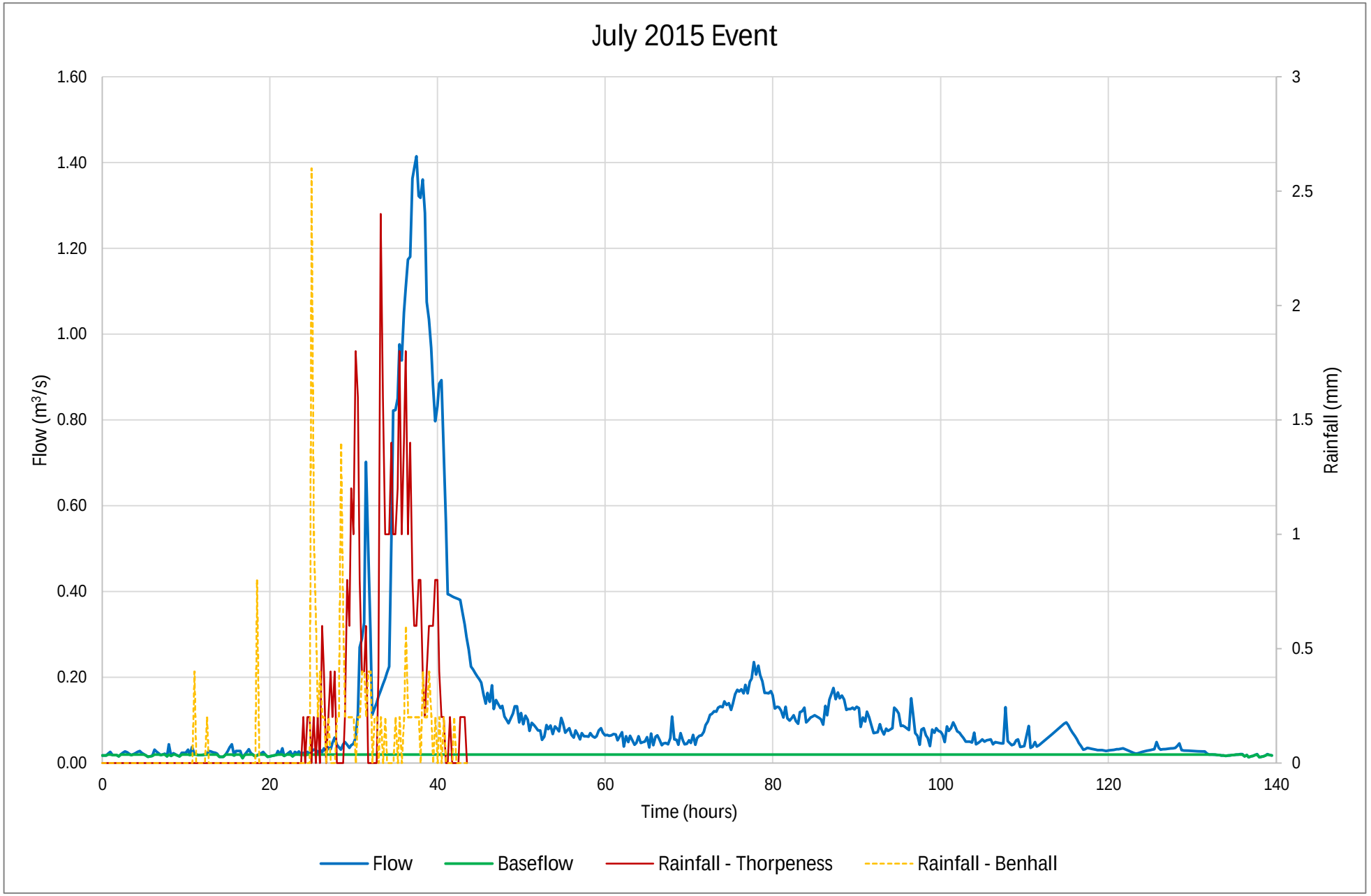
Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
25/11/2014 21:00	0.05	0.02	0.03	.	252	.
25/11/2014 21:15	0.06	0.02	0.04	0.2	252.25	0.2
25/11/2014 21:30	0.06	0.02	0.04	.	252.5	.
25/11/2014 21:45	0.05	0.02	0.03	.	252.75	.
25/11/2014 22:00	0.05	0.02	0.03	.	253	.
25/11/2014 22:15	0.05	0.02	0.03	.	253.25	.
25/11/2014 22:30	0.05	0.02	0.03	.	253.5	.
25/11/2014 22:45	0.05	0.02	0.03	.	253.75	.
25/11/2014 23:00	0.05	0.02	0.03	.	254	.
25/11/2014 23:15	0.05	0.02	0.03	.	254.25	.
25/11/2014 23:30	0.05	0.02	0.03	.	254.5	.
25/11/2014 23:45	0.05	0.02	0.03	.	254.75	.
26/11/2014 00:00	0.04	0.02	0.02	.	255	.
26/11/2014 00:15	0.05	0.02	0.03	0.6	255.25	.
26/11/2014 00:30	0.04	0.02	0.02	0.2	255.5	0.8
26/11/2014 00:45	0.04	0.02	0.02	.	255.75	0.4
26/11/2014 01:00	0.05	0.02	0.03	0.4	256	.
26/11/2014 01:15	0.04	0.02	0.02	.	256.25	0.2
26/11/2014 01:30	0.05	0.02	0.03	0.2	256.5	.

Catchment Area = Combined areas of LEIS ABBEY and LEIS LEISTON

Total Rain = rainfall only up to start of the event


July 2015 Event
1.60
1.40
1.20
1.00
0.80
0.60
0.40
0.20
0.00
Flow (m³/s)
3
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
20
40
60
80
100
120
140
Time (hours)
Flow
Baseflow
Rainfall - Thorpeness
Rainfall - Benhall

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
23/07/2015 13:00	0.02	0 02	0.00	.	0	.
23/07/2015 13:15	0.02	0 02	0.00	.	0.25	.
23/07/2015 13:30	0.02	0 02	0.00	.	0.5	.
23/07/2015 13:45	0.02	0 02	0.00	.	0.75	.
23/07/2015 14:00	0.03	0 02	0.01	.	1	.
23/07/2015 14:15	0.02	0 02	0.00	.	1.25	.
23/07/2015 14:30	0.02	0 02	0.00	.	1.5	.
23/07/2015 14:45	0.02	0 02	0.00	.	1.75	.
23/07/2015 15:00	0.02	0 02	0.00	.	2	.
23/07/2015 15:15	0.02	0 02	0.00	.	2.25	.
23/07/2015 15:30	0.02	0 02	0.00	.	2.5	.
23/07/2015 15:45	0.03	0 02	0.01	.	2.75	.
23/07/2015 16:00	0.02	0 02	0.00	.	3	.
23/07/2015 16:15	0.02	0 02	0.00	.	3.25	.
23/07/2015 16:30	0.02	0 02	0.00	.	3.5	.
23/07/2015 16:45	0.02	0 02	0.00	.	3.75	.
23/07/2015 17:00	0.02	0 02	0.00	.	4	.
23/07/2015 17:15	0.03	0 02	0.01	.	4.25	.
23/07/2015 17:30	0.03	0 02	0.01	.	4.5	.
23/07/2015 17:45	0.02	0 02	0.00	.	4.75	.
23/07/2015 18:00	0.02	0 02	0.00	.	5	.
23/07/2015 18:15	0.02	0 02	0.00	.	5.25	.
23/07/2015 18:30	0.01	0 01	0.00	.	5.5	.
23/07/2015 18:45	0.02	0 02	0.00	.	5.75	.
23/07/2015 19:00	0.02	0 02	0.00	.	6	.
23/07/2015 19:15	0.03	0 02	0.01	.	6.25	.
23/07/2015 19:30	0.03	0 02	0.01	.	6.5	.
23/07/2015 19:45	0.02	0 02	0.00	.	6.75	.
23/07/2015 20:00	0.02	0 02	0.00	.	7	.
23/07/2015 20:15	0.02	0 02	0.00	.	7.25	.
23/07/2015 20:30	0.02	0 02	0.00	.	7.5	.
23/07/2015 20:45	0.02	0 02	0.00	.	7.75	.
23/07/2015 21:00	0.04	0 02	0.02	.	8	.
23/07/2015 21:15	0.02	0 02	0.00	.	8.25	.
23/07/2015 21:30	0.02	0 02	0.00	.	8.5	.
23/07/2015 21:45	0.02	0 02	0.00	.	8.75	.
23/07/2015 22:00	0.02	0 02	0.00	.	9	.
23/07/2015 22:15	0.02	0 02	0.00	.	9.25	.
23/07/2015 22:30	0.02	0 02	0.00	.	9.5	.
23/07/2015 22:45	0.02	0 02	0.00	.	9.75	.
23/07/2015 23:00	0.02	0 02	0.00	.	10	.
23/07/2015 23:15	0.03	0 02	0.01	.	10.25	.
23/07/2015 23:30	0.02	0 02	0.00	.	10.5	.
23/07/2015 23:45	0.04	0 02	0.02	.	10.75	.
24/07/2015 00:00	0.02	0 02	0.00	.	11	0.4
24/07/2015 00:15	0.02	0 02	0.00	.	11.25	.
24/07/2015 00:30	0.02	0 02	0.00	.	11.5	.
24/07/2015 00:45	0.02	0 02	0.00	.	11.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

Thorpeness	
Area (km^2)	5.04
Total Rain (P) mm	42.6
Time Interval (hour)	0.25
Percentage Runoff	24%

Benhall	
Area (km^2)	5.04
Total Rain (P) mm	17.8
Time Interval (hour)	0.25
Percentage Runoff	57%

Average PR	40%

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
24/07/2015 01:00	0.02	0 02	0.00	.	12	.
24/07/2015 01:15	0.02	0 02	0.00	.	12.25	.
24/07/2015 01:30	0.02	0 02	0.00	.	12.5	0.2
24/07/2015 01:45	0.03	0 02	0.01	.	12.75	.
24/07/2015 02:00	0.03	0 02	0.01	.	13	.
24/07/2015 02:15	0.02	0 02	0.00	.	13.25	.
24/07/2015 02:30	0.02	0 02	0.00	.	13.5	.
24/07/2015 02:45	0.02	0 02	0.00	.	13.75	.
24/07/2015 03:00	0.01	0 01	0.00	.	14	.
24/07/2015 03:15	0.01	0 01	0.00	.	14.25	.
24/07/2015 03:30	0.01	0 01	0.00	.	14.5	.
24/07/2015 03:45	0.02	0 02	0.00	.	14.75	.
24/07/2015 04:00	0.03	0 02	0.01	.	15	.
24/07/2015 04:15	0.04	0 02	0.02	.	15.25	.
24/07/2015 04:30	0.04	0 02	0.02	.	15.5	.
24/07/2015 04:45	0.02	0 02	0.00	.	15.75	.
24/07/2015 05:00	0.03	0 02	0.01	.	16	.
24/07/2015 05:15	0.03	0 02	0.01	.	16.25	.
24/07/2015 05:30	0.03	0 02	0.01	.	16.5	.
24/07/2015 05:45	0.01	0 01	0.00	.	16.75	.
24/07/2015 06:00	0.02	0 02	0.00	.	17	.
24/07/2015 06:15	0.02	0 02	0.00	.	17.25	.
24/07/2015 06:30	0.03	0 02	0.01	.	17.5	.
24/07/2015 06:45	0.02	0 02	0.00	.	17.75	.
24/07/2015 07:00	0.02	0 02	0.00	.	18	.
24/07/2015 07:15	0.02	0 02	0.00	.	18.25	.
24/07/2015 07:30	0.02	0 02	0.00	.	18.5	0.8
24/07/2015 07:45	0.02	0 02	0.00	.	18.75	.
24/07/2015 08:00	0.02	0 02	0.00	.	19	.
24/07/2015 08:15	0.03	0 02	0.01	.	19.25	.
24/07/2015 08:30	0.02	0 02	0.00	.	19.5	.
24/07/2015 08:45	0.01	0 01	0.00	.	19.75	.
24/07/2015 09:00	0.02	0 02	0.00	.	20	.
24/07/2015 09:15	0.02	0 02	0.00	.	20.25	.
24/07/2015 09:30	0.02	0 02	0.00	.	20.5	.
24/07/2015 09:45	0.02	0 02	0.00	.	20.75	.
24/07/2015 10:00	0.03	0 02	0.01	.	21	.
24/07/2015 10:15	0.02	0 02	0.00	.	21.25	.
24/07/2015 10:30	0.03	0 02	0.01	.	21.5	.
24/07/2015 10:45	0.02	0 02	0.00	.	21.75	.
24/07/2015 11:00	0.02	0 02	0.00	.	22	.
24/07/2015 11:15	0.02	0 02	0.00	.	22.25	.
24/07/2015 11:30	0.03	0 02	0.01	.	22.5	.
24/07/2015 11:45	0.02	0 02	0.00	.	22.75	.
24/07/2015 12:00	0.03	0 02	0.01	.	23	.
24/07/2015 12:15	0.02	0 02	0.00	.	23.25	.
24/07/2015 12:30	0.03	0 02	0.01	.	23.5	.
24/07/2015 12:45	0.02	0 02	0.00	.	23.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
24/07/2015 13:00	0.02	0 02	0.00	0.2	24	.
24/07/2015 13:15	0.02	0 02	0.00	.	24.25	.
24/07/2015 13:30	0.03	0 02	0.01	0.2	24.5	.
24/07/2015 13:45	0.02	0 02	0.00	0.2	24.75	.
24/07/2015 14:00	0.03	0 02	0.01	.	25	2.6
24/07/2015 14:15	0.03	0 02	0.01	0.2	25.25	1
24/07/2015 14:30	0.03	0 02	0.01	.	25.5	0.6
24/07/2015 14:45	0.02	0 02	0.00	0.2	25.75	0.2
24/07/2015 15:00	0.03	0 02	0.01	.	26	0.4
24/07/2015 15:15	0.02	0 02	0.00	0.6	26.25	0.2
24/07/2015 15:30	0.03	0 02	0.01	0.4	26.5	0.2
24/07/2015 15:45	0.03	0 02	0.01	.	26.75	.
24/07/2015 16:00	0.04	0 02	0.02	0.2	27	0.2
24/07/2015 16:15	0.03	0 02	0.01	0.4	27.25	.
24/07/2015 16:30	0.05	0 02	0.03	0.2	27.5	.
24/07/2015 16:45	0.06	0 02	0.04	0.4	27.75	.
24/07/2015 17:00	0.04	0 02	0.02	.	28	0.2
24/07/2015 17:15	0.04	0 02	0.02	.	28.25	0.2
24/07/2015 17:30	0.03	0 02	0.01	.	28.5	1.4
24/07/2015 17:45	0.04	0 02	0.02	.	28.75	0.6
24/07/2015 18:00	0.05	0 02	0.03	0.2	29	0.2
24/07/2015 18:15	0.04	0 02	0.02	0.8	29.25	0.2
24/07/2015 18:30	0.04	0 02	0.02	0.6	29.5	0.2
24/07/2015 18:45	0.04	0 02	0.02	1.2	29.75	0.2
24/07/2015 19:00	0.04	0 02	0.02	1	30	0.2
24/07/2015 19:15	0.06	0 02	0.04	1.8	30.25	.
24/07/2015 19:30	0.11	0 02	0.09	1.6	30.5	0.2
24/07/2015 19:45	0.27	0 02	0.25	0.8	30.75	0.2
24/07/2015 20:00	0.29	0 02	0.27	0.4	31	0.4
24/07/2015 20:15	0.33	0 02	0.31	0.4	31.25	0.4
24/07/2015 20:30	0.70	0 02	0.68	0.6	31.5	0.2
24/07/2015 20:45	0.51	0 02	0.49	.	31.75	0.4
24/07/2015 21:00	0.31	0 02	0.29	.	32	0.4
24/07/2015 21:15	0.11	0 02	0.09	.	32.25	.
24/07/2015 21:30	0.13	0 02	0.11	.	32.5	0.2
24/07/2015 21:45	0.14	0 02	0.12	.	32.75	0.2
24/07/2015 22:00	0.15	0 02	0.13	0.4	33	.
24/07/2015 22:15	0.17	0 02	0.15	2.4	33.25	0.2
24/07/2015 22:30	0.18	0 02	0.16	1.6	33.5	.
24/07/2015 22:45	0.20	0 02	0.18	1	33.75	0.2
24/07/2015 23:00	0.21	0 02	0.19	1	34	.
24/07/2015 23:15	0.22	0 02	0.20	1	34.25	.
24/07/2015 23:30	0.52	0 02	0.50	1.4	34.5	.
24/07/2015 23:45	0.82	0 02	0.80	1	34.75	.
25/07/2015 00:00	0.82	0 02	0.80	1	35	0.2
25/07/2015 00:15	0.85	0 02	0.83	1.2	35.25	.
25/07/2015 00:30	0.98	0 02	0.96	1.8	35.5	0.2
25/07/2015 00:45	0.94	0 02	0.92	1	35.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
25/07/2015 01:00	1.05	0 02	1.03	1.4	36	0.2
25/07/2015 01:15	1.11	0 02	1.09	1.8	36.25	0.6
25/07/2015 01:30	1.17	0 02	1.15	1	36.5	0.2
25/07/2015 01:45	1.18	0 02	1.16	1.4	36.75	0.2
25/07/2015 02:00	1.36	0 02	1.34	0.8	37	0.2
25/07/2015 02:15	1.39	0 02	1.37	0.6	37.25	0.2
25/07/2015 02:30	1.42	0 02	1.40	0.6	37.5	0.2
25/07/2015 02:45	1.32	0 02	1.30	0.8	37.75	0.2
25/07/2015 03:00	1.32	0 02	1.30	0.8	38	.
25/07/2015 03:15	1.36	0 02	1.34	0.4	38.25	0.4
25/07/2015 03:30	1.28	0 02	1.26	0.2	38.5	0.2
25/07/2015 03:45	1.07	0 02	1.05	0.4	38.75	0.2
25/07/2015 04:00	1.03	0 02	1.01	0.6	39	0.4
25/07/2015 04:15	0.97	0 02	0.95	0.6	39.25	0.2
25/07/2015 04:30	0.88	0 02	0.86	0.6	39.5	.
25/07/2015 04:45	0.80	0 02	0.78	0.8	39.75	0.2
25/07/2015 05:00	0.83	0 02	0.81	0.8	40	.
25/07/2015 05:15	0.88	0 02	0.86	0.4	40.25	0.2
25/07/2015 05:30	0.89	0 02	0.87	0.2	40.5	.
25/07/2015 05:45	0.73	0 02	0.71	0.2	40.75	0.2
25/07/2015 06:00	0.56	0 02	0.54	.	41	.
25/07/2015 06:15	0.39	0 02	0.37	.	41.25	.
25/07/2015 06:30	0.39	0 02	0.37	0.2	41.5	.
25/07/2015 06:45	0.39	0 02	0.37	.	41.75	.
25/07/2015 07:00	0.39	0 02	0.37	.	42	0.2
25/07/2015 07:15	0.38	0 02	0.36	.	42.25	.
25/07/2015 07:30	0.38	0 02	0.36	.	42.5	.
25/07/2015 07:45	0.38	0 02	0.36	0.2	42.75	.
25/07/2015 08:00	0.35	0 02	0.33	0.2	43	.
25/07/2015 08:15	0.32	0 02	0.30	0.2	43.25	.
25/07/2015 08:30	0.29	0 02	0.27	.	43.5	.
25/07/2015 08:45	0.26	0 02	0.24	.	43.75	.
25/07/2015 09:00	0.23	0 02	0.21	.	44	.
25/07/2015 09:15	0.22	0 02	0.20	.	44.25	.
25/07/2015 09:30	0.21	0 02	0.19	.	44.5	.
25/07/2015 09:45	0.20	0 02	0.18	.	44.75	.
25/07/2015 10:00	0.19	0 02	0.17	.	45	.
25/07/2015 10:15	0.19	0 02	0.17	.	45.25	.
25/07/2015 10:30	0.16	0 02	0.14	.	45.5	.
25/07/2015 10:45	0.14	0 02	0.12	.	45.75	.
25/07/2015 11:00	0.16	0 02	0.14	.	46	.
25/07/2015 11:15	0.14	0 02	0.12	.	46.25	.
25/07/2015 11:30	0.18	0 02	0.16	.	46.5	.
25/07/2015 11:45	0.13	0 02	0.11	.	46.75	.
25/07/2015 12:00	0.15	0 02	0.13	.	47	.
25/07/2015 12:15	0.14	0 02	0.12	.	47.25	.
25/07/2015 12:30	0.13	0 02	0.11	.	47.5	.
25/07/2015 12:45	0.13	0 02	0.11	.	47.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
25/07/2015 13:00	0.11	0 02	0.09	.	48	.
25/07/2015 13:15	0.10	0 02	0.08	.	48.25	.
25/07/2015 13:30	0.09	0 02	0.07	.	48.5	.
25/07/2015 13:45	0.10	0 02	0.08	.	48.75	.
25/07/2015 14:00	0.12	0 02	0.10	.	49	.
25/07/2015 14:15	0.13	0 02	0.11	.	49.25	.
25/07/2015 14:30	0.13	0 02	0.11	.	49.5	0.6
25/07/2015 14:45	0.09	0 02	0.07	.	49.75	.
25/07/2015 15:00	0.12	0 02	0.10	.	50	.
25/07/2015 15:15	0.09	0 02	0.07	.	50.25	.
25/07/2015 15:30	0.11	0 02	0.09	.	50.5	.
25/07/2015 15:45	0.10	0 02	0.08	.	50.75	.
25/07/2015 16:00	0.07	0 02	0.05	.	51	.
25/07/2015 16:15	0.09	0 02	0.07	.	51.25	.
25/07/2015 16:30	0.09	0 02	0.07	.	51.5	.
25/07/2015 16:45	0.08	0 02	0.06	.	51.75	.
25/07/2015 17:00	0.08	0 02	0.06	.	52	.
25/07/2015 17:15	0.08	0 02	0.06	.	52.25	.
25/07/2015 17:30	0.05	0 02	0.03	.	52.5	.
25/07/2015 17:45	0.06	0 02	0.04	.	52.75	.
25/07/2015 18:00	0.09	0 02	0.07	.	53	0.8
25/07/2015 18:15	0.08	0 02	0.06	.	53.25	0.6
25/07/2015 18:30	0.09	0 02	0.07	.	53.5	1
25/07/2015 18:45	0.07	0 02	0.05	.	53.75	0.2
25/07/2015 19:00	0.09	0 02	0.07	.	54	0.2
25/07/2015 19:15	0.08	0 02	0.06	.	54.25	.
25/07/2015 19:30	0.07	0 02	0.05	.	54.5	0.2
25/07/2015 19:45	0.10	0 02	0.08	.	54.75	.
25/07/2015 20:00	0.09	0 02	0.07	.	55	.
25/07/2015 20:15	0.07	0 02	0.05	.	55.25	.
25/07/2015 20:30	0.08	0 02	0.06	.	55.5	.
25/07/2015 20:45	0.08	0 02	0.06	.	55.75	.
25/07/2015 21:00	0.06	0 02	0.04	.	56	.
25/07/2015 21:15	0.06	0 02	0.04	.	56.25	.
25/07/2015 21:30	0.08	0 02	0.06	.	56.5	.
25/07/2015 21:45	0.07	0 02	0.05	.	56.75	.
25/07/2015 22:00	0.05	0 02	0.03	.	57	.
25/07/2015 22:15	0.07	0 02	0.05	.	57.25	.
25/07/2015 22:30	0.06	0 02	0.04	.	57.5	0.8
25/07/2015 22:45	0.06	0 02	0.04	.	57.75	0.2
25/07/2015 23:00	0.06	0 02	0.04	.	58	.
25/07/2015 23:15	0.07	0 02	0.05	.	58.25	.
25/07/2015 23:30	0.06	0 02	0.04	.	58.5	.
25/07/2015 23:45	0.06	0 02	0.04	.	58.75	.
26/07/2015 00:00	0.06	0 02	0.04	.	59	.
26/07/2015 00:15	0.08	0 02	0.06	.	59.25	.
26/07/2015 00:30	0.08	0 02	0.06	.	59.5	.
26/07/2015 00:45	0.07	0 02	0.05	.	59.75	0.4

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
26/07/2015 01:00	0.06	0 02	0.04	.	60	.
26/07/2015 01:15	0.07	0 02	0.05	.	60.25	.
26/07/2015 01:30	0.06	0 02	0.04	.	60.5	.
26/07/2015 01:45	0.06	0 02	0.04	.	60.75	.
26/07/2015 02:00	0.07	0 02	0.05	.	61	.
26/07/2015 02:15	0.07	0 02	0.05	.	61.25	.
26/07/2015 02:30	0.05	0 02	0.03	.	61.5	0.8
26/07/2015 02:45	0.06	0 02	0.04	.	61.75	.
26/07/2015 03:00	0.07	0 02	0.05	.	62	.
26/07/2015 03:15	0.04	0 02	0.02	.	62.25	.
26/07/2015 03:30	0.06	0 02	0.04	.	62.5	.
26/07/2015 03:45	0.05	0 02	0.03	.	62.75	.
26/07/2015 04:00	0.06	0 02	0.04	.	63	.
26/07/2015 04:15	0.05	0 02	0.03	.	63.25	.
26/07/2015 04:30	0.04	0 02	0.02	.	63.5	.
26/07/2015 04:45	0.05	0 02	0.03	.	63.75	.
26/07/2015 05:00	0.06	0 02	0.04	.	64	.
26/07/2015 05:15	0.05	0 02	0.03	.	64.25	.
26/07/2015 05:30	0.05	0 02	0.03	.	64.5	.
26/07/2015 05:45	0.05	0 02	0.03	.	64.75	.
26/07/2015 06:00	0.06	0 02	0.04	.	65	.
26/07/2015 06:15	0.04	0 02	0.02	.	65.25	.
26/07/2015 06:30	0.07	0 02	0.05	.	65.5	.
26/07/2015 06:45	0.04	0 02	0.02	.	65.75	.
26/07/2015 07:00	0.06	0 02	0.04	.	66	.
26/07/2015 07:15	0.06	0 02	0.04	.	66.25	.
26/07/2015 07:30	0.05	0 02	0.03	.	66.5	.
26/07/2015 07:45	0.04	0 02	0.02	.	66.75	.
26/07/2015 08:00	0.05	0 02	0.03	.	67	.
26/07/2015 08:15	0.05	0 02	0.03	.	67.25	.
26/07/2015 08:30	0.04	0 02	0.02	.	67.5	.
26/07/2015 08:45	0.06	0 02	0.04	.	67.75	.
26/07/2015 09:00	0.11	0 02	0.09	.	68	.
26/07/2015 09:15	0.06	0 02	0.04	.	68.25	.
26/07/2015 09:30	0.05	0 02	0.03	.	68.5	.
26/07/2015 09:45	0.04	0 02	0.02	.	68.75	.
26/07/2015 10:00	0.07	0 02	0.05	.	69	.
26/07/2015 10:15	0.05	0 02	0.03	.	69.25	.
26/07/2015 10:30	0.04	0 02	0.02	.	69.5	.
26/07/2015 10:45	0.04	0 02	0.02	0.4	69.75	.
26/07/2015 11:00	0.05	0 02	0.03	0.4	70	.
26/07/2015 11:15	0.05	0 02	0.03	.	70.25	.
26/07/2015 11:30	0.07	0 02	0.05	0.2	70.5	.
26/07/2015 11:45	0.04	0 02	0.02	0.4	70.75	0.2
26/07/2015 12:00	0.06	0 02	0.04	0.4	71	.
26/07/2015 12:15	0.06	0 02	0.04	0.4	71.25	.
26/07/2015 12:30	0.06	0 02	0.04	0.6	71.5	.
26/07/2015 12:45	0.07	0 02	0.05	0.2	71.75	0.2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
26/07/2015 13:00	0.09	0 02	0.07	0.2	72	.
26/07/2015 13:15	0.10	0 02	0.08	1.4	72.25	.
26/07/2015 13:30	0.11	0 02	0.09	0.8	72.5	.
26/07/2015 13:45	0.11	0 02	0.09	1.2	72.75	.
26/07/2015 14:00	0.12	0 02	0.10	0.4	73	.
26/07/2015 14:15	0.12	0 02	0.10	0.4	73.25	.
26/07/2015 14:30	0.13	0 02	0.11	.	73.5	.
26/07/2015 14:45	0.13	0 02	0.11	.	73.75	.
26/07/2015 15:00	0.13	0 02	0.11	0.2	74	.
26/07/2015 15:15	0.14	0 02	0.12	.	74.25	.
26/07/2015 15:30	0.13	0 02	0.11	0.4	74.5	.
26/07/2015 15:45	0.14	0 02	0.12	0.2	74.75	.
26/07/2015 16:00	0.12	0 02	0.10	0.4	75	.
26/07/2015 16:15	0.14	0 02	0.12	0.4	75.25	.
26/07/2015 16:30	0.16	0 02	0.14	0.2	75.5	.
26/07/2015 16:45	0.17	0 02	0.15	.	75.75	.
26/07/2015 17:00	0.17	0 02	0.15	0.2	76	.
26/07/2015 17:15	0.17	0 02	0.15	0.2	76.25	.
26/07/2015 17:30	0.16	0 02	0.14	0.8	76.5	.
26/07/2015 17:45	0.18	0 02	0.16	0.4	76.75	.
26/07/2015 18:00	0.16	0 02	0.14	0.8	77	.
26/07/2015 18:15	0.19	0 02	0.17	0.4	77.25	.
26/07/2015 18:30	0.20	0 02	0.18	0.2	77.5	.
26/07/2015 18:45	0.23	0 02	0.21	.	77.75	.
26/07/2015 19:00	0.21	0 02	0.19	.	78	.
26/07/2015 19:15	0.23	0 02	0.21	.	78.25	.
26/07/2015 19:30	0.20	0 02	0.18	0.2	78.5	.
26/07/2015 19:45	0.19	0 02	0.17	.	78.75	0.2
26/07/2015 20:00	0.16	0 02	0.14	.	79	.
26/07/2015 20:15	0.16	0 02	0.14	0.2	79.25	.
26/07/2015 20:30	0.16	0 02	0.14	.	79.5	.
26/07/2015 20:45	0.17	0 02	0.15	.	79.75	.
26/07/2015 21:00	0.16	0 02	0.14	.	80	.
26/07/2015 21:15	0.13	0 02	0.11	.	80.25	.
26/07/2015 21:30	0.13	0 02	0.11	.	80.5	.
26/07/2015 21:45	0.13	0 02	0.11	.	80.75	.
26/07/2015 22:00	0.12	0 02	0.10	.	81	.
26/07/2015 22:15	0.11	0 02	0.09	.	81.25	.
26/07/2015 22:30	0.13	0 02	0.11	.	81.5	.
26/07/2015 22:45	0.10	0 02	0.08	.	81.75	.
26/07/2015 23:00	0.10	0 02	0.08	.	82	.
26/07/2015 23:15	0.10	0 02	0.08	0.2	82.25	.
26/07/2015 23:30	0.11	0 02	0.09	0.2	82.5	.
26/07/2015 23:45	0.10	0 02	0.08	.	82.75	.
27/07/2015 00:00	0.09	0 02	0.07	.	83	.
27/07/2015 00:15	0.12	0 02	0.10	.	83.25	.
27/07/2015 00:30	0.12	0 02	0.10	.	83.5	.
27/07/2015 00:45	0.13	0 02	0.11	.	83.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
27/07/2015 01:00	0.09	0 02	0.07	.	84	.
27/07/2015 01:15	0.10	0 02	0.08	.	84.25	.
27/07/2015 01:30	0.11	0 02	0.09	.	84.5	.
27/07/2015 01:45	0.11	0 02	0.09	.	84.75	.
27/07/2015 02:00	0.11	0 02	0.09	.	85	.
27/07/2015 02:15	0.11	0 02	0.09	0.4	85.25	.
27/07/2015 02:30	0.10	0 02	0.08	0.2	85.5	.
27/07/2015 02:45	0.10	0 02	0.08	0.8	85.75	.
27/07/2015 03:00	0.09	0 02	0.07	0.6	86	.
27/07/2015 03:15	0.13	0 02	0.11	0.8	86.25	.
27/07/2015 03:30	0.11	0 02	0.09	.	86.5	.
27/07/2015 03:45	0.15	0 02	0.13	.	86.75	.
27/07/2015 04:00	0.16	0 02	0.14	.	87	.
27/07/2015 04:15	0.17	0 02	0.15	.	87.25	.
27/07/2015 04:30	0.15	0 02	0.13	.	87.5	.
27/07/2015 04:45	0.16	0 02	0.14	.	87.75	.
27/07/2015 05:00	0.15	0 02	0.13	.	88	.
27/07/2015 05:15	0.16	0 02	0.14	0.2	88.25	.
27/07/2015 05:30	0.15	0 02	0.13	.	88.5	.
27/07/2015 05:45	0.12	0 02	0.10	.	88.75	.
27/07/2015 06:00	0.13	0 02	0.11	.	89	.
27/07/2015 06:15	0.13	0 02	0.11	.	89.25	.
27/07/2015 06:30	0.13	0 02	0.11	.	89.5	.
27/07/2015 06:45	0.12	0 02	0.10	.	89.75	.
27/07/2015 07:00	0.13	0 02	0.11	.	90	.
27/07/2015 07:15	0.13	0 02	0.11	.	90.25	.
27/07/2015 07:30	0.08	0 02	0.06	.	90.5	.
27/07/2015 07:45	0.11	0 02	0.09	.	90.75	.
27/07/2015 08:00	0.10	0 02	0.08	.	91	.
27/07/2015 08:15	0.12	0 02	0.10	.	91.25	.
27/07/2015 08:30	0.11	0 02	0.09	.	91.5	.
27/07/2015 08:45	0.09	0 02	0.07	.	91.75	.
27/07/2015 09:00	0.07	0 02	0.05	.	92	.
27/07/2015 09:15	0.07	0 02	0.05	.	92.25	.
27/07/2015 09:30	0.07	0 02	0.05	.	92.5	.
27/07/2015 09:45	0.09	0 02	0.07	.	92.75	.
27/07/2015 10:00	0.08	0 02	0.06	.	93	.
27/07/2015 10:15	0.07	0 02	0.05	.	93.25	.
27/07/2015 10:30	0.08	0 02	0.06	.	93.5	.
27/07/2015 10:45	0.07	0 02	0.05	.	93.75	.
27/07/2015 11:00	0.08	0 02	0.06	.	94	.
27/07/2015 11:15	0.08	0 02	0.06	.	94.25	.
27/07/2015 11:30	0.13	0 02	0.11	.	94.5	.
27/07/2015 11:45	0.12	0 02	0.10	.	94.75	.
27/07/2015 12:00	0.12	0 02	0.10	.	95	.
27/07/2015 12:15	0.09	0 02	0.07	.	95.25	.
27/07/2015 12:30	0.09	0 02	0.07	.	95.5	.
27/07/2015 12:45	0.08	0 02	0.06	.	95.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
27/07/2015 13:00	0.08	0 02	0.06	.	96	.
27/07/2015 13:15	0.08	0 02	0.06	.	96.25	.
27/07/2015 13:30	0.15	0 02	0.13	.	96.5	.
27/07/2015 13:45	0.11	0 02	0.09	0.2	96.75	.
27/07/2015 14:00	0.07	0 02	0.05	.	97	.
27/07/2015 14:15	0.06	0 02	0.04	.	97.25	.
27/07/2015 14:30	0.04	0 02	0.02	.	97.5	.
27/07/2015 14:45	0.08	0 02	0.06	.	97.75	.
27/07/2015 15:00	0.08	0 02	0.06	.	98	.
27/07/2015 15:15	0.06	0 02	0.04	.	98.25	.
27/07/2015 15:30	0.06	0 02	0.04	.	98.5	.
27/07/2015 15:45	0.04	0 02	0.02	.	98.75	.
27/07/2015 16:00	0.08	0 02	0.06	.	99	.
27/07/2015 16:15	0.07	0 02	0.05	.	99.25	.
27/07/2015 16:30	0.08	0 02	0.06	.	99.5	.
27/07/2015 16:45	0.07	0 02	0.05	.	99.75	.
27/07/2015 17:00	0.07	0 02	0.05	.	100	.
27/07/2015 17:15	0.07	0 02	0.05	.	100.25	.
27/07/2015 17:30	0.05	0 02	0.03	.	100.5	.
27/07/2015 17:45	0.09	0 02	0.07	.	100.75	.
27/07/2015 18:00	0.07	0 02	0.05	.	101	.
27/07/2015 18:15	0.08	0 02	0.06	.	101.25	.
27/07/2015 18:30	0.09	0 02	0.07	.	101.5	.
27/07/2015 18:45	0.09	0 02	0.07	.	101.75	.
27/07/2015 19:00	0.07	0 02	0.05	.	102	.
27/07/2015 19:15	0.07	0 02	0.05	.	102.25	.
27/07/2015 19:30	0.06	0 02	0.04	.	102.5	.
27/07/2015 19:45	0.06	0 02	0.04	.	102.75	.
27/07/2015 20:00	0.05	0 02	0.03	.	103	0.2
27/07/2015 20:15	0.05	0 02	0.03	.	103.25	0.2
27/07/2015 20:30	0.05	0 02	0.03	.	103.5	.
27/07/2015 20:45	0.05	0 02	0.03	.	103.75	.
27/07/2015 21:00	0.07	0 02	0.05	.	104	.
27/07/2015 21:15	0.04	0 02	0.02	.	104.25	.
27/07/2015 21:30	0.05	0 02	0.03	.	104.5	.
27/07/2015 21:45	0.05	0 02	0.03	.	104.75	.
27/07/2015 22:00	0.05	0 02	0.03	.	105	.
27/07/2015 22:15	0.05	0 02	0.03	.	105.25	.
27/07/2015 22:30	0.05	0 02	0.03	.	105.5	.
27/07/2015 22:45	0.05	0 02	0.03	.	105.75	.
27/07/2015 23:00	0.05	0 02	0.03	.	106	.
27/07/2015 23:15	0.04	0 02	0.02	.	106.25	.
27/07/2015 23:30	0.05	0 02	0.03	.	106.5	.
27/07/2015 23:45	0.05	0 02	0.03	.	106.75	.
28/07/2015 00:00	0.05	0 02	0.03	.	107	.
28/07/2015 00:15	0.05	0 02	0.03	.	107.25	.
28/07/2015 00:30	0.05	0 02	0.03	.	107.5	.
28/07/2015 00:45	0.13	0 02	0.11	.	107.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
28/07/2015 01:00	0.05	0 02	0.03	.	108	.
28/07/2015 01:15	0.05	0 02	0.03	.	108.25	.
28/07/2015 01:30	0.04	0 02	0.02	.	108.5	.
28/07/2015 01:45	0.04	0 02	0.02	.	108.75	.
28/07/2015 02:00	0.05	0 02	0.03	.	109	.
28/07/2015 02:15	0.05	0 02	0.03	.	109.25	.
28/07/2015 02:30	0.04	0 02	0.02	.	109.5	.
28/07/2015 02:45	0.04	0 02	0.02	.	109.75	.
28/07/2015 03:00	0.04	0 02	0.02	.	110	.
28/07/2015 03:15	0.06	0 02	0.04	.	110.25	.
28/07/2015 03:30	0.09	0 02	0.07	.	110.5	.
28/07/2015 03:45	0.04	0 02	0.02	.	110.75	.
28/07/2015 04:00	0.04	0 02	0.02	.	111	.
28/07/2015 04:15	0.05	0 02	0.03	.	111.25	.
28/07/2015 04:30	0.04	0 02	0.02	.	111.5	.
28/07/2015 04:45	0.04	0 02	0.02	.	111.75	.
28/07/2015 05:00	0.05	0 02	0.03	.	112	.
28/07/2015 05:15	0.05	0 02	0.03	.	112.25	.
28/07/2015 05:30	0.05	0 02	0.03	.	112.5	.
28/07/2015 05:45	0.06	0 02	0.04	.	112.75	.
28/07/2015 06:00	0.06	0 02	0.04	.	113	.
28/07/2015 06:15	0.07	0 02	0.05	.	113.25	.
28/07/2015 06:30	0.07	0 02	0.05	.	113.5	.
28/07/2015 06:45	0.07	0 02	0.05	.	113.75	.
28/07/2015 07:00	0.08	0 02	0.06	.	114	.
28/07/2015 07:15	0.08	0 02	0.06	.	114.25	.
28/07/2015 07:30	0.09	0 02	0.07	.	114.5	.
28/07/2015 07:45	0.09	0 02	0.07	.	114.75	.
28/07/2015 08:00	0.09	0 02	0.07	.	115	.
28/07/2015 08:15	0.09	0 02	0.07	.	115.25	.
28/07/2015 08:30	0.08	0 02	0.06	.	115.5	.
28/07/2015 08:45	0.07	0 02	0.05	.	115.75	.
28/07/2015 09:00	0.06	0 02	0.04	.	116	.
28/07/2015 09:15	0.05	0 02	0.03	.	116.25	.
28/07/2015 09:30	0.05	0 02	0.03	.	116.5	.
28/07/2015 09:45	0.04	0 02	0.02	.	116.75	.
28/07/2015 10:00	0.03	0 02	0.01	.	117	.
28/07/2015 10:15	0.03	0 02	0.01	.	117.25	.
28/07/2015 10:30	0.03	0 02	0.01	.	117.5	.
28/07/2015 10:45	0.03	0 02	0.01	.	117.75	.
28/07/2015 11:00	0.03	0 02	0.01	.	118	.
28/07/2015 11:15	0.03	0 02	0.01	.	118.25	.
28/07/2015 11:30	0.03	0 02	0.01	.	118.5	.
28/07/2015 11:45	0.03	0 02	0.01	.	118.75	.
28/07/2015 12:00	0.03	0 02	0.01	.	119	.
28/07/2015 12:15	0.03	0 02	0.01	.	119.25	.
28/07/2015 12:30	0.03	0 02	0.01	.	119.5	.
28/07/2015 12:45	0.03	0 02	0.01	.	119.75	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
28/07/2015 13:00	0.03	0 02	0.01	.	120	.
28/07/2015 13:15	0.03	0 02	0.01	.	120.25	.
28/07/2015 13:30	0.03	0 02	0.01	.	120.5	.
28/07/2015 13:45	0.03	0 02	0.01	.	120.75	.
28/07/2015 14:00	0.03	0 02	0.01	.	121	.
28/07/2015 14:15	0.03	0 02	0.01	.	121.25	.
28/07/2015 14:30	0.03	0 02	0.01	.	121.5	.
28/07/2015 14:45	0.03	0 02	0.01	.	121.75	.
28/07/2015 15:00	0.03	0 02	0.01	.	122	.
28/07/2015 15:15	0.03	0 02	0.01	0.2	122.25	.
28/07/2015 15:30	0.03	0 02	0.01	0.6	122.5	.
28/07/2015 15:45	0.03	0 02	0.01	.	122.75	.
28/07/2015 16:00	0.02	0 02	0.00	.	123	.
28/07/2015 16:15	0.02	0 02	0.00	1.4	123.25	.
28/07/2015 16:30	0.02	0 02	0.00	0.2	123.5	.
28/07/2015 16:45	0.02	0 02	0.00	.	123.75	.
28/07/2015 17:00	0.03	0 02	0.01	.	124	.
28/07/2015 17:15	0.03	0 02	0.01	.	124.25	.
28/07/2015 17:30	0.03	0 02	0.01	.	124.5	.
28/07/2015 17:45	0.03	0 02	0.01	.	124.75	.
28/07/2015 18:00	0.03	0 02	0.01	.	125	.
28/07/2015 18:15	0.03	0 02	0.01	.	125.25	.
28/07/2015 18:30	0.03	0 02	0.01	.	125.5	.
28/07/2015 18:45	0.05	0 02	0.03	.	125.75	.
28/07/2015 19:00	0.04	0 02	0.02	.	126	.
28/07/2015 19:15	0.03	0 02	0.01	.	126.25	.
28/07/2015 19:30	0.03	0 02	0.01	.	126.5	.
28/07/2015 19:45	0.03	0 02	0.01	.	126.75	.
28/07/2015 20:00	0.03	0 02	0.01	.	127	.
28/07/2015 20:15	0.03	0 02	0.01	.	127.25	.
28/07/2015 20:30	0.03	0 02	0.01	.	127.5	.
28/07/2015 20:45	0.03	0 02	0.01	.	127.75	.
28/07/2015 21:00	0.03	0 02	0.01	.	128	.
28/07/2015 21:15	0.04	0 02	0.02	.	128.25	.
28/07/2015 21:30	0.05	0 02	0.03	.	128.5	.
28/07/2015 21:45	0.03	0 02	0.01	.	128.75	.
28/07/2015 22:00	0.03	0 02	0.01	.	129	.
28/07/2015 22:15	0.03	0 02	0.01	.	129.25	.
28/07/2015 22:30	0.03	0 02	0.01	.	129.5	.
28/07/2015 22:45	0.03	0 02	0.01	.	129.75	.
28/07/2015 23:00	0.03	0 02	0.01	.	130	.
28/07/2015 23:15	0.03	0 02	0.01	.	130.25	.
28/07/2015 23:30	0.03	0 02	0.01	.	130.5	.
28/07/2015 23:45	0.03	0 02	0.01	.	130.75	.
29/07/2015 00:00	0.03	0 02	0.01	.	131	.
29/07/2015 00:15	0.03	0 02	0.01	.	131.25	.
29/07/2015 00:30	0.03	0 02	0.01	.	131.5	.
29/07/2015 00:45	0.02	0 02	0.00	.	131.75	.

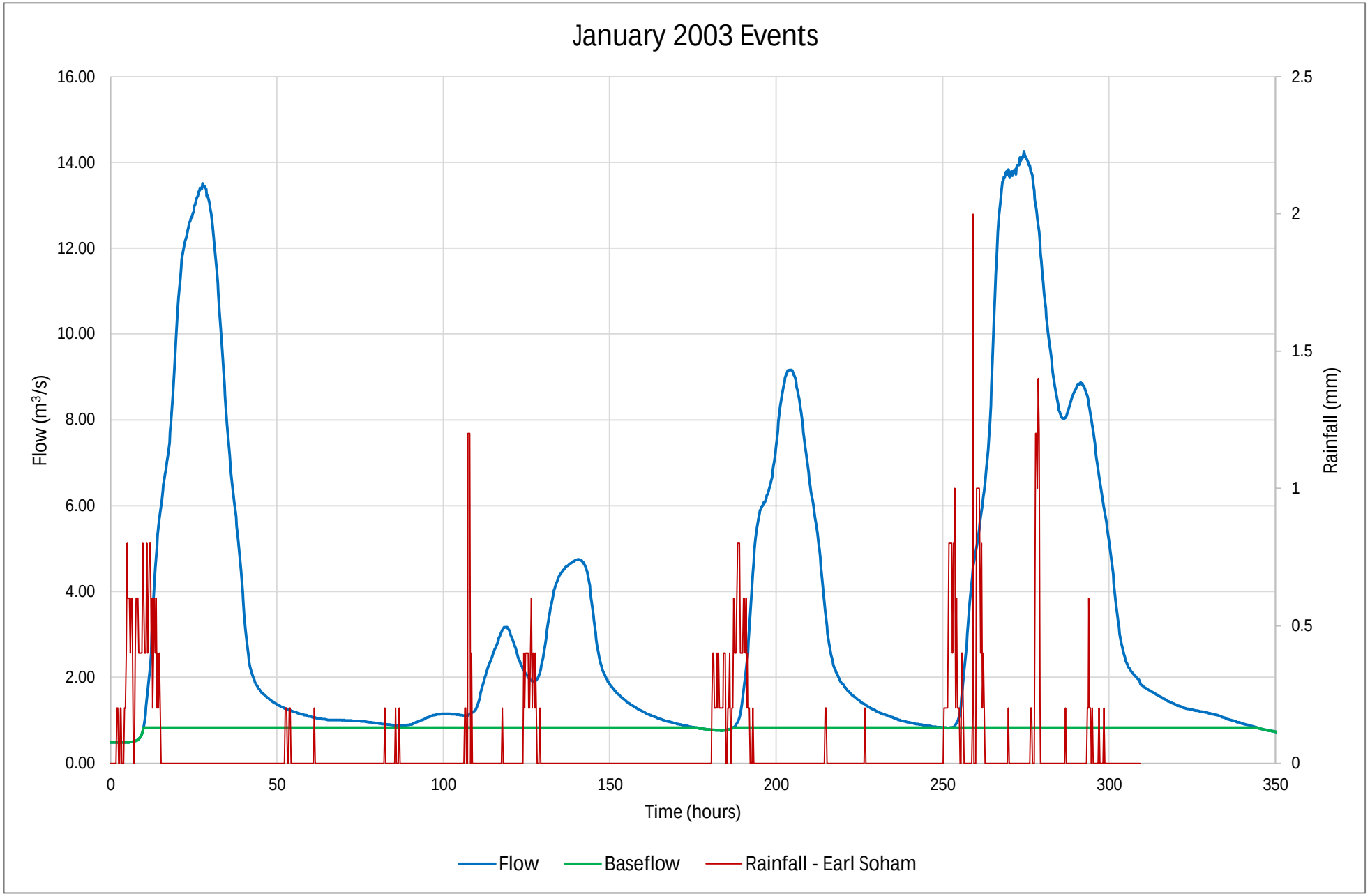
Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event

	G5			Thorpeness		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
29/07/2015 01:00	0.02	0 02	0.00	.	132	.
29/07/2015 01:15	0.02	0 02	0.00	.	132.25	.
29/07/2015 01:30	0.02	0 02	0.00	.	132.5	.
29/07/2015 01:45	0.02	0 02	0.00	.	132.75	.
29/07/2015 02:00	0.02	0 02	0.00	.	133	.
29/07/2015 02:15	0.02	0 02	0.00	.	133.25	.
29/07/2015 02:30	0.02	0 02	0.00	.	133.5	.
29/07/2015 02:45	0.02	0 02	0.00	.	133.75	.
29/07/2015 03:00	0.02	0 02	0.00	.	134	.
29/07/2015 03:15	0.02	0 02	0.00	.	134.25	.
29/07/2015 03:30	0.02	0 02	0.00	.	134.5	.
29/07/2015 03:45	0.02	0 02	0.00	.	134.75	.
29/07/2015 04:00	0.02	0 02	0.00	.	135	.
29/07/2015 04:15	0.02	0 02	0.00	.	135.25	.
29/07/2015 04:30	0.02	0 02	0.00	.	135.5	.
29/07/2015 04:45	0.02	0 02	0.00	.	135.75	.
29/07/2015 05:00	0.02	0 02	0.00	.	136	.
29/07/2015 05:15	0.01	0 01	0.00	.	136.25	.
29/07/2015 05:30	0.02	0 02	0.00	.	136.5	.
29/07/2015 05:45	0.01	0 01	0.00	.	136.75	.
29/07/2015 06:00	0.02	0 02	0.00	.	137	.
29/07/2015 06:15	0.02	0 02	0.00	.	137.25	.
29/07/2015 06:30	0.02	0 02	0.00	.	137.5	.
29/07/2015 06:45	0.02	0 02	0.00	.	137.75	.
29/07/2015 07:00	0.01	0 01	0.00	.	138	.
29/07/2015 07:15	0.01	0 01	0.00	.	138.25	.
29/07/2015 07:30	0.02	0 02	0.00	.	138.5	.
29/07/2015 07:45	0.02	0 02	0.00	.	138.75	.
29/07/2015 08:00	0.02	0 02	0.00	.	139	.
29/07/2015 08:15	0.02	0 02	0.00	.	139.25	.
29/07/2015 08:30	0.02	0 02	0.00	.	139.5	.

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

Total Rain = rainfall only up to start of the event


January 2003 Events
16.00
14.00
12.00
10.00
8.00
6.00
4.00
2.00
0.00
Flow (m³/s)
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
50
100
150
200
250
300
350
Time (hours)
Flow
Baseflow
Rainfall - Earl Soham

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
21/12/2002 19:15	0.48	0.48	0.00	0	0
21/12/2002 19:30	0.48	0.48	0.00	0	0.25
21/12/2002 19:45	0.48	0.48	0.00	0	0.5
21/12/2002 20:00	0.48	0.48	0.00	0	0.75
21/12/2002 20:15	0.48	0.48	0.00	0	1
21/12/2002 20:30	0.48	0.48	0.00	0	1.25
21/12/2002 20:45	0.48	0.48	0.00	0	1.5
21/12/2002 21:00	0.48	0.48	0.00	0	1.75
21/12/2002 21:15	0.48	0.48	0.00	0.2	2
21/12/2002 21:30	0.48	0.48	0.00	0.2	2.25
21/12/2002 21:45	0.48	0.48	0.00	0	2.5
21/12/2002 22:00	0.48	0.48	0.00	0	2.75
21/12/2002 22:15	0.48	0.48	0.00	0.2	3
21/12/2002 22:30	0.48	0.48	0.00	0.2	3.25
21/12/2002 22:45	0.48	0.48	0.00	0	3.5
21/12/2002 23:00	0.48	0.48	0.00	0	3.75
21/12/2002 23:15	0.48	0.48	0.00	0	4
21/12/2002 23:30	0.48	0.48	0.00	0.2	4.25
21/12/2002 23:45	0.48	0.48	0.00	0.2	4.5
22/12/2002 00:00	0.48	0.48	0.00	0.4	4.75
22/12/2002 00:15	0.48	0.48	0.00	0.8	5
22/12/2002 00:30	0.49	0.49	0.00	0.6	5.25
22/12/2002 00:45	0.49	0.49	0.00	0.6	5.5
22/12/2002 01:00	0.49	0.49	0.00	0.6	5.75
22/12/2002 01:15	0.49	0.49	0.00	0.4	6
22/12/2002 01:30	0.49	0.49	0.00	0.6	6.25
22/12/2002 01:45	0.50	0.50	0.00	0.6	6.5
22/12/2002 02:00	0.50	0.50	0.00	0.2	6.75
22/12/2002 02:15	0.51	0.51	0.00	0	7
22/12/2002 02:30	0.51	0.51	0.00	0	7.25
22/12/2002 02:45	0.52	0.52	0.00	0.4	7.5
22/12/2002 03:00	0.53	0.53	0.00	0.6	7.75
22/12/2002 03:15	0.53	0.53	0.00	0.6	8
22/12/2002 03:30	0.54	0.54	0.00	0.6	8.25
22/12/2002 03:45	0.55	0.55	0.00	0.4	8.5
22/12/2002 04:00	0.57	0.57	0.00	0.4	8.75
22/12/2002 04:15	0.60	0.60	0.00	0.4	9
22/12/2002 04:30	0.63	0.63	0.00	0.4	9.25
22/12/2002 04:45	0.68	0.68	0.00	0.4	9.5
22/12/2002 05:00	0.75	0.75	0.00	0.8	9.75
22/12/2002 05:15	0.84	0.83	0.01	0.6	10
22/12/2002 05:30	0.97	0.83	0.14	0.4	10.25

First peak	
Area (km^2)	50.16
Total Rain (P) mm	20.8
Time Interval (hour)	0.25
Percentage Runoff	89%

Second peak	
Area (km^2)	50.16
Total Rain (P) mm	10.8
Time Interval (hour)	0.25
Percentage Runoff	69%

Third peak	
Area (km^2)	50.16
Total Rain (P) mm	16.00
Time Interval (hour)	0.25
Percentage Runoff	70%

Fourth peak	
Area (km^2)	50.16
Total Rain (P) mm	28.6
Time Interval (hour)	0.25
Percentage Runoff	102%

Average PR	83%

Benhall or Thorpeness rainfall gauge data was not avaialble for this event

Overall Average	67%

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
22/12/2002 05:45	1.12	0.83	0.29	0.4	10.5		
22/12/2002 06:00	1.30	0.83	0.47	0.4	10.75		
22/12/2002 06:15	1.50	0.83	0.67	0.8	11		
22/12/2002 06:30	1.69	0.83	0.86	0.4	11.25		
22/12/2002 06:45	1.89	0.83	1.06	0.6	11.5		
22/12/2002 07:00	2.09	0.83	1.26	0.8	11.75		
22/12/2002 07:15	2.30	0.83	1.47	0.8	12		
22/12/2002 07:30	2.58	0.83	1.75	0.4	12.25		
22/12/2002 07:45	2.99	0.83	2.16	0.6	12.5		
22/12/2002 08:00	3.42	0.83	2.59	0.2	12.75		
22/12/2002 08:15	3.83	0.83	3.00	0.4	13		
22/12/2002 08:30	4.21	0.83	3.38	0.6	13.25		
22/12/2002 08:45	4.55	0.83	3.72	0.4	13.5		
22/12/2002 09:00	4.81	0.83	3.98	0.6	13.75		
22/12/2002 09:15	5.08	0.83	4.25	0.2	14		
22/12/2002 09:30	5.31	0.83	4.48	0.4	14.25		
22/12/2002 09:45	5.51	0.83	4.68	0.2	14.5		
22/12/2002 10:00	5.69	0.83	4.86	0.4	14.75		
22/12/2002 10:15	5.85	0.83	5.02	0.2	15		
22/12/2002 10:30	6.00	0.83	5.17	0	15.25		
22/12/2002 10:45	6.15	0.83	5.32	0	15.5		
22/12/2002 11:00	6.35	0.83	5.52	0	15.75		
22/12/2002 11:15	6.49	0.83	5.66	0	16		
22/12/2002 11:30	6.62	0.83	5.79	0	16.25		
22/12/2002 11:45	6.74	0.83	5.91	0	16.5		
22/12/2002 12:00	6.86	0.83	6.03	0	16.75		
22/12/2002 12:15	7.02	0.83	6.19	0	17		
22/12/2002 12:30	7.15	0.83	6.32	0	17.25		
22/12/2002 12:45	7.31	0.83	6.48	0	17.5		
22/12/2002 13:00	7.47	0.83	6.64	0	17.75		
22/12/2002 13:15	7.73	0.83	6.90	0	18		
22/12/2002 13:30	7.94	0.83	7.11	0	18.25		
22/12/2002 13:45	8.24	0.83	7.41	0	18.5		
22/12/2002 14:00	8.54	0.83	7.71	0	18.75		
22/12/2002 14:15	8.88	0.83	8.05	0	19		
22/12/2002 14:30	9.26	0.83	8.43	0	19.25		
22/12/2002 14:45	9.54	0.83	8.71	0	19.5		
22/12/2002 15:00	9.88	0.83	9.05	0	19.75		
22/12/2002 15:15	10.20	0.83	9.37	0	20		
22/12/2002 15:30	10.57	0.83	9.74	0	20.25		
22/12/2002 15:45	10.86	0.83	10.03	0	20.5		
22/12/2002 16:00	11.08	0.83	10.25	0	20.75		

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
22/12/2002 16:15	11.29	0.83	10.46	0	21
22/12/2002 16:30	11.55	0.83	10.72	0	21.25
22/12/2002 16:45	11.74	0.83	10.91	0	21.5
22/12/2002 17:00	11.86	0.83	11.03	0	21.75
22/12/2002 17:15	11.97	0.83	11.14	0	22
22/12/2002 17:30	12.09	0.83	11.26	0	22.25
22/12/2002 17:45	12.17	0.83	11.34	0	22.5
22/12/2002 18:00	12.23	0.83	11.40	0	22.75
22/12/2002 18:15	12.32	0.83	11.49	0	23
22/12/2002 18:30	12.44	0.83	11.61	0	23.25
22/12/2002 18:45	12.47	0.83	11.64	0	23.5
22/12/2002 19:00	12.60	0.83	11.77	0	23.75
22/12/2002 19:15	12.63	0.83	11.80	0	24
22/12/2002 19:30	12.72	0.83	11.89	0	24.25
22/12/2002 19:45	12.72	0.83	11.89	0	24.5
22/12/2002 20:00	12.82	0.83	11.99	0	24.75
22/12/2002 20:15	12.85	0.83	12.02	0	25
22/12/2002 20:30	12.98	0.83	12.15	0	25.25
22/12/2002 20:45	13.01	0.83	12.18	0	25.5
22/12/2002 21:00	13.11	0.83	12.28	0	25.75
22/12/2002 21:15	13.17	0.83	12.34	0	26
22/12/2002 21:30	13.21	0.83	12.38	0	26.25
22/12/2002 21:45	13.31	0.83	12.48	0	26.5
22/12/2002 22:00	13.34	0.83	12.51	0	26.75
22/12/2002 22:15	13.41	0.83	12.58	0	27
22/12/2002 22:30	13.38	0.83	12.55	0	27.25
22/12/2002 22:45	13.38	0.83	12.55	0	27.5
22/12/2002 23:00	13.51	0.83	12.68	0	27.75
22/12/2002 23:15	13.44	0.83	12.61	0	28
22/12/2002 23:30	13.44	0.83	12.61	0	28.25
22/12/2002 23:45	13.41	0.83	12.58	0	28.5
23/12/2002 00:00	13.38	0.83	12.55	0	28.75
23/12/2002 00:15	13.21	0.83	12.38	0	29
23/12/2002 00:30	13.24	0.83	12.41	0	29.25
23/12/2002 00:45	13.14	0.83	12.31	0	29.5
23/12/2002 01:00	13.08	0.83	12.25	0	29.75
23/12/2002 01:15	12.91	0.83	12.08	0	30
23/12/2002 01:30	12.82	0.83	11.99	0	30.25
23/12/2002 01:45	12.66	0.83	11.83	0	30.5
23/12/2002 02:00	12.50	0.83	11.67	0	30.75
23/12/2002 02:15	12.35	0.83	11.52	0	31
23/12/2002 02:30	12.09	0.83	11.26	0	31.25

First peak	Second peak

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
23/12/2002 02:45	11.88	0.83	11.05	0	31.5		
23/12/2002 03:00	11.66	0.83	10.83	0	31.75		
23/12/2002 03:15	11.44	0.83	10.61	0	32		
23/12/2002 03:30	11.18	0.83	10.35	0	32.25		
23/12/2002 03:45	10.90	0.83	10.07	0	32.5		
23/12/2002 04:00	10.64	0.83	9.81	0	32.75		
23/12/2002 04:15	10.32	0.83	9.49	0	33		
23/12/2002 04:30	10.03	0.83	9.20	0	33.25		
23/12/2002 04:45	9.74	0.83	8.91	0	33.5		
23/12/2002 05:00	9.44	0.83	8.61	0	33.75		
23/12/2002 05:15	9.11	0.83	8.28	0	34		
23/12/2002 05:30	8.82	0.83	7.99	0	34.25		
23/12/2002 05:45	8.56	0.83	7.73	0	34.5		
23/12/2002 06:00	8.25	0.83	7.42	0	34.75		
23/12/2002 06:15	7.98	0.83	7.15	0	35		
23/12/2002 06:30	7.71	0.83	6.88	0	35.25		
23/12/2002 06:45	7.47	0.83	6.64	0	35.5		
23/12/2002 07:00	7.22	0.83	6.39	0	35.75		
23/12/2002 07:15	7.00	0.83	6.17	0	36		
23/12/2002 07:30	6.79	0.83	5.96	0	36.25		
23/12/2002 07:45	6.60	0.83	5.77	0	36.5		
23/12/2002 08:00	6.41	0.83	5.58	0	36.75		
23/12/2002 08:15	6.24	0.83	5.41	0	37		
23/12/2002 08:30	6.05	0.83	5.22	0	37.25		
23/12/2002 08:45	5.90	0.83	5.07	0	37.5		
23/12/2002 09:00	5.73	0.83	4.90	0	37.75		
23/12/2002 09:15	5.52	0.83	4.69	0	38		
23/12/2002 09:30	5.35	0.83	4.52	0	38.25		
23/12/2002 09:45	5.14	0.83	4.31	0	38.5		
23/12/2002 10:00	4.93	0.83	4.10	0	38.75		
23/12/2002 10:15	4.71	0.83	3.88	0	39		
23/12/2002 10:30	4.48	0.83	3.65	0	39.25		
23/12/2002 10:45	4.21	0.83	3.38	0	39.5		
23/12/2002 11:00	3.94	0.83	3.11	0	39.75		
23/12/2002 11:15	3.71	0.83	2.88	0	40		
23/12/2002 11:30	3.44	0.83	2.61	0	40.25		
23/12/2002 11:45	3.21	0.83	2.38	0	40.5		
23/12/2002 12:00	2.99	0.83	2.16	0	40.75		
23/12/2002 12:15	2.80	0.83	1.97	0	41		
23/12/2002 12:30	2.64	0.83	1.81	0	41.25		
23/12/2002 12:45	2.48	0.83	1.65	0	41.5		
23/12/2002 13:00	2.35	0.83	1.52	0	41.75		

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
23/12/2002 13:15	2.25	0.83	1.42	0	42
23/12/2002 13:30	2.17	0.83	1.34	0	42.25
23/12/2002 13:45	2.10	0.83	1.27	0	42.5
23/12/2002 14:00	2.03	0.83	1.20	0	42.75
23/12/2002 14:15	1.98	0.83	1.15	0	43
23/12/2002 14:30	1.93	0.83	1.10	0	43.25
23/12/2002 14:45	1.88	0.83	1.05	0	43.5
23/12/2002 15:00	1.85	0.83	1.02	0	43.75
23/12/2002 15:15	1.81	0.83	0.98	0	44
23/12/2002 15:30	1.78	0.83	0.95	0	44.25
23/12/2002 15:45	1.75	0.83	0.92	0	44.5
23/12/2002 16:00	1.72	0.83	0.89	0	44.75
23/12/2002 16:15	1.69	0.83	0.86	0	45
23/12/2002 16:30	1.67	0.83	0.84	0	45.25
23/12/2002 16:45	1.64	0.83	0.81	0	45.5
23/12/2002 17:00	1.63	0.83	0.80	0	45.75
23/12/2002 17:15	1.61	0.83	0.78	0	46
23/12/2002 17:30	1.59	0.83	0.76	0	46.25
23/12/2002 17:45	1.57	0.83	0.74	0	46.5
23/12/2002 18:00	1.56	0.83	0.73	0	46.75
23/12/2002 18:15	1.53	0.83	0.70	0	47
23/12/2002 18:30	1.53	0.83	0.70	0	47.25
23/12/2002 18:45	1.51	0.83	0.68	0	47.5
23/12/2002 19:00	1.49	0.83	0.66	0	47.75
23/12/2002 19:15	1.48	0.83	0.65	0	48
23/12/2002 19:30	1.46	0.83	0.63	0	48.25
23/12/2002 19:45	1.44	0.83	0.61	0	48.5
23/12/2002 20:00	1.44	0.83	0.61	0	48.75
23/12/2002 20:15	1.42	0.83	0.59	0	49
23/12/2002 20:30	1.40	0.83	0.57	0	49.25
23/12/2002 20:45	1.39	0.83	0.56	0	49.5
23/12/2002 21:00	1.39	0.83	0.56	0	49.75
23/12/2002 21:15	1.37	0.83	0.54	0	50
23/12/2002 21:30	1.36	0.83	0.53	0	50.25
23/12/2002 21:45	1.35	0.83	0.52	0	50.5
23/12/2002 22:00	1.34	0.83	0.51	0	50.75
23/12/2002 22:15	1.33	0.83	0.50	0	51
23/12/2002 22:30	1.32	0.83	0.49	0	51.25
23/12/2002 22:45	1.31	0.83	0.48	0	51.5
23/12/2002 23:00	1.30	0.83	0.47	0	51.75
23/12/2002 23:15	1.29	0.83	0.46	0	52
23/12/2002 23:30	1.28	0.83	0.45	0	52.25

First peak	Second peak

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
23/12/2002 23:45	1.28	0.83	0.45	0.2	52.5		
24/12/2002 00:00	1.27	0.83	0.44	0.2	52.75		
24/12/2002 00:15	1.25	0.83	0.42	0.2	53		
24/12/2002 00:30	1.25	0.83	0.42	0	53.25		
24/12/2002 00:45	1.24	0.83	0.41	0	53.5		
24/12/2002 01:00	1.23	0.83	0.40	0.2	53.75		
24/12/2002 01:15	1.23	0.83	0.40	0.2	54		
24/12/2002 01:30	1.22	0.83	0.39	0	54.25		
24/12/2002 01:45	1.22	0.83	0.39	0	54.5		
24/12/2002 02:00	1.21	0.83	0.38	0	54.75		
24/12/2002 02:15	1.20	0.83	0.37	0	55		
24/12/2002 02:30	1.19	0.83	0.36	0	55.25		
24/12/2002 02:45	1.19	0.83	0.36	0	55.5		
24/12/2002 03:00	1.19	0.83	0.36	0	55.75		
24/12/2002 03:15	1.17	0.83	0.34	0	56		
24/12/2002 03:30	1.17	0.83	0.34	0	56.25		
24/12/2002 03:45	1.16	0.83	0.33	0	56.5		
24/12/2002 04:00	1.16	0.83	0.33	0	56.75		
24/12/2002 04:15	1.15	0.83	0.32	0	57		
24/12/2002 04:30	1.14	0.83	0.31	0	57.25		
24/12/2002 04:45	1.14	0.83	0.31	0	57.5		
24/12/2002 05:00	1.13	0.83	0.30	0	57.75		
24/12/2002 05:15	1.13	0.83	0.30	0	58		
24/12/2002 05:30	1.12	0.83	0.29	0	58.25		
24/12/2002 05:45	1.12	0.83	0.29	0	58.5		
24/12/2002 06:00	1.11	0.83	0.28	0	58.75		
24/12/2002 06:15	1.11	0.83	0.28	0	59		
24/12/2002 06:30	1.10	0.83	0.27	0	59.25		
24/12/2002 06:45	1.09	0.83	0.26	0	59.5		
24/12/2002 07:00	1.09	0.83	0.26	0	59.75		
24/12/2002 07:15	1.08	0.83	0.25	0	60		
24/12/2002 07:30	1.08	0.83	0.25	0	60.25		
24/12/2002 07:45	1.08	0.83	0.25	0	60.5		
24/12/2002 08:00	1.07	0.83	0.24	0	60.75		
24/12/2002 08:15	1.07	0.83	0.24	0	61		
24/12/2002 08:30	1.06	0.83	0.23	0.2	61.25		
24/12/2002 08:45	1.06	0.83	0.23	0	61.5		
24/12/2002 09:00	1.06	0.83	0.23	0	61.75		
24/12/2002 09:15	1.05	0.83	0.22	0	62		
24/12/2002 09:30	1.05	0.83	0.22	0	62.25		
24/12/2002 09:45	1.05	0.83	0.22	0	62.5		
24/12/2002 10:00	1.04	0.83	0.21	0	62.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
24/12/2002 10:15	1.03	0.83	0.20	0	63		
24/12/2002 10:30	1.03	0.83	0.20	0	63.25		
24/12/2002 10:45	1.03	0.83	0.20	0	63.5		
24/12/2002 11:00	1.03	0.83	0.20	0	63.75		
24/12/2002 11:15	1.02	0.83	0.19	0	64		
24/12/2002 11:30	1.02	0.83	0.19	0	64.25		
24/12/2002 11:45	1.02	0.83	0.19	0	64.5		
24/12/2002 12:00	1.01	0.83	0.18	0	64.75		
24/12/2002 12:15	1.01	0.83	0.18	0	65		
24/12/2002 12:30	1.01	0.83	0.18	0	65.25		
24/12/2002 12:45	1.01	0.83	0.18	0	65.5		
24/12/2002 13:00	1.01	0.83	0.18	0	65.75		
24/12/2002 13:15	1.00	0.83	0.17	0	66		
24/12/2002 13:30	1.00	0.83	0.17	0	66.25		
24/12/2002 13:45	1.01	0.83	0.18	0	66.5		
24/12/2002 14:00	1.00	0.83	0.17	0	66.75		
24/12/2002 14:15	1.00	0.83	0.17	0	67		
24/12/2002 14:30	1.00	0.83	0.17	0	67.25		
24/12/2002 14:45	1.00	0.83	0.17	0	67.5		
24/12/2002 15:00	1.00	0.83	0.17	0	67.75		
24/12/2002 15:15	1.00	0.83	0.17	0	68		
24/12/2002 15:30	1.00	0.83	0.17	0	68.25		
24/12/2002 15:45	1.00	0.83	0.17	0	68.5		
24/12/2002 16:00	1.00	0.83	0.17	0	68.75		
24/12/2002 16:15	1.00	0.83	0.17	0	69		
24/12/2002 16:30	1.00	0.83	0.17	0	69.25		
24/12/2002 16:45	1.00	0.83	0.17	0	69.5		
24/12/2002 17:00	0.99	0.83	0.16	0	69.75		
24/12/2002 17:15	1.00	0.83	0.17	0	70		
24/12/2002 17:30	1.00	0.83	0.17	0	70.25		
24/12/2002 17:45	0.99	0.83	0.16	0	70.5		
24/12/2002 18:00	0.99	0.83	0.16	0	70.75		
24/12/2002 18:15	0.99	0.83	0.16	0	71		
24/12/2002 18:30	0.99	0.83	0.16	0	71.25		
24/12/2002 18:45	0.99	0.83	0.16	0	71.5		
24/12/2002 19:00	0.99	0.83	0.16	0	71.75		
24/12/2002 19:15	0.99	0.83	0.16	0	72		
24/12/2002 19:30	0.99	0.83	0.16	0	72.25		
24/12/2002 19:45	0.99	0.83	0.16	0	72.5		
24/12/2002 20:00	0.99	0.83	0.16	0	72.75		
24/12/2002 20:15	0.99	0.83	0.16	0	73		
24/12/2002 20:30	0.99	0.83	0.16	0	73.25		

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
24/12/2002 20:45	0.99	0.83	0.16	0	73.5		
24/12/2002 21:00	0.99	0.83	0.16	0	73.75		
24/12/2002 21:15	0.99	0.83	0.16	0	74		
24/12/2002 21:30	0.98	0.83	0.15	0	74.25		
24/12/2002 21:45	0.98	0.83	0.15	0	74.5		
24/12/2002 22:00	0.98	0.83	0.15	0	74.75		
24/12/2002 22:15	0.98	0.83	0.15	0	75		
24/12/2002 22:30	0.97	0.83	0.14	0	75.25		
24/12/2002 22:45	0.97	0.83	0.14	0	75.5		
24/12/2002 23:00	0.97	0.83	0.14	0	75.75		
24/12/2002 23:15	0.97	0.83	0.14	0	76		
24/12/2002 23:30	0.97	0.83	0.14	0	76.25		
24/12/2002 23:45	0.97	0.83	0.14	0	76.5		
25/12/2002 00:00	0.96	0.83	0.13	0	76.75		
25/12/2002 00:15	0.96	0.83	0.13	0	77		
25/12/2002 00:30	0.96	0.83	0.13	0	77.25		
25/12/2002 00:45	0.95	0.83	0.12	0	77.5		
25/12/2002 01:00	0.95	0.83	0.12	0	77.75		
25/12/2002 01:15	0.95	0.83	0.12	0	78		
25/12/2002 01:30	0.95	0.83	0.12	0	78.25		
25/12/2002 01:45	0.95	0.83	0.12	0	78.5		
25/12/2002 02:00	0.94	0.83	0.11	0	78.75		
25/12/2002 02:15	0.94	0.83	0.11	0	79		
25/12/2002 02:30	0.94	0.83	0.11	0	79.25		
25/12/2002 02:45	0.93	0.83	0.10	0	79.5		
25/12/2002 03:00	0.93	0.83	0.10	0	79.75		
25/12/2002 03:15	0.93	0.83	0.10	0	80		
25/12/2002 03:30	0.93	0.83	0.10	0	80.25		
25/12/2002 03:45	0.93	0.83	0.10	0	80.5		
25/12/2002 04:00	0.92	0.83	0.09	0	80.75		
25/12/2002 04:15	0.92	0.83	0.09	0	81		
25/12/2002 04:30	0.92	0.83	0.09	0	81.25		
25/12/2002 04:45	0.91	0.83	0.08	0	81.5		
25/12/2002 05:00	0.91	0.83	0.08	0	81.75		
25/12/2002 05:15	0.91	0.83	0.08	0	82		
25/12/2002 05:30	0.91	0.83	0.08	0	82.25		
25/12/2002 05:45	0.91	0.83	0.08	0.2	82.5		
25/12/2002 06:00	0.91	0.83	0.08	0	82.75		
25/12/2002 06:15	0.90	0.83	0.07	0	83		
25/12/2002 06:30	0.90	0.83	0.07	0	83.25		
25/12/2002 06:45	0.89	0.83	0.06	0	83.5		
25/12/2002 07:00	0.89	0.83	0.06	0	83.75		

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
25/12/2002 07:15	0.89	0.83	0.06	0	84
25/12/2002 07:30	0.89	0.83	0.06	0	84.25
25/12/2002 07:45	0.89	0.83	0.06	0	84.5
25/12/2002 08:00	0.89	0.83	0.06	0	84.75
25/12/2002 08:15	0.88	0.83	0.05	0	85
25/12/2002 08:30	0.88	0.83	0.05	0	85.25
25/12/2002 08:45	0.88	0.83	0.05	0	85.5
25/12/2002 09:00	0.88	0.83	0.05	0.2	85.75
25/12/2002 09:15	0.88	0.83	0.05	0	86
25/12/2002 09:30	0.88	0.83	0.05	0	86.25
25/12/2002 09:45	0.88	0.83	0.05	0	86.5
25/12/2002 10:00	0.88	0.83	0.05	0.2	86.75
25/12/2002 10:15	0.88	0.83	0.05	0	87
25/12/2002 10:30	0.88	0.83	0.05	0	87.25
25/12/2002 10:45	0.88	0.83	0.05	0	87.5
25/12/2002 11:00	0.88	0.83	0.05	0	87.75
25/12/2002 11:15	0.88	0.83	0.05	0	88
25/12/2002 11:30	0.88	0.83	0.05	0	88.25
25/12/2002 11:45	0.88	0.83	0.05	0	88.5
25/12/2002 12:00	0.88	0.83	0.05	0	88.75
25/12/2002 12:15	0.89	0.83	0.06	0	89
25/12/2002 12:30	0.89	0.83	0.06	0	89.25
25/12/2002 12:45	0.89	0.83	0.06	0	89.5
25/12/2002 13:00	0.89	0.83	0.06	0	89.75
25/12/2002 13:15	0.89	0.83	0.06	0	90
25/12/2002 13:30	0.90	0.83	0.07	0	90.25
25/12/2002 13:45	0.90	0.83	0.07	0	90.5
25/12/2002 14:00	0.91	0.83	0.08	0	90.75
25/12/2002 14:15	0.92	0.83	0.09	0	91
25/12/2002 14:30	0.93	0.83	0.10	0	91.25
25/12/2002 14:45	0.93	0.83	0.10	0	91.5
25/12/2002 15:00	0.95	0.83	0.12	0	91.75
25/12/2002 15:15	0.95	0.83	0.12	0	92
25/12/2002 15:30	0.96	0.83	0.13	0	92.25
25/12/2002 15:45	0.97	0.83	0.14	0	92.5
25/12/2002 16:00	0.97	0.83	0.14	0	92.75
25/12/2002 16:15	0.98	0.83	0.15	0	93
25/12/2002 16:30	0.99	0.83	0.16	0	93.25
25/12/2002 16:45	1.00	0.83	0.17	0	93.5
25/12/2002 17:00	1.01	0.83	0.18	0	93.75
25/12/2002 17:15	1.01	0.83	0.18	0	94
25/12/2002 17:30	1.03	0.83	0.20	0	94.25

First peak	Second peak

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
25/12/2002 17:45	1.03	0.83	0.20	0	94.5
25/12/2002 18:00	1.05	0.83	0.22	0	94.75
25/12/2002 18:15	1.06	0.83	0.23	0	95
25/12/2002 18:30	1.06	0.83	0.23	0	95.25
25/12/2002 18:45	1.07	0.83	0.24	0	95.5
25/12/2002 19:00	1.08	0.83	0.25	0	95.75
25/12/2002 19:15	1.09	0.83	0.26	0	96
25/12/2002 19:30	1.09	0.83	0.26	0	96.25
25/12/2002 19:45	1.10	0.83	0.27	0	96.5
25/12/2002 20:00	1.11	0.83	0.28	0	96.75
25/12/2002 20:15	1.11	0.83	0.28	0	97
25/12/2002 20:30	1.11	0.83	0.28	0	97.25
25/12/2002 20:45	1.12	0.83	0.29	0	97.5
25/12/2002 21:00	1.13	0.83	0.30	0	97.75
25/12/2002 21:15	1.13	0.83	0.30	0	98
25/12/2002 21:30	1.13	0.83	0.30	0	98.25
25/12/2002 21:45	1.13	0.83	0.30	0	98.5
25/12/2002 22:00	1.14	0.83	0.31	0	98.75
25/12/2002 22:15	1.14	0.83	0.31	0	99
25/12/2002 22:30	1.14	0.83	0.31	0	99.25
25/12/2002 22:45	1.15	0.83	0.32	0	99.5
25/12/2002 23:00	1.15	0.83	0.32	0	99.75
25/12/2002 23:15	1.15	0.83	0.32	0	100
25/12/2002 23:30	1.15	0.83	0.32	0	100.25
25/12/2002 23:45	1.15	0.83	0.32	0	100.5
26/12/2002 00:00	1.15	0.83	0.32	0	100.75
26/12/2002 00:15	1.15	0.83	0.32	0	101
26/12/2002 00:30	1.15	0.83	0.32	0	101.25
26/12/2002 00:45	1.15	0.83	0.32	0	101.5
26/12/2002 01:00	1.15	0.83	0.32	0	101.75
26/12/2002 01:15	1.15	0.83	0.32	0	102
26/12/2002 01:30	1.15	0.83	0.32	0	102.25
26/12/2002 01:45	1.14	0.83	0.31	0	102.5
26/12/2002 02:00	1.14	0.83	0.31	0	102.75
26/12/2002 02:15	1.14	0.83	0.31	0	103
26/12/2002 02:30	1.13	0.83	0.30	0	103.25
26/12/2002 02:45	1.13	0.83	0.30	0	103.5
26/12/2002 03:00	1.13	0.83	0.30	0	103.75
26/12/2002 03:15	1.13	0.83	0.30	0	104
26/12/2002 03:30	1.13	0.83	0.30	0	104.25
26/12/2002 03:45	1.13	0.83	0.30	0	104.5
26/12/2002 04:00	1.13	0.83	0.30	0	104.75

First peak	Second peak

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
26/12/2002 04:15	1.12	0.83	0.29	0	105		
26/12/2002 04:30	1.12	0.83	0.29	0	105.25		
26/12/2002 04:45	1.11	0.83	0.28	0	105.5		
26/12/2002 05:00	1.11	0.83	0.28	0	105.75		
26/12/2002 05:15	1.11	0.83	0.28	0	106		
26/12/2002 05:30	1.11	0.83	0.28	0	106.25		
26/12/2002 05:45	1.11	0.83	0.28	0.2	106.5		
26/12/2002 06:00	1.10	0.83	0.27	0.2	106.75		
26/12/2002 06:15	1.11	0.83	0.28	0	107		
26/12/2002 06:30	1.10	0.83	0.27	0	107.25		
26/12/2002 06:45	1.11	0.83	0.28	1.2	107.5		
26/12/2002 07:00	1.13	0.83	0.30	1.2	107.75		
26/12/2002 07:15	1.14	0.83	0.31	1.2	108		
26/12/2002 07:30	1.16	0.83	0.33	0	108.25		
26/12/2002 07:45	1.17	0.83	0.34	0.4	108.5		
26/12/2002 08:00	1.18	0.83	0.35	0	108.75		
26/12/2002 08:15	1.19	0.83	0.36	0	109		
26/12/2002 08:30	1.21	0.83	0.38	0	109.25		
26/12/2002 08:45	1.22	0.83	0.39	0	109.5		
26/12/2002 09:00	1.24	0.83	0.41	0	109.75		
26/12/2002 09:15	1.28	0.83	0.45	0	110		
26/12/2002 09:30	1.34	0.83	0.51	0	110.25		
26/12/2002 09:45	1.39	0.83	0.56	0	110.5		
26/12/2002 10:00	1.46	0.83	0.63	0	110.75		
26/12/2002 10:15	1.54	0.83	0.71	0	111		
26/12/2002 10:30	1.63	0.83	0.80	0	111.25		
26/12/2002 10:45	1.70	0.83	0.87	0	111.5		
26/12/2002 11:00	1.78	0.83	0.95	0	111.75		
26/12/2002 11:15	1.85	0.83	1.02	0	112		
26/12/2002 11:30	1.92	0.83	1.09	0	112.25		
26/12/2002 11:45	2.00	0.83	1.17	0	112.5		
26/12/2002 12:00	2.05	0.83	1.22	0	112.75		
26/12/2002 12:15	2.12	0.83	1.29	0	113		
26/12/2002 12:30	2.17	0.83	1.34	0	113.25		
26/12/2002 12:45	2.24	0.83	1.41	0	113.5		
26/12/2002 13:00	2.30	0.83	1.47	0	113.75		
26/12/2002 13:15	2.33	0.83	1.50	0	114		
26/12/2002 13:30	2.40	0.83	1.57	0	114.25		
26/12/2002 13:45	2.44	0.83	1.61	0	114.5		
26/12/2002 14:00	2.48	0.83	1.65	0	114.75		
26/12/2002 14:15	2.54	0.83	1.71	0	115		
26/12/2002 14:30	2.60	0.83	1.77	0	115.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
26/12/2002 14:45	2.65	0.83	1.82	0	115.5		
26/12/2002 15:00	2.69	0.83	1.86	0	115.75		
26/12/2002 15:15	2.74	0.83	1.91	0	116		
26/12/2002 15:30	2.79	0.83	1.96	0	116.25		
26/12/2002 15:45	2.85	0.83	2.02	0	116.5		
26/12/2002 16:00	2.92	0.83	2.09	0	116.75		
26/12/2002 16:15	2.95	0.83	2.12	0	117		
26/12/2002 16:30	3.01	0.83	2.18	0	117.25		
26/12/2002 16:45	3.05	0.83	2.22	0	117.5		
26/12/2002 17:00	3.10	0.83	2.27	0.2	117.75		
26/12/2002 17:15	3.14	0.83	2.31	0	118		
26/12/2002 17:30	3.16	0.83	2.33	0	118.25		
26/12/2002 17:45	3.15	0.83	2.32	0	118.5		
26/12/2002 18:00	3.16	0.83	2.33	0	118.75		
26/12/2002 18:15	3.16	0.83	2.33	0	119		
26/12/2002 18:30	3.16	0.83	2.33	0	119.25		
26/12/2002 18:45	3.13	0.83	2.30	0	119.5		
26/12/2002 19:00	3.10	0.83	2.27	0	119.75		
26/12/2002 19:15	3.05	0.83	2.22	0	120		
26/12/2002 19:30	3.00	0.83	2.17	0	120.25		
26/12/2002 19:45	2.95	0.83	2.12	0	120.5		
26/12/2002 20:00	2.91	0.83	2.08	0	120.75		
26/12/2002 20:15	2.85	0.83	2.02	0	121		
26/12/2002 20:30	2.79	0.83	1.96	0	121.25		
26/12/2002 20:45	2.72	0.83	1.89	0	121.5		
26/12/2002 21:00	2.68	0.83	1.85	0	121.75		
26/12/2002 21:15	2.59	0.83	1.76	0	122		
26/12/2002 21:30	2.55	0.83	1.72	0	122.25		
26/12/2002 21:45	2.48	0.83	1.65	0	122.5		
26/12/2002 22:00	2.41	0.83	1.58	0	122.75		
26/12/2002 22:15	2.38	0.83	1.55	0	123		
26/12/2002 22:30	2.31	0.83	1.48	0	123.25		
26/12/2002 22:45	2.27	0.83	1.44	0	123.5		
26/12/2002 23:00	2.23	0.83	1.40	0	123.75		
26/12/2002 23:15	2.19	0.83	1.36	0	124		
26/12/2002 23:30	2.16	0.83	1.33	0.4	124.25		
26/12/2002 23:45	2.12	0.83	1.29	0.2	124.5		
27/12/2002 00:00	2.08	0.83	1.25	0.4	124.75		
27/12/2002 00:15	2.06	0.83	1.23	0.4	125		
27/12/2002 00:30	2.03	0.83	1.20	0.4	125.25		
27/12/2002 00:45	2.00	0.83	1.17	0.4	125.5		
27/12/2002 01:00	1.98	0.83	1.15	0.2	125.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
27/12/2002 01:15	1.96	0.83	1.13	0.2	126		
27/12/2002 01:30	1.94	0.83	1.11	0.4	126.25		
27/12/2002 01:45	1.92	0.83	1.09	0.6	126.5		
27/12/2002 02:00	1.92	0.83	1.09	0.2	126.75		
27/12/2002 02:15	1.90	0.83	1.07	0.4	127		
27/12/2002 02:30	1.90	0.83	1.07	0.4	127.25		
27/12/2002 02:45	1.89	0.83	1.06	0.2	127.5		
27/12/2002 03:00	1.92	0.83	1.09	0.4	127.75		
27/12/2002 03:15	1.93	0.83	1.10	0.2	128		
27/12/2002 03:30	1.95	0.83	1.12	0	128.25		
27/12/2002 03:45	1.99	0.83	1.16	0	128.5		
27/12/2002 04:00	2.04	0.83	1.21	0	128.75		
27/12/2002 04:15	2.11	0.83	1.28	0.2	129		
27/12/2002 04:30	2.18	0.83	1.35	0	129.25		
27/12/2002 04:45	2.26	0.83	1.43	0	129.5		
27/12/2002 05:00	2.35	0.83	1.52	0	129.75		
27/12/2002 05:15	2.44	0.83	1.61	0	130		
27/12/2002 05:30	2.57	0.83	1.74	0	130.25		
27/12/2002 05:45	2.70	0.83	1.87	0	130.5		
27/12/2002 06:00	2.83	0.83	2.00	0	130.75		
27/12/2002 06:15	2.97	0.83	2.14	0	131		
27/12/2002 06:30	3.10	0.83	2.27	0	131.25		
27/12/2002 06:45	3.24	0.83	2.41	0	131.5		
27/12/2002 07:00	3.36	0.83	2.53	0	131.75		
27/12/2002 07:15	3.49	0.83	2.66	0	132		
27/12/2002 07:30	3.62	0.83	2.79	0	132.25		
27/12/2002 07:45	3.71	0.83	2.88	0	132.5		
27/12/2002 08:00	3.81	0.83	2.98	0	132.75		
27/12/2002 08:15	3.92	0.83	3.09	0	133		
27/12/2002 08:30	4.01	0.83	3.18	0	133.25		
27/12/2002 08:45	4.06	0.83	3.23	0	133.5		
27/12/2002 09:00	4.13	0.83	3.30	0	133.75		
27/12/2002 09:15	4.20	0.83	3.37	0	134		
27/12/2002 09:30	4.24	0.83	3.41	0	134.25		
27/12/2002 09:45	4.31	0.83	3.48	0	134.5		
27/12/2002 10:00	4.36	0.83	3.53	0	134.75		
27/12/2002 10:15	4.37	0.83	3.54	0	135		
27/12/2002 10:30	4.41	0.83	3.58	0	135.25		
27/12/2002 10:45	4.44	0.83	3.61	0	135.5		
27/12/2002 11:00	4.46	0.83	3.63	0	135.75		
27/12/2002 11:15	4.50	0.83	3.67	0	136		
27/12/2002 11:30	4.51	0.83	3.68	0	136.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
27/12/2002 11:45	4.54	0.83	3.71	0	136.5		
27/12/2002 12:00	4.56	0.83	3.73	0	136.75		
27/12/2002 12:15	4.58	0.83	3.75	0	137		
27/12/2002 12:30	4.60	0.83	3.77	0	137.25		
27/12/2002 12:45	4.60	0.83	3.77	0	137.5		
27/12/2002 13:00	4.62	0.83	3.79	0	137.75		
27/12/2002 13:15	4.64	0.83	3.81	0	138		
27/12/2002 13:30	4.65	0.83	3.82	0	138.25		
27/12/2002 13:45	4.67	0.83	3.84	0	138.5		
27/12/2002 14:00	4.68	0.83	3.85	0	138.75		
27/12/2002 14:15	4.69	0.83	3.86	0	139		
27/12/2002 14:30	4.69	0.83	3.86	0	139.25		
27/12/2002 14:45	4.72	0.83	3.89	0	139.5		
27/12/2002 15:00	4.73	0.83	3.90	0	139.75		
27/12/2002 15:15	4.73	0.83	3.90	0	140		
27/12/2002 15:30	4.74	0.83	3.91	0	140.25		
27/12/2002 15:45	4.75	0.83	3.92	0	140.5		
27/12/2002 16:00	4.75	0.83	3.92	0	140.75		
27/12/2002 16:15	4.74	0.83	3.91	0	141		
27/12/2002 16:30	4.73	0.83	3.90	0	141.25		
27/12/2002 16:45	4.73	0.83	3.90	0	141.5		
27/12/2002 17:00	4.70	0.83	3.87	0	141.75		
27/12/2002 17:15	4.69	0.83	3.86	0	142		
27/12/2002 17:30	4.65	0.83	3.82	0	142.25		
27/12/2002 17:45	4.62	0.83	3.79	0	142.5		
27/12/2002 18:00	4.58	0.83	3.75	0	142.75		
27/12/2002 18:15	4.52	0.83	3.69	0	143		
27/12/2002 18:30	4.46	0.83	3.63	0	143.25		
27/12/2002 18:45	4.35	0.83	3.52	0	143.5		
27/12/2002 19:00	4.24	0.83	3.41	0	143.75		
27/12/2002 19:15	4.13	0.83	3.30	0	144		
27/12/2002 19:30	3.97	0.83	3.14	0	144.25		
27/12/2002 19:45	3.82	0.83	2.99	0	144.5		
27/12/2002 20:00	3.69	0.83	2.86	0	144.75		
27/12/2002 20:15	3.51	0.83	2.68	0	145		
27/12/2002 20:30	3.34	0.83	2.51	0	145.25		
27/12/2002 20:45	3.18	0.83	2.35	0	145.5		
27/12/2002 21:00	3.04	0.83	2.21	0	145.75		
27/12/2002 21:15	2.88	0.83	2.05	0	146		
27/12/2002 21:30	2.74	0.83	1.91	0	146.25		
27/12/2002 21:45	2.63	0.83	1.80	0	146.5		
27/12/2002 22:00	2.51	0.83	1.68	0	146.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
27/12/2002 22:15	2.41	0.83	1.58	0	147		
27/12/2002 22:30	2.32	0.83	1.49	0	147.25		
27/12/2002 22:45	2.26	0.83	1.43	0	147.5		
27/12/2002 23:00	2.21	0.83	1.38	0	147.75		
27/12/2002 23:15	2.15	0.83	1.32	0	148		
27/12/2002 23:30	2.11	0.83	1.28	0	148.25		
27/12/2002 23:45	2.06	0.83	1.23	0	148.5		
28/12/2002 00:00	2.01	0.83	1.18	0	148.75		
28/12/2002 00:15	1.97	0.83	1.14	0	149		
28/12/2002 00:30	1.95	0.83	1.12	0	149.25		
28/12/2002 00:45	1.90	0.83	1.07	0	149.5		
28/12/2002 01:00	1.88	0.83	1.05	0	149.75		
28/12/2002 01:15	1.84	0.83	1.01	0	150		
28/12/2002 01:30	1.81	0.83	0.98	0	150.25		
28/12/2002 01:45	1.79	0.83	0.96	0	150.5		
28/12/2002 02:00	1.76	0.83	0.93	0	150.75		
28/12/2002 02:15	1.75	0.83	0.92	0	151		
28/12/2002 02:30	1.73	0.83	0.90	0	151.25		
28/12/2002 02:45	1.69	0.83	0.86	0	151.5		
28/12/2002 03:00	1.68	0.83	0.85	0	151.75		
28/12/2002 03:15	1.65	0.83	0.82	0	152		
28/12/2002 03:30	1.63	0.83	0.80	0	152.25		
28/12/2002 03:45	1.61	0.83	0.78	0	152.5		
28/12/2002 04:00	1.59	0.83	0.76	0	152.75		
28/12/2002 04:15	1.58	0.83	0.75	0	153		
28/12/2002 04:30	1.55	0.83	0.72	0	153.25		
28/12/2002 04:45	1.54	0.83	0.71	0	153.5		
28/12/2002 05:00	1.53	0.83	0.70	0	153.75		
28/12/2002 05:15	1.50	0.83	0.67	0	154		
28/12/2002 05:30	1.49	0.83	0.66	0	154.25		
28/12/2002 05:45	1.48	0.83	0.65	0	154.5		
28/12/2002 06:00	1.46	0.83	0.63	0	154.75		
28/12/2002 06:15	1.44	0.83	0.61	0	155		
28/12/2002 06:30	1.43	0.83	0.60	0	155.25		
28/12/2002 06:45	1.41	0.83	0.58	0	155.5		
28/12/2002 07:00	1.40	0.83	0.57	0	155.75		
28/12/2002 07:15	1.39	0.83	0.56	0	156		
28/12/2002 07:30	1.37	0.83	0.54	0	156.25		
28/12/2002 07:45	1.36	0.83	0.53	0	156.5		
28/12/2002 08:00	1.35	0.83	0.52	0	156.75		
28/12/2002 08:15	1.33	0.83	0.50	0	157		
28/12/2002 08:30	1.32	0.83	0.49	0	157.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
28/12/2002 08:45	1.31	0.83	0.48	0	157.5		
28/12/2002 09:00	1.30	0.83	0.47	0	157.75		
28/12/2002 09:15	1.28	0.83	0.45	0	158		
28/12/2002 09:30	1.27	0.83	0.44	0	158.25		
28/12/2002 09:45	1.26	0.83	0.43	0	158.5		
28/12/2002 10:00	1.25	0.83	0.42	0	158.75		
28/12/2002 10:15	1.24	0.83	0.41	0	159		
28/12/2002 10:30	1.23	0.83	0.40	0	159.25		
28/12/2002 10:45	1.22	0.83	0.39	0	159.5		
28/12/2002 11:00	1.21	0.83	0.38	0	159.75		
28/12/2002 11:15	1.20	0.83	0.37	0	160		
28/12/2002 11:30	1.19	0.83	0.36	0	160.25		
28/12/2002 11:45	1.19	0.83	0.36	0	160.5		
28/12/2002 12:00	1.17	0.83	0.34	0	160.75		
28/12/2002 12:15	1.16	0.83	0.33	0	161		
28/12/2002 12:30	1.15	0.83	0.32	0	161.25		
28/12/2002 12:45	1.14	0.83	0.31	0	161.5		
28/12/2002 13:00	1.13	0.83	0.30	0	161.75		
28/12/2002 13:15	1.12	0.83	0.29	0	162		
28/12/2002 13:30	1.12	0.83	0.29	0	162.25		
28/12/2002 13:45	1.11	0.83	0.28	0	162.5		
28/12/2002 14:00	1.10	0.83	0.27	0	162.75		
28/12/2002 14:15	1.10	0.83	0.27	0	163		
28/12/2002 14:30	1.08	0.83	0.25	0	163.25		
28/12/2002 14:45	1.08	0.83	0.25	0	163.5		
28/12/2002 15:00	1.08	0.83	0.25	0	163.75		
28/12/2002 15:15	1.06	0.83	0.23	0	164		
28/12/2002 15:30	1.06	0.83	0.23	0	164.25		
28/12/2002 15:45	1.05	0.83	0.22	0	164.5		
28/12/2002 16:00	1.04	0.83	0.21	0	164.75		
28/12/2002 16:15	1.03	0.83	0.20	0	165		
28/12/2002 16:30	1.03	0.83	0.20	0	165.25		
28/12/2002 16:45	1.02	0.83	0.19	0	165.5		
28/12/2002 17:00	1.01	0.83	0.18	0	165.75		
28/12/2002 17:15	1.01	0.83	0.18	0	166		
28/12/2002 17:30	1.00	0.83	0.17	0	166.25		
28/12/2002 17:45	0.99	0.83	0.16	0	166.5		
28/12/2002 18:00	0.99	0.83	0.16	0	166.75		
28/12/2002 18:15	0.99	0.83	0.16	0	167		
28/12/2002 18:30	0.97	0.83	0.14	0	167.25		
28/12/2002 18:45	0.97	0.83	0.14	0	167.5		
28/12/2002 19:00	0.97	0.83	0.14	0	167.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
28/12/2002 19:15	0.96	0.83	0.13	0	168		
28/12/2002 19:30	0.96	0.83	0.13	0	168.25		
28/12/2002 19:45	0.95	0.83	0.12	0	168.5		
28/12/2002 20:00	0.95	0.83	0.12	0	168.75		
28/12/2002 20:15	0.94	0.83	0.11	0	169		
28/12/2002 20:30	0.93	0.83	0.10	0	169.25		
28/12/2002 20:45	0.93	0.83	0.10	0	169.5		
28/12/2002 21:00	0.93	0.83	0.10	0	169.75		
28/12/2002 21:15	0.93	0.83	0.10	0	170		
28/12/2002 21:30	0.91	0.83	0.08	0	170.25		
28/12/2002 21:45	0.91	0.83	0.08	0	170.5		
28/12/2002 22:00	0.91	0.83	0.08	0	170.75		
28/12/2002 22:15	0.90	0.83	0.07	0	171		
28/12/2002 22:30	0.90	0.83	0.07	0	171.25		
28/12/2002 22:45	0.89	0.83	0.06	0	171.5		
28/12/2002 23:00	0.89	0.83	0.06	0	171.75		
28/12/2002 23:15	0.88	0.83	0.05	0	172		
28/12/2002 23:30	0.88	0.83	0.05	0	172.25		
28/12/2002 23:45	0.88	0.83	0.05	0	172.5		
29/12/2002 00:00	0.87	0.83	0.04	0	172.75		
29/12/2002 00:15	0.87	0.83	0.04	0	173		
29/12/2002 00:30	0.86	0.83	0.03	0	173.25		
29/12/2002 00:45	0.86	0.83	0.03	0	173.5		
29/12/2002 01:00	0.86	0.83	0.03	0	173.75		
29/12/2002 01:15	0.85	0.83	0.02	0	174		
29/12/2002 01:30	0.85	0.83	0.02	0	174.25		
29/12/2002 01:45	0.84	0.83	0.01	0	174.5		
29/12/2002 02:00	0.84	0.83	0.01	0	174.75		
29/12/2002 02:15	0.84	0.83	0.01	0	175		
29/12/2002 02:30	0.84	0.83	0.01	0	175.25		
29/12/2002 02:45	0.83	0.83	0.00	0	175.5		
29/12/2002 03:00	0.83	0.83	0.00	0	175.75		
29/12/2002 03:15	0.83	0.83	0.00	0	176		
29/12/2002 03:30	0.82	0.82	0.00	0	176.25		
29/12/2002 03:45	0.81	0.81	0.00	0	176.5		
29/12/2002 04:00	0.81	0.81	0.00	0	176.75		
29/12/2002 04:15	0.81	0.81	0.00	0	177		
29/12/2002 04:30	0.81	0.81	0.00	0	177.25		
29/12/2002 04:45	0.81	0.81	0.00	0	177.5		
29/12/2002 05:00	0.80	0.80	0.00	0	177.75		
29/12/2002 05:15	0.80	0.80	0.00	0	178		
29/12/2002 05:30	0.80	0.80	0.00	0	178.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
29/12/2002 05:45	0.80	0.80	0.00	0	178.5		
29/12/2002 06:00	0.79	0.79	0.00	0	178.75		
29/12/2002 06:15	0.79	0.79	0.00	0	179		
29/12/2002 06:30	0.79	0.79	0.00	0	179.25		
29/12/2002 06:45	0.79	0.79	0.00	0	179.5		
29/12/2002 07:00	0.78	0.78	0.00	0	179.75		
29/12/2002 07:15	0.78	0.78	0.00	0	180		
29/12/2002 07:30	0.77	0.77	0.00	0	180.25		
29/12/2002 07:45	0.77	0.77	0.00	0	180.5		
29/12/2002 08:00	0.77	0.77	0.00	0.2	180.75		
29/12/2002 08:15	0.77	0.77	0.00	0.4	181		
29/12/2002 08:30	0.77	0.77	0.00	0.4	181.25		
29/12/2002 08:45	0.77	0.77	0.00	0.2	181.5		
29/12/2002 09:00	0.76	0.76	0.00	0.2	181.75		
29/12/2002 09:15	0.76	0.76	0.00	0.2	182		
29/12/2002 09:30	0.76	0.76	0.00	0.4	182.25		
29/12/2002 09:45	0.76	0.76	0.00	0.2	182.5		
29/12/2002 10:00	0.76	0.76	0.00	0.4	182.75		
29/12/2002 10:15	0.76	0.76	0.00	0.2	183		
29/12/2002 10:30	0.76	0.76	0.00	0.2	183.25		
29/12/2002 10:45	0.76	0.76	0.00	0.2	183.5		
29/12/2002 11:00	0.76	0.76	0.00	0.2	183.75		
29/12/2002 11:15	0.76	0.76	0.00	0.2	184		
29/12/2002 11:30	0.76	0.76	0.00	0.4	184.25		
29/12/2002 11:45	0.76	0.76	0.00	0.4	184.5		
29/12/2002 12:00	0.76	0.76	0.00	0.4	184.75		
29/12/2002 12:15	0.77	0.77	0.00	0	185		
29/12/2002 12:30	0.77	0.77	0.00	0	185.25		
29/12/2002 12:45	0.77	0.77	0.00	0.2	185.5		
29/12/2002 13:00	0.78	0.78	0.00	0.2	185.75		
29/12/2002 13:15	0.79	0.79	0.00	0.4	186		
29/12/2002 13:30	0.79	0.79	0.00	0.2	186.25		
29/12/2002 13:45	0.80	0.80	0.00	0	186.5		
29/12/2002 14:00	0.81	0.81	0.00	0.2	186.75		
29/12/2002 14:15	0.82	0.82	0.00	0.2	187		
29/12/2002 14:30	0.83	0.83	0.00	0.6	187.25		
29/12/2002 14:45	0.85	0.83	0.02	0.4	187.5		
29/12/2002 15:00	0.87	0.83	0.04	0.4	187.75		
29/12/2002 15:15	0.89	0.83	0.06	0.4	188		
29/12/2002 15:30	0.92	0.83	0.09	0.6	188.25		
29/12/2002 15:45	0.96	0.83	0.13	0.8	188.5		
29/12/2002 16:00	1.01	0.83	0.18	0.8	188.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
29/12/2002 16:15	1.07	0.83	0.24	0.8	189		
29/12/2002 16:30	1.15	0.83	0.32	0.4	189.25		
29/12/2002 16:45	1.25	0.83	0.42	0.4	189.5		
29/12/2002 17:00	1.37	0.83	0.54	0.4	189.75		
29/12/2002 17:15	1.51	0.83	0.68	0.4	190		
29/12/2002 17:30	1.68	0.83	0.85	0.6	190.25		
29/12/2002 17:45	1.84	0.83	1.01	0.6	190.5		
29/12/2002 18:00	2.01	0.83	1.18	0.4	190.75		
29/12/2002 18:15	2.21	0.83	1.38	0.6	191		
29/12/2002 18:30	2.39	0.83	1.56	0.2	191.25		
29/12/2002 18:45	2.58	0.83	1.75	0.4	191.5		
29/12/2002 19:00	2.84	0.83	2.01	0.2	191.75		
29/12/2002 19:15	3.14	0.83	2.31	0.2	192		
29/12/2002 19:30	3.46	0.83	2.63	0	192.25		
29/12/2002 19:45	3.80	0.83	2.97	0	192.5		
29/12/2002 20:00	4.13	0.83	3.30	0	192.75		
29/12/2002 20:15	4.43	0.83	3.60	0.2	193		
29/12/2002 20:30	4.69	0.83	3.86	0	193.25		
29/12/2002 20:45	4.92	0.83	4.09	0	193.5		
29/12/2002 21:00	5.17	0.83	4.34	0	193.75		
29/12/2002 21:15	5.31	0.83	4.48	0	194		
29/12/2002 21:30	5.48	0.83	4.65	0	194.25		
29/12/2002 21:45	5.61	0.83	4.78	0	194.5		
29/12/2002 22:00	5.71	0.83	4.88	0	194.75		
29/12/2002 22:15	5.82	0.83	4.99	0	195		
29/12/2002 22:30	5.89	0.83	5.06	0	195.25		
29/12/2002 22:45	5.92	0.83	5.09	0	195.5		
29/12/2002 23:00	5.98	0.83	5.15	0	195.75		
29/12/2002 23:15	6.00	0.83	5.17	0	196		
29/12/2002 23:30	6.07	0.83	5.24	0	196.25		
29/12/2002 23:45	6.06	0.83	5.23	0	196.5		
30/12/2002 00:00	6.11	0.83	5.28	0	196.75		
30/12/2002 00:15	6.17	0.83	5.34	0	197		
30/12/2002 00:30	6.24	0.83	5.41	0	197.25		
30/12/2002 00:45	6.27	0.83	5.44	0	197.5		
30/12/2002 01:00	6.34	0.83	5.51	0	197.75		
30/12/2002 01:15	6.42	0.83	5.59	0	198		
30/12/2002 01:30	6.48	0.83	5.65	0	198.25		
30/12/2002 01:45	6.58	0.83	5.75	0	198.5		
30/12/2002 02:00	6.65	0.83	5.82	0	198.75		
30/12/2002 02:15	6.77	0.83	5.94	0	199		
30/12/2002 02:30	6.93	0.83	6.10	0	199.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
30/12/2002 02:45	7.03	0.83	6.20	0	199.5		
30/12/2002 03:00	7.19	0.83	6.36	0	199.75		
30/12/2002 03:15	7.39	0.83	6.56	0	200		
30/12/2002 03:30	7.55	0.83	6.72	0	200.25		
30/12/2002 03:45	7.75	0.83	6.92	0	200.5		
30/12/2002 04:00	7.95	0.83	7.12	0	200.75		
30/12/2002 04:15	8.13	0.83	7.30	0	201		
30/12/2002 04:30	8.31	0.83	7.48	0	201.25		
30/12/2002 04:45	8.43	0.83	7.60	0	201.5		
30/12/2002 05:00	8.57	0.83	7.74	0	201.75		
30/12/2002 05:15	8.68	0.83	7.85	0	202		
30/12/2002 05:30	8.80	0.83	7.97	0	202.25		
30/12/2002 05:45	8.88	0.83	8.05	0	202.5		
30/12/2002 06:00	8.99	0.83	8.16	0	202.75		
30/12/2002 06:15	9.04	0.83	8.21	0	203		
30/12/2002 06:30	9.08	0.83	8.25	0	203.25		
30/12/2002 06:45	9.15	0.83	8.32	0	203.5		
30/12/2002 07:00	9.15	0.83	8.32	0	203.75		
30/12/2002 07:15	9.17	0.83	8.34	0	204		
30/12/2002 07:30	9.17	0.83	8.34	0	204.25		
30/12/2002 07:45	9.17	0.83	8.34	0	204.5		
30/12/2002 08:00	9.17	0.83	8.34	0	204.75		
30/12/2002 08:15	9.13	0.83	8.30	0	205		
30/12/2002 08:30	9.06	0.83	8.23	0	205.25		
30/12/2002 08:45	9.02	0.83	8.19	0	205.5		
30/12/2002 09:00	8.97	0.83	8.14	0	205.75		
30/12/2002 09:15	8.87	0.83	8.04	0	206		
30/12/2002 09:30	8.75	0.83	7.92	0	206.25		
30/12/2002 09:45	8.68	0.83	7.85	0	206.5		
30/12/2002 10:00	8.57	0.83	7.74	0	206.75		
30/12/2002 10:15	8.48	0.83	7.65	0	207		
30/12/2002 10:30	8.31	0.83	7.48	0	207.25		
30/12/2002 10:45	8.18	0.83	7.35	0	207.5		
30/12/2002 11:00	8.02	0.83	7.19	0	207.75		
30/12/2002 11:15	7.86	0.83	7.03	0	208		
30/12/2002 11:30	7.70	0.83	6.87	0	208.25		
30/12/2002 11:45	7.55	0.83	6.72	0	208.5		
30/12/2002 12:00	7.37	0.83	6.54	0	208.75		
30/12/2002 12:15	7.23	0.83	6.40	0	209		
30/12/2002 12:30	7.08	0.83	6.25	0	209.25		
30/12/2002 12:45	6.93	0.83	6.10	0	209.5		
30/12/2002 13:00	6.76	0.83	5.93	0	209.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
30/12/2002 13:15	6.63	0.83	5.80	0	210		
30/12/2002 13:30	6.48	0.83	5.65	0	210.25		
30/12/2002 13:45	6.32	0.83	5.49	0	210.5		
30/12/2002 14:00	6.21	0.83	5.38	0	210.75		
30/12/2002 14:15	6.11	0.83	5.28	0	211		
30/12/2002 14:30	5.97	0.83	5.14	0	211.25		
30/12/2002 14:45	5.83	0.83	5.00	0	211.5		
30/12/2002 15:00	5.71	0.83	4.88	0	211.75		
30/12/2002 15:15	5.61	0.83	4.78	0	212		
30/12/2002 15:30	5.47	0.83	4.64	0	212.25		
30/12/2002 15:45	5.33	0.83	4.50	0	212.5		
30/12/2002 16:00	5.14	0.83	4.31	0	212.75		
30/12/2002 16:15	4.98	0.83	4.15	0	213		
30/12/2002 16:30	4.79	0.83	3.96	0	213.25		
30/12/2002 16:45	4.60	0.83	3.77	0	213.5		
30/12/2002 17:00	4.40	0.83	3.57	0	213.75		
30/12/2002 17:15	4.19	0.83	3.36	0	214		
30/12/2002 17:30	3.96	0.83	3.13	0	214.25		
30/12/2002 17:45	3.75	0.83	2.92	0	214.5		
30/12/2002 18:00	3.54	0.83	2.71	0.2	214.75		
30/12/2002 18:15	3.36	0.83	2.53	0.2	215		
30/12/2002 18:30	3.19	0.83	2.36	0	215.25		
30/12/2002 18:45	3.02	0.83	2.19	0	215.5		
30/12/2002 19:00	2.89	0.83	2.06	0	215.75		
30/12/2002 19:15	2.76	0.83	1.93	0	216		
30/12/2002 19:30	2.64	0.83	1.81	0	216.25		
30/12/2002 19:45	2.52	0.83	1.69	0	216.5		
30/12/2002 20:00	2.45	0.83	1.62	0	216.75		
30/12/2002 20:15	2.37	0.83	1.54	0	217		
30/12/2002 20:30	2.30	0.83	1.47	0	217.25		
30/12/2002 20:45	2.23	0.83	1.40	0	217.5		
30/12/2002 21:00	2.20	0.83	1.37	0	217.75		
30/12/2002 21:15	2.12	0.83	1.29	0	218		
30/12/2002 21:30	2.08	0.83	1.25	0	218.25		
30/12/2002 21:45	2.04	0.83	1.21	0	218.5		
30/12/2002 22:00	2.00	0.83	1.17	0	218.75		
30/12/2002 22:15	1.96	0.83	1.13	0	219		
30/12/2002 22:30	1.93	0.83	1.10	0	219.25		
30/12/2002 22:45	1.88	0.83	1.05	0	219.5		
30/12/2002 23:00	1.86	0.83	1.03	0	219.75		
30/12/2002 23:15	1.84	0.83	1.01	0	220		
30/12/2002 23:30	1.82	0.83	0.99	0	220.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
30/12/2002 23:45	1.78	0.83	0.95	0	220.5		
31/12/2002 00:00	1.75	0.83	0.92	0	220.75		
31/12/2002 00:15	1.75	0.83	0.92	0	221		
31/12/2002 00:30	1.72	0.83	0.89	0	221.25		
31/12/2002 00:45	1.69	0.83	0.86	0	221.5		
31/12/2002 01:00	1.68	0.83	0.85	0	221.75		
31/12/2002 01:15	1.65	0.83	0.82	0	222		
31/12/2002 01:30	1.64	0.83	0.81	0	222.25		
31/12/2002 01:45	1.61	0.83	0.78	0	222.5		
31/12/2002 02:00	1.60	0.83	0.77	0	222.75		
31/12/2002 02:15	1.58	0.83	0.75	0	223		
31/12/2002 02:30	1.57	0.83	0.74	0	223.25		
31/12/2002 02:45	1.54	0.83	0.71	0	223.5		
31/12/2002 03:00	1.53	0.83	0.70	0	223.75		
31/12/2002 03:15	1.52	0.83	0.69	0	224		
31/12/2002 03:30	1.50	0.83	0.67	0	224.25		
31/12/2002 03:45	1.48	0.83	0.65	0	224.5		
31/12/2002 04:00	1.47	0.83	0.64	0	224.75		
31/12/2002 04:15	1.46	0.83	0.63	0	225		
31/12/2002 04:30	1.44	0.83	0.61	0	225.25		
31/12/2002 04:45	1.42	0.83	0.59	0	225.5		
31/12/2002 05:00	1.41	0.83	0.58	0	225.75		
31/12/2002 05:15	1.39	0.83	0.56	0	226		
31/12/2002 05:30	1.39	0.83	0.56	0	226.25		
31/12/2002 05:45	1.38	0.83	0.55	0	226.5		
31/12/2002 06:00	1.36	0.83	0.53	0.2	226.75		
31/12/2002 06:15	1.35	0.83	0.52	0	227		
31/12/2002 06:30	1.34	0.83	0.51	0	227.25		
31/12/2002 06:45	1.32	0.83	0.49	0	227.5		
31/12/2002 07:00	1.31	0.83	0.48	0	227.75		
31/12/2002 07:15	1.31	0.83	0.48	0	228		
31/12/2002 07:30	1.29	0.83	0.46	0	228.25		
31/12/2002 07:45	1.28	0.83	0.45	0	228.5		
31/12/2002 08:00	1.28	0.83	0.45	0	228.75		
31/12/2002 08:15	1.25	0.83	0.42	0	229		
31/12/2002 08:30	1.25	0.83	0.42	0	229.25		
31/12/2002 08:45	1.24	0.83	0.41	0	229.5		
31/12/2002 09:00	1.23	0.83	0.40	0	229.75		
31/12/2002 09:15	1.22	0.83	0.39	0	230		
31/12/2002 09:30	1.21	0.83	0.38	0	230.25		
31/12/2002 09:45	1.20	0.83	0.37	0	230.5		
31/12/2002 10:00	1.19	0.83	0.36	0	230.75		

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
31/12/2002 10:15	1.18	0.83	0.35	0	231
31/12/2002 10:30	1.17	0.83	0.34	0	231.25
31/12/2002 10:45	1.16	0.83	0.33	0	231.5
31/12/2002 11:00	1.16	0.83	0.33	0	231.75
31/12/2002 11:15	1.14	0.83	0.31	0	232
31/12/2002 11:30	1.14	0.83	0.31	0	232.25
31/12/2002 11:45	1.13	0.83	0.30	0	232.5
31/12/2002 12:00	1.13	0.83	0.30	0	232.75
31/12/2002 12:15	1.11	0.83	0.28	0	233
31/12/2002 12:30	1.11	0.83	0.28	0	233.25
31/12/2002 12:45	1.11	0.83	0.28	0	233.5
31/12/2002 13:00	1.10	0.83	0.27	0	233.75
31/12/2002 13:15	1.09	0.83	0.26	0	234
31/12/2002 13:30	1.09	0.83	0.26	0	234.25
31/12/2002 13:45	1.08	0.83	0.25	0	234.5
31/12/2002 14:00	1.08	0.83	0.25	0	234.75
31/12/2002 14:15	1.07	0.83	0.24	0	235
31/12/2002 14:30	1.06	0.83	0.23	0	235.25
31/12/2002 14:45	1.05	0.83	0.22	0	235.5
31/12/2002 15:00	1.04	0.83	0.21	0	235.75
31/12/2002 15:15	1.03	0.83	0.20	0	236
31/12/2002 15:30	1.03	0.83	0.20	0	236.25
31/12/2002 15:45	1.02	0.83	0.19	0	236.5
31/12/2002 16:00	1.01	0.83	0.18	0	236.75
31/12/2002 16:15	1.01	0.83	0.18	0	237
31/12/2002 16:30	1.00	0.83	0.17	0	237.25
31/12/2002 16:45	0.99	0.83	0.16	0	237.5
31/12/2002 17:00	0.99	0.83	0.16	0	237.75
31/12/2002 17:15	0.98	0.83	0.15	0	238
31/12/2002 17:30	0.98	0.83	0.15	0	238.25
31/12/2002 17:45	0.97	0.83	0.14	0	238.5
31/12/2002 18:00	0.97	0.83	0.14	0	238.75
31/12/2002 18:15	0.96	0.83	0.13	0	239
31/12/2002 18:30	0.96	0.83	0.13	0	239.25
31/12/2002 18:45	0.95	0.83	0.12	0	239.5
31/12/2002 19:00	0.95	0.83	0.12	0	239.75
31/12/2002 19:15	0.95	0.83	0.12	0	240
31/12/2002 19:30	0.94	0.83	0.11	0	240.25
31/12/2002 19:45	0.94	0.83	0.11	0	240.5
31/12/2002 20:00	0.93	0.83	0.10	0	240.75
31/12/2002 20:15	0.93	0.83	0.10	0	241
31/12/2002 20:30	0.93	0.83	0.10	0	241.25

First peak	Second peak

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
31/12/2002 20:45	0.92	0.83	0.09	0	241.5
31/12/2002 21:00	0.92	0.83	0.09	0	241.75
31/12/2002 21:15	0.91	0.83	0.08	0	242
31/12/2002 21:30	0.91	0.83	0.08	0	242.25
31/12/2002 21:45	0.91	0.83	0.08	0	242.5
31/12/2002 22:00	0.91	0.83	0.08	0	242.75
31/12/2002 22:15	0.90	0.83	0.07	0	243
31/12/2002 22:30	0.90	0.83	0.07	0	243.25
31/12/2002 22:45	0.89	0.83	0.06	0	243.5
31/12/2002 23:00	0.89	0.83	0.06	0	243.75
31/12/2002 23:15	0.89	0.83	0.06	0	244
31/12/2002 23:30	0.88	0.83	0.05	0	244.25
31/12/2002 23:45	0.88	0.83	0.05	0	244.5
01/01/2003 00:00	0.88	0.83	0.05	0	244.75
01/01/2003 00:15	0.88	0.83	0.05	0	245
01/01/2003 00:30	0.88	0.83	0.05	0	245.25
01/01/2003 00:45	0.87	0.83	0.04	0	245.5
01/01/2003 01:00	0.87	0.83	0.04	0	245.75
01/01/2003 01:15	0.87	0.83	0.04	0	246
01/01/2003 01:30	0.86	0.83	0.03	0	246.25
01/01/2003 01:45	0.86	0.83	0.03	0	246.5
01/01/2003 02:00	0.86	0.83	0.03	0	246.75
01/01/2003 02:15	0.85	0.83	0.02	0	247
01/01/2003 02:30	0.85	0.83	0.02	0	247.25
01/01/2003 02:45	0.85	0.83	0.02	0	247.5
01/01/2003 03:00	0.84	0.83	0.01	0	247.75
01/01/2003 03:15	0.84	0.83	0.01	0	248
01/01/2003 03:30	0.84	0.83	0.01	0	248.25
01/01/2003 03:45	0.84	0.83	0.01	0	248.5
01/01/2003 04:00	0.84	0.83	0.01	0	248.75
01/01/2003 04:15	0.83	0.83	0.00	0	249
01/01/2003 04:30	0.83	0.83	0.00	0	249.25
01/01/2003 04:45	0.83	0.83	0.00	0	249.5
01/01/2003 05:00	0.83	0.83	0.00	0	249.75
01/01/2003 05:15	0.83	0.83	0.00	0	250
01/01/2003 05:30	0.83	0.83	0.00	0	250.25
01/01/2003 05:45	0.83	0.83	0.00	0.2	250.5
01/01/2003 06:00	0.82	0.82	0.00	0.2	250.75
01/01/2003 06:15	0.82	0.82	0.00	0.2	251
01/01/2003 06:30	0.82	0.82	0.00	0.2	251.25
01/01/2003 06:45	0.81	0.81	0.00	0.2	251.5
01/01/2003 07:00	0.81	0.81	0.00	0.6	251.75

First peak	Second peak

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
01/01/2003 07:15	0.81	0.81	0.00	0.8	252		
01/01/2003 07:30	0.82	0.82	0.00	0.8	252.25		
01/01/2003 07:45	0.82	0.82	0.00	0.8	252.5		
01/01/2003 08:00	0.83	0.83	0.00	0.8	252.75		
01/01/2003 08:15	0.83	0.83	0.00	0.4	253		
01/01/2003 08:30	0.84	0.83	0.01	0.8	253.25		
01/01/2003 08:45	0.85	0.83	0.02	0.8	253.5		
01/01/2003 09:00	0.87	0.83	0.04	1	253.75		
01/01/2003 09:15	0.89	0.83	0.06	0.2	254		
01/01/2003 09:30	0.93	0.83	0.10	0.6	254.25		
01/01/2003 09:45	0.96	0.83	0.13	0.2	254.5		
01/01/2003 10:00	1.02	0.83	0.19	0.2	254.75		
01/01/2003 10:15	1.10	0.83	0.27	0.2	255		
01/01/2003 10:30	1.20	0.83	0.37	0	255.25		
01/01/2003 10:45	1.34	0.83	0.51	0	255.5		
01/01/2003 11:00	1.52	0.83	0.69	0.4	255.75		
01/01/2003 11:15	1.71	0.83	0.88	0.4	256		
01/01/2003 11:30	1.92	0.83	1.09	0.2	256.25		
01/01/2003 11:45	2.16	0.83	1.33	0	256.5		
01/01/2003 12:00	2.35	0.83	1.52	0	256.75		
01/01/2003 12:15	2.56	0.83	1.73	0	257		
01/01/2003 12:30	2.77	0.83	1.94	0	257.25		
01/01/2003 12:45	3.00	0.83	2.17	0	257.5		
01/01/2003 13:00	3.26	0.83	2.43	0	257.75		
01/01/2003 13:15	3.53	0.83	2.70	0	258		
01/01/2003 13:30	3.80	0.83	2.97	0	258.25		
01/01/2003 13:45	4.01	0.83	3.18	0	258.5		
01/01/2003 14:00	4.22	0.83	3.39	0	258.75		
01/01/2003 14:15	4.41	0.83	3.58	0.2	259		
01/01/2003 14:30	4.57	0.83	3.74	2	259.25		
01/01/2003 14:45	4.69	0.83	3.86	0	259.5		
01/01/2003 15:00	4.79	0.83	3.96	0	259.75		
01/01/2003 15:15	4.93	0.83	4.10	0	260		
01/01/2003 15:30	5.04	0.83	4.21	1	260.25		
01/01/2003 15:45	5.16	0.83	4.33	1	260.5		
01/01/2003 16:00	5.30	0.83	4.47	1	260.75		
01/01/2003 16:15	5.46	0.83	4.63	1	261		
01/01/2003 16:30	5.58	0.83	4.75	0.8	261.25		
01/01/2003 16:45	5.73	0.83	4.90	0.4	261.5		
01/01/2003 17:00	5.87	0.83	5.04	0.8	261.75		
01/01/2003 17:15	6.02	0.83	5.19	0.2	262		
01/01/2003 17:30	6.22	0.83	5.39	0.4	262.25		

	Middleton			Earl Soham	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
01/01/2003 17:45	6.37	0.83	5.54	0.2	262.5
01/01/2003 18:00	6.51	0.83	5.68	0	262.75
01/01/2003 18:15	6.67	0.83	5.84	0	263
01/01/2003 18:30	6.89	0.83	6.06	0	263.25
01/01/2003 18:45	7.09	0.83	6.26	0	263.5
01/01/2003 19:00	7.32	0.83	6.49	0	263.75
01/01/2003 19:15	7.65	0.83	6.82	0	264
01/01/2003 19:30	7.94	0.83	7.11	0	264.25
01/01/2003 19:45	8.34	0.83	7.51	0	264.5
01/01/2003 20:00	8.77	0.83	7.94	0	264.75
01/01/2003 20:15	9.28	0.83	8.45	0	265
01/01/2003 20:30	9.82	0.83	8.99	0	265.25
01/01/2003 20:45	10.38	0.83	9.55	0	265.5
01/01/2003 21:00	10.88	0.83	10.05	0	265.75
01/01/2003 21:15	11.42	0.83	10.59	0	266
01/01/2003 21:30	11.86	0.83	11.03	0	266.25
01/01/2003 21:45	12.20	0.83	11.37	0	266.5
01/01/2003 22:00	12.47	0.83	11.64	0	266.75
01/01/2003 22:15	12.79	0.83	11.96	0	267
01/01/2003 22:30	12.95	0.83	12.12	0	267.25
01/01/2003 22:45	13.14	0.83	12.31	0	267.5
01/01/2003 23:00	13.38	0.83	12.55	0	267.75
01/01/2003 23:15	13.55	0.83	12.72	0	268
01/01/2003 23:30	13.58	0.83	12.75	0	268.25
01/01/2003 23:45	13.65	0.83	12.82	0	268.5
02/01/2003 00:00	13.65	0.83	12.82	0	268.75
02/01/2003 00:15	13.76	0.83	12.93	0	269
02/01/2003 00:30	13.79	0.83	12.96	0	269.25
02/01/2003 00:45	13.72	0.83	12.89	0	269.5
02/01/2003 01:00	13.83	0.83	13.00	0.2	269.75
02/01/2003 01:15	13.69	0.83	12.86	0	270
02/01/2003 01:30	13.65	0.83	12.82	0	270.25
02/01/2003 01:45	13.76	0.83	12.93	0	270.5
02/01/2003 02:00	13.79	0.83	12.96	0	270.75
02/01/2003 02:15	13.69	0.83	12.86	0	271
02/01/2003 02:30	13.79	0.83	12.96	0	271.25
02/01/2003 02:45	13.79	0.83	12.96	0	271.5
02/01/2003 03:00	13.83	0.83	13.00	0	271.75
02/01/2003 03:15	13.72	0.83	12.89	0	272
02/01/2003 03:30	13.86	0.83	13.03	0	272.25
02/01/2003 03:45	13.93	0.83	13.10	0	272.5
02/01/2003 04:00	13.93	0.83	13.10	0	272.75

First peak

Second peak

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
02/01/2003 04:15	13.93	0.83	13.10	0	273		
02/01/2003 04:30	14.12	0.83	13.29	0	273.25		
02/01/2003 04:45	14.04	0.83	13.21	0	273.5		
02/01/2003 05:00	14.12	0.83	13.29	0	273.75		
02/01/2003 05:15	14.12	0.83	13.29	0	274		
02/01/2003 05:30	14.12	0.83	13.29	0	274.25		
02/01/2003 05:45	14.26	0.83	13.43	0	274.5		
02/01/2003 06:00	14.15	0.83	13.32	0	274.75		
02/01/2003 06:15	14.12	0.83	13.29	0	275		
02/01/2003 06:30	14.08	0.83	13.25	0	275.25		
02/01/2003 06:45	14.04	0.83	13.21	0	275.5		
02/01/2003 07:00	14.01	0.83	13.18	0	275.75		
02/01/2003 07:15	13.93	0.83	13.10	0	276		
02/01/2003 07:30	13.93	0.83	13.10	0	276.25		
02/01/2003 07:45	13.79	0.83	12.96	0.2	276.5		
02/01/2003 08:00	13.76	0.83	12.93	0.2	276.75		
02/01/2003 08:15	13.69	0.83	12.86	0	277		
02/01/2003 08:30	13.48	0.83	12.65	0	277.25		
02/01/2003 08:45	13.34	0.83	12.51	0	277.5		
02/01/2003 09:00	13.14	0.83	12.31	0.4	277.75		
02/01/2003 09:15	13.01	0.83	12.18	1.2	278		
02/01/2003 09:30	12.88	0.83	12.05	1.2	278.25		
02/01/2003 09:45	12.69	0.83	11.86	1	278.5		
02/01/2003 10:00	12.54	0.83	11.71	1.4	278.75		
02/01/2003 10:15	12.38	0.83	11.55	1.2	279		
02/01/2003 10:30	12.11	0.83	11.28	0.2	279.25		
02/01/2003 10:45	11.88	0.83	11.05	0	279.5		
02/01/2003 11:00	11.69	0.83	10.86	0	279.75		
02/01/2003 11:15	11.42	0.83	10.59	0	280		
02/01/2003 11:30	11.21	0.83	10.38	0	280.25		
02/01/2003 11:45	10.95	0.83	10.12	0	280.5		
02/01/2003 12:00	10.76	0.83	9.93	0	280.75		
02/01/2003 12:15	10.59	0.83	9.76	0	281		
02/01/2003 12:30	10.38	0.83	9.55	0	281.25		
02/01/2003 12:45	10.23	0.83	9.40	0	281.5		
02/01/2003 13:00	10.01	0.83	9.18	0	281.75		
02/01/2003 13:15	9.86	0.83	9.03	0	282		
02/01/2003 13:30	9.70	0.83	8.87	0	282.25		
02/01/2003 13:45	9.56	0.83	8.73	0	282.5		
02/01/2003 14:00	9.39	0.83	8.56	0	282.75		
02/01/2003 14:15	9.24	0.83	8.41	0	283		
02/01/2003 14:30	9.06	0.83	8.23	0	283.25		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
02/01/2003 14:45	8.94	0.83	8.11	0	283.5		
02/01/2003 15:00	8.78	0.83	7.95	0	283.75		
02/01/2003 15:15	8.67	0.83	7.84	0	284		
02/01/2003 15:30	8.56	0.83	7.73	0	284.25		
02/01/2003 15:45	8.45	0.83	7.62	0	284.5		
02/01/2003 16:00	8.34	0.83	7.51	0	284.75		
02/01/2003 16:15	8.22	0.83	7.39	0	285		
02/01/2003 16:30	8.18	0.83	7.35	0	285.25		
02/01/2003 16:45	8.12	0.83	7.29	0	285.5		
02/01/2003 17:00	8.06	0.83	7.23	0	285.75		
02/01/2003 17:15	8.04	0.83	7.21	0	286		
02/01/2003 17:30	8.02	0.83	7.19	0	286.25		
02/01/2003 17:45	8.02	0.83	7.19	0	286.5		
02/01/2003 18:00	8.04	0.83	7.21	0	286.75		
02/01/2003 18:15	8.05	0.83	7.22	0.2	287		
02/01/2003 18:30	8.09	0.83	7.26	0	287.25		
02/01/2003 18:45	8.15	0.83	7.32	0	287.5		
02/01/2003 19:00	8.22	0.83	7.39	0	287.75		
02/01/2003 19:15	8.30	0.83	7.47	0	288		
02/01/2003 19:30	8.36	0.83	7.53	0	288.25		
02/01/2003 19:45	8.40	0.83	7.57	0	288.5		
02/01/2003 20:00	8.48	0.83	7.65	0	288.75		
02/01/2003 20:15	8.52	0.83	7.69	0	289		
02/01/2003 20:30	8.59	0.83	7.76	0	289.25		
02/01/2003 20:45	8.64	0.83	7.81	0	289.5		
02/01/2003 21:00	8.68	0.83	7.85	0	289.75		
02/01/2003 21:15	8.72	0.83	7.89	0	290		
02/01/2003 21:30	8.77	0.83	7.94	0	290.25		
02/01/2003 21:45	8.82	0.83	7.99	0	290.5		
02/01/2003 22:00	8.83	0.83	8.00	0	290.75		
02/01/2003 22:15	8.82	0.83	7.99	0	291		
02/01/2003 22:30	8.85	0.83	8.02	0	291.25		
02/01/2003 22:45	8.87	0.83	8.04	0	291.5		
02/01/2003 23:00	8.83	0.83	8.00	0	291.75		
02/01/2003 23:15	8.85	0.83	8.02	0	292		
02/01/2003 23:30	8.80	0.83	7.97	0	292.25		
02/01/2003 23:45	8.78	0.83	7.95	0	292.5		
03/01/2003 00:00	8.73	0.83	7.90	0	292.75		
03/01/2003 00:15	8.67	0.83	7.84	0	293		
03/01/2003 00:30	8.60	0.83	7.77	0	293.25		
03/01/2003 00:45	8.56	0.83	7.73	0.2	293.5		
03/01/2003 01:00	8.46	0.83	7.63	0.2	293.75		

	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
03/01/2003 01:15	8.36	0.83	7.53	0.6	294		
03/01/2003 01:30	8.25	0.83	7.42	0.2	294.25		
03/01/2003 01:45	8.12	0.83	7.29	0.2	294.5		
03/01/2003 02:00	8.01	0.83	7.18	0	294.75		
03/01/2003 02:15	7.86	0.83	7.03	0.2	295		
03/01/2003 02:30	7.74	0.83	6.91	0	295.25		
03/01/2003 02:45	7.59	0.83	6.76	0	295.5		
03/01/2003 03:00	7.44	0.83	6.61	0	295.75		
03/01/2003 03:15	7.30	0.83	6.47	0	296		
03/01/2003 03:30	7.12	0.83	6.29	0	296.25		
03/01/2003 03:45	6.99	0.83	6.16	0	296.5		
03/01/2003 04:00	6.87	0.83	6.04	0	296.75		
03/01/2003 04:15	6.70	0.83	5.87	0.2	297		
03/01/2003 04:30	6.54	0.83	5.71	0	297.25		
03/01/2003 04:45	6.45	0.83	5.62	0	297.5		
03/01/2003 05:00	6.33	0.83	5.50	0	297.75		
03/01/2003 05:15	6.19	0.83	5.36	0	298		
03/01/2003 05:30	6.07	0.83	5.24	0	298.25		
03/01/2003 05:45	5.95	0.83	5.12	0.2	298.5		
03/01/2003 06:00	5.85	0.83	5.02	0	298.75		
03/01/2003 06:15	5.73	0.83	4.90	0	299		
03/01/2003 06:30	5.60	0.83	4.77	0	299.25		
03/01/2003 06:45	5.49	0.83	4.66	0	299.5		
03/01/2003 07:00	5.34	0.83	4.51	0	299.75		
03/01/2003 07:15	5.21	0.83	4.38	0	300		
03/01/2003 07:30	5.04	0.83	4.21	0	300.25		
03/01/2003 07:45	4.89	0.83	4.06	0	300.5		
03/01/2003 08:00	4.72	0.83	3.89	0	300.75		
03/01/2003 08:15	4.56	0.83	3.73	0	301		
03/01/2003 08:30	4.39	0.83	3.56	0	301.25		
03/01/2003 08:45	4.17	0.83	3.34	0	301.5		
03/01/2003 09:00	3.99	0.83	3.16	0	301.75		
03/01/2003 09:15	3.79	0.83	2.96	0	302		
03/01/2003 09:30	3.63	0.83	2.80	0	302.25		
03/01/2003 09:45	3.46	0.83	2.63	0	302.5		
03/01/2003 10:00	3.29	0.83	2.46	0	302.75		
03/01/2003 10:15	3.15	0.83	2.32	0	303		
03/01/2003 10:30	3.02	0.83	2.19	0	303.25		
03/01/2003 10:45	2.90	0.83	2.07	0	303.5		
03/01/2003 11:00	2.79	0.83	1.96	0	303.75		
03/01/2003 11:15	2.71	0.83	1.88	0	304		
03/01/2003 11:30	2.62	0.83	1.79	0	304.25		

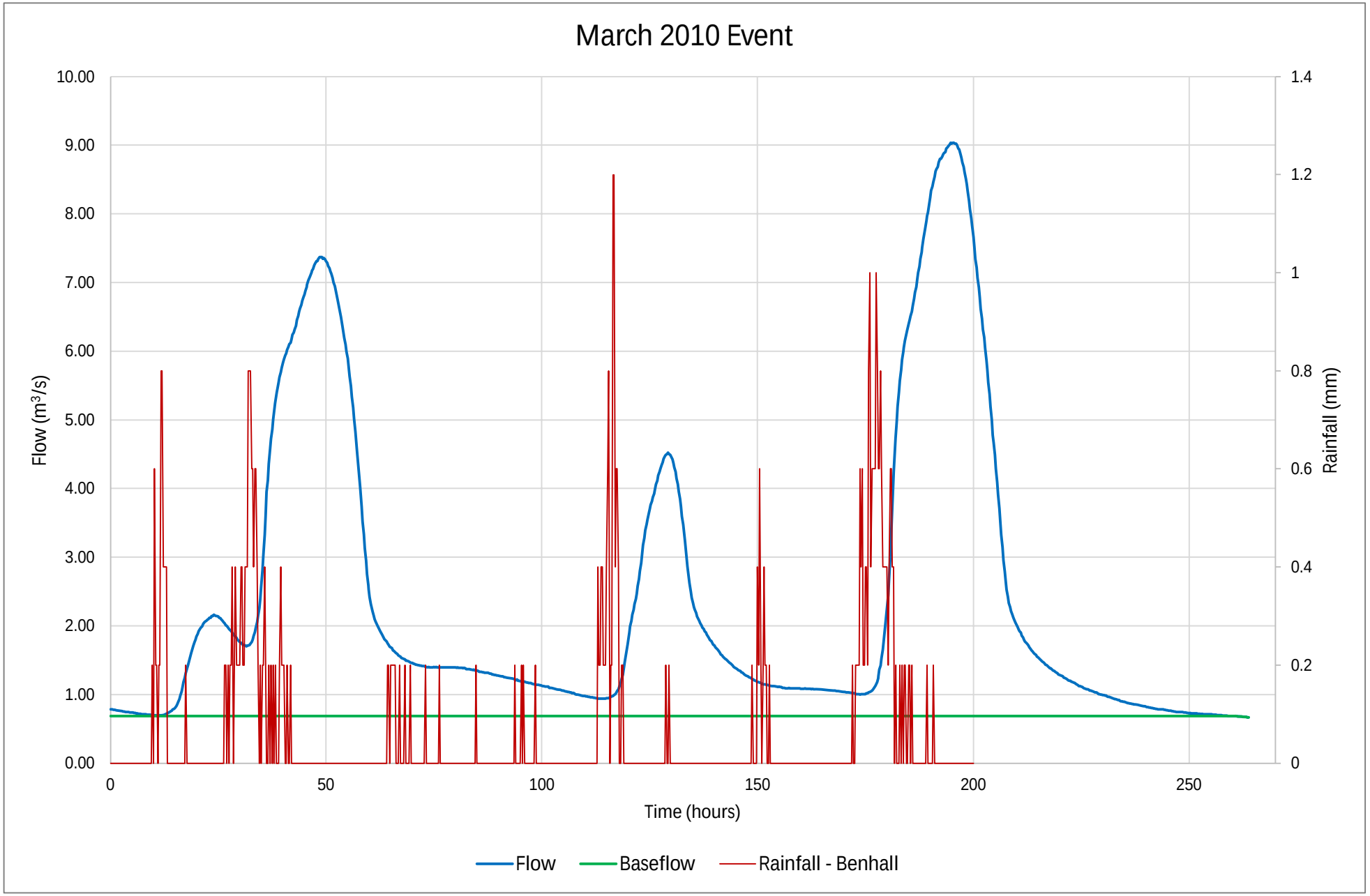
	Middleton			Earl Soham		First peak	Second peak
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours		
03/01/2003 11:45	2.53	0.83	1.70	0	304.5		
03/01/2003 12:00	2.47	0.83	1.64	0	304.75		
03/01/2003 12:15	2.40	0.83	1.57	0	305		
03/01/2003 12:30	2.35	0.83	1.52	0	305.25		
03/01/2003 12:45	2.31	0.83	1.48	0	305.5		
03/01/2003 13:00	2.25	0.83	1.42	0	305.75		
03/01/2003 13:15	2.22	0.83	1.39	0	306		
03/01/2003 13:30	2.20	0.83	1.37	0	306.25		
03/01/2003 13:45	2.15	0.83	1.32	0	306.5		
03/01/2003 14:00	2.12	0.83	1.29	0	306.75		
03/01/2003 14:15	2.12	0.83	1.29	0	307		
03/01/2003 14:30	2.08	0.83	1.25	0	307.25		
03/01/2003 14:45	2.06	0.83	1.23	0	307.5		
03/01/2003 15:00	2.03	0.83	1.20	0	307.75		
03/01/2003 15:15	2.02	0.83	1.19	0	308		
03/01/2003 15:30	1.99	0.83	1.16	0	308.25		
03/01/2003 15:45	1.97	0.83	1.14	0	308.5		
03/01/2003 16:00	1.95	0.83	1.12	0	308.75		
03/01/2003 16:15	1.95	0.83	1.12	0	309		
03/01/2003 16:30	1.91	0.83	1.08	0	309.25		
03/01/2003 16:45	1.83	0.83	1.00		309.5		
03/01/2003 17:00	1.82	0.83	0.99		309.75		
03/01/2003 17:15	1.82	0.83	0.99		310		
03/01/2003 17:30	1.79	0.83	0.96		310.25		
03/01/2003 17:45	1.77	0.83	0.94		310.5		
03/01/2003 18:00	1.76	0.83	0.93		310.75		
03/01/2003 18:15	1.76	0.83	0.93		311		
03/01/2003 18:30	1.74	0.83	0.91		311.25		
03/01/2003 18:45	1.73	0.83	0.90		311.5		
03/01/2003 19:00	1.71	0.83	0.88		311.75		
03/01/2003 19:15	1.70	0.83	0.87		312		
03/01/2003 19:30	1.70	0.83	0.87		312.25		
03/01/2003 19:45	1.68	0.83	0.85		312.5		
03/01/2003 20:00	1.67	0.83	0.84		312.75		
03/01/2003 20:15	1.66	0.83	0.83		313		
03/01/2003 20:30	1.65	0.83	0.82		313.25		
03/01/2003 20:45	1.64	0.83	0.81		313.5		
03/01/2003 21:00	1.62	0.83	0.79		313.75		
03/01/2003 21:15	1.61	0.83	0.78		314		
03/01/2003 21:30	1.59	0.83	0.76		314.25		
03/01/2003 21:45	1.59	0.83	0.76		314.5		
03/01/2003 22:00	1.58	0.83	0.75		314.75		

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
03/01/2003 22:15	1.57	0.83	0.74		315		
03/01/2003 22:30	1.55	0.83	0.72		315.25		
03/01/2003 22:45	1.54	0.83	0.71		315.5		
03/01/2003 23:00	1.53	0.83	0.70		315.75		
03/01/2003 23:15	1.52	0.83	0.69		316		
03/01/2003 23:30	1.51	0.83	0.68		316.25		
03/01/2003 23:45	1.50	0.83	0.67		316.5		
04/01/2003 00:00	1.49	0.83	0.66		316.75		
04/01/2003 00:15	1.48	0.83	0.65		317		
04/01/2003 00:30	1.47	0.83	0.64		317.25		
04/01/2003 00:45	1.45	0.83	0.62		317.5		
04/01/2003 01:00	1.44	0.83	0.61		317.75		
04/01/2003 01:15	1.44	0.83	0.61		318		
04/01/2003 01:30	1.43	0.83	0.60		318.25		
04/01/2003 01:45	1.42	0.83	0.59		318.5		
04/01/2003 02:00	1.41	0.83	0.58		318.75		
04/01/2003 02:15	1.40	0.83	0.57		319		
04/01/2003 02:30	1.38	0.83	0.55		319.25		
04/01/2003 02:45	1.38	0.83	0.55		319.5		
04/01/2003 03:00	1.38	0.83	0.55		319.75		
04/01/2003 03:15	1.37	0.83	0.54		320		
04/01/2003 03:30	1.35	0.83	0.52		320.25		
04/01/2003 03:45	1.34	0.83	0.51		320.5		
04/01/2003 04:00	1.34	0.83	0.51		320.75		
04/01/2003 04:15	1.33	0.83	0.50		321		
04/01/2003 04:30	1.32	0.83	0.49		321.25		
04/01/2003 04:45	1.32	0.83	0.49		321.5		
04/01/2003 05:00	1.31	0.83	0.48		321.75		
04/01/2003 05:15	1.30	0.83	0.47		322		
04/01/2003 05:30	1.30	0.83	0.47		322.25		
04/01/2003 05:45	1.29	0.83	0.46		322.5		
04/01/2003 06:00	1.28	0.83	0.45		322.75		
04/01/2003 06:15	1.27	0.83	0.44		323		
04/01/2003 06:30	1.27	0.83	0.44		323.25		
04/01/2003 06:45	1.27	0.83	0.44		323.5		
04/01/2003 07:00	1.26	0.83	0.43		323.75		
04/01/2003 07:15	1.26	0.83	0.43		324		
04/01/2003 07:30	1.25	0.83	0.42		324.25		
04/01/2003 07:45	1.25	0.83	0.42		324.5		
04/01/2003 08:00	1.24	0.83	0.41		324.75		
04/01/2003 08:15	1.24	0.83	0.41		325		
04/01/2003 08:30	1.24	0.83	0.41		325.25		

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
04/01/2003 08:45	1.23	0.83	0.40		325.5		
04/01/2003 09:00	1.23	0.83	0.40		325.75		
04/01/2003 09:15	1.22	0.83	0.39		326		
04/01/2003 09:30	1.22	0.83	0.39		326.25		
04/01/2003 09:45	1.22	0.83	0.39		326.5		
04/01/2003 10:00	1.22	0.83	0.39		326.75		
04/01/2003 10:15	1.21	0.83	0.38		327		
04/01/2003 10:30	1.21	0.83	0.38		327.25		
04/01/2003 10:45	1.20	0.83	0.37		327.5		
04/01/2003 11:00	1.20	0.83	0.37		327.75		
04/01/2003 11:15	1.20	0.83	0.37		328		
04/01/2003 11:30	1.19	0.83	0.36		328.25		
04/01/2003 11:45	1.19	0.83	0.36		328.5		
04/01/2003 12:00	1.19	0.83	0.36		328.75		
04/01/2003 12:15	1.18	0.83	0.35		329		
04/01/2003 12:30	1.18	0.83	0.35		329.25		
04/01/2003 12:45	1.17	0.83	0.34		329.5		
04/01/2003 13:00	1.17	0.83	0.34		329.75		
04/01/2003 13:15	1.16	0.83	0.33		330		
04/01/2003 13:30	1.16	0.83	0.33		330.25		
04/01/2003 13:45	1.15	0.83	0.32		330.5		
04/01/2003 14:00	1.15	0.83	0.32		330.75		
04/01/2003 14:15	1.14	0.83	0.31		331		
04/01/2003 14:30	1.13	0.83	0.30		331.25		
04/01/2003 14:45	1.13	0.83	0.30		331.5		
04/01/2003 15:00	1.13	0.83	0.30		331.75		
04/01/2003 15:15	1.13	0.83	0.30		332		
04/01/2003 15:30	1.12	0.83	0.29		332.25		
04/01/2003 15:45	1.12	0.83	0.29		332.5		
04/01/2003 16:00	1.11	0.83	0.28		332.75		
04/01/2003 16:15	1.11	0.83	0.28		333		
04/01/2003 16:30	1.10	0.83	0.27		333.25		
04/01/2003 16:45	1.09	0.83	0.26		333.5		
04/01/2003 17:00	1.07	0.83	0.24		333.75		
04/01/2003 17:15	1.07	0.83	0.24		334		
04/01/2003 17:30	1.06	0.83	0.23		334.25		
04/01/2003 17:45	1.06	0.83	0.23		334.5		
04/01/2003 18:00	1.05	0.83	0.22		334.75		
04/01/2003 18:15	1.05	0.83	0.22		335		
04/01/2003 18:30	1.04	0.83	0.21		335.25		
04/01/2003 18:45	1.03	0.83	0.20		335.5		
04/01/2003 19:00	1.03	0.83	0.20		335.75		

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
04/01/2003 19:15	1.01	0.83	0.18		336		
04/01/2003 19:30	1.01	0.83	0.18		336.25		
04/01/2003 19:45	1.00	0.83	0.17		336.5		
04/01/2003 20:00	1.00	0.83	0.17		336.75		
04/01/2003 20:15	0.99	0.83	0.16		337		
04/01/2003 20:30	0.99	0.83	0.16		337.25		
04/01/2003 20:45	0.98	0.83	0.15		337.5		
04/01/2003 21:00	0.98	0.83	0.15		337.75		
04/01/2003 21:15	0.97	0.83	0.14		338		
04/01/2003 21:30	0.97	0.83	0.14		338.25		
04/01/2003 21:45	0.96	0.83	0.13		338.5		
04/01/2003 22:00	0.96	0.83	0.13		338.75		
04/01/2003 22:15	0.96	0.83	0.13		339		
04/01/2003 22:30	0.96	0.83	0.13		339.25		
04/01/2003 22:45	0.93	0.83	0.10		339.5		
04/01/2003 23:00	0.93	0.83	0.10		339.75		
04/01/2003 23:15	0.92	0.83	0.09		340		
04/01/2003 23:30	0.92	0.83	0.09		340.25		
04/01/2003 23:45	0.91	0.83	0.08		340.5		
05/01/2003 00:00	0.91	0.83	0.08		340.75		
05/01/2003 00:15	0.90	0.83	0.07		341		
05/01/2003 00:30	0.90	0.83	0.07		341.25		
05/01/2003 00:45	0.89	0.83	0.06		341.5		
05/01/2003 01:00	0.89	0.83	0.06		341.75		
05/01/2003 01:15	0.89	0.83	0.06		342		
05/01/2003 01:30	0.88	0.83	0.05		342.25		
05/01/2003 01:45	0.87	0.83	0.04		342.5		
05/01/2003 02:00	0.87	0.83	0.04		342.75		
05/01/2003 02:15	0.86	0.83	0.03		343		
05/01/2003 02:30	0.86	0.83	0.03		343.25		
05/01/2003 02:45	0.85	0.83	0.02		343.5		
05/01/2003 03:00	0.85	0.83	0.02		343.75		
05/01/2003 03:15	0.84	0.83	0.01		344		
05/01/2003 03:30	0.84	0.83	0.01		344.25		
05/01/2003 03:45	0.82	0.82	0.00		344.5		
05/01/2003 04:00	0.81	0.81	0.00		344.75		
05/01/2003 04:15	0.81	0.81	0.00		345		
05/01/2003 04:30	0.80	0.80	0.00		345.25		
05/01/2003 04:45	0.80	0.80	0.00		345.5		
05/01/2003 05:00	0.79	0.79	0.00		345.75		
05/01/2003 05:15	0.79	0.79	0.00		346		
05/01/2003 05:30	0.78	0.78	0.00		346.25		

	Middleton			Earl Soham			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
05/01/2003 05:45	0.78	0.78	0.00		346.5		
05/01/2003 06:00	0.77	0.77	0.00		346.75		
05/01/2003 06:15	0.77	0.77	0.00		347		
05/01/2003 06:30	0.77	0.77	0.00		347.25		
05/01/2003 06:45	0.76	0.76	0.00		347.5		
05/01/2003 07:00	0.76	0.76	0.00		347.75		
05/01/2003 07:15	0.76	0.76	0.00		348		
05/01/2003 07:30	0.76	0.76	0.00		348.25		
05/01/2003 07:45	0.76	0.76	0.00		348.5		
05/01/2003 08:00	0.76	0.76	0.00		348.75		
05/01/2003 08:15	0.75	0.75	0.00		349		
05/01/2003 08:30	0.75	0.75	0.00		349.25		
05/01/2003 08:45	0.75	0.75	0.00		349.5		
05/01/2003 09:00	0.74	0.74	0.00		349.75		
05/01/2003 09:15	0.74	0.74	0.00		350		
05/01/2003 09:30	0.73	0.73	0.00		350.25		
05/01/2003 09:45	0.73	0.73	0.00		350.5		
05/01/2003 10:00	0.72	0.72	0.00		350.75		
05/01/2003 10:15	0.72	0.72	0.00		351		
05/01/2003 10:30	0.72	0.72	0.00		351.25		
05/01/2003 10:45	0.71	0.71	0.00		351.5		
05/01/2003 11:00	0.72	0.72	0.00		351.75		
05/01/2003 11:15	0.71	0.71	0.00		352		


March 2010 Event
10.00
9.00
8.00
7.00
6.00
5.00
4.00
3.00
2.00
1.00
0.00
Flow (m3/s)
1.4
1.2
1
0.8
0.6
0.4
0.2
0
Rainfall (mm)
0
50
100
150
200
250
Time (hours)
Flow
Baseflow
Rainfall - Benhall

	Middleton			Benhall	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
21/02/2010 00:00	0.79	0.69	0.10	0	0
21/02/2010 00:15	0.78	0.69	0.09	0	0.25
21/02/2010 00:30	0.78	0.69	0.09	0	0.5
21/02/2010 00:45	0.77	0.69	0.08	0	0.75
21/02/2010 01:00	0.77	0.69	0.08	0	1
21/02/2010 01:15	0.77	0.69	0.08	0	1.25
21/02/2010 01:30	0.77	0.69	0.08	0	1.5
21/02/2010 01:45	0.76	0.69	0.07	0	1.75
21/02/2010 02:00	0.76	0.69	0.07	0	2
21/02/2010 02:15	0.76	0.69	0.07	0	2.25
21/02/2010 02:30	0.76	0.69	0.07	0	2.5
21/02/2010 02:45	0.76	0.69	0.07	0	2.75
21/02/2010 03:00	0.75	0.69	0.06	0	3
21/02/2010 03:15	0.75	0.69	0.06	0	3.25
21/02/2010 03:30	0.75	0.69	0.06	0	3.5
21/02/2010 03:45	0.75	0.69	0.06	0	3.75
21/02/2010 04:00	0.74	0.69	0.05	0	4
21/02/2010 04:15	0.74	0.69	0.05	0	4.25
21/02/2010 04:30	0.74	0.69	0.05	0	4.5
21/02/2010 04:45	0.74	0.69	0.05	0	4.75
21/02/2010 05:00	0.74	0.69	0.05	0	5
21/02/2010 05:15	0.74	0.69	0.05	0	5.25
21/02/2010 05:30	0.73	0.69	0.04	0	5.5
21/02/2010 05:45	0.73	0.69	0.04	0	5.75
21/02/2010 06:00	0.72	0.69	0.03	0	6
21/02/2010 06:15	0.72	0.69	0.03	0	6.25
21/02/2010 06:30	0.72	0.69	0.03	0	6.5
21/02/2010 06:45	0.72	0.69	0.03	0	6.75
21/02/2010 07:00	0.72	0.69	0.03	0	7
21/02/2010 07:15	0.71	0.69	0.02	0	7.25
21/02/2010 07:30	0.71	0.69	0.02	0	7.5
21/02/2010 07:45	0.71	0.69	0.02	0	7.75
21/02/2010 08:00	0.71	0.69	0.02	0	8
21/02/2010 08:15	0.71	0.69	0.02	0	8.25
21/02/2010 08:30	0.70	0.69	0.01	0	8.5
21/02/2010 08:45	0.70	0.69	0.01	0	8.75
21/02/2010 09:00	0.70	0.69	0.01	0	9
21/02/2010 09:15	0.70	0.69	0.01	0	9.25
21/02/2010 09:30	0.70	0.69	0.01	0	9.5

Benhall	
Area (km^2)	50.16
Total Rain (P) mm	55
Time Interval (hour)	0.25
Percentage Runoff	58%

Thorpeness rainfall gauge data was not avaialble for this event

	Middleton			Benhall	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
21/02/2010 09:45	0.70	0.69	0.01	0.2	9.75
21/02/2010 10:00	0.70	0.69	0.01	0	10
21/02/2010 10:15	0.69	0.69	0.00	0.6	10.25
21/02/2010 10:30	0.70	0.69	0.01	0.2	10.5
21/02/2010 10:45	0.69	0.69	0.00	0.2	10.75
21/02/2010 11:00	0.69	0.69	0.00	0	11
21/02/2010 11:15	0.69	0.69	0.00	0.2	11.25
21/02/2010 11:30	0.70	0.69	0.01	0.2	11.5
21/02/2010 11:45	0.69	0.69	0.00	0.8	11.75
21/02/2010 12:00	0.70	0.69	0.01	0.8	12
21/02/2010 12:15	0.70	0.69	0.01	0.4	12.25
21/02/2010 12:30	0.70	0.69	0.01	0.4	12.5
21/02/2010 12:45	0.71	0.69	0.02	0.4	12.75
21/02/2010 13:00	0.72	0.69	0.03	0.4	13
21/02/2010 13:15	0.72	0.69	0.03	0	13.25
21/02/2010 13:30	0.74	0.69	0.05	0	13.5
21/02/2010 13:45	0.75	0.69	0.06	0	13.75
21/02/2010 14:00	0.76	0.69	0.07	0	14
21/02/2010 14:15	0.76	0.69	0.07	0	14.25
21/02/2010 14:30	0.78	0.69	0.09	0	14.5
21/02/2010 14:45	0.79	0.69	0.10	0	14.75
21/02/2010 15:00	0.80	0.69	0.11	0	15
21/02/2010 15:15	0.83	0.69	0.14	0	15.25
21/02/2010 15:30	0.85	0.69	0.16	0	15.5
21/02/2010 15:45	0.89	0.69	0.20	0	15.75
21/02/2010 16:00	0.93	0.69	0.24	0	16
21/02/2010 16:15	0.99	0.69	0.30	0	16.25
21/02/2010 16:30	1.04	0.69	0.35	0	16.5
21/02/2010 16:45	1.11	0.69	0.42	0	16.75
21/02/2010 17:00	1.18	0.69	0.49	0	17
21/02/2010 17:15	1.25	0.69	0.56	0	17.25
21/02/2010 17:30	1.31	0.69	0.62	0.2	17.5
21/02/2010 17:45	1.37	0.69	0.68	0	17.75
21/02/2010 18:00	1.44	0.69	0.75	0	18
21/02/2010 18:15	1.49	0.69	0.80	0	18.25
21/02/2010 18:30	1.54	0.69	0.85	0	18.5
21/02/2010 18:45	1.60	0.69	0.91	0	18.75
21/02/2010 19:00	1.65	0.69	0.96	0	19
21/02/2010 19:15	1.71	0.69	1.02	0	19.25

Benhall

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
21/02/2010 19:30	1.76	0.69	1.07	0	19.5	
21/02/2010 19:45	1.80	0.69	1.11	0	19.75	
21/02/2010 20:00	1.84	0.69	1.15	0	20	
21/02/2010 20:15	1.88	0.69	1.19	0	20.25	
21/02/2010 20:30	1.92	0.69	1.23	0	20.5	
21/02/2010 20:45	1.95	0.69	1.26	0	20.75	
21/02/2010 21:00	1.97	0.69	1.28	0	21	
21/02/2010 21:15	1.99	0.69	1.30	0	21.25	
21/02/2010 21:30	2.03	0.69	1.34	0	21.5	
21/02/2010 21:45	2.04	0.69	1.35	0	21.75	
21/02/2010 22:00	2.06	0.69	1.37	0	22	
21/02/2010 22:15	2.07	0.69	1.38	0	22.25	
21/02/2010 22:30	2.09	0.69	1.40	0	22.5	
21/02/2010 22:45	2.10	0.69	1.41	0	22.75	
21/02/2010 23:00	2.12	0.69	1.43	0	23	
21/02/2010 23:15	2.12	0.69	1.43	0	23.25	
21/02/2010 23:30	2.14	0.69	1.45	0	23.5	
21/02/2010 23:45	2.14	0.69	1.45	0	23.75	
22/02/2010 00:00	2.16	0.69	1.47	0	24	
22/02/2010 00:15	2.15	0.69	1.46	0	24.25	
22/02/2010 00:30	2.14	0.69	1.45	0	24.5	
22/02/2010 00:45	2.14	0.69	1.45	0	24.75	
22/02/2010 01:00	2.13	0.69	1.44	0	25	
22/02/2010 01:15	2.12	0.69	1.43	0	25.25	
22/02/2010 01:30	2.11	0.69	1.42	0	25.5	
22/02/2010 01:45	2.09	0.69	1.40	0	25.75	
22/02/2010 02:00	2.08	0.69	1.39	0	26	
22/02/2010 02:15	2.05	0.69	1.36	0	26.25	
22/02/2010 02:30	2.03	0.69	1.34	0.2	26.5	
22/02/2010 02:45	2.01	0.69	1.32	0.2	26.75	
22/02/2010 03:00	2.00	0.69	1.31	0	27	
22/02/2010 03:15	1.97	0.69	1.28	0.2	27.25	
22/02/2010 03:30	1.95	0.69	1.26	0	27.5	
22/02/2010 03:45	1.94	0.69	1.25	0.2	27.75	
22/02/2010 04:00	1.92	0.69	1.23	0.2	28	
22/02/2010 04:15	1.90	0.69	1.21	0.4	28.25	
22/02/2010 04:30	1.88	0.69	1.19	0	28.5	
22/02/2010 04:45	1.86	0.69	1.17	0.2	28.75	
22/02/2010 05:00	1.84	0.69	1.15	0.4	29	

	Middleton			Benhall	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
22/02/2010 05:15	1.82	0.69	1.13	0.2	29.25
22/02/2010 05:30	1.80	0.69	1.11	0.2	29.5
22/02/2010 05:45	1.78	0.69	1.09	0.2	29.75
22/02/2010 06:00	1.76	0.69	1.07	0.2	30
22/02/2010 06:15	1.75	0.69	1.06	0.4	30.25
22/02/2010 06:30	1.75	0.69	1.06	0.4	30.5
22/02/2010 06:45	1.72	0.69	1.03	0.2	30.75
22/02/2010 07:00	1.72	0.69	1.03	0.2	31
22/02/2010 07:15	1.71	0.69	1.02	0.4	31.25
22/02/2010 07:30	1.70	0.69	1.01	0.4	31.5
22/02/2010 07:45	1.71	0.69	1.02	0.4	31.75
22/02/2010 08:00	1.71	0.69	1.02	0.8	32
22/02/2010 08:15	1.72	0.69	1.03	0.8	32.25
22/02/2010 08:30	1.74	0.69	1.05	0.8	32.5
22/02/2010 08:45	1.76	0.69	1.07	0.6	32.75
22/02/2010 09:00	1.80	0.69	1.11	0.6	33
22/02/2010 09:15	1.85	0.69	1.16	0.4	33.25
22/02/2010 09:30	1.91	0.69	1.22	0.6	33.5
22/02/2010 09:45	1.97	0.69	1.28	0.6	33.75
22/02/2010 10:00	2.05	0.69	1.36	0.4	34
22/02/2010 10:15	2.14	0.69	1.45	0.2	34.25
22/02/2010 10:30	2.26	0.69	1.57	0	34.5
22/02/2010 10:45	2.39	0.69	1.70	0.2	34.75
22/02/2010 11:00	2.57	0.69	1.88	0	35
22/02/2010 11:15	2.81	0.69	2.12	0.2	35.25
22/02/2010 11:30	3.04	0.69	2.35	0.2	35.5
22/02/2010 11:45	3.33	0.69	2.64	0.4	35.75
22/02/2010 12:00	3.60	0.69	2.91	0.2	36
22/02/2010 12:15	3.95	0.69	3.26	0	36.25
22/02/2010 12:30	4.12	0.69	3.43	0	36.5
22/02/2010 12:45	4.36	0.69	3.67	0.2	36.75
22/02/2010 13:00	4.57	0.69	3.88	0	37
22/02/2010 13:15	4.73	0.69	4.04	0.2	37.25
22/02/2010 13:30	4.86	0.69	4.17	0	37.5
22/02/2010 13:45	5.01	0.69	4.32	0.2	37.75
22/02/2010 14:00	5.14	0.69	4.45	0	38
22/02/2010 14:15	5.26	0.69	4.57	0.2	38.25
22/02/2010 14:30	5.38	0.69	4.69	0	38.5
22/02/2010 14:45	5.47	0.69	4.78	0	38.75

Benhall

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
22/02/2010 15:00	5.55	0.69	4.86	0	39	
22/02/2010 15:15	5.62	0.69	4.93	0.2	39.25	
22/02/2010 15:30	5.69	0.69	5.00	0.4	39.5	
22/02/2010 15:45	5.76	0.69	5.07	0.2	39.75	
22/02/2010 16:00	5.83	0.69	5.14	0.2	40	
22/02/2010 16:15	5.88	0.69	5.19	0.2	40.25	
22/02/2010 16:30	5.94	0.69	5.25	0	40.5	
22/02/2010 16:45	5.97	0.69	5.28	0	40.75	
22/02/2010 17:00	6.02	0.69	5.33	0.2	41	
22/02/2010 17:15	6.06	0.69	5.37	0	41.25	
22/02/2010 17:30	6.10	0.69	5.41	0	41.5	
22/02/2010 17:45	6.12	0.69	5.43	0.2	41.75	
22/02/2010 18:00	6.17	0.69	5.48	0	42	
22/02/2010 18:15	6.24	0.69	5.55	0	42.25	
22/02/2010 18:30	6.27	0.69	5.58	0	42.5	
22/02/2010 18:45	6.32	0.69	5.63	0	42.75	
22/02/2010 19:00	6.37	0.69	5.68	0	43	
22/02/2010 19:15	6.45	0.69	5.76	0	43.25	
22/02/2010 19:30	6.51	0.69	5.82	0	43.5	
22/02/2010 19:45	6.58	0.69	5.89	0	43.75	
22/02/2010 20:00	6.63	0.69	5.94	0	44	
22/02/2010 20:15	6.67	0.69	5.98	0	44.25	
22/02/2010 20:30	6.73	0.69	6.04	0	44.5	
22/02/2010 20:45	6.79	0.69	6.10	0	44.75	
22/02/2010 21:00	6.82	0.69	6.13	0	45	
22/02/2010 21:15	6.88	0.69	6.19	0	45.25	
22/02/2010 21:30	6.94	0.69	6.25	0	45.5	
22/02/2010 21:45	7.00	0.69	6.31	0	45.75	
22/02/2010 22:00	7.06	0.69	6.37	0	46	
22/02/2010 22:15	7.09	0.69	6.40	0	46.25	
22/02/2010 22:30	7.13	0.69	6.44	0	46.5	
22/02/2010 22:45	7.18	0.69	6.49	0	46.75	
22/02/2010 23:00	7.20	0.69	6.51	0	47	
22/02/2010 23:15	7.25	0.69	6.56	0	47.25	
22/02/2010 23:30	7.28	0.69	6.59	0	47.5	
22/02/2010 23:45	7.31	0.69	6.62	0	47.75	
23/02/2010 00:00	7.31	0.69	6.62	0	48	
23/02/2010 00:15	7.35	0.69	6.66	0	48.25	
23/02/2010 00:30	7.37	0.69	6.68	0	48.5	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
23/02/2010 00:45	7.37	0.69	6.68	0	48.75	
23/02/2010 01:00	7.37	0.69	6.68	0	49	
23/02/2010 01:15	7.35	0.69	6.66	0	49.25	
23/02/2010 01:30	7.36	0.69	6.67	0	49.5	
23/02/2010 01:45	7.34	0.69	6.65	0	49.75	
23/02/2010 02:00	7.31	0.69	6.62	0	50	
23/02/2010 02:15	7.29	0.69	6.60	0	50.25	
23/02/2010 02:30	7.24	0.69	6.55	0	50.5	
23/02/2010 02:45	7.21	0.69	6.52	0	50.75	
23/02/2010 03:00	7.16	0.69	6.47	0	51	
23/02/2010 03:15	7.13	0.69	6.44	0	51.25	
23/02/2010 03:30	7.07	0.69	6.38	0	51.5	
23/02/2010 03:45	7.00	0.69	6.31	0	51.75	
23/02/2010 04:00	6.95	0.69	6.26	0	52	
23/02/2010 04:15	6.89	0.69	6.20	0	52.25	
23/02/2010 04:30	6.80	0.69	6.11	0	52.5	
23/02/2010 04:45	6.72	0.69	6.03	0	52.75	
23/02/2010 05:00	6.66	0.69	5.97	0	53	
23/02/2010 05:15	6.56	0.69	5.87	0	53.25	
23/02/2010 05:30	6.47	0.69	5.78	0	53.5	
23/02/2010 05:45	6.36	0.69	5.67	0	53.75	
23/02/2010 06:00	6.28	0.69	5.59	0	54	
23/02/2010 06:15	6.19	0.69	5.50	0	54.25	
23/02/2010 06:30	6.10	0.69	5.41	0	54.5	
23/02/2010 06:45	5.99	0.69	5.30	0	54.75	
23/02/2010 07:00	5.89	0.69	5.20	0	55	
23/02/2010 07:15	5.77	0.69	5.08	0	55.25	
23/02/2010 07:30	5.63	0.69	4.94	0	55.5	
23/02/2010 07:45	5.49	0.69	4.80	0	55.75	
23/02/2010 08:00	5.34	0.69	4.65	0	56	
23/02/2010 08:15	5.18	0.69	4.49	0	56.25	
23/02/2010 08:30	5.02	0.69	4.33	0	56.5	
23/02/2010 08:45	4.83	0.69	4.14	0	56.75	
23/02/2010 09:00	4.69	0.69	4.00	0	57	
23/02/2010 09:15	4.51	0.69	3.82	0	57.25	
23/02/2010 09:30	4.31	0.69	3.62	0	57.5	
23/02/2010 09:45	4.11	0.69	3.42	0	57.75	
23/02/2010 10:00	3.93	0.69	3.24	0	58	
23/02/2010 10:15	3.73	0.69	3.04	0	58.25	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
23/02/2010 10:30	3.52	0.69	2.83	0	58.5	
23/02/2010 10:45	3.34	0.69	2.65	0	58.75	
23/02/2010 11:00	3.13	0.69	2.44	0	59	
23/02/2010 11:15	2.95	0.69	2.26	0	59.25	
23/02/2010 11:30	2.75	0.69	2.06	0	59.5	
23/02/2010 11:45	2.59	0.69	1.90	0	59.75	
23/02/2010 12:00	2.46	0.69	1.77	0	60	
23/02/2010 12:15	2.36	0.69	1.67	0	60.25	
23/02/2010 12:30	2.27	0.69	1.58	0	60.5	
23/02/2010 12:45	2.22	0.69	1.53	0	60.75	
23/02/2010 13:00	2.15	0.69	1.46	0	61	
23/02/2010 13:15	2.10	0.69	1.41	0	61.25	
23/02/2010 13:30	2.06	0.69	1.37	0	61.5	
23/02/2010 13:45	2.03	0.69	1.34	0	61.75	
23/02/2010 14:00	1.99	0.69	1.30	0	62	
23/02/2010 14:15	1.95	0.69	1.26	0	62.25	
23/02/2010 14:30	1.93	0.69	1.24	0	62.5	
23/02/2010 14:45	1.89	0.69	1.20	0	62.75	
23/02/2010 15:00	1.87	0.69	1.18	0	63	
23/02/2010 15:15	1.84	0.69	1.15	0	63.25	
23/02/2010 15:30	1.81	0.69	1.12	0	63.5	
23/02/2010 15:45	1.79	0.69	1.10	0	63.75	
23/02/2010 16:00	1.77	0.69	1.08	0	64	
23/02/2010 16:15	1.75	0.69	1.06	0.2	64.25	
23/02/2010 16:30	1.73	0.69	1.04	0.2	64.5	
23/02/2010 16:45	1.69	0.69	1.00	0	64.75	
23/02/2010 17:00	1.68	0.69	0.99	0.2	65	
23/02/2010 17:15	1.68	0.69	0.99	0.2	65.25	
23/02/2010 17:30	1.64	0.69	0.95	0.2	65.5	
23/02/2010 17:45	1.63	0.69	0.94	0.2	65.75	
23/02/2010 18:00	1.62	0.69	0.93	0.2	66	
23/02/2010 18:15	1.60	0.69	0.91	0	66.25	
23/02/2010 18:30	1.59	0.69	0.90	0	66.5	
23/02/2010 18:45	1.57	0.69	0.88	0	66.75	
23/02/2010 19:00	1.56	0.69	0.87	0.2	67	
23/02/2010 19:15	1.55	0.69	0.86	0	67.25	
23/02/2010 19:30	1.53	0.69	0.84	0	67.5	
23/02/2010 19:45	1.53	0.69	0.84	0	67.75	
23/02/2010 20:00	1.52	0.69	0.83	0	68	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
23/02/2010 20:15	1.51	0.69	0.82	0.2	68.25	
23/02/2010 20:30	1.49	0.69	0.80	0	68.5	
23/02/2010 20:45	1.49	0.69	0.80	0	68.75	
23/02/2010 21:00	1.48	0.69	0.79	0	69	
23/02/2010 21:15	1.48	0.69	0.79	0	69.25	
23/02/2010 21:30	1.47	0.69	0.78	0.2	69.5	
23/02/2010 21:45	1.46	0.69	0.77	0	69.75	
23/02/2010 22:00	1.46	0.69	0.77	0	70	
23/02/2010 22:15	1.44	0.69	0.75	0	70.25	
23/02/2010 22:30	1.44	0.69	0.75	0	70.5	
23/02/2010 22:45	1.44	0.69	0.75	0	70.75	
23/02/2010 23:00	1.44	0.69	0.75	0	71	
23/02/2010 23:15	1.43	0.69	0.74	0	71.25	
23/02/2010 23:30	1.43	0.69	0.74	0	71.5	
23/02/2010 23:45	1.42	0.69	0.73	0	71.75	
24/02/2010 00:00	1.42	0.69	0.73	0	72	
24/02/2010 00:15	1.41	0.69	0.72	0	72.25	
24/02/2010 00:30	1.41	0.69	0.72	0	72.5	
24/02/2010 00:45	1.41	0.69	0.72	0	72.75	
24/02/2010 01:00	1.40	0.69	0.71	0.2	73	
24/02/2010 01:15	1.40	0.69	0.71	0	73.25	
24/02/2010 01:30	1.39	0.69	0.70	0	73.5	
24/02/2010 01:45	1.40	0.69	0.71	0	73.75	
24/02/2010 02:00	1.39	0.69	0.70	0	74	
24/02/2010 02:15	1.39	0.69	0.70	0	74.25	
24/02/2010 02:30	1.39	0.69	0.70	0	74.5	
24/02/2010 02:45	1.39	0.69	0.70	0	74.75	
24/02/2010 03:00	1.40	0.69	0.71	0	75	
24/02/2010 03:15	1.39	0.69	0.70	0	75.25	
24/02/2010 03:30	1.40	0.69	0.71	0	75.5	
24/02/2010 03:45	1.39	0.69	0.70	0	75.75	
24/02/2010 04:00	1.39	0.69	0.70	0	76	
24/02/2010 04:15	1.39	0.69	0.70	0.2	76.25	
24/02/2010 04:30	1.39	0.69	0.70	0	76.5	
24/02/2010 04:45	1.39	0.69	0.70	0	76.75	
24/02/2010 05:00	1.39	0.69	0.70	0	77	
24/02/2010 05:15	1.39	0.69	0.70	0	77.25	
24/02/2010 05:30	1.39	0.69	0.70	0	77.5	
24/02/2010 05:45	1.39	0.69	0.70	0	77.75	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
24/02/2010 06:00	1.39	0.69	0.70	0	78	
24/02/2010 06:15	1.39	0.69	0.70	0	78.25	
24/02/2010 06:30	1.39	0.69	0.70	0	78.5	
24/02/2010 06:45	1.39	0.69	0.70	0	78.75	
24/02/2010 07:00	1.39	0.69	0.70	0	79	
24/02/2010 07:15	1.39	0.69	0.70	0	79.25	
24/02/2010 07:30	1.39	0.69	0.70	0	79.5	
24/02/2010 07:45	1.39	0.69	0.70	0	79.75	
24/02/2010 08:00	1.39	0.69	0.70	0	80	
24/02/2010 08:15	1.39	0.69	0.70	0	80.25	
24/02/2010 08:30	1.39	0.69	0.70	0	80.5	
24/02/2010 08:45	1.39	0.69	0.70	0	80.75	
24/02/2010 09:00	1.39	0.69	0.70	0	81	
24/02/2010 09:15	1.39	0.69	0.70	0	81.25	
24/02/2010 09:30	1.39	0.69	0.70	0	81.5	
24/02/2010 09:45	1.38	0.69	0.69	0	81.75	
24/02/2010 10:00	1.39	0.69	0.70	0	82	
24/02/2010 10:15	1.38	0.69	0.69	0	82.25	
24/02/2010 10:30	1.37	0.69	0.68	0	82.5	
24/02/2010 10:45	1.37	0.69	0.68	0	82.75	
24/02/2010 11:00	1.37	0.69	0.68	0	83	
24/02/2010 11:15	1.37	0.69	0.68	0	83.25	
24/02/2010 11:30	1.36	0.69	0.67	0	83.5	
24/02/2010 11:45	1.36	0.69	0.67	0	83.75	
24/02/2010 12:00	1.36	0.69	0.67	0	84	
24/02/2010 12:15	1.36	0.69	0.67	0	84.25	
24/02/2010 12:30	1.35	0.69	0.66	0	84.5	
24/02/2010 12:45	1.35	0.69	0.66	0.2	84.75	
24/02/2010 13:00	1.35	0.69	0.66	0	85	
24/02/2010 13:15	1.34	0.69	0.65	0	85.25	
24/02/2010 13:30	1.33	0.69	0.64	0	85.5	
24/02/2010 13:45	1.33	0.69	0.64	0	85.75	
24/02/2010 14:00	1.33	0.69	0.64	0	86	
24/02/2010 14:15	1.32	0.69	0.63	0	86.25	
24/02/2010 14:30	1.32	0.69	0.63	0	86.5	
24/02/2010 14:45	1.32	0.69	0.63	0	86.75	
24/02/2010 15:00	1.32	0.69	0.63	0	87	
24/02/2010 15:15	1.32	0.69	0.63	0	87.25	
24/02/2010 15:30	1.32	0.69	0.63	0	87.5	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
24/02/2010 15:45	1.31	0.69	0.62	0	87.75	
24/02/2010 16:00	1.30	0.69	0.61	0	88	
24/02/2010 16:15	1.30	0.69	0.61	0	88.25	
24/02/2010 16:30	1.29	0.69	0.60	0	88.5	
24/02/2010 16:45	1.29	0.69	0.60	0	88.75	
24/02/2010 17:00	1.28	0.69	0.59	0	89	
24/02/2010 17:15	1.28	0.69	0.59	0	89.25	
24/02/2010 17:30	1.28	0.69	0.59	0	89.5	
24/02/2010 17:45	1.28	0.69	0.59	0	89.75	
24/02/2010 18:00	1.27	0.69	0.58	0	90	
24/02/2010 18:15	1.27	0.69	0.58	0	90.25	
24/02/2010 18:30	1.26	0.69	0.57	0	90.5	
24/02/2010 18:45	1.26	0.69	0.57	0	90.75	
24/02/2010 19:00	1.26	0.69	0.57	0	91	
24/02/2010 19:15	1.25	0.69	0.56	0	91.25	
24/02/2010 19:30	1.25	0.69	0.56	0	91.5	
24/02/2010 19:45	1.25	0.69	0.56	0	91.75	
24/02/2010 20:00	1.25	0.69	0.56	0	92	
24/02/2010 20:15	1.24	0.69	0.55	0	92.25	
24/02/2010 20:30	1.24	0.69	0.55	0	92.5	
24/02/2010 20:45	1.24	0.69	0.55	0	92.75	
24/02/2010 21:00	1.23	0.69	0.54	0	93	
24/02/2010 21:15	1.23	0.69	0.54	0	93.25	
24/02/2010 21:30	1.22	0.69	0.53	0	93.5	
24/02/2010 21:45	1.22	0.69	0.53	0.2	93.75	
24/02/2010 22:00	1.21	0.69	0.52	0	94	
24/02/2010 22:15	1.22	0.69	0.53	0	94.25	
24/02/2010 22:30	1.20	0.69	0.51	0	94.5	
24/02/2010 22:45	1.20	0.69	0.51	0	94.75	
24/02/2010 23:00	1.19	0.69	0.50	0	95	
24/02/2010 23:15	1.19	0.69	0.50	0.2	95.25	
24/02/2010 23:30	1.19	0.69	0.50	0	95.5	
24/02/2010 23:45	1.19	0.69	0.50	0.2	95.75	
25/02/2010 00:00	1.19	0.69	0.50	0	96	
25/02/2010 00:15	1.18	0.69	0.49	0	96.25	
25/02/2010 00:30	1.17	0.69	0.48	0	96.5	
25/02/2010 00:45	1.17	0.69	0.48	0	96.75	
25/02/2010 01:00	1.16	0.69	0.47	0	97	
25/02/2010 01:15	1.16	0.69	0.47	0	97.25	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
25/02/2010 01:30	1.16	0.69	0.47	0	97.5	
25/02/2010 01:45	1.16	0.69	0.47	0	97.75	
25/02/2010 02:00	1.16	0.69	0.47	0	98	
25/02/2010 02:15	1.15	0.69	0.46	0	98.25	
25/02/2010 02:30	1.15	0.69	0.46	0.2	98.5	
25/02/2010 02:45	1.14	0.69	0.45	0	98.75	
25/02/2010 03:00	1.14	0.69	0.45	0	99	
25/02/2010 03:15	1.14	0.69	0.45	0	99.25	
25/02/2010 03:30	1.13	0.69	0.44	0	99.5	
25/02/2010 03:45	1.13	0.69	0.44	0	99.75	
25/02/2010 04:00	1.13	0.69	0.44	0	100	
25/02/2010 04:15	1.12	0.69	0.43	0	100.25	
25/02/2010 04:30	1.12	0.69	0.43	0	100.5	
25/02/2010 04:45	1.11	0.69	0.42	0	100.75	
25/02/2010 05:00	1.11	0.69	0.42	0	101	
25/02/2010 05:15	1.11	0.69	0.42	0	101.25	
25/02/2010 05:30	1.11	0.69	0.42	0	101.5	
25/02/2010 05:45	1.10	0.69	0.41	0	101.75	
25/02/2010 06:00	1.10	0.69	0.41	0	102	
25/02/2010 06:15	1.10	0.69	0.41	0	102.25	
25/02/2010 06:30	1.09	0.69	0.40	0	102.5	
25/02/2010 06:45	1.09	0.69	0.40	0	102.75	
25/02/2010 07:00	1.08	0.69	0.39	0	103	
25/02/2010 07:15	1.08	0.69	0.39	0	103.25	
25/02/2010 07:30	1.08	0.69	0.39	0	103.5	
25/02/2010 07:45	1.07	0.69	0.38	0	103.75	
25/02/2010 08:00	1.07	0.69	0.38	0	104	
25/02/2010 08:15	1.07	0.69	0.38	0	104.25	
25/02/2010 08:30	1.06	0.69	0.37	0	104.5	
25/02/2010 08:45	1.06	0.69	0.37	0	104.75	
25/02/2010 09:00	1.06	0.69	0.37	0	105	
25/02/2010 09:15	1.05	0.69	0.36	0	105.25	
25/02/2010 09:30	1.04	0.69	0.35	0	105.5	
25/02/2010 09:45	1.04	0.69	0.35	0	105.75	
25/02/2010 10:00	1.03	0.69	0.34	0	106	
25/02/2010 10:15	1.03	0.69	0.34	0	106.25	
25/02/2010 10:30	1.03	0.69	0.34	0	106.5	
25/02/2010 10:45	1.03	0.69	0.34	0	106.75	
25/02/2010 11:00	1.01	0.69	0.32	0	107	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
25/02/2010 11:15	1.02	0.69	0.33	0	107.25	
25/02/2010 11:30	1.01	0.69	0.32	0	107.5	
25/02/2010 11:45	1.01	0.69	0.32	0	107.75	
25/02/2010 12:00	1.00	0.69	0.31	0	108	
25/02/2010 12:15	1.00	0.69	0.31	0	108.25	
25/02/2010 12:30	1.00	0.69	0.31	0	108.5	
25/02/2010 12:45	0.99	0.69	0.30	0	108.75	
25/02/2010 13:00	0.99	0.69	0.30	0	109	
25/02/2010 13:15	0.99	0.69	0.30	0	109.25	
25/02/2010 13:30	0.98	0.69	0.29	0	109.5	
25/02/2010 13:45	0.98	0.69	0.29	0	109.75	
25/02/2010 14:00	0.98	0.69	0.29	0	110	
25/02/2010 14:15	0.97	0.69	0.28	0	110.25	
25/02/2010 14:30	0.97	0.69	0.28	0	110.5	
25/02/2010 14:45	0.97	0.69	0.28	0	110.75	
25/02/2010 15:00	0.97	0.69	0.28	0	111	
25/02/2010 15:15	0.96	0.69	0.27	0	111.25	
25/02/2010 15:30	0.96	0.69	0.27	0	111.5	
25/02/2010 15:45	0.96	0.69	0.27	0	111.75	
25/02/2010 16:00	0.95	0.69	0.26	0	112	
25/02/2010 16:15	0.95	0.69	0.26	0	112.25	
25/02/2010 16:30	0.95	0.69	0.26	0	112.5	
25/02/2010 16:45	0.95	0.69	0.26	0	112.75	
25/02/2010 17:00	0.94	0.69	0.25	0.4	113	
25/02/2010 17:15	0.94	0.69	0.25	0.2	113.25	
25/02/2010 17:30	0.94	0.69	0.25	0.2	113.5	
25/02/2010 17:45	0.94	0.69	0.25	0.4	113.75	
25/02/2010 18:00	0.94	0.69	0.25	0.4	114	
25/02/2010 18:15	0.94	0.69	0.25	0.2	114.25	
25/02/2010 18:30	0.94	0.69	0.25	0.2	114.5	
25/02/2010 18:45	0.94	0.69	0.25	0.2	114.75	
25/02/2010 19:00	0.95	0.69	0.26	0.4	115	
25/02/2010 19:15	0.95	0.69	0.26	0.6	115.25	
25/02/2010 19:30	0.95	0.69	0.26	0.8	115.5	
25/02/2010 19:45	0.96	0.69	0.27	0	115.75	
25/02/2010 20:00	0.97	0.69	0.28	0.2	116	
25/02/2010 20:15	0.97	0.69	0.28	0.2	116.25	
25/02/2010 20:30	0.98	0.69	0.29	1.2	116.5	
25/02/2010 20:45	0.99	0.69	0.30	1.2	116.75	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
25/02/2010 21:00	1.01	0.69	0.32	0.4	117	
25/02/2010 21:15	1.02	0.69	0.33	0.6	117.25	
25/02/2010 21:30	1.05	0.69	0.36	0.6	117.5	
25/02/2010 21:45	1.08	0.69	0.39	0.4	117.75	
25/02/2010 22:00	1.11	0.69	0.42	0	118	
25/02/2010 22:15	1.16	0.69	0.47	0	118.25	
25/02/2010 22:30	1.22	0.69	0.53	0.2	118.5	
25/02/2010 22:45	1.29	0.69	0.60	0.2	118.75	
25/02/2010 23:00	1.38	0.69	0.69	0	119	
25/02/2010 23:15	1.48	0.69	0.79	0	119.25	
25/02/2010 23:30	1.57	0.69	0.88	0	119.5	
25/02/2010 23:45	1.68	0.69	0.99	0	119.75	
26/02/2010 00:00	1.79	0.69	1.10	0	120	
26/02/2010 00:15	1.88	0.69	1.19	0	120.25	
26/02/2010 00:30	1.99	0.69	1.30	0	120.5	
26/02/2010 00:45	2.07	0.69	1.38	0	120.75	
26/02/2010 01:00	2.16	0.69	1.47	0	121	
26/02/2010 01:15	2.23	0.69	1.54	0	121.25	
26/02/2010 01:30	2.31	0.69	1.62	0	121.5	
26/02/2010 01:45	2.39	0.69	1.70	0	121.75	
26/02/2010 02:00	2.47	0.69	1.78	0	122	
26/02/2010 02:15	2.58	0.69	1.89	0	122.25	
26/02/2010 02:30	2.68	0.69	1.99	0	122.5	
26/02/2010 02:45	2.80	0.69	2.11	0	122.75	
26/02/2010 03:00	2.92	0.69	2.23	0	123	
26/02/2010 03:15	3.05	0.69	2.36	0	123.25	
26/02/2010 03:30	3.17	0.69	2.48	0	123.5	
26/02/2010 03:45	3.28	0.69	2.59	0	123.75	
26/02/2010 04:00	3.39	0.69	2.70	0	124	
26/02/2010 04:15	3.48	0.69	2.79	0	124.25	
26/02/2010 04:30	3.55	0.69	2.86	0	124.5	
26/02/2010 04:45	3.64	0.69	2.95	0	124.75	
26/02/2010 05:00	3.70	0.69	3.01	0	125	
26/02/2010 05:15	3.76	0.69	3.07	0	125.25	
26/02/2010 05:30	3.81	0.69	3.12	0	125.5	
26/02/2010 05:45	3.87	0.69	3.18	0	125.75	
26/02/2010 06:00	3.93	0.69	3.24	0	126	
26/02/2010 06:15	3.99	0.69	3.30	0	126.25	
26/02/2010 06:30	4.06	0.69	3.37	0	126.5	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
26/02/2010 06:45	4.11	0.69	3.42	0	126.75	
26/02/2010 07:00	4.19	0.69	3.50	0	127	
26/02/2010 07:15	4.24	0.69	3.55	0	127.25	
26/02/2010 07:30	4.29	0.69	3.60	0	127.5	
26/02/2010 07:45	4.35	0.69	3.66	0	127.75	
26/02/2010 08:00	4.38	0.69	3.69	0	128	
26/02/2010 08:15	4.43	0.69	3.74	0	128.25	
26/02/2010 08:30	4.47	0.69	3.78	0	128.5	
26/02/2010 08:45	4.49	0.69	3.80	0.2	128.75	
26/02/2010 09:00	4.51	0.69	3.82	0	129	
26/02/2010 09:15	4.52	0.69	3.83	0	129.25	
26/02/2010 09:30	4.51	0.69	3.82	0.2	129.5	
26/02/2010 09:45	4.49	0.69	3.80	0	129.75	
26/02/2010 10:00	4.46	0.69	3.77	0	130	
26/02/2010 10:15	4.42	0.69	3.73	0	130.25	
26/02/2010 10:30	4.37	0.69	3.68	0	130.5	
26/02/2010 10:45	4.31	0.69	3.62	0	130.75	
26/02/2010 11:00	4.24	0.69	3.55	0	131	
26/02/2010 11:15	4.15	0.69	3.46	0	131.25	
26/02/2010 11:30	4.06	0.69	3.37	0	131.5	
26/02/2010 11:45	3.96	0.69	3.27	0	131.75	
26/02/2010 12:00	3.85	0.69	3.16	0	132	
26/02/2010 12:15	3.73	0.69	3.04	0	132.25	
26/02/2010 12:30	3.59	0.69	2.90	0	132.5	
26/02/2010 12:45	3.48	0.69	2.79	0	132.75	
26/02/2010 13:00	3.34	0.69	2.65	0	133	
26/02/2010 13:15	3.18	0.69	2.49	0	133.25	
26/02/2010 13:30	3.03	0.69	2.34	0	133.5	
26/02/2010 13:45	2.88	0.69	2.19	0	133.75	
26/02/2010 14:00	2.74	0.69	2.05	0	134	
26/02/2010 14:15	2.61	0.69	1.92	0	134.25	
26/02/2010 14:30	2.50	0.69	1.81	0	134.5	
26/02/2010 14:45	2.41	0.69	1.72	0	134.75	
26/02/2010 15:00	2.33	0.69	1.64	0	135	
26/02/2010 15:15	2.27	0.69	1.58	0	135.25	
26/02/2010 15:30	2.23	0.69	1.54	0	135.5	
26/02/2010 15:45	2.19	0.69	1.50	0	135.75	
26/02/2010 16:00	2.13	0.69	1.44	0	136	
26/02/2010 16:15	2.10	0.69	1.41	0	136.25	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
26/02/2010 16:30	2.07	0.69	1.38	0	136.5	
26/02/2010 16:45	2.03	0.69	1.34	0	136.75	
26/02/2010 17:00	2.01	0.69	1.32	0	137	
26/02/2010 17:15	1.97	0.69	1.28	0	137.25	
26/02/2010 17:30	1.95	0.69	1.26	0	137.5	
26/02/2010 17:45	1.92	0.69	1.23	0	137.75	
26/02/2010 18:00	1.90	0.69	1.21	0	138	
26/02/2010 18:15	1.87	0.69	1.18	0	138.25	
26/02/2010 18:30	1.85	0.69	1.16	0	138.5	
26/02/2010 18:45	1.81	0.69	1.12	0	138.75	
26/02/2010 19:00	1.79	0.69	1.10	0	139	
26/02/2010 19:15	1.78	0.69	1.09	0	139.25	
26/02/2010 19:30	1.75	0.69	1.06	0	139.5	
26/02/2010 19:45	1.73	0.69	1.04	0	139.75	
26/02/2010 20:00	1.71	0.69	1.02	0	140	
26/02/2010 20:15	1.68	0.69	0.99	0	140.25	
26/02/2010 20:30	1.67	0.69	0.98	0	140.5	
26/02/2010 20:45	1.65	0.69	0.96	0	140.75	
26/02/2010 21:00	1.63	0.69	0.94	0	141	
26/02/2010 21:15	1.61	0.69	0.92	0	141.25	
26/02/2010 21:30	1.58	0.69	0.89	0	141.5	
26/02/2010 21:45	1.57	0.69	0.88	0	141.75	
26/02/2010 22:00	1.55	0.69	0.86	0	142	
26/02/2010 22:15	1.53	0.69	0.84	0	142.25	
26/02/2010 22:30	1.52	0.69	0.83	0	142.5	
26/02/2010 22:45	1.51	0.69	0.82	0	142.75	
26/02/2010 23:00	1.49	0.69	0.80	0	143	
26/02/2010 23:15	1.48	0.69	0.79	0	143.25	
26/02/2010 23:30	1.46	0.69	0.77	0	143.5	
26/02/2010 23:45	1.45	0.69	0.76	0	143.75	
27/02/2010 00:00	1.44	0.69	0.75	0	144	
27/02/2010 00:15	1.42	0.69	0.73	0	144.25	
27/02/2010 00:30	1.40	0.69	0.71	0	144.5	
27/02/2010 00:45	1.39	0.69	0.70	0	144.75	
27/02/2010 01:00	1.38	0.69	0.69	0	145	
27/02/2010 01:15	1.37	0.69	0.68	0	145.25	
27/02/2010 01:30	1.36	0.69	0.67	0	145.5	
27/02/2010 01:45	1.35	0.69	0.66	0	145.75	
27/02/2010 02:00	1.34	0.69	0.65	0	146	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
27/02/2010 02:15	1.32	0.69	0.63	0	146.25	
27/02/2010 02:30	1.32	0.69	0.63	0	146.5	
27/02/2010 02:45	1.30	0.69	0.61	0	146.75	
27/02/2010 03:00	1.29	0.69	0.60	0	147	
27/02/2010 03:15	1.28	0.69	0.59	0	147.25	
27/02/2010 03:30	1.27	0.69	0.58	0	147.5	
27/02/2010 03:45	1.26	0.69	0.57	0	147.75	
27/02/2010 04:00	1.25	0.69	0.56	0	148	
27/02/2010 04:15	1.25	0.69	0.56	0	148.25	
27/02/2010 04:30	1.24	0.69	0.55	0	148.5	
27/02/2010 04:45	1.22	0.69	0.53	0.2	148.75	
27/02/2010 05:00	1.22	0.69	0.53	0	149	
27/02/2010 05:15	1.21	0.69	0.52	0	149.25	
27/02/2010 05:30	1.20	0.69	0.51	0	149.5	
27/02/2010 05:45	1.19	0.69	0.50	0	149.75	
27/02/2010 06:00	1.18	0.69	0.49	0.4	150	
27/02/2010 06:15	1.18	0.69	0.49	0.2	150.25	
27/02/2010 06:30	1.17	0.69	0.48	0.6	150.5	
27/02/2010 06:45	1.16	0.69	0.47	0.2	150.75	
27/02/2010 07:00	1.16	0.69	0.47	0	151	
27/02/2010 07:15	1.15	0.69	0.46	0.2	151.25	
27/02/2010 07:30	1.15	0.69	0.46	0.4	151.5	
27/02/2010 07:45	1.15	0.69	0.46	0.2	151.75	
27/02/2010 08:00	1.14	0.69	0.45	0.2	152	
27/02/2010 08:15	1.14	0.69	0.45	0	152.25	
27/02/2010 08:30	1.13	0.69	0.44	0	152.5	
27/02/2010 08:45	1.13	0.69	0.44	0.2	152.75	
27/02/2010 09:00	1.13	0.69	0.44	0	153	
27/02/2010 09:15	1.12	0.69	0.43	0	153.25	
27/02/2010 09:30	1.12	0.69	0.43	0	153.5	
27/02/2010 09:45	1.12	0.69	0.43	0	153.75	
27/02/2010 10:00	1.12	0.69	0.43	0	154	
27/02/2010 10:15	1.11	0.69	0.42	0	154.25	
27/02/2010 10:30	1.11	0.69	0.42	0	154.5	
27/02/2010 10:45	1.11	0.69	0.42	0	154.75	
27/02/2010 11:00	1.11	0.69	0.42	0	155	
27/02/2010 11:15	1.11	0.69	0.42	0	155.25	
27/02/2010 11:30	1.11	0.69	0.42	0	155.5	
27/02/2010 11:45	1.10	0.69	0.41	0	155.75	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
27/02/2010 12:00	1.10	0.69	0.41	0	156	
27/02/2010 12:15	1.10	0.69	0.41	0	156.25	
27/02/2010 12:30	1.09	0.69	0.40	0	156.5	
27/02/2010 12:45	1.09	0.69	0.40	0	156.75	
27/02/2010 13:00	1.09	0.69	0.40	0	157	
27/02/2010 13:15	1.10	0.69	0.41	0	157.25	
27/02/2010 13:30	1.09	0.69	0.40	0	157.5	
27/02/2010 13:45	1.09	0.69	0.40	0	157.75	
27/02/2010 14:00	1.09	0.69	0.40	0	158	
27/02/2010 14:15	1.09	0.69	0.40	0	158.25	
27/02/2010 14:30	1.09	0.69	0.40	0	158.5	
27/02/2010 14:45	1.09	0.69	0.40	0	158.75	
27/02/2010 15:00	1.09	0.69	0.40	0	159	
27/02/2010 15:15	1.09	0.69	0.40	0	159.25	
27/02/2010 15:30	1.09	0.69	0.40	0	159.5	
27/02/2010 15:45	1.09	0.69	0.40	0	159.75	
27/02/2010 16:00	1.08	0.69	0.39	0	160	
27/02/2010 16:15	1.08	0.69	0.39	0	160.25	
27/02/2010 16:30	1.08	0.69	0.39	0	160.5	
27/02/2010 16:45	1.08	0.69	0.39	0	160.75	
27/02/2010 17:00	1.09	0.69	0.40	0	161	
27/02/2010 17:15	1.08	0.69	0.39	0	161.25	
27/02/2010 17:30	1.08	0.69	0.39	0	161.5	
27/02/2010 17:45	1.08	0.69	0.39	0	161.75	
27/02/2010 18:00	1.08	0.69	0.39	0	162	
27/02/2010 18:15	1.08	0.69	0.39	0	162.25	
27/02/2010 18:30	1.08	0.69	0.39	0	162.5	
27/02/2010 18:45	1.08	0.69	0.39	0	162.75	
27/02/2010 19:00	1.08	0.69	0.39	0	163	
27/02/2010 19:15	1.08	0.69	0.39	0	163.25	
27/02/2010 19:30	1.08	0.69	0.39	0	163.5	
27/02/2010 19:45	1.08	0.69	0.39	0	163.75	
27/02/2010 20:00	1.08	0.69	0.39	0	164	
27/02/2010 20:15	1.08	0.69	0.39	0	164.25	
27/02/2010 20:30	1.08	0.69	0.39	0	164.5	
27/02/2010 20:45	1.08	0.69	0.39	0	164.75	
27/02/2010 21:00	1.07	0.69	0.38	0	165	
27/02/2010 21:15	1.07	0.69	0.38	0	165.25	
27/02/2010 21:30	1.07	0.69	0.38	0	165.5	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
27/02/2010 21:45	1.07	0.69	0.38	0	165.75	
27/02/2010 22:00	1.06	0.69	0.37	0	166	
27/02/2010 22:15	1.06	0.69	0.37	0	166.25	
27/02/2010 22:30	1.06	0.69	0.37	0	166.5	
27/02/2010 22:45	1.06	0.69	0.37	0	166.75	
27/02/2010 23:00	1.06	0.69	0.37	0	167	
27/02/2010 23:15	1.06	0.69	0.37	0	167.25	
27/02/2010 23:30	1.06	0.69	0.37	0	167.5	
27/02/2010 23:45	1.06	0.69	0.37	0	167.75	
28/02/2010 00:00	1.06	0.69	0.37	0	168	
28/02/2010 00:15	1.05	0.69	0.36	0	168.25	
28/02/2010 00:30	1.05	0.69	0.36	0	168.5	
28/02/2010 00:45	1.05	0.69	0.36	0	168.75	
28/02/2010 01:00	1.04	0.69	0.35	0	169	
28/02/2010 01:15	1.04	0.69	0.35	0	169.25	
28/02/2010 01:30	1.04	0.69	0.35	0	169.5	
28/02/2010 01:45	1.03	0.69	0.34	0	169.75	
28/02/2010 02:00	1.03	0.69	0.34	0	170	
28/02/2010 02:15	1.03	0.69	0.34	0	170.25	
28/02/2010 02:30	1.03	0.69	0.34	0	170.5	
28/02/2010 02:45	1.03	0.69	0.34	0	170.75	
28/02/2010 03:00	1.03	0.69	0.34	0	171	
28/02/2010 03:15	1.03	0.69	0.34	0	171.25	
28/02/2010 03:30	1.02	0.69	0.33	0	171.5	
28/02/2010 03:45	1.02	0.69	0.33	0	171.75	
28/02/2010 04:00	1.02	0.69	0.33	0.2	172	
28/02/2010 04:15	1.01	0.69	0.32	0	172.25	
28/02/2010 04:30	1.01	0.69	0.32	0	172.5	
28/02/2010 04:45	1.01	0.69	0.32	0.2	172.75	
28/02/2010 05:00	1.01	0.69	0.32	0.2	173	
28/02/2010 05:15	1.01	0.69	0.32	0.2	173.25	
28/02/2010 05:30	1.01	0.69	0.32	0.2	173.5	
28/02/2010 05:45	1.00	0.69	0.31	0.6	173.75	
28/02/2010 06:00	1.01	0.69	0.32	0.4	174	
28/02/2010 06:15	1.01	0.69	0.32	0.6	174.25	
28/02/2010 06:30	1.01	0.69	0.32	0.2	174.5	
28/02/2010 06:45	1.01	0.69	0.32	0.2	174.75	
28/02/2010 07:00	1.01	0.69	0.32	0.4	175	
28/02/2010 07:15	1.01	0.69	0.32	0.4	175.25	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
28/02/2010 07:30	1.01	0.69	0.32	0.2	175.5	
28/02/2010 07:45	1.03	0.69	0.34	0.8	175.75	
28/02/2010 08:00	1.03	0.69	0.34	1	176	
28/02/2010 08:15	1.04	0.69	0.35	0.4	176.25	
28/02/2010 08:30	1.06	0.69	0.37	0.6	176.5	
28/02/2010 08:45	1.08	0.69	0.39	0.6	176.75	
28/02/2010 09:00	1.09	0.69	0.40	0.6	177	
28/02/2010 09:15	1.12	0.69	0.43	0.6	177.25	
28/02/2010 09:30	1.15	0.69	0.46	1	177.5	
28/02/2010 09:45	1.19	0.69	0.50	0.8	177.75	
28/02/2010 10:00	1.26	0.69	0.57	0.6	178	
28/02/2010 10:15	1.36	0.69	0.67	0.6	178.25	
28/02/2010 10:30	1.42	0.69	0.73	0.8	178.5	
28/02/2010 10:45	1.53	0.69	0.84	0.6	178.75	
28/02/2010 11:00	1.65	0.69	0.96	0.4	179	
28/02/2010 11:15	1.79	0.69	1.10	0.4	179.25	
28/02/2010 11:30	1.93	0.69	1.24	0.4	179.5	
28/02/2010 11:45	2.09	0.69	1.40	0.4	179.75	
28/02/2010 12:00	2.25	0.69	1.56	0.4	180	
28/02/2010 12:15	2.44	0.69	1.75	0.2	180.25	
28/02/2010 12:30	2.69	0.69	2.00	0.4	180.5	
28/02/2010 12:45	3.03	0.69	2.34	0.6	180.75	
28/02/2010 13:00	3.42	0.69	2.73	0.6	181	
28/02/2010 13:15	3.68	0.69	2.99	0.4	181.25	
28/02/2010 13:30	4.16	0.69	3.47	0.4	181.5	
28/02/2010 13:45	4.51	0.69	3.82	0	181.75	
28/02/2010 14:00	4.75	0.69	4.06	0.2	182	
28/02/2010 14:15	4.97	0.69	4.28	0	182.25	
28/02/2010 14:30	5.19	0.69	4.50	0	182.5	
28/02/2010 14:45	5.40	0.69	4.71	0	182.75	
28/02/2010 15:00	5.57	0.69	4.88	0.2	183	
28/02/2010 15:15	5.72	0.69	5.03	0	183.25	
28/02/2010 15:30	5.87	0.69	5.18	0.2	183.5	
28/02/2010 15:45	6.00	0.69	5.31	0	183.75	
28/02/2010 16:00	6.10	0.69	5.41	0.2	184	
28/02/2010 16:15	6.18	0.69	5.49	0.2	184.25	
28/02/2010 16:30	6.25	0.69	5.56	0	184.5	
28/02/2010 16:45	6.33	0.69	5.64	0	184.75	
28/02/2010 17:00	6.40	0.69	5.71	0.2	185	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
28/02/2010 17:15	6.45	0.69	5.76	0.2	185.25	
28/02/2010 17:30	6.51	0.69	5.82	0	185.5	
28/02/2010 17:45	6.58	0.69	5.89	0.2	185.75	
28/02/2010 18:00	6.66	0.69	5.97	0	186	
28/02/2010 18:15	6.76	0.69	6.07	0	186.25	
28/02/2010 18:30	6.86	0.69	6.17	0	186.5	
28/02/2010 18:45	6.94	0.69	6.25	0	186.75	
28/02/2010 19:00	7.04	0.69	6.35	0	187	
28/02/2010 19:15	7.14	0.69	6.45	0	187.25	
28/02/2010 19:30	7.23	0.69	6.54	0	187.5	
28/02/2010 19:45	7.35	0.69	6.66	0	187.75	
28/02/2010 20:00	7.44	0.69	6.75	0	188	
28/02/2010 20:15	7.55	0.69	6.86	0	188.25	
28/02/2010 20:30	7.65	0.69	6.96	0	188.5	
28/02/2010 20:45	7.75	0.69	7.06	0	188.75	
28/02/2010 21:00	7.83	0.69	7.14	0	189	
28/02/2010 21:15	7.97	0.69	7.28	0.2	189.25	
28/02/2010 21:30	8.02	0.69	7.33	0	189.5	
28/02/2010 21:45	8.15	0.69	7.46	0	189.75	
28/02/2010 22:00	8.24	0.69	7.55	0	190	
28/02/2010 22:15	8.34	0.69	7.65	0	190.25	
28/02/2010 22:30	8.40	0.69	7.71	0	190.5	
28/02/2010 22:45	8.46	0.69	7.77	0.2	190.75	
28/02/2010 23:00	8.54	0.69	7.85	0	191	
28/02/2010 23:15	8.62	0.69	7.93	0	191.25	
28/02/2010 23:30	8.65	0.69	7.96	0	191.5	
28/02/2010 23:45	8.68	0.69	7.99	0	191.75	
01/03/2010 00:00	8.75	0.69	8.06	0	192	
01/03/2010 00:15	8.80	0.69	8.11	0	192.25	
01/03/2010 00:30	8.80	0.69	8.11	0	192.5	
01/03/2010 00:45	8.83	0.69	8.14	0	192.75	
01/03/2010 01:00	8.87	0.69	8.18	0	193	
01/03/2010 01:15	8.88	0.69	8.19	0	193.25	
01/03/2010 01:30	8.90	0.69	8.21	0	193.5	
01/03/2010 01:45	8.95	0.69	8.26	0	193.75	
01/03/2010 02:00	8.97	0.69	8.28	0	194	
01/03/2010 02:15	8.99	0.69	8.30	0	194.25	
01/03/2010 02:30	9.01	0.69	8.32	0	194.5	
01/03/2010 02:45	9.04	0.69	8.35	0	194.75	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
01/03/2010 03:00	9.02	0.69	8.33	0	195	
01/03/2010 03:15	9.04	0.69	8.35	0	195.25	
01/03/2010 03:30	9.04	0.69	8.35	0	195.5	
01/03/2010 03:45	9.02	0.69	8.33	0	195.75	
01/03/2010 04:00	9.02	0.69	8.33	0	196	
01/03/2010 04:15	9.01	0.69	8.32	0	196.25	
01/03/2010 04:30	8.95	0.69	8.26	0	196.5	
01/03/2010 04:45	8.94	0.69	8.25	0	196.75	
01/03/2010 05:00	8.87	0.69	8.18	0	197	
01/03/2010 05:15	8.82	0.69	8.13	0	197.25	
01/03/2010 05:30	8.75	0.69	8.06	0	197.5	
01/03/2010 05:45	8.68	0.69	7.99	0	197.75	
01/03/2010 06:00	8.60	0.69	7.91	0	198	
01/03/2010 06:15	8.51	0.69	7.82	0	198.25	
01/03/2010 06:30	8.43	0.69	7.74	0	198.5	
01/03/2010 06:45	8.33	0.69	7.64	0	198.75	
01/03/2010 07:00	8.19	0.69	7.50	0	199	
01/03/2010 07:15	8.06	0.69	7.37	0	199.25	
01/03/2010 07:30	7.94	0.69	7.25	0	199.5	
01/03/2010 07:45	7.82	0.69	7.13	0	199.75	
01/03/2010 08:00	7.66	0.69	6.97	0	200	
01/03/2010 08:15	7.51	0.69	6.82		200.25	
01/03/2010 08:30	7.35	0.69	6.66		200.5	
01/03/2010 08:45	7.22	0.69	6.53		200.75	
01/03/2010 09:00	7.07	0.69	6.38		201	
01/03/2010 09:15	6.93	0.69	6.24		201.25	
01/03/2010 09:30	6.78	0.69	6.09		201.5	
01/03/2010 09:45	6.62	0.69	5.93		201.75	
01/03/2010 10:00	6.47	0.69	5.78		202	
01/03/2010 10:15	6.32	0.69	5.63		202.25	
01/03/2010 10:30	6.20	0.69	5.51		202.5	
01/03/2010 10:45	6.04	0.69	5.35		202.75	
01/03/2010 11:00	5.87	0.69	5.18		203	
01/03/2010 11:15	5.72	0.69	5.03		203.25	
01/03/2010 11:30	5.55	0.69	4.86		203.5	
01/03/2010 11:45	5.38	0.69	4.69		203.75	
01/03/2010 12:00	5.19	0.69	4.50		204	
01/03/2010 12:15	5.00	0.69	4.31		204.25	
01/03/2010 12:30	4.77	0.69	4.08		204.5	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
01/03/2010 12:45	4.67	0.69	3.98		204.75	
01/03/2010 13:00	4.49	0.69	3.80		205	
01/03/2010 13:15	4.29	0.69	3.60		205.25	
01/03/2010 13:30	4.10	0.69	3.41		205.5	
01/03/2010 13:45	3.91	0.69	3.22		205.75	
01/03/2010 14:00	3.71	0.69	3.02		206	
01/03/2010 14:15	3.51	0.69	2.82		206.25	
01/03/2010 14:30	3.33	0.69	2.64		206.5	
01/03/2010 14:45	3.15	0.69	2.46		206.75	
01/03/2010 15:00	2.95	0.69	2.26		207	
01/03/2010 15:15	2.79	0.69	2.10		207.25	
01/03/2010 15:30	2.65	0.69	1.96		207.5	
01/03/2010 15:45	2.52	0.69	1.83		207.75	
01/03/2010 16:00	2.42	0.69	1.73		208	
01/03/2010 16:15	2.33	0.69	1.64		208.25	
01/03/2010 16:30	2.27	0.69	1.58		208.5	
01/03/2010 16:45	2.21	0.69	1.52		208.75	
01/03/2010 17:00	2.16	0.69	1.47		209	
01/03/2010 17:15	2.12	0.69	1.43		209.25	
01/03/2010 17:30	2.09	0.69	1.40		209.5	
01/03/2010 17:45	2.04	0.69	1.35		209.75	
01/03/2010 18:00	2.02	0.69	1.33		210	
01/03/2010 18:15	1.98	0.69	1.29		210.25	
01/03/2010 18:30	1.95	0.69	1.26		210.5	
01/03/2010 18:45	1.92	0.69	1.23		210.75	
01/03/2010 19:00	1.90	0.69	1.21		211	
01/03/2010 19:15	1.86	0.69	1.17		211.25	
01/03/2010 19:30	1.83	0.69	1.14		211.5	
01/03/2010 19:45	1.80	0.69	1.11		211.75	
01/03/2010 20:00	1.77	0.69	1.08		212	
01/03/2010 20:15	1.75	0.69	1.06		212.25	
01/03/2010 20:30	1.74	0.69	1.05		212.5	
01/03/2010 20:45	1.71	0.69	1.02		212.75	
01/03/2010 21:00	1.68	0.69	0.99		213	
01/03/2010 21:15	1.66	0.69	0.97		213.25	
01/03/2010 21:30	1.64	0.69	0.95		213.5	
01/03/2010 21:45	1.63	0.69	0.94		213.75	
01/03/2010 22:00	1.60	0.69	0.91		214	
01/03/2010 22:15	1.59	0.69	0.90		214.25	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
01/03/2010 22:30	1.58	0.69	0.89		214.5	
01/03/2010 22:45	1.55	0.69	0.86		214.75	
01/03/2010 23:00	1.54	0.69	0.85		215	
01/03/2010 23:15	1.53	0.69	0.84		215.25	
01/03/2010 23:30	1.51	0.69	0.82		215.5	
01/03/2010 23:45	1.49	0.69	0.80		215.75	
02/03/2010 00:00	1.48	0.69	0.79		216	
02/03/2010 00:15	1.47	0.69	0.78		216.25	
02/03/2010 00:30	1.45	0.69	0.76		216.5	
02/03/2010 00:45	1.44	0.69	0.75		216.75	
02/03/2010 01:00	1.43	0.69	0.74		217	
02/03/2010 01:15	1.41	0.69	0.72		217.25	
02/03/2010 01:30	1.39	0.69	0.70		217.5	
02/03/2010 01:45	1.38	0.69	0.69		217.75	
02/03/2010 02:00	1.38	0.69	0.69		218	
02/03/2010 02:15	1.36	0.69	0.67		218.25	
02/03/2010 02:30	1.35	0.69	0.66		218.5	
02/03/2010 02:45	1.34	0.69	0.65		218.75	
02/03/2010 03:00	1.33	0.69	0.64		219	
02/03/2010 03:15	1.32	0.69	0.63		219.25	
02/03/2010 03:30	1.31	0.69	0.62		219.5	
02/03/2010 03:45	1.29	0.69	0.60		219.75	
02/03/2010 04:00	1.28	0.69	0.59		220	
02/03/2010 04:15	1.28	0.69	0.59		220.25	
02/03/2010 04:30	1.27	0.69	0.58		220.5	
02/03/2010 04:45	1.26	0.69	0.57		220.75	
02/03/2010 05:00	1.25	0.69	0.56		221	
02/03/2010 05:15	1.24	0.69	0.55		221.25	
02/03/2010 05:30	1.23	0.69	0.54		221.5	
02/03/2010 05:45	1.22	0.69	0.53		221.75	
02/03/2010 06:00	1.21	0.69	0.52		222	
02/03/2010 06:15	1.20	0.69	0.51		222.25	
02/03/2010 06:30	1.20	0.69	0.51		222.5	
02/03/2010 06:45	1.19	0.69	0.50		222.75	
02/03/2010 07:00	1.18	0.69	0.49		223	
02/03/2010 07:15	1.17	0.69	0.48		223.25	
02/03/2010 07:30	1.16	0.69	0.47		223.5	
02/03/2010 07:45	1.16	0.69	0.47		223.75	
02/03/2010 08:00	1.15	0.69	0.46		224	

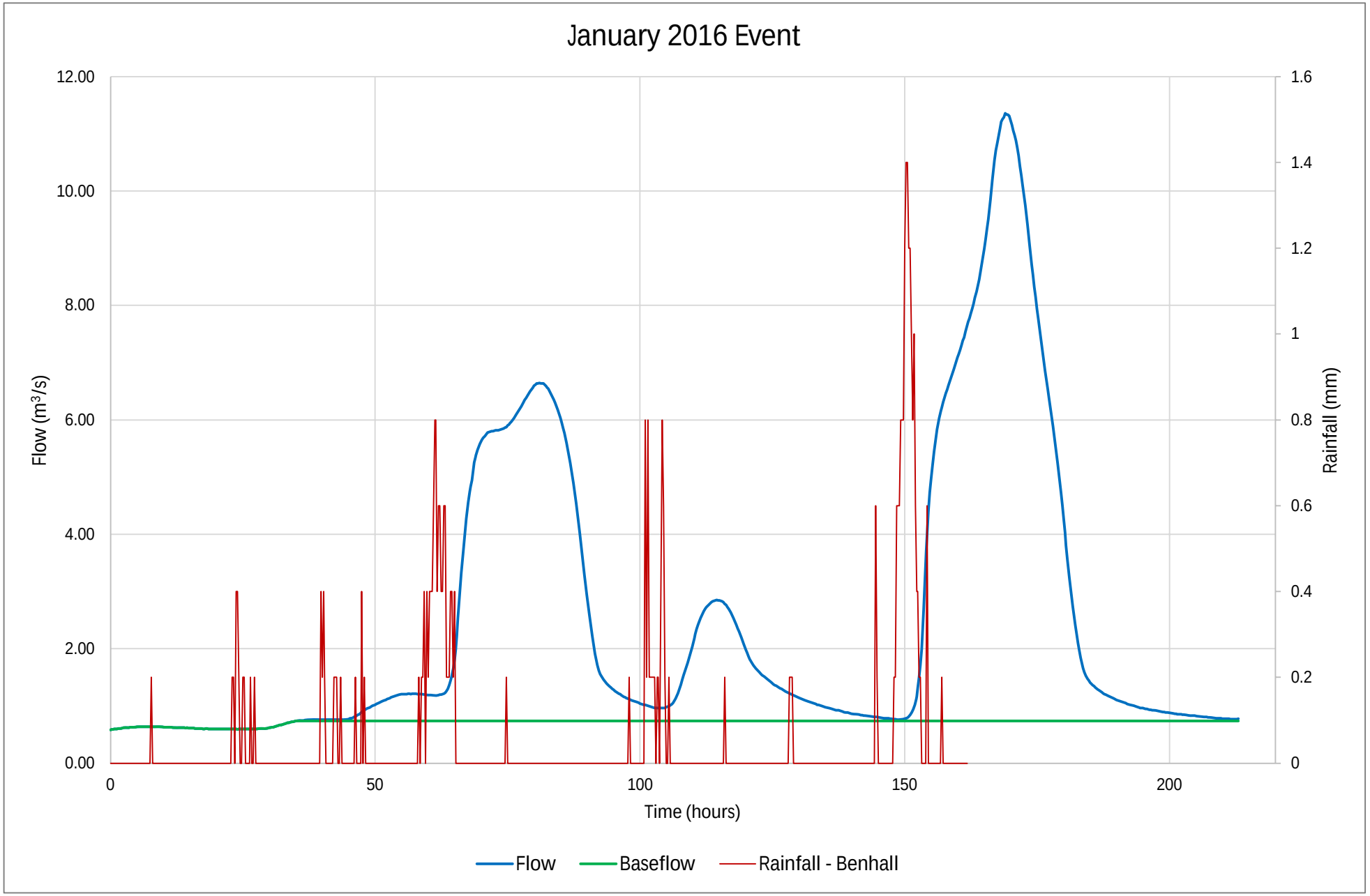
	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
02/03/2010 08:15	1.13	0.69	0.44		224.25	
02/03/2010 08:30	1.12	0.69	0.43		224.5	
02/03/2010 08:45	1.12	0.69	0.43		224.75	
02/03/2010 09:00	1.11	0.69	0.42		225	
02/03/2010 09:15	1.11	0.69	0.42		225.25	
02/03/2010 09:30	1.10	0.69	0.41		225.5	
02/03/2010 09:45	1.09	0.69	0.40		225.75	
02/03/2010 10:00	1.08	0.69	0.39		226	
02/03/2010 10:15	1.08	0.69	0.39		226.25	
02/03/2010 10:30	1.08	0.69	0.39		226.5	
02/03/2010 10:45	1.07	0.69	0.38		226.75	
02/03/2010 11:00	1.06	0.69	0.37		227	
02/03/2010 11:15	1.06	0.69	0.37		227.25	
02/03/2010 11:30	1.05	0.69	0.36		227.5	
02/03/2010 11:45	1.04	0.69	0.35		227.75	
02/03/2010 12:00	1.03	0.69	0.34		228	
02/03/2010 12:15	1.03	0.69	0.34		228.25	
02/03/2010 12:30	1.03	0.69	0.34		228.5	
02/03/2010 12:45	1.02	0.69	0.33		228.75	
02/03/2010 13:00	1.01	0.69	0.32		229	
02/03/2010 13:15	1.01	0.69	0.32		229.25	
02/03/2010 13:30	1.00	0.69	0.31		229.5	
02/03/2010 13:45	1.00	0.69	0.31		229.75	
02/03/2010 14:00	0.99	0.69	0.30		230	
02/03/2010 14:15	0.99	0.69	0.30		230.25	
02/03/2010 14:30	0.99	0.69	0.30		230.5	
02/03/2010 14:45	0.99	0.69	0.30		230.75	
02/03/2010 15:00	0.97	0.69	0.28		231	
02/03/2010 15:15	0.97	0.69	0.28		231.25	
02/03/2010 15:30	0.97	0.69	0.28		231.5	
02/03/2010 15:45	0.96	0.69	0.27		231.75	
02/03/2010 16:00	0.95	0.69	0.26		232	
02/03/2010 16:15	0.95	0.69	0.26		232.25	
02/03/2010 16:30	0.94	0.69	0.25		232.5	
02/03/2010 16:45	0.93	0.69	0.24		232.75	
02/03/2010 17:00	0.93	0.69	0.24		233	
02/03/2010 17:15	0.93	0.69	0.24		233.25	
02/03/2010 17:30	0.92	0.69	0.23		233.5	
02/03/2010 17:45	0.92	0.69	0.23		233.75	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
02/03/2010 18:00	0.91	0.69	0.22		234	
02/03/2010 18:15	0.90	0.69	0.21		234.25	
02/03/2010 18:30	0.90	0.69	0.21		234.5	
02/03/2010 18:45	0.89	0.69	0.20		234.75	
02/03/2010 19:00	0.89	0.69	0.20		235	
02/03/2010 19:15	0.89	0.69	0.20		235.25	
02/03/2010 19:30	0.88	0.69	0.19		235.5	
02/03/2010 19:45	0.88	0.69	0.19		235.75	
02/03/2010 20:00	0.88	0.69	0.19		236	
02/03/2010 20:15	0.87	0.69	0.18		236.25	
02/03/2010 20:30	0.87	0.69	0.18		236.5	
02/03/2010 20:45	0.86	0.69	0.17		236.75	
02/03/2010 21:00	0.86	0.69	0.17		237	
02/03/2010 21:15	0.86	0.69	0.17		237.25	
02/03/2010 21:30	0.85	0.69	0.16		237.5	
02/03/2010 21:45	0.85	0.69	0.16		237.75	
02/03/2010 22:00	0.84	0.69	0.15		238	
02/03/2010 22:15	0.84	0.69	0.15		238.25	
02/03/2010 22:30	0.84	0.69	0.15		238.5	
02/03/2010 22:45	0.84	0.69	0.15		238.75	
02/03/2010 23:00	0.83	0.69	0.14		239	
02/03/2010 23:15	0.83	0.69	0.14		239.25	
02/03/2010 23:30	0.83	0.69	0.14		239.5	
02/03/2010 23:45	0.83	0.69	0.14		239.75	
03/03/2010 00:00	0.82	0.69	0.13		240	
03/03/2010 00:15	0.81	0.69	0.12		240.25	
03/03/2010 00:30	0.81	0.69	0.12		240.5	
03/03/2010 00:45	0.81	0.69	0.12		240.75	
03/03/2010 01:00	0.81	0.69	0.12		241	
03/03/2010 01:15	0.80	0.69	0.11		241.25	
03/03/2010 01:30	0.80	0.69	0.11		241.5	
03/03/2010 01:45	0.80	0.69	0.11		241.75	
03/03/2010 02:00	0.80	0.69	0.11		242	
03/03/2010 02:15	0.79	0.69	0.10		242.25	
03/03/2010 02:30	0.79	0.69	0.10		242.5	
03/03/2010 02:45	0.79	0.69	0.10		242.75	
03/03/2010 03:00	0.79	0.69	0.10		243	
03/03/2010 03:15	0.79	0.69	0.10		243.25	
03/03/2010 03:30	0.78	0.69	0.09		243.5	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
03/03/2010 03:45	0.78	0.69	0.09		243.75	
03/03/2010 04:00	0.78	0.69	0.09		244	
03/03/2010 04:15	0.77	0.69	0.08		244.25	
03/03/2010 04:30	0.77	0.69	0.08		244.5	
03/03/2010 04:45	0.77	0.69	0.08		244.75	
03/03/2010 05:00	0.77	0.69	0.08		245	
03/03/2010 05:15	0.76	0.69	0.07		245.25	
03/03/2010 05:30	0.76	0.69	0.07		245.5	
03/03/2010 05:45	0.76	0.69	0.07		245.75	
03/03/2010 06:00	0.76	0.69	0.07		246	
03/03/2010 06:15	0.76	0.69	0.07		246.25	
03/03/2010 06:30	0.75	0.69	0.06		246.5	
03/03/2010 06:45	0.75	0.69	0.06		246.75	
03/03/2010 07:00	0.75	0.69	0.06		247	
03/03/2010 07:15	0.75	0.69	0.06		247.25	
03/03/2010 07:30	0.75	0.69	0.06		247.5	
03/03/2010 07:45	0.75	0.69	0.06		247.75	
03/03/2010 08:00	0.74	0.69	0.05		248	
03/03/2010 08:15	0.74	0.69	0.05		248.25	
03/03/2010 08:30	0.74	0.69	0.05		248.5	
03/03/2010 08:45	0.74	0.69	0.05		248.75	
03/03/2010 09:00	0.74	0.69	0.05		249	
03/03/2010 09:15	0.74	0.69	0.05		249.25	
03/03/2010 09:30	0.73	0.69	0.04		249.5	
03/03/2010 09:45	0.73	0.69	0.04		249.75	
03/03/2010 10:00	0.72	0.69	0.03		250	
03/03/2010 10:15	0.73	0.69	0.04		250.25	
03/03/2010 10:30	0.72	0.69	0.03		250.5	
03/03/2010 10:45	0.72	0.69	0.03		250.75	
03/03/2010 11:00	0.72	0.69	0.03		251	
03/03/2010 11:15	0.72	0.69	0.03		251.25	
03/03/2010 11:30	0.72	0.69	0.03		251.5	
03/03/2010 11:45	0.72	0.69	0.03		251.75	
03/03/2010 12:00	0.72	0.69	0.03		252	
03/03/2010 12:15	0.72	0.69	0.03		252.25	
03/03/2010 12:30	0.72	0.69	0.03		252.5	
03/03/2010 12:45	0.71	0.69	0.02		252.75	
03/03/2010 13:00	0.72	0.69	0.03		253	
03/03/2010 13:15	0.71	0.69	0.02		253.25	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
03/03/2010 13:30	0.71	0.69	0.02		253.5	
03/03/2010 13:45	0.71	0.69	0.02		253.75	
03/03/2010 14:00	0.71	0.69	0.02		254	
03/03/2010 14:15	0.71	0.69	0.02		254.25	
03/03/2010 14:30	0.71	0.69	0.02		254.5	
03/03/2010 14:45	0.71	0.69	0.02		254.75	
03/03/2010 15:00	0.71	0.69	0.02		255	
03/03/2010 15:15	0.71	0.69	0.02		255.25	
03/03/2010 15:30	0.70	0.69	0.01		255.5	
03/03/2010 15:45	0.70	0.69	0.01		255.75	
03/03/2010 16:00	0.70	0.69	0.01		256	
03/03/2010 16:15	0.70	0.69	0.01		256.25	
03/03/2010 16:30	0.70	0.69	0.01		256.5	
03/03/2010 16:45	0.70	0.69	0.01		256.75	
03/03/2010 17:00	0.70	0.69	0.01		257	
03/03/2010 17:15	0.70	0.69	0.01		257.25	
03/03/2010 17:30	0.70	0.69	0.01		257.5	
03/03/2010 17:45	0.69	0.69	0.00		257.75	
03/03/2010 18:00	0.69	0.69	0.00		258	
03/03/2010 18:15	0.69	0.69	0.00		258.25	
03/03/2010 18:30	0.69	0.69	0.00		258.5	
03/03/2010 18:45	0.69	0.69	0.00		258.75	
03/03/2010 19:00	0.69	0.69	0.00		259	
03/03/2010 19:15	0.69	0.69	0.00		259.25	
03/03/2010 19:30	0.69	0.69	0.00		259.5	
03/03/2010 19:45	0.69	0.69	0.00		259.75	
03/03/2010 20:00	0.68	0.68	0.00		260	
03/03/2010 20:15	0.68	0.68	0.00		260.25	
03/03/2010 20:30	0.68	0.68	0.00		260.5	
03/03/2010 20:45	0.68	0.68	0.00		260.75	
03/03/2010 21:00	0.68	0.68	0.00		261	
03/03/2010 21:15	0.68	0.68	0.00		261.25	
03/03/2010 21:30	0.68	0.68	0.00		261.5	
03/03/2010 21:45	0.68	0.68	0.00		261.75	
03/03/2010 22:00	0.68	0.68	0.00		262	
03/03/2010 22:15	0.68	0.68	0.00		262.25	
03/03/2010 22:30	0.67	0.67	0.00		262.5	
03/03/2010 22:45	0.67	0.67	0.00		262.75	
03/03/2010 23:00	0.67	0.67	0.00		263	

	Middleton			Benhall		Benhall
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	
03/03/2010 23:15	0.67	0.67	0.00		263.25	
03/03/2010 23:30	0.67	0.67	0.00		263.5	
03/03/2010 23:45	0.67	0.67	0.00		263.75	


January 2016 Event
12.00
10.00
8.00
6.00
4.00
2.00
0.00
Flow (m³/s)
1.6
1.4
1.2
1
0.8
0.6
0.4
0.2
0
Rainfall (mm)
0
50
100
150
200
Time (hours)
Flow
Baseflow
Rainfall - Benhall

	Middleton			Benhall	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours
01/01/2016 02:00	0.58	0.58	0.00	0	0
01/01/2016 02:15	0.59	0.59	0.00	0	0.25
01/01/2016 02:30	0.59	0.59	0.00	0	0.5
01/01/2016 02:45	0.59	0.59	0.00	0	0.75
01/01/2016 03:00	0.60	0.60	0.00	0	1
01/01/2016 03:15	0.60	0.60	0.00	0	1.25
01/01/2016 03:30	0.60	0.60	0.00	0	1.5
01/01/2016 03:45	0.61	0.61	0.00	0	1.75
01/01/2016 04:00	0.61	0.61	0.00	0	2
01/01/2016 04:15	0.61	0.61	0.00	0	2.25
01/01/2016 04:30	0.62	0.62	0.00	0	2.5
01/01/2016 04:45	0.62	0.62	0.00	0	2.75
01/01/2016 05:00	0.62	0.62	0.00	0	3
01/01/2016 05:15	0.62	0.62	0.00	0	3.25
01/01/2016 05:30	0.62	0.62	0.00	0	3.5
01/01/2016 05:45	0.62	0.62	0.00	0	3.75
01/01/2016 06:00	0.62	0.62	0.00	0	4
01/01/2016 06:15	0.63	0.63	0.00	0	4.25
01/01/2016 06:30	0.63	0.63	0.00	0	4.5
01/01/2016 06:45	0.63	0.63	0.00	0	4.75
01/01/2016 07:00	0.63	0.63	0.00	0	5
01/01/2016 07:15	0.63	0.63	0.00	0	5.25
01/01/2016 07:30	0.63	0.63	0.00	0	5.5
01/01/2016 07:45	0.64	0.64	0.00	0	5.75
01/01/2016 08:00	0.64	0.64	0.00	0	6
01/01/2016 08:15	0.64	0.64	0.00	0	6.25
01/01/2016 08:30	0.64	0.64	0.00	0	6.5
01/01/2016 08:45	0.64	0.64	0.00	0	6.75
01/01/2016 09:00	0.64	0.64	0.00	0	7
01/01/2016 09:15	0.64	0.64	0.00	0	7.25
01/01/2016 09:30	0.64	0.64	0.00	0	7.5
01/01/2016 09:45	0.64	0.64	0.00	0.2	7.75
01/01/2016 10:00	0.64	0.64	0.00	0	8
01/01/2016 10:15	0.64	0.64	0.00	0	8.25
01/01/2016 10:30	0.64	0.64	0.00	0	8.5
01/01/2016 10:45	0.63	0.63	0.00	0	8.75
01/01/2016 11:00	0.63	0.63	0.00	0	9
01/01/2016 11:15	0.63	0.63	0.00	0	9.25
01/01/2016 11:30	0.63	0.63	0.00	0	9.5
01/01/2016 11:45	0.63	0.63	0.00	0	9.75
01/01/2016 12:00	0.63	0.63	0.00	0	10

First peak	
Area (km^2)	50.16
Total Rain (P) mm	21.6
Time Interval (hour)	0.25
Percentage Runoff	55%
Average PR	64%

Second peak	
Area (km^2)	50.16
Total Rain (P) mm	20.2
Time Interval (hour)	0.25
Percentage Runoff	73%

Thorpeness rainfall gauge data was not avaialble for this event

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
01/01/2016 12:15	0.63	0.63	0.00	0	10.25		
01/01/2016 12:30	0.63	0.63	0.00	0	10.5		
01/01/2016 12:45	0.62	0.62	0.00	0	10.75		
01/01/2016 13:00	0.62	0.62	0.00	0	11		
01/01/2016 13:15	0.62	0.62	0.00	0	11.25		
01/01/2016 13:30	0.62	0.62	0.00	0	11.5		
01/01/2016 13:45	0.62	0.62	0.00	0	11.75		
01/01/2016 14:00	0.62	0.62	0.00	0	12		
01/01/2016 14:15	0.62	0.62	0.00	0	12.25		
01/01/2016 14:30	0.62	0.62	0.00	0	12.5		
01/01/2016 14:45	0.62	0.62	0.00	0	12.75		
01/01/2016 15:00	0.62	0.62	0.00	0	13		
01/01/2016 15:15	0.62	0.62	0.00	0	13.25		
01/01/2016 15:30	0.62	0.62	0.00	0	13.5		
01/01/2016 15:45	0.62	0.62	0.00	0	13.75		
01/01/2016 16:00	0.62	0.62	0.00	0	14		
01/01/2016 16:15	0.61	0.61	0.00	0	14.25		
01/01/2016 16:30	0.62	0.62	0.00	0	14.5		
01/01/2016 16:45	0.61	0.61	0.00	0	14.75		
01/01/2016 17:00	0.61	0.61	0.00	0	15		
01/01/2016 17:15	0.61	0.61	0.00	0	15.25		
01/01/2016 17:30	0.61	0.61	0.00	0	15.5		
01/01/2016 17:45	0.61	0.61	0.00	0	15.75		
01/01/2016 18:00	0.61	0.61	0.00	0	16		
01/01/2016 18:15	0.61	0.61	0.00	0	16.25		
01/01/2016 18:30	0.61	0.61	0.00	0	16.5		
01/01/2016 18:45	0.61	0.61	0.00	0	16.75		
01/01/2016 19:00	0.61	0.61	0.00	0	17		
01/01/2016 19:15	0.60	0.60	0.00	0	17.25		
01/01/2016 19:30	0.60	0.60	0.00	0	17.5		
01/01/2016 19:45	0.60	0.60	0.00	0	17.75		
01/01/2016 20:00	0.60	0.60	0.00	0	18		
01/01/2016 20:15	0.60	0.60	0.00	0	18.25		
01/01/2016 20:30	0.59	0.59	0.00	0	18.5		
01/01/2016 20:45	0.60	0.60	0.00	0	18.75		
01/01/2016 21:00	0.60	0.60	0.00	0	19		
01/01/2016 21:15	0.60	0.60	0.00	0	19.25		
01/01/2016 21:30	0.60	0.60	0.00	0	19.5		
01/01/2016 21:45	0.60	0.60	0.00	0	19.75		
01/01/2016 22:00	0.60	0.60	0.00	0	20		
01/01/2016 22:15	0.60	0.60	0.00	0	20.25		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
01/01/2016 22:30	0.59	0.59	0.00	0	20.5		
01/01/2016 22:45	0.59	0.59	0.00	0	20.75		
01/01/2016 23:00	0.59	0.59	0.00	0	21		
01/01/2016 23:15	0.59	0.59	0.00	0	21.25		
01/01/2016 23:30	0.59	0.59	0.00	0	21.5		
01/01/2016 23:45	0.59	0.59	0.00	0	21.75		
02/01/2016 00:00	0.59	0.59	0.00	0	22		
02/01/2016 00:15	0.59	0.59	0.00	0	22.25		
02/01/2016 00:30	0.60	0.60	0.00	0	22.5		
02/01/2016 00:45	0.59	0.59	0.00	0	22.75		
02/01/2016 01:00	0.59	0.59	0.00	0.2	23		
02/01/2016 01:15	0.59	0.59	0.00	0.2	23.25		
02/01/2016 01:30	0.59	0.59	0.00	0	23.5		
02/01/2016 01:45	0.59	0.59	0.00	0.4	23.75		
02/01/2016 02:00	0.59	0.59	0.00	0.4	24		
02/01/2016 02:15	0.59	0.59	0.00	0.2	24.25		
02/01/2016 02:30	0.59	0.59	0.00	0	24.5		
02/01/2016 02:45	0.59	0.59	0.00	0	24.75		
02/01/2016 03:00	0.59	0.59	0.00	0.2	25		
02/01/2016 03:15	0.59	0.59	0.00	0.2	25.25		
02/01/2016 03:30	0.59	0.59	0.00	0	25.5		
02/01/2016 03:45	0.59	0.59	0.00	0	25.75		
02/01/2016 04:00	0.59	0.59	0.00	0	26		
02/01/2016 04:15	0.60	0.60	0.00	0	26.25		
02/01/2016 04:30	0.59	0.59	0.00	0.2	26.5		
02/01/2016 04:45	0.60	0.60	0.00	0	26.75		
02/01/2016 05:00	0.60	0.60	0.00	0	27		
02/01/2016 05:15	0.60	0.60	0.00	0.2	27.25		
02/01/2016 05:30	0.60	0.60	0.00	0	27.5		
02/01/2016 05:45	0.60	0.60	0.00	0	27.75		
02/01/2016 06:00	0.60	0.60	0.00	0	28		
02/01/2016 06:15	0.60	0.60	0.00	0	28.25		
02/01/2016 06:30	0.60	0.60	0.00	0	28.5		
02/01/2016 06:45	0.60	0.60	0.00	0	28.75		
02/01/2016 07:00	0.61	0.61	0.00	0	29		
02/01/2016 07:15	0.61	0.61	0.00	0	29.25		
02/01/2016 07:30	0.61	0.61	0.00	0	29.5		
02/01/2016 07:45	0.61	0.61	0.00	0	29.75		
02/01/2016 08:00	0.62	0.62	0.00	0	30		
02/01/2016 08:15	0.62	0.62	0.00	0	30.25		
02/01/2016 08:30	0.62	0.62	0.00	0	30.5		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
02/01/2016 08:45	0.63	0.63	0.00	0	30.75		
02/01/2016 09:00	0.63	0.63	0.00	0	31		
02/01/2016 09:15	0.64	0.64	0.00	0	31.25		
02/01/2016 09:30	0.65	0.65	0.00	0	31.5		
02/01/2016 09:45	0.66	0.66	0.00	0	31.75		
02/01/2016 10:00	0.66	0.66	0.00	0	32		
02/01/2016 10:15	0.67	0.67	0.00	0	32.25		
02/01/2016 10:30	0.68	0.68	0.00	0	32.5		
02/01/2016 10:45	0.68	0.68	0.00	0	32.75		
02/01/2016 11:00	0.69	0.69	0.00	0	33		
02/01/2016 11:15	0.70	0.70	0.00	0	33.25		
02/01/2016 11:30	0.70	0.70	0.00	0	33.5		
02/01/2016 11:45	0.71	0.71	0.00	0	33.75		
02/01/2016 12:00	0.71	0.71	0.00	0	34		
02/01/2016 12:15	0.72	0.72	0.00	0	34.25		
02/01/2016 12:30	0.72	0.72	0.00	0	34.5		
02/01/2016 12:45	0.73	0.73	0.00	0	34.75		
02/01/2016 13:00	0.74	0.74	0.00	0	35		
02/01/2016 13:15	0.74	0.74	0.00	0	35.25		
02/01/2016 13:30	0.74	0.74	0.00	0	35.5		
02/01/2016 13:45	0.74	0.74	0.00	0	35.75		
02/01/2016 14:00	0.75	0.74	0.01	0	36		
02/01/2016 14:15	0.75	0.74	0.01	0	36.25		
02/01/2016 14:30	0.75	0.74	0.01	0	36.5		
02/01/2016 14:45	0.75	0.74	0.01	0	36.75		
02/01/2016 15:00	0.75	0.74	0.01	0	37		
02/01/2016 15:15	0.76	0.74	0.02	0	37.25		
02/01/2016 15:30	0.76	0.74	0.02	0	37.5		
02/01/2016 15:45	0.76	0.74	0.02	0	37.75		
02/01/2016 16:00	0.76	0.74	0.02	0	38		
02/01/2016 16:15	0.76	0.74	0.02	0	38.25		
02/01/2016 16:30	0.76	0.74	0.02	0	38.5		
02/01/2016 16:45	0.76	0.74	0.02	0	38.75		
02/01/2016 17:00	0.76	0.74	0.02	0	39		
02/01/2016 17:15	0.76	0.74	0.02	0	39.25		
02/01/2016 17:30	0.76	0.74	0.02	0	39.5		
02/01/2016 17:45	0.76	0.74	0.02	0.4	39.75		
02/01/2016 18:00	0.76	0.74	0.02	0.2	40		
02/01/2016 18:15	0.76	0.74	0.02	0.4	40.25		
02/01/2016 18:30	0.76	0.74	0.02	0.2	40.5		
02/01/2016 18:45	0.76	0.74	0.02	0	40.75		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
02/01/2016 19:00	0.76	0.74	0.02	0	41		
02/01/2016 19:15	0.76	0.74	0.02	0	41.25		
02/01/2016 19:30	0.76	0.74	0.02	0	41.5		
02/01/2016 19:45	0.76	0.74	0.02	0	41.75		
02/01/2016 20:00	0.76	0.74	0.02	0	42		
02/01/2016 20:15	0.76	0.74	0.02	0.2	42.25		
02/01/2016 20:30	0.76	0.74	0.02	0.2	42.5		
02/01/2016 20:45	0.76	0.74	0.02	0.2	42.75		
02/01/2016 21:00	0.76	0.74	0.02	0	43		
02/01/2016 21:15	0.76	0.74	0.02	0	43.25		
02/01/2016 21:30	0.76	0.74	0.02	0.2	43.5		
02/01/2016 21:45	0.76	0.74	0.02	0	43.75		
02/01/2016 22:00	0.76	0.74	0.02	0	44		
02/01/2016 22:15	0.76	0.74	0.02	0	44.25		
02/01/2016 22:30	0.76	0.74	0.02	0	44.5		
02/01/2016 22:45	0.77	0.74	0.03	0	44.75		
02/01/2016 23:00	0.77	0.74	0.03	0	45		
02/01/2016 23:15	0.78	0.74	0.04	0	45.25		
02/01/2016 23:30	0.79	0.74	0.05	0	45.5		
02/01/2016 23:45	0.79	0.74	0.05	0	45.75		
03/01/2016 00:00	0.80	0.74	0.06	0	46		
03/01/2016 00:15	0.81	0.74	0.07	0.2	46.25		
03/01/2016 00:30	0.83	0.74	0.09	0	46.5		
03/01/2016 00:45	0.84	0.74	0.10	0	46.75		
03/01/2016 01:00	0.86	0.74	0.12	0	47		
03/01/2016 01:15	0.88	0.74	0.14	0	47.25		
03/01/2016 01:30	0.89	0.74	0.15	0.4	47.5		
03/01/2016 01:45	0.91	0.74	0.17	0	47.75		
03/01/2016 02:00	0.92	0.74	0.18	0.2	48		
03/01/2016 02:15	0.94	0.74	0.20	0	48.25		
03/01/2016 02:30	0.95	0.74	0.21	0	48.5		
03/01/2016 02:45	0.97	0.74	0.23	0	48.75		
03/01/2016 03:00	0.97	0.74	0.23	0	49		
03/01/2016 03:15	0.99	0.74	0.25	0	49.25		
03/01/2016 03:30	1.00	0.74	0.26	0	49.5		
03/01/2016 03:45	1.01	0.74	0.27	0	49.75		
03/01/2016 04:00	1.02	0.74	0.28	0	50		
03/01/2016 04:15	1.03	0.74	0.29	0	50.25		
03/01/2016 04:30	1.04	0.74	0.30	0	50.5		
03/01/2016 04:45	1.06	0.74	0.32	0	50.75		
03/01/2016 05:00	1.06	0.74	0.32	0	51		

		Middleton		Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
03/01/2016 05:15	1.08	0.74	0.34	0	51.25		
03/01/2016 05:30	1.08	0.74	0.34	0	51.5		
03/01/2016 05:45	1.10	0.74	0.36	0	51.75		
03/01/2016 06:00	1.11	0.74	0.37	0	52		
03/01/2016 06:15	1.12	0.74	0.38	0	52.25		
03/01/2016 06:30	1.13	0.74	0.39	0	52.5		
03/01/2016 06:45	1.13	0.74	0.39	0	52.75		
03/01/2016 07:00	1.15	0.74	0.41	0	53		
03/01/2016 07:15	1.16	0.74	0.42	0	53.25		
03/01/2016 07:30	1.16	0.74	0.42	0	53.5		
03/01/2016 07:45	1.17	0.74	0.43	0	53.75		
03/01/2016 08:00	1.18	0.74	0.44	0	54		
03/01/2016 08:15	1.19	0.74	0.45	0	54.25		
03/01/2016 08:30	1.19	0.74	0.45	0	54.5		
03/01/2016 08:45	1.19	0.74	0.45	0	54.75		
03/01/2016 09:00	1.20	0.74	0.46	0	55		
03/01/2016 09:15	1.21	0.74	0.47	0	55.25		
03/01/2016 09:30	1.21	0.74	0.47	0	55.5		
03/01/2016 09:45	1.21	0.74	0.47	0	55.75		
03/01/2016 10:00	1.21	0.74	0.47	0	56		
03/01/2016 10:15	1.22	0.74	0.48	0	56.25		
03/01/2016 10:30	1.22	0.74	0.48	0	56.5		
03/01/2016 10:45	1.21	0.74	0.47	0	56.75		
03/01/2016 11:00	1.22	0.74	0.48	0	57		
03/01/2016 11:15	1.22	0.74	0.48	0	57.25		
03/01/2016 11:30	1.22	0.74	0.48	0	57.5		
03/01/2016 11:45	1.22	0.74	0.48	0	57.75		
03/01/2016 12:00	1.21	0.74	0.47	0	58		
03/01/2016 12:15	1.21	0.74	0.47	0.2	58.25		
03/01/2016 12:30	1.21	0.74	0.47	0	58.5		
03/01/2016 12:45	1.20	0.74	0.46	0.2	58.75		
03/01/2016 13:00	1.20	0.74	0.46	0.2	59		
03/01/2016 13:15	1.19	0.74	0.45	0.4	59.25		
03/01/2016 13:30	1.19	0.74	0.45	0	59.5		
03/01/2016 13:45	1.19	0.74	0.45	0.4	59.75		
03/01/2016 14:00	1.19	0.74	0.45	0.2	60		
03/01/2016 14:15	1.19	0.74	0.45	0.4	60.25		
03/01/2016 14:30	1.19	0.74	0.45	0.4	60.5		
03/01/2016 14:45	1.19	0.74	0.45	0.4	60.75		
03/01/2016 15:00	1.18	0.74	0.44	0.6	61		
03/01/2016 15:15	1.18	0.74	0.44	0.8	61.25		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
03/01/2016 15:30	1.18	0.74	0.44	0.8	61.5		
03/01/2016 15:45	1.18	0.74	0.44	0.4	61.75		
03/01/2016 16:00	1.19	0.74	0.45	0.6	62		
03/01/2016 16:15	1.19	0.74	0.45	0.6	62.25		
03/01/2016 16:30	1.19	0.74	0.45	0.4	62.5		
03/01/2016 16:45	1.21	0.74	0.47	0.4	62.75		
03/01/2016 17:00	1.22	0.74	0.48	0.6	63		
03/01/2016 17:15	1.23	0.74	0.49	0.6	63.25		
03/01/2016 17:30	1.26	0.74	0.52	0.2	63.5		
03/01/2016 17:45	1.30	0.74	0.56	0.2	63.75		
03/01/2016 18:00	1.36	0.74	0.62	0.2	64		
03/01/2016 18:15	1.44	0.74	0.70	0.4	64.25		
03/01/2016 18:30	1.53	0.74	0.79	0.4	64.5		
03/01/2016 18:45	1.65	0.74	0.91	0.2	64.75		
03/01/2016 19:00	1.80	0.74	1.06	0.4	65		
03/01/2016 19:15	2.03	0.74	1.29	0	65.25		
03/01/2016 19:30	2.33	0.74	1.59	0	65.5		
03/01/2016 19:45	2.70	0.74	1.96	0	65.75		
03/01/2016 20:00	3.01	0.74	2.27	0	66		
03/01/2016 20:15	3.32	0.74	2.58	0	66.25		
03/01/2016 20:30	3.58	0.74	2.84	0	66.5		
03/01/2016 20:45	3.84	0.74	3.10	0	66.75		
03/01/2016 21:00	4.09	0.74	3.35	0	67		
03/01/2016 21:15	4.31	0.74	3.57	0	67.25		
03/01/2016 21:30	4.53	0.74	3.79	0	67.5		
03/01/2016 21:45	4.71	0.74	3.97	0	67.75		
03/01/2016 22:00	4.83	0.74	4.09	0	68		
03/01/2016 22:15	4.94	0.74	4.20	0	68.25		
03/01/2016 22:30	5.06	0.74	4.32	0	68.5		
03/01/2016 22:45	5.26	0.74	4.52	0	68.75		
03/01/2016 23:00	5.35	0.74	4.61	0	69		
03/01/2016 23:15	5.44	0.74	4.70	0	69.25		
03/01/2016 23:30	5.50	0.74	4.76	0	69.5		
03/01/2016 23:45	5.56	0.74	4.82	0	69.75		
04/01/2016 00:00	5.62	0.74	4.88	0	70		
04/01/2016 00:15	5.66	0.74	4.92	0	70.25		
04/01/2016 00:30	5.69	0.74	4.95	0	70.5		
04/01/2016 00:45	5.72	0.74	4.98	0	70.75		
04/01/2016 01:00	5.75	0.74	5.01	0	71		
04/01/2016 01:15	5.77	0.74	5.03	0	71.25		
04/01/2016 01:30	5.78	0.74	5.04	0	71.5		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
04/01/2016 01:45	5.79	0.74	5.05	0	71.75		
04/01/2016 02:00	5.80	0.74	5.06	0	72		
04/01/2016 02:15	5.80	0.74	5.06	0	72.25		
04/01/2016 02:30	5.81	0.74	5.07	0	72.5		
04/01/2016 02:45	5.82	0.74	5.08	0	72.75		
04/01/2016 03:00	5.82	0.74	5.08	0	73		
04/01/2016 03:15	5.82	0.74	5.08	0	73.25		
04/01/2016 03:30	5.82	0.74	5.08	0	73.5		
04/01/2016 03:45	5.83	0.74	5.09	0	73.75		
04/01/2016 04:00	5.84	0.74	5.10	0	74		
04/01/2016 04:15	5.85	0.74	5.11	0	74.25		
04/01/2016 04:30	5.87	0.74	5.13	0	74.5		
04/01/2016 04:45	5.87	0.74	5.13	0.2	74.75		
04/01/2016 05:00	5.90	0.74	5.16	0	75		
04/01/2016 05:15	5.92	0.74	5.18	0	75.25		
04/01/2016 05:30	5.94	0.74	5.20	0	75.5		
04/01/2016 05:45	5.97	0.74	5.23	0	75.75		
04/01/2016 06:00	5.99	0.74	5.25	0	76		
04/01/2016 06:15	6.03	0.74	5.29	0	76.25		
04/01/2016 06:30	6.07	0.74	5.33	0	76.5		
04/01/2016 06:45	6.10	0.74	5.36	0	76.75		
04/01/2016 07:00	6.14	0.74	5.40	0	77		
04/01/2016 07:15	6.18	0.74	5.44	0	77.25		
04/01/2016 07:30	6.22	0.74	5.48	0	77.5		
04/01/2016 07:45	6.25	0.74	5.51	0	77.75		
04/01/2016 08:00	6.30	0.74	5.56	0	78		
04/01/2016 08:15	6.34	0.74	5.60	0	78.25		
04/01/2016 08:30	6.38	0.74	5.64	0	78.5		
04/01/2016 08:45	6.42	0.74	5.68	0	78.75		
04/01/2016 09:00	6.45	0.74	5.71	0	79		
04/01/2016 09:15	6.49	0.74	5.75	0	79.25		
04/01/2016 09:30	6.53	0.74	5.79	0	79.5		
04/01/2016 09:45	6.56	0.74	5.82	0	79.75		
04/01/2016 10:00	6.60	0.74	5.86	0	80		
04/01/2016 10:15	6.62	0.74	5.88	0	80.25		
04/01/2016 10:30	6.64	0.74	5.90	0	80.5		
04/01/2016 10:45	6.64	0.74	5.90	0	80.75		
04/01/2016 11:00	6.65	0.74	5.91	0	81		
04/01/2016 11:15	6.64	0.74	5.90	0	81.25		
04/01/2016 11:30	6.64	0.74	5.90	0	81.5		
04/01/2016 11:45	6.64	0.74	5.90	0	81.75		

		Middleton		Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
04/01/2016 12:00	6.62	0.74	5.88	0	82		
04/01/2016 12:15	6.59	0.74	5.85	0	82.25		
04/01/2016 12:30	6.57	0.74	5.83	0	82.5		
04/01/2016 12:45	6.54	0.74	5.80	0	82.75		
04/01/2016 13:00	6.49	0.74	5.75	0	83		
04/01/2016 13:15	6.45	0.74	5.71	0	83.25		
04/01/2016 13:30	6.40	0.74	5.66	0	83.5		
04/01/2016 13:45	6.35	0.74	5.61	0	83.75		
04/01/2016 14:00	6.30	0.74	5.56	0	84		
04/01/2016 14:15	6.24	0.74	5.50	0	84.25		
04/01/2016 14:30	6.17	0.74	5.43	0	84.5		
04/01/2016 14:45	6.10	0.74	5.36	0	84.75		
04/01/2016 15:00	6.04	0.74	5.30	0	85		
04/01/2016 15:15	5.95	0.74	5.21	0	85.25		
04/01/2016 15:30	5.86	0.74	5.12	0	85.5		
04/01/2016 15:45	5.77	0.74	5.03	0	85.75		
04/01/2016 16:00	5.66	0.74	4.92	0	86		
04/01/2016 16:15	5.55	0.74	4.81	0	86.25		
04/01/2016 16:30	5.42	0.74	4.68	0	86.5		
04/01/2016 16:45	5.30	0.74	4.56	0	86.75		
04/01/2016 17:00	5.15	0.74	4.41	0	87		
04/01/2016 17:15	4.99	0.74	4.25	0	87.25		
04/01/2016 17:30	4.85	0.74	4.11	0	87.5		
04/01/2016 17:45	4.69	0.74	3.95	0	87.75		
04/01/2016 18:00	4.51	0.74	3.77	0	88		
04/01/2016 18:15	4.30	0.74	3.56	0	88.25		
04/01/2016 18:30	4.10	0.74	3.36	0	88.5		
04/01/2016 18:45	3.90	0.74	3.16	0	88.75		
04/01/2016 19:00	3.71	0.74	2.97	0	89		
04/01/2016 19:15	3.51	0.74	2.77	0	89.25		
04/01/2016 19:30	3.32	0.74	2.58	0	89.5		
04/01/2016 19:45	3.13	0.74	2.39	0	89.75		
04/01/2016 20:00	2.95	0.74	2.21	0	90		
04/01/2016 20:15	2.76	0.74	2.02	0	90.25		
04/01/2016 20:30	2.59	0.74	1.85	0	90.5		
04/01/2016 20:45	2.41	0.74	1.67	0	90.75		
04/01/2016 21:00	2.24	0.74	1.50	0	91		
04/01/2016 21:15	2.08	0.74	1.34	0	91.25		
04/01/2016 21:30	1.94	0.74	1.20	0	91.5		
04/01/2016 21:45	1.81	0.74	1.07	0	91.75		
04/01/2016 22:00	1.70	0.74	0.96	0	92		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
04/01/2016 22:15	1.62	0.74	0.88	0	92.25		
04/01/2016 22:30	1.56	0.74	0.82	0	92.5		
04/01/2016 22:45	1.52	0.74	0.78	0	92.75		
04/01/2016 23:00	1.48	0.74	0.74	0	93		
04/01/2016 23:15	1.44	0.74	0.70	0	93.25		
04/01/2016 23:30	1.42	0.74	0.68	0	93.5		
04/01/2016 23:45	1.39	0.74	0.65	0	93.75		
05/01/2016 00:00	1.36	0.74	0.62	0	94		
05/01/2016 00:15	1.35	0.74	0.61	0	94.25		
05/01/2016 00:30	1.32	0.74	0.58	0	94.5		
05/01/2016 00:45	1.30	0.74	0.56	0	94.75		
05/01/2016 01:00	1.28	0.74	0.54	0	95		
05/01/2016 01:15	1.26	0.74	0.52	0	95.25		
05/01/2016 01:30	1.25	0.74	0.51	0	95.5		
05/01/2016 01:45	1.23	0.74	0.49	0	95.75		
05/01/2016 02:00	1.22	0.74	0.48	0	96		
05/01/2016 02:15	1.20	0.74	0.46	0	96.25		
05/01/2016 02:30	1.19	0.74	0.45	0	96.5		
05/01/2016 02:45	1.17	0.74	0.43	0	96.75		
05/01/2016 03:00	1.16	0.74	0.42	0	97		
05/01/2016 03:15	1.15	0.74	0.41	0	97.25		
05/01/2016 03:30	1.13	0.74	0.39	0	97.5		
05/01/2016 03:45	1.13	0.74	0.39	0	97.75		
05/01/2016 04:00	1.12	0.74	0.38	0.2	98		
05/01/2016 04:15	1.11	0.74	0.37	0	98.25		
05/01/2016 04:30	1.10	0.74	0.36	0	98.5		
05/01/2016 04:45	1.08	0.74	0.34	0	98.75		
05/01/2016 05:00	1.08	0.74	0.34	0	99		
05/01/2016 05:15	1.07	0.74	0.33	0	99.25		
05/01/2016 05:30	1.06	0.74	0.32	0	99.5		
05/01/2016 05:45	1.06	0.74	0.32	0	99.75		
05/01/2016 06:00	1.04	0.74	0.30	0	100		
05/01/2016 06:15	1.03	0.74	0.29	0	100.25		
05/01/2016 06:30	1.03	0.74	0.29	0	100.5		
05/01/2016 06:45	1.02	0.74	0.28	0	100.75		
05/01/2016 07:00	1.01	0.74	0.27	0.8	101		
05/01/2016 07:15	1.01	0.74	0.27	0.2	101.25		
05/01/2016 07:30	1.00	0.74	0.26	0.8	101.5		
05/01/2016 07:45	0.99	0.74	0.25	0.2	101.75		
05/01/2016 08:00	0.99	0.74	0.25	0.2	102		
05/01/2016 08:15	0.98	0.74	0.24	0.2	102.25		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
05/01/2016 08:30	0.97	0.74	0.23	0.2	102.5		
05/01/2016 08:45	0.97	0.74	0.23	0.2	102.75		
05/01/2016 09:00	0.97	0.74	0.23	0	103		
05/01/2016 09:15	0.97	0.74	0.23	0.2	103.25		
05/01/2016 09:30	0.96	0.74	0.22	0.2	103.5		
05/01/2016 09:45	0.96	0.74	0.22	0	103.75		
05/01/2016 10:00	0.96	0.74	0.22	0.4	104		
05/01/2016 10:15	0.96	0.74	0.22	0.8	104.25		
05/01/2016 10:30	0.97	0.74	0.23	0.6	104.5		
05/01/2016 10:45	0.97	0.74	0.23	0.2	104.75		
05/01/2016 11:00	0.98	0.74	0.24	0	105		
05/01/2016 11:15	0.99	0.74	0.25	0	105.25		
05/01/2016 11:30	0.99	0.74	0.25	0.2	105.5		
05/01/2016 11:45	1.01	0.74	0.27	0	105.75		
05/01/2016 12:00	1.03	0.74	0.29	0	106		
05/01/2016 12:15	1.05	0.74	0.31	0	106.25		
05/01/2016 12:30	1.08	0.74	0.34	0	106.5		
05/01/2016 12:45	1.13	0.74	0.39	0	106.75		
05/01/2016 13:00	1.18	0.74	0.44	0	107		
05/01/2016 13:15	1.24	0.74	0.50	0	107.25		
05/01/2016 13:30	1.31	0.74	0.57	0	107.5		
05/01/2016 13:45	1.38	0.74	0.64	0	107.75		
05/01/2016 14:00	1.46	0.74	0.72	0	108		
05/01/2016 14:15	1.54	0.74	0.80	0	108.25		
05/01/2016 14:30	1.61	0.74	0.87	0	108.5		
05/01/2016 14:45	1.68	0.74	0.94	0	108.75		
05/01/2016 15:00	1.75	0.74	1.01	0	109		
05/01/2016 15:15	1.83	0.74	1.09	0	109.25		
05/01/2016 15:30	1.91	0.74	1.17	0	109.5		
05/01/2016 15:45	2.00	0.74	1.26	0	109.75		
05/01/2016 16:00	2.09	0.74	1.35	0	110		
05/01/2016 16:15	2.18	0.74	1.44	0	110.25		
05/01/2016 16:30	2.26	0.74	1.52	0	110.5		
05/01/2016 16:45	2.34	0.74	1.60	0	110.75		
05/01/2016 17:00	2.41	0.74	1.67	0	111		
05/01/2016 17:15	2.48	0.74	1.74	0	111.25		
05/01/2016 17:30	2.54	0.74	1.80	0	111.5		
05/01/2016 17:45	2.59	0.74	1.85	0	111.75		
05/01/2016 18:00	2.64	0.74	1.90	0	112		
05/01/2016 18:15	2.68	0.74	1.94	0	112.25		
05/01/2016 18:30	2.72	0.74	1.98	0	112.5		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
05/01/2016 18:45	2.74	0.74	2.00	0	112.75		
05/01/2016 19:00	2.76	0.74	2.02	0	113		
05/01/2016 19:15	2.79	0.74	2.05	0	113.25		
05/01/2016 19:30	2.81	0.74	2.07	0	113.5		
05/01/2016 19:45	2.83	0.74	2.09	0	113.75		
05/01/2016 20:00	2.84	0.74	2.10	0	114		
05/01/2016 20:15	2.85	0.74	2.11	0	114.25		
05/01/2016 20:30	2.85	0.74	2.11	0	114.5		
05/01/2016 20:45	2.85	0.74	2.11	0	114.75		
05/01/2016 21:00	2.85	0.74	2.11	0	115		
05/01/2016 21:15	2.84	0.74	2.10	0	115.25		
05/01/2016 21:30	2.83	0.74	2.09	0	115.5		
05/01/2016 21:45	2.81	0.74	2.07	0	115.75		
05/01/2016 22:00	2.78	0.74	2.04	0.2	116		
05/01/2016 22:15	2.76	0.74	2.02	0	116.25		
05/01/2016 22:30	2.73	0.74	1.99	0	116.5		
05/01/2016 22:45	2.69	0.74	1.95	0	116.75		
05/01/2016 23:00	2.65	0.74	1.91	0	117		
05/01/2016 23:15	2.62	0.74	1.88	0	117.25		
05/01/2016 23:30	2.57	0.74	1.83	0	117.5		
05/01/2016 23:45	2.52	0.74	1.78	0	117.75		
06/01/2016 00:00	2.47	0.74	1.73	0	118		
06/01/2016 00:15	2.41	0.74	1.67	0	118.25		
06/01/2016 00:30	2.35	0.74	1.61	0	118.5		
06/01/2016 00:45	2.30	0.74	1.56	0	118.75		
06/01/2016 01:00	2.24	0.74	1.50	0	119		
06/01/2016 01:15	2.18	0.74	1.44	0	119.25		
06/01/2016 01:30	2.11	0.74	1.37	0	119.5		
06/01/2016 01:45	2.04	0.74	1.30	0	119.75		
06/01/2016 02:00	1.98	0.74	1.24	0	120		
06/01/2016 02:15	1.93	0.74	1.19	0	120.25		
06/01/2016 02:30	1.87	0.74	1.13	0	120.5		
06/01/2016 02:45	1.81	0.74	1.07	0	120.75		
06/01/2016 03:00	1.77	0.74	1.03	0	121		
06/01/2016 03:15	1.74	0.74	1.00	0	121.25		
06/01/2016 03:30	1.70	0.74	0.96	0	121.5		
06/01/2016 03:45	1.67	0.74	0.93	0	121.75		
06/01/2016 04:00	1.64	0.74	0.90	0	122		
06/01/2016 04:15	1.62	0.74	0.88	0	122.25		
06/01/2016 04:30	1.59	0.74	0.85	0	122.5		
06/01/2016 04:45	1.57	0.74	0.83	0	122.75		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
06/01/2016 05:00	1.54	0.74	0.80	0	123		
06/01/2016 05:15	1.53	0.74	0.79	0	123.25		
06/01/2016 05:30	1.51	0.74	0.77	0	123.5		
06/01/2016 05:45	1.48	0.74	0.74	0	123.75		
06/01/2016 06:00	1.47	0.74	0.73	0	124		
06/01/2016 06:15	1.45	0.74	0.71	0	124.25		
06/01/2016 06:30	1.44	0.74	0.70	0	124.5		
06/01/2016 06:45	1.42	0.74	0.68	0	124.75		
06/01/2016 07:00	1.40	0.74	0.66	0	125		
06/01/2016 07:15	1.38	0.74	0.64	0	125.25		
06/01/2016 07:30	1.36	0.74	0.62	0	125.5		
06/01/2016 07:45	1.36	0.74	0.62	0	125.75		
06/01/2016 08:00	1.34	0.74	0.60	0	126		
06/01/2016 08:15	1.32	0.74	0.58	0	126.25		
06/01/2016 08:30	1.31	0.74	0.57	0	126.5		
06/01/2016 08:45	1.30	0.74	0.56	0	126.75		
06/01/2016 09:00	1.28	0.74	0.54	0	127		
06/01/2016 09:15	1.27	0.74	0.53	0	127.25		
06/01/2016 09:30	1.25	0.74	0.51	0	127.5		
06/01/2016 09:45	1.25	0.74	0.51	0	127.75		
06/01/2016 10:00	1.23	0.74	0.49	0	128		
06/01/2016 10:15	1.22	0.74	0.48	0.2	128.25		
06/01/2016 10:30	1.21	0.74	0.47	0.2	128.5		
06/01/2016 10:45	1.19	0.74	0.45	0.2	128.75		
06/01/2016 11:00	1.18	0.74	0.44	0	129		
06/01/2016 11:15	1.17	0.74	0.43	0	129.25		
06/01/2016 11:30	1.16	0.74	0.42	0	129.5		
06/01/2016 11:45	1.15	0.74	0.41	0	129.75		
06/01/2016 12:00	1.14	0.74	0.40	0	130		
06/01/2016 12:15	1.13	0.74	0.39	0	130.25		
06/01/2016 12:30	1.12	0.74	0.38	0	130.5		
06/01/2016 12:45	1.11	0.74	0.37	0	130.75		
06/01/2016 13:00	1.11	0.74	0.37	0	131		
06/01/2016 13:15	1.10	0.74	0.36	0	131.25		
06/01/2016 13:30	1.09	0.74	0.35	0	131.5		
06/01/2016 13:45	1.08	0.74	0.34	0	131.75		
06/01/2016 14:00	1.07	0.74	0.33	0	132		
06/01/2016 14:15	1.06	0.74	0.32	0	132.25		
06/01/2016 14:30	1.06	0.74	0.32	0	132.5		
06/01/2016 14:45	1.05	0.74	0.31	0	132.75		
06/01/2016 15:00	1.04	0.74	0.30	0	133		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
06/01/2016 15:15	1.03	0.74	0.29	0	133.25		
06/01/2016 15:30	1.02	0.74	0.28	0	133.5		
06/01/2016 15:45	1.01	0.74	0.27	0	133.75		
06/01/2016 16:00	1.01	0.74	0.27	0	134		
06/01/2016 16:15	1.00	0.74	0.26	0	134.25		
06/01/2016 16:30	0.99	0.74	0.25	0	134.5		
06/01/2016 16:45	0.99	0.74	0.25	0	134.75		
06/01/2016 17:00	0.98	0.74	0.24	0	135		
06/01/2016 17:15	0.97	0.74	0.23	0	135.25		
06/01/2016 17:30	0.97	0.74	0.23	0	135.5		
06/01/2016 17:45	0.96	0.74	0.22	0	135.75		
06/01/2016 18:00	0.95	0.74	0.21	0	136		
06/01/2016 18:15	0.95	0.74	0.21	0	136.25		
06/01/2016 18:30	0.94	0.74	0.20	0	136.5		
06/01/2016 18:45	0.93	0.74	0.19	0	136.75		
06/01/2016 19:00	0.93	0.74	0.19	0	137		
06/01/2016 19:15	0.92	0.74	0.18	0	137.25		
06/01/2016 19:30	0.92	0.74	0.18	0	137.5		
06/01/2016 19:45	0.91	0.74	0.17	0	137.75		
06/01/2016 20:00	0.91	0.74	0.17	0	138		
06/01/2016 20:15	0.90	0.74	0.16	0	138.25		
06/01/2016 20:30	0.89	0.74	0.15	0	138.5		
06/01/2016 20:45	0.89	0.74	0.15	0	138.75		
06/01/2016 21:00	0.89	0.74	0.15	0	139		
06/01/2016 21:15	0.88	0.74	0.14	0	139.25		
06/01/2016 21:30	0.88	0.74	0.14	0	139.5		
06/01/2016 21:45	0.87	0.74	0.13	0	139.75		
06/01/2016 22:00	0.86	0.74	0.12	0	140		
06/01/2016 22:15	0.86	0.74	0.12	0	140.25		
06/01/2016 22:30	0.86	0.74	0.12	0	140.5		
06/01/2016 22:45	0.86	0.74	0.12	0	140.75		
06/01/2016 23:00	0.85	0.74	0.11	0	141		
06/01/2016 23:15	0.85	0.74	0.11	0	141.25		
06/01/2016 23:30	0.84	0.74	0.10	0	141.5		
06/01/2016 23:45	0.84	0.74	0.10	0	141.75		
07/01/2016 00:00	0.84	0.74	0.10	0	142		
07/01/2016 00:15	0.83	0.74	0.09	0	142.25		
07/01/2016 00:30	0.83	0.74	0.09	0	142.5		
07/01/2016 00:45	0.83	0.74	0.09	0	142.75		
07/01/2016 01:00	0.82	0.74	0.08	0	143		
07/01/2016 01:15	0.82	0.74	0.08	0	143.25		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
07/01/2016 01:30	0.81	0.74	0.07	0	143.5		
07/01/2016 01:45	0.81	0.74	0.07	0	143.75		
07/01/2016 02:00	0.81	0.74	0.07	0	144		
07/01/2016 02:15	0.81	0.74	0.07	0	144.25		
07/01/2016 02:30	0.80	0.74	0.06	0.6	144.5		
07/01/2016 02:45	0.80	0.74	0.06	0.2	144.75		
07/01/2016 03:00	0.80	0.74	0.06	0	145		
07/01/2016 03:15	0.80	0.74	0.06	0	145.25		
07/01/2016 03:30	0.79	0.74	0.05	0	145.5		
07/01/2016 03:45	0.79	0.74	0.05	0	145.75		
07/01/2016 04:00	0.79	0.74	0.05	0	146		
07/01/2016 04:15	0.79	0.74	0.05	0	146.25		
07/01/2016 04:30	0.78	0.74	0.04	0	146.5		
07/01/2016 04:45	0.78	0.74	0.04	0	146.75		
07/01/2016 05:00	0.78	0.74	0.04	0	147		
07/01/2016 05:15	0.77	0.74	0.03	0	147.25		
07/01/2016 05:30	0.77	0.74	0.03	0	147.5		
07/01/2016 05:45	0.77	0.74	0.03	0	147.75		
07/01/2016 06:00	0.77	0.74	0.03	0.2	148		
07/01/2016 06:15	0.77	0.74	0.03	0.2	148.25		
07/01/2016 06:30	0.76	0.74	0.02	0.6	148.5		
07/01/2016 06:45	0.76	0.74	0.02	0.6	148.75		
07/01/2016 07:00	0.76	0.74	0.02	0.6	149		
07/01/2016 07:15	0.76	0.74	0.02	0.8	149.25		
07/01/2016 07:30	0.77	0.74	0.03	0.8	149.5		
07/01/2016 07:45	0.77	0.74	0.03	0.8	149.75		
07/01/2016 08:00	0.77	0.74	0.03	1.2	150		
07/01/2016 08:15	0.78	0.74	0.04	1.4	150.25		
07/01/2016 08:30	0.79	0.74	0.05	1.4	150.5		
07/01/2016 08:45	0.81	0.74	0.07	1.2	150.75		
07/01/2016 09:00	0.84	0.74	0.10	1.2	151		
07/01/2016 09:15	0.88	0.74	0.14	1	151.25		
07/01/2016 09:30	0.92	0.74	0.18	0.8	151.5		
07/01/2016 09:45	0.98	0.74	0.24	1	151.75		
07/01/2016 10:00	1.06	0.74	0.32	0.6	152		
07/01/2016 10:15	1.16	0.74	0.42	0.4	152.25		
07/01/2016 10:30	1.31	0.74	0.57	0.4	152.5		
07/01/2016 10:45	1.49	0.74	0.75	0.2	152.75		
07/01/2016 11:00	1.71	0.74	0.97	0.2	153		
07/01/2016 11:15	1.99	0.74	1.25	0	153.25		
07/01/2016 11:30	2.45	0.74	1.71	0	153.5		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
07/01/2016 11:45	2.99	0.74	2.25	0	153.75		
07/01/2016 12:00	3.53	0.74	2.79	0	154		
07/01/2016 12:15	4.00	0.74	3.26	0.6	154.25		
07/01/2016 12:30	4.39	0.74	3.65	0	154.5		
07/01/2016 12:45	4.73	0.74	3.99	0	154.75		
07/01/2016 13:00	4.97	0.74	4.23	0	155		
07/01/2016 13:15	5.18	0.74	4.44	0	155.25		
07/01/2016 13:30	5.40	0.74	4.66	0	155.5		
07/01/2016 13:45	5.59	0.74	4.85	0	155.75		
07/01/2016 14:00	5.76	0.74	5.02	0	156		
07/01/2016 14:15	5.91	0.74	5.17	0	156.25		
07/01/2016 14:30	6.03	0.74	5.29	0	156.5		
07/01/2016 14:45	6.12	0.74	5.38	0	156.75		
07/01/2016 15:00	6.22	0.74	5.48	0.2	157		
07/01/2016 15:15	6.31	0.74	5.57	0	157.25		
07/01/2016 15:30	6.39	0.74	5.65	0	157.5		
07/01/2016 15:45	6.46	0.74	5.72	0	157.75		
07/01/2016 16:00	6.53	0.74	5.79	0	158		
07/01/2016 16:15	6.61	0.74	5.87	0	158.25		
07/01/2016 16:30	6.67	0.74	5.93	0	158.5		
07/01/2016 16:45	6.74	0.74	6.00	0	158.75		
07/01/2016 17:00	6.81	0.74	6.07	0	159		
07/01/2016 17:15	6.88	0.74	6.14	0	159.25		
07/01/2016 17:30	6.95	0.74	6.21	0	159.5		
07/01/2016 17:45	7.01	0.74	6.27	0	159.75		
07/01/2016 18:00	7.09	0.74	6.35	0	160		
07/01/2016 18:15	7.15	0.74	6.41	0	160.25		
07/01/2016 18:30	7.22	0.74	6.48	0	160.5		
07/01/2016 18:45	7.30	0.74	6.56	0	160.75		
07/01/2016 19:00	7.38	0.74	6.64	0	161		
07/01/2016 19:15	7.44	0.74	6.70	0	161.25		
07/01/2016 19:30	7.54	0.74	6.80	0	161.5		
07/01/2016 19:45	7.63	0.74	6.89	0	161.75		
07/01/2016 20:00	7.71	0.74	6.97	0	162		
07/01/2016 20:15	7.78	0.74	7.04	0	162.25		
07/01/2016 20:30	7.86	0.74	7.12	0	162.5		
07/01/2016 20:45	7.94	0.74	7.20	0	162.75		
07/01/2016 21:00	8.02	0.74	7.28	0	163		
07/01/2016 21:15	8.13	0.74	7.39	0	163.25		
07/01/2016 21:30	8.22	0.74	7.48	0	163.5		
07/01/2016 21:45	8.31	0.74	7.57	0	163.75		

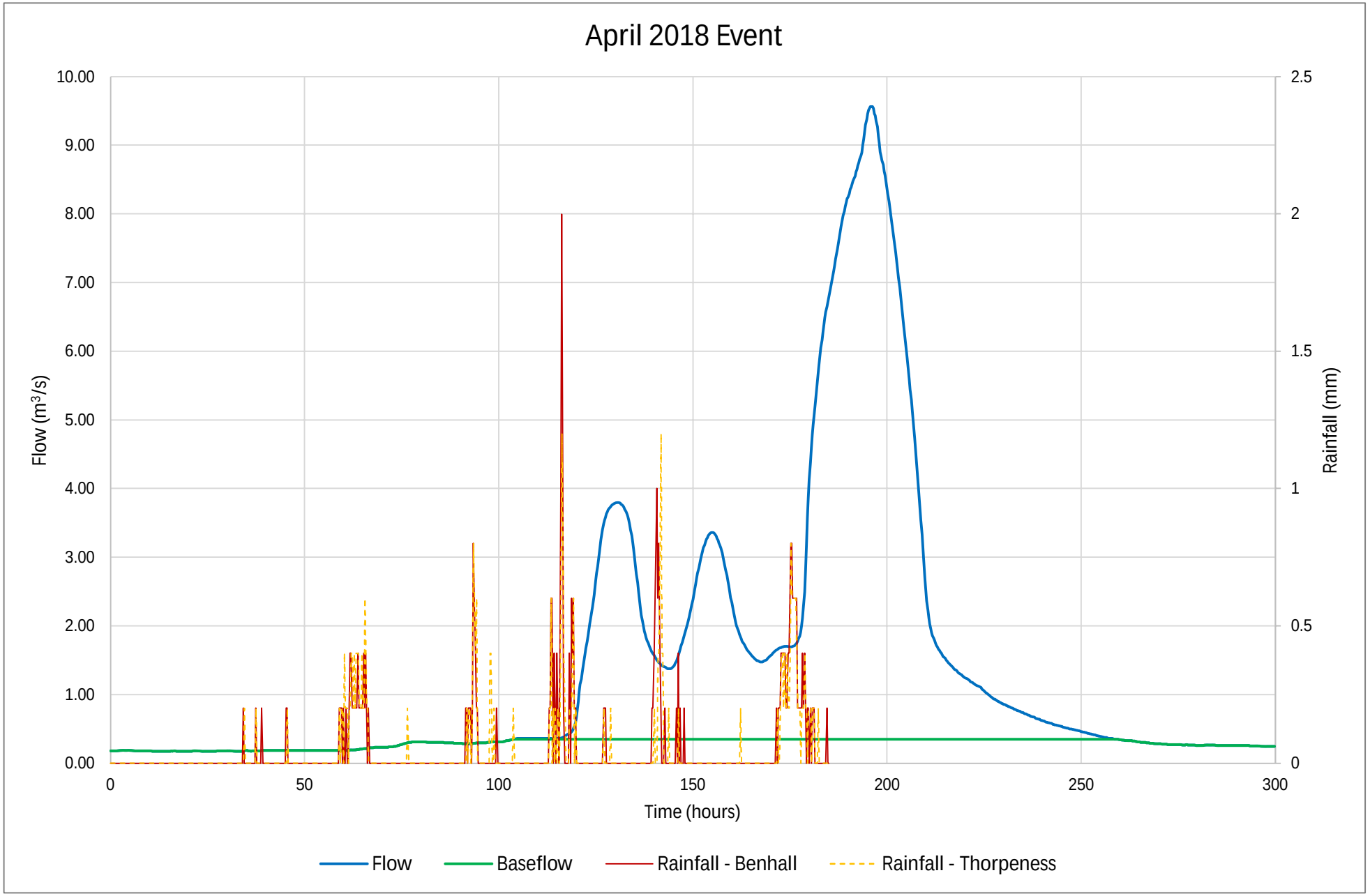
	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
07/01/2016 22:00	8.42	0.74	7.68	0	164		
07/01/2016 22:15	8.56	0.74	7.82	0	164.25		
07/01/2016 22:30	8.70	0.74	7.96	0	164.5		
07/01/2016 22:45	8.83	0.74	8.09	0	164.75		
07/01/2016 23:00	8.99	0.74	8.25	0	165		
07/01/2016 23:15	9.15	0.74	8.41	0	165.25		
07/01/2016 23:30	9.33	0.74	8.59	0	165.5		
07/01/2016 23:45	9.50	0.74	8.76	0	165.75		
08/01/2016 00:00	9.70	0.74	8.96	0	166		
08/01/2016 00:15	9.93	0.74	9.19	0	166.25		
08/01/2016 00:30	10.12	0.74	9.38	0	166.5		
08/01/2016 00:45	10.34	0.74	9.60	0	166.75		
08/01/2016 01:00	10.52	0.74	9.78	0	167		
08/01/2016 01:15	10.71	0.74	9.97	0	167.25		
08/01/2016 01:30	10.83	0.74	10.09	0	167.5		
08/01/2016 01:45	10.95	0.74	10.21	0	167.75		
08/01/2016 02:00	11.08	0.74	10.34	0	168		
08/01/2016 02:15	11.21	0.74	10.47	0	168.25		
08/01/2016 02:30	11.26	0.74	10.52	0	168.5		
08/01/2016 02:45	11.29	0.74	10.55	0	168.75		
08/01/2016 03:00	11.36	0.74	10.62	0	169		
08/01/2016 03:15	11.34	0.74	10.60	0	169.25		
08/01/2016 03:30	11.34	0.74	10.60	0	169.5		
08/01/2016 03:45	11.31	0.74	10.57	0	169.75		
08/01/2016 04:00	11.23	0.74	10.49	0	170		
08/01/2016 04:15	11.16	0.74	10.42	0	170.25		
08/01/2016 04:30	11.05	0.74	10.31	0	170.5		
08/01/2016 04:45	10.98	0.74	10.24	0	170.75		
08/01/2016 05:00	10.88	0.74	10.14	0	171		
08/01/2016 05:15	10.76	0.74	10.02	0	171.25		
08/01/2016 05:30	10.61	0.74	9.87	0	171.5		
08/01/2016 05:45	10.43	0.74	9.69	0	171.75		
08/01/2016 06:00	10.27	0.74	9.53	0	172		
08/01/2016 06:15	10.10	0.74	9.36	0	172.25		
08/01/2016 06:30	9.93	0.74	9.19	0	172.5		
08/01/2016 06:45	9.74	0.74	9.00	0	172.75		
08/01/2016 07:00	9.54	0.74	8.80	0	173		
08/01/2016 07:15	9.35	0.74	8.61	0	173.25		
08/01/2016 07:30	9.15	0.74	8.41	0	173.5		
08/01/2016 07:45	8.95	0.74	8.21	0	173.75		
08/01/2016 08:00	8.73	0.74	7.99	0	174		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
08/01/2016 08:15	8.54	0.74	7.80	0	174.25		
08/01/2016 08:30	8.33	0.74	7.59	0	174.5		
08/01/2016 08:45	8.15	0.74	7.41	0	174.75		
08/01/2016 09:00	7.94	0.74	7.20	0	175		
08/01/2016 09:15	7.77	0.74	7.03	0	175.25		
08/01/2016 09:30	7.60	0.74	6.86	0	175.5		
08/01/2016 09:45	7.41	0.74	6.67	0.2	175.75		
08/01/2016 10:00	7.21	0.74	6.47	0	176		
08/01/2016 10:15	7.04	0.74	6.30	0	176.25		
08/01/2016 10:30	6.88	0.74	6.14	0	176.5		
08/01/2016 10:45	6.71	0.74	5.97	0	176.75		
08/01/2016 11:00	6.55	0.74	5.81	0	177		
08/01/2016 11:15	6.38	0.74	5.64	0	177.25		
08/01/2016 11:30	6.22	0.74	5.48	0	177.5		
08/01/2016 11:45	6.05	0.74	5.31	0	177.75		
08/01/2016 12:00	5.88	0.74	5.14	0	178		
08/01/2016 12:15	5.71	0.74	4.97	0	178.25		
08/01/2016 12:30	5.52	0.74	4.78	0	178.5		
08/01/2016 12:45	5.33	0.74	4.59	0	178.75		
08/01/2016 13:00	5.13	0.74	4.39	0	179		
08/01/2016 13:15	4.93	0.74	4.19	0	179.25		
08/01/2016 13:30	4.73	0.74	3.99	0	179.5		
08/01/2016 13:45	4.51	0.74	3.77	0	179.75		
08/01/2016 14:00	4.26	0.74	3.52	0	180		
08/01/2016 14:15	4.03	0.74	3.29	0	180.25		
08/01/2016 14:30	3.80	0.74	3.06	0	180.5		
08/01/2016 14:45	3.57	0.74	2.83	0	180.75		
08/01/2016 15:00	3.35	0.74	2.61	0	181		
08/01/2016 15:15	3.15	0.74	2.41	0	181.25		
08/01/2016 15:30	2.95	0.74	2.21	0	181.5		
08/01/2016 15:45	2.75	0.74	2.01	0	181.75		
08/01/2016 16:00	2.58	0.74	1.84	0	182		
08/01/2016 16:15	2.41	0.74	1.67	0	182.25		
08/01/2016 16:30	2.25	0.74	1.51	0	182.5		
08/01/2016 16:45	2.10	0.74	1.36	0	182.75		
08/01/2016 17:00	1.96	0.74	1.22	0	183		
08/01/2016 17:15	1.84	0.74	1.10	0	183.25		
08/01/2016 17:30	1.73	0.74	0.99	0	183.5		
08/01/2016 17:45	1.64	0.74	0.90	0	183.75		
08/01/2016 18:00	1.58	0.74	0.84	0	184		
08/01/2016 18:15	1.52	0.74	0.78	0	184.25		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
08/01/2016 18:30	1.48	0.74	0.74	0	184.5		
08/01/2016 18:45	1.44	0.74	0.70	0	184.75		
08/01/2016 19:00	1.41	0.74	0.67	0	185		
08/01/2016 19:15	1.39	0.74	0.65	0	185.25		
08/01/2016 19:30	1.36	0.74	0.62	0	185.5		
08/01/2016 19:45	1.35	0.74	0.61	0	185.75		
08/01/2016 20:00	1.32	0.74	0.58	0	186		
08/01/2016 20:15	1.30	0.74	0.56	0	186.25		
08/01/2016 20:30	1.28	0.74	0.54	0	186.5		
08/01/2016 20:45	1.27	0.74	0.53	0	186.75		
08/01/2016 21:00	1.25	0.74	0.51	0	187		
08/01/2016 21:15	1.24	0.74	0.50	0	187.25		
08/01/2016 21:30	1.22	0.74	0.48	0	187.5		
08/01/2016 21:45	1.21	0.74	0.47	0	187.75		
08/01/2016 22:00	1.19	0.74	0.45	0	188		
08/01/2016 22:15	1.18	0.74	0.44	0	188.25		
08/01/2016 22:30	1.17	0.74	0.43	0	188.5		
08/01/2016 22:45	1.16	0.74	0.42	0	188.75		
08/01/2016 23:00	1.15	0.74	0.41	0	189		
08/01/2016 23:15	1.14	0.74	0.40	0	189.25		
08/01/2016 23:30	1.13	0.74	0.39	0	189.5		
08/01/2016 23:45	1.12	0.74	0.38	0	189.75		
09/01/2016 00:00	1.11	0.74	0.37	0	190		
09/01/2016 00:15	1.10	0.74	0.36	0	190.25		
09/01/2016 00:30	1.09	0.74	0.35	0	190.5		
09/01/2016 00:45	1.08	0.74	0.34	0	190.75		
09/01/2016 01:00	1.07	0.74	0.33	0	191		
09/01/2016 01:15	1.06	0.74	0.32	0	191.25		
09/01/2016 01:30	1.06	0.74	0.32	0	191.5		
09/01/2016 01:45	1.05	0.74	0.31	0	191.75		
09/01/2016 02:00	1.03	0.74	0.29	0	192		
09/01/2016 02:15	1.03	0.74	0.29	0	192.25		
09/01/2016 02:30	1.02	0.74	0.28	0	192.5		
09/01/2016 02:45	1.01	0.74	0.27	0.2	192.75		
09/01/2016 03:00	1.01	0.74	0.27	0	193		
09/01/2016 03:15	1.00	0.74	0.26	0	193.25		
09/01/2016 03:30	0.99	0.74	0.25	0.2	193.5		
09/01/2016 03:45	0.99	0.74	0.25	0	193.75		
09/01/2016 04:00	0.98	0.74	0.24	0	194		
09/01/2016 04:15	0.97	0.74	0.23	0	194.25		
09/01/2016 04:30	0.97	0.74	0.23	0	194.5		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
09/01/2016 04:45	0.97	0.74	0.23	0.2	194.75		
09/01/2016 05:00	0.96	0.74	0.22	0	195		
09/01/2016 05:15	0.95	0.74	0.21	0.2	195.25		
09/01/2016 05:30	0.95	0.74	0.21	0	195.5		
09/01/2016 05:45	0.95	0.74	0.21	0	195.75		
09/01/2016 06:00	0.94	0.74	0.20	0.2	196		
09/01/2016 06:15	0.93	0.74	0.19	0	196.25		
09/01/2016 06:30	0.93	0.74	0.19	0	196.5		
09/01/2016 06:45	0.93	0.74	0.19	0	196.75		
09/01/2016 07:00	0.92	0.74	0.18	0	197		
09/01/2016 07:15	0.92	0.74	0.18	0	197.25		
09/01/2016 07:30	0.91	0.74	0.17	0	197.5		
09/01/2016 07:45	0.91	0.74	0.17	0	197.75		
09/01/2016 08:00	0.91	0.74	0.17	0	198		
09/01/2016 08:15	0.90	0.74	0.16	0	198.25		
09/01/2016 08:30	0.90	0.74	0.16	0	198.5		
09/01/2016 08:45	0.89	0.74	0.15	0	198.75		
09/01/2016 09:00	0.89	0.74	0.15	0	199		
09/01/2016 09:15	0.89	0.74	0.15	0	199.25		
09/01/2016 09:30	0.88	0.74	0.14	0	199.5		
09/01/2016 09:45	0.88	0.74	0.14	0	199.75		
09/01/2016 10:00	0.88	0.74	0.14	0	200		
09/01/2016 10:15	0.88	0.74	0.14	0	200.25		
09/01/2016 10:30	0.87	0.74	0.13	0	200.5		
09/01/2016 10:45	0.87	0.74	0.13	0	200.75		
09/01/2016 11:00	0.86	0.74	0.12	0	201		
09/01/2016 11:15	0.86	0.74	0.12	0	201.25		
09/01/2016 11:30	0.86	0.74	0.12	0	201.5		
09/01/2016 11:45	0.86	0.74	0.12	0	201.75		
09/01/2016 12:00	0.85	0.74	0.11	0	202		
09/01/2016 12:15	0.85	0.74	0.11	0	202.25		
09/01/2016 12:30	0.84	0.74	0.10	0	202.5		
09/01/2016 12:45	0.84	0.74	0.10	0	202.75		
09/01/2016 13:00	0.84	0.74	0.10	0	203		
09/01/2016 13:15	0.84	0.74	0.10	0	203.25		
09/01/2016 13:30	0.84	0.74	0.10	0	203.5		
09/01/2016 13:45	0.83	0.74	0.09	0	203.75		
09/01/2016 14:00	0.83	0.74	0.09	0	204		
09/01/2016 14:15	0.83	0.74	0.09	0	204.25		
09/01/2016 14:30	0.83	0.74	0.09	0	204.5		
09/01/2016 14:45	0.83	0.74	0.09	0	204.75		

	Middleton			Benhall			
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	First peak	Second peak
09/01/2016 15:00	0.82	0.74	0.08	0	205		
09/01/2016 15:15	0.82	0.74	0.08	0	205.25		
09/01/2016 15:30	0.81	0.74	0.07	0	205.5		
09/01/2016 15:45	0.81	0.74	0.07	0	205.75		
09/01/2016 16:00	0.81	0.74	0.07	0	206		
09/01/2016 16:15	0.81	0.74	0.07	0	206.25		
09/01/2016 16:30	0.81	0.74	0.07	0	206.5		
09/01/2016 16:45	0.80	0.74	0.06	0	206.75		
09/01/2016 17:00	0.80	0.74	0.06	0	207		
09/01/2016 17:15	0.80	0.74	0.06	0	207.25		
09/01/2016 17:30	0.80	0.74	0.06	0	207.5		
09/01/2016 17:45	0.80	0.74	0.06	0	207.75		
09/01/2016 18:00	0.79	0.74	0.05	0	208		
09/01/2016 18:15	0.79	0.74	0.05	0	208.25		
09/01/2016 18:30	0.79	0.74	0.05	0	208.5		
09/01/2016 18:45	0.79	0.74	0.05	0	208.75		
09/01/2016 19:00	0.79	0.74	0.05	0	209		
09/01/2016 19:15	0.78	0.74	0.04	0.2	209.25		
09/01/2016 19:30	0.78	0.74	0.04	0.6	209.5		
09/01/2016 19:45	0.78	0.74	0.04	0.2	209.75		
09/01/2016 20:00	0.77	0.74	0.03	0.2	210		
09/01/2016 20:15	0.77	0.74	0.03	0.2	210.25		
09/01/2016 20:30	0.77	0.74	0.03	0	210.5		
09/01/2016 20:45	0.77	0.74	0.03	0	210.75		
09/01/2016 21:00	0.77	0.74	0.03	0	211		
09/01/2016 21:15	0.77	0.74	0.03	0	211.25		
09/01/2016 21:30	0.77	0.74	0.03	0	211.5		
09/01/2016 21:45	0.77	0.74	0.03	0	211.75		
09/01/2016 22:00	0.77	0.74	0.03	0	212		
09/01/2016 22:15	0.77	0.74	0.03	0	212.25		
09/01/2016 22:30	0.77	0.74	0.03	0	212.5		
09/01/2016 22:45	0.77	0.74	0.03	0.2	212.75		
09/01/2016 23:00	0.77	0.74	0.03	0.2	213		


April 2018 Event
10.00
9.00
8.00
7.00
6.00
5.00
4.00
3.00
2.00
1.00
0.00
Flow (m³/s)
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
50
100
150
200
250
300
Time (hours)
Flow
Baseflow
Rainfall - Benhall
Rainfall - Thorpeness

		Middleton		Benhall		Thorpeness
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
25/03/2018 21:00	0.18	0.18	0.00	0	0	0
25/03/2018 21:15	0.18	0.18	0.00	0	0.25	0
25/03/2018 21:30	0.18	0.18	0.00	0	0.5	0
25/03/2018 21:45	0.18	0.18	0.00	0	0.75	0
25/03/2018 22:00	0.18	0.18	0.00	0	1	0
25/03/2018 22:15	0.18	0.18	0.00	0	1.25	0
25/03/2018 22:30	0.18	0.18	0.00	0	1.5	0
25/03/2018 22:45	0.18	0.18	0.00	0	1.75	0
25/03/2018 23:00	0.18	0.18	0.00	0	2	0
25/03/2018 23:15	0.18	0.18	0.00	0	2.25	0
25/03/2018 23:30	0.18	0.18	0.00	0	2.5	0
25/03/2018 23:45	0.18	0.18	0.00	0	2.75	0
26/03/2018 00:00	0.18	0.18	0.00	0	3	0
26/03/2018 00:15	0.18	0.18	0.00	0	3.25	0
26/03/2018 00:30	0.18	0.18	0.00	0	3.5	0
26/03/2018 00:45	0.18	0.18	0.00	0	3.75	0
26/03/2018 01:00	0.18	0.18	0.00	0	4	0
26/03/2018 01:15	0.18	0.18	0.00	0	4.25	0
26/03/2018 01:30	0.18	0.18	0.00	0	4.5	0
26/03/2018 01:45	0.18	0.18	0.00	0	4.75	0
26/03/2018 02:00	0.18	0.18	0.00	0	5	0
26/03/2018 02:15	0.18	0.18	0.00	0	5.25	0
26/03/2018 02:30	0.18	0.18	0.00	0	5.5	0
26/03/2018 02:45	0.18	0.18	0.00	0	5.75	0
26/03/2018 03:00	0.18	0.18	0.00	0	6	0
26/03/2018 03:15	0.18	0.18	0.00	0	6.25	0
26/03/2018 03:30	0.18	0.18	0.00	0	6.5	0
26/03/2018 03:45	0.18	0.18	0.00	0	6.75	0
26/03/2018 04:00	0.18	0.18	0.00	0	7	0
26/03/2018 04:15	0.18	0.18	0.00	0	7.25	0
26/03/2018 04:30	0.18	0.18	0.00	0	7.5	0
26/03/2018 04:45	0.18	0.18	0.00	0	7.75	0
26/03/2018 05:00	0.18	0.18	0.00	0	8	0
26/03/2018 05:15	0.18	0.18	0.00	0	8.25	0
26/03/2018 05:30	0.18	0.18	0.00	0	8.5	0

Benhall	
Area (km^2)	50.16
Total Rain (P) mm	40.4
Time Interval (hour)	0.25
Percentage Runoff	61%

Thorpeness	
Area (km^2)	50.16
Total Rain (P) mm	35.6
Time Interval (hour)	0.25
Percentage Runoff	70%

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
26/03/2018 05:45	0.18	0.18	0.00	0	8.75	0	
26/03/2018 06:00	0.18	0.18	0.00	0	9	0	
26/03/2018 06:15	0.18	0.18	0.00	0	9.25	0	
26/03/2018 06:30	0.18	0.18	0.00	0	9.5	0	
26/03/2018 06:45	0.18	0.18	0.00	0	9.75	0	
26/03/2018 07:00	0.18	0.18	0.00	0	10	0	
26/03/2018 07:15	0.18	0.18	0.00	0	10.25	0	
26/03/2018 07:30	0.18	0.18	0.00	0	10.5	0	
26/03/2018 07:45	0.18	0.18	0.00	0	10.75	0	
26/03/2018 08:00	0.18	0.18	0.00	0	11	0	
26/03/2018 08:15	0.18	0.18	0.00	0	11.25	0	
26/03/2018 08:30	0.18	0.18	0.00	0	11.5	0	
26/03/2018 08:45	0.18	0.18	0.00	0	11.75	0	
26/03/2018 09:00	0.18	0.18	0.00	0	12	0	
26/03/2018 09:15	0.18	0.18	0.00	0	12.25	0	
26/03/2018 09:30	0.18	0.18	0.00	0	12.5	0	
26/03/2018 09:45	0.18	0.18	0.00	0	12.75	0	
26/03/2018 10:00	0.18	0.18	0.00	0	13	0	
26/03/2018 10:15	0.18	0.18	0.00	0	13.25	0	
26/03/2018 10:30	0.18	0.18	0.00	0	13.5	0	
26/03/2018 10:45	0.18	0.18	0.00	0	13.75	0	
26/03/2018 11:00	0.18	0.18	0.00	0	14	0	
26/03/2018 11:15	0.18	0.18	0.00	0	14.25	0	
26/03/2018 11:30	0.18	0.18	0.00	0	14.5	0	
26/03/2018 11:45	0.18	0.18	0.00	0	14.75	0	
26/03/2018 12:00	0.18	0.18	0.00	0	15	0	
26/03/2018 12:15	0.18	0.18	0.00	0	15.25	0	
26/03/2018 12:30	0.18	0.18	0.00	0	15.5	0	
26/03/2018 12:45	0.18	0.18	0.00	0	15.75	0	
26/03/2018 13:00	0.18	0.18	0.00	0	16	0	
26/03/2018 13:15	0.18	0.18	0.00	0	16.25	0	
26/03/2018 13:30	0.18	0.18	0.00	0	16.5	0	
26/03/2018 13:45	0.18	0.18	0.00	0	16.75	0	
26/03/2018 14:00	0.18	0.18	0.00	0	17	0	
26/03/2018 14:15	0.18	0.18	0.00	0	17.25	0	
26/03/2018 14:30	0.18	0.18	0.00	0	17.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
26/03/2018 14:45	0.18	0.18	0.00	0	17.75	0	
26/03/2018 15:00	0.18	0.18	0.00	0	18	0	
26/03/2018 15:15	0.18	0.18	0.00	0	18.25	0	
26/03/2018 15:30	0.18	0.18	0.00	0	18.5	0	
26/03/2018 15:45	0.18	0.18	0.00	0	18.75	0	
26/03/2018 16:00	0.18	0.18	0.00	0	19	0	
26/03/2018 16:15	0.18	0.18	0.00	0	19.25	0	
26/03/2018 16:30	0.18	0.18	0.00	0	19.5	0	
26/03/2018 16:45	0.18	0.18	0.00	0	19.75	0	
26/03/2018 17:00	0.18	0.18	0.00	0	20	0	
26/03/2018 17:15	0.18	0.18	0.00	0	20.25	0	
26/03/2018 17:30	0.18	0.18	0.00	0	20.5	0	
26/03/2018 17:45	0.18	0.18	0.00	0	20.75	0	
26/03/2018 18:00	0.18	0.18	0.00	0	21	0	
26/03/2018 18:15	0.18	0.18	0.00	0	21.25	0	
26/03/2018 18:30	0.18	0.18	0.00	0	21.5	0	
26/03/2018 18:45	0.18	0.18	0.00	0	21.75	0	
26/03/2018 19:00	0.18	0.18	0.00	0	22	0	
26/03/2018 19:15	0.18	0.18	0.00	0	22.25	0	
26/03/2018 19:30	0.18	0.18	0.00	0	22.5	0	
26/03/2018 19:45	0.18	0.18	0.00	0	22.75	0	
26/03/2018 20:00	0.18	0.18	0.00	0	23	0	
26/03/2018 20:15	0.18	0.18	0.00	0	23.25	0	
26/03/2018 20:30	0.18	0.18	0.00	0	23.5	0	
26/03/2018 20:45	0.18	0.18	0.00	0	23.75	0	
26/03/2018 21:00	0.18	0.18	0.00	0	24	0	
26/03/2018 21:15	0.18	0.18	0.00	0	24.25	0	
26/03/2018 21:30	0.18	0.18	0.00	0	24.5	0	
26/03/2018 21:45	0.18	0.18	0.00	0	24.75	0	
26/03/2018 22:00	0.18	0.18	0.00	0	25	0	
26/03/2018 22:15	0.18	0.18	0.00	0	25.25	0	
26/03/2018 22:30	0.18	0.18	0.00	0	25.5	0	
26/03/2018 22:45	0.18	0.18	0.00	0	25.75	0	
26/03/2018 23:00	0.18	0.18	0.00	0	26	0	
26/03/2018 23:15	0.18	0.18	0.00	0	26.25	0	
26/03/2018 23:30	0.18	0.18	0.00	0	26.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
26/03/2018 23:45	0.18	0.18	0.00	0	26.75	0	
27/03/2018 00:00	0.18	0.18	0.00	0	27	0	
27/03/2018 00:15	0.18	0.18	0.00	0	27.25	0	
27/03/2018 00:30	0.18	0.18	0.00	0	27.5	0	
27/03/2018 00:45	0.18	0.18	0.00	0	27.75	0	
27/03/2018 01:00	0.18	0.18	0.00	0	28	0	
27/03/2018 01:15	0.18	0.18	0.00	0	28.25	0	
27/03/2018 01:30	0.18	0.18	0.00	0	28.5	0	
27/03/2018 01:45	0.18	0.18	0.00	0	28.75	0	
27/03/2018 02:00	0.18	0.18	0.00	0	29	0	
27/03/2018 02:15	0.18	0.18	0.00	0	29.25	0	
27/03/2018 02:30	0.18	0.18	0.00	0	29.5	0	
27/03/2018 02:45	0.18	0.18	0.00	0	29.75	0	
27/03/2018 03:00	0.18	0.18	0.00	0	30	0	
27/03/2018 03:15	0.18	0.18	0.00	0	30.25	0	
27/03/2018 03:30	0.18	0.18	0.00	0	30.5	0	
27/03/2018 03:45	0.18	0.18	0.00	0	30.75	0	
27/03/2018 04:00	0.18	0.18	0.00	0	31	0	
27/03/2018 04:15	0.18	0.18	0.00	0	31.25	0	
27/03/2018 04:30	0.18	0.18	0.00	0	31.5	0	
27/03/2018 04:45	0.18	0.18	0.00	0	31.75	0	
27/03/2018 05:00	0.18	0.18	0.00	0	32	0	
27/03/2018 05:15	0.18	0.18	0.00	0	32.25	0	
27/03/2018 05:30	0.18	0.18	0.00	0	32.5	0	
27/03/2018 05:45	0.18	0.18	0.00	0	32.75	0	
27/03/2018 06:00	0.18	0.18	0.00	0	33	0	
27/03/2018 06:15	0.18	0.18	0.00	0	33.25	0	
27/03/2018 06:30	0.18	0.18	0.00	0	33.5	0	
27/03/2018 06:45	0.18	0.18	0.00	0	33.75	0	
27/03/2018 07:00	0.18	0.18	0.00	0	34	0	
27/03/2018 07:15	0.18	0.18	0.00	0.2	34.25	0	
27/03/2018 07:30	0.18	0.18	0.00	0	34.5	0.2	
27/03/2018 07:45	0.18	0.18	0.00	0	34.75	0	
27/03/2018 08:00	0.18	0.18	0.00	0	35	0	
27/03/2018 08:15	0.18	0.18	0.00	0	35.25	0	
27/03/2018 08:30	0.18	0.18	0.00	0	35.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
27/03/2018 08:45	0.18	0.18	0.00	0	35.75	0	
27/03/2018 09:00	0.18	0.18	0.00	0	36	0	
27/03/2018 09:15	0.18	0.18	0.00	0	36.25	0	
27/03/2018 09:30	0.18	0.18	0.00	0	36.5	0	
27/03/2018 09:45	0.18	0.18	0.00	0	36.75	0	
27/03/2018 10:00	0.18	0.18	0.00	0	37	0	
27/03/2018 10:15	0.18	0.18	0.00	0	37.25	0	
27/03/2018 10:30	0.18	0.18	0.00	0.2	37.5	0.2	
27/03/2018 10:45	0.18	0.18	0.00	0	37.75	0	
27/03/2018 11:00	0.18	0.18	0.00	0	38	0	
27/03/2018 11:15	0.18	0.18	0.00	0	38.25	0	
27/03/2018 11:30	0.18	0.18	0.00	0	38.5	0	
27/03/2018 11:45	0.18	0.18	0.00	0	38.75	0	
27/03/2018 12:00	0.18	0.18	0.00	0.2	39	0	
27/03/2018 12:15	0.18	0.18	0.00	0	39.25	0	
27/03/2018 12:30	0.18	0.18	0.00	0	39.5	0	
27/03/2018 12:45	0.18	0.18	0.00	0	39.75	0	
27/03/2018 13:00	0.18	0.18	0.00	0	40	0	
27/03/2018 13:15	0.18	0.18	0.00	0	40.25	0	
27/03/2018 13:30	0.19	0.19	0.00	0	40.5	0	
27/03/2018 13:45	0.19	0.19	0.00	0	40.75	0	
27/03/2018 14:00	0.19	0.19	0.00	0	41	0	
27/03/2018 14:15	0.19	0.19	0.00	0	41.25	0	
27/03/2018 14:30	0.19	0.19	0.00	0	41.5	0	
27/03/2018 14:45	0.19	0.19	0.00	0	41.75	0	
27/03/2018 15:00	0.19	0.19	0.00	0	42	0	
27/03/2018 15:15	0.19	0.19	0.00	0	42.25	0	
27/03/2018 15:30	0.19	0.19	0.00	0	42.5	0	
27/03/2018 15:45	0.19	0.19	0.00	0	42.75	0	
27/03/2018 16:00	0.19	0.19	0.00	0	43	0	
27/03/2018 16:15	0.19	0.19	0.00	0	43.25	0	
27/03/2018 16:30	0.19	0.19	0.00	0	43.5	0	
27/03/2018 16:45	0.19	0.19	0.00	0	43.75	0	
27/03/2018 17:00	0.18	0.18	0.00	0	44	0	
27/03/2018 17:15	0.18	0.18	0.00	0	44.25	0	
27/03/2018 17:30	0.18	0.18	0.00	0	44.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
27/03/2018 17:45	0.18	0.18	0.00	0	44.75	0	
27/03/2018 18:00	0.18	0.18	0.00	0	45	0	
27/03/2018 18:15	0.18	0.18	0.00	0.2	45.25	0	
27/03/2018 18:30	0.18	0.18	0.00	0.2	45.5	0.2	
27/03/2018 18:45	0.18	0.18	0.00	0	45.75	0	
27/03/2018 19:00	0.18	0.18	0.00	0	46	0	
27/03/2018 19:15	0.18	0.18	0.00	0	46.25	0	
27/03/2018 19:30	0.18	0.18	0.00	0	46.5	0	
27/03/2018 19:45	0.18	0.18	0.00	0	46.75	0	
27/03/2018 20:00	0.19	0.19	0.00	0	47	0	
27/03/2018 20:15	0.19	0.19	0.00	0	47.25	0	
27/03/2018 20:30	0.19	0.19	0.00	0	47.5	0	
27/03/2018 20:45	0.19	0.19	0.00	0	47.75	0	
27/03/2018 21:00	0.19	0.19	0.00	0	48	0	
27/03/2018 21:15	0.19	0.19	0.00	0	48.25	0	
27/03/2018 21:30	0.19	0.19	0.00	0	48.5	0	
27/03/2018 21:45	0.19	0.19	0.00	0	48.75	0	
27/03/2018 22:00	0.19	0.19	0.00	0	49	0	
27/03/2018 22:15	0.19	0.19	0.00	0	49.25	0	
27/03/2018 22:30	0.19	0.19	0.00	0	49.5	0	
27/03/2018 22:45	0.19	0.19	0.00	0	49.75	0	
27/03/2018 23:00	0.19	0.19	0.00	0	50	0	
27/03/2018 23:15	0.19	0.19	0.00	0	50.25	0	
27/03/2018 23:30	0.19	0.19	0.00	0	50.5	0	
27/03/2018 23:45	0.19	0.19	0.00	0	50.75	0	
28/03/2018 00:00	0.19	0.19	0.00	0	51	0	
28/03/2018 00:15	0.19	0.19	0.00	0	51.25	0	
28/03/2018 00:30	0.19	0.19	0.00	0	51.5	0	
28/03/2018 00:45	0.19	0.19	0.00	0	51.75	0	
28/03/2018 01:00	0.19	0.19	0.00	0	52	0	
28/03/2018 01:15	0.19	0.19	0.00	0	52.25	0	
28/03/2018 01:30	0.19	0.19	0.00	0	52.5	0	
28/03/2018 01:45	0.19	0.19	0.00	0	52.75	0	
28/03/2018 02:00	0.19	0.19	0.00	0	53	0	
28/03/2018 02:15	0.19	0.19	0.00	0	53.25	0	
28/03/2018 02:30	0.19	0.19	0.00	0	53.5	0	

		Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
28/03/2018 02:45	0.19	0.19	0.00	0	53.75	0	
28/03/2018 03:00	0.19	0.19	0.00	0	54	0	
28/03/2018 03:15	0.19	0.19	0.00	0	54.25	0	
28/03/2018 03:30	0.19	0.19	0.00	0	54.5	0	
28/03/2018 03:45	0.19	0.19	0.00	0	54.75	0	
28/03/2018 04:00	0.19	0.19	0.00	0	55	0	
28/03/2018 04:15	0.19	0.19	0.00	0	55.25	0	
28/03/2018 04:30	0.19	0.19	0.00	0	55.5	0	
28/03/2018 04:45	0.19	0.19	0.00	0	55.75	0	
28/03/2018 05:00	0.19	0.19	0.00	0	56	0	
28/03/2018 05:15	0.19	0.19	0.00	0	56.25	0	
28/03/2018 05:30	0.19	0.19	0.00	0	56.5	0	
28/03/2018 05:45	0.19	0.19	0.00	0	56.75	0	
28/03/2018 06:00	0.19	0.19	0.00	0	57	0	
28/03/2018 06:15	0.19	0.19	0.00	0	57.25	0	
28/03/2018 06:30	0.19	0.19	0.00	0	57.5	0	
28/03/2018 06:45	0.19	0.19	0.00	0	57.75	0	
28/03/2018 07:00	0.19	0.19	0.00	0	58	0	
28/03/2018 07:15	0.19	0.19	0.00	0	58.25	0	
28/03/2018 07:30	0.19	0.19	0.00	0	58.5	0	
28/03/2018 07:45	0.19	0.19	0.00	0	58.75	0	
28/03/2018 08:00	0.19	0.19	0.00	0.2	59	0.2	
28/03/2018 08:15	0.19	0.19	0.00	0.2	59.25	0	
28/03/2018 08:30	0.19	0.19	0.00	0.2	59.5	0.2	
28/03/2018 08:45	0.19	0.19	0.00	0	59.75	0.2	
28/03/2018 09:00	0.19	0.19	0.00	0.2	60	0	
28/03/2018 09:15	0.19	0.19	0.00	0	60.25	0.4	
28/03/2018 09:30	0.19	0.19	0.00	0	60.5	0.2	
28/03/2018 09:45	0.19	0.19	0.00	0.2	60.75	0.2	
28/03/2018 10:00	0.19	0.19	0.00	0	61	0.2	
28/03/2018 10:15	0.19	0.19	0.00	0	61.25	0	
28/03/2018 10:30	0.19	0.19	0.00	0.2	61.5	0.2	
28/03/2018 10:45	0.19	0.19	0.00	0.4	61.75	0.2	
28/03/2018 11:00	0.19	0.19	0.00	0.4	62	0.4	
28/03/2018 11:15	0.19	0.19	0.00	0.2	62.25	0.4	
28/03/2018 11:30	0.19	0.19	0.00	0.2	62.5	0.2	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
28/03/2018 11:45	0.19	0.19	0.00	0.2	62.75	0.4	
28/03/2018 12:00	0.19	0.19	0.00	0.2	63	0.2	
28/03/2018 12:15	0.19	0.19	0.00	0.2	63.25	0.4	
28/03/2018 12:30	0.20	0.20	0.00	0.2	63.5	0.4	
28/03/2018 12:45	0.20	0.20	0.00	0.4	63.75	0.4	
28/03/2018 13:00	0.20	0.20	0.00	0.2	64	0.2	
28/03/2018 13:15	0.20	0.20	0.00	0.2	64.25	0.2	
28/03/2018 13:30	0.20	0.20	0.00	0.2	64.5	0.2	
28/03/2018 13:45	0.20	0.20	0.00	0.2	64.75	0.4	
28/03/2018 14:00	0.20	0.20	0.00	0.2	65	0.2	
28/03/2018 14:15	0.21	0.21	0.00	0.4	65.25	0.2	
28/03/2018 14:30	0.21	0.21	0.00	0.2	65.5	0.6	
28/03/2018 14:45	0.21	0.21	0.00	0.4	65.75	0.4	
28/03/2018 15:00	0.21	0.21	0.00	0.2	66	0.2	
28/03/2018 15:15	0.22	0.22	0.00	0	66.25	0.2	
28/03/2018 15:30	0.22	0.22	0.00	0.2	66.5	0	
28/03/2018 15:45	0.22	0.22	0.00	0	66.75	0	
28/03/2018 16:00	0.22	0.22	0.00	0	67	0	
28/03/2018 16:15	0.22	0.22	0.00	0	67.25	0	
28/03/2018 16:30	0.22	0.22	0.00	0	67.5	0	
28/03/2018 16:45	0.22	0.22	0.00	0	67.75	0	
28/03/2018 17:00	0.23	0.23	0.00	0	68	0	
28/03/2018 17:15	0.23	0.23	0.00	0	68.25	0	
28/03/2018 17:30	0.23	0.23	0.00	0	68.5	0	
28/03/2018 17:45	0.23	0.23	0.00	0	68.75	0	
28/03/2018 18:00	0.23	0.23	0.00	0	69	0	
28/03/2018 18:15	0.23	0.23	0.00	0	69.25	0	
28/03/2018 18:30	0.23	0.23	0.00	0	69.5	0	
28/03/2018 18:45	0.23	0.23	0.00	0	69.75	0	
28/03/2018 19:00	0.23	0.23	0.00	0	70	0	
28/03/2018 19:15	0.23	0.23	0.00	0	70.25	0	
28/03/2018 19:30	0.23	0.23	0.00	0	70.5	0	
28/03/2018 19:45	0.23	0.23	0.00	0	70.75	0	
28/03/2018 20:00	0.23	0.23	0.00	0	71	0	
28/03/2018 20:15	0.23	0.23	0.00	0	71.25	0	
28/03/2018 20:30	0.23	0.23	0.00	0	71.5	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
28/03/2018 20:45	0.24	0.24	0.00	0	71.75	0	
28/03/2018 21:00	0.24	0.24	0.00	0	72	0	
28/03/2018 21:15	0.24	0.24	0.00	0	72.25	0	
28/03/2018 21:30	0.24	0.24	0.00	0	72.5	0	
28/03/2018 21:45	0.24	0.24	0.00	0	72.75	0	
28/03/2018 22:00	0.24	0.24	0.00	0	73	0	
28/03/2018 22:15	0.24	0.24	0.00	0	73.25	0	
28/03/2018 22:30	0.24	0.24	0.00	0	73.5	0	
28/03/2018 22:45	0.25	0.25	0.00	0	73.75	0	
28/03/2018 23:00	0.25	0.25	0.00	0	74	0	
28/03/2018 23:15	0.26	0.26	0.00	0	74.25	0	
28/03/2018 23:30	0.26	0.26	0.00	0	74.5	0	
28/03/2018 23:45	0.27	0.27	0.00	0	74.75	0	
29/03/2018 00:00	0.27	0.27	0.00	0	75	0	
29/03/2018 00:15	0.28	0.28	0.00	0	75.25	0	
29/03/2018 00:30	0.28	0.28	0.00	0	75.5	0	
29/03/2018 00:45	0.29	0.29	0.00	0	75.75	0	
29/03/2018 01:00	0.29	0.29	0.00	0	76	0	
29/03/2018 01:15	0.29	0.29	0.00	0	76.25	0	
29/03/2018 01:30	0.29	0.29	0.00	0	76.5	0.2	
29/03/2018 01:45	0.30	0.30	0.00	0	76.75	0	
29/03/2018 02:00	0.30	0.30	0.00	0	77	0	
29/03/2018 02:15	0.30	0.30	0.00	0	77.25	0	
29/03/2018 02:30	0.30	0.30	0.00	0	77.5	0	
29/03/2018 02:45	0.31	0.31	0.00	0	77.75	0	
29/03/2018 03:00	0.31	0.31	0.00	0	78	0	
29/03/2018 03:15	0.31	0.31	0.00	0	78.25	0	
29/03/2018 03:30	0.31	0.31	0.00	0	78.5	0	
29/03/2018 03:45	0.31	0.31	0.00	0	78.75	0	
29/03/2018 04:00	0.31	0.31	0.00	0	79	0	
29/03/2018 04:15	0.31	0.31	0.00	0	79.25	0	
29/03/2018 04:30	0.31	0.31	0.00	0	79.5	0	
29/03/2018 04:45	0.31	0.31	0.00	0	79.75	0	
29/03/2018 05:00	0.31	0.31	0.00	0	80	0	
29/03/2018 05:15	0.31	0.31	0.00	0	80.25	0	
29/03/2018 05:30	0.31	0.31	0.00	0	80.5	0	

		Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)	Benhall
29/03/2018 05:45	0.31	0.31	0.00		0	80.75	0	
29/03/2018 06:00	0.31	0.31	0.00		0	81	0	
29/03/2018 06:15	0.31	0.31	0.00		0	81.25	0	
29/03/2018 06:30	0.30	0.30	0.00		0	81.5	0	
29/03/2018 06:45	0.30	0.30	0.00		0	81.75	0	
29/03/2018 07:00	0.30	0.30	0.00		0	82	0	
29/03/2018 07:15	0.30	0.30	0.00		0	82.25	0	
29/03/2018 07:30	0.30	0.30	0.00		0	82.5	0	
29/03/2018 07:45	0.30	0.30	0.00		0	82.75	0	
29/03/2018 08:00	0.30	0.30	0.00		0	83	0	
29/03/2018 08:15	0.30	0.30	0.00		0	83.25	0	
29/03/2018 08:30	0.30	0.30	0.00		0	83.5	0	
29/03/2018 08:45	0.30	0.30	0.00		0	83.75	0	
29/03/2018 09:00	0.30	0.30	0.00		0	84	0	
29/03/2018 09:15	0.30	0.30	0.00		0	84.25	0	
29/03/2018 09:30	0.30	0.30	0.00		0	84.5	0	
29/03/2018 09:45	0.30	0.30	0.00		0	84.75	0	
29/03/2018 10:00	0.30	0.30	0.00		0	85	0	
29/03/2018 10:15	0.30	0.30	0.00		0	85.25	0	
29/03/2018 10:30	0.30	0.30	0.00		0	85.5	0	
29/03/2018 10:45	0.30	0.30	0.00		0	85.75	0	
29/03/2018 11:00	0.29	0.29	0.00		0	86	0	
29/03/2018 11:15	0.29	0.29	0.00		0	86.25	0	
29/03/2018 11:30	0.29	0.29	0.00		0	86.5	0	
29/03/2018 11:45	0.29	0.29	0.00		0	86.75	0	
29/03/2018 12:00	0.29	0.29	0.00		0	87	0	
29/03/2018 12:15	0.29	0.29	0.00		0	87.25	0	
29/03/2018 12:30	0.29	0.29	0.00		0	87.5	0	
29/03/2018 12:45	0.29	0.29	0.00		0	87.75	0	
29/03/2018 13:00	0.29	0.29	0.00		0	88	0	
29/03/2018 13:15	0.29	0.29	0.00		0	88.25	0	
29/03/2018 13:30	0.29	0.29	0.00		0	88.5	0	
29/03/2018 13:45	0.29	0.29	0.00		0	88.75	0	
29/03/2018 14:00	0.29	0.29	0.00		0	89	0	
29/03/2018 14:15	0.29	0.29	0.00		0	89.25	0	
29/03/2018 14:30	0.29	0.29	0.00		0	89.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
29/03/2018 14:45	0.29	0.29	0.00	0	89.75	0	
29/03/2018 15:00	0.29	0.29	0.00	0	90	0	
29/03/2018 15:15	0.29	0.29	0.00	0	90.25	0	
29/03/2018 15:30	0.29	0.29	0.00	0	90.5	0	
29/03/2018 15:45	0.29	0.29	0.00	0	90.75	0	
29/03/2018 16:00	0.29	0.29	0.00	0	91	0	
29/03/2018 16:15	0.29	0.29	0.00	0	91.25	0	
29/03/2018 16:30	0.29	0.29	0.00	0.2	91.5	0	
29/03/2018 16:45	0.29	0.29	0.00	0.2	91.75	0.2	
29/03/2018 17:00	0.29	0.29	0.00	0	92	0	
29/03/2018 17:15	0.29	0.29	0.00	0.2	92.25	0.2	
29/03/2018 17:30	0.29	0.29	0.00	0.2	92.5	0.2	
29/03/2018 17:45	0.29	0.29	0.00	0.2	92.75	0	
29/03/2018 18:00	0.29	0.29	0.00	0	93	0	
29/03/2018 18:15	0.29	0.29	0.00	0.2	93.25	0.4	
29/03/2018 18:30	0.29	0.29	0.00	0.8	93.5	0.8	
29/03/2018 18:45	0.29	0.29	0.00	0.6	93.75	0.6	
29/03/2018 19:00	0.29	0.29	0.00	0.4	94	0.4	
29/03/2018 19:15	0.29	0.29	0.00	0.2	94.25	0.6	
29/03/2018 19:30	0.29	0.29	0.00	0.2	94.5	0	
29/03/2018 19:45	0.29	0.29	0.00	0	94.75	0	
29/03/2018 20:00	0.29	0.29	0.00	0	95	0	
29/03/2018 20:15	0.29	0.29	0.00	0	95.25	0	
29/03/2018 20:30	0.29	0.29	0.00	0	95.5	0	
29/03/2018 20:45	0.29	0.29	0.00	0	95.75	0	
29/03/2018 21:00	0.29	0.29	0.00	0	96	0	
29/03/2018 21:15	0.29	0.29	0.00	0	96.25	0	
29/03/2018 21:30	0.29	0.29	0.00	0	96.5	0	
29/03/2018 21:45	0.29	0.29	0.00	0	96.75	0	
29/03/2018 22:00	0.30	0.30	0.00	0	97	0	
29/03/2018 22:15	0.30	0.30	0.00	0	97.25	0	
29/03/2018 22:30	0.30	0.30	0.00	0	97.5	0	
29/03/2018 22:45	0.30	0.30	0.00	0	97.75	0.4	
29/03/2018 23:00	0.31	0.31	0.00	0	98	0.4	
29/03/2018 23:15	0.31	0.31	0.00	0	98.25	0	
29/03/2018 23:30	0.31	0.31	0.00	0	98.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
29/03/2018 23:45	0.31	0.31	0.00	0	98.75	0.2	
30/03/2018 00:00	0.31	0.31	0.00	0	99	0	
30/03/2018 00:15	0.31	0.31	0.00	0	99.25	0	
30/03/2018 00:30	0.31	0.31	0.00	0.2	99.5	0	
30/03/2018 00:45	0.31	0.31	0.00	0	99.75	0	
30/03/2018 01:00	0.31	0.31	0.00	0	100	0	
30/03/2018 01:15	0.31	0.31	0.00	0	100.25	0	
30/03/2018 01:30	0.31	0.31	0.00	0	100.5	0	
30/03/2018 01:45	0.31	0.31	0.00	0	100.75	0	
30/03/2018 02:00	0.31	0.31	0.00	0	101	0	
30/03/2018 02:15	0.31	0.31	0.00	0	101.25	0	
30/03/2018 02:30	0.31	0.31	0.00	0	101.5	0	
30/03/2018 02:45	0.32	0.32	0.00	0	101.75	0	
30/03/2018 03:00	0.32	0.32	0.00	0	102	0	
30/03/2018 03:15	0.33	0.33	0.00	0	102.25	0	
30/03/2018 03:30	0.33	0.33	0.00	0	102.5	0	
30/03/2018 03:45	0.34	0.34	0.00	0	102.75	0	
30/03/2018 04:00	0.34	0.34	0.00	0	103	0	
30/03/2018 04:15	0.34	0.34	0.00	0	103.25	0	
30/03/2018 04:30	0.34	0.34	0.00	0	103.5	0	
30/03/2018 04:45	0.35	0.35	0.00	0	103.75	0.2	
30/03/2018 05:00	0.35	0.35	0.00	0	104	0	
30/03/2018 05:15	0.35	0.35	0.00	0	104.25	0	
30/03/2018 05:30	0.35	0.35	0.00	0	104.5	0	
30/03/2018 05:45	0.36	0.35	0.01	0	104.75	0	
30/03/2018 06:00	0.36	0.35	0.01	0	105	0	
30/03/2018 06:15	0.36	0.35	0.01	0	105.25	0	
30/03/2018 06:30	0.36	0.35	0.01	0	105.5	0	
30/03/2018 06:45	0.36	0.35	0.01	0	105.75	0	
30/03/2018 07:00	0.36	0.35	0.01	0	106	0	
30/03/2018 07:15	0.36	0.35	0.01	0	106.25	0	
30/03/2018 07:30	0.36	0.35	0.01	0	106.5	0	
30/03/2018 07:45	0.36	0.35	0.01	0	106.75	0	
30/03/2018 08:00	0.36	0.35	0.01	0	107	0	
30/03/2018 08:15	0.36	0.35	0.01	0	107.25	0	
30/03/2018 08:30	0.36	0.35	0.01	0	107.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
30/03/2018 08:45	0.36	0.35	0.01	0	107.75	0	
30/03/2018 09:00	0.36	0.35	0.01	0	108	0	
30/03/2018 09:15	0.36	0.35	0.01	0	108.25	0	
30/03/2018 09:30	0.36	0.35	0.01	0	108.5	0	
30/03/2018 09:45	0.36	0.35	0.01	0	108.75	0	
30/03/2018 10:00	0.36	0.35	0.01	0	109	0	
30/03/2018 10:15	0.36	0.35	0.01	0	109.25	0	
30/03/2018 10:30	0.36	0.35	0.01	0	109.5	0	
30/03/2018 10:45	0.36	0.35	0.01	0	109.75	0	
30/03/2018 11:00	0.36	0.35	0.01	0	110	0	
30/03/2018 11:15	0.36	0.35	0.01	0	110.25	0	
30/03/2018 11:30	0.36	0.35	0.01	0	110.5	0	
30/03/2018 11:45	0.36	0.35	0.01	0	110.75	0	
30/03/2018 12:00	0.36	0.35	0.01	0	111	0	
30/03/2018 12:15	0.36	0.35	0.01	0	111.25	0	
30/03/2018 12:30	0.36	0.35	0.01	0	111.5	0	
30/03/2018 12:45	0.36	0.35	0.01	0	111.75	0	
30/03/2018 13:00	0.36	0.35	0.01	0	112	0	
30/03/2018 13:15	0.36	0.35	0.01	0	112.25	0	
30/03/2018 13:30	0.36	0.35	0.01	0	112.5	0	
30/03/2018 13:45	0.36	0.35	0.01	0	112.75	0	
30/03/2018 14:00	0.36	0.35	0.01	0.2	113	0.2	
30/03/2018 14:15	0.36	0.35	0.01	0.2	113.25	0.2	
30/03/2018 14:30	0.36	0.35	0.01	0.6	113.5	0.6	
30/03/2018 14:45	0.36	0.35	0.01	0.6	113.75	0	
30/03/2018 15:00	0.36	0.35	0.01	0	114	0.2	
30/03/2018 15:15	0.36	0.35	0.01	0.4	114.25	0	
30/03/2018 15:30	0.36	0.35	0.01	0.2	114.5	0.2	
30/03/2018 15:45	0.36	0.35	0.01	0	114.75	0	
30/03/2018 16:00	0.36	0.35	0.01	0.4	115	0	
30/03/2018 16:15	0.36	0.35	0.01	0.2	115.25	0.2	
30/03/2018 16:30	0.36	0.35	0.01	0	115.5	0	
30/03/2018 16:45	0.36	0.35	0.01	0.4	115.75	0.2	
30/03/2018 17:00	0.37	0.35	0.02	1	116	0.6	
30/03/2018 17:15	0.37	0.35	0.02	2	116.25	1.2	
30/03/2018 17:30	0.37	0.35	0.02	1.2	116.5	0.8	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
30/03/2018 17:45	0.38	0.35	0.03	0.2	116.75	0.4	
30/03/2018 18:00	0.39	0.35	0.04	0	117	0.2	
30/03/2018 18:15	0.40	0.35	0.05	0	117.25	0	
30/03/2018 18:30	0.41	0.35	0.06	0	117.5	0	
30/03/2018 18:45	0.42	0.35	0.07	0	117.75	0	
30/03/2018 19:00	0.42	0.35	0.07	0	118	0	
30/03/2018 19:15	0.43	0.35	0.08	0.4	118.25	0.2	
30/03/2018 19:30	0.44	0.35	0.09	0	118.5	0.2	
30/03/2018 19:45	0.45	0.35	0.10	0.6	118.75	0.2	
30/03/2018 20:00	0.47	0.35	0.12	0.4	119	0.4	
30/03/2018 20:15	0.50	0.35	0.15	0.6	119.25	0.6	
30/03/2018 20:30	0.53	0.35	0.18	0.2	119.5	0	
30/03/2018 20:45	0.59	0.35	0.24	0.2	119.75	0.2	
30/03/2018 21:00	0.67	0.35	0.32	0	120	0	
30/03/2018 21:15	0.78	0.35	0.43	0	120.25	0	
30/03/2018 21:30	0.89	0.35	0.54	0	120.5	0	
30/03/2018 21:45	1.04	0.35	0.69	0	120.75	0	
30/03/2018 22:00	1.15	0.35	0.80	0	121	0	
30/03/2018 22:15	1.22	0.35	0.87	0	121.25	0	
30/03/2018 22:30	1.32	0.35	0.97	0	121.5	0	
30/03/2018 22:45	1.41	0.35	1.06	0	121.75	0	
30/03/2018 23:00	1.50	0.35	1.15	0	122	0	
30/03/2018 23:15	1.58	0.35	1.23	0	122.25	0	
30/03/2018 23:30	1.67	0.35	1.32	0	122.5	0	
30/03/2018 23:45	1.77	0.35	1.42	0	122.75	0	
31/03/2018 00:00	1.86	0.35	1.51	0	123	0	
31/03/2018 00:15	1.95	0.35	1.60	0	123.25	0	
31/03/2018 00:30	2.04	0.35	1.69	0	123.5	0	
31/03/2018 00:45	2.12	0.35	1.77	0	123.75	0	
31/03/2018 01:00	2.21	0.35	1.86	0	124	0	
31/03/2018 01:15	2.31	0.35	1.96	0	124.25	0	
31/03/2018 01:30	2.42	0.35	2.07	0	124.5	0	
31/03/2018 01:45	2.53	0.35	2.18	0	124.75	0	
31/03/2018 02:00	2.65	0.35	2.30	0	125	0	
31/03/2018 02:15	2.77	0.35	2.42	0	125.25	0	
31/03/2018 02:30	2.88	0.35	2.53	0	125.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
31/03/2018 02:45	3.00	0.35	2.65	0	125.75	0	
31/03/2018 03:00	3.11	0.35	2.76	0	126	0	
31/03/2018 03:15	3.21	0.35	2.86	0	126.25	0	
31/03/2018 03:30	3.30	0.35	2.95	0	126.5	0	
31/03/2018 03:45	3.41	0.35	3.06	0	126.75	0	
31/03/2018 04:00	3.48	0.35	3.13	0.2	127	0.2	
31/03/2018 04:15	3.54	0.35	3.19	0.2	127.25	0	
31/03/2018 04:30	3.58	0.35	3.23	0.2	127.5	0	
31/03/2018 04:45	3.63	0.35	3.28	0	127.75	0	
31/03/2018 05:00	3.66	0.35	3.31	0	128	0	
31/03/2018 05:15	3.69	0.35	3.34	0	128.25	0	
31/03/2018 05:30	3.71	0.35	3.36	0	128.5	0	
31/03/2018 05:45	3.73	0.35	3.38	0	128.75	0.2	
31/03/2018 06:00	3.75	0.35	3.40	0	129	0	
31/03/2018 06:15	3.76	0.35	3.41	0	129.25	0	
31/03/2018 06:30	3.77	0.35	3.42	0	129.5	0	
31/03/2018 06:45	3.78	0.35	3.43	0	129.75	0	
31/03/2018 07:00	3.79	0.35	3.44	0	130	0	
31/03/2018 07:15	3.80	0.35	3.45	0	130.25	0	
31/03/2018 07:30	3.80	0.35	3.45	0	130.5	0	
31/03/2018 07:45	3.80	0.35	3.45	0	130.75	0	
31/03/2018 08:00	3.80	0.35	3.45	0	131	0	
31/03/2018 08:15	3.79	0.35	3.44	0	131.25	0	
31/03/2018 08:30	3.77	0.35	3.42	0	131.5	0	
31/03/2018 08:45	3.76	0.35	3.41	0	131.75	0	
31/03/2018 09:00	3.75	0.35	3.40	0	132	0	
31/03/2018 09:15	3.73	0.35	3.38	0	132.25	0	
31/03/2018 09:30	3.70	0.35	3.35	0	132.5	0	
31/03/2018 09:45	3.66	0.35	3.31	0	132.75	0	
31/03/2018 10:00	3.63	0.35	3.28	0	133	0	
31/03/2018 10:15	3.59	0.35	3.24	0	133.25	0	
31/03/2018 10:30	3.54	0.35	3.19	0	133.5	0	
31/03/2018 10:45	3.48	0.35	3.13	0	133.75	0	
31/03/2018 11:00	3.39	0.35	3.04	0	134	0	
31/03/2018 11:15	3.31	0.35	2.96	0	134.25	0	
31/03/2018 11:30	3.21	0.35	2.86	0	134.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
31/03/2018 11:45	3.11	0.35	2.76	0	134.75	0	
31/03/2018 12:00	2.99	0.35	2.64	0	135	0	
31/03/2018 12:15	2.87	0.35	2.52	0	135.25	0	
31/03/2018 12:30	2.76	0.35	2.41	0	135.5	0	
31/03/2018 12:45	2.63	0.35	2.28	0	135.75	0	
31/03/2018 13:00	2.50	0.35	2.15	0	136	0	
31/03/2018 13:15	2.38	0.35	2.03	0	136.25	0	
31/03/2018 13:30	2.27	0.35	1.92	0	136.5	0	
31/03/2018 13:45	2.15	0.35	1.80	0	136.75	0	
31/03/2018 14:00	2.06	0.35	1.71	0	137	0	
31/03/2018 14:15	1.99	0.35	1.64	0	137.25	0	
31/03/2018 14:30	1.92	0.35	1.57	0	137.5	0	
31/03/2018 14:45	1.88	0.35	1.53	0	137.75	0	
31/03/2018 15:00	1.82	0.35	1.47	0	138	0	
31/03/2018 15:15	1.78	0.35	1.43	0	138.25	0	
31/03/2018 15:30	1.75	0.35	1.40	0	138.5	0	
31/03/2018 15:45	1.71	0.35	1.36	0	138.75	0	
31/03/2018 16:00	1.67	0.35	1.32	0	139	0	
31/03/2018 16:15	1.64	0.35	1.29	0	139.25	0	
31/03/2018 16:30	1.62	0.35	1.27	0.2	139.5	0	
31/03/2018 16:45	1.59	0.35	1.24	0.2	139.75	0	
31/03/2018 17:00	1.57	0.35	1.22	0.4	140	0.2	
31/03/2018 17:15	1.54	0.35	1.19	0.6	140.25	0	
31/03/2018 17:30	1.52	0.35	1.17	0.8	140.5	0	
31/03/2018 17:45	1.50	0.35	1.15	1	140.75	0	
31/03/2018 18:00	1.48	0.35	1.13	0.6	141	0.4	
31/03/2018 18:15	1.47	0.35	1.12	0.8	141.25	0.4	
31/03/2018 18:30	1.45	0.35	1.10	0.4	141.5	0.8	
31/03/2018 18:45	1.44	0.35	1.09	0.2	141.75	1.2	
31/03/2018 19:00	1.42	0.35	1.07	0	142	0.4	
31/03/2018 19:15	1.41	0.35	1.06	0	142.25	0.4	
31/03/2018 19:30	1.41	0.35	1.06	0	142.5	0	
31/03/2018 19:45	1.40	0.35	1.05	0.2	142.75	0	
31/03/2018 20:00	1.39	0.35	1.04	0	143	0	
31/03/2018 20:15	1.38	0.35	1.03	0	143.25	0	
31/03/2018 20:30	1.38	0.35	1.03	0	143.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
31/03/2018 20:45	1.38	0.35	1.03	0	143.75	0.2	
31/03/2018 21:00	1.38	0.35	1.03	0	144	0	
31/03/2018 21:15	1.38	0.35	1.03	0	144.25	0	
31/03/2018 21:30	1.38	0.35	1.03	0	144.5	0	
31/03/2018 21:45	1.39	0.35	1.04	0	144.75	0	
31/03/2018 22:00	1.41	0.35	1.06	0	145	0	
31/03/2018 22:15	1.42	0.35	1.07	0	145.25	0	
31/03/2018 22:30	1.45	0.35	1.10	0	145.5	0	
31/03/2018 22:45	1.48	0.35	1.13	0.2	145.75	0	
31/03/2018 23:00	1.52	0.35	1.17	0	146	0	
31/03/2018 23:15	1.56	0.35	1.21	0.4	146.25	0.2	
31/03/2018 23:30	1.61	0.35	1.26	0	146.5	0	
31/03/2018 23:45	1.66	0.35	1.31	0.2	146.75	0	
01/04/2018 00:00	1.71	0.35	1.36	0	147	0	
01/04/2018 00:15	1.76	0.35	1.41	0	147.25	0	
01/04/2018 00:30	1.80	0.35	1.45	0	147.5	0	
01/04/2018 00:45	1.85	0.35	1.50	0.2	147.75	0	
01/04/2018 01:00	1.90	0.35	1.55	0	148	0	
01/04/2018 01:15	1.95	0.35	1.60	0	148.25	0	
01/04/2018 01:30	2.01	0.35	1.66	0	148.5	0	
01/04/2018 01:45	2.06	0.35	1.71	0	148.75	0	
01/04/2018 02:00	2.12	0.35	1.77	0	149	0	
01/04/2018 02:15	2.18	0.35	1.83	0	149.25	0	
01/04/2018 02:30	2.24	0.35	1.89	0	149.5	0	
01/04/2018 02:45	2.31	0.35	1.96	0	149.75	0	
01/04/2018 03:00	2.38	0.35	2.03	0	150	0	
01/04/2018 03:15	2.46	0.35	2.11	0	150.25	0	
01/04/2018 03:30	2.54	0.35	2.19	0	150.5	0	
01/04/2018 03:45	2.61	0.35	2.26	0	150.75	0	
01/04/2018 04:00	2.69	0.35	2.34	0	151	0	
01/04/2018 04:15	2.77	0.35	2.42	0	151.25	0	
01/04/2018 04:30	2.84	0.35	2.49	0	151.5	0	
01/04/2018 04:45	2.90	0.35	2.55	0	151.75	0	
01/04/2018 05:00	2.97	0.35	2.62	0	152	0	
01/04/2018 05:15	3.02	0.35	2.67	0	152.25	0	
01/04/2018 05:30	3.08	0.35	2.73	0	152.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
01/04/2018 05:45	3.13	0.35	2.78	0	152.75	0	
01/04/2018 06:00	3.18	0.35	2.83	0	153	0	
01/04/2018 06:15	3.22	0.35	2.87	0	153.25	0	
01/04/2018 06:30	3.26	0.35	2.91	0	153.5	0	
01/04/2018 06:45	3.28	0.35	2.93	0	153.75	0	
01/04/2018 07:00	3.31	0.35	2.96	0	154	0	
01/04/2018 07:15	3.34	0.35	2.99	0	154.25	0	
01/04/2018 07:30	3.35	0.35	3.00	0	154.5	0	
01/04/2018 07:45	3.36	0.35	3.01	0	154.75	0	
01/04/2018 08:00	3.36	0.35	3.01	0	155	0	
01/04/2018 08:15	3.36	0.35	3.01	0	155.25	0	
01/04/2018 08:30	3.35	0.35	3.00	0	155.5	0	
01/04/2018 08:45	3.33	0.35	2.98	0	155.75	0	
01/04/2018 09:00	3.30	0.35	2.95	0	156	0	
01/04/2018 09:15	3.27	0.35	2.92	0	156.25	0	
01/04/2018 09:30	3.25	0.35	2.90	0	156.5	0	
01/04/2018 09:45	3.20	0.35	2.85	0	156.75	0	
01/04/2018 10:00	3.17	0.35	2.82	0	157	0	
01/04/2018 10:15	3.12	0.35	2.77	0	157.25	0	
01/04/2018 10:30	3.07	0.35	2.72	0	157.5	0	
01/04/2018 10:45	3.01	0.35	2.66	0	157.75	0	
01/04/2018 11:00	2.95	0.35	2.60	0	158	0	
01/04/2018 11:15	2.87	0.35	2.52	0	158.25	0	
01/04/2018 11:30	2.81	0.35	2.46	0	158.5	0	
01/04/2018 11:45	2.74	0.35	2.39	0	158.75	0	
01/04/2018 12:00	2.65	0.35	2.30	0	159	0	
01/04/2018 12:15	2.58	0.35	2.23	0	159.25	0	
01/04/2018 12:30	2.50	0.35	2.15	0	159.5	0	
01/04/2018 12:45	2.41	0.35	2.06	0	159.75	0	
01/04/2018 13:00	2.33	0.35	1.98	0	160	0	
01/04/2018 13:15	2.27	0.35	1.92	0	160.25	0	
01/04/2018 13:30	2.19	0.35	1.84	0	160.5	0	
01/04/2018 13:45	2.13	0.35	1.78	0	160.75	0	
01/04/2018 14:00	2.06	0.35	1.71	0	161	0	
01/04/2018 14:15	2.01	0.35	1.66	0	161.25	0	
01/04/2018 14:30	1.95	0.35	1.60	0	161.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
01/04/2018 14:45	1.92	0.35	1.57	0	161.75	0	
01/04/2018 15:00	1.88	0.35	1.53	0	162	0	
01/04/2018 15:15	1.84	0.35	1.49	0	162.25	0.2	
01/04/2018 15:30	1.81	0.35	1.46	0	162.5	0	
01/04/2018 15:45	1.77	0.35	1.42	0	162.75	0	
01/04/2018 16:00	1.75	0.35	1.40	0	163	0	
01/04/2018 16:15	1.72	0.35	1.37	0	163.25	0	
01/04/2018 16:30	1.70	0.35	1.35	0	163.5	0	
01/04/2018 16:45	1.67	0.35	1.32	0	163.75	0	
01/04/2018 17:00	1.65	0.35	1.30	0	164	0	
01/04/2018 17:15	1.63	0.35	1.28	0	164.25	0	
01/04/2018 17:30	1.61	0.35	1.26	0	164.5	0	
01/04/2018 17:45	1.59	0.35	1.24	0	164.75	0	
01/04/2018 18:00	1.58	0.35	1.23	0	165	0	
01/04/2018 18:15	1.56	0.35	1.21	0	165.25	0	
01/04/2018 18:30	1.54	0.35	1.19	0	165.5	0	
01/04/2018 18:45	1.53	0.35	1.18	0	165.75	0	
01/04/2018 19:00	1.51	0.35	1.16	0	166	0	
01/04/2018 19:15	1.51	0.35	1.16	0	166.25	0	
01/04/2018 19:30	1.49	0.35	1.14	0	166.5	0	
01/04/2018 19:45	1.49	0.35	1.14	0	166.75	0	
01/04/2018 20:00	1.48	0.35	1.13	0	167	0	
01/04/2018 20:15	1.47	0.35	1.12	0	167.25	0	
01/04/2018 20:30	1.47	0.35	1.12	0	167.5	0	
01/04/2018 20:45	1.47	0.35	1.12	0	167.75	0	
01/04/2018 21:00	1.47	0.35	1.12	0	168	0	
01/04/2018 21:15	1.48	0.35	1.13	0	168.25	0	
01/04/2018 21:30	1.49	0.35	1.14	0	168.5	0	
01/04/2018 21:45	1.50	0.35	1.15	0	168.75	0	
01/04/2018 22:00	1.51	0.35	1.16	0	169	0	
01/04/2018 22:15	1.52	0.35	1.17	0	169.25	0	
01/04/2018 22:30	1.54	0.35	1.19	0	169.5	0	
01/04/2018 22:45	1.55	0.35	1.20	0	169.75	0	
01/04/2018 23:00	1.56	0.35	1.21	0	170	0	
01/04/2018 23:15	1.58	0.35	1.23	0	170.25	0	
01/04/2018 23:30	1.59	0.35	1.24	0	170.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
01/04/2018 23:45	1.61	0.35	1.26	0	170.75	0	
02/04/2018 00:00	1.62	0.35	1.27	0	171	0	
02/04/2018 00:15	1.63	0.35	1.28	0	171.25	0	
02/04/2018 00:30	1.65	0.35	1.30	0.2	171.5	0	
02/04/2018 00:45	1.66	0.35	1.31	0	171.75	0.2	
02/04/2018 01:00	1.67	0.35	1.32	0.2	172	0	
02/04/2018 01:15	1.67	0.35	1.32	0.2	172.25	0	
02/04/2018 01:30	1.68	0.35	1.33	0.2	172.5	0.2	
02/04/2018 01:45	1.68	0.35	1.33	0.4	172.75	0.4	
02/04/2018 02:00	1.69	0.35	1.34	0.4	173	0.4	
02/04/2018 02:15	1.69	0.35	1.34	0.4	173.25	0.2	
02/04/2018 02:30	1.70	0.35	1.35	0.4	173.5	0.4	
02/04/2018 02:45	1.70	0.35	1.35	0.4	173.75	0.2	
02/04/2018 03:00	1.70	0.35	1.35	0.2	174	0.2	
02/04/2018 03:15	1.70	0.35	1.35	0.2	174.25	0.4	
02/04/2018 03:30	1.70	0.35	1.35	0.4	174.5	0.2	
02/04/2018 03:45	1.69	0.35	1.34	0.4	174.75	0.2	
02/04/2018 04:00	1.69	0.35	1.34	0.6	175	0.4	
02/04/2018 04:15	1.69	0.35	1.34	0.8	175.25	0.8	
02/04/2018 04:30	1.69	0.35	1.34	0.8	175.5	0.6	
02/04/2018 04:45	1.70	0.35	1.35	0.6	175.75	0.6	
02/04/2018 05:00	1.71	0.35	1.36	0.6	176	0.6	
02/04/2018 05:15	1.71	0.35	1.36	0.6	176.25	0.6	
02/04/2018 05:30	1.73	0.35	1.38	0.6	176.5	0.6	
02/04/2018 05:45	1.75	0.35	1.40	0.6	176.75	0.4	
02/04/2018 06:00	1.77	0.35	1.42	0.2	177	0.2	
02/04/2018 06:15	1.81	0.35	1.46	0.2	177.25	0.2	
02/04/2018 06:30	1.85	0.35	1.50	0.2	177.5	0.2	
02/04/2018 06:45	1.91	0.35	1.56	0.2	177.75	0	
02/04/2018 07:00	2.00	0.35	1.65	0.2	178	0.2	
02/04/2018 07:15	2.11	0.35	1.76	0.4	178.25	0.2	
02/04/2018 07:30	2.27	0.35	1.92	0.2	178.5	0.2	
02/04/2018 07:45	2.49	0.35	2.14	0.4	178.75	0.4	
02/04/2018 08:00	2.81	0.35	2.46	0.2	179	0.2	
02/04/2018 08:15	3.18	0.35	2.83	0	179.25	0.2	
02/04/2018 08:30	3.57	0.35	3.22	0.2	179.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
02/04/2018 08:45	3.86	0.35	3.51	0.2	179.75	0.2	
02/04/2018 09:00	4.13	0.35	3.78	0	180	0.2	
02/04/2018 09:15	4.38	0.35	4.03	0.2	180.25	0.2	
02/04/2018 09:30	4.60	0.35	4.25	0	180.5	0	
02/04/2018 09:45	4.78	0.35	4.43	0.2	180.75	0.2	
02/04/2018 10:00	4.93	0.35	4.58	0.2	181	0.2	
02/04/2018 10:15	5.07	0.35	4.72	0.2	181.25	0.2	
02/04/2018 10:30	5.21	0.35	4.86	0	181.5	0	
02/04/2018 10:45	5.37	0.35	5.02	0	181.75	0	
02/04/2018 11:00	5.52	0.35	5.17	0	182	0	
02/04/2018 11:15	5.67	0.35	5.32	0	182.25	0.2	
02/04/2018 11:30	5.81	0.35	5.46	0	182.5	0	
02/04/2018 11:45	5.93	0.35	5.58	0	182.75	0	
02/04/2018 12:00	6.05	0.35	5.70	0	183	0	
02/04/2018 12:15	6.16	0.35	5.81	0	183.25	0	
02/04/2018 12:30	6.28	0.35	5.93	0	183.5	0	
02/04/2018 12:45	6.38	0.35	6.03	0	183.75	0	
02/04/2018 13:00	6.49	0.35	6.14	0	184	0	
02/04/2018 13:15	6.57	0.35	6.22	0	184.25	0	
02/04/2018 13:30	6.65	0.35	6.30	0.2	184.5	0	
02/04/2018 13:45	6.71	0.35	6.36	0	184.75	0	
02/04/2018 14:00	6.78	0.35	6.43	0	185	0	
02/04/2018 14:15	6.85	0.35	6.50	0	185.25	0	
02/04/2018 14:30	6.93	0.35	6.58	0	185.5	0	
02/04/2018 14:45	7.00	0.35	6.65	0.2	185.75	0.2	
02/04/2018 15:00	7.08	0.35	6.73	0	186	0	
02/04/2018 15:15	7.17	0.35	6.82	0	186.25	0	
02/04/2018 15:30	7.25	0.35	6.90	0	186.5	0	
02/04/2018 15:45	7.34	0.35	6.99	0	186.75	0	
02/04/2018 16:00	7.41	0.35	7.06	0	187	0	
02/04/2018 16:15	7.49	0.35	7.14	0	187.25	0.2	
02/04/2018 16:30	7.58	0.35	7.23	0.2	187.5	0.2	
02/04/2018 16:45	7.66	0.35	7.31	0	187.75	0.2	
02/04/2018 17:00	7.76	0.35	7.41	0.2	188	0	
02/04/2018 17:15	7.84	0.35	7.49	0.2	188.25	0.2	
02/04/2018 17:30	7.90	0.35	7.55	0.2	188.5	0.2	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
02/04/2018 17:45	7.97	0.35	7.62	0	188.75	0	
02/04/2018 18:00	8.04	0.35	7.69	0	189	0.2	
02/04/2018 18:15	8.11	0.35	7.76	0	189.25	0	
02/04/2018 18:30	8.16	0.35	7.81	0	189.5	0	
02/04/2018 18:45	8.23	0.35	7.88	0	189.75	0	
02/04/2018 19:00	8.25	0.35	7.90	0.2	190	0	
02/04/2018 19:15	8.30	0.35	7.95	0	190.25	0	
02/04/2018 19:30	8.36	0.35	8.01	0	190.5	0	
02/04/2018 19:45	8.39	0.35	8.04	0	190.75	0	
02/04/2018 20:00	8.43	0.35	8.08	0	191	0	
02/04/2018 20:15	8.48	0.35	8.13	0	191.25	0	
02/04/2018 20:30	8.51	0.35	8.16	0	191.5	0	
02/04/2018 20:45	8.55	0.35	8.20	0	191.75	0	
02/04/2018 21:00	8.61	0.35	8.26	0	192	0	
02/04/2018 21:15	8.64	0.35	8.29	0	192.25	0	
02/04/2018 21:30	8.70	0.35	8.35	0	192.5	0	
02/04/2018 21:45	8.75	0.35	8.40	0	192.75	0	
02/04/2018 22:00	8.80	0.35	8.45	0	193	0	
02/04/2018 22:15	8.85	0.35	8.50	0	193.25	0	
02/04/2018 22:30	8.89	0.35	8.54	0	193.5	0	
02/04/2018 22:45	9.00	0.35	8.65	0	193.75	0	
02/04/2018 23:00	9.08	0.35	8.73	0	194	0	
02/04/2018 23:15	9.19	0.35	8.84	0	194.25	0.2	
02/04/2018 23:30	9.29	0.35	8.94	0	194.5	0	
02/04/2018 23:45	9.38	0.35	9.03	0	194.75	0	
03/04/2018 00:00	9.46	0.35	9.11	0	195	0	
03/04/2018 00:15	9.51	0.35	9.16	0	195.25	0	
03/04/2018 00:30	9.54	0.35	9.19	0	195.5	0	
03/04/2018 00:45	9.56	0.35	9.21	0	195.75	0	
03/04/2018 01:00	9.56	0.35	9.21	0	196	0	
03/04/2018 01:15	9.56	0.35	9.21	0	196.25	0	
03/04/2018 01:30	9.54	0.35	9.19	0	196.5	0	
03/04/2018 01:45	9.46	0.35	9.11	0	196.75	0	
03/04/2018 02:00	9.43	0.35	9.08	0	197	0	
03/04/2018 02:15	9.35	0.35	9.00	0.2	197.25	0	
03/04/2018 02:30	9.27	0.35	8.92	0	197.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
03/04/2018 02:45	9.14	0.35	8.79	0	197.75	0	
03/04/2018 03:00	9.03	0.35	8.68	0	198	0	
03/04/2018 03:15	8.90	0.35	8.55	0	198.25	0	
03/04/2018 03:30	8.84	0.35	8.49	0	198.5	0.2	
03/04/2018 03:45	8.78	0.35	8.43	0	198.75	0	
03/04/2018 04:00	8.71	0.35	8.36	0	199	0	
03/04/2018 04:15	8.62	0.35	8.27	0	199.25	0	
03/04/2018 04:30	8.56	0.35	8.21	0	199.5	0	
03/04/2018 04:45	8.47	0.35	8.12	0	199.75	0	
03/04/2018 05:00	8.38	0.35	8.03	0	200	0	
03/04/2018 05:15	8.29	0.35	7.94	0	200.25	0	
03/04/2018 05:30	8.17	0.35	7.82	0	200.5	0	
03/04/2018 05:45	8.08	0.35	7.73	0	200.75	0	
03/04/2018 06:00	7.97	0.35	7.62	0	201	0	
03/04/2018 06:15	7.86	0.35	7.51	0	201.25	0	
03/04/2018 06:30	7.75	0.35	7.40	0	201.5	0	
03/04/2018 06:45	7.64	0.35	7.29	0	201.75	0	
03/04/2018 07:00	7.53	0.35	7.18	0	202	0	
03/04/2018 07:15	7.42	0.35	7.07	0	202.25	0	
03/04/2018 07:30	7.30	0.35	6.95	0	202.5	0	
03/04/2018 07:45	7.19	0.35	6.84	0	202.75	0	
03/04/2018 08:00	7.06	0.35	6.71	0	203	0	
03/04/2018 08:15	6.93	0.35	6.58	0	203.25	0	
03/04/2018 08:30	6.80	0.35	6.45	0	203.5	0	
03/04/2018 08:45	6.67	0.35	6.32	0	203.75	0	
03/04/2018 09:00	6.54	0.35	6.19	0	204	0	
03/04/2018 09:15	6.41	0.35	6.06	0	204.25	0	
03/04/2018 09:30	6.27	0.35	5.92	0	204.5	0	
03/04/2018 09:45	6.14	0.35	5.79	0	204.75	0	
03/04/2018 10:00	6.00	0.35	5.65	0	205	0	
03/04/2018 10:15	5.86	0.35	5.51	0	205.25	0	
03/04/2018 10:30	5.73	0.35	5.38	0	205.5	0	
03/04/2018 10:45	5.59	0.35	5.24	0	205.75	0	
03/04/2018 11:00	5.44	0.35	5.09	0	206	0	
03/04/2018 11:15	5.29	0.35	4.94	0	206.25	0	
03/04/2018 11:30	5.13	0.35	4.78	0	206.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
03/04/2018 11:45	4.97	0.35	4.62	0	206.75	0	
03/04/2018 12:00	4.82	0.35	4.47	0	207	0	
03/04/2018 12:15	4.64	0.35	4.29	0	207.25	0	
03/04/2018 12:30	4.46	0.35	4.11	0	207.5	0	
03/04/2018 12:45	4.26	0.35	3.91	0	207.75	0	
03/04/2018 13:00	4.06	0.35	3.71	0	208	0.2	
03/04/2018 13:15	3.89	0.35	3.54	0	208.25	0	
03/04/2018 13:30	3.70	0.35	3.35	0	208.5	0	
03/04/2018 13:45	3.54	0.35	3.19	0	208.75	0	
03/04/2018 14:00	3.33	0.35	2.98	0	209	0	
03/04/2018 14:15	3.11	0.35	2.76	0	209.25	0	
03/04/2018 14:30	2.90	0.35	2.55	0	209.5	0	
03/04/2018 14:45	2.70	0.35	2.35	0	209.75	0	
03/04/2018 15:00	2.53	0.35	2.18	0	210	0	
03/04/2018 15:15	2.36	0.35	2.01	0	210.25	0	
03/04/2018 15:30	2.23	0.35	1.88	0	210.5	0	
03/04/2018 15:45	2.12	0.35	1.77	0	210.75	0	
03/04/2018 16:00	2.03	0.35	1.68	0	211	0	
03/04/2018 16:15	1.96	0.35	1.61	0	211.25	0	
03/04/2018 16:30	1.90	0.35	1.55	0	211.5	0	
03/04/2018 16:45	1.86	0.35	1.51	0	211.75	0	
03/04/2018 17:00	1.82	0.35	1.47	0	212	0	
03/04/2018 17:15	1.78	0.35	1.43	0	212.25	0	
03/04/2018 17:30	1.75	0.35	1.40	0	212.5	0	
03/04/2018 17:45	1.71	0.35	1.36	0	212.75	0	
03/04/2018 18:00	1.69	0.35	1.34	0	213	0	
03/04/2018 18:15	1.66	0.35	1.31	0	213.25	0	
03/04/2018 18:30	1.64	0.35	1.29	0	213.5	0	
03/04/2018 18:45	1.62	0.35	1.27	0	213.75	0	
03/04/2018 19:00	1.60	0.35	1.25	0	214	0	
03/04/2018 19:15	1.58	0.35	1.23	0	214.25	0	
03/04/2018 19:30	1.55	0.35	1.20	0	214.5	0	
03/04/2018 19:45	1.54	0.35	1.19	0	214.75	0	
03/04/2018 20:00	1.52	0.35	1.17	0	215	0	
03/04/2018 20:15	1.50	0.35	1.15	0	215.25	0	
03/04/2018 20:30	1.48	0.35	1.13	0	215.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
03/04/2018 20:45	1.47	0.35	1.12	0	215.75	0	
03/04/2018 21:00	1.45	0.35	1.10	0	216	0	
03/04/2018 21:15	1.44	0.35	1.09	0	216.25	0	
03/04/2018 21:30	1.42	0.35	1.07	0	216.5	0	
03/04/2018 21:45	1.41	0.35	1.06	0	216.75	0	
03/04/2018 22:00	1.39	0.35	1.04	0	217	0	
03/04/2018 22:15	1.38	0.35	1.03	0	217.25	0	
03/04/2018 22:30	1.36	0.35	1.01	0	217.5	0	
03/04/2018 22:45	1.35	0.35	1.00	0	217.75	0	
03/04/2018 23:00	1.34	0.35	0.99	0	218	0	
03/04/2018 23:15	1.32	0.35	0.97	0	218.25	0	
03/04/2018 23:30	1.31	0.35	0.96	0	218.5	0	
03/04/2018 23:45	1.30	0.35	0.95	0	218.75	0	
04/04/2018 00:00	1.29	0.35	0.94	0	219	0	
04/04/2018 00:15	1.28	0.35	0.93	0	219.25	0	
04/04/2018 00:30	1.27	0.35	0.92	0	219.5	0	
04/04/2018 00:45	1.26	0.35	0.91	0	219.75	0	
04/04/2018 01:00	1.24	0.35	0.89	0	220	0	
04/04/2018 01:15	1.24	0.35	0.89	0	220.25	0	
04/04/2018 01:30	1.23	0.35	0.88	0	220.5	0	
04/04/2018 01:45	1.22	0.35	0.87	0	220.75	0	
04/04/2018 02:00	1.21	0.35	0.86	0	221	0	
04/04/2018 02:15	1.20	0.35	0.85	0	221.25	0	
04/04/2018 02:30	1.19	0.35	0.84	0	221.5	0	
04/04/2018 02:45	1.18	0.35	0.83	0	221.75	0	
04/04/2018 03:00	1.17	0.35	0.82	0	222	0	
04/04/2018 03:15	1.16	0.35	0.81	0	222.25	0	
04/04/2018 03:30	1.15	0.35	0.80	0	222.5	0	
04/04/2018 03:45	1.14	0.35	0.79	0	222.75	0	
04/04/2018 04:00	1.13	0.35	0.78	0	223	0	
04/04/2018 04:15	1.13	0.35	0.78	0	223.25	0	
04/04/2018 04:30	1.12	0.35	0.77	0	223.5	0	
04/04/2018 04:45	1.11	0.35	0.76	0	223.75	0	
04/04/2018 05:00	1.11	0.35	0.76	0	224	0	
04/04/2018 05:15	1.10	0.35	0.75	0	224.25	0	
04/04/2018 05:30	1.07	0.35	0.72	0	224.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
04/04/2018 05:45	1.06	0.35	0.71	0	224.75	0	
04/04/2018 06:00	1.05	0.35	0.70	0	225	0	
04/04/2018 06:15	1.04	0.35	0.69	0	225.25	0	
04/04/2018 06:30	1.03	0.35	0.68	0	225.5	0	
04/04/2018 06:45	1.01	0.35	0.66	0	225.75	0	
04/04/2018 07:00	1.00	0.35	0.65	0	226	0	
04/04/2018 07:15	0.99	0.35	0.64	0	226.25	0	
04/04/2018 07:30	0.98	0.35	0.63	0	226.5	0	
04/04/2018 07:45	0.97	0.35	0.62	0	226.75	0	
04/04/2018 08:00	0.96	0.35	0.61	0	227	0	
04/04/2018 08:15	0.94	0.35	0.59	0	227.25	0	
04/04/2018 08:30	0.93	0.35	0.58	0	227.5	0	
04/04/2018 08:45	0.93	0.35	0.58	0	227.75	0	
04/04/2018 09:00	0.92	0.35	0.57	0	228	0	
04/04/2018 09:15	0.91	0.35	0.56	0	228.25	0	
04/04/2018 09:30	0.90	0.35	0.55	0	228.5	0	
04/04/2018 09:45	0.90	0.35	0.55	0	228.75	0	
04/04/2018 10:00	0.89	0.35	0.54	0	229	0	
04/04/2018 10:15	0.88	0.35	0.53	0	229.25	0	
04/04/2018 10:30	0.87	0.35	0.52	0	229.5	0	
04/04/2018 10:45	0.87	0.35	0.52	0	229.75	0	
04/04/2018 11:00	0.86	0.35	0.51	0	230	0	
04/04/2018 11:15	0.86	0.35	0.51	0	230.25	0	
04/04/2018 11:30	0.85	0.35	0.50	0	230.5	0	
04/04/2018 11:45	0.84	0.35	0.49	0	230.75	0	
04/04/2018 12:00	0.84	0.35	0.49	0	231	0	
04/04/2018 12:15	0.82	0.35	0.47	0	231.25	0	
04/04/2018 12:30	0.82	0.35	0.47	0	231.5	0	
04/04/2018 12:45	0.81	0.35	0.46	0	231.75	0	
04/04/2018 13:00	0.80	0.35	0.45	0	232	0	
04/04/2018 13:15	0.80	0.35	0.45	0	232.25	0	
04/04/2018 13:30	0.79	0.35	0.44	0	232.5	0	
04/04/2018 13:45	0.78	0.35	0.43	0	232.75	0	
04/04/2018 14:00	0.78	0.35	0.43	0	233	0	
04/04/2018 14:15	0.77	0.35	0.42	0	233.25	0	
04/04/2018 14:30	0.76	0.35	0.41	0	233.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
04/04/2018 14:45	0.76	0.35	0.41	0	233.75	0	
04/04/2018 15:00	0.76	0.35	0.41	0	234	0	
04/04/2018 15:15	0.76	0.35	0.41	0	234.25	0	
04/04/2018 15:30	0.75	0.35	0.40	0	234.5	0	
04/04/2018 15:45	0.74	0.35	0.39	0	234.75	0	
04/04/2018 16:00	0.74	0.35	0.39	0	235	0	
04/04/2018 16:15	0.73	0.35	0.38	0	235.25	0	
04/04/2018 16:30	0.72	0.35	0.37	0	235.5	0	
04/04/2018 16:45	0.72	0.35	0.37	0	235.75	0	
04/04/2018 17:00	0.71	0.35	0.36	0	236	0	
04/04/2018 17:15	0.70	0.35	0.35	0	236.25	0	
04/04/2018 17:30	0.70	0.35	0.35	0	236.5	0	
04/04/2018 17:45	0.69	0.35	0.34	0	236.75	0	
04/04/2018 18:00	0.68	0.35	0.33	0	237	0	
04/04/2018 18:15	0.68	0.35	0.33	0	237.25	0	
04/04/2018 18:30	0.67	0.35	0.32	0	237.5	0	
04/04/2018 18:45	0.67	0.35	0.32	0	237.75	0	
04/04/2018 19:00	0.66	0.35	0.31	0	238	0	
04/04/2018 19:15	0.65	0.35	0.30	0	238.25	0	
04/04/2018 19:30	0.65	0.35	0.30	0	238.5	0	
04/04/2018 19:45	0.65	0.35	0.30	0	238.75	0	
04/04/2018 20:00	0.64	0.35	0.29	0	239	0	
04/04/2018 20:15	0.64	0.35	0.29	0	239.25	0	
04/04/2018 20:30	0.63	0.35	0.28	0	239.5	0	
04/04/2018 20:45	0.62	0.35	0.27	0	239.75	0	
04/04/2018 21:00	0.62	0.35	0.27	0	240	0	
04/04/2018 21:15	0.61	0.35	0.26	0	240.25	0	
04/04/2018 21:30	0.61	0.35	0.26	0	240.5	0	
04/04/2018 21:45	0.60	0.35	0.25	0	240.75	0	
04/04/2018 22:00	0.60	0.35	0.25	0.2	241	0.2	
04/04/2018 22:15	0.60	0.35	0.25	0	241.25	0	
04/04/2018 22:30	0.59	0.35	0.24	0	241.5	0	
04/04/2018 22:45	0.59	0.35	0.24	0	241.75	0	
04/04/2018 23:00	0.58	0.35	0.23	0	242	0	
04/04/2018 23:15	0.58	0.35	0.23	0	242.25	0	
04/04/2018 23:30	0.57	0.35	0.22	0	242.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
04/04/2018 23:45	0.56	0.35	0.21	0	242.75	0	
05/04/2018 00:00	0.56	0.35	0.21	0	243	0	
05/04/2018 00:15	0.56	0.35	0.21	0	243.25	0	
05/04/2018 00:30	0.56	0.35	0.21	0	243.5	0	
05/04/2018 00:45	0.55	0.35	0.20	0	243.75	0	
05/04/2018 01:00	0.55	0.35	0.20	0	244	0	
05/04/2018 01:15	0.54	0.35	0.19	0	244.25	0	
05/04/2018 01:30	0.54	0.35	0.19	0	244.5	0	
05/04/2018 01:45	0.53	0.35	0.18	0	244.75	0	
05/04/2018 02:00	0.53	0.35	0.18	0	245	0	
05/04/2018 02:15	0.53	0.35	0.18	0	245.25	0	
05/04/2018 02:30	0.53	0.35	0.18	0	245.5	0	
05/04/2018 02:45	0.52	0.35	0.17	0	245.75	0	
05/04/2018 03:00	0.52	0.35	0.17	0	246	0	
05/04/2018 03:15	0.51	0.35	0.16	0	246.25	0	
05/04/2018 03:30	0.51	0.35	0.16	0	246.5	0	
05/04/2018 03:45	0.50	0.35	0.15	0	246.75	0	
05/04/2018 04:00	0.50	0.35	0.15	0	247	0	
05/04/2018 04:15	0.50	0.35	0.15	0	247.25	0	
05/04/2018 04:30	0.50	0.35	0.15	0	247.5	0	
05/04/2018 04:45	0.49	0.35	0.14	0	247.75	0	
05/04/2018 05:00	0.49	0.35	0.14	0	248	0	
05/04/2018 05:15	0.48	0.35	0.13	0	248.25	0	
05/04/2018 05:30	0.48	0.35	0.13	0	248.5	0	
05/04/2018 05:45	0.48	0.35	0.13	0	248.75	0	
05/04/2018 06:00	0.48	0.35	0.13	0	249	0	
05/04/2018 06:15	0.47	0.35	0.12	0	249.25	0	
05/04/2018 06:30	0.47	0.35	0.12	0	249.5	0	
05/04/2018 06:45	0.46	0.35	0.11	0	249.75	0	
05/04/2018 07:00	0.46	0.35	0.11	0	250	0	
05/04/2018 07:15	0.46	0.35	0.11	0	250.25	0	
05/04/2018 07:30	0.45	0.35	0.10	0	250.5	0	
05/04/2018 07:45	0.45	0.35	0.10	0	250.75	0	
05/04/2018 08:00	0.44	0.35	0.09	0	251	0	
05/04/2018 08:15	0.44	0.35	0.09	0	251.25	0	
05/04/2018 08:30	0.44	0.35	0.09	0	251.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
05/04/2018 08:45	0.43	0.35	0.08	0	251.75	0	
05/04/2018 09:00	0.43	0.35	0.08	0	252	0	
05/04/2018 09:15	0.42	0.35	0.07	0	252.25	0	
05/04/2018 09:30	0.42	0.35	0.07	0	252.5	0	
05/04/2018 09:45	0.42	0.35	0.07	0	252.75	0	
05/04/2018 10:00	0.42	0.35	0.07	0	253	0	
05/04/2018 10:15	0.41	0.35	0.06	0	253.25	0	
05/04/2018 10:30	0.41	0.35	0.06	0	253.5	0	
05/04/2018 10:45	0.40	0.35	0.05	0	253.75	0	
05/04/2018 11:00	0.40	0.35	0.05	0	254	0	
05/04/2018 11:15	0.40	0.35	0.05	0	254.25	0	
05/04/2018 11:30	0.39	0.35	0.04	0	254.5	0	
05/04/2018 11:45	0.39	0.35	0.04	0	254.75	0	
05/04/2018 12:00	0.39	0.35	0.04	0	255	0	
05/04/2018 12:15	0.39	0.35	0.04	0	255.25	0	
05/04/2018 12:30	0.38	0.35	0.03	0	255.5	0	
05/04/2018 12:45	0.38	0.35	0.03	0	255.75	0	
05/04/2018 13:00	0.37	0.35	0.02	0	256	0	
05/04/2018 13:15	0.37	0.35	0.02	0	256.25	0	
05/04/2018 13:30	0.37	0.35	0.02	0	256.5	0	
05/04/2018 13:45	0.37	0.35	0.02	0	256.75	0	
05/04/2018 14:00	0.36	0.35	0.01	0	257	0	
05/04/2018 14:15	0.36	0.35	0.01	0	257.25	0	
05/04/2018 14:30	0.36	0.35	0.01	0	257.5	0	
05/04/2018 14:45	0.36	0.35	0.01	0	257.75	0	
05/04/2018 15:00	0.36	0.35	0.01	0	258	0	
05/04/2018 15:15	0.35	0.35	0.00	0	258.25	0	
05/04/2018 15:30	0.35	0.35	0.00	0	258.5	0	
05/04/2018 15:45	0.35	0.35	0.00	0	258.75	0	
05/04/2018 16:00	0.35	0.35	0.00	0	259	0	
05/04/2018 16:15	0.35	0.35	0.00	0	259.25	0	
05/04/2018 16:30	0.35	0.35	0.00	0	259.5	0	
05/04/2018 16:45	0.34	0.34	0.00	0	259.75	0	
05/04/2018 17:00	0.34	0.34	0.00	0	260	0	
05/04/2018 17:15	0.34	0.34	0.00	0	260.25	0	
05/04/2018 17:30	0.34	0.34	0.00	0	260.5	0	

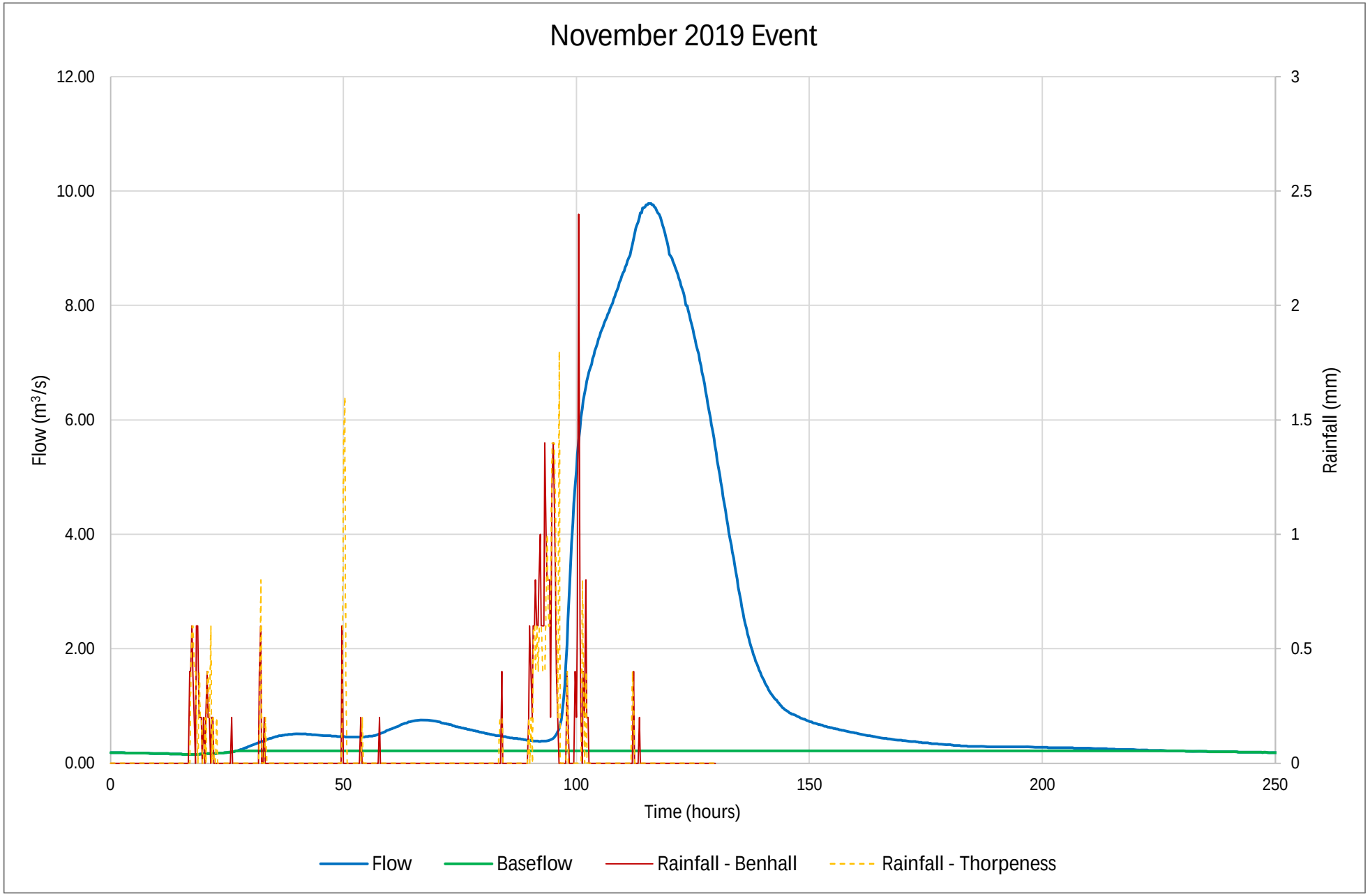
		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
05/04/2018 17:45	0.34	0.34	0.00	0	260.75	0	
05/04/2018 18:00	0.34	0.34	0.00	0	261	0	
05/04/2018 18:15	0.33	0.33	0.00	0	261.25	0	
05/04/2018 18:30	0.33	0.33	0.00	0	261.5	0	
05/04/2018 18:45	0.33	0.33	0.00	0	261.75	0	
05/04/2018 19:00	0.32	0.32	0.00	0	262	0	
05/04/2018 19:15	0.32	0.32	0.00	0	262.25	0	
05/04/2018 19:30	0.32	0.32	0.00	0	262.5	0	
05/04/2018 19:45	0.32	0.32	0.00	0	262.75	0	
05/04/2018 20:00	0.32	0.32	0.00	0	263	0	
05/04/2018 20:15	0.32	0.32	0.00	0	263.25	0	
05/04/2018 20:30	0.32	0.32	0.00	0	263.5	0	
05/04/2018 20:45	0.32	0.32	0.00	0	263.75	0	
05/04/2018 21:00	0.31	0.31	0.00	0	264	0	
05/04/2018 21:15	0.31	0.31	0.00	0	264.25	0	
05/04/2018 21:30	0.31	0.31	0.00	0	264.5	0	
05/04/2018 21:45	0.31	0.31	0.00	0	264.75	0	
05/04/2018 22:00	0.31	0.31	0.00	0	265	0	
05/04/2018 22:15	0.30	0.30	0.00	0	265.25	0	
05/04/2018 22:30	0.30	0.30	0.00	0	265.5	0	
05/04/2018 22:45	0.30	0.30	0.00	0	265.75	0	
05/04/2018 23:00	0.30	0.30	0.00	0	266	0	
05/04/2018 23:15	0.30	0.30	0.00	0	266.25	0	
05/04/2018 23:30	0.30	0.30	0.00	0	266.5	0	
05/04/2018 23:45	0.29	0.29	0.00	0	266.75	0	
06/04/2018 00:00	0.29	0.29	0.00	0	267	0	
06/04/2018 00:15	0.29	0.29	0.00	0	267.25	0	
06/04/2018 00:30	0.29	0.29	0.00	0	267.5	0	
06/04/2018 00:45	0.29	0.29	0.00	0	267.75	0	
06/04/2018 01:00	0.29	0.29	0.00	0	268	0	
06/04/2018 01:15	0.29	0.29	0.00	0	268.25	0	
06/04/2018 01:30	0.29	0.29	0.00	0	268.5	0	
06/04/2018 01:45	0.29	0.29	0.00	0	268.75	0	
06/04/2018 02:00	0.29	0.29	0.00	0	269	0	
06/04/2018 02:15	0.29	0.29	0.00	0	269.25	0	
06/04/2018 02:30	0.29	0.29	0.00	0	269.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
06/04/2018 02:45	0.28	0.28	0.00	0	269.75	0	
06/04/2018 03:00	0.28	0.28	0.00	0	270	0	
06/04/2018 03:15	0.28	0.28	0.00	0	270.25	0	
06/04/2018 03:30	0.28	0.28	0.00	0	270.5	0	
06/04/2018 03:45	0.28	0.28	0.00	0	270.75	0	
06/04/2018 04:00	0.28	0.28	0.00	0	271	0	
06/04/2018 04:15	0.28	0.28	0.00	0	271.25	0	
06/04/2018 04:30	0.28	0.28	0.00	0	271.5	0	
06/04/2018 04:45	0.28	0.28	0.00	0	271.75	0	
06/04/2018 05:00	0.28	0.28	0.00	0	272	0	
06/04/2018 05:15	0.27	0.27	0.00	0	272.25	0	
06/04/2018 05:30	0.27	0.27	0.00	0	272.5	0	
06/04/2018 05:45	0.27	0.27	0.00	0	272.75	0	
06/04/2018 06:00	0.27	0.27	0.00	0	273	0	
06/04/2018 06:15	0.27	0.27	0.00	0	273.25	0	
06/04/2018 06:30	0.27	0.27	0.00	0	273.5	0	
06/04/2018 06:45	0.27	0.27	0.00	0	273.75	0	
06/04/2018 07:00	0.27	0.27	0.00	0	274	0	
06/04/2018 07:15	0.27	0.27	0.00	0	274.25	0	
06/04/2018 07:30	0.27	0.27	0.00	0	274.5	0	
06/04/2018 07:45	0.27	0.27	0.00	0	274.75	0	
06/04/2018 08:00	0.27	0.27	0.00	0	275	0	
06/04/2018 08:15	0.27	0.27	0.00	0	275.25	0	
06/04/2018 08:30	0.27	0.27	0.00	0	275.5	0	
06/04/2018 08:45	0.27	0.27	0.00	0	275.75	0	
06/04/2018 09:00	0.26	0.26	0.00	0	276	0	
06/04/2018 09:15	0.26	0.26	0.00	0	276.25	0	
06/04/2018 09:30	0.26	0.26	0.00	0	276.5	0	
06/04/2018 09:45	0.26	0.26	0.00	0	276.75	0	
06/04/2018 10:00	0.27	0.27	0.00	0	277	0	
06/04/2018 10:15	0.27	0.27	0.00	0	277.25	0	
06/04/2018 10:30	0.26	0.26	0.00	0	277.5	0	
06/04/2018 10:45	0.26	0.26	0.00	0	277.75	0	
06/04/2018 11:00	0.26	0.26	0.00	0	278	0	
06/04/2018 11:15	0.26	0.26	0.00	0	278.25	0	
06/04/2018 11:30	0.26	0.26	0.00	0	278.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
06/04/2018 11:45	0.26	0.26	0.00	0	278.75	0	
06/04/2018 12:00	0.26	0.26	0.00	0	279	0	
06/04/2018 12:15	0.26	0.26	0.00	0	279.25	0	
06/04/2018 12:30	0.26	0.26	0.00	0	279.5	0	
06/04/2018 12:45	0.26	0.26	0.00	0	279.75	0	
06/04/2018 13:00	0.26	0.26	0.00	0	280	0	
06/04/2018 13:15	0.26	0.26	0.00	0	280.25	0	
06/04/2018 13:30	0.26	0.26	0.00	0	280.5	0	
06/04/2018 13:45	0.26	0.26	0.00	0	280.75	0	
06/04/2018 14:00	0.26	0.26	0.00	0	281	0	
06/04/2018 14:15	0.26	0.26	0.00	0	281.25	0	
06/04/2018 14:30	0.26	0.26	0.00	0	281.5	0	
06/04/2018 14:45	0.26	0.26	0.00	0	281.75	0	
06/04/2018 15:00	0.26	0.26	0.00	0	282	0	
06/04/2018 15:15	0.26	0.26	0.00	0	282.25	0	
06/04/2018 15:30	0.26	0.26	0.00	0	282.5	0	
06/04/2018 15:45	0.26	0.26	0.00	0	282.75	0	
06/04/2018 16:00	0.26	0.26	0.00	0	283	0	
06/04/2018 16:15	0.26	0.26	0.00	0	283.25	0	
06/04/2018 16:30	0.26	0.26	0.00	0	283.5	0	
06/04/2018 16:45	0.26	0.26	0.00	0	283.75	0	
06/04/2018 17:00	0.26	0.26	0.00	0	284	0	
06/04/2018 17:15	0.26	0.26	0.00	0	284.25	0	
06/04/2018 17:30	0.26	0.26	0.00	0	284.5	0	
06/04/2018 17:45	0.26	0.26	0.00	0	284.75	0	
06/04/2018 18:00	0.26	0.26	0.00	0	285	0	
06/04/2018 18:15	0.26	0.26	0.00	0	285.25	0	
06/04/2018 18:30	0.26	0.26	0.00	0	285.5	0	
06/04/2018 18:45	0.26	0.26	0.00	0	285.75	0	
06/04/2018 19:00	0.26	0.26	0.00	0	286	0	
06/04/2018 19:15	0.26	0.26	0.00	0	286.25	0	
06/04/2018 19:30	0.26	0.26	0.00	0	286.5	0	
06/04/2018 19:45	0.26	0.26	0.00	0	286.75	0	
06/04/2018 20:00	0.26	0.26	0.00	0	287	0	
06/04/2018 20:15	0.26	0.26	0.00	0	287.25	0	
06/04/2018 20:30	0.26	0.26	0.00	0	287.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
06/04/2018 20:45	0.26	0.26	0.00	0	287.75	0	
06/04/2018 21:00	0.26	0.26	0.00	0	288	0	
06/04/2018 21:15	0.26	0.26	0.00	0	288.25	0	
06/04/2018 21:30	0.26	0.26	0.00	0	288.5	0	
06/04/2018 21:45	0.26	0.26	0.00	0	288.75	0	
06/04/2018 22:00	0.26	0.26	0.00	0	289	0	
06/04/2018 22:15	0.26	0.26	0.00	0	289.25	0	
06/04/2018 22:30	0.26	0.26	0.00	0	289.5	0	
06/04/2018 22:45	0.26	0.26	0.00	0	289.75	0	
06/04/2018 23:00	0.25	0.25	0.00	0	290	0	
06/04/2018 23:15	0.25	0.25	0.00	0	290.25	0	
06/04/2018 23:30	0.25	0.25	0.00	0	290.5	0	
06/04/2018 23:45	0.25	0.25	0.00	0	290.75	0	
07/04/2018 00:00	0.25	0.25	0.00	0	291	0	
07/04/2018 00:15	0.25	0.25	0.00	0	291.25	0	
07/04/2018 00:30	0.25	0.25	0.00	0	291.5	0	
07/04/2018 00:45	0.25	0.25	0.00	0	291.75	0	
07/04/2018 01:00	0.25	0.25	0.00	0	292	0	
07/04/2018 01:15	0.25	0.25	0.00	0	292.25	0	
07/04/2018 01:30	0.25	0.25	0.00	0	292.5	0	
07/04/2018 01:45	0.25	0.25	0.00	0	292.75	0	
07/04/2018 02:00	0.25	0.25	0.00	0	293	0	
07/04/2018 02:15	0.25	0.25	0.00	0	293.25	0	
07/04/2018 02:30	0.25	0.25	0.00	0	293.5	0	
07/04/2018 02:45	0.25	0.25	0.00	0	293.75	0	
07/04/2018 03:00	0.25	0.25	0.00	0	294	0	
07/04/2018 03:15	0.25	0.25	0.00	0	294.25	0	
07/04/2018 03:30	0.25	0.25	0.00	0	294.5	0	
07/04/2018 03:45	0.25	0.25	0.00	0	294.75	0	
07/04/2018 04:00	0.25	0.25	0.00	0	295	0	
07/04/2018 04:15	0.25	0.25	0.00	0	295.25	0	
07/04/2018 04:30	0.25	0.25	0.00	0	295.5	0	
07/04/2018 04:45	0.25	0.25	0.00	0	295.75	0	
07/04/2018 05:00	0.25	0.25	0.00	0	296	0	
07/04/2018 05:15	0.24	0.24	0.00	0	296.25	0	
07/04/2018 05:30	0.24	0.24	0.00	0	296.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
07/04/2018 05:45	0.24	0.24	0.00	0	296.75	0	
07/04/2018 06:00	0.24	0.24	0.00	0	297	0	
07/04/2018 06:15	0.24	0.24	0.00	0	297.25	0	
07/04/2018 06:30	0.24	0.24	0.00	0	297.5	0	
07/04/2018 06:45	0.24	0.24	0.00	0	297.75	0	
07/04/2018 07:00	0.24	0.24	0.00	0	298	0	
07/04/2018 07:15	0.24	0.24	0.00	0	298.25	0	
07/04/2018 07:30	0.24	0.24	0.00	0	298.5	0	
07/04/2018 07:45	0.24	0.24	0.00	0	298.75	0	
07/04/2018 08:00	0.24	0.24	0.00	0	299	0	
07/04/2018 08:15	0.24	0.24	0.00	0	299.25	0	
07/04/2018 08:30	0.24	0.24	0.00	0	299.5	0	
07/04/2018 08:45	0.24	0.24	0.00	0	299.75	0	


November 2019 Event
12.00
10.00
8.00
6.00
4.00
2.00
0.00
Flow (m³/s)
3
2.5
2
1.5
1
0.5
0
Rainfall (mm)
0
50
100
150
200
250
Time (hours)
Flow
Baseflow
Rainfall - Benhall
Rainfall - Thorpeness

	Middleton			Benhall		Thorpeness
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
10/11/2019 11:30	0.18	0.18	0.00	0	0	0
10/11/2019 11:45	0.18	0.18	0.00	0	0.25	0
10/11/2019 12:00	0.18	0.18	0.00	0	0.5	0
10/11/2019 12:15	0.18	0.18	0.00	0	0.75	0
10/11/2019 12:30	0.18	0.18	0.00	0	1	0
10/11/2019 12:45	0.18	0.18	0.00	0	1.25	0
10/11/2019 13:00	0.18	0.18	0.00	0	1.5	0
10/11/2019 13:15	0.18	0.18	0.00	0	1.75	0
10/11/2019 13:30	0.18	0.18	0.00	0	2	0
10/11/2019 13:45	0.18	0.18	0.00	0	2.25	0
10/11/2019 14:00	0.18	0.18	0.00	0	2.5	0
10/11/2019 14:15	0.18	0.18	0.00	0	2.75	0
10/11/2019 14:30	0.18	0.18	0.00	0	3	0
10/11/2019 14:45	0.18	0.18	0.00	0	3.25	0
10/11/2019 15:00	0.18	0.18	0.00	0	3.5	0
10/11/2019 15:15	0.18	0.18	0.00	0	3.75	0
10/11/2019 15:30	0.18	0.18	0.00	0	4	0
10/11/2019 15:45	0.18	0.18	0.00	0	4.25	0
10/11/2019 16:00	0.18	0.18	0.00	0	4.5	0
10/11/2019 16:15	0.18	0.18	0.00	0	4.75	0
10/11/2019 16:30	0.18	0.18	0.00	0	5	0
10/11/2019 16:45	0.18	0.18	0.00	0	5.25	0
10/11/2019 17:00	0.18	0.18	0.00	0	5.5	0
10/11/2019 17:15	0.18	0.18	0.00	0	5.75	0
10/11/2019 17:30	0.18	0.18	0.00	0	6	0
10/11/2019 17:45	0.18	0.18	0.00	0	6.25	0
10/11/2019 18:00	0.17	0.17	0.00	0	6.5	0
10/11/2019 18:15	0.17	0.17	0.00	0	6.75	0
10/11/2019 18:30	0.17	0.17	0.00	0	7	0
10/11/2019 18:45	0.17	0.17	0.00	0	7.25	0
10/11/2019 19:00	0.17	0.17	0.00	0	7.5	0
10/11/2019 19:15	0.17	0.17	0.00	0	7.75	0
10/11/2019 19:30	0.17	0.17	0.00	0	8	0
10/11/2019 19:45	0.17	0.17	0.00	0	8.25	0
10/11/2019 20:00	0.17	0.17	0.00	0	8.5	0

Benhall	
Area (km^2)	50.16
Total Rain (P) mm	34
Time Interval (hour)	0.25
Percentage Runoff	65%

Thorpeness	
Area (km^2)	50.16
Total Rain (P) mm	31.4
Time Interval (hour)	0.25
Percentage Runoff	71%

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
10/11/2019 20:15	0.17	0.17	0.00	0	8.75	0	
10/11/2019 20:30	0.17	0.17	0.00	0	9	0	
10/11/2019 20:45	0.17	0.17	0.00	0	9.25	0	
10/11/2019 21:00	0.17	0.17	0.00	0	9.5	0	
10/11/2019 21:15	0.17	0.17	0.00	0	9.75	0	
10/11/2019 21:30	0.17	0.17	0.00	0	10	0	
10/11/2019 21:45	0.17	0.17	0.00	0	10.25	0	
10/11/2019 22:00	0.16	0.16	0.00	0	10.5	0	
10/11/2019 22:15	0.16	0.16	0.00	0	10.75	0	
10/11/2019 22:30	0.16	0.16	0.00	0	11	0	
10/11/2019 22:45	0.16	0.16	0.00	0	11.25	0	
10/11/2019 23:00	0.16	0.16	0.00	0	11.5	0	
10/11/2019 23:15	0.16	0.16	0.00	0	11.75	0	
10/11/2019 23:30	0.16	0.16	0.00	0	12	0	
10/11/2019 23:45	0.16	0.16	0.00	0	12.25	0	
11/11/2019 00:00	0.16	0.16	0.00	0	12.5	0	
11/11/2019 00:15	0.16	0.16	0.00	0	12.75	0	
11/11/2019 00:30	0.16	0.16	0.00	0	13	0	
11/11/2019 00:45	0.16	0.16	0.00	0	13.25	0	
11/11/2019 01:00	0.16	0.16	0.00	0	13.5	0	
11/11/2019 01:15	0.16	0.16	0.00	0	13.75	0	
11/11/2019 01:30	0.16	0.16	0.00	0	14	0	
11/11/2019 01:45	0.16	0.16	0.00	0	14.25	0	
11/11/2019 02:00	0.16	0.16	0.00	0	14.5	0	
11/11/2019 02:15	0.16	0.16	0.00	0	14.75	0	
11/11/2019 02:30	0.16	0.16	0.00	0	15	0	
11/11/2019 02:45	0.16	0.16	0.00	0	15.25	0	
11/11/2019 03:00	0.16	0.16	0.00	0	15.5	0	
11/11/2019 03:15	0.16	0.16	0.00	0	15.75	0	
11/11/2019 03:30	0.16	0.16	0.00	0	16	0	
11/11/2019 03:45	0.16	0.16	0.00	0	16.25	0	
11/11/2019 04:00	0.16	0.16	0.00	0	16.5	0	
11/11/2019 04:15	0.16	0.16	0.00	0	16.75	0	
11/11/2019 04:30	0.16	0.16	0.00	0.4	17	0	
11/11/2019 04:45	0.16	0.16	0.00	0.4	17.25	0.4	
11/11/2019 05:00	0.16	0.16	0.00	0.6	17.5	0.6	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
11/11/2019 05:15	0.16	0.16	0.00	0.4	17.75	0.6	
11/11/2019 05:30	0.16	0.16	0.00	0.2	18	0.4	
11/11/2019 05:45	0.16	0.16	0.00	0	18.25	0.4	
11/11/2019 06:00	0.16	0.16	0.00	0.6	18.5	0.2	
11/11/2019 06:15	0.16	0.16	0.00	0.6	18.75	0	
11/11/2019 06:30	0.16	0.16	0.00	0.2	19	0.4	
11/11/2019 06:45	0.16	0.16	0.00	0.2	19.25	0.2	
11/11/2019 07:00	0.16	0.16	0.00	0.2	19.5	0.2	
11/11/2019 07:15	0.16	0.16	0.00	0	19.75	0	
11/11/2019 07:30	0.16	0.16	0.00	0.2	20	0	
11/11/2019 07:45	0.16	0.16	0.00	0	20.25	0.2	
11/11/2019 08:00	0.16	0.16	0.00	0.2	20.5	0	
11/11/2019 08:15	0.16	0.16	0.00	0.4	20.75	0.4	
11/11/2019 08:30	0.16	0.16	0.00	0.2	21	0.4	
11/11/2019 08:45	0.17	0.17	0.00	0.2	21.25	0.2	
11/11/2019 09:00	0.17	0.17	0.00	0	21.5	0.6	
11/11/2019 09:15	0.17	0.17	0.00	0.2	21.75	0	
11/11/2019 09:30	0.17	0.17	0.00	0.2	22	0.2	
11/11/2019 09:45	0.17	0.17	0.00	0	22.25	0	
11/11/2019 10:00	0.17	0.17	0.00	0	22.5	0	
11/11/2019 10:15	0.17	0.17	0.00	0	22.75	0.2	
11/11/2019 10:30	0.17	0.17	0.00	0	23	0	
11/11/2019 10:45	0.17	0.17	0.00	0	23.25	0	
11/11/2019 11:00	0.17	0.17	0.00	0	23.5	0	
11/11/2019 11:15	0.18	0.18	0.00	0	23.75	0	
11/11/2019 11:30	0.18	0.18	0.00	0	24	0	
11/11/2019 11:45	0.18	0.18	0.00	0	24.25	0	
11/11/2019 12:00	0.18	0.18	0.00	0	24.5	0	
11/11/2019 12:15	0.18	0.18	0.00	0	24.75	0	
11/11/2019 12:30	0.18	0.18	0.00	0	25	0	
11/11/2019 12:45	0.19	0.19	0.00	0	25.25	0	
11/11/2019 13:00	0.19	0.19	0.00	0	25.5	0	
11/11/2019 13:15	0.19	0.19	0.00	0	25.75	0	
11/11/2019 13:30	0.19	0.19	0.00	0.2	26	0	
11/11/2019 13:45	0.20	0.20	0.00	0	26.25	0	
11/11/2019 14:00	0.20	0.20	0.00	0	26.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
11/11/2019 14:15	0.21	0.21	0.00	0	26.75	0	
11/11/2019 14:30	0.21	0.21	0.00	0	27	0	
11/11/2019 14:45	0.22	0.22	0.00	0	27.25	0	
11/11/2019 15:00	0.22	0.22	0.00	0	27.5	0	
11/11/2019 15:15	0.23	0.22	0.01	0	27.75	0	
11/11/2019 15:30	0.24	0.22	0.02	0	28	0	
11/11/2019 15:45	0.24	0.22	0.02	0	28.25	0	
11/11/2019 16:00	0.25	0.22	0.03	0	28.5	0	
11/11/2019 16:15	0.26	0.22	0.04	0	28.75	0	
11/11/2019 16:30	0.27	0.22	0.05	0	29	0	
11/11/2019 16:45	0.27	0.22	0.05	0	29.25	0	
11/11/2019 17:00	0.28	0.22	0.06	0	29.5	0	
11/11/2019 17:15	0.29	0.22	0.07	0	29.75	0	
11/11/2019 17:30	0.30	0.22	0.08	0	30	0	
11/11/2019 17:45	0.30	0.22	0.08	0	30.25	0	
11/11/2019 18:00	0.31	0.22	0.09	0	30.5	0	
11/11/2019 18:15	0.32	0.22	0.10	0	30.75	0	
11/11/2019 18:30	0.33	0.22	0.11	0	31	0	
11/11/2019 18:45	0.34	0.22	0.12	0	31.25	0	
11/11/2019 19:00	0.35	0.22	0.13	0	31.5	0	
11/11/2019 19:15	0.35	0.22	0.13	0	31.75	0	
11/11/2019 19:30	0.36	0.22	0.14	0.4	32	0.2	
11/11/2019 19:45	0.37	0.22	0.15	0.6	32.25	0.8	
11/11/2019 20:00	0.37	0.22	0.15	0	32.5	0	
11/11/2019 20:15	0.38	0.22	0.16	0	32.75	0	
11/11/2019 20:30	0.39	0.22	0.17	0.2	33	0	
11/11/2019 20:45	0.40	0.22	0.18	0	33.25	0.2	
11/11/2019 21:00	0.41	0.22	0.19	0	33.5	0	
11/11/2019 21:15	0.42	0.22	0.20	0	33.75	0	
11/11/2019 21:30	0.42	0.22	0.20	0	34	0	
11/11/2019 21:45	0.43	0.22	0.21	0	34.25	0	
11/11/2019 22:00	0.44	0.22	0.22	0	34.5	0	
11/11/2019 22:15	0.44	0.22	0.22	0	34.75	0	
11/11/2019 22:30	0.45	0.22	0.23	0	35	0	
11/11/2019 22:45	0.46	0.22	0.24	0	35.25	0	
11/11/2019 23:00	0.46	0.22	0.24	0	35.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
11/11/2019 23:15	0.46	0.22	0.24	0	35.75	0	
11/11/2019 23:30	0.47	0.22	0.25	0	36	0	
11/11/2019 23:45	0.48	0.22	0.26	0	36.25	0	
12/11/2019 00:00	0.48	0.22	0.26	0	36.5	0	
12/11/2019 00:15	0.48	0.22	0.26	0	36.75	0	
12/11/2019 00:30	0.49	0.22	0.27	0	37	0	
12/11/2019 00:45	0.49	0.22	0.27	0	37.25	0	
12/11/2019 01:00	0.50	0.22	0.28	0	37.5	0	
12/11/2019 01:15	0.50	0.22	0.28	0	37.75	0	
12/11/2019 01:30	0.50	0.22	0.28	0	38	0	
12/11/2019 01:45	0.50	0.22	0.28	0	38.25	0	
12/11/2019 02:00	0.50	0.22	0.28	0	38.5	0	
12/11/2019 02:15	0.50	0.22	0.28	0	38.75	0	
12/11/2019 02:30	0.50	0.22	0.28	0	39	0	
12/11/2019 02:45	0.51	0.22	0.29	0	39.25	0	
12/11/2019 03:00	0.51	0.22	0.29	0	39.5	0	
12/11/2019 03:15	0.51	0.22	0.29	0	39.75	0	
12/11/2019 03:30	0.51	0.22	0.29	0	40	0	
12/11/2019 03:45	0.51	0.22	0.29	0	40.25	0	
12/11/2019 04:00	0.51	0.22	0.29	0	40.5	0	
12/11/2019 04:15	0.51	0.22	0.29	0	40.75	0	
12/11/2019 04:30	0.51	0.22	0.29	0	41	0	
12/11/2019 04:45	0.51	0.22	0.29	0	41.25	0	
12/11/2019 05:00	0.51	0.22	0.29	0	41.5	0	
12/11/2019 05:15	0.51	0.22	0.29	0	41.75	0	
12/11/2019 05:30	0.51	0.22	0.29	0	42	0	
12/11/2019 05:45	0.50	0.22	0.28	0	42.25	0	
12/11/2019 06:00	0.50	0.22	0.28	0	42.5	0	
12/11/2019 06:15	0.50	0.22	0.28	0	42.75	0	
12/11/2019 06:30	0.50	0.22	0.28	0	43	0	
12/11/2019 06:45	0.50	0.22	0.28	0	43.25	0	
12/11/2019 07:00	0.50	0.22	0.28	0	43.5	0	
12/11/2019 07:15	0.50	0.22	0.28	0	43.75	0	
12/11/2019 07:30	0.50	0.22	0.28	0	44	0	
12/11/2019 07:45	0.50	0.22	0.28	0	44.25	0	
12/11/2019 08:00	0.49	0.22	0.27	0	44.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
12/11/2019 08:15	0.49	0.22	0.27	0	44.75	0	
12/11/2019 08:30	0.49	0.22	0.27	0	45	0	
12/11/2019 08:45	0.49	0.22	0.27	0	45.25	0	
12/11/2019 09:00	0.48	0.22	0.26	0	45.5	0	
12/11/2019 09:15	0.48	0.22	0.26	0	45.75	0	
12/11/2019 09:30	0.48	0.22	0.26	0	46	0	
12/11/2019 09:45	0.48	0.22	0.26	0	46.25	0	
12/11/2019 10:00	0.48	0.22	0.26	0	46.5	0	
12/11/2019 10:15	0.48	0.22	0.26	0	46.75	0	
12/11/2019 10:30	0.48	0.22	0.26	0	47	0	
12/11/2019 10:45	0.48	0.22	0.26	0	47.25	0	
12/11/2019 11:00	0.47	0.22	0.25	0	47.5	0	
12/11/2019 11:15	0.47	0.22	0.25	0	47.75	0	
12/11/2019 11:30	0.47	0.22	0.25	0	48	0	
12/11/2019 11:45	0.47	0.22	0.25	0	48.25	0	
12/11/2019 12:00	0.47	0.22	0.25	0	48.5	0	
12/11/2019 12:15	0.46	0.22	0.24	0	48.75	0	
12/11/2019 12:30	0.46	0.22	0.24	0	49	0	
12/11/2019 12:45	0.46	0.22	0.24	0	49.25	0	
12/11/2019 13:00	0.46	0.22	0.24	0	49.5	0	
12/11/2019 13:15	0.46	0.22	0.24	0.6	49.75	0.2	
12/11/2019 13:30	0.46	0.22	0.24	0	50	1.4	
12/11/2019 13:45	0.46	0.22	0.24	0	50.25	1.6	
12/11/2019 14:00	0.46	0.22	0.24	0	50.5	0.4	
12/11/2019 14:15	0.46	0.22	0.24	0	50.75	0	
12/11/2019 14:30	0.46	0.22	0.24	0	51	0	
12/11/2019 14:45	0.46	0.22	0.24	0	51.25	0	
12/11/2019 15:00	0.46	0.22	0.24	0	51.5	0	
12/11/2019 15:15	0.46	0.22	0.24	0	51.75	0	
12/11/2019 15:30	0.46	0.22	0.24	0	52	0	
12/11/2019 15:45	0.46	0.22	0.24	0	52.25	0	
12/11/2019 16:00	0.46	0.22	0.24	0	52.5	0	
12/11/2019 16:15	0.46	0.22	0.24	0	52.75	0	
12/11/2019 16:30	0.46	0.22	0.24	0	53	0	
12/11/2019 16:45	0.46	0.22	0.24	0	53.25	0	
12/11/2019 17:00	0.46	0.22	0.24	0	53.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
12/11/2019 17:15	0.46	0.22	0.24	0.2	53.75	0	
12/11/2019 17:30	0.46	0.22	0.24	0	54	0.2	
12/11/2019 17:45	0.46	0.22	0.24	0	54.25	0	
12/11/2019 18:00	0.46	0.22	0.24	0	54.5	0	
12/11/2019 18:15	0.46	0.22	0.24	0	54.75	0	
12/11/2019 18:30	0.46	0.22	0.24	0	55	0	
12/11/2019 18:45	0.46	0.22	0.24	0	55.25	0	
12/11/2019 19:00	0.47	0.22	0.25	0	55.5	0	
12/11/2019 19:15	0.47	0.22	0.25	0	55.75	0	
12/11/2019 19:30	0.47	0.22	0.25	0	56	0	
12/11/2019 19:45	0.47	0.22	0.25	0	56.25	0	
12/11/2019 20:00	0.48	0.22	0.26	0	56.5	0	
12/11/2019 20:15	0.48	0.22	0.26	0	56.75	0	
12/11/2019 20:30	0.49	0.22	0.27	0	57	0	
12/11/2019 20:45	0.50	0.22	0.28	0	57.25	0	
12/11/2019 21:00	0.50	0.22	0.28	0	57.5	0	
12/11/2019 21:15	0.51	0.22	0.29	0.2	57.75	0	
12/11/2019 21:30	0.52	0.22	0.30	0	58	0	
12/11/2019 21:45	0.53	0.22	0.31	0	58.25	0	
12/11/2019 22:00	0.53	0.22	0.31	0	58.5	0	
12/11/2019 22:15	0.54	0.22	0.32	0	58.75	0	
12/11/2019 22:30	0.55	0.22	0.33	0	59	0	
12/11/2019 22:45	0.56	0.22	0.34	0	59.25	0	
12/11/2019 23:00	0.57	0.22	0.35	0	59.5	0	
12/11/2019 23:15	0.58	0.22	0.36	0	59.75	0	
12/11/2019 23:30	0.59	0.22	0.37	0	60	0	
12/11/2019 23:45	0.60	0.22	0.38	0	60.25	0	
13/11/2019 00:00	0.60	0.22	0.38	0	60.5	0	
13/11/2019 00:15	0.61	0.22	0.39	0	60.75	0	
13/11/2019 00:30	0.62	0.22	0.40	0	61	0	
13/11/2019 00:45	0.63	0.22	0.41	0	61.25	0	
13/11/2019 01:00	0.64	0.22	0.42	0	61.5	0	
13/11/2019 01:15	0.65	0.22	0.43	0	61.75	0	
13/11/2019 01:30	0.65	0.22	0.43	0	62	0	
13/11/2019 01:45	0.66	0.22	0.44	0	62.25	0	
13/11/2019 02:00	0.67	0.22	0.45	0	62.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
13/11/2019 02:15	0.68	0.22	0.46	0	62.75	0	
13/11/2019 02:30	0.69	0.22	0.47	0	63	0	
13/11/2019 02:45	0.70	0.22	0.48	0	63.25	0	
13/11/2019 03:00	0.70	0.22	0.48	0	63.5	0	
13/11/2019 03:15	0.71	0.22	0.49	0	63.75	0	
13/11/2019 03:30	0.72	0.22	0.50	0	64	0	
13/11/2019 03:45	0.72	0.22	0.50	0	64.25	0	
13/11/2019 04:00	0.73	0.22	0.51	0	64.5	0	
13/11/2019 04:15	0.73	0.22	0.51	0	64.75	0	
13/11/2019 04:30	0.74	0.22	0.52	0	65	0	
13/11/2019 04:45	0.74	0.22	0.52	0	65.25	0	
13/11/2019 05:00	0.75	0.22	0.53	0	65.5	0	
13/11/2019 05:15	0.75	0.22	0.53	0	65.75	0	
13/11/2019 05:30	0.76	0.22	0.54	0	66	0	
13/11/2019 05:45	0.76	0.22	0.54	0	66.25	0	
13/11/2019 06:00	0.76	0.22	0.54	0	66.5	0	
13/11/2019 06:15	0.76	0.22	0.54	0	66.75	0	
13/11/2019 06:30	0.76	0.22	0.54	0	67	0	
13/11/2019 06:45	0.76	0.22	0.54	0	67.25	0	
13/11/2019 07:00	0.76	0.22	0.54	0	67.5	0	
13/11/2019 07:15	0.76	0.22	0.54	0	67.75	0	
13/11/2019 07:30	0.76	0.22	0.54	0	68	0	
13/11/2019 07:45	0.76	0.22	0.54	0	68.25	0	
13/11/2019 08:00	0.75	0.22	0.53	0	68.5	0	
13/11/2019 08:15	0.75	0.22	0.53	0	68.75	0	
13/11/2019 08:30	0.75	0.22	0.53	0	69	0	
13/11/2019 08:45	0.74	0.22	0.52	0	69.25	0	
13/11/2019 09:00	0.74	0.22	0.52	0	69.5	0	
13/11/2019 09:15	0.74	0.22	0.52	0	69.75	0	
13/11/2019 09:30	0.73	0.22	0.51	0	70	0	
13/11/2019 09:45	0.73	0.22	0.51	0	70.25	0	
13/11/2019 10:00	0.72	0.22	0.50	0	70.5	0	
13/11/2019 10:15	0.72	0.22	0.50	0	70.75	0	
13/11/2019 10:30	0.71	0.22	0.49	0	71	0	
13/11/2019 10:45	0.70	0.22	0.48	0	71.25	0	
13/11/2019 11:00	0.70	0.22	0.48	0	71.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
13/11/2019 11:15	0.69	0.22	0.47	0	71.75	0	
13/11/2019 11:30	0.69	0.22	0.47	0	72	0	
13/11/2019 11:45	0.68	0.22	0.46	0	72.25	0	
13/11/2019 12:00	0.68	0.22	0.46	0	72.5	0	
13/11/2019 12:15	0.67	0.22	0.45	0	72.75	0	
13/11/2019 12:30	0.67	0.22	0.45	0	73	0	
13/11/2019 12:45	0.66	0.22	0.44	0	73.25	0	
13/11/2019 13:00	0.65	0.22	0.43	0	73.5	0	
13/11/2019 13:15	0.65	0.22	0.43	0	73.75	0	
13/11/2019 13:30	0.65	0.22	0.43	0	74	0	
13/11/2019 13:45	0.64	0.22	0.42	0	74.25	0	
13/11/2019 14:00	0.64	0.22	0.42	0	74.5	0	
13/11/2019 14:15	0.63	0.22	0.41	0	74.75	0	
13/11/2019 14:30	0.63	0.22	0.41	0	75	0	
13/11/2019 14:45	0.62	0.22	0.40	0	75.25	0	
13/11/2019 15:00	0.61	0.22	0.39	0	75.5	0	
13/11/2019 15:15	0.61	0.22	0.39	0	75.75	0	
13/11/2019 15:30	0.60	0.22	0.38	0	76	0	
13/11/2019 15:45	0.60	0.22	0.38	0	76.25	0	
13/11/2019 16:00	0.60	0.22	0.38	0	76.5	0	
13/11/2019 16:15	0.59	0.22	0.37	0	76.75	0	
13/11/2019 16:30	0.59	0.22	0.37	0	77	0	
13/11/2019 16:45	0.58	0.22	0.36	0	77.25	0	
13/11/2019 17:00	0.58	0.22	0.36	0	77.5	0	
13/11/2019 17:15	0.57	0.22	0.35	0	77.75	0	
13/11/2019 17:30	0.56	0.22	0.34	0	78	0	
13/11/2019 17:45	0.56	0.22	0.34	0	78.25	0	
13/11/2019 18:00	0.56	0.22	0.34	0	78.5	0	
13/11/2019 18:15	0.56	0.22	0.34	0	78.75	0	
13/11/2019 18:30	0.55	0.22	0.33	0	79	0	
13/11/2019 18:45	0.54	0.22	0.32	0	79.25	0	
13/11/2019 19:00	0.54	0.22	0.32	0	79.5	0	
13/11/2019 19:15	0.53	0.22	0.31	0	79.75	0	
13/11/2019 19:30	0.53	0.22	0.31	0	80	0	
13/11/2019 19:45	0.53	0.22	0.31	0	80.25	0	
13/11/2019 20:00	0.52	0.22	0.30	0	80.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
13/11/2019 20:15	0.52	0.22	0.30	0	80.75	0	
13/11/2019 20:30	0.51	0.22	0.29	0	81	0	
13/11/2019 20:45	0.51	0.22	0.29	0	81.25	0	
13/11/2019 21:00	0.50	0.22	0.28	0	81.5	0	
13/11/2019 21:15	0.50	0.22	0.28	0	81.75	0	
13/11/2019 21:30	0.50	0.22	0.28	0	82	0	
13/11/2019 21:45	0.50	0.22	0.28	0	82.25	0	
13/11/2019 22:00	0.49	0.22	0.27	0	82.5	0	
13/11/2019 22:15	0.48	0.22	0.26	0	82.75	0	
13/11/2019 22:30	0.48	0.22	0.26	0	83	0	
13/11/2019 22:45	0.48	0.22	0.26	0	83.25	0	
13/11/2019 23:00	0.48	0.22	0.26	0	83.5	0.2	
13/11/2019 23:15	0.47	0.22	0.25	0	83.75	0.2	
13/11/2019 23:30	0.47	0.22	0.25	0.4	84	0.2	
13/11/2019 23:45	0.46	0.22	0.24	0	84.25	0	
14/11/2019 00:00	0.46	0.22	0.24	0	84.5	0	
14/11/2019 00:15	0.46	0.22	0.24	0	84.75	0	
14/11/2019 00:30	0.46	0.22	0.24	0	85	0	
14/11/2019 00:45	0.45	0.22	0.23	0	85.25	0	
14/11/2019 01:00	0.45	0.22	0.23	0	85.5	0	
14/11/2019 01:15	0.44	0.22	0.22	0	85.75	0	
14/11/2019 01:30	0.44	0.22	0.22	0	86	0	
14/11/2019 01:45	0.44	0.22	0.22	0	86.25	0	
14/11/2019 02:00	0.44	0.22	0.22	0	86.5	0	
14/11/2019 02:15	0.44	0.22	0.22	0	86.75	0	
14/11/2019 02:30	0.43	0.22	0.21	0	87	0	
14/11/2019 02:45	0.43	0.22	0.21	0	87.25	0	
14/11/2019 03:00	0.42	0.22	0.20	0	87.5	0	
14/11/2019 03:15	0.42	0.22	0.20	0	87.75	0	
14/11/2019 03:30	0.42	0.22	0.20	0	88	0	
14/11/2019 03:45	0.42	0.22	0.20	0	88.25	0	
14/11/2019 04:00	0.42	0.22	0.20	0	88.5	0	
14/11/2019 04:15	0.41	0.22	0.19	0	88.75	0	
14/11/2019 04:30	0.41	0.22	0.19	0	89	0	
14/11/2019 04:45	0.40	0.22	0.18	0	89.25	0	
14/11/2019 05:00	0.40	0.22	0.18	0	89.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
14/11/2019 05:15	0.40	0.22	0.18	0.2	89.75	0.2	
14/11/2019 05:30	0.40	0.22	0.18	0.6	90	0	
14/11/2019 05:45	0.39	0.22	0.17	0.4	90.25	0.2	
14/11/2019 06:00	0.39	0.22	0.17	0.2	90.5	0	
14/11/2019 06:15	0.39	0.22	0.17	0.6	90.75	0.6	
14/11/2019 06:30	0.39	0.22	0.17	0.6	91	0.6	
14/11/2019 06:45	0.39	0.22	0.17	0.8	91.25	0.4	
14/11/2019 07:00	0.39	0.22	0.17	0.6	91.5	0.6	
14/11/2019 07:15	0.39	0.22	0.17	0.6	91.75	0.4	
14/11/2019 07:30	0.38	0.22	0.16	0.8	92	0.6	
14/11/2019 07:45	0.38	0.22	0.16	1	92.25	0.6	
14/11/2019 08:00	0.39	0.22	0.17	0.6	92.5	0.6	
14/11/2019 08:15	0.39	0.22	0.17	0.6	92.75	0.4	
14/11/2019 08:30	0.39	0.22	0.17	0.6	93	0.4	
14/11/2019 08:45	0.39	0.22	0.17	1.4	93.25	0.4	
14/11/2019 09:00	0.39	0.22	0.17	1	93.5	0.8	
14/11/2019 09:15	0.39	0.22	0.17	0.8	93.75	1	
14/11/2019 09:30	0.39	0.22	0.17	0.8	94	0.6	
14/11/2019 09:45	0.40	0.22	0.18	0.8	94.25	0.6	
14/11/2019 10:00	0.41	0.22	0.19	0.2	94.5	0.8	
14/11/2019 10:15	0.42	0.22	0.20	1.2	94.75	1.4	
14/11/2019 10:30	0.43	0.22	0.21	1.4	95	1.4	
14/11/2019 10:45	0.45	0.22	0.23	1.2	95.25	1.4	
14/11/2019 11:00	0.48	0.22	0.26	0.8	95.5	1	
14/11/2019 11:15	0.50	0.22	0.28	0.4	95.75	0.6	
14/11/2019 11:30	0.55	0.22	0.33	0.2	96	0.2	
14/11/2019 11:45	0.60	0.22	0.38	0	96.25	1.8	
14/11/2019 12:00	0.66	0.22	0.44	0	96.5	0	
14/11/2019 12:15	0.76	0.22	0.54	0	96.75	0	
14/11/2019 12:30	0.88	0.22	0.66	0	97	0	
14/11/2019 12:45	1.11	0.22	0.89	0	97.25	0	
14/11/2019 13:00	1.36	0.22	1.14	0	97.5	0	
14/11/2019 13:15	1.70	0.22	1.48	0	97.75	0	
14/11/2019 13:30	2.08	0.22	1.86	0.4	98	0.4	
14/11/2019 13:45	2.52	0.22	2.30	0.2	98.25	0	
14/11/2019 14:00	2.99	0.22	2.77	0	98.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
14/11/2019 14:15	3.49	0.22	3.27	0	98.75	0	
14/11/2019 14:30	3.85	0.22	3.63	0	99	0	
14/11/2019 14:45	4.19	0.22	3.97	0	99.25	0	
14/11/2019 15:00	4.53	0.22	4.31	0	99.5	0	
14/11/2019 15:15	4.85	0.22	4.63	0.4	99.75	0	
14/11/2019 15:30	5.12	0.22	4.90	0.2	100	0	
14/11/2019 15:45	5.40	0.22	5.18	0.6	100.25	0	
14/11/2019 16:00	5.64	0.22	5.42	2.4	100.5	0	
14/11/2019 16:15	5.86	0.22	5.64	0.6	100.75	0	
14/11/2019 16:30	6.04	0.22	5.82	0.2	101	0	
14/11/2019 16:45	6.19	0.22	5.97	0	101.25	0.8	
14/11/2019 17:00	6.33	0.22	6.11	0.4	101.5	0.4	
14/11/2019 17:15	6.46	0.22	6.24	0.2	101.75	0	
14/11/2019 17:30	6.57	0.22	6.35	0.8	102	0.4	
14/11/2019 17:45	6.68	0.22	6.46	0.2	102.25	0	
14/11/2019 18:00	6.77	0.22	6.55	0.2	102.5	0	
14/11/2019 18:15	6.84	0.22	6.62	0	102.75	0	
14/11/2019 18:30	6.91	0.22	6.69	0	103	0	
14/11/2019 18:45	6.98	0.22	6.76	0	103.25	0	
14/11/2019 19:00	7.06	0.22	6.84	0	103.5	0	
14/11/2019 19:15	7.13	0.22	6.91	0	103.75	0	
14/11/2019 19:30	7.21	0.22	6.99	0	104	0	
14/11/2019 19:45	7.27	0.22	7.05	0	104.25	0	
14/11/2019 20:00	7.34	0.22	7.12	0	104.5	0	
14/11/2019 20:15	7.41	0.22	7.19	0	104.75	0	
14/11/2019 20:30	7.47	0.22	7.25	0	105	0	
14/11/2019 20:45	7.52	0.22	7.30	0	105.25	0	
14/11/2019 21:00	7.58	0.22	7.36	0	105.5	0	
14/11/2019 21:15	7.63	0.22	7.41	0	105.75	0	
14/11/2019 21:30	7.69	0.22	7.47	0	106	0	
14/11/2019 21:45	7.74	0.22	7.52	0	106.25	0	
14/11/2019 22:00	7.79	0.22	7.57	0	106.5	0	
14/11/2019 22:15	7.84	0.22	7.62	0	106.75	0	
14/11/2019 22:30	7.88	0.22	7.66	0	107	0	
14/11/2019 22:45	7.94	0.22	7.72	0	107.25	0	
14/11/2019 23:00	7.99	0.22	7.77	0	107.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
14/11/2019 23:15	8.04	0.22	7.82	0	107.75	0	
14/11/2019 23:30	8.10	0.22	7.88	0	108	0	
14/11/2019 23:45	8.15	0.22	7.93	0	108.25	0	
15/11/2019 00:00	8.21	0.22	7.99	0	108.5	0	
15/11/2019 00:15	8.27	0.22	8.05	0	108.75	0	
15/11/2019 00:30	8.33	0.22	8.11	0	109	0	
15/11/2019 00:45	8.40	0.22	8.18	0	109.25	0	
15/11/2019 01:00	8.45	0.22	8.23	0	109.5	0	
15/11/2019 01:15	8.50	0.22	8.28	0	109.75	0	
15/11/2019 01:30	8.56	0.22	8.34	0	110	0	
15/11/2019 01:45	8.60	0.22	8.38	0	110.25	0	
15/11/2019 02:00	8.66	0.22	8.44	0	110.5	0	
15/11/2019 02:15	8.71	0.22	8.49	0	110.75	0	
15/11/2019 02:30	8.78	0.22	8.56	0	111	0	
15/11/2019 02:45	8.83	0.22	8.61	0	111.25	0	
15/11/2019 03:00	8.88	0.22	8.66	0	111.5	0	
15/11/2019 03:15	8.95	0.22	8.73	0	111.75	0	
15/11/2019 03:30	9.06	0.22	8.84	0	112	0.4	
15/11/2019 03:45	9.16	0.22	8.94	0.4	112.25	0.2	
15/11/2019 04:00	9.24	0.22	9.02	0	112.5	0	
15/11/2019 04:15	9.35	0.22	9.13	0	112.75	0	
15/11/2019 04:30	9.40	0.22	9.18	0	113	0	
15/11/2019 04:45	9.46	0.22	9.24	0	113.25	0	
15/11/2019 05:00	9.54	0.22	9.32	0.2	113.5	0	
15/11/2019 05:15	9.62	0.22	9.40	0	113.75	0	
15/11/2019 05:30	9.62	0.22	9.40	0	114	0	
15/11/2019 05:45	9.70	0.22	9.48	0	114.25	0	
15/11/2019 06:00	9.70	0.22	9.48	0	114.5	0	
15/11/2019 06:15	9.73	0.22	9.51	0	114.75	0	
15/11/2019 06:30	9.76	0.22	9.54	0	115	0	
15/11/2019 06:45	9.76	0.22	9.54	0	115.25	0	
15/11/2019 07:00	9.78	0.22	9.56	0	115.5	0	
15/11/2019 07:15	9.78	0.22	9.56	0	115.75	0	
15/11/2019 07:30	9.78	0.22	9.56	0	116	0	
15/11/2019 07:45	9.76	0.22	9.54	0	116.25	0	
15/11/2019 08:00	9.76	0.22	9.54	0	116.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
15/11/2019 08:15	9.73	0.22	9.51	0	116.75	0	
15/11/2019 08:30	9.70	0.22	9.48	0	117	0	
15/11/2019 08:45	9.65	0.22	9.43	0	117.25	0	
15/11/2019 09:00	9.62	0.22	9.40	0	117.5	0	
15/11/2019 09:15	9.59	0.22	9.37	0	117.75	0	
15/11/2019 09:30	9.54	0.22	9.32	0	118	0	
15/11/2019 09:45	9.48	0.22	9.26	0	118.25	0	
15/11/2019 10:00	9.40	0.22	9.18	0	118.5	0	
15/11/2019 10:15	9.35	0.22	9.13	0	118.75	0	
15/11/2019 10:30	9.27	0.22	9.05	0	119	0	
15/11/2019 10:45	9.16	0.22	8.94	0	119.25	0	
15/11/2019 11:00	9.11	0.22	8.89	0	119.5	0	
15/11/2019 11:15	9.00	0.22	8.78	0	119.75	0	
15/11/2019 11:30	8.89	0.22	8.67	0	120	0	
15/11/2019 11:45	8.86	0.22	8.64	0	120.25	0	
15/11/2019 12:00	8.82	0.22	8.60	0	120.5	0	
15/11/2019 12:15	8.77	0.22	8.55	0	120.75	0	
15/11/2019 12:30	8.71	0.22	8.49	0	121	0	
15/11/2019 12:45	8.66	0.22	8.44	0	121.25	0	
15/11/2019 13:00	8.60	0.22	8.38	0	121.5	0	
15/11/2019 13:15	8.54	0.22	8.32	0	121.75	0	
15/11/2019 13:30	8.48	0.22	8.26	0	122	0	
15/11/2019 13:45	8.42	0.22	8.20	0	122.25	0	
15/11/2019 14:00	8.35	0.22	8.13	0	122.5	0	
15/11/2019 14:15	8.29	0.22	8.07	0	122.75	0	
15/11/2019 14:30	8.21	0.22	7.99	0	123	0	
15/11/2019 14:45	8.14	0.22	7.92	0	123.25	0	
15/11/2019 15:00	8.00	0.22	7.78	0	123.5	0	
15/11/2019 15:15	7.99	0.22	7.77	0	123.75	0	
15/11/2019 15:30	7.91	0.22	7.69	0	124	0	
15/11/2019 15:45	7.83	0.22	7.61	0	124.25	0	
15/11/2019 16:00	7.75	0.22	7.53	0	124.5	0	
15/11/2019 16:15	7.66	0.22	7.44	0	124.75	0	
15/11/2019 16:30	7.57	0.22	7.35	0	125	0	
15/11/2019 16:45	7.48	0.22	7.26	0	125.25	0	
15/11/2019 17:00	7.40	0.22	7.18	0	125.5	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
15/11/2019 17:15	7.31	0.22	7.09	0	125.75	0	
15/11/2019 17:30	7.22	0.22	7.00	0	126	0	
15/11/2019 17:45	7.14	0.22	6.92	0	126.25	0	
15/11/2019 18:00	7.03	0.22	6.81	0	126.5	0	
15/11/2019 18:15	6.94	0.22	6.72	0	126.75	0	
15/11/2019 18:30	6.83	0.22	6.61	0	127	0	
15/11/2019 18:45	6.73	0.22	6.51	0	127.25	0	
15/11/2019 19:00	6.62	0.22	6.40	0	127.5	0	
15/11/2019 19:15	6.50	0.22	6.28	0	127.75	0	
15/11/2019 19:30	6.39	0.22	6.17	0	128	0	
15/11/2019 19:45	6.28	0.22	6.06	0	128.25	0	
15/11/2019 20:00	6.15	0.22	5.93	0	128.5	0	
15/11/2019 20:15	6.03	0.22	5.81	0	128.75	0	
15/11/2019 20:30	5.92	0.22	5.70	0	129	0	
15/11/2019 20:45	5.81	0.22	5.59	0	129.25	0	
15/11/2019 21:00	5.68	0.22	5.46	0	129.5	0	
15/11/2019 21:15	5.55	0.22	5.33	0	129.75	0	
15/11/2019 21:30	5.42	0.22	5.20		130		
15/11/2019 21:45	5.29	0.22	5.07		130.25		
15/11/2019 22:00	5.16	0.22	4.94		130.5		
15/11/2019 22:15	5.04	0.22	4.82		130.75		
15/11/2019 22:30	4.92	0.22	4.70		131		
15/11/2019 22:45	4.80	0.22	4.58		131.25		
15/11/2019 23:00	4.67	0.22	4.45		131.5		
15/11/2019 23:15	4.53	0.22	4.31		131.75		
15/11/2019 23:30	4.40	0.22	4.18		132		
15/11/2019 23:45	4.28	0.22	4.06		132.25		
16/11/2019 00:00	4.16	0.22	3.94		132.5		
16/11/2019 00:15	4.04	0.22	3.82		132.75		
16/11/2019 00:30	3.91	0.22	3.69		133		
16/11/2019 00:45	3.80	0.22	3.58		133.25		
16/11/2019 01:00	3.69	0.22	3.47		133.5		
16/11/2019 01:15	3.58	0.22	3.36		133.75		
16/11/2019 01:30	3.48	0.22	3.26		134		
16/11/2019 01:45	3.34	0.22	3.12		134.25		
16/11/2019 02:00	3.21	0.22	2.99		134.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
16/11/2019 02:15	3.08	0.22	2.86		134.75		
16/11/2019 02:30	2.96	0.22	2.74		135		
16/11/2019 02:45	2.84	0.22	2.62		135.25		
16/11/2019 03:00	2.74	0.22	2.52		135.5		
16/11/2019 03:15	2.62	0.22	2.40		135.75		
16/11/2019 03:30	2.53	0.22	2.31		136		
16/11/2019 03:45	2.43	0.22	2.21		136.25		
16/11/2019 04:00	2.34	0.22	2.12		136.5		
16/11/2019 04:15	2.26	0.22	2.04		136.75		
16/11/2019 04:30	2.18	0.22	1.96		137		
16/11/2019 04:45	2.11	0.22	1.89		137.25		
16/11/2019 05:00	2.04	0.22	1.82		137.5		
16/11/2019 05:15	1.96	0.22	1.74		137.75		
16/11/2019 05:30	1.90	0.22	1.68		138		
16/11/2019 05:45	1.84	0.22	1.62		138.25		
16/11/2019 06:00	1.78	0.22	1.56		138.5		
16/11/2019 06:15	1.73	0.22	1.51		138.75		
16/11/2019 06:30	1.67	0.22	1.45		139		
16/11/2019 06:45	1.62	0.22	1.40		139.25		
16/11/2019 07:00	1.58	0.22	1.36		139.5		
16/11/2019 07:15	1.53	0.22	1.31		139.75		
16/11/2019 07:30	1.48	0.22	1.26		140		
16/11/2019 07:45	1.44	0.22	1.22		140.25		
16/11/2019 08:00	1.40	0.22	1.18		140.5		
16/11/2019 08:15	1.36	0.22	1.14		140.75		
16/11/2019 08:30	1.32	0.22	1.10		141		
16/11/2019 08:45	1.28	0.22	1.06		141.25		
16/11/2019 09:00	1.24	0.22	1.02		141.5		
16/11/2019 09:15	1.22	0.22	1.00		141.75		
16/11/2019 09:30	1.19	0.22	0.97		142		
16/11/2019 09:45	1.16	0.22	0.94		142.25		
16/11/2019 10:00	1.13	0.22	0.91		142.5		
16/11/2019 10:15	1.11	0.22	0.89		142.75		
16/11/2019 10:30	1.10	0.22	0.88		143		
16/11/2019 10:45	1.06	0.22	0.84		143.25		
16/11/2019 11:00	1.04	0.22	0.82		143.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
16/11/2019 11:15	1.01	0.22	0.79		143.75		
16/11/2019 11:30	0.99	0.22	0.77		144		
16/11/2019 11:45	0.97	0.22	0.75		144.25		
16/11/2019 12:00	0.96	0.22	0.74		144.5		
16/11/2019 12:15	0.93	0.22	0.71		144.75		
16/11/2019 12:30	0.92	0.22	0.70		145		
16/11/2019 12:45	0.91	0.22	0.69		145.25		
16/11/2019 13:00	0.90	0.22	0.68		145.5		
16/11/2019 13:15	0.88	0.22	0.66		145.75		
16/11/2019 13:30	0.87	0.22	0.65		146		
16/11/2019 13:45	0.86	0.22	0.64		146.25		
16/11/2019 14:00	0.86	0.22	0.64		146.5		
16/11/2019 14:15	0.85	0.22	0.63		146.75		
16/11/2019 14:30	0.84	0.22	0.62		147		
16/11/2019 14:45	0.82	0.22	0.60		147.25		
16/11/2019 15:00	0.81	0.22	0.59		147.5		
16/11/2019 15:15	0.80	0.22	0.58		147.75		
16/11/2019 15:30	0.79	0.22	0.57		148		
16/11/2019 15:45	0.78	0.22	0.56		148.25		
16/11/2019 16:00	0.77	0.22	0.55		148.5		
16/11/2019 16:15	0.76	0.22	0.54		148.75		
16/11/2019 16:30	0.76	0.22	0.54		149		
16/11/2019 16:45	0.76	0.22	0.54		149.25		
16/11/2019 17:00	0.75	0.22	0.53		149.5		
16/11/2019 17:15	0.74	0.22	0.52		149.75		
16/11/2019 17:30	0.73	0.22	0.51		150		
16/11/2019 17:45	0.72	0.22	0.50		150.25		
16/11/2019 18:00	0.72	0.22	0.50		150.5		
16/11/2019 18:15	0.71	0.22	0.49		150.75		
16/11/2019 18:30	0.70	0.22	0.48		151		
16/11/2019 18:45	0.70	0.22	0.48		151.25		
16/11/2019 19:00	0.69	0.22	0.47		151.5		
16/11/2019 19:15	0.68	0.22	0.46		151.75		
16/11/2019 19:30	0.67	0.22	0.45		152		
16/11/2019 19:45	0.67	0.22	0.45		152.25		
16/11/2019 20:00	0.66	0.22	0.44		152.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
16/11/2019 20:15	0.66	0.22	0.44		152.75		
16/11/2019 20:30	0.65	0.22	0.43		153		
16/11/2019 20:45	0.65	0.22	0.43		153.25		
16/11/2019 21:00	0.65	0.22	0.43		153.5		
16/11/2019 21:15	0.64	0.22	0.42		153.75		
16/11/2019 21:30	0.63	0.22	0.41		154		
16/11/2019 21:45	0.63	0.22	0.41		154.25		
16/11/2019 22:00	0.62	0.22	0.40		154.5		
16/11/2019 22:15	0.62	0.22	0.40		154.75		
16/11/2019 22:30	0.61	0.22	0.39		155		
16/11/2019 22:45	0.60	0.22	0.38		155.25		
16/11/2019 23:00	0.60	0.22	0.38		155.5		
16/11/2019 23:15	0.60	0.22	0.38		155.75		
16/11/2019 23:30	0.60	0.22	0.38		156		
16/11/2019 23:45	0.59	0.22	0.37		156.25		
17/11/2019 00:00	0.58	0.22	0.36		156.5		
17/11/2019 00:15	0.58	0.22	0.36		156.75		
17/11/2019 00:30	0.57	0.22	0.35		157		
17/11/2019 00:45	0.57	0.22	0.35		157.25		
17/11/2019 01:00	0.56	0.22	0.34		157.5		
17/11/2019 01:15	0.56	0.22	0.34		157.75		
17/11/2019 01:30	0.56	0.22	0.34		158		
17/11/2019 01:45	0.55	0.22	0.33		158.25		
17/11/2019 02:00	0.55	0.22	0.33		158.5		
17/11/2019 02:15	0.54	0.22	0.32		158.75		
17/11/2019 02:30	0.54	0.22	0.32		159		
17/11/2019 02:45	0.53	0.22	0.31		159.25		
17/11/2019 03:00	0.53	0.22	0.31		159.5		
17/11/2019 03:15	0.53	0.22	0.31		159.75		
17/11/2019 03:30	0.53	0.22	0.31		160		
17/11/2019 03:45	0.52	0.22	0.30		160.25		
17/11/2019 04:00	0.52	0.22	0.30		160.5		
17/11/2019 04:15	0.51	0.22	0.29		160.75		
17/11/2019 04:30	0.50	0.22	0.28		161		
17/11/2019 04:45	0.50	0.22	0.28		161.25		
17/11/2019 05:00	0.50	0.22	0.28		161.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
17/11/2019 05:15	0.50	0.22	0.28		161.75		
17/11/2019 05:30	0.49	0.22	0.27		162		
17/11/2019 05:45	0.49	0.22	0.27		162.25		
17/11/2019 06:00	0.48	0.22	0.26		162.5		
17/11/2019 06:15	0.48	0.22	0.26		162.75		
17/11/2019 06:30	0.48	0.22	0.26		163		
17/11/2019 06:45	0.47	0.22	0.25		163.25		
17/11/2019 07:00	0.47	0.22	0.25		163.5		
17/11/2019 07:15	0.46	0.22	0.24		163.75		
17/11/2019 07:30	0.46	0.22	0.24		164		
17/11/2019 07:45	0.46	0.22	0.24		164.25		
17/11/2019 08:00	0.46	0.22	0.24		164.5		
17/11/2019 08:15	0.45	0.22	0.23		164.75		
17/11/2019 08:30	0.45	0.22	0.23		165		
17/11/2019 08:45	0.44	0.22	0.22		165.25		
17/11/2019 09:00	0.44	0.22	0.22		165.5		
17/11/2019 09:15	0.44	0.22	0.22		165.75		
17/11/2019 09:30	0.44	0.22	0.22		166		
17/11/2019 09:45	0.43	0.22	0.21		166.25		
17/11/2019 10:00	0.43	0.22	0.21		166.5		
17/11/2019 10:15	0.42	0.22	0.20		166.75		
17/11/2019 10:30	0.42	0.22	0.20		167		
17/11/2019 10:45	0.42	0.22	0.20		167.25		
17/11/2019 11:00	0.42	0.22	0.20		167.5		
17/11/2019 11:15	0.42	0.22	0.20		167.75		
17/11/2019 11:30	0.41	0.22	0.19		168		
17/11/2019 11:45	0.41	0.22	0.19		168.25		
17/11/2019 12:00	0.41	0.22	0.19		168.5		
17/11/2019 12:15	0.40	0.22	0.18		168.75		
17/11/2019 12:30	0.40	0.22	0.18		169		
17/11/2019 12:45	0.40	0.22	0.18		169.25		
17/11/2019 13:00	0.40	0.22	0.18		169.5		
17/11/2019 13:15	0.40	0.22	0.18		169.75		
17/11/2019 13:30	0.39	0.22	0.17		170		
17/11/2019 13:45	0.39	0.22	0.17		170.25		
17/11/2019 14:00	0.39	0.22	0.17		170.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
17/11/2019 14:15	0.39	0.22	0.17		170.75		
17/11/2019 14:30	0.39	0.22	0.17		171		
17/11/2019 14:45	0.39	0.22	0.17		171.25		
17/11/2019 15:00	0.38	0.22	0.16		171.5		
17/11/2019 15:15	0.38	0.22	0.16		171.75		
17/11/2019 15:30	0.38	0.22	0.16		172		
17/11/2019 15:45	0.37	0.22	0.15		172.25		
17/11/2019 16:00	0.37	0.22	0.15		172.5		
17/11/2019 16:15	0.37	0.22	0.15		172.75		
17/11/2019 16:30	0.37	0.22	0.15		173		
17/11/2019 16:45	0.37	0.22	0.15		173.25		
17/11/2019 17:00	0.36	0.22	0.14		173.5		
17/11/2019 17:15	0.36	0.22	0.14		173.75		
17/11/2019 17:30	0.36	0.22	0.14		174		
17/11/2019 17:45	0.36	0.22	0.14		174.25		
17/11/2019 18:00	0.36	0.22	0.14		174.5		
17/11/2019 18:15	0.35	0.22	0.13		174.75		
17/11/2019 18:30	0.35	0.22	0.13		175		
17/11/2019 18:45	0.35	0.22	0.13		175.25		
17/11/2019 19:00	0.35	0.22	0.13		175.5		
17/11/2019 19:15	0.35	0.22	0.13		175.75		
17/11/2019 19:30	0.35	0.22	0.13		176		
17/11/2019 19:45	0.34	0.22	0.12		176.25		
17/11/2019 20:00	0.34	0.22	0.12		176.5		
17/11/2019 20:15	0.34	0.22	0.12		176.75		
17/11/2019 20:30	0.34	0.22	0.12		177		
17/11/2019 20:45	0.34	0.22	0.12		177.25		
17/11/2019 21:00	0.34	0.22	0.12		177.5		
17/11/2019 21:15	0.33	0.22	0.11		177.75		
17/11/2019 21:30	0.33	0.22	0.11		178		
17/11/2019 21:45	0.33	0.22	0.11		178.25		
17/11/2019 22:00	0.33	0.22	0.11		178.5		
17/11/2019 22:15	0.32	0.22	0.10		178.75		
17/11/2019 22:30	0.32	0.22	0.10		179		
17/11/2019 22:45	0.32	0.22	0.10		179.25		
17/11/2019 23:00	0.32	0.22	0.10		179.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
17/11/2019 23:15	0.32	0.22	0.10		179.75		
17/11/2019 23:30	0.32	0.22	0.10		180		
17/11/2019 23:45	0.32	0.22	0.10		180.25		
18/11/2019 00:00	0.31	0.22	0.09		180.5		
18/11/2019 00:15	0.31	0.22	0.09		180.75		
18/11/2019 00:30	0.31	0.22	0.09		181		
18/11/2019 00:45	0.31	0.22	0.09		181.25		
18/11/2019 01:00	0.30	0.22	0.08		181.5		
18/11/2019 01:15	0.30	0.22	0.08		181.75		
18/11/2019 01:30	0.30	0.22	0.08		182		
18/11/2019 01:45	0.30	0.22	0.08		182.25		
18/11/2019 02:00	0.30	0.22	0.08		182.5		
18/11/2019 02:15	0.30	0.22	0.08		182.75		
18/11/2019 02:30	0.30	0.22	0.08		183		
18/11/2019 02:45	0.30	0.22	0.08		183.25		
18/11/2019 03:00	0.30	0.22	0.08		183.5		
18/11/2019 03:15	0.30	0.22	0.08		183.75		
18/11/2019 03:30	0.29	0.22	0.07		184		
18/11/2019 03:45	0.29	0.22	0.07		184.25		
18/11/2019 04:00	0.29	0.22	0.07		184.5		
18/11/2019 04:15	0.29	0.22	0.07		184.75		
18/11/2019 04:30	0.29	0.22	0.07		185		
18/11/2019 04:45	0.29	0.22	0.07		185.25		
18/11/2019 05:00	0.29	0.22	0.07		185.5		
18/11/2019 05:15	0.29	0.22	0.07		185.75		
18/11/2019 05:30	0.29	0.22	0.07		186		
18/11/2019 05:45	0.29	0.22	0.07		186.25		
18/11/2019 06:00	0.29	0.22	0.07		186.5		
18/11/2019 06:15	0.29	0.22	0.07		186.75		
18/11/2019 06:30	0.29	0.22	0.07		187		
18/11/2019 06:45	0.29	0.22	0.07		187.25		
18/11/2019 07:00	0.29	0.22	0.07		187.5		
18/11/2019 07:15	0.29	0.22	0.07		187.75		
18/11/2019 07:30	0.29	0.22	0.07		188		
18/11/2019 07:45	0.29	0.22	0.07		188.25		
18/11/2019 08:00	0.29	0.22	0.07		188.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
18/11/2019 08:15	0.29	0.22	0.07		188.75		
18/11/2019 08:30	0.29	0.22	0.07		189		
18/11/2019 08:45	0.29	0.22	0.07		189.25		
18/11/2019 09:00	0.29	0.22	0.07		189.5		
18/11/2019 09:15	0.29	0.22	0.07		189.75		
18/11/2019 09:30	0.28	0.22	0.06		190		
18/11/2019 09:45	0.28	0.22	0.06		190.25		
18/11/2019 10:00	0.28	0.22	0.06		190.5		
18/11/2019 10:15	0.28	0.22	0.06		190.75		
18/11/2019 10:30	0.28	0.22	0.06		191		
18/11/2019 10:45	0.28	0.22	0.06		191.25		
18/11/2019 11:00	0.28	0.22	0.06		191.5		
18/11/2019 11:15	0.28	0.22	0.06		191.75		
18/11/2019 11:30	0.28	0.22	0.06		192		
18/11/2019 11:45	0.28	0.22	0.06		192.25		
18/11/2019 12:00	0.28	0.22	0.06		192.5		
18/11/2019 12:15	0.28	0.22	0.06		192.75		
18/11/2019 12:30	0.28	0.22	0.06		193		
18/11/2019 12:45	0.28	0.22	0.06		193.25		
18/11/2019 13:00	0.28	0.22	0.06		193.5		
18/11/2019 13:15	0.28	0.22	0.06		193.75		
18/11/2019 13:30	0.28	0.22	0.06		194		
18/11/2019 13:45	0.28	0.22	0.06		194.25		
18/11/2019 14:00	0.28	0.22	0.06		194.5		
18/11/2019 14:15	0.28	0.22	0.06		194.75		
18/11/2019 14:30	0.28	0.22	0.06		195		
18/11/2019 14:45	0.28	0.22	0.06		195.25		
18/11/2019 15:00	0.28	0.22	0.06		195.5		
18/11/2019 15:15	0.28	0.22	0.06		195.75		
18/11/2019 15:30	0.28	0.22	0.06		196		
18/11/2019 15:45	0.28	0.22	0.06		196.25		
18/11/2019 16:00	0.28	0.22	0.06		196.5		
18/11/2019 16:15	0.28	0.22	0.06		196.75		
18/11/2019 16:30	0.28	0.22	0.06		197		
18/11/2019 16:45	0.28	0.22	0.06		197.25		
18/11/2019 17:00	0.28	0.22	0.06		197.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
18/11/2019 17:15	0.28	0.22	0.06		197.75		
18/11/2019 17:30	0.28	0.22	0.06		198		
18/11/2019 17:45	0.28	0.22	0.06		198.25		
18/11/2019 18:00	0.28	0.22	0.06		198.5		
18/11/2019 18:15	0.28	0.22	0.06		198.75		
18/11/2019 18:30	0.28	0.22	0.06		199		
18/11/2019 18:45	0.28	0.22	0.06		199.25		
18/11/2019 19:00	0.28	0.22	0.06		199.5		
18/11/2019 19:15	0.28	0.22	0.06		199.75		
18/11/2019 19:30	0.28	0.22	0.06		200		
18/11/2019 19:45	0.28	0.22	0.06		200.25		
18/11/2019 20:00	0.28	0.22	0.06		200.5		
18/11/2019 20:15	0.28	0.22	0.06		200.75		
18/11/2019 20:30	0.28	0.22	0.06		201		
18/11/2019 20:45	0.27	0.22	0.05		201.25		
18/11/2019 21:00	0.27	0.22	0.05		201.5		
18/11/2019 21:15	0.27	0.22	0.05		201.75		
18/11/2019 21:30	0.27	0.22	0.05		202		
18/11/2019 21:45	0.27	0.22	0.05		202.25		
18/11/2019 22:00	0.27	0.22	0.05		202.5		
18/11/2019 22:15	0.27	0.22	0.05		202.75		
18/11/2019 22:30	0.27	0.22	0.05		203		
18/11/2019 22:45	0.27	0.22	0.05		203.25		
18/11/2019 23:00	0.27	0.22	0.05		203.5		
18/11/2019 23:15	0.27	0.22	0.05		203.75		
18/11/2019 23:30	0.27	0.22	0.05		204		
18/11/2019 23:45	0.27	0.22	0.05		204.25		
19/11/2019 00:00	0.27	0.22	0.05		204.5		
19/11/2019 00:15	0.27	0.22	0.05		204.75		
19/11/2019 00:30	0.27	0.22	0.05		205		
19/11/2019 00:45	0.27	0.22	0.05		205.25		
19/11/2019 01:00	0.27	0.22	0.05		205.5		
19/11/2019 01:15	0.27	0.22	0.05		205.75		
19/11/2019 01:30	0.27	0.22	0.05		206		
19/11/2019 01:45	0.27	0.22	0.05		206.25		
19/11/2019 02:00	0.27	0.22	0.05		206.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
19/11/2019 02:15	0.26	0.22	0.04		206.75		
19/11/2019 02:30	0.26	0.22	0.04		207		
19/11/2019 02:45	0.26	0.22	0.04		207.25		
19/11/2019 03:00	0.26	0.22	0.04		207.5		
19/11/2019 03:15	0.26	0.22	0.04		207.75		
19/11/2019 03:30	0.26	0.22	0.04		208		
19/11/2019 03:45	0.26	0.22	0.04		208.25		
19/11/2019 04:00	0.26	0.22	0.04		208.5		
19/11/2019 04:15	0.26	0.22	0.04		208.75		
19/11/2019 04:30	0.26	0.22	0.04		209		
19/11/2019 04:45	0.26	0.22	0.04		209.25		
19/11/2019 05:00	0.26	0.22	0.04		209.5		
19/11/2019 05:15	0.26	0.22	0.04		209.75		
19/11/2019 05:30	0.26	0.22	0.04		210		
19/11/2019 05:45	0.26	0.22	0.04		210.25		
19/11/2019 06:00	0.26	0.22	0.04		210.5		
19/11/2019 06:15	0.25	0.22	0.03		210.75		
19/11/2019 06:30	0.25	0.22	0.03		211		
19/11/2019 06:45	0.25	0.22	0.03		211.25		
19/11/2019 07:00	0.25	0.22	0.03		211.5		
19/11/2019 07:15	0.25	0.22	0.03		211.75		
19/11/2019 07:30	0.25	0.22	0.03		212		
19/11/2019 07:45	0.25	0.22	0.03		212.25		
19/11/2019 08:00	0.25	0.22	0.03		212.5		
19/11/2019 08:15	0.25	0.22	0.03		212.75		
19/11/2019 08:30	0.25	0.22	0.03		213		
19/11/2019 08:45	0.25	0.22	0.03		213.25		
19/11/2019 09:00	0.25	0.22	0.03		213.5		
19/11/2019 09:15	0.25	0.22	0.03		213.75		
19/11/2019 09:30	0.24	0.22	0.02		214		
19/11/2019 09:45	0.24	0.22	0.02		214.25		
19/11/2019 10:00	0.24	0.22	0.02		214.5		
19/11/2019 10:15	0.24	0.22	0.02		214.75		
19/11/2019 10:30	0.24	0.22	0.02		215		
19/11/2019 10:45	0.24	0.22	0.02		215.25		
19/11/2019 11:00	0.24	0.22	0.02		215.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
19/11/2019 11:15	0.24	0.22	0.02		215.75		
19/11/2019 11:30	0.24	0.22	0.02		216		
19/11/2019 11:45	0.24	0.22	0.02		216.25		
19/11/2019 12:00	0.24	0.22	0.02		216.5		
19/11/2019 12:15	0.24	0.22	0.02		216.75		
19/11/2019 12:30	0.24	0.22	0.02		217		
19/11/2019 12:45	0.24	0.22	0.02		217.25		
19/11/2019 13:00	0.24	0.22	0.02		217.5		
19/11/2019 13:15	0.24	0.22	0.02		217.75		
19/11/2019 13:30	0.24	0.22	0.02		218		
19/11/2019 13:45	0.24	0.22	0.02		218.25		
19/11/2019 14:00	0.24	0.22	0.02		218.5		
19/11/2019 14:15	0.24	0.22	0.02		218.75		
19/11/2019 14:30	0.24	0.22	0.02		219		
19/11/2019 14:45	0.24	0.22	0.02		219.25		
19/11/2019 15:00	0.24	0.22	0.02		219.5		
19/11/2019 15:15	0.24	0.22	0.02		219.75		
19/11/2019 15:30	0.23	0.22	0.01		220		
19/11/2019 15:45	0.23	0.22	0.01		220.25		
19/11/2019 16:00	0.23	0.22	0.01		220.5		
19/11/2019 16:15	0.23	0.22	0.01		220.75		
19/11/2019 16:30	0.23	0.22	0.01		221		
19/11/2019 16:45	0.23	0.22	0.01		221.25		
19/11/2019 17:00	0.23	0.22	0.01		221.5		
19/11/2019 17:15	0.23	0.22	0.01		221.75		
19/11/2019 17:30	0.23	0.22	0.01		222		
19/11/2019 17:45	0.23	0.22	0.01		222.25		
19/11/2019 18:00	0.23	0.22	0.01		222.5		
19/11/2019 18:15	0.22	0.22	0.00		222.75		
19/11/2019 18:30	0.22	0.22	0.00		223		
19/11/2019 18:45	0.22	0.22	0.00		223.25		
19/11/2019 19:00	0.22	0.22	0.00		223.5		
19/11/2019 19:15	0.22	0.22	0.00		223.75		
19/11/2019 19:30	0.22	0.22	0.00		224		
19/11/2019 19:45	0.22	0.22	0.00		224.25		
19/11/2019 20:00	0.22	0.22	0.00		224.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
19/11/2019 20:15	0.22	0.22	0.00		224.75		
19/11/2019 20:30	0.22	0.22	0.00		225		
19/11/2019 20:45	0.22	0.22	0.00		225.25		
19/11/2019 21:00	0.22	0.22	0.00		225.5		
19/11/2019 21:15	0.22	0.22	0.00		225.75		
19/11/2019 21:30	0.22	0.22	0.00		226		
19/11/2019 21:45	0.22	0.22	0.00		226.25		
19/11/2019 22:00	0.22	0.22	0.00		226.5		
19/11/2019 22:15	0.22	0.22	0.00		226.75		
19/11/2019 22:30	0.22	0.22	0.00		227		
19/11/2019 22:45	0.22	0.22	0.00		227.25		
19/11/2019 23:00	0.22	0.22	0.00		227.5		
19/11/2019 23:15	0.22	0.22	0.00		227.75		
19/11/2019 23:30	0.22	0.22	0.00		228		
19/11/2019 23:45	0.22	0.22	0.00		228.25		
20/11/2019 00:00	0.22	0.22	0.00		228.5		
20/11/2019 00:15	0.21	0.21	0.00		228.75		
20/11/2019 00:30	0.21	0.21	0.00		229		
20/11/2019 00:45	0.21	0.21	0.00		229.25		
20/11/2019 01:00	0.21	0.21	0.00		229.5		
20/11/2019 01:15	0.21	0.21	0.00		229.75		
20/11/2019 01:30	0.21	0.21	0.00		230		
20/11/2019 01:45	0.21	0.21	0.00		230.25		
20/11/2019 02:00	0.21	0.21	0.00		230.5		
20/11/2019 02:15	0.21	0.21	0.00		230.75		
20/11/2019 02:30	0.21	0.21	0.00		231		
20/11/2019 02:45	0.21	0.21	0.00		231.25		
20/11/2019 03:00	0.21	0.21	0.00		231.5		
20/11/2019 03:15	0.21	0.21	0.00		231.75		
20/11/2019 03:30	0.21	0.21	0.00		232		
20/11/2019 03:45	0.21	0.21	0.00		232.25		
20/11/2019 04:00	0.21	0.21	0.00		232.5		
20/11/2019 04:15	0.20	0.20	0.00		232.75		
20/11/2019 04:30	0.20	0.20	0.00		233		
20/11/2019 04:45	0.20	0.20	0.00		233.25		
20/11/2019 05:00	0.20	0.20	0.00		233.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
20/11/2019 05:15	0.20	0.20	0.00		233.75		
20/11/2019 05:30	0.20	0.20	0.00		234		
20/11/2019 05:45	0.20	0.20	0.00		234.25		
20/11/2019 06:00	0.20	0.20	0.00		234.5		
20/11/2019 06:15	0.20	0.20	0.00		234.75		
20/11/2019 06:30	0.20	0.20	0.00		235		
20/11/2019 06:45	0.20	0.20	0.00		235.25		
20/11/2019 07:00	0.20	0.20	0.00		235.5		
20/11/2019 07:15	0.20	0.20	0.00		235.75		
20/11/2019 07:30	0.20	0.20	0.00		236		
20/11/2019 07:45	0.20	0.20	0.00		236.25		
20/11/2019 08:00	0.20	0.20	0.00		236.5		
20/11/2019 08:15	0.20	0.20	0.00		236.75		
20/11/2019 08:30	0.20	0.20	0.00		237		
20/11/2019 08:45	0.20	0.20	0.00		237.25		
20/11/2019 09:00	0.20	0.20	0.00		237.5		
20/11/2019 09:15	0.20	0.20	0.00		237.75		
20/11/2019 09:30	0.20	0.20	0.00		238		
20/11/2019 09:45	0.20	0.20	0.00		238.25		
20/11/2019 10:00	0.20	0.20	0.00		238.5		
20/11/2019 10:15	0.20	0.20	0.00		238.75		
20/11/2019 10:30	0.20	0.20	0.00		239		
20/11/2019 10:45	0.19	0.19	0.00		239.25		
20/11/2019 11:00	0.19	0.19	0.00		239.5		
20/11/2019 11:15	0.19	0.19	0.00		239.75		
20/11/2019 11:30	0.19	0.19	0.00		240		
20/11/2019 11:45	0.19	0.19	0.00		240.25		
20/11/2019 12:00	0.19	0.19	0.00		240.5		
20/11/2019 12:15	0.19	0.19	0.00		240.75		
20/11/2019 12:30	0.19	0.19	0.00		241		
20/11/2019 12:45	0.19	0.19	0.00		241.25		
20/11/2019 13:00	0.19	0.19	0.00		241.5		
20/11/2019 13:15	0.19	0.19	0.00		241.75		
20/11/2019 13:30	0.19	0.19	0.00		242		
20/11/2019 13:45	0.19	0.19	0.00		242.25		
20/11/2019 14:00	0.19	0.19	0.00		242.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
20/11/2019 14:15	0.19	0.19	0.00		242.75		
20/11/2019 14:30	0.19	0.19	0.00		243		
20/11/2019 14:45	0.19	0.19	0.00		243.25		
20/11/2019 15:00	0.19	0.19	0.00		243.5		
20/11/2019 15:15	0.19	0.19	0.00		243.75		
20/11/2019 15:30	0.19	0.19	0.00		244		
20/11/2019 15:45	0.19	0.19	0.00		244.25		
20/11/2019 16:00	0.19	0.19	0.00		244.5		
20/11/2019 16:15	0.19	0.19	0.00		244.75		
20/11/2019 16:30	0.19	0.19	0.00		245		
20/11/2019 16:45	0.19	0.19	0.00		245.25		
20/11/2019 17:00	0.19	0.19	0.00		245.5		
20/11/2019 17:15	0.19	0.19	0.00		245.75		
20/11/2019 17:30	0.19	0.19	0.00		246		
20/11/2019 17:45	0.19	0.19	0.00		246.25		
20/11/2019 18:00	0.19	0.19	0.00		246.5		
20/11/2019 18:15	0.19	0.19	0.00		246.75		
20/11/2019 18:30	0.19	0.19	0.00		247		
20/11/2019 18:45	0.18	0.18	0.00		247.25		
20/11/2019 19:00	0.19	0.19	0.00		247.5		
20/11/2019 19:15	0.19	0.19	0.00		247.75		
20/11/2019 19:30	0.19	0.19	0.00		248		
20/11/2019 19:45	0.18	0.18	0.00		248.25		
20/11/2019 20:00	0.18	0.18	0.00		248.5		
20/11/2019 20:15	0.18	0.18	0.00		248.75		
20/11/2019 20:30	0.18	0.18	0.00		249		
20/11/2019 20:45	0.18	0.18	0.00		249.25		
20/11/2019 21:00	0.18	0.18	0.00		249.5		
20/11/2019 21:15	0.18	0.18	0.00		249.75		
20/11/2019 21:30	0.18	0.18	0.00		250		
20/11/2019 21:45	0.18	0.18	0.00		250.25		
20/11/2019 22:00	0.18	0.18	0.00		250.5		
20/11/2019 22:15	0.18	0.18	0.00		250.75		
20/11/2019 22:30	0.18	0.18	0.00		251		
20/11/2019 22:45	0.18	0.18	0.00		251.25		
20/11/2019 23:00	0.18	0.18	0.00		251.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
20/11/2019 23:15	0.18	0.18	0.00		251.75		
20/11/2019 23:30	0.18	0.18	0.00		252		
20/11/2019 23:45	0.18	0.18	0.00		252.25		
21/11/2019 00:00	0.18	0.18	0.00		252.5		
21/11/2019 00:15	0.18	0.18	0.00		252.75		
21/11/2019 00:30	0.18	0.18	0.00		253		
21/11/2019 00:45	0.18	0.18	0.00		253.25		
21/11/2019 01:00	0.18	0.18	0.00		253.5		
21/11/2019 01:15	0.18	0.18	0.00		253.75		
21/11/2019 01:30	0.18	0.18	0.00		254		
21/11/2019 01:45	0.18	0.18	0.00		254.25		
21/11/2019 02:00	0.18	0.18	0.00		254.5		
21/11/2019 02:15	0.18	0.18	0.00		254.75		
21/11/2019 02:30	0.18	0.18	0.00		255		
21/11/2019 02:45	0.18	0.18	0.00		255.25		
21/11/2019 03:00	0.18	0.18	0.00		255.5		
21/11/2019 03:15	0.18	0.18	0.00		255.75		
21/11/2019 03:30	0.18	0.18	0.00		256		
21/11/2019 03:45	0.18	0.18	0.00		256.25		
21/11/2019 04:00	0.18	0.18	0.00		256.5		
21/11/2019 04:15	0.18	0.18	0.00		256.75		
21/11/2019 04:30	0.18	0.18	0.00		257		
21/11/2019 04:45	0.18	0.18	0.00		257.25		
21/11/2019 05:00	0.18	0.18	0.00		257.5		
21/11/2019 05:15	0.18	0.18	0.00		257.75		
21/11/2019 05:30	0.18	0.18	0.00		258		
21/11/2019 05:45	0.18	0.18	0.00		258.25		
21/11/2019 06:00	0.18	0.18	0.00		258.5		
21/11/2019 06:15	0.18	0.18	0.00		258.75		
21/11/2019 06:30	0.18	0.18	0.00		259		
21/11/2019 06:45	0.18	0.18	0.00		259.25		
21/11/2019 07:00	0.18	0.18	0.00		259.5		
21/11/2019 07:15	0.18	0.18	0.00		259.75		
21/11/2019 07:30	0.18	0.18	0.00		260		
21/11/2019 07:45	0.18	0.18	0.00		260.25		
21/11/2019 08:00	0.18	0.18	0.00		260.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
21/11/2019 08:15	0.18	0.18	0.00		260.75		
21/11/2019 08:30	0.18	0.18	0.00		261		
21/11/2019 08:45	0.18	0.18	0.00		261.25		
21/11/2019 09:00	0.17	0.17	0.00		261.5		
21/11/2019 09:15	0.17	0.17	0.00		261.75		
21/11/2019 09:30	0.17	0.17	0.00		262		
21/11/2019 09:45	0.17	0.17	0.00		262.25		
21/11/2019 10:00	0.17	0.17	0.00		262.5		
21/11/2019 10:15	0.17	0.17	0.00		262.75		
21/11/2019 10:30	0.17	0.17	0.00		263		
21/11/2019 10:45	0.17	0.17	0.00		263.25		
21/11/2019 11:00	0.17	0.17	0.00		263.5		
21/11/2019 11:15	0.17	0.17	0.00		263.75		
21/11/2019 11:30	0.17	0.17	0.00		264		
21/11/2019 11:45	0.17	0.17	0.00		264.25		
21/11/2019 12:00	0.17	0.17	0.00		264.5		
21/11/2019 12:15	0.17	0.17	0.00		264.75		
21/11/2019 12:30	0.17	0.17	0.00		265		
21/11/2019 12:45	0.17	0.17	0.00		265.25		
21/11/2019 13:00	0.17	0.17	0.00		265.5		
21/11/2019 13:15	0.17	0.17	0.00		265.75		
21/11/2019 13:30	0.17	0.17	0.00		266		
21/11/2019 13:45	0.17	0.17	0.00		266.25		
21/11/2019 14:00	0.17	0.17	0.00		266.5		
21/11/2019 14:15	0.17	0.17	0.00		266.75		
21/11/2019 14:30	0.17	0.17	0.00		267		
21/11/2019 14:45	0.17	0.17	0.00		267.25		
21/11/2019 15:00	0.17	0.17	0.00		267.5		
21/11/2019 15:15	0.17	0.17	0.00		267.75		
21/11/2019 15:30	0.17	0.17	0.00		268		
21/11/2019 15:45	0.17	0.17	0.00		268.25		
21/11/2019 16:00	0.17	0.17	0.00		268.5		
21/11/2019 16:15	0.17	0.17	0.00		268.75		
21/11/2019 16:30	0.17	0.17	0.00		269		
21/11/2019 16:45	0.17	0.17	0.00		269.25		
21/11/2019 17:00	0.17	0.17	0.00		269.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
21/11/2019 17:15	0.17	0.17	0.00		269.75		
21/11/2019 17:30	0.17	0.17	0.00		270		
21/11/2019 17:45	0.17	0.17	0.00		270.25		
21/11/2019 18:00	0.17	0.17	0.00		270.5		
21/11/2019 18:15	0.17	0.17	0.00		270.75		
21/11/2019 18:30	0.17	0.17	0.00		271		
21/11/2019 18:45	0.17	0.17	0.00		271.25		
21/11/2019 19:00	0.17	0.17	0.00		271.5		
21/11/2019 19:15	0.17	0.17	0.00		271.75		
21/11/2019 19:30	0.17	0.17	0.00		272		
21/11/2019 19:45	0.17	0.17	0.00		272.25		
21/11/2019 20:00	0.17	0.17	0.00		272.5		
21/11/2019 20:15	0.17	0.17	0.00		272.75		
21/11/2019 20:30	0.17	0.17	0.00		273		
21/11/2019 20:45	0.17	0.17	0.00		273.25		
21/11/2019 21:00	0.17	0.17	0.00		273.5		
21/11/2019 21:15	0.17	0.17	0.00		273.75		
21/11/2019 21:30	0.17	0.17	0.00		274		
21/11/2019 21:45	0.17	0.17	0.00		274.25		
21/11/2019 22:00	0.17	0.17	0.00		274.5		
21/11/2019 22:15	0.17	0.17	0.00		274.75		
21/11/2019 22:30	0.17	0.17	0.00		275		
21/11/2019 22:45	0.17	0.17	0.00		275.25		
21/11/2019 23:00	0.17	0.17	0.00		275.5		
21/11/2019 23:15	0.17	0.17	0.00		275.75		
21/11/2019 23:30	0.17	0.17	0.00		276		
21/11/2019 23:45	0.17	0.17	0.00		276.25		
22/11/2019 00:00	0.17	0.17	0.00		276.5		
22/11/2019 00:15	0.17	0.17	0.00		276.75		
22/11/2019 00:30	0.17	0.17	0.00		277		
22/11/2019 00:45	0.17	0.17	0.00		277.25		
22/11/2019 01:00	0.17	0.17	0.00		277.5		
22/11/2019 01:15	0.17	0.17	0.00		277.75		
22/11/2019 01:30	0.17	0.17	0.00		278		
22/11/2019 01:45	0.17	0.17	0.00		278.25		
22/11/2019 02:00	0.17	0.17	0.00		278.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
22/11/2019 02:15	0.17	0.17	0.00		278.75		
22/11/2019 02:30	0.17	0.17	0.00		279		
22/11/2019 02:45	0.17	0.17	0.00		279.25		
22/11/2019 03:00	0.17	0.17	0.00		279.5		
22/11/2019 03:15	0.17	0.17	0.00		279.75		
22/11/2019 03:30	0.17	0.17	0.00		280		
22/11/2019 03:45	0.17	0.17	0.00		280.25		
22/11/2019 04:00	0.17	0.17	0.00		280.5		
22/11/2019 04:15	0.17	0.17	0.00		280.75		
22/11/2019 04:30	0.17	0.17	0.00		281		
22/11/2019 04:45	0.17	0.17	0.00		281.25		
22/11/2019 05:00	0.17	0.17	0.00		281.5		
22/11/2019 05:15	0.17	0.17	0.00		281.75		
22/11/2019 05:30	0.17	0.17	0.00		282		
22/11/2019 05:45	0.17	0.17	0.00		282.25		
22/11/2019 06:00	0.17	0.17	0.00		282.5		
22/11/2019 06:15	0.17	0.17	0.00		282.75		
22/11/2019 06:30	0.17	0.17	0.00		283		
22/11/2019 06:45	0.17	0.17	0.00		283.25		
22/11/2019 07:00	0.17	0.17	0.00		283.5		
22/11/2019 07:15	0.17	0.17	0.00		283.75		
22/11/2019 07:30	0.17	0.17	0.00		284		
22/11/2019 07:45	0.17	0.17	0.00		284.25		
22/11/2019 08:00	0.17	0.17	0.00		284.5		
22/11/2019 08:15	0.17	0.17	0.00		284.75		
22/11/2019 08:30	0.17	0.17	0.00		285		
22/11/2019 08:45	0.17	0.17	0.00		285.25		
22/11/2019 09:00	0.17	0.17	0.00		285.5		
22/11/2019 09:15	0.17	0.17	0.00		285.75		
22/11/2019 09:30	0.17	0.17	0.00		286		
22/11/2019 09:45	0.17	0.17	0.00		286.25		
22/11/2019 10:00	0.17	0.17	0.00		286.5		
22/11/2019 10:15	0.17	0.17	0.00		286.75		
22/11/2019 10:30	0.17	0.17	0.00		287		
22/11/2019 10:45	0.17	0.17	0.00		287.25		
22/11/2019 11:00	0.17	0.17	0.00		287.5		

		Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)	Benhall
22/11/2019 11:15	0.17	0.17	0.00			287.75		
22/11/2019 11:30	0.17	0.17	0.00			288		
22/11/2019 11:45	0.17	0.17	0.00			288.25		
22/11/2019 12:00	0.17	0.17	0.00			288.5		
22/11/2019 12:15	0.17	0.17	0.00			288.75		
22/11/2019 12:30	0.17	0.17	0.00			289		
22/11/2019 12:45	0.17	0.17	0.00			289.25		
22/11/2019 13:00	0.17	0.17	0.00			289.5		
22/11/2019 13:15	0.17	0.17	0.00			289.75		
22/11/2019 13:30	0.16	0.16	0.00			290		
22/11/2019 13:45	0.16	0.16	0.00			290.25		
22/11/2019 14:00	0.16	0.16	0.00			290.5		
22/11/2019 14:15	0.16	0.16	0.00			290.75		
22/11/2019 14:30	0.16	0.16	0.00			291		
22/11/2019 14:45	0.16	0.16	0.00			291.25		
22/11/2019 15:00	0.16	0.16	0.00			291.5		
22/11/2019 15:15	0.16	0.16	0.00			291.75		
22/11/2019 15:30	0.16	0.16	0.00			292		
22/11/2019 15:45	0.16	0.16	0.00			292.25		
22/11/2019 16:00	0.16	0.16	0.00			292.5		
22/11/2019 16:15	0.16	0.16	0.00			292.75		
22/11/2019 16:30	0.16	0.16	0.00			293		
22/11/2019 16:45	0.16	0.16	0.00			293.25		
22/11/2019 17:00	0.16	0.16	0.00			293.5		
22/11/2019 17:15	0.16	0.16	0.00			293.75		
22/11/2019 17:30	0.16	0.16	0.00			294		
22/11/2019 17:45	0.16	0.16	0.00			294.25		
22/11/2019 18:00	0.16	0.16	0.00			294.5		
22/11/2019 18:15	0.16	0.16	0.00			294.75		
22/11/2019 18:30	0.16	0.16	0.00			295		
22/11/2019 18:45	0.16	0.16	0.00			295.25		
22/11/2019 19:00	0.16	0.16	0.00			295.5		
22/11/2019 19:15	0.16	0.16	0.00			295.75		
22/11/2019 19:30	0.16	0.16	0.00			296		
22/11/2019 19:45	0.16	0.16	0.00			296.25		
22/11/2019 20:00	0.16	0.16	0.00			296.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
22/11/2019 20:15	0.16	0.16	0.00		296.75		
22/11/2019 20:30	0.16	0.16	0.00		297		
22/11/2019 20:45	0.16	0.16	0.00		297.25		
22/11/2019 21:00	0.16	0.16	0.00		297.5		
22/11/2019 21:15	0.16	0.16	0.00		297.75		
22/11/2019 21:30	0.16	0.16	0.00		298		
22/11/2019 21:45	0.16	0.16	0.00		298.25		
22/11/2019 22:00	0.16	0.16	0.00		298.5		
22/11/2019 22:15	0.16	0.16	0.00		298.75		
22/11/2019 22:30	0.16	0.16	0.00		299		
22/11/2019 22:45	0.16	0.16	0.00		299.25		
22/11/2019 23:00	0.16	0.16	0.00		299.5		
22/11/2019 23:15	0.16	0.16	0.00		299.75		
22/11/2019 23:30	0.16	0.16	0.00		300		
22/11/2019 23:45	0.16	0.16	0.00		300.25		
23/11/2019 00:00	0.16	0.16	0.00		300.5		
23/11/2019 00:15	0.16	0.16	0.00		300.75		
23/11/2019 00:30	0.16	0.16	0.00		301		
23/11/2019 00:45	0.16	0.16	0.00		301.25		
23/11/2019 01:00	0.16	0.16	0.00		301.5		
23/11/2019 01:15	0.16	0.16	0.00		301.75		
23/11/2019 01:30	0.16	0.16	0.00		302		
23/11/2019 01:45	0.16	0.16	0.00		302.25		
23/11/2019 02:00	0.16	0.16	0.00		302.5		
23/11/2019 02:15	0.16	0.16	0.00		302.75		
23/11/2019 02:30	0.16	0.16	0.00		303		
23/11/2019 02:45	0.16	0.16	0.00		303.25		
23/11/2019 03:00	0.16	0.16	0.00		303.5		
23/11/2019 03:15	0.16	0.16	0.00		303.75		
23/11/2019 03:30	0.16	0.16	0.00		304		
23/11/2019 03:45	0.16	0.16	0.00		304.25		
23/11/2019 04:00	0.16	0.16	0.00		304.5		
23/11/2019 04:15	0.16	0.16	0.00		304.75		
23/11/2019 04:30	0.16	0.16	0.00		305		
23/11/2019 04:45	0.16	0.16	0.00		305.25		
23/11/2019 05:00	0.16	0.16	0.00		305.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
23/11/2019 05:15	0.16	0.16	0.00		305.75		
23/11/2019 05:30	0.16	0.16	0.00		306		
23/11/2019 05:45	0.16	0.16	0.00		306.25		
23/11/2019 06:00	0.16	0.16	0.00		306.5		
23/11/2019 06:15	0.16	0.16	0.00		306.75		
23/11/2019 06:30	0.16	0.16	0.00		307		
23/11/2019 06:45	0.16	0.16	0.00		307.25		
23/11/2019 07:00	0.16	0.16	0.00		307.5		
23/11/2019 07:15	0.16	0.16	0.00		307.75		
23/11/2019 07:30	0.16	0.16	0.00		308		
23/11/2019 07:45	0.16	0.16	0.00		308.25		
23/11/2019 08:00	0.16	0.16	0.00		308.5		
23/11/2019 08:15	0.16	0.16	0.00		308.75		
23/11/2019 08:30	0.16	0.16	0.00		309		
23/11/2019 08:45	0.16	0.16	0.00		309.25		
23/11/2019 09:00	0.16	0.16	0.00		309.5		
23/11/2019 09:15	0.16	0.16	0.00		309.75		
23/11/2019 09:30	0.16	0.16	0.00		310		
23/11/2019 09:45	0.16	0.16	0.00		310.25		
23/11/2019 10:00	0.16	0.16	0.00		310.5		
23/11/2019 10:15	0.16	0.16	0.00		310.75		
23/11/2019 10:30	0.16	0.16	0.00		311		
23/11/2019 10:45	0.16	0.16	0.00		311.25		
23/11/2019 11:00	0.16	0.16	0.00		311.5		
23/11/2019 11:15	0.16	0.16	0.00		311.75		
23/11/2019 11:30	0.16	0.16	0.00		312		
23/11/2019 11:45	0.16	0.16	0.00		312.25		
23/11/2019 12:00	0.16	0.16	0.00		312.5		
23/11/2019 12:15	0.16	0.16	0.00		312.75		
23/11/2019 12:30	0.16	0.16	0.00		313		
23/11/2019 12:45	0.16	0.16	0.00		313.25		
23/11/2019 13:00	0.16	0.16	0.00		313.5		
23/11/2019 13:15	0.16	0.16	0.00		313.75		
23/11/2019 13:30	0.16	0.16	0.00		314		
23/11/2019 13:45	0.16	0.16	0.00		314.25		
23/11/2019 14:00	0.16	0.16	0.00		314.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
23/11/2019 14:15	0.16	0.16	0.00		314.75		
23/11/2019 14:30	0.16	0.16	0.00		315		
23/11/2019 14:45	0.16	0.16	0.00		315.25		
23/11/2019 15:00	0.16	0.16	0.00		315.5		
23/11/2019 15:15	0.16	0.16	0.00		315.75		
23/11/2019 15:30	0.16	0.16	0.00		316		
23/11/2019 15:45	0.16	0.16	0.00		316.25		
23/11/2019 16:00	0.16	0.16	0.00		316.5		
23/11/2019 16:15	0.16	0.16	0.00		316.75		
23/11/2019 16:30	0.16	0.16	0.00		317		
23/11/2019 16:45	0.16	0.16	0.00		317.25		
23/11/2019 17:00	0.16	0.16	0.00		317.5		
23/11/2019 17:15	0.16	0.16	0.00		317.75		
23/11/2019 17:30	0.16	0.16	0.00		318		
23/11/2019 17:45	0.16	0.16	0.00		318.25		
23/11/2019 18:00	0.16	0.16	0.00		318.5		
23/11/2019 18:15	0.16	0.16	0.00		318.75		
23/11/2019 18:30	0.16	0.16	0.00		319		
23/11/2019 18:45	0.16	0.16	0.00		319.25		
23/11/2019 19:00	0.16	0.16	0.00		319.5		
23/11/2019 19:15	0.16	0.16	0.00		319.75		
23/11/2019 19:30	0.16	0.16	0.00		320		
23/11/2019 19:45	0.16	0.16	0.00		320.25		
23/11/2019 20:00	0.16	0.16	0.00		320.5		
23/11/2019 20:15	0.16	0.16	0.00		320.75		
23/11/2019 20:30	0.16	0.16	0.00		321		
23/11/2019 20:45	0.16	0.16	0.00		321.25		
23/11/2019 21:00	0.16	0.16	0.00		321.5		
23/11/2019 21:15	0.16	0.16	0.00		321.75		
23/11/2019 21:30	0.16	0.16	0.00		322		
23/11/2019 21:45	0.16	0.16	0.00		322.25		
23/11/2019 22:00	0.16	0.16	0.00		322.5		
23/11/2019 22:15	0.16	0.16	0.00		322.75		
23/11/2019 22:30	0.16	0.16	0.00		323		
23/11/2019 22:45	0.16	0.16	0.00		323.25		
23/11/2019 23:00	0.16	0.16	0.00		323.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
23/11/2019 23:15	0.16	0.16	0.00		323.75		
23/11/2019 23:30	0.17	0.17	0.00		324		
23/11/2019 23:45	0.17	0.17	0.00		324.25		
24/11/2019 00:00	0.17	0.17	0.00		324.5		
24/11/2019 00:15	0.17	0.17	0.00		324.75		
24/11/2019 00:30	0.17	0.17	0.00		325		
24/11/2019 00:45	0.17	0.17	0.00		325.25		
24/11/2019 01:00	0.17	0.17	0.00		325.5		
24/11/2019 01:15	0.17	0.17	0.00		325.75		
24/11/2019 01:30	0.17	0.17	0.00		326		
24/11/2019 01:45	0.17	0.17	0.00		326.25		
24/11/2019 02:00	0.17	0.17	0.00		326.5		
24/11/2019 02:15	0.17	0.17	0.00		326.75		
24/11/2019 02:30	0.17	0.17	0.00		327		
24/11/2019 02:45	0.17	0.17	0.00		327.25		
24/11/2019 03:00	0.17	0.17	0.00		327.5		
24/11/2019 03:15	0.17	0.17	0.00		327.75		
24/11/2019 03:30	0.17	0.17	0.00		328		
24/11/2019 03:45	0.17	0.17	0.00		328.25		
24/11/2019 04:00	0.17	0.17	0.00		328.5		
24/11/2019 04:15	0.17	0.17	0.00		328.75		
24/11/2019 04:30	0.17	0.17	0.00		329		
24/11/2019 04:45	0.17	0.17	0.00		329.25		
24/11/2019 05:00	0.17	0.17	0.00		329.5		
24/11/2019 05:15	0.17	0.17	0.00		329.75		
24/11/2019 05:30	0.17	0.17	0.00		330		
24/11/2019 05:45	0.17	0.17	0.00		330.25		
24/11/2019 06:00	0.17	0.17	0.00		330.5		
24/11/2019 06:15	0.17	0.17	0.00		330.75		
24/11/2019 06:30	0.17	0.17	0.00		331		
24/11/2019 06:45	0.17	0.17	0.00		331.25		
24/11/2019 07:00	0.17	0.17	0.00		331.5		
24/11/2019 07:15	0.17	0.17	0.00		331.75		
24/11/2019 07:30	0.17	0.17	0.00		332		
24/11/2019 07:45	0.17	0.17	0.00		332.25		
24/11/2019 08:00	0.17	0.17	0.00		332.5		

		Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)		Rainfall (mm)	Hours	Rainfall (mm)	Benhall
24/11/2019 08:15	0.17	0.17	0.00			332.75		
24/11/2019 08:30	0.17	0.17	0.00			333		
24/11/2019 08:45	0.17	0.17	0.00			333.25		
24/11/2019 09:00	0.17	0.17	0.00			333.5		
24/11/2019 09:15	0.17	0.17	0.00			333.75		
24/11/2019 09:30	0.17	0.17	0.00			334		
24/11/2019 09:45	0.17	0.17	0.00			334.25		
24/11/2019 10:00	0.17	0.17	0.00			334.5		
						334.75		
						335		
						335.25		
						335.5		
						335.75		
						336		
						336.25		
						336.5		
						336.75		
						337		
						337.25		
						337.5		
						337.75		
						338		
						338.25		
						338.5		
						338.75		
						339		
						339.25		
						339.5		
						339.75		
						340		
						340.25		
						340.5		
						340.75		
						341		
						341.25		
						341.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					341.75		
					342		
					342.25		
					342.5		
					342.75		
					343		
					343.25		
					343.5		
					343.75		
					344		
					344.25		
					344.5		
					344.75		
					345		
					345.25		
					345.5		
					345.75		
					346		
					346.25		
					346.5		
					346.75		
					347		
					347.25		
					347.5		
					347.75		
					348		
					348.25		
					348.5		
					348.75		
					349		
					349.25		
					349.5		
					349.75		
					350		
					350.25		
					350.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					350.75		
					351		
					351.25		
					351.5		
					351.75		
					352		
					352.25		
					352.5		
					352.75		
					353		
					353.25		
					353.5		
					353.75		
					354		
					354.25		
					354.5		
					354.75		
					355		
					355.25		
					355.5		
					355.75		
					356		
					356.25		
					356.5		
					356.75		
					357		
					357.25		
					357.5		
					357.75		
					358		
					358.25		
					358.5		
					358.75		
					359		
					359.25		
					359.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					359.75		
					360		
					360.25		
					360.5		
					360.75		
					361		
					361.25		
					361.5		
					361.75		
					362		
					362.25		
					362.5		
					362.75		
					363		
					363.25		
					363.5		
					363.75		
					364		
					364.25		
					364.5		
					364.75		
					365		
					365.25		
					365.5		
					365.75		
					366		
					366.25		
					366.5		
					366.75		
					367		
					367.25		
					367.5		
					367.75		
					368		
					368.25		
					368.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					368.75		
					369		
					369.25		
					369.5		
					369.75		
					370		
					370.25		
					370.5		
					370.75		
					371		
					371.25		
					371.5		
					371.75		
					372		
					372.25		
					372.5		
					372.75		
					373		
					373.25		
					373.5		
					373.75		
					374		
					374.25		
					374.5		
					374.75		
					375		
					375.25		
					375.5		
					375.75		
					376		
					376.25		
					376.5		
					376.75		
					377		
					377.25		
					377.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					377.75		
					378		
					378.25		
					378.5		
					378.75		
					379		
					379.25		
					379.5		
					379.75		
					380		
					380.25		
					380.5		
					380.75		
					381		
					381.25		
					381.5		
					381.75		
					382		
					382.25		
					382.5		
					382.75		
					383		
					383.25		
					383.5		
					383.75		
					384		
					384.25		
					384.5		
					384.75		
					385		
					385.25		
					385.5		
					385.75		
					386		
					386.25		
					386.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					386.75		
					387		
					387.25		
					387.5		
					387.75		
					388		
					388.25		
					388.5		
					388.75		
					389		
					389.25		
					389.5		
					389.75		
					390		
					390.25		
					390.5		
					390.75		
					391		
					391.25		
					391.5		
					391.75		
					392		
					392.25		
					392.5		
					392.75		
					393		
					393.25		
					393.5		
					393.75		
					394		
					394.25		
					394.5		
					394.75		
					395		
					395.25		
					395.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					395.75		
					396		
					396.25		
					396.5		
					396.75		
					397		
					397.25		
					397.5		
					397.75		
					398		
					398.25		
					398.5		
					398.75		
					399		
					399.25		
					399.5		
					399.75		
					400		
					400.25		
					400.5		
					400.75		
					401		
					401.25		
					401.5		
					401.75		
					402		
					402.25		
					402.5		
					402.75		
					403		
					403.25		
					403.5		
					403.75		
					404		
					404.25		
					404.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					404.75		
					405		
					405.25		
					405.5		
					405.75		
					406		
					406.25		
					406.5		
					406.75		
					407		
					407.25		
					407.5		
					407.75		
					408		
					408.25		
					408.5		
					408.75		
					409		
					409.25		
					409.5		
					409.75		
					410		
					410.25		
					410.5		
					410.75		
					411		
					411.25		
					411.5		
					411.75		
					412		
					412.25		
					412.5		
					412.75		
					413		
					413.25		
					413.5		

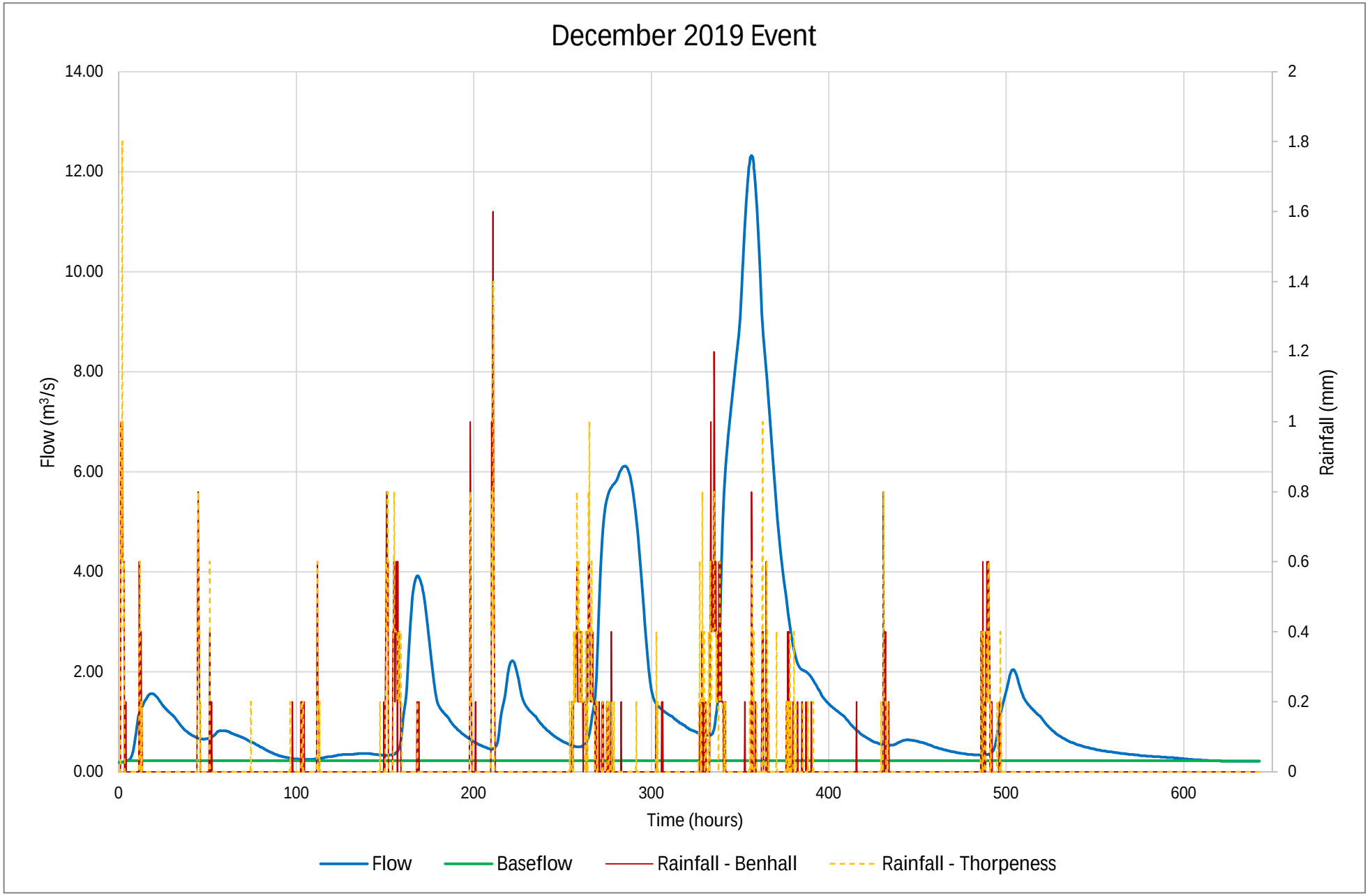
Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					413.75		
					414		
					414.25		
					414.5		
					414.75		
					415		
					415.25		
					415.5		
					415.75		
					416		
					416.25		
					416.5		
					416.75		
					417		
					417.25		
					417.5		
					417.75		
					418		
					418.25		
					418.5		
					418.75		
					419		
					419.25		
					419.5		
					419.75		
					420		
					420.25		
					420.5		
					420.75		
					421		
					421.25		
					421.5		
					421.75		
					422		
					422.25		
					422.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					422.75		
					423		
					423.25		
					423.5		
					423.75		
					424		
					424.25		
					424.5		
					424.75		
					425		
					425.25		
					425.5		
					425.75		
					426		
					426.25		
					426.5		
					426.75		
					427		
					427.25		
					427.5		
					427.75		
					428		
					428.25		
					428.5		
					428.75		
					429		
					429.25		
					429.5		
					429.75		
					430		
					430.25		
					430.5		
					430.75		
					431		
					431.25		
					431.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					431.75		
					432		
					432.25		
					432.5		
					432.75		
					433		
					433.25		
					433.5		
					433.75		
					434		
					434.25		
					434.5		
					434.75		
					435		
					435.25		
					435.5		
					435.75		
					436		
					436.25		
					436.5		
					436.75		
					437		
					437.25		
					437.5		
					437.75		
					438		
					438.25		
					438.5		
					438.75		
					439		
					439.25		
					439.5		
					439.75		
					440		
					440.25		
					440.5		

Date & Time	Flow (m^3/s)	Middleton Baseflow (m^3/s)	NetFlow (m^3/s)	Benhall Rainfall (mm)	Hours	Thorpeness Rainfall (mm)	Benhall
					440.75		
					441		
					441.25		
					441.5		
					441.75		
					442		
					442.25		
					442.5		
					442.75		
					443		
					443.25		
					443.5		
					443.75		
					444		
					444.25		
					444.5		
					444.75		
					445		
					445.25		
					445.5		
					445.75		
					446		
					446.25		
					446.5		
					446.75		
					447		
					447.25		
					447.5		
					447.75		
					448		
					448.25		
					448.5		
					448.75		
					449		
					449.25		
					449.5		

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
					449.75		
					450		
					450.25		
					450.5		
					450.75		
					451		
					451.25		
					451.5		
					451.75		
					452		
					452.25		
					452.5		
					452.75		
					453		
					453.25		
					453.5		
					453.75		
					454		
					454.25		
					454.5		


December 2019 Event
14.00
12.00
10.00
8.00
6.00
4.00
2.00
0.00
Flow (m³/s)
2
1.8
1.6
1.4
1.2
1
0.8
0.6
0.4
0.2
0
Rainfall (mm)
0
100
200
300
400
500
600
Time (hours)
Flow
Baseflow
Rainfall - Benhall
Rainfall - Thorpeness

	Middleton			Benhall		Thorpeness
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)
06/12/2019 06:00	0.18	0.18	0.00	0	0	0
06/12/2019 06:15	0.18	0.18	0.00	0	0.25	0
06/12/2019 06:30	0.18	0.18	0.00	0	0.5	0
06/12/2019 06:45	0.18	0.18	0.00	0	0.75	0
06/12/2019 07:00	0.18	0.18	0.00	0	1	0
06/12/2019 07:15	0.18	0.18	0.00	1	1.25	1
06/12/2019 07:30	0.18	0.18	0.00	0.6	1.5	1
06/12/2019 07:45	0.18	0.18	0.00	0.6	1.75	0.6
06/12/2019 08:00	0.19	0.19	0.00	1	2	1.8
06/12/2019 08:15	0.19	0.19	0.00	0.6	2.25	0.6
06/12/2019 08:30	0.19	0.19	0.00	0.6	2.5	0.4
06/12/2019 08:45	0.19	0.19	0.00	0.6	2.75	0.4
06/12/2019 09:00	0.20	0.20	0.00	0.6	3	0.6
06/12/2019 09:15	0.20	0.20	0.00	0	3.25	0.2
06/12/2019 09:30	0.20	0.20	0.00	0	3.5	0
06/12/2019 09:45	0.21	0.21	0.00	0	3.75	0
06/12/2019 10:00	0.21	0.21	0.00	0.2	4	0
06/12/2019 10:15	0.22	0.22	0.00	0	4.25	0
06/12/2019 10:30	0.22	0.22	0.00	0	4.5	0
06/12/2019 10:45	0.22	0.22	0.00	0	4.75	0
06/12/2019 11:00	0.22	0.22	0.00	0	5	0
06/12/2019 11:15	0.22	0.22	0.00	0	5.25	0
06/12/2019 11:30	0.23	0.22	0.01	0	5.5	0
06/12/2019 11:45	0.23	0.22	0.01	0	5.75	0
06/12/2019 12:00	0.23	0.22	0.01	0	6	0
06/12/2019 12:15	0.24	0.22	0.02	0	6.25	0
06/12/2019 12:30	0.25	0.22	0.03	0	6.5	0
06/12/2019 12:45	0.27	0.22	0.05	0	6.75	0
06/12/2019 13:00	0.29	0.22	0.07	0	7	0
06/12/2019 13:15	0.31	0.22	0.09	0	7.25	0
06/12/2019 13:30	0.33	0.22	0.11	0	7.5	0
06/12/2019 13:45	0.36	0.22	0.14	0	7.75	0
06/12/2019 14:00	0.39	0.22	0.17	0	8	0
06/12/2019 14:15	0.44	0.22	0.22	0	8.25	0
06/12/2019 14:30	0.49	0.22	0.27	0	8.5	0
06/12/2019 14:45	0.54	0.22	0.32	0	8.75	0

Benhall	
Area (km^2)	50.16
Total Rain (P) mm	82.8
Time Interval (hour)	0.25
Percentage Runoff	66%

Thorpeness	
Area (km^2)	50.16
Total Rain (P) mm	8.4
Time Interval (hour)	0.25
Percentage Runoff	49%

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
06/12/2019 15:00	0.60	0.22	0.38	0	9	0	
06/12/2019 15:15	0.66	0.22	0.44	0	9.25	0	
06/12/2019 15:30	0.72	0.22	0.50	0	9.5	0	
06/12/2019 15:45	0.77	0.22	0.55	0	9.75	0	
06/12/2019 16:00	0.85	0.22	0.63	0	10	0	
06/12/2019 16:15	0.91	0.22	0.69	0	10.25	0	
06/12/2019 16:30	0.97	0.22	0.75	0	10.5	0	
06/12/2019 16:45	1.04	0.22	0.82	0	10.75	0	
06/12/2019 17:00	1.10	0.22	0.88	0	11	0	
06/12/2019 17:15	1.13	0.22	0.91	0	11.25	0	
06/12/2019 17:30	1.16	0.22	0.94	0.6	11.5	0.4	
06/12/2019 17:45	1.19	0.22	0.97	0.4	11.75	0.4	
06/12/2019 18:00	1.20	0.22	0.98	0.4	12	0.6	
06/12/2019 18:15	1.22	0.22	1.00	0	12.25	0	
06/12/2019 18:30	1.24	0.22	1.02	0.4	12.5	0.2	
06/12/2019 18:45	1.27	0.22	1.05	0.2	12.75	0	
06/12/2019 19:00	1.29	0.22	1.07	0.2	13	0.2	
06/12/2019 19:15	1.31	0.22	1.09	0	13.25	0	
06/12/2019 19:30	1.33	0.22	1.11	0	13.5	0	
06/12/2019 19:45	1.35	0.22	1.13	0	13.75	0	
06/12/2019 20:00	1.37	0.22	1.15	0	14	0	
06/12/2019 20:15	1.39	0.22	1.17	0	14.25	0	
06/12/2019 20:30	1.41	0.22	1.19	0	14.5	0	
06/12/2019 20:45	1.42	0.22	1.20	0	14.75	0	
06/12/2019 21:00	1.43	0.22	1.21	0	15	0	
06/12/2019 21:15	1.44	0.22	1.22	0	15.25	0	
06/12/2019 21:30	1.46	0.22	1.24	0	15.5	0	
06/12/2019 21:45	1.47	0.22	1.25	0	15.75	0	
06/12/2019 22:00	1.48	0.22	1.26	0	16	0	
06/12/2019 22:15	1.50	0.22	1.28	0	16.25	0	
06/12/2019 22:30	1.51	0.22	1.29	0	16.5	0	
06/12/2019 22:45	1.52	0.22	1.30	0	16.75	0	
06/12/2019 23:00	1.53	0.22	1.31	0	17	0	
06/12/2019 23:15	1.54	0.22	1.32	0	17.25	0	
06/12/2019 23:30	1.54	0.22	1.32	0	17.5	0	
06/12/2019 23:45	1.54	0.22	1.32	0	17.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
07/12/2019 00:00	1.56	0.22	1.34	0	18	0	
07/12/2019 00:15	1.56	0.22	1.34	0	18.25	0	
07/12/2019 00:30	1.56	0.22	1.34	0	18.5	0	
07/12/2019 00:45	1.56	0.22	1.34	0	18.75	0	
07/12/2019 01:00	1.56	0.22	1.34	0	19	0	
07/12/2019 01:15	1.55	0.22	1.33	0	19.25	0	
07/12/2019 01:30	1.55	0.22	1.33	0	19.5	0	
07/12/2019 01:45	1.54	0.22	1.32	0	19.75	0	
07/12/2019 02:00	1.54	0.22	1.32	0	20	0	
07/12/2019 02:15	1.54	0.22	1.32	0	20.25	0	
07/12/2019 02:30	1.53	0.22	1.31	0	20.5	0	
07/12/2019 02:45	1.52	0.22	1.30	0	20.75	0	
07/12/2019 03:00	1.51	0.22	1.29	0	21	0	
07/12/2019 03:15	1.51	0.22	1.29	0	21.25	0	
07/12/2019 03:30	1.50	0.22	1.28	0	21.5	0	
07/12/2019 03:45	1.48	0.22	1.26	0	21.75	0	
07/12/2019 04:00	1.47	0.22	1.25	0	22	0	
07/12/2019 04:15	1.46	0.22	1.24	0	22.25	0	
07/12/2019 04:30	1.45	0.22	1.23	0	22.5	0	
07/12/2019 04:45	1.44	0.22	1.22	0	22.75	0	
07/12/2019 05:00	1.42	0.22	1.20	0	23	0	
07/12/2019 05:15	1.41	0.22	1.19	0	23.25	0	
07/12/2019 05:30	1.40	0.22	1.18	0	23.5	0	
07/12/2019 05:45	1.38	0.22	1.16	0	23.75	0	
07/12/2019 06:00	1.37	0.22	1.15	0	24	0	
07/12/2019 06:15	1.36	0.22	1.14	0	24.25	0	
07/12/2019 06:30	1.35	0.22	1.13	0	24.5	0	
07/12/2019 06:45	1.33	0.22	1.11	0	24.75	0	
07/12/2019 07:00	1.32	0.22	1.10	0	25	0	
07/12/2019 07:15	1.31	0.22	1.09	0	25.25	0	
07/12/2019 07:30	1.30	0.22	1.08	0	25.5	0	
07/12/2019 07:45	1.29	0.22	1.07	0	25.75	0	
07/12/2019 08:00	1.28	0.22	1.06	0	26	0	
07/12/2019 08:15	1.27	0.22	1.05	0	26.25	0	
07/12/2019 08:30	1.26	0.22	1.04	0	26.5	0	
07/12/2019 08:45	1.25	0.22	1.03	0	26.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
07/12/2019 09:00	1.24	0.22	1.02	0	27	0	
07/12/2019 09:15	1.23	0.22	1.01	0	27.25	0	
07/12/2019 09:30	1.22	0.22	1.00	0	27.5	0	
07/12/2019 09:45	1.22	0.22	1.00	0	27.75	0	
07/12/2019 10:00	1.20	0.22	0.98	0	28	0	
07/12/2019 10:15	1.20	0.22	0.98	0	28.25	0	
07/12/2019 10:30	1.19	0.22	0.97	0	28.5	0	
07/12/2019 10:45	1.18	0.22	0.96	0	28.75	0	
07/12/2019 11:00	1.17	0.22	0.95	0	29	0	
07/12/2019 11:15	1.16	0.22	0.94	0	29.25	0	
07/12/2019 11:30	1.15	0.22	0.93	0	29.5	0	
07/12/2019 11:45	1.15	0.22	0.93	0	29.75	0	
07/12/2019 12:00	1.14	0.22	0.92	0	30	0	
07/12/2019 12:15	1.13	0.22	0.91	0	30.25	0	
07/12/2019 12:30	1.13	0.22	0.91	0	30.5	0	
07/12/2019 12:45	1.11	0.22	0.89	0	30.75	0	
07/12/2019 13:00	1.11	0.22	0.89	0	31	0	
07/12/2019 13:15	1.10	0.22	0.88	0	31.25	0	
07/12/2019 13:30	1.09	0.22	0.87	0	31.5	0	
07/12/2019 13:45	1.07	0.22	0.85	0	31.75	0	
07/12/2019 14:00	1.06	0.22	0.84	0	32	0	
07/12/2019 14:15	1.05	0.22	0.83	0	32.25	0	
07/12/2019 14:30	1.04	0.22	0.82	0	32.5	0	
07/12/2019 14:45	1.03	0.22	0.81	0	32.75	0	
07/12/2019 15:00	1.01	0.22	0.79	0	33	0	
07/12/2019 15:15	1.00	0.22	0.78	0	33.25	0	
07/12/2019 15:30	0.99	0.22	0.77	0	33.5	0	
07/12/2019 15:45	0.98	0.22	0.76	0	33.75	0	
07/12/2019 16:00	0.97	0.22	0.75	0	34	0	
07/12/2019 16:15	0.96	0.22	0.74	0	34.25	0	
07/12/2019 16:30	0.94	0.22	0.72	0	34.5	0	
07/12/2019 16:45	0.93	0.22	0.71	0	34.75	0	
07/12/2019 17:00	0.92	0.22	0.70	0	35	0	
07/12/2019 17:15	0.91	0.22	0.69	0	35.25	0	
07/12/2019 17:30	0.90	0.22	0.68	0	35.5	0	
07/12/2019 17:45	0.89	0.22	0.67	0	35.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
07/12/2019 18:00	0.88	0.22	0.66	0	36	0	
07/12/2019 18:15	0.87	0.22	0.65	0	36.25	0	
07/12/2019 18:30	0.86	0.22	0.64	0	36.5	0	
07/12/2019 18:45	0.85	0.22	0.63	0	36.75	0	
07/12/2019 19:00	0.85	0.22	0.63	0	37	0	
07/12/2019 19:15	0.84	0.22	0.62	0	37.25	0	
07/12/2019 19:30	0.82	0.22	0.60	0	37.5	0	
07/12/2019 19:45	0.81	0.22	0.59	0	37.75	0	
07/12/2019 20:00	0.80	0.22	0.58	0	38	0	
07/12/2019 20:15	0.80	0.22	0.58	0	38.25	0	
07/12/2019 20:30	0.79	0.22	0.57	0	38.5	0	
07/12/2019 20:45	0.78	0.22	0.56	0	38.75	0	
07/12/2019 21:00	0.78	0.22	0.56	0	39	0	
07/12/2019 21:15	0.77	0.22	0.55	0	39.25	0	
07/12/2019 21:30	0.76	0.22	0.54	0	39.5	0	
07/12/2019 21:45	0.76	0.22	0.54	0	39.75	0	
07/12/2019 22:00	0.76	0.22	0.54	0	40	0	
07/12/2019 22:15	0.76	0.22	0.54	0	40.25	0	
07/12/2019 22:30	0.75	0.22	0.53	0	40.5	0	
07/12/2019 22:45	0.74	0.22	0.52	0	40.75	0	
07/12/2019 23:00	0.74	0.22	0.52	0	41	0	
07/12/2019 23:15	0.73	0.22	0.51	0	41.25	0	
07/12/2019 23:30	0.72	0.22	0.50	0	41.5	0	
07/12/2019 23:45	0.72	0.22	0.50	0	41.75	0	
08/12/2019 00:00	0.72	0.22	0.50	0	42	0	
08/12/2019 00:15	0.71	0.22	0.49	0	42.25	0	
08/12/2019 00:30	0.70	0.22	0.48	0	42.5	0	
08/12/2019 00:45	0.70	0.22	0.48	0	42.75	0	
08/12/2019 01:00	0.69	0.22	0.47	0	43	0	
08/12/2019 01:15	0.69	0.22	0.47	0	43.25	0	
08/12/2019 01:30	0.69	0.22	0.47	0	43.5	0	
08/12/2019 01:45	0.68	0.22	0.46	0	43.75	0	
08/12/2019 02:00	0.67	0.22	0.45	0	44	0	
08/12/2019 02:15	0.67	0.22	0.45	0.2	44.25	0.2	
08/12/2019 02:30	0.67	0.22	0.45	0.6	44.5	0.4	
08/12/2019 02:45	0.66	0.22	0.44	0.8	44.75	0.8	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
08/12/2019 03:00	0.66	0.22	0.44	0.6	45	0.6	
08/12/2019 03:15	0.66	0.22	0.44	0.4	45.25	0.4	
08/12/2019 03:30	0.66	0.22	0.44	0.2	45.5	0.4	
08/12/2019 03:45	0.65	0.22	0.43	0.2	45.75	0	
08/12/2019 04:00	0.65	0.22	0.43	0	46	0.2	
08/12/2019 04:15	0.65	0.22	0.43	0	46.25	0	
08/12/2019 04:30	0.65	0.22	0.43	0	46.5	0	
08/12/2019 04:45	0.65	0.22	0.43	0	46.75	0	
08/12/2019 05:00	0.65	0.22	0.43	0	47	0	
08/12/2019 05:15	0.65	0.22	0.43	0	47.25	0	
08/12/2019 05:30	0.65	0.22	0.43	0	47.5	0	
08/12/2019 05:45	0.65	0.22	0.43	0	47.75	0	
08/12/2019 06:00	0.65	0.22	0.43	0	48	0	
08/12/2019 06:15	0.65	0.22	0.43	0	48.25	0	
08/12/2019 06:30	0.65	0.22	0.43	0	48.5	0	
08/12/2019 06:45	0.65	0.22	0.43	0	48.75	0	
08/12/2019 07:00	0.65	0.22	0.43	0	49	0	
08/12/2019 07:15	0.65	0.22	0.43	0	49.25	0	
08/12/2019 07:30	0.65	0.22	0.43	0	49.5	0	
08/12/2019 07:45	0.65	0.22	0.43	0	49.75	0	
08/12/2019 08:00	0.65	0.22	0.43	0	50	0	
08/12/2019 08:15	0.66	0.22	0.44	0	50.25	0	
08/12/2019 08:30	0.66	0.22	0.44	0	50.5	0	
08/12/2019 08:45	0.66	0.22	0.44	0	50.75	0	
08/12/2019 09:00	0.66	0.22	0.44	0.2	51	0.2	
08/12/2019 09:15	0.67	0.22	0.45	0.4	51.25	0.6	
08/12/2019 09:30	0.67	0.22	0.45	0	51.5	0	
08/12/2019 09:45	0.68	0.22	0.46	0	51.75	0	
08/12/2019 10:00	0.68	0.22	0.46	0	52	0	
08/12/2019 10:15	0.69	0.22	0.47	0.2	52.25	0	
08/12/2019 10:30	0.69	0.22	0.47	0	52.5	0	
08/12/2019 10:45	0.70	0.22	0.48	0	52.75	0	
08/12/2019 11:00	0.71	0.22	0.49	0	53	0	
08/12/2019 11:15	0.71	0.22	0.49	0	53.25	0	
08/12/2019 11:30	0.72	0.22	0.50	0	53.5	0	
08/12/2019 11:45	0.73	0.22	0.51	0	53.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
08/12/2019 12:00	0.74	0.22	0.52	0	54	0	
08/12/2019 12:15	0.74	0.22	0.52	0	54.25	0	
08/12/2019 12:30	0.75	0.22	0.53	0	54.5	0	
08/12/2019 12:45	0.76	0.22	0.54	0	54.75	0	
08/12/2019 13:00	0.76	0.22	0.54	0	55	0	
08/12/2019 13:15	0.77	0.22	0.55	0	55.25	0	
08/12/2019 13:30	0.78	0.22	0.56	0	55.5	0	
08/12/2019 13:45	0.79	0.22	0.57	0	55.75	0	
08/12/2019 14:00	0.79	0.22	0.57	0	56	0	
08/12/2019 14:15	0.80	0.22	0.58	0	56.25	0	
08/12/2019 14:30	0.80	0.22	0.58	0	56.5	0	
08/12/2019 14:45	0.81	0.22	0.59	0	56.75	0	
08/12/2019 15:00	0.81	0.22	0.59	0	57	0	
08/12/2019 15:15	0.81	0.22	0.59	0	57.25	0	
08/12/2019 15:30	0.81	0.22	0.59	0	57.5	0	
08/12/2019 15:45	0.81	0.22	0.59	0	57.75	0	
08/12/2019 16:00	0.81	0.22	0.59	0	58	0	
08/12/2019 16:15	0.81	0.22	0.59	0	58.25	0	
08/12/2019 16:30	0.81	0.22	0.59	0	58.5	0	
08/12/2019 16:45	0.81	0.22	0.59	0	58.75	0	
08/12/2019 17:00	0.81	0.22	0.59	0	59	0	
08/12/2019 17:15	0.81	0.22	0.59	0	59.25	0	
08/12/2019 17:30	0.81	0.22	0.59	0	59.5	0	
08/12/2019 17:45	0.81	0.22	0.59	0	59.75	0	
08/12/2019 18:00	0.81	0.22	0.59	0	60	0	
08/12/2019 18:15	0.81	0.22	0.59	0	60.25	0	
08/12/2019 18:30	0.81	0.22	0.59	0	60.5	0	
08/12/2019 18:45	0.80	0.22	0.58	0	60.75	0	
08/12/2019 19:00	0.80	0.22	0.58	0	61	0	
08/12/2019 19:15	0.80	0.22	0.58	0	61.25	0	
08/12/2019 19:30	0.80	0.22	0.58	0	61.5	0	
08/12/2019 19:45	0.79	0.22	0.57	0	61.75	0	
08/12/2019 20:00	0.79	0.22	0.57	0	62	0	
08/12/2019 20:15	0.79	0.22	0.57	0	62.25	0	
08/12/2019 20:30	0.78	0.22	0.56	0	62.5	0	
08/12/2019 20:45	0.78	0.22	0.56	0	62.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
08/12/2019 21:00	0.77	0.22	0.55	0	63	0	
08/12/2019 21:15	0.77	0.22	0.55	0	63.25	0	
08/12/2019 21:30	0.77	0.22	0.55	0	63.5	0	
08/12/2019 21:45	0.76	0.22	0.54	0	63.75	0	
08/12/2019 22:00	0.76	0.22	0.54	0	64	0	
08/12/2019 22:15	0.76	0.22	0.54	0	64.25	0	
08/12/2019 22:30	0.76	0.22	0.54	0	64.5	0	
08/12/2019 22:45	0.76	0.22	0.54	0	64.75	0	
08/12/2019 23:00	0.75	0.22	0.53	0	65	0	
08/12/2019 23:15	0.75	0.22	0.53	0	65.25	0	
08/12/2019 23:30	0.74	0.22	0.52	0	65.5	0	
08/12/2019 23:45	0.74	0.22	0.52	0	65.75	0	
09/12/2019 00:00	0.74	0.22	0.52	0	66	0	
09/12/2019 00:15	0.74	0.22	0.52	0	66.25	0	
09/12/2019 00:30	0.73	0.22	0.51	0	66.5	0	
09/12/2019 00:45	0.73	0.22	0.51	0	66.75	0	
09/12/2019 01:00	0.72	0.22	0.50	0	67	0	
09/12/2019 01:15	0.72	0.22	0.50	0	67.25	0	
09/12/2019 01:30	0.72	0.22	0.50	0	67.5	0	
09/12/2019 01:45	0.71	0.22	0.49	0	67.75	0	
09/12/2019 02:00	0.71	0.22	0.49	0	68	0	
09/12/2019 02:15	0.70	0.22	0.48	0	68.25	0	
09/12/2019 02:30	0.70	0.22	0.48	0	68.5	0	
09/12/2019 02:45	0.70	0.22	0.48	0	68.75	0	
09/12/2019 03:00	0.69	0.22	0.47	0	69	0	
09/12/2019 03:15	0.69	0.22	0.47	0	69.25	0	
09/12/2019 03:30	0.68	0.22	0.46	0	69.5	0	
09/12/2019 03:45	0.68	0.22	0.46	0	69.75	0	
09/12/2019 04:00	0.68	0.22	0.46	0	70	0	
09/12/2019 04:15	0.67	0.22	0.45	0	70.25	0	
09/12/2019 04:30	0.67	0.22	0.45	0	70.5	0	
09/12/2019 04:45	0.66	0.22	0.44	0	70.75	0	
09/12/2019 05:00	0.66	0.22	0.44	0	71	0	
09/12/2019 05:15	0.65	0.22	0.43	0	71.25	0	
09/12/2019 05:30	0.65	0.22	0.43	0	71.5	0	
09/12/2019 05:45	0.65	0.22	0.43	0	71.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
09/12/2019 06:00	0.65	0.22	0.43	0	72	0	
09/12/2019 06:15	0.64	0.22	0.42	0	72.25	0	
09/12/2019 06:30	0.63	0.22	0.41	0	72.5	0	
09/12/2019 06:45	0.63	0.22	0.41	0	72.75	0	
09/12/2019 07:00	0.62	0.22	0.40	0	73	0	
09/12/2019 07:15	0.62	0.22	0.40	0	73.25	0	
09/12/2019 07:30	0.61	0.22	0.39	0	73.5	0	
09/12/2019 07:45	0.60	0.22	0.38	0	73.75	0	
09/12/2019 08:00	0.60	0.22	0.38	0	74	0	
09/12/2019 08:15	0.60	0.22	0.38	0	74.25	0	
09/12/2019 08:30	0.60	0.22	0.38	0	74.5	0.2	
09/12/2019 08:45	0.59	0.22	0.37	0	74.75	0	
09/12/2019 09:00	0.59	0.22	0.37	0	75	0	
09/12/2019 09:15	0.58	0.22	0.36	0	75.25	0	
09/12/2019 09:30	0.58	0.22	0.36	0	75.5	0	
09/12/2019 09:45	0.58	0.22	0.36	0	75.75	0	
09/12/2019 10:00	0.57	0.22	0.35	0	76	0	
09/12/2019 10:15	0.56	0.22	0.34	0	76.25	0	
09/12/2019 10:30	0.56	0.22	0.34	0	76.5	0	
09/12/2019 10:45	0.56	0.22	0.34	0	76.75	0	
09/12/2019 11:00	0.55	0.22	0.33	0	77	0	
09/12/2019 11:15	0.55	0.22	0.33	0	77.25	0	
09/12/2019 11:30	0.54	0.22	0.32	0	77.5	0	
09/12/2019 11:45	0.53	0.22	0.31	0	77.75	0	
09/12/2019 12:00	0.53	0.22	0.31	0	78	0	
09/12/2019 12:15	0.53	0.22	0.31	0	78.25	0	
09/12/2019 12:30	0.52	0.22	0.30	0	78.5	0	
09/12/2019 12:45	0.52	0.22	0.30	0	78.75	0	
09/12/2019 13:00	0.51	0.22	0.29	0	79	0	
09/12/2019 13:15	0.50	0.22	0.28	0	79.25	0	
09/12/2019 13:30	0.50	0.22	0.28	0	79.5	0	
09/12/2019 13:45	0.50	0.22	0.28	0	79.75	0	
09/12/2019 14:00	0.49	0.22	0.27	0	80	0	
09/12/2019 14:15	0.49	0.22	0.27	0	80.25	0	
09/12/2019 14:30	0.48	0.22	0.26	0	80.5	0	
09/12/2019 14:45	0.48	0.22	0.26	0	80.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
09/12/2019 15:00	0.48	0.22	0.26	0	81	0	
09/12/2019 15:15	0.47	0.22	0.25	0	81.25	0	
09/12/2019 15:30	0.46	0.22	0.24	0	81.5	0	
09/12/2019 15:45	0.46	0.22	0.24	0	81.75	0	
09/12/2019 16:00	0.46	0.22	0.24	0	82	0	
09/12/2019 16:15	0.45	0.22	0.23	0	82.25	0	
09/12/2019 16:30	0.44	0.22	0.22	0	82.5	0	
09/12/2019 16:45	0.44	0.22	0.22	0	82.75	0	
09/12/2019 17:00	0.44	0.22	0.22	0	83	0	
09/12/2019 17:15	0.43	0.22	0.21	0	83.25	0	
09/12/2019 17:30	0.42	0.22	0.20	0	83.5	0	
09/12/2019 17:45	0.42	0.22	0.20	0	83.75	0	
09/12/2019 18:00	0.41	0.22	0.19	0	84	0	
09/12/2019 18:15	0.41	0.22	0.19	0	84.25	0	
09/12/2019 18:30	0.40	0.22	0.18	0	84.5	0	
09/12/2019 18:45	0.40	0.22	0.18	0	84.75	0	
09/12/2019 19:00	0.39	0.22	0.17	0	85	0	
09/12/2019 19:15	0.39	0.22	0.17	0	85.25	0	
09/12/2019 19:30	0.39	0.22	0.17	0	85.5	0	
09/12/2019 19:45	0.38	0.22	0.16	0	85.75	0	
09/12/2019 20:00	0.38	0.22	0.16	0	86	0	
09/12/2019 20:15	0.37	0.22	0.15	0	86.25	0	
09/12/2019 20:30	0.37	0.22	0.15	0	86.5	0	
09/12/2019 20:45	0.37	0.22	0.15	0	86.75	0	
09/12/2019 21:00	0.36	0.22	0.14	0	87	0	
09/12/2019 21:15	0.36	0.22	0.14	0	87.25	0	
09/12/2019 21:30	0.36	0.22	0.14	0	87.5	0	
09/12/2019 21:45	0.35	0.22	0.13	0	87.75	0	
09/12/2019 22:00	0.35	0.22	0.13	0	88	0	
09/12/2019 22:15	0.35	0.22	0.13	0	88.25	0	
09/12/2019 22:30	0.34	0.22	0.12	0	88.5	0	
09/12/2019 22:45	0.34	0.22	0.12	0	88.75	0	
09/12/2019 23:00	0.34	0.22	0.12	0	89	0	
09/12/2019 23:15	0.33	0.22	0.11	0	89.25	0	
09/12/2019 23:30	0.33	0.22	0.11	0	89.5	0	
09/12/2019 23:45	0.32	0.22	0.10	0	89.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
10/12/2019 00:00	0.32	0.22	0.10	0	90	0	
10/12/2019 00:15	0.32	0.22	0.10	0	90.25	0	
10/12/2019 00:30	0.31	0.22	0.09	0	90.5	0	
10/12/2019 00:45	0.31	0.22	0.09	0	90.75	0	
10/12/2019 01:00	0.31	0.22	0.09	0	91	0	
10/12/2019 01:15	0.31	0.22	0.09	0	91.25	0	
10/12/2019 01:30	0.31	0.22	0.09	0	91.5	0	
10/12/2019 01:45	0.30	0.22	0.08	0	91.75	0	
10/12/2019 02:00	0.30	0.22	0.08	0	92	0	
10/12/2019 02:15	0.30	0.22	0.08	0	92.25	0	
10/12/2019 02:30	0.30	0.22	0.08	0	92.5	0	
10/12/2019 02:45	0.29	0.22	0.07	0	92.75	0	
10/12/2019 03:00	0.29	0.22	0.07	0	93	0	
10/12/2019 03:15	0.29	0.22	0.07	0	93.25	0	
10/12/2019 03:30	0.29	0.22	0.07	0	93.5	0	
10/12/2019 03:45	0.29	0.22	0.07	0	93.75	0	
10/12/2019 04:00	0.29	0.22	0.07	0	94	0	
10/12/2019 04:15	0.29	0.22	0.07	0	94.25	0	
10/12/2019 04:30	0.28	0.22	0.06	0	94.5	0	
10/12/2019 04:45	0.28	0.22	0.06	0	94.75	0	
10/12/2019 05:00	0.28	0.22	0.06	0	95	0	
10/12/2019 05:15	0.28	0.22	0.06	0	95.25	0	
10/12/2019 05:30	0.28	0.22	0.06	0	95.5	0	
10/12/2019 05:45	0.28	0.22	0.06	0	95.75	0	
10/12/2019 06:00	0.27	0.22	0.05	0	96	0	
10/12/2019 06:15	0.27	0.22	0.05	0	96.25	0	
10/12/2019 06:30	0.27	0.22	0.05	0	96.5	0.2	
10/12/2019 06:45	0.26	0.22	0.04	0	96.75	0	
10/12/2019 07:00	0.26	0.22	0.04	0	97	0	
10/12/2019 07:15	0.26	0.22	0.04	0	97.25	0	
10/12/2019 07:30	0.26	0.22	0.04	0	97.5	0	
10/12/2019 07:45	0.26	0.22	0.04	0.2	97.75	0	
10/12/2019 08:00	0.26	0.22	0.04	0	98	0	
10/12/2019 08:15	0.26	0.22	0.04	0	98.25	0	
10/12/2019 08:30	0.25	0.22	0.03	0	98.5	0	
10/12/2019 08:45	0.25	0.22	0.03	0	98.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
10/12/2019 09:00	0.25	0.22	0.03	0	99	0	
10/12/2019 09:15	0.25	0.22	0.03	0	99.25	0	
10/12/2019 09:30	0.25	0.22	0.03	0	99.5	0	
10/12/2019 09:45	0.25	0.22	0.03	0	99.75	0	
10/12/2019 10:00	0.25	0.22	0.03	0	100	0	
10/12/2019 10:15	0.25	0.22	0.03	0	100.25	0	
10/12/2019 10:30	0.25	0.22	0.03	0	100.5	0	
10/12/2019 10:45	0.25	0.22	0.03	0	100.75	0	
10/12/2019 11:00	0.25	0.22	0.03	0	101	0	
10/12/2019 11:15	0.25	0.22	0.03	0	101.25	0	
10/12/2019 11:30	0.24	0.22	0.02	0	101.5	0	
10/12/2019 11:45	0.24	0.22	0.02	0	101.75	0	
10/12/2019 12:00	0.24	0.22	0.02	0	102	0	
10/12/2019 12:15	0.24	0.22	0.02	0	102.25	0	
10/12/2019 12:30	0.24	0.22	0.02	0.2	102.5	0	
10/12/2019 12:45	0.24	0.22	0.02	0.2	102.75	0.2	
10/12/2019 13:00	0.24	0.22	0.02	0	103	0.2	
10/12/2019 13:15	0.24	0.22	0.02	0.2	103.25	0.2	
10/12/2019 13:30	0.24	0.22	0.02	0	103.5	0	
10/12/2019 13:45	0.24	0.22	0.02	0	103.75	0.2	
10/12/2019 14:00	0.24	0.22	0.02	0	104	0	
10/12/2019 14:15	0.24	0.22	0.02	0.2	104.25	0	
10/12/2019 14:30	0.24	0.22	0.02	0	104.5	0	
10/12/2019 14:45	0.24	0.22	0.02	0	104.75	0	
10/12/2019 15:00	0.24	0.22	0.02	0	105	0	
10/12/2019 15:15	0.24	0.22	0.02	0	105.25	0	
10/12/2019 15:30	0.24	0.22	0.02	0	105.5	0	
10/12/2019 15:45	0.24	0.22	0.02	0	105.75	0	
10/12/2019 16:00	0.24	0.22	0.02	0	106	0	
10/12/2019 16:15	0.24	0.22	0.02	0	106.25	0	
10/12/2019 16:30	0.24	0.22	0.02	0	106.5	0	
10/12/2019 16:45	0.24	0.22	0.02	0	106.75	0	
10/12/2019 17:00	0.24	0.22	0.02	0	107	0	
10/12/2019 17:15	0.24	0.22	0.02	0	107.25	0	
10/12/2019 17:30	0.24	0.22	0.02	0	107.5	0	
10/12/2019 17:45	0.24	0.22	0.02	0	107.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
10/12/2019 18:00	0.24	0.22	0.02	0	108	0	
10/12/2019 18:15	0.24	0.22	0.02	0	108.25	0	
10/12/2019 18:30	0.24	0.22	0.02	0	108.5	0	
10/12/2019 18:45	0.24	0.22	0.02	0	108.75	0	
10/12/2019 19:00	0.24	0.22	0.02	0	109	0	
10/12/2019 19:15	0.24	0.22	0.02	0	109.25	0	
10/12/2019 19:30	0.24	0.22	0.02	0	109.5	0	
10/12/2019 19:45	0.24	0.22	0.02	0	109.75	0	
10/12/2019 20:00	0.24	0.22	0.02	0	110	0	
10/12/2019 20:15	0.25	0.22	0.03	0	110.25	0	
10/12/2019 20:30	0.25	0.22	0.03	0	110.5	0	
10/12/2019 20:45	0.25	0.22	0.03	0	110.75	0	
10/12/2019 21:00	0.25	0.22	0.03	0	111	0	
10/12/2019 21:15	0.25	0.22	0.03	0	111.25	0	
10/12/2019 21:30	0.25	0.22	0.03	0	111.5	0	
10/12/2019 21:45	0.25	0.22	0.03	0.4	111.75	0.2	
10/12/2019 22:00	0.25	0.22	0.03	0.6	112	0.6	
10/12/2019 22:15	0.25	0.22	0.03	0.2	112.25	0.2	
10/12/2019 22:30	0.25	0.22	0.03	0.2	112.5	0.2	
10/12/2019 22:45	0.26	0.22	0.04	0.2	112.75	0	
10/12/2019 23:00	0.26	0.22	0.04	0	113	0	
10/12/2019 23:15	0.26	0.22	0.04	0	113.25	0.2	
10/12/2019 23:30	0.26	0.22	0.04	0	113.5	0	
10/12/2019 23:45	0.26	0.22	0.04	0	113.75	0	
11/12/2019 00:00	0.27	0.22	0.05	0	114	0	
11/12/2019 00:15	0.27	0.22	0.05	0	114.25	0	
11/12/2019 00:30	0.27	0.22	0.05	0	114.5	0	
11/12/2019 00:45	0.27	0.22	0.05	0	114.75	0	
11/12/2019 01:00	0.27	0.22	0.05	0	115	0	
11/12/2019 01:15	0.27	0.22	0.05	0	115.25	0	
11/12/2019 01:30	0.28	0.22	0.06	0	115.5	0	
11/12/2019 01:45	0.28	0.22	0.06	0	115.75	0	
11/12/2019 02:00	0.28	0.22	0.06	0	116	0	
11/12/2019 02:15	0.28	0.22	0.06	0	116.25	0	
11/12/2019 02:30	0.29	0.22	0.07	0	116.5	0	
11/12/2019 02:45	0.29	0.22	0.07	0	116.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
11/12/2019 03:00	0.29	0.22	0.07	0	117	0	
11/12/2019 03:15	0.29	0.22	0.07	0	117.25	0	
11/12/2019 03:30	0.29	0.22	0.07	0	117.5	0	
11/12/2019 03:45	0.29	0.22	0.07	0	117.75	0	
11/12/2019 04:00	0.29	0.22	0.07	0	118	0	
11/12/2019 04:15	0.29	0.22	0.07	0	118.25	0	
11/12/2019 04:30	0.29	0.22	0.07	0	118.5	0	
11/12/2019 04:45	0.29	0.22	0.07	0	118.75	0	
11/12/2019 05:00	0.29	0.22	0.07	0	119	0	
11/12/2019 05:15	0.29	0.22	0.07	0	119.25	0	
11/12/2019 05:30	0.29	0.22	0.07	0	119.5	0	
11/12/2019 05:45	0.30	0.22	0.08	0	119.75	0	
11/12/2019 06:00	0.30	0.22	0.08	0	120	0	
11/12/2019 06:15	0.30	0.22	0.08	0	120.25	0	
11/12/2019 06:30	0.30	0.22	0.08	0	120.5	0	
11/12/2019 06:45	0.30	0.22	0.08	0	120.75	0	
11/12/2019 07:00	0.31	0.22	0.09	0	121	0	
11/12/2019 07:15	0.31	0.22	0.09	0	121.25	0	
11/12/2019 07:30	0.31	0.22	0.09	0	121.5	0	
11/12/2019 07:45	0.31	0.22	0.09	0	121.75	0	
11/12/2019 08:00	0.31	0.22	0.09	0	122	0	
11/12/2019 08:15	0.32	0.22	0.10	0	122.25	0	
11/12/2019 08:30	0.32	0.22	0.10	0	122.5	0	
11/12/2019 08:45	0.32	0.22	0.10	0	122.75	0	
11/12/2019 09:00	0.32	0.22	0.10	0	123	0	
11/12/2019 09:15	0.32	0.22	0.10	0	123.25	0	
11/12/2019 09:30	0.32	0.22	0.10	0	123.5	0	
11/12/2019 09:45	0.33	0.22	0.11	0	123.75	0	
11/12/2019 10:00	0.33	0.22	0.11	0	124	0	
11/12/2019 10:15	0.33	0.22	0.11	0	124.25	0	
11/12/2019 10:30	0.34	0.22	0.12	0	124.5	0	
11/12/2019 10:45	0.34	0.22	0.12	0	124.75	0	
11/12/2019 11:00	0.34	0.22	0.12	0	125	0	
11/12/2019 11:15	0.34	0.22	0.12	0	125.25	0	
11/12/2019 11:30	0.34	0.22	0.12	0	125.5	0	
11/12/2019 11:45	0.34	0.22	0.12	0	125.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
11/12/2019 12:00	0.34	0.22	0.12	0	126	0	
11/12/2019 12:15	0.34	0.22	0.12	0	126.25	0	
11/12/2019 12:30	0.34	0.22	0.12	0	126.5	0	
11/12/2019 12:45	0.34	0.22	0.12	0	126.75	0	
11/12/2019 13:00	0.34	0.22	0.12	0	127	0	
11/12/2019 13:15	0.34	0.22	0.12	0	127.25	0	
11/12/2019 13:30	0.34	0.22	0.12	0	127.5	0	
11/12/2019 13:45	0.34	0.22	0.12	0	127.75	0	
11/12/2019 14:00	0.35	0.22	0.13	0	128	0	
11/12/2019 14:15	0.35	0.22	0.13	0	128.25	0	
11/12/2019 14:30	0.35	0.22	0.13	0	128.5	0	
11/12/2019 14:45	0.35	0.22	0.13	0	128.75	0	
11/12/2019 15:00	0.35	0.22	0.13	0	129	0	
11/12/2019 15:15	0.35	0.22	0.13	0	129.25	0	
11/12/2019 15:30	0.35	0.22	0.13	0	129.5	0	
11/12/2019 15:45	0.35	0.22	0.13	0	129.75	0	
11/12/2019 16:00	0.35	0.22	0.13	0	130	0	
11/12/2019 16:15	0.35	0.22	0.13	0	130.25	0	
11/12/2019 16:30	0.35	0.22	0.13	0	130.5	0	
11/12/2019 16:45	0.35	0.22	0.13	0	130.75	0	
11/12/2019 17:00	0.35	0.22	0.13	0	131	0	
11/12/2019 17:15	0.35	0.22	0.13	0	131.25	0	
11/12/2019 17:30	0.35	0.22	0.13	0	131.5	0	
11/12/2019 17:45	0.35	0.22	0.13	0	131.75	0	
11/12/2019 18:00	0.35	0.22	0.13	0	132	0	
11/12/2019 18:15	0.35	0.22	0.13	0	132.25	0	
11/12/2019 18:30	0.35	0.22	0.13	0	132.5	0	
11/12/2019 18:45	0.35	0.22	0.13	0	132.75	0	
11/12/2019 19:00	0.35	0.22	0.13	0	133	0	
11/12/2019 19:15	0.35	0.22	0.13	0	133.25	0	
11/12/2019 19:30	0.35	0.22	0.13	0	133.5	0	
11/12/2019 19:45	0.35	0.22	0.13	0	133.75	0	
11/12/2019 20:00	0.35	0.22	0.13	0	134	0	
11/12/2019 20:15	0.35	0.22	0.13	0	134.25	0	
11/12/2019 20:30	0.35	0.22	0.13	0	134.5	0	
11/12/2019 20:45	0.36	0.22	0.14	0	134.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
11/12/2019 21:00	0.36	0.22	0.14	0	135	0	
11/12/2019 21:15	0.36	0.22	0.14	0	135.25	0	
11/12/2019 21:30	0.36	0.22	0.14	0	135.5	0	
11/12/2019 21:45	0.36	0.22	0.14	0	135.75	0	
11/12/2019 22:00	0.36	0.22	0.14	0	136	0	
11/12/2019 22:15	0.36	0.22	0.14	0	136.25	0	
11/12/2019 22:30	0.36	0.22	0.14	0	136.5	0	
11/12/2019 22:45	0.36	0.22	0.14	0	136.75	0	
11/12/2019 23:00	0.36	0.22	0.14	0	137	0	
11/12/2019 23:15	0.36	0.22	0.14	0	137.25	0	
11/12/2019 23:30	0.36	0.22	0.14	0	137.5	0	
11/12/2019 23:45	0.36	0.22	0.14	0	137.75	0	
12/12/2019 00:00	0.36	0.22	0.14	0	138	0	
12/12/2019 00:15	0.36	0.22	0.14	0	138.25	0	
12/12/2019 00:30	0.36	0.22	0.14	0	138.5	0	
12/12/2019 00:45	0.36	0.22	0.14	0	138.75	0	
12/12/2019 01:00	0.36	0.22	0.14	0	139	0	
12/12/2019 01:15	0.36	0.22	0.14	0	139.25	0	
12/12/2019 01:30	0.36	0.22	0.14	0	139.5	0	
12/12/2019 01:45	0.36	0.22	0.14	0	139.75	0	
12/12/2019 02:00	0.36	0.22	0.14	0	140	0	
12/12/2019 02:15	0.36	0.22	0.14	0	140.25	0	
12/12/2019 02:30	0.36	0.22	0.14	0	140.5	0	
12/12/2019 02:45	0.36	0.22	0.14	0	140.75	0	
12/12/2019 03:00	0.36	0.22	0.14	0	141	0	
12/12/2019 03:15	0.36	0.22	0.14	0	141.25	0	
12/12/2019 03:30	0.36	0.22	0.14	0	141.5	0	
12/12/2019 03:45	0.36	0.22	0.14	0	141.75	0	
12/12/2019 04:00	0.36	0.22	0.14	0	142	0	
12/12/2019 04:15	0.35	0.22	0.13	0	142.25	0	
12/12/2019 04:30	0.35	0.22	0.13	0	142.5	0	
12/12/2019 04:45	0.35	0.22	0.13	0	142.75	0	
12/12/2019 05:00	0.35	0.22	0.13	0	143	0	
12/12/2019 05:15	0.35	0.22	0.13	0	143.25	0	
12/12/2019 05:30	0.35	0.22	0.13	0	143.5	0	
12/12/2019 05:45	0.35	0.22	0.13	0	143.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
12/12/2019 06:00	0.35	0.22	0.13	0	144	0	
12/12/2019 06:15	0.35	0.22	0.13	0	144.25	0	
12/12/2019 06:30	0.35	0.22	0.13	0	144.5	0	
12/12/2019 06:45	0.35	0.22	0.13	0	144.75	0	
12/12/2019 07:00	0.34	0.22	0.12	0	145	0	
12/12/2019 07:15	0.34	0.22	0.12	0	145.25	0	
12/12/2019 07:30	0.34	0.22	0.12	0	145.5	0	
12/12/2019 07:45	0.34	0.22	0.12	0	145.75	0	
12/12/2019 08:00	0.34	0.22	0.12	0	146	0	
12/12/2019 08:15	0.34	0.22	0.12	0	146.25	0	
12/12/2019 08:30	0.34	0.22	0.12	0	146.5	0	
12/12/2019 08:45	0.34	0.22	0.12	0	146.75	0	
12/12/2019 09:00	0.34	0.22	0.12	0	147	0.2	
12/12/2019 09:15	0.33	0.22	0.11	0	147.25	0	
12/12/2019 09:30	0.33	0.22	0.11	0	147.5	0	
12/12/2019 09:45	0.33	0.22	0.11	0	147.75	0	
12/12/2019 10:00	0.33	0.22	0.11	0	148	0	
12/12/2019 10:15	0.33	0.22	0.11	0	148.25	0	
12/12/2019 10:30	0.32	0.22	0.10	0	148.5	0	
12/12/2019 10:45	0.32	0.22	0.10	0	148.75	0	
12/12/2019 11:00	0.32	0.22	0.10	0	149	0	
12/12/2019 11:15	0.32	0.22	0.10	0	149.25	0	
12/12/2019 11:30	0.32	0.22	0.10	0.2	149.5	0	
12/12/2019 11:45	0.32	0.22	0.10	0	149.75	0	
12/12/2019 12:00	0.32	0.22	0.10	0	150	0	
12/12/2019 12:15	0.32	0.22	0.10	0.2	150.25	0.2	
12/12/2019 12:30	0.32	0.22	0.10	0.4	150.5	0.2	
12/12/2019 12:45	0.32	0.22	0.10	0.6	150.75	0.6	
12/12/2019 13:00	0.32	0.22	0.10	0.8	151	0.4	
12/12/2019 13:15	0.32	0.22	0.10	0.8	151.25	0.6	
12/12/2019 13:30	0.32	0.22	0.10	0.4	151.5	0.8	
12/12/2019 13:45	0.32	0.22	0.10	0.6	151.75	0.2	
12/12/2019 14:00	0.32	0.22	0.10	0	152	0	
12/12/2019 14:15	0.32	0.22	0.10	0	152.25	0	
12/12/2019 14:30	0.33	0.22	0.11	0	152.5	0	
12/12/2019 14:45	0.33	0.22	0.11	0	152.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
12/12/2019 15:00	0.33	0.22	0.11	0	153	0	
12/12/2019 15:15	0.34	0.22	0.12	0	153.25	0	
12/12/2019 15:30	0.34	0.22	0.12	0	153.5	0	
12/12/2019 15:45	0.34	0.22	0.12	0	153.75	0	
12/12/2019 16:00	0.34	0.22	0.12	0	154	0	
12/12/2019 16:15	0.34	0.22	0.12	0	154.25	0	
12/12/2019 16:30	0.34	0.22	0.12	0.4	154.5	0	
12/12/2019 16:45	0.34	0.22	0.12	0.4	154.75	0.4	
12/12/2019 17:00	0.35	0.22	0.13	0.6	155	0.6	
12/12/2019 17:15	0.35	0.22	0.13	0.6	155.25	0.8	
12/12/2019 17:30	0.35	0.22	0.13	0.2	155.5	0.4	
12/12/2019 17:45	0.36	0.22	0.14	0.2	155.75	0.4	
12/12/2019 18:00	0.36	0.22	0.14	0.4	156	0.4	
12/12/2019 18:15	0.37	0.22	0.15	0.6	156.25	0.4	
12/12/2019 18:30	0.38	0.22	0.16	0.4	156.5	0.4	
12/12/2019 18:45	0.39	0.22	0.17	0.6	156.75	0.4	
12/12/2019 19:00	0.40	0.22	0.18	0	157	0.4	
12/12/2019 19:15	0.41	0.22	0.19	0.6	157.25	0.2	
12/12/2019 19:30	0.43	0.22	0.21	0.2	157.5	0.4	
12/12/2019 19:45	0.45	0.22	0.23	0.4	157.75	0.2	
12/12/2019 20:00	0.47	0.22	0.25	0.2	158	0.2	
12/12/2019 20:15	0.50	0.22	0.28	0.2	158.25	0.4	
12/12/2019 20:30	0.53	0.22	0.31	0.2	158.5	0.2	
12/12/2019 20:45	0.57	0.22	0.35	0.2	158.75	0.2	
12/12/2019 21:00	0.64	0.22	0.42	0	159	0.4	
12/12/2019 21:15	0.71	0.22	0.49	0	159.25	0.2	
12/12/2019 21:30	0.78	0.22	0.56	0	159.5	0	
12/12/2019 21:45	0.88	0.22	0.66	0	159.75	0	
12/12/2019 22:00	0.98	0.22	0.76	0	160	0	
12/12/2019 22:15	1.09	0.22	0.87	0	160.25	0	
12/12/2019 22:30	1.15	0.22	0.93	0	160.5	0	
12/12/2019 22:45	1.21	0.22	0.99	0	160.75	0	
12/12/2019 23:00	1.27	0.22	1.05	0	161	0	
12/12/2019 23:15	1.32	0.22	1.10	0	161.25	0	
12/12/2019 23:30	1.38	0.22	1.16	0	161.5	0	
12/12/2019 23:45	1.46	0.22	1.24	0	161.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
13/12/2019 00:00	1.54	0.22	1.32	0	162	0	
13/12/2019 00:15	1.67	0.22	1.45	0	162.25	0	
13/12/2019 00:30	1.82	0.22	1.60	0	162.5	0	
13/12/2019 00:45	1.98	0.22	1.76	0	162.75	0	
13/12/2019 01:00	2.15	0.22	1.93	0	163	0	
13/12/2019 01:15	2.32	0.22	2.10	0	163.25	0	
13/12/2019 01:30	2.48	0.22	2.26	0	163.5	0	
13/12/2019 01:45	2.63	0.22	2.41	0	163.75	0	
13/12/2019 02:00	2.78	0.22	2.56	0	164	0	
13/12/2019 02:15	2.92	0.22	2.70	0	164.25	0	
13/12/2019 02:30	3.06	0.22	2.84	0	164.5	0	
13/12/2019 02:45	3.18	0.22	2.96	0	164.75	0	
13/12/2019 03:00	3.28	0.22	3.06	0	165	0	
13/12/2019 03:15	3.42	0.22	3.20	0	165.25	0	
13/12/2019 03:30	3.52	0.22	3.30	0	165.5	0	
13/12/2019 03:45	3.59	0.22	3.37	0	165.75	0	
13/12/2019 04:00	3.65	0.22	3.43	0	166	0	
13/12/2019 04:15	3.70	0.22	3.48	0	166.25	0	
13/12/2019 04:30	3.75	0.22	3.53	0	166.5	0	
13/12/2019 04:45	3.79	0.22	3.57	0	166.75	0	
13/12/2019 05:00	3.83	0.22	3.61	0	167	0	
13/12/2019 05:15	3.86	0.22	3.64	0	167.25	0	
13/12/2019 05:30	3.88	0.22	3.66	0	167.5	0	
13/12/2019 05:45	3.90	0.22	3.68	0	167.75	0	
13/12/2019 06:00	3.90	0.22	3.68	0.2	168	0	
13/12/2019 06:15	3.91	0.22	3.69	0	168.25	0.2	
13/12/2019 06:30	3.91	0.22	3.69	0	168.5	0	
13/12/2019 06:45	3.91	0.22	3.69	0	168.75	0	
13/12/2019 07:00	3.90	0.22	3.68	0.2	169	0	
13/12/2019 07:15	3.90	0.22	3.68	0	169.25	0	
13/12/2019 07:30	3.87	0.22	3.65	0	169.5	0	
13/12/2019 07:45	3.85	0.22	3.63	0	169.75	0	
13/12/2019 08:00	3.83	0.22	3.61	0	170	0	
13/12/2019 08:15	3.80	0.22	3.58	0	170.25	0	
13/12/2019 08:30	3.77	0.22	3.55	0	170.5	0	
13/12/2019 08:45	3.75	0.22	3.53	0	170.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
13/12/2019 09:00	3.71	0.22	3.49	0	171	0	
13/12/2019 09:15	3.67	0.22	3.45	0	171.25	0	
13/12/2019 09:30	3.62	0.22	3.40	0	171.5	0	
13/12/2019 09:45	3.58	0.22	3.36	0	171.75	0	
13/12/2019 10:00	3.54	0.22	3.32	0	172	0	
13/12/2019 10:15	3.49	0.22	3.27	0	172.25	0	
13/12/2019 10:30	3.42	0.22	3.20	0	172.5	0	
13/12/2019 10:45	3.34	0.22	3.12	0	172.75	0	
13/12/2019 11:00	3.28	0.22	3.06	0	173	0	
13/12/2019 11:15	3.20	0.22	2.98	0	173.25	0	
13/12/2019 11:30	3.13	0.22	2.91	0	173.5	0	
13/12/2019 11:45	3.06	0.22	2.84	0	173.75	0	
13/12/2019 12:00	2.98	0.22	2.76	0	174	0	
13/12/2019 12:15	2.89	0.22	2.67	0	174.25	0	
13/12/2019 12:30	2.81	0.22	2.59	0	174.5	0	
13/12/2019 12:45	2.72	0.22	2.50	0	174.75	0	
13/12/2019 13:00	2.65	0.22	2.43	0	175	0	
13/12/2019 13:15	2.57	0.22	2.35	0	175.25	0	
13/12/2019 13:30	2.48	0.22	2.26	0	175.5	0	
13/12/2019 13:45	2.40	0.22	2.18	0	175.75	0	
13/12/2019 14:00	2.31	0.22	2.09	0	176	0	
13/12/2019 14:15	2.24	0.22	2.02	0	176.25	0	
13/12/2019 14:30	2.16	0.22	1.94	0	176.5	0	
13/12/2019 14:45	2.08	0.22	1.86	0	176.75	0	
13/12/2019 15:00	2.01	0.22	1.79	0	177	0	
13/12/2019 15:15	1.93	0.22	1.71	0	177.25	0	
13/12/2019 15:30	1.86	0.22	1.64	0	177.5	0	
13/12/2019 15:45	1.79	0.22	1.57	0	177.75	0	
13/12/2019 16:00	1.71	0.22	1.49	0	178	0	
13/12/2019 16:15	1.65	0.22	1.43	0	178.25	0	
13/12/2019 16:30	1.59	0.22	1.37	0	178.5	0	
13/12/2019 16:45	1.54	0.22	1.32	0	178.75	0	
13/12/2019 17:00	1.49	0.22	1.27	0	179	0	
13/12/2019 17:15	1.44	0.22	1.22	0	179.25	0	
13/12/2019 17:30	1.41	0.22	1.19	0	179.5	0	
13/12/2019 17:45	1.38	0.22	1.16	0	179.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
13/12/2019 18:00	1.35	0.22	1.13	0	180	0	
13/12/2019 18:15	1.32	0.22	1.10	0	180.25	0	
13/12/2019 18:30	1.31	0.22	1.09	0	180.5	0	
13/12/2019 18:45	1.30	0.22	1.08	0	180.75	0	
13/12/2019 19:00	1.28	0.22	1.06	0	181	0	
13/12/2019 19:15	1.26	0.22	1.04	0	181.25	0	
13/12/2019 19:30	1.25	0.22	1.03	0	181.5	0	
13/12/2019 19:45	1.24	0.22	1.02	0	181.75	0	
13/12/2019 20:00	1.22	0.22	1.00	0	182	0	
13/12/2019 20:15	1.22	0.22	1.00	0	182.25	0	
13/12/2019 20:30	1.20	0.22	0.98	0	182.5	0	
13/12/2019 20:45	1.20	0.22	0.98	0	182.75	0	
13/12/2019 21:00	1.18	0.22	0.96	0	183	0	
13/12/2019 21:15	1.17	0.22	0.95	0	183.25	0	
13/12/2019 21:30	1.16	0.22	0.94	0	183.5	0	
13/12/2019 21:45	1.15	0.22	0.93	0	183.75	0	
13/12/2019 22:00	1.14	0.22	0.92	0	184	0	
13/12/2019 22:15	1.13	0.22	0.91	0	184.25	0	
13/12/2019 22:30	1.13	0.22	0.91	0	184.5	0	
13/12/2019 22:45	1.11	0.22	0.89	0	184.75	0	
13/12/2019 23:00	1.11	0.22	0.89	0	185	0	
13/12/2019 23:15	1.10	0.22	0.88	0	185.25	0	
13/12/2019 23:30	1.09	0.22	0.87	0	185.5	0	
13/12/2019 23:45	1.07	0.22	0.85	0	185.75	0	
14/12/2019 00:00	1.06	0.22	0.84	0	186	0	
14/12/2019 00:15	1.05	0.22	0.83	0	186.25	0	
14/12/2019 00:30	1.04	0.22	0.82	0	186.5	0	
14/12/2019 00:45	1.01	0.22	0.79	0	186.75	0	
14/12/2019 01:00	1.00	0.22	0.78	0	187	0	
14/12/2019 01:15	0.99	0.22	0.77	0	187.25	0	
14/12/2019 01:30	0.98	0.22	0.76	0	187.5	0	
14/12/2019 01:45	0.97	0.22	0.75	0	187.75	0	
14/12/2019 02:00	0.96	0.22	0.74	0	188	0	
14/12/2019 02:15	0.94	0.22	0.72	0	188.25	0	
14/12/2019 02:30	0.93	0.22	0.71	0	188.5	0	
14/12/2019 02:45	0.92	0.22	0.70	0	188.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
14/12/2019 03:00	0.91	0.22	0.69	0	189	0	
14/12/2019 03:15	0.90	0.22	0.68	0	189.25	0	
14/12/2019 03:30	0.90	0.22	0.68	0	189.5	0	
14/12/2019 03:45	0.89	0.22	0.67	0	189.75	0	
14/12/2019 04:00	0.88	0.22	0.66	0	190	0	
14/12/2019 04:15	0.87	0.22	0.65	0	190.25	0	
14/12/2019 04:30	0.86	0.22	0.64	0	190.5	0	
14/12/2019 04:45	0.85	0.22	0.63	0	190.75	0	
14/12/2019 05:00	0.84	0.22	0.62	0	191	0	
14/12/2019 05:15	0.84	0.22	0.62	0	191.25	0	
14/12/2019 05:30	0.82	0.22	0.60	0	191.5	0	
14/12/2019 05:45	0.81	0.22	0.59	0	191.75	0	
14/12/2019 06:00	0.80	0.22	0.58	0	192	0	
14/12/2019 06:15	0.80	0.22	0.58	0	192.25	0	
14/12/2019 06:30	0.79	0.22	0.57	0	192.5	0	
14/12/2019 06:45	0.78	0.22	0.56	0	192.75	0	
14/12/2019 07:00	0.77	0.22	0.55	0	193	0	
14/12/2019 07:15	0.76	0.22	0.54	0	193.25	0	
14/12/2019 07:30	0.76	0.22	0.54	0	193.5	0	
14/12/2019 07:45	0.76	0.22	0.54	0	193.75	0	
14/12/2019 08:00	0.75	0.22	0.53	0	194	0	
14/12/2019 08:15	0.75	0.22	0.53	0	194.25	0	
14/12/2019 08:30	0.74	0.22	0.52	0	194.5	0	
14/12/2019 08:45	0.73	0.22	0.51	0	194.75	0	
14/12/2019 09:00	0.72	0.22	0.50	0	195	0	
14/12/2019 09:15	0.72	0.22	0.50	0	195.25	0	
14/12/2019 09:30	0.71	0.22	0.49	0	195.5	0	
14/12/2019 09:45	0.70	0.22	0.48	0	195.75	0	
14/12/2019 10:00	0.69	0.22	0.47	0	196	0	
14/12/2019 10:15	0.69	0.22	0.47	0	196.25	0	
14/12/2019 10:30	0.68	0.22	0.46	0	196.5	0	
14/12/2019 10:45	0.67	0.22	0.45	0	196.75	0	
14/12/2019 11:00	0.67	0.22	0.45	0	197	0	
14/12/2019 11:15	0.66	0.22	0.44	0	197.25	0	
14/12/2019 11:30	0.65	0.22	0.43	0	197.5	0	
14/12/2019 11:45	0.65	0.22	0.43	0.2	197.75	0.2	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
14/12/2019 12:00	0.65	0.22	0.43	1	198	0.8	
14/12/2019 12:15	0.64	0.22	0.42	0.8	198.25	0.8	
14/12/2019 12:30	0.63	0.22	0.41	0.2	198.5	0.2	
14/12/2019 12:45	0.63	0.22	0.41	0.2	198.75	0.2	
14/12/2019 13:00	0.62	0.22	0.40	0	199	0	
14/12/2019 13:15	0.61	0.22	0.39	0	199.25	0	
14/12/2019 13:30	0.61	0.22	0.39	0	199.5	0	
14/12/2019 13:45	0.60	0.22	0.38	0	199.75	0	
14/12/2019 14:00	0.60	0.22	0.38	0	200	0	
14/12/2019 14:15	0.60	0.22	0.38	0	200.25	0	
14/12/2019 14:30	0.59	0.22	0.37	0	200.5	0	
14/12/2019 14:45	0.58	0.22	0.36	0	200.75	0	
14/12/2019 15:00	0.57	0.22	0.35	0.2	201	0	
14/12/2019 15:15	0.57	0.22	0.35	0	201.25	0	
14/12/2019 15:30	0.56	0.22	0.34	0	201.5	0	
14/12/2019 15:45	0.56	0.22	0.34	0	201.75	0	
14/12/2019 16:00	0.56	0.22	0.34	0	202	0	
14/12/2019 16:15	0.56	0.22	0.34	0	202.25	0	
14/12/2019 16:30	0.55	0.22	0.33	0	202.5	0	
14/12/2019 16:45	0.54	0.22	0.32	0	202.75	0	
14/12/2019 17:00	0.54	0.22	0.32	0	203	0	
14/12/2019 17:15	0.53	0.22	0.31	0	203.25	0	
14/12/2019 17:30	0.53	0.22	0.31	0	203.5	0	
14/12/2019 17:45	0.53	0.22	0.31	0	203.75	0	
14/12/2019 18:00	0.53	0.22	0.31	0	204	0	
14/12/2019 18:15	0.52	0.22	0.30	0	204.25	0	
14/12/2019 18:30	0.51	0.22	0.29	0	204.5	0	
14/12/2019 18:45	0.51	0.22	0.29	0	204.75	0	
14/12/2019 19:00	0.50	0.22	0.28	0	205	0	
14/12/2019 19:15	0.50	0.22	0.28	0	205.25	0	
14/12/2019 19:30	0.50	0.22	0.28	0	205.5	0	
14/12/2019 19:45	0.50	0.22	0.28	0	205.75	0	
14/12/2019 20:00	0.50	0.22	0.28	0	206	0	
14/12/2019 20:15	0.50	0.22	0.28	0	206.25	0	
14/12/2019 20:30	0.49	0.22	0.27	0	206.5	0	
14/12/2019 20:45	0.49	0.22	0.27	0	206.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
14/12/2019 21:00	0.48	0.22	0.26	0	207	0	
14/12/2019 21:15	0.48	0.22	0.26	0	207.25	0	
14/12/2019 21:30	0.48	0.22	0.26	0	207.5	0	
14/12/2019 21:45	0.47	0.22	0.25	0	207.75	0	
14/12/2019 22:00	0.47	0.22	0.25	0	208	0	
14/12/2019 22:15	0.46	0.22	0.24	0	208.25	0	
14/12/2019 22:30	0.46	0.22	0.24	0	208.5	0	
14/12/2019 22:45	0.46	0.22	0.24	0	208.75	0	
14/12/2019 23:00	0.46	0.22	0.24	0	209	0	
14/12/2019 23:15	0.46	0.22	0.24	0	209.25	0	
14/12/2019 23:30	0.45	0.22	0.23	0	209.5	0	
14/12/2019 23:45	0.45	0.22	0.23	0.2	209.75	0.6	
15/12/2019 00:00	0.45	0.22	0.23	1	210	0.8	
15/12/2019 00:15	0.45	0.22	0.23	0.8	210.25	0.8	
15/12/2019 00:30	0.44	0.22	0.22	1.2	210.5	0.4	
15/12/2019 00:45	0.45	0.22	0.23	1.6	210.75	1.2	
15/12/2019 01:00	0.46	0.22	0.24	1.2	211	1.4	
15/12/2019 01:15	0.46	0.22	0.24	0.6	211.25	0.6	
15/12/2019 01:30	0.46	0.22	0.24	0.4	211.5	0.4	
15/12/2019 01:45	0.47	0.22	0.25	0.2	211.75	0	
15/12/2019 02:00	0.48	0.22	0.26	0	212	0	
15/12/2019 02:15	0.49	0.22	0.27	0	212.25	0	
15/12/2019 02:30	0.50	0.22	0.28	0	212.5	0	
15/12/2019 02:45	0.51	0.22	0.29	0	212.75	0	
15/12/2019 03:00	0.53	0.22	0.31	0	213	0	
15/12/2019 03:15	0.54	0.22	0.32	0	213.25	0	
15/12/2019 03:30	0.57	0.22	0.35	0	213.5	0	
15/12/2019 03:45	0.61	0.22	0.39	0	213.75	0	
15/12/2019 04:00	0.66	0.22	0.44	0	214	0	
15/12/2019 04:15	0.73	0.22	0.51	0	214.25	0	
15/12/2019 04:30	0.79	0.22	0.57	0	214.5	0	
15/12/2019 04:45	0.88	0.22	0.66	0	214.75	0	
15/12/2019 05:00	0.97	0.22	0.75	0	215	0	
15/12/2019 05:15	1.06	0.22	0.84	0	215.25	0	
15/12/2019 05:30	1.13	0.22	0.91	0	215.5	0	
15/12/2019 05:45	1.17	0.22	0.95	0	215.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
15/12/2019 06:00	1.22	0.22	1.00	0	216	0	
15/12/2019 06:15	1.26	0.22	1.04	0	216.25	0	
15/12/2019 06:30	1.30	0.22	1.08	0	216.5	0	
15/12/2019 06:45	1.34	0.22	1.12	0	216.75	0	
15/12/2019 07:00	1.38	0.22	1.16	0	217	0	
15/12/2019 07:15	1.42	0.22	1.20	0	217.25	0	
15/12/2019 07:30	1.47	0.22	1.25	0	217.5	0	
15/12/2019 07:45	1.51	0.22	1.29	0	217.75	0	
15/12/2019 08:00	1.58	0.22	1.36	0	218	0	
15/12/2019 08:15	1.64	0.22	1.42	0	218.25	0	
15/12/2019 08:30	1.71	0.22	1.49	0	218.5	0	
15/12/2019 08:45	1.79	0.22	1.57	0	218.75	0	
15/12/2019 09:00	1.86	0.22	1.64	0	219	0	
15/12/2019 09:15	1.92	0.22	1.70	0	219.25	0	
15/12/2019 09:30	1.98	0.22	1.76	0	219.5	0	
15/12/2019 09:45	2.04	0.22	1.82	0	219.75	0	
15/12/2019 10:00	2.08	0.22	1.86	0	220	0	
15/12/2019 10:15	2.11	0.22	1.89	0	220.25	0	
15/12/2019 10:30	2.14	0.22	1.92	0	220.5	0	
15/12/2019 10:45	2.17	0.22	1.95	0	220.75	0	
15/12/2019 11:00	2.19	0.22	1.97	0	221	0	
15/12/2019 11:15	2.20	0.22	1.98	0	221.25	0	
15/12/2019 11:30	2.21	0.22	1.99	0	221.5	0	
15/12/2019 11:45	2.22	0.22	2.00	0	221.75	0	
15/12/2019 12:00	2.22	0.22	2.00	0	222	0	
15/12/2019 12:15	2.21	0.22	1.99	0	222.25	0	
15/12/2019 12:30	2.20	0.22	1.98	0	222.5	0	
15/12/2019 12:45	2.19	0.22	1.97	0	222.75	0	
15/12/2019 13:00	2.17	0.22	1.95	0	223	0	
15/12/2019 13:15	2.14	0.22	1.92	0	223.25	0	
15/12/2019 13:30	2.11	0.22	1.89	0	223.5	0	
15/12/2019 13:45	2.08	0.22	1.86	0	223.75	0	
15/12/2019 14:00	2.04	0.22	1.82	0	224	0	
15/12/2019 14:15	2.01	0.22	1.79	0	224.25	0	
15/12/2019 14:30	1.97	0.22	1.75	0	224.5	0	
15/12/2019 14:45	1.93	0.22	1.71	0	224.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
15/12/2019 15:00	1.88	0.22	1.66	0	225	0	
15/12/2019 15:15	1.84	0.22	1.62	0	225.25	0	
15/12/2019 15:30	1.80	0.22	1.58	0	225.5	0	
15/12/2019 15:45	1.76	0.22	1.54	0	225.75	0	
15/12/2019 16:00	1.71	0.22	1.49	0	226	0	
15/12/2019 16:15	1.67	0.22	1.45	0	226.25	0	
15/12/2019 16:30	1.62	0.22	1.40	0	226.5	0	
15/12/2019 16:45	1.58	0.22	1.36	0	226.75	0	
15/12/2019 17:00	1.54	0.22	1.32	0	227	0	
15/12/2019 17:15	1.51	0.22	1.29	0	227.25	0	
15/12/2019 17:30	1.47	0.22	1.25	0	227.5	0	
15/12/2019 17:45	1.44	0.22	1.22	0	227.75	0	
15/12/2019 18:00	1.41	0.22	1.19	0	228	0	
15/12/2019 18:15	1.39	0.22	1.17	0	228.25	0	
15/12/2019 18:30	1.37	0.22	1.15	0	228.5	0	
15/12/2019 18:45	1.35	0.22	1.13	0	228.75	0	
15/12/2019 19:00	1.34	0.22	1.12	0	229	0	
15/12/2019 19:15	1.32	0.22	1.10	0	229.25	0	
15/12/2019 19:30	1.31	0.22	1.09	0	229.5	0	
15/12/2019 19:45	1.30	0.22	1.08	0	229.75	0	
15/12/2019 20:00	1.28	0.22	1.06	0	230	0	
15/12/2019 20:15	1.27	0.22	1.05	0	230.25	0	
15/12/2019 20:30	1.26	0.22	1.04	0	230.5	0	
15/12/2019 20:45	1.25	0.22	1.03	0	230.75	0	
15/12/2019 21:00	1.24	0.22	1.02	0	231	0	
15/12/2019 21:15	1.23	0.22	1.01	0	231.25	0	
15/12/2019 21:30	1.22	0.22	1.00	0	231.5	0	
15/12/2019 21:45	1.21	0.22	0.99	0	231.75	0	
15/12/2019 22:00	1.20	0.22	0.98	0	232	0	
15/12/2019 22:15	1.19	0.22	0.97	0	232.25	0	
15/12/2019 22:30	1.18	0.22	0.96	0	232.5	0	
15/12/2019 22:45	1.17	0.22	0.95	0	232.75	0	
15/12/2019 23:00	1.16	0.22	0.94	0	233	0	
15/12/2019 23:15	1.15	0.22	0.93	0	233.25	0	
15/12/2019 23:30	1.15	0.22	0.93	0	233.5	0	
15/12/2019 23:45	1.13	0.22	0.91	0	233.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
16/12/2019 00:00	1.13	0.22	0.91	0	234	0	
16/12/2019 00:15	1.12	0.22	0.90	0	234.25	0	
16/12/2019 00:30	1.11	0.22	0.89	0	234.5	0	
16/12/2019 00:45	1.11	0.22	0.89	0	234.75	0	
16/12/2019 01:00	1.10	0.22	0.88	0	235	0	
16/12/2019 01:15	1.09	0.22	0.87	0	235.25	0	
16/12/2019 01:30	1.07	0.22	0.85	0	235.5	0	
16/12/2019 01:45	1.05	0.22	0.83	0	235.75	0	
16/12/2019 02:00	1.04	0.22	0.82	0	236	0	
16/12/2019 02:15	1.03	0.22	0.81	0	236.25	0	
16/12/2019 02:30	1.01	0.22	0.79	0	236.5	0	
16/12/2019 02:45	1.00	0.22	0.78	0	236.75	0	
16/12/2019 03:00	0.99	0.22	0.77	0	237	0	
16/12/2019 03:15	0.98	0.22	0.76	0	237.25	0	
16/12/2019 03:30	0.97	0.22	0.75	0	237.5	0	
16/12/2019 03:45	0.96	0.22	0.74	0	237.75	0	
16/12/2019 04:00	0.96	0.22	0.74	0	238	0	
16/12/2019 04:15	0.94	0.22	0.72	0	238.25	0	
16/12/2019 04:30	0.93	0.22	0.71	0	238.5	0	
16/12/2019 04:45	0.92	0.22	0.70	0	238.75	0	
16/12/2019 05:00	0.91	0.22	0.69	0	239	0	
16/12/2019 05:15	0.90	0.22	0.68	0	239.25	0	
16/12/2019 05:30	0.89	0.22	0.67	0	239.5	0	
16/12/2019 05:45	0.88	0.22	0.66	0	239.75	0	
16/12/2019 06:00	0.88	0.22	0.66	0	240	0	
16/12/2019 06:15	0.87	0.22	0.65	0	240.25	0	
16/12/2019 06:30	0.86	0.22	0.64	0	240.5	0	
16/12/2019 06:45	0.85	0.22	0.63	0	240.75	0	
16/12/2019 07:00	0.84	0.22	0.62	0	241	0	
16/12/2019 07:15	0.82	0.22	0.60	0	241.25	0	
16/12/2019 07:30	0.82	0.22	0.60	0	241.5	0	
16/12/2019 07:45	0.81	0.22	0.59	0	241.75	0	
16/12/2019 08:00	0.80	0.22	0.58	0	242	0	
16/12/2019 08:15	0.80	0.22	0.58	0	242.25	0	
16/12/2019 08:30	0.79	0.22	0.57	0	242.5	0	
16/12/2019 08:45	0.78	0.22	0.56	0	242.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
16/12/2019 09:00	0.77	0.22	0.55	0	243	0	
16/12/2019 09:15	0.77	0.22	0.55	0	243.25	0	
16/12/2019 09:30	0.76	0.22	0.54	0	243.5	0	
16/12/2019 09:45	0.76	0.22	0.54	0	243.75	0	
16/12/2019 10:00	0.76	0.22	0.54	0	244	0	
16/12/2019 10:15	0.75	0.22	0.53	0	244.25	0	
16/12/2019 10:30	0.74	0.22	0.52	0	244.5	0	
16/12/2019 10:45	0.74	0.22	0.52	0	244.75	0	
16/12/2019 11:00	0.73	0.22	0.51	0	245	0	
16/12/2019 11:15	0.72	0.22	0.50	0	245.25	0	
16/12/2019 11:30	0.71	0.22	0.49	0	245.5	0	
16/12/2019 11:45	0.71	0.22	0.49	0	245.75	0	
16/12/2019 12:00	0.70	0.22	0.48	0	246	0	
16/12/2019 12:15	0.69	0.22	0.47	0	246.25	0	
16/12/2019 12:30	0.69	0.22	0.47	0	246.5	0	
16/12/2019 12:45	0.68	0.22	0.46	0	246.75	0	
16/12/2019 13:00	0.67	0.22	0.45	0	247	0	
16/12/2019 13:15	0.67	0.22	0.45	0	247.25	0	
16/12/2019 13:30	0.66	0.22	0.44	0	247.5	0	
16/12/2019 13:45	0.65	0.22	0.43	0	247.75	0	
16/12/2019 14:00	0.65	0.22	0.43	0	248	0	
16/12/2019 14:15	0.65	0.22	0.43	0	248.25	0	
16/12/2019 14:30	0.65	0.22	0.43	0	248.5	0	
16/12/2019 14:45	0.64	0.22	0.42	0	248.75	0	
16/12/2019 15:00	0.63	0.22	0.41	0	249	0	
16/12/2019 15:15	0.63	0.22	0.41	0	249.25	0	
16/12/2019 15:30	0.62	0.22	0.40	0	249.5	0	
16/12/2019 15:45	0.62	0.22	0.40	0	249.75	0	
16/12/2019 16:00	0.61	0.22	0.39	0	250	0	
16/12/2019 16:15	0.60	0.22	0.38	0	250.25	0	
16/12/2019 16:30	0.60	0.22	0.38	0	250.5	0	
16/12/2019 16:45	0.60	0.22	0.38	0	250.75	0	
16/12/2019 17:00	0.60	0.22	0.38	0	251	0	
16/12/2019 17:15	0.59	0.22	0.37	0	251.25	0	
16/12/2019 17:30	0.59	0.22	0.37	0	251.5	0	
16/12/2019 17:45	0.58	0.22	0.36	0	251.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
16/12/2019 18:00	0.57	0.22	0.35	0	252	0	
16/12/2019 18:15	0.57	0.22	0.35	0	252.25	0	
16/12/2019 18:30	0.56	0.22	0.34	0	252.5	0	
16/12/2019 18:45	0.56	0.22	0.34	0	252.75	0	
16/12/2019 19:00	0.56	0.22	0.34	0	253	0	
16/12/2019 19:15	0.56	0.22	0.34	0	253.25	0	
16/12/2019 19:30	0.55	0.22	0.33	0	253.5	0	
16/12/2019 19:45	0.55	0.22	0.33	0	253.75	0	
16/12/2019 20:00	0.54	0.22	0.32	0	254	0.2	
16/12/2019 20:15	0.54	0.22	0.32	0	254.25	0	
16/12/2019 20:30	0.53	0.22	0.31	0	254.5	0	
16/12/2019 20:45	0.53	0.22	0.31	0	254.75	0	
16/12/2019 21:00	0.53	0.22	0.31	0	255	0	
16/12/2019 21:15	0.53	0.22	0.31	0.2	255.25	0	
16/12/2019 21:30	0.52	0.22	0.30	0	255.5	0.2	
16/12/2019 21:45	0.52	0.22	0.30	0	255.75	0	
16/12/2019 22:00	0.52	0.22	0.30	0.2	256	0.2	
16/12/2019 22:15	0.51	0.22	0.29	0.2	256.25	0.4	
16/12/2019 22:30	0.51	0.22	0.29	0.2	256.5	0.2	
16/12/2019 22:45	0.50	0.22	0.28	0.2	256.75	0.4	
16/12/2019 23:00	0.50	0.22	0.28	0.2	257	0.2	
16/12/2019 23:15	0.50	0.22	0.28	0.2	257.25	0.2	
16/12/2019 23:30	0.50	0.22	0.28	0.4	257.5	0.4	
16/12/2019 23:45	0.50	0.22	0.28	0.4	257.75	0.4	
17/12/2019 00:00	0.50	0.22	0.28	0.6	258	0.8	
17/12/2019 00:15	0.50	0.22	0.28	0.4	258.25	0.6	
17/12/2019 00:30	0.50	0.22	0.28	0.2	258.5	0.4	
17/12/2019 00:45	0.50	0.22	0.28	0.2	258.75	0.4	
17/12/2019 01:00	0.50	0.22	0.28	0.2	259	0.6	
17/12/2019 01:15	0.50	0.22	0.28	0.2	259.25	0.4	
17/12/2019 01:30	0.50	0.22	0.28	0.2	259.5	0.2	
17/12/2019 01:45	0.50	0.22	0.28	0.2	259.75	0.2	
17/12/2019 02:00	0.50	0.22	0.28	0.4	260	0.4	
17/12/2019 02:15	0.50	0.22	0.28	0.2	260.25	0.4	
17/12/2019 02:30	0.50	0.22	0.28	0.4	260.5	0.2	
17/12/2019 02:45	0.50	0.22	0.28	0.2	260.75	0.4	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
17/12/2019 03:00	0.50	0.22	0.28	0.2	261	0.2	
17/12/2019 03:15	0.51	0.22	0.29	0.2	261.25	0.2	
17/12/2019 03:30	0.51	0.22	0.29	0	261.5	0.2	
17/12/2019 03:45	0.52	0.22	0.30	0.2	261.75	0.2	
17/12/2019 04:00	0.53	0.22	0.31	0.2	262	0.2	
17/12/2019 04:15	0.53	0.22	0.31	0.2	262.25	0.2	
17/12/2019 04:30	0.54	0.22	0.32	0.2	262.5	0	
17/12/2019 04:45	0.55	0.22	0.33	0.2	262.75	0	
17/12/2019 05:00	0.56	0.22	0.34	0.2	263	0.4	
17/12/2019 05:15	0.57	0.22	0.35	0.2	263.25	0.2	
17/12/2019 05:30	0.59	0.22	0.37	0	263.5	0	
17/12/2019 05:45	0.60	0.22	0.38	0	263.75	0	
17/12/2019 06:00	0.62	0.22	0.40	0.4	264	0.2	
17/12/2019 06:15	0.64	0.22	0.42	0.2	264.25	0	
17/12/2019 06:30	0.66	0.22	0.44	0.4	264.5	0.4	
17/12/2019 06:45	0.69	0.22	0.47	0.6	264.75	0.8	
17/12/2019 07:00	0.73	0.22	0.51	0.4	265	0.6	
17/12/2019 07:15	0.76	0.22	0.54	0.6	265.25	1	
17/12/2019 07:30	0.80	0.22	0.58	0.4	265.5	0.4	
17/12/2019 07:45	0.86	0.22	0.64	0.2	265.75	0.4	
17/12/2019 08:00	0.91	0.22	0.69	0.2	266	0.2	
17/12/2019 08:15	0.97	0.22	0.75	0.2	266.25	0.2	
17/12/2019 08:30	1.04	0.22	0.82	0.2	266.5	0.6	
17/12/2019 08:45	1.11	0.22	0.89	0.2	266.75	0.4	
17/12/2019 09:00	1.15	0.22	0.93	0.4	267	0.2	
17/12/2019 09:15	1.20	0.22	0.98	0.2	267.25	0.2	
17/12/2019 09:30	1.24	0.22	1.02	0.2	267.5	0.2	
17/12/2019 09:45	1.30	0.22	1.08	0.2	267.75	0.2	
17/12/2019 10:00	1.36	0.22	1.14	0.2	268	0.2	
17/12/2019 10:15	1.42	0.22	1.20	0.2	268.25	0	
17/12/2019 10:30	1.49	0.22	1.27	0	268.5	0.2	
17/12/2019 10:45	1.60	0.22	1.38	0.2	268.75	0.2	
17/12/2019 11:00	1.75	0.22	1.53	0.2	269	0.2	
17/12/2019 11:15	1.94	0.22	1.72	0.2	269.25	0.2	
17/12/2019 11:30	2.15	0.22	1.93	0	269.5	0	
17/12/2019 11:45	2.39	0.22	2.17	0	269.75	0.2	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
17/12/2019 12:00	2.63	0.22	2.41	0	270	0	
17/12/2019 12:15	2.89	0.22	2.67	0	270.25	0	
17/12/2019 12:30	3.16	0.22	2.94	0	270.5	0	
17/12/2019 12:45	3.43	0.22	3.21	0.2	270.75	0	
17/12/2019 13:00	3.66	0.22	3.44	0	271	0	
17/12/2019 13:15	3.85	0.22	3.63	0	271.25	0	
17/12/2019 13:30	4.04	0.22	3.82	0	271.5	0	
17/12/2019 13:45	4.22	0.22	4.00	0	271.75	0	
17/12/2019 14:00	4.39	0.22	4.17	0	272	0	
17/12/2019 14:15	4.55	0.22	4.33	0	272.25	0	
17/12/2019 14:30	4.70	0.22	4.48	0.2	272.5	0	
17/12/2019 14:45	4.82	0.22	4.60	0	272.75	0.2	
17/12/2019 15:00	4.93	0.22	4.71	0.2	273	0	
17/12/2019 15:15	5.02	0.22	4.80	0	273.25	0	
17/12/2019 15:30	5.11	0.22	4.89	0	273.5	0	
17/12/2019 15:45	5.18	0.22	4.96	0	273.75	0	
17/12/2019 16:00	5.25	0.22	5.03	0	274	0	
17/12/2019 16:15	5.31	0.22	5.09	0	274.25	0	
17/12/2019 16:30	5.36	0.22	5.14	0	274.5	0	
17/12/2019 16:45	5.41	0.22	5.19	0	274.75	0.2	
17/12/2019 17:00	5.44	0.22	5.22	0.2	275	0.2	
17/12/2019 17:15	5.48	0.22	5.26	0	275.25	0	
17/12/2019 17:30	5.51	0.22	5.29	0	275.5	0	
17/12/2019 17:45	5.54	0.22	5.32	0	275.75	0	
17/12/2019 18:00	5.57	0.22	5.35	0	276	0	
17/12/2019 18:15	5.60	0.22	5.38	0.2	276.25	0.2	
17/12/2019 18:30	5.62	0.22	5.40	0	276.5	0.2	
17/12/2019 18:45	5.63	0.22	5.41	0	276.75	0	
17/12/2019 19:00	5.65	0.22	5.43	0	277	0	
17/12/2019 19:15	5.66	0.22	5.44	0	277.25	0	
17/12/2019 19:30	5.68	0.22	5.46	0.4	277.5	0	
17/12/2019 19:45	5.69	0.22	5.47	0.2	277.75	0.2	
17/12/2019 20:00	5.71	0.22	5.49	0	278	0	
17/12/2019 20:15	5.73	0.22	5.51	0	278.25	0	
17/12/2019 20:30	5.74	0.22	5.52	0	278.5	0	
17/12/2019 20:45	5.74	0.22	5.52	0	278.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
17/12/2019 21:00	5.75	0.22	5.53	0	279	0.2	
17/12/2019 21:15	5.76	0.22	5.54	0	279.25	0	
17/12/2019 21:30	5.77	0.22	5.55	0	279.5	0	
17/12/2019 21:45	5.78	0.22	5.56	0	279.75	0	
17/12/2019 22:00	5.80	0.22	5.58	0	280	0	
17/12/2019 22:15	5.82	0.22	5.60	0	280.25	0	
17/12/2019 22:30	5.83	0.22	5.61	0	280.5	0	
17/12/2019 22:45	5.85	0.22	5.63	0	280.75	0	
17/12/2019 23:00	5.86	0.22	5.64	0	281	0	
17/12/2019 23:15	5.88	0.22	5.66	0	281.25	0	
17/12/2019 23:30	5.91	0.22	5.69	0	281.5	0	
17/12/2019 23:45	5.93	0.22	5.71	0	281.75	0	
18/12/2019 00:00	5.95	0.22	5.73	0	282	0	
18/12/2019 00:15	5.97	0.22	5.75	0	282.25	0	
18/12/2019 00:30	6.00	0.22	5.78	0	282.5	0	
18/12/2019 00:45	6.00	0.22	5.78	0	282.75	0	
18/12/2019 01:00	6.02	0.22	5.80	0.2	283	0	
18/12/2019 01:15	6.04	0.22	5.82	0	283.25	0	
18/12/2019 01:30	6.05	0.22	5.83	0	283.5	0	
18/12/2019 01:45	6.07	0.22	5.85	0	283.75	0	
18/12/2019 02:00	6.08	0.22	5.86	0	284	0	
18/12/2019 02:15	6.09	0.22	5.87	0	284.25	0	
18/12/2019 02:30	6.10	0.22	5.88	0	284.5	0	
18/12/2019 02:45	6.10	0.22	5.88	0	284.75	0	
18/12/2019 03:00	6.10	0.22	5.88	0	285	0	
18/12/2019 03:15	6.11	0.22	5.89	0	285.25	0	
18/12/2019 03:30	6.11	0.22	5.89	0	285.5	0	
18/12/2019 03:45	6.11	0.22	5.89	0	285.75	0	
18/12/2019 04:00	6.10	0.22	5.88	0	286	0	
18/12/2019 04:15	6.09	0.22	5.87	0	286.25	0	
18/12/2019 04:30	6.08	0.22	5.86	0	286.5	0	
18/12/2019 04:45	6.07	0.22	5.85	0	286.75	0	
18/12/2019 05:00	6.05	0.22	5.83	0	287	0	
18/12/2019 05:15	6.03	0.22	5.81	0	287.25	0	
18/12/2019 05:30	6.00	0.22	5.78	0	287.5	0	
18/12/2019 05:45	5.98	0.22	5.76	0	287.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
18/12/2019 06:00	5.95	0.22	5.73	0	288	0	
18/12/2019 06:15	5.91	0.22	5.69	0	288.25	0	
18/12/2019 06:30	5.87	0.22	5.65	0	288.5	0	
18/12/2019 06:45	5.83	0.22	5.61	0	288.75	0	
18/12/2019 07:00	5.78	0.22	5.56	0	289	0	
18/12/2019 07:15	5.74	0.22	5.52	0	289.25	0	
18/12/2019 07:30	5.68	0.22	5.46	0	289.5	0	
18/12/2019 07:45	5.62	0.22	5.40	0	289.75	0	
18/12/2019 08:00	5.56	0.22	5.34	0	290	0	
18/12/2019 08:15	5.51	0.22	5.29	0	290.25	0	
18/12/2019 08:30	5.43	0.22	5.21	0	290.5	0	
18/12/2019 08:45	5.37	0.22	5.15	0	290.75	0	
18/12/2019 09:00	5.30	0.22	5.08	0	291	0	
18/12/2019 09:15	5.22	0.22	5.00	0	291.25	0	
18/12/2019 09:30	5.13	0.22	4.91	0	291.5	0.2	
18/12/2019 09:45	5.05	0.22	4.83	0	291.75	0	
18/12/2019 10:00	4.97	0.22	4.75	0	292	0	
18/12/2019 10:15	4.89	0.22	4.67	0	292.25	0	
18/12/2019 10:30	4.81	0.22	4.59	0	292.5	0	
18/12/2019 10:45	4.70	0.22	4.48	0	292.75	0	
18/12/2019 11:00	4.60	0.22	4.38	0	293	0	
18/12/2019 11:15	4.48	0.22	4.26	0	293.25	0	
18/12/2019 11:30	4.37	0.22	4.15	0	293.5	0	
18/12/2019 11:45	4.26	0.22	4.04	0	293.75	0	
18/12/2019 12:00	4.15	0.22	3.93	0	294	0	
18/12/2019 12:15	4.04	0.22	3.82	0	294.25	0	
18/12/2019 12:30	3.92	0.22	3.70	0	294.5	0	
18/12/2019 12:45	3.82	0.22	3.60	0	294.75	0	
18/12/2019 13:00	3.71	0.22	3.49	0	295	0	
18/12/2019 13:15	3.61	0.22	3.39	0	295.25	0	
18/12/2019 13:30	3.51	0.22	3.29	0	295.5	0	
18/12/2019 13:45	3.36	0.22	3.14	0	295.75	0	
18/12/2019 14:00	3.23	0.22	3.01	0	296	0	
18/12/2019 14:15	3.10	0.22	2.88	0	296.25	0	
18/12/2019 14:30	2.97	0.22	2.75	0	296.5	0	
18/12/2019 14:45	2.85	0.22	2.63	0	296.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
18/12/2019 15:00	2.74	0.22	2.52	0	297	0	
18/12/2019 15:15	2.62	0.22	2.40	0	297.25	0	
18/12/2019 15:30	2.53	0.22	2.31	0	297.5	0	
18/12/2019 15:45	2.42	0.22	2.20	0	297.75	0	
18/12/2019 16:00	2.32	0.22	2.10	0	298	0	
18/12/2019 16:15	2.22	0.22	2.00	0	298.25	0	
18/12/2019 16:30	2.12	0.22	1.90	0	298.5	0	
18/12/2019 16:45	2.03	0.22	1.81	0	298.75	0	
18/12/2019 17:00	1.94	0.22	1.72	0	299	0	
18/12/2019 17:15	1.86	0.22	1.64	0	299.25	0	
18/12/2019 17:30	1.80	0.22	1.58	0	299.5	0	
18/12/2019 17:45	1.73	0.22	1.51	0	299.75	0	
18/12/2019 18:00	1.67	0.22	1.45	0	300	0	
18/12/2019 18:15	1.62	0.22	1.40	0	300.25	0	
18/12/2019 18:30	1.58	0.22	1.36	0	300.5	0	
18/12/2019 18:45	1.54	0.22	1.32	0	300.75	0	
18/12/2019 19:00	1.51	0.22	1.29	0	301	0	
18/12/2019 19:15	1.47	0.22	1.25	0	301.25	0	
18/12/2019 19:30	1.45	0.22	1.23	0	301.5	0	
18/12/2019 19:45	1.43	0.22	1.21	0	301.75	0	
18/12/2019 20:00	1.41	0.22	1.19	0	302	0	
18/12/2019 20:15	1.39	0.22	1.17	0	302.25	0	
18/12/2019 20:30	1.38	0.22	1.16	0	302.5	0	
18/12/2019 20:45	1.36	0.22	1.14	0.2	302.75	0	
18/12/2019 21:00	1.35	0.22	1.13	0.2	303	0.4	
18/12/2019 21:15	1.34	0.22	1.12	0	303.25	0	
18/12/2019 21:30	1.32	0.22	1.10	0	303.5	0	
18/12/2019 21:45	1.32	0.22	1.10	0	303.75	0.2	
18/12/2019 22:00	1.31	0.22	1.09	0	304	0	
18/12/2019 22:15	1.30	0.22	1.08	0	304.25	0	
18/12/2019 22:30	1.29	0.22	1.07	0	304.5	0	
18/12/2019 22:45	1.28	0.22	1.06	0	304.75	0	
18/12/2019 23:00	1.27	0.22	1.05	0	305	0	
18/12/2019 23:15	1.27	0.22	1.05	0	305.25	0	
18/12/2019 23:30	1.26	0.22	1.04	0	305.5	0	
18/12/2019 23:45	1.25	0.22	1.03	0	305.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
19/12/2019 00:00	1.24	0.22	1.02	0.2	306	0	
19/12/2019 00:15	1.24	0.22	1.02	0	306.25	0	
19/12/2019 00:30	1.22	0.22	1.00	0.2	306.5	0	
19/12/2019 00:45	1.22	0.22	1.00	0	306.75	0	
19/12/2019 01:00	1.21	0.22	0.99	0	307	0	
19/12/2019 01:15	1.20	0.22	0.98	0	307.25	0	
19/12/2019 01:30	1.20	0.22	0.98	0	307.5	0	
19/12/2019 01:45	1.20	0.22	0.98	0	307.75	0	
19/12/2019 02:00	1.18	0.22	0.96	0	308	0	
19/12/2019 02:15	1.17	0.22	0.95	0	308.25	0	
19/12/2019 02:30	1.17	0.22	0.95	0	308.5	0	
19/12/2019 02:45	1.17	0.22	0.95	0	308.75	0	
19/12/2019 03:00	1.16	0.22	0.94	0	309	0	
19/12/2019 03:15	1.15	0.22	0.93	0	309.25	0	
19/12/2019 03:30	1.15	0.22	0.93	0	309.5	0	
19/12/2019 03:45	1.14	0.22	0.92	0	309.75	0	
19/12/2019 04:00	1.13	0.22	0.91	0	310	0	
19/12/2019 04:15	1.13	0.22	0.91	0	310.25	0	
19/12/2019 04:30	1.13	0.22	0.91	0	310.5	0	
19/12/2019 04:45	1.12	0.22	0.90	0	310.75	0	
19/12/2019 05:00	1.11	0.22	0.89	0	311	0	
19/12/2019 05:15	1.11	0.22	0.89	0	311.25	0	
19/12/2019 05:30	1.11	0.22	0.89	0	311.5	0	
19/12/2019 05:45	1.10	0.22	0.88	0	311.75	0	
19/12/2019 06:00	1.10	0.22	0.88	0	312	0	
19/12/2019 06:15	1.09	0.22	0.87	0	312.25	0	
19/12/2019 06:30	1.07	0.22	0.85	0	312.5	0	
19/12/2019 06:45	1.06	0.22	0.84	0	312.75	0	
19/12/2019 07:00	1.06	0.22	0.84	0	313	0	
19/12/2019 07:15	1.05	0.22	0.83	0	313.25	0	
19/12/2019 07:30	1.05	0.22	0.83	0	313.5	0	
19/12/2019 07:45	1.04	0.22	0.82	0	313.75	0	
19/12/2019 08:00	1.03	0.22	0.81	0	314	0	
19/12/2019 08:15	1.03	0.22	0.81	0	314.25	0	
19/12/2019 08:30	1.01	0.22	0.79	0	314.5	0	
19/12/2019 08:45	1.01	0.22	0.79	0	314.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
19/12/2019 09:00	1.00	0.22	0.78	0	315	0	
19/12/2019 09:15	1.00	0.22	0.78	0	315.25	0	
19/12/2019 09:30	0.99	0.22	0.77	0	315.5	0	
19/12/2019 09:45	0.98	0.22	0.76	0	315.75	0	
19/12/2019 10:00	0.98	0.22	0.76	0	316	0	
19/12/2019 10:15	0.97	0.22	0.75	0	316.25	0	
19/12/2019 10:30	0.97	0.22	0.75	0	316.5	0	
19/12/2019 10:45	0.96	0.22	0.74	0	316.75	0	
19/12/2019 11:00	0.96	0.22	0.74	0	317	0	
19/12/2019 11:15	0.96	0.22	0.74	0	317.25	0	
19/12/2019 11:30	0.94	0.22	0.72	0	317.5	0	
19/12/2019 11:45	0.94	0.22	0.72	0	317.75	0	
19/12/2019 12:00	0.93	0.22	0.71	0	318	0	
19/12/2019 12:15	0.93	0.22	0.71	0	318.25	0	
19/12/2019 12:30	0.92	0.22	0.70	0	318.5	0	
19/12/2019 12:45	0.92	0.22	0.70	0	318.75	0	
19/12/2019 13:00	0.91	0.22	0.69	0	319	0	
19/12/2019 13:15	0.91	0.22	0.69	0	319.25	0	
19/12/2019 13:30	0.90	0.22	0.68	0	319.5	0	
19/12/2019 13:45	0.89	0.22	0.67	0	319.75	0	
19/12/2019 14:00	0.89	0.22	0.67	0	320	0	
19/12/2019 14:15	0.88	0.22	0.66	0	320.25	0	
19/12/2019 14:30	0.88	0.22	0.66	0	320.5	0	
19/12/2019 14:45	0.87	0.22	0.65	0	320.75	0	
19/12/2019 15:00	0.87	0.22	0.65	0	321	0	
19/12/2019 15:15	0.86	0.22	0.64	0	321.25	0	
19/12/2019 15:30	0.86	0.22	0.64	0	321.5	0	
19/12/2019 15:45	0.85	0.22	0.63	0	321.75	0	
19/12/2019 16:00	0.85	0.22	0.63	0	322	0	
19/12/2019 16:15	0.84	0.22	0.62	0	322.25	0	
19/12/2019 16:30	0.84	0.22	0.62	0	322.5	0	
19/12/2019 16:45	0.84	0.22	0.62	0	322.75	0	
19/12/2019 17:00	0.82	0.22	0.60	0	323	0	
19/12/2019 17:15	0.82	0.22	0.60	0	323.25	0	
19/12/2019 17:30	0.82	0.22	0.60	0	323.5	0	
19/12/2019 17:45	0.81	0.22	0.59	0	323.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
19/12/2019 18:00	0.81	0.22	0.59	0	324	0	
19/12/2019 18:15	0.80	0.22	0.58	0	324.25	0	
19/12/2019 18:30	0.80	0.22	0.58	0	324.5	0	
19/12/2019 18:45	0.80	0.22	0.58	0	324.75	0	
19/12/2019 19:00	0.79	0.22	0.57	0	325	0	
19/12/2019 19:15	0.79	0.22	0.57	0	325.25	0	
19/12/2019 19:30	0.78	0.22	0.56	0	325.5	0	
19/12/2019 19:45	0.78	0.22	0.56	0	325.75	0	
19/12/2019 20:00	0.78	0.22	0.56	0	326	0	
19/12/2019 20:15	0.77	0.22	0.55	0	326.25	0	
19/12/2019 20:30	0.77	0.22	0.55	0	326.5	0	
19/12/2019 20:45	0.77	0.22	0.55	0	326.75	0.2	
19/12/2019 21:00	0.76	0.22	0.54	0	327	0.2	
19/12/2019 21:15	0.76	0.22	0.54	0.2	327.25	0.6	
19/12/2019 21:30	0.76	0.22	0.54	0	327.5	0.2	
19/12/2019 21:45	0.76	0.22	0.54	0.2	327.75	0	
19/12/2019 22:00	0.76	0.22	0.54	0	328	0.2	
19/12/2019 22:15	0.76	0.22	0.54	0	328.25	0	
19/12/2019 22:30	0.75	0.22	0.53	0.4	328.5	0.2	
19/12/2019 22:45	0.75	0.22	0.53	0.2	328.75	0.8	
19/12/2019 23:00	0.75	0.22	0.53	0	329	0.4	
19/12/2019 23:15	0.75	0.22	0.53	0.2	329.25	0.2	
19/12/2019 23:30	0.75	0.22	0.53	0	329.5	0.4	
19/12/2019 23:45	0.74	0.22	0.52	0	329.75	0.4	
20/12/2019 00:00	0.74	0.22	0.52	0.2	330	0	
20/12/2019 00:15	0.74	0.22	0.52	0	330.25	0	
20/12/2019 00:30	0.74	0.22	0.52	0.2	330.5	0.2	
20/12/2019 00:45	0.74	0.22	0.52	0	330.75	0	
20/12/2019 01:00	0.73	0.22	0.51	0	331	0	
20/12/2019 01:15	0.73	0.22	0.51	0	331.25	0	
20/12/2019 01:30	0.73	0.22	0.51	0	331.5	0	
20/12/2019 01:45	0.73	0.22	0.51	0	331.75	0	
20/12/2019 02:00	0.73	0.22	0.51	0	332	0.2	
20/12/2019 02:15	0.73	0.22	0.51	0	332.25	0.4	
20/12/2019 02:30	0.73	0.22	0.51	0	332.5	0	
20/12/2019 02:45	0.73	0.22	0.51	0	332.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
20/12/2019 03:00	0.73	0.22	0.51	0.2	333	0.2	
20/12/2019 03:15	0.73	0.22	0.51	0.6	333.25	0.6	
20/12/2019 03:30	0.73	0.22	0.51	1	333.5	0.4	
20/12/2019 03:45	0.73	0.22	0.51	0.4	333.75	0.2	
20/12/2019 04:00	0.74	0.22	0.52	0.4	334	0.4	
20/12/2019 04:15	0.75	0.22	0.53	0.6	334.25	0.4	
20/12/2019 04:30	0.76	0.22	0.54	0.4	334.5	0.4	
20/12/2019 04:45	0.76	0.22	0.54	0.6	334.75	0.4	
20/12/2019 05:00	0.79	0.22	0.57	0.4	335	0.6	
20/12/2019 05:15	0.81	0.22	0.59	1.2	335.25	0.8	
20/12/2019 05:30	0.85	0.22	0.63	1	335.5	0.8	
20/12/2019 05:45	0.89	0.22	0.67	0.6	335.75	0.4	
20/12/2019 06:00	0.94	0.22	0.72	0.4	336	0.4	
20/12/2019 06:15	1.01	0.22	0.79	0.6	336.25	0.4	
20/12/2019 06:30	1.10	0.22	0.88	0.4	336.5	0.2	
20/12/2019 06:45	1.15	0.22	0.93	0.4	336.75	0.4	
20/12/2019 07:00	1.22	0.22	1.00	0.4	337	0.2	
20/12/2019 07:15	1.29	0.22	1.07	0.2	337.25	0.2	
20/12/2019 07:30	1.37	0.22	1.15	0.4	337.5	0.2	
20/12/2019 07:45	1.47	0.22	1.25	0.2	337.75	0	
20/12/2019 08:00	1.62	0.22	1.40	0.6	338	0.2	
20/12/2019 08:15	1.88	0.22	1.66	0.2	338.25	0.2	
20/12/2019 08:30	2.24	0.22	2.02	0.4	338.5	0.6	
20/12/2019 08:45	2.65	0.22	2.43	0.4	338.75	0.4	
20/12/2019 09:00	3.12	0.22	2.90	0.6	339	0.4	
20/12/2019 09:15	3.59	0.22	3.37	0.2	339.25	0.2	
20/12/2019 09:30	3.93	0.22	3.71	0.4	339.5	0.2	
20/12/2019 09:45	4.25	0.22	4.03	0.2	339.75	0.2	
20/12/2019 10:00	4.55	0.22	4.33	0.2	340	0.2	
20/12/2019 10:15	4.84	0.22	4.62	0.2	340.25	0.2	
20/12/2019 10:30	5.07	0.22	4.85	0.2	340.5	0	
20/12/2019 10:45	5.30	0.22	5.08	0	340.75	0	
20/12/2019 11:00	5.50	0.22	5.28	0	341	0	
20/12/2019 11:15	5.66	0.22	5.44	0.2	341.25	0.2	
20/12/2019 11:30	5.82	0.22	5.60	0	341.5	0	
20/12/2019 11:45	5.97	0.22	5.75	0.2	341.75	0.2	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
20/12/2019 12:00	6.09	0.22	5.87	0	342	0	
20/12/2019 12:15	6.21	0.22	5.99	0	342.25	0	
20/12/2019 12:30	6.31	0.22	6.09	0	342.5	0	
20/12/2019 12:45	6.42	0.22	6.20	0	342.75	0	
20/12/2019 13:00	6.51	0.22	6.29	0	343	0	
20/12/2019 13:15	6.62	0.22	6.40	0	343.25	0	
20/12/2019 13:30	6.73	0.22	6.51	0	343.5	0	
20/12/2019 13:45	6.83	0.22	6.61	0	343.75	0	
20/12/2019 14:00	6.93	0.22	6.71	0	344	0	
20/12/2019 14:15	7.02	0.22	6.80	0	344.25	0	
20/12/2019 14:30	7.11	0.22	6.89	0	344.5	0	
20/12/2019 14:45	7.20	0.22	6.98	0	344.75	0	
20/12/2019 15:00	7.29	0.22	7.07	0	345	0	
20/12/2019 15:15	7.37	0.22	7.15	0	345.25	0	
20/12/2019 15:30	7.44	0.22	7.22	0	345.5	0	
20/12/2019 15:45	7.51	0.22	7.29	0	345.75	0	
20/12/2019 16:00	7.60	0.22	7.38	0	346	0	
20/12/2019 16:15	7.67	0.22	7.45	0	346.25	0	
20/12/2019 16:30	7.76	0.22	7.54	0	346.5	0	
20/12/2019 16:45	7.84	0.22	7.62	0	346.75	0	
20/12/2019 17:00	7.92	0.22	7.70	0	347	0	
20/12/2019 17:15	8.01	0.22	7.79	0	347.25	0	
20/12/2019 17:30	8.10	0.22	7.88	0	347.5	0	
20/12/2019 17:45	8.19	0.22	7.97	0	347.75	0	
20/12/2019 18:00	8.29	0.22	8.07	0	348	0	
20/12/2019 18:15	8.37	0.22	8.15	0	348.25	0	
20/12/2019 18:30	8.45	0.22	8.23	0	348.5	0	
20/12/2019 18:45	8.53	0.22	8.31	0	348.75	0	
20/12/2019 19:00	8.62	0.22	8.40	0	349	0	
20/12/2019 19:15	8.71	0.22	8.49	0	349.25	0	
20/12/2019 19:30	8.78	0.22	8.56	0	349.5	0	
20/12/2019 19:45	8.86	0.22	8.64	0	349.75	0	
20/12/2019 20:00	8.98	0.22	8.76	0	350	0	
20/12/2019 20:15	9.14	0.22	8.92	0	350.25	0	
20/12/2019 20:30	9.32	0.22	9.10	0	350.5	0	
20/12/2019 20:45	9.48	0.22	9.26	0	350.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
20/12/2019 21:00	9.65	0.22	9.43	0	351	0	
20/12/2019 21:15	9.84	0.22	9.62	0	351.25	0	
20/12/2019 21:30	10.06	0.22	9.84	0	351.5	0	
20/12/2019 21:45	10.21	0.22	9.99	0	351.75	0	
20/12/2019 22:00	10.41	0.22	10.19	0	352	0	
20/12/2019 22:15	10.58	0.22	10.36	0	352.25	0	
20/12/2019 22:30	10.76	0.22	10.54	0	352.5	0	
20/12/2019 22:45	10.94	0.22	10.72	0.2	352.75	0	
20/12/2019 23:00	11.09	0.22	10.87	0	353	0	
20/12/2019 23:15	11.21	0.22	10.99	0	353.25	0	
20/12/2019 23:30	11.33	0.22	11.11	0	353.5	0	
20/12/2019 23:45	11.52	0.22	11.30	0	353.75	0	
21/12/2019 00:00	11.61	0.22	11.39	0	354	0	
21/12/2019 00:15	11.77	0.22	11.55	0	354.25	0	
21/12/2019 00:30	11.90	0.22	11.68	0	354.5	0	
21/12/2019 00:45	11.96	0.22	11.74	0	354.75	0	
21/12/2019 01:00	12.09	0.22	11.87	0	355	0	
21/12/2019 01:15	12.12	0.22	11.90	0	355.25	0	
21/12/2019 01:30	12.18	0.22	11.96	0	355.5	0.2	
21/12/2019 01:45	12.28	0.22	12.06	0	355.75	0	
21/12/2019 02:00	12.25	0.22	12.03	0	356	0	
21/12/2019 02:15	12.31	0.22	12.09	0	356.25	0	
21/12/2019 02:30	12.28	0.22	12.06	0.8	356.5	0.4	
21/12/2019 02:45	12.31	0.22	12.09	0.6	356.75	0.6	
21/12/2019 03:00	12.28	0.22	12.06	0	357	0	
21/12/2019 03:15	12.28	0.22	12.06	0.2	357.25	0.2	
21/12/2019 03:30	12.22	0.22	12.00	0	357.5	0.2	
21/12/2019 03:45	12.15	0.22	11.93	0	357.75	0.4	
21/12/2019 04:00	12.05	0.22	11.83	0	358	0	
21/12/2019 04:15	12.02	0.22	11.80	0	358.25	0	
21/12/2019 04:30	11.93	0.22	11.71	0	358.5	0	
21/12/2019 04:45	11.83	0.22	11.61	0.2	358.75	0	
21/12/2019 05:00	11.74	0.22	11.52	0	359	0	
21/12/2019 05:15	11.55	0.22	11.33	0	359.25	0.2	
21/12/2019 05:30	11.43	0.22	11.21	0	359.5	0	
21/12/2019 05:45	11.24	0.22	11.02	0	359.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
21/12/2019 06:00	11.12	0.22	10.90	0	360	0	
21/12/2019 06:15	10.97	0.22	10.75	0	360.25	0	
21/12/2019 06:30	10.82	0.22	10.60	0	360.5	0	
21/12/2019 06:45	10.61	0.22	10.39	0	360.75	0	
21/12/2019 07:00	10.44	0.22	10.22	0	361	0	
21/12/2019 07:15	10.24	0.22	10.02	0	361.25	0	
21/12/2019 07:30	10.04	0.22	9.82	0	361.5	0	
21/12/2019 07:45	9.84	0.22	9.62	0	361.75	0	
21/12/2019 08:00	9.59	0.22	9.37	0	362	0	
21/12/2019 08:15	9.40	0.22	9.18	0.2	362.25	0	
21/12/2019 08:30	9.19	0.22	8.97	0.4	362.5	0.6	
21/12/2019 08:45	8.98	0.22	8.76	0.4	362.75	1	
21/12/2019 09:00	8.84	0.22	8.62	0.4	363	0.2	
21/12/2019 09:15	8.76	0.22	8.54	0	363.25	0	
21/12/2019 09:30	8.65	0.22	8.43	0	363.5	0	
21/12/2019 09:45	8.55	0.22	8.33	0	363.75	0	
21/12/2019 10:00	8.44	0.22	8.22	0	364	0	
21/12/2019 10:15	8.34	0.22	8.12	0	364.25	0	
21/12/2019 10:30	8.24	0.22	8.02	0	364.5	0	
21/12/2019 10:45	8.12	0.22	7.90	0.6	364.75	0	
21/12/2019 11:00	8.01	0.22	7.79	0	365	0.6	
21/12/2019 11:15	7.89	0.22	7.67	0	365.25	0.4	
21/12/2019 11:30	7.78	0.22	7.56	0	365.5	0.2	
21/12/2019 11:45	7.67	0.22	7.45	0.2	365.75	0.2	
21/12/2019 12:00	7.54	0.22	7.32	0	366	0	
21/12/2019 12:15	7.44	0.22	7.22	0	366.25	0.2	
21/12/2019 12:30	7.31	0.22	7.09	0	366.5	0	
21/12/2019 12:45	7.20	0.22	6.98	0	366.75	0	
21/12/2019 13:00	7.09	0.22	6.87	0	367	0	
21/12/2019 13:15	6.97	0.22	6.75	0	367.25	0	
21/12/2019 13:30	6.84	0.22	6.62	0	367.5	0	
21/12/2019 13:45	6.71	0.22	6.49	0	367.75	0	
21/12/2019 14:00	6.59	0.22	6.37	0	368	0	
21/12/2019 14:15	6.47	0.22	6.25	0	368.25	0	
21/12/2019 14:30	6.34	0.22	6.12	0	368.5	0	
21/12/2019 14:45	6.21	0.22	5.99	0	368.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
21/12/2019 15:00	6.08	0.22	5.86	0	369	0	
21/12/2019 15:15	5.96	0.22	5.74	0	369.25	0	
21/12/2019 15:30	5.84	0.22	5.62	0	369.5	0	
21/12/2019 15:45	5.72	0.22	5.50	0	369.75	0	
21/12/2019 16:00	5.60	0.22	5.38	0	370	0	
21/12/2019 16:15	5.48	0.22	5.26	0	370.25	0	
21/12/2019 16:30	5.37	0.22	5.15	0	370.5	0.4	
21/12/2019 16:45	5.26	0.22	5.04	0	370.75	0	
21/12/2019 17:00	5.15	0.22	4.93	0	371	0	
21/12/2019 17:15	5.05	0.22	4.83	0	371.25	0	
21/12/2019 17:30	4.96	0.22	4.74	0	371.5	0	
21/12/2019 17:45	4.87	0.22	4.65	0	371.75	0	
21/12/2019 18:00	4.77	0.22	4.55	0	372	0	
21/12/2019 18:15	4.67	0.22	4.45	0	372.25	0	
21/12/2019 18:30	4.57	0.22	4.35	0	372.5	0	
21/12/2019 18:45	4.47	0.22	4.25	0	372.75	0	
21/12/2019 19:00	4.39	0.22	4.17	0	373	0	
21/12/2019 19:15	4.30	0.22	4.08	0	373.25	0	
21/12/2019 19:30	4.22	0.22	4.00	0	373.5	0	
21/12/2019 19:45	4.14	0.22	3.92	0	373.75	0	
21/12/2019 20:00	4.05	0.22	3.83	0	374	0	
21/12/2019 20:15	3.99	0.22	3.77	0	374.25	0	
21/12/2019 20:30	3.91	0.22	3.69	0	374.5	0	
21/12/2019 20:45	3.85	0.22	3.63	0	374.75	0	
21/12/2019 21:00	3.78	0.22	3.56	0	375	0	
21/12/2019 21:15	3.72	0.22	3.50	0	375.25	0	
21/12/2019 21:30	3.66	0.22	3.44	0	375.5	0	
21/12/2019 21:45	3.60	0.22	3.38	0	375.75	0	
21/12/2019 22:00	3.53	0.22	3.31	0.2	376	0.2	
21/12/2019 22:15	3.46	0.22	3.24	0.2	376.25	0.2	
21/12/2019 22:30	3.38	0.22	3.16	0	376.5	0	
21/12/2019 22:45	3.30	0.22	3.08	0	376.75	0	
21/12/2019 23:00	3.22	0.22	3.00	0.4	377	0.2	
21/12/2019 23:15	3.16	0.22	2.94	0	377.25	0	
21/12/2019 23:30	3.09	0.22	2.87	0.4	377.5	0.2	
21/12/2019 23:45	3.02	0.22	2.80	0.2	377.75	0.2	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
22/12/2019 00:00	2.96	0.22	2.74	0.2	378	0	
22/12/2019 00:15	2.89	0.22	2.67	0	378.25	0.4	
22/12/2019 00:30	2.84	0.22	2.62	0.2	378.5	0	
22/12/2019 00:45	2.79	0.22	2.57	0	378.75	0.2	
22/12/2019 01:00	2.72	0.22	2.50	0	379	0	
22/12/2019 01:15	2.67	0.22	2.45	0	379.25	0	
22/12/2019 01:30	2.62	0.22	2.40	0	379.5	0	
22/12/2019 01:45	2.57	0.22	2.35	0	379.75	0	
22/12/2019 02:00	2.52	0.22	2.30	0.2	380	0	
22/12/2019 02:15	2.48	0.22	2.26	0	380.25	0	
22/12/2019 02:30	2.43	0.22	2.21	0	380.5	0.4	
22/12/2019 02:45	2.39	0.22	2.17	0	380.75	0	
22/12/2019 03:00	2.35	0.22	2.13	0	381	0	
22/12/2019 03:15	2.31	0.22	2.09	0	381.25	0	
22/12/2019 03:30	2.28	0.22	2.06	0	381.5	0	
22/12/2019 03:45	2.25	0.22	2.03	0	381.75	0.2	
22/12/2019 04:00	2.22	0.22	2.00	0	382	0	
22/12/2019 04:15	2.19	0.22	1.97	0	382.25	0	
22/12/2019 04:30	2.16	0.22	1.94	0.2	382.5	0	
22/12/2019 04:45	2.14	0.22	1.92	0	382.75	0	
22/12/2019 05:00	2.13	0.22	1.91	0	383	0	
22/12/2019 05:15	2.10	0.22	1.88	0	383.25	0	
22/12/2019 05:30	2.09	0.22	1.87	0	383.5	0	
22/12/2019 05:45	2.07	0.22	1.85	0	383.75	0	
22/12/2019 06:00	2.06	0.22	1.84	0	384	0	
22/12/2019 06:15	2.05	0.22	1.83	0	384.25	0	
22/12/2019 06:30	2.04	0.22	1.82	0	384.5	0	
22/12/2019 06:45	2.04	0.22	1.82	0	384.75	0	
22/12/2019 07:00	2.04	0.22	1.82	0.2	385	0	
22/12/2019 07:15	2.03	0.22	1.81	0	385.25	0	
22/12/2019 07:30	2.03	0.22	1.81	0	385.5	0.2	
22/12/2019 07:45	2.02	0.22	1.80	0	385.75	0	
22/12/2019 08:00	2.02	0.22	1.80	0	386	0	
22/12/2019 08:15	2.01	0.22	1.79	0	386.25	0	
22/12/2019 08:30	2.01	0.22	1.79	0	386.5	0	
22/12/2019 08:45	2.00	0.22	1.78	0	386.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
22/12/2019 09:00	2.00	0.22	1.78	0	387	0	
22/12/2019 09:15	1.99	0.22	1.77	0.2	387.25	0	
22/12/2019 09:30	1.99	0.22	1.77	0	387.5	0	
22/12/2019 09:45	1.98	0.22	1.76	0	387.75	0	
22/12/2019 10:00	1.97	0.22	1.75	0	388	0	
22/12/2019 10:15	1.96	0.22	1.74	0	388.25	0.2	
22/12/2019 10:30	1.95	0.22	1.73	0	388.5	0	
22/12/2019 10:45	1.95	0.22	1.73	0	388.75	0	
22/12/2019 11:00	1.94	0.22	1.72	0	389	0	
22/12/2019 11:15	1.93	0.22	1.71	0	389.25	0	
22/12/2019 11:30	1.92	0.22	1.70	0	389.5	0	
22/12/2019 11:45	1.90	0.22	1.68	0	389.75	0	
22/12/2019 12:00	1.89	0.22	1.67	0	390	0	
22/12/2019 12:15	1.88	0.22	1.66	0.2	390.25	0	
22/12/2019 12:30	1.87	0.22	1.65	0	390.5	0	
22/12/2019 12:45	1.85	0.22	1.63	0	390.75	0	
22/12/2019 13:00	1.84	0.22	1.62	0	391	0	
22/12/2019 13:15	1.82	0.22	1.60	0	391.25	0.2	
22/12/2019 13:30	1.82	0.22	1.60	0	391.5	0	
22/12/2019 13:45	1.80	0.22	1.58	0	391.75	0	
22/12/2019 14:00	1.78	0.22	1.56	0	392	0	
22/12/2019 14:15	1.76	0.22	1.54	0	392.25	0	
22/12/2019 14:30	1.76	0.22	1.54	0	392.5	0	
22/12/2019 14:45	1.74	0.22	1.52	0	392.75	0	
22/12/2019 15:00	1.72	0.22	1.50	0	393	0	
22/12/2019 15:15	1.71	0.22	1.49	0	393.25	0	
22/12/2019 15:30	1.69	0.22	1.47	0	393.5	0	
22/12/2019 15:45	1.67	0.22	1.45	0	393.75	0	
22/12/2019 16:00	1.66	0.22	1.44	0	394	0	
22/12/2019 16:15	1.64	0.22	1.42	0	394.25	0	
22/12/2019 16:30	1.63	0.22	1.41	0	394.5	0	
22/12/2019 16:45	1.62	0.22	1.40	0	394.75	0	
22/12/2019 17:00	1.60	0.22	1.38	0	395	0	
22/12/2019 17:15	1.58	0.22	1.36	0	395.25	0	
22/12/2019 17:30	1.57	0.22	1.35	0	395.5	0	
22/12/2019 17:45	1.55	0.22	1.33	0	395.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
22/12/2019 18:00	1.54	0.22	1.32	0	396	0	
22/12/2019 18:15	1.52	0.22	1.30	0	396.25	0	
22/12/2019 18:30	1.51	0.22	1.29	0	396.5	0	
22/12/2019 18:45	1.50	0.22	1.28	0	396.75	0	
22/12/2019 19:00	1.48	0.22	1.26	0	397	0	
22/12/2019 19:15	1.47	0.22	1.25	0	397.25	0	
22/12/2019 19:30	1.46	0.22	1.24	0	397.5	0	
22/12/2019 19:45	1.45	0.22	1.23	0	397.75	0	
22/12/2019 20:00	1.44	0.22	1.22	0	398	0	
22/12/2019 20:15	1.43	0.22	1.21	0	398.25	0	
22/12/2019 20:30	1.42	0.22	1.20	0	398.5	0	
22/12/2019 20:45	1.41	0.22	1.19	0	398.75	0	
22/12/2019 21:00	1.40	0.22	1.18	0	399	0	
22/12/2019 21:15	1.39	0.22	1.17	0	399.25	0	
22/12/2019 21:30	1.38	0.22	1.16	0	399.5	0	
22/12/2019 21:45	1.37	0.22	1.15	0	399.75	0	
22/12/2019 22:00	1.36	0.22	1.14	0	400	0	
22/12/2019 22:15	1.35	0.22	1.13	0	400.25	0	
22/12/2019 22:30	1.35	0.22	1.13	0	400.5	0	
22/12/2019 22:45	1.34	0.22	1.12	0	400.75	0	
22/12/2019 23:00	1.32	0.22	1.10	0	401	0	
22/12/2019 23:15	1.32	0.22	1.10	0	401.25	0	
22/12/2019 23:30	1.31	0.22	1.09	0	401.5	0	
22/12/2019 23:45	1.30	0.22	1.08	0	401.75	0	
23/12/2019 00:00	1.30	0.22	1.08	0	402	0	
23/12/2019 00:15	1.29	0.22	1.07	0	402.25	0	
23/12/2019 00:30	1.28	0.22	1.06	0	402.5	0	
23/12/2019 00:45	1.27	0.22	1.05	0	402.75	0	
23/12/2019 01:00	1.27	0.22	1.05	0	403	0	
23/12/2019 01:15	1.26	0.22	1.04	0	403.25	0	
23/12/2019 01:30	1.25	0.22	1.03	0	403.5	0	
23/12/2019 01:45	1.24	0.22	1.02	0	403.75	0	
23/12/2019 02:00	1.24	0.22	1.02	0	404	0	
23/12/2019 02:15	1.23	0.22	1.01	0	404.25	0	
23/12/2019 02:30	1.22	0.22	1.00	0	404.5	0	
23/12/2019 02:45	1.22	0.22	1.00	0	404.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
23/12/2019 03:00	1.21	0.22	0.99	0	405	0	
23/12/2019 03:15	1.20	0.22	0.98	0	405.25	0	
23/12/2019 03:30	1.20	0.22	0.98	0	405.5	0	
23/12/2019 03:45	1.19	0.22	0.97	0	405.75	0	
23/12/2019 04:00	1.18	0.22	0.96	0	406	0	
23/12/2019 04:15	1.17	0.22	0.95	0	406.25	0	
23/12/2019 04:30	1.17	0.22	0.95	0	406.5	0	
23/12/2019 04:45	1.16	0.22	0.94	0	406.75	0	
23/12/2019 05:00	1.15	0.22	0.93	0	407	0	
23/12/2019 05:15	1.15	0.22	0.93	0	407.25	0	
23/12/2019 05:30	1.14	0.22	0.92	0	407.5	0	
23/12/2019 05:45	1.13	0.22	0.91	0	407.75	0	
23/12/2019 06:00	1.13	0.22	0.91	0	408	0	
23/12/2019 06:15	1.12	0.22	0.90	0	408.25	0	
23/12/2019 06:30	1.11	0.22	0.89	0	408.5	0	
23/12/2019 06:45	1.11	0.22	0.89	0	408.75	0	
23/12/2019 07:00	1.10	0.22	0.88	0	409	0	
23/12/2019 07:15	1.09	0.22	0.87	0	409.25	0	
23/12/2019 07:30	1.07	0.22	0.85	0	409.5	0	
23/12/2019 07:45	1.06	0.22	0.84	0	409.75	0	
23/12/2019 08:00	1.05	0.22	0.83	0	410	0	
23/12/2019 08:15	1.04	0.22	0.82	0	410.25	0	
23/12/2019 08:30	1.03	0.22	0.81	0	410.5	0	
23/12/2019 08:45	1.03	0.22	0.81	0	410.75	0	
23/12/2019 09:00	1.01	0.22	0.79	0	411	0	
23/12/2019 09:15	1.00	0.22	0.78	0	411.25	0	
23/12/2019 09:30	0.99	0.22	0.77	0	411.5	0	
23/12/2019 09:45	0.98	0.22	0.76	0	411.75	0	
23/12/2019 10:00	0.97	0.22	0.75	0	412	0	
23/12/2019 10:15	0.96	0.22	0.74	0	412.25	0	
23/12/2019 10:30	0.94	0.22	0.72	0	412.5	0	
23/12/2019 10:45	0.93	0.22	0.71	0	412.75	0	
23/12/2019 11:00	0.92	0.22	0.70	0	413	0	
23/12/2019 11:15	0.92	0.22	0.70	0	413.25	0	
23/12/2019 11:30	0.91	0.22	0.69	0	413.5	0	
23/12/2019 11:45	0.90	0.22	0.68	0	413.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
23/12/2019 12:00	0.89	0.22	0.67	0	414	0	
23/12/2019 12:15	0.88	0.22	0.66	0	414.25	0	
23/12/2019 12:30	0.87	0.22	0.65	0	414.5	0	
23/12/2019 12:45	0.87	0.22	0.65	0	414.75	0	
23/12/2019 13:00	0.86	0.22	0.64	0	415	0	
23/12/2019 13:15	0.85	0.22	0.63	0	415.25	0	
23/12/2019 13:30	0.84	0.22	0.62	0	415.5	0	
23/12/2019 13:45	0.82	0.22	0.60	0.2	415.75	0	
23/12/2019 14:00	0.82	0.22	0.60	0	416	0	
23/12/2019 14:15	0.81	0.22	0.59	0	416.25	0	
23/12/2019 14:30	0.80	0.22	0.58	0	416.5	0	
23/12/2019 14:45	0.80	0.22	0.58	0	416.75	0	
23/12/2019 15:00	0.79	0.22	0.57	0	417	0	
23/12/2019 15:15	0.78	0.22	0.56	0	417.25	0	
23/12/2019 15:30	0.77	0.22	0.55	0	417.5	0	
23/12/2019 15:45	0.76	0.22	0.54	0	417.75	0	
23/12/2019 16:00	0.76	0.22	0.54	0	418	0	
23/12/2019 16:15	0.76	0.22	0.54	0	418.25	0	
23/12/2019 16:30	0.75	0.22	0.53	0	418.5	0	
23/12/2019 16:45	0.74	0.22	0.52	0	418.75	0	
23/12/2019 17:00	0.73	0.22	0.51	0	419	0	
23/12/2019 17:15	0.73	0.22	0.51	0	419.25	0	
23/12/2019 17:30	0.72	0.22	0.50	0	419.5	0	
23/12/2019 17:45	0.72	0.22	0.50	0	419.75	0	
23/12/2019 18:00	0.71	0.22	0.49	0	420	0	
23/12/2019 18:15	0.70	0.22	0.48	0	420.25	0	
23/12/2019 18:30	0.70	0.22	0.48	0	420.5	0	
23/12/2019 18:45	0.69	0.22	0.47	0	420.75	0	
23/12/2019 19:00	0.69	0.22	0.47	0	421	0	
23/12/2019 19:15	0.68	0.22	0.46	0	421.25	0	
23/12/2019 19:30	0.67	0.22	0.45	0	421.5	0	
23/12/2019 19:45	0.67	0.22	0.45	0	421.75	0	
23/12/2019 20:00	0.66	0.22	0.44	0	422	0	
23/12/2019 20:15	0.66	0.22	0.44	0	422.25	0	
23/12/2019 20:30	0.65	0.22	0.43	0	422.5	0	
23/12/2019 20:45	0.65	0.22	0.43	0	422.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
23/12/2019 21:00	0.65	0.22	0.43	0	423	0	
23/12/2019 21:15	0.64	0.22	0.42	0	423.25	0	
23/12/2019 21:30	0.64	0.22	0.42	0	423.5	0	
23/12/2019 21:45	0.63	0.22	0.41	0	423.75	0	
23/12/2019 22:00	0.62	0.22	0.40	0	424	0	
23/12/2019 22:15	0.62	0.22	0.40	0	424.25	0	
23/12/2019 22:30	0.61	0.22	0.39	0	424.5	0	
23/12/2019 22:45	0.60	0.22	0.38	0	424.75	0	
23/12/2019 23:00	0.60	0.22	0.38	0	425	0	
23/12/2019 23:15	0.60	0.22	0.38	0	425.25	0	
23/12/2019 23:30	0.60	0.22	0.38	0	425.5	0	
23/12/2019 23:45	0.60	0.22	0.38	0	425.75	0	
24/12/2019 00:00	0.59	0.22	0.37	0	426	0	
24/12/2019 00:15	0.59	0.22	0.37	0	426.25	0	
24/12/2019 00:30	0.58	0.22	0.36	0	426.5	0	
24/12/2019 00:45	0.58	0.22	0.36	0	426.75	0	
24/12/2019 01:00	0.57	0.22	0.35	0	427	0	
24/12/2019 01:15	0.57	0.22	0.35	0	427.25	0	
24/12/2019 01:30	0.57	0.22	0.35	0	427.5	0	
24/12/2019 01:45	0.56	0.22	0.34	0	427.75	0	
24/12/2019 02:00	0.56	0.22	0.34	0	428	0	
24/12/2019 02:15	0.56	0.22	0.34	0	428.25	0	
24/12/2019 02:30	0.56	0.22	0.34	0	428.5	0	
24/12/2019 02:45	0.56	0.22	0.34	0	428.75	0	
24/12/2019 03:00	0.55	0.22	0.33	0	429	0	
24/12/2019 03:15	0.55	0.22	0.33	0	429.25	0	
24/12/2019 03:30	0.54	0.22	0.32	0	429.5	0.2	
24/12/2019 03:45	0.54	0.22	0.32	0	429.75	0	
24/12/2019 04:00	0.54	0.22	0.32	0	430	0	
24/12/2019 04:15	0.53	0.22	0.31	0	430.25	0	
24/12/2019 04:30	0.53	0.22	0.31	0	430.5	0	
24/12/2019 04:45	0.53	0.22	0.31	0.8	430.75	0.6	
24/12/2019 05:00	0.53	0.22	0.31	0.4	431	0.8	
24/12/2019 05:15	0.53	0.22	0.31	0.4	431.25	0.2	
24/12/2019 05:30	0.53	0.22	0.31	0	431.5	0.2	
24/12/2019 05:45	0.53	0.22	0.31	0.2	431.75	0.2	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
24/12/2019 06:00	0.53	0.22	0.31	0.4	432	0.2	
24/12/2019 06:15	0.53	0.22	0.31	0	432.25	0	
24/12/2019 06:30	0.52	0.22	0.30	0	432.5	0	
24/12/2019 06:45	0.52	0.22	0.30	0	432.75	0	
24/12/2019 07:00	0.52	0.22	0.30	0	433	0	
24/12/2019 07:15	0.52	0.22	0.30	0	433.25	0.2	
24/12/2019 07:30	0.52	0.22	0.30	0	433.5	0	
24/12/2019 07:45	0.52	0.22	0.30	0.2	433.75	0	
24/12/2019 08:00	0.52	0.22	0.30	0	434	0	
24/12/2019 08:15	0.52	0.22	0.30	0	434.25	0	
24/12/2019 08:30	0.52	0.22	0.30	0	434.5	0	
24/12/2019 08:45	0.53	0.22	0.31	0	434.75	0	
24/12/2019 09:00	0.53	0.22	0.31	0	435	0	
24/12/2019 09:15	0.53	0.22	0.31	0	435.25	0	
24/12/2019 09:30	0.53	0.22	0.31	0	435.5	0	
24/12/2019 09:45	0.53	0.22	0.31	0	435.75	0	
24/12/2019 10:00	0.53	0.22	0.31	0	436	0	
24/12/2019 10:15	0.53	0.22	0.31	0	436.25	0	
24/12/2019 10:30	0.53	0.22	0.31	0	436.5	0	
24/12/2019 10:45	0.53	0.22	0.31	0	436.75	0	
24/12/2019 11:00	0.54	0.22	0.32	0	437	0	
24/12/2019 11:15	0.54	0.22	0.32	0	437.25	0	
24/12/2019 11:30	0.54	0.22	0.32	0	437.5	0	
24/12/2019 11:45	0.55	0.22	0.33	0	437.75	0	
24/12/2019 12:00	0.55	0.22	0.33	0	438	0	
24/12/2019 12:15	0.56	0.22	0.34	0	438.25	0	
24/12/2019 12:30	0.56	0.22	0.34	0	438.5	0	
24/12/2019 12:45	0.56	0.22	0.34	0	438.75	0	
24/12/2019 13:00	0.57	0.22	0.35	0	439	0	
24/12/2019 13:15	0.57	0.22	0.35	0	439.25	0	
24/12/2019 13:30	0.58	0.22	0.36	0	439.5	0	
24/12/2019 13:45	0.59	0.22	0.37	0	439.75	0	
24/12/2019 14:00	0.59	0.22	0.37	0	440	0	
24/12/2019 14:15	0.60	0.22	0.38	0	440.25	0	
24/12/2019 14:30	0.60	0.22	0.38	0	440.5	0	
24/12/2019 14:45	0.60	0.22	0.38	0	440.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
24/12/2019 15:00	0.60	0.22	0.38	0	441	0	
24/12/2019 15:15	0.61	0.22	0.39	0	441.25	0	
24/12/2019 15:30	0.61	0.22	0.39	0	441.5	0	
24/12/2019 15:45	0.62	0.22	0.40	0	441.75	0	
24/12/2019 16:00	0.62	0.22	0.40	0	442	0	
24/12/2019 16:15	0.62	0.22	0.40	0	442.25	0	
24/12/2019 16:30	0.63	0.22	0.41	0	442.5	0	
24/12/2019 16:45	0.63	0.22	0.41	0	442.75	0	
24/12/2019 17:00	0.63	0.22	0.41	0	443	0	
24/12/2019 17:15	0.63	0.22	0.41	0	443.25	0	
24/12/2019 17:30	0.63	0.22	0.41	0	443.5	0	
24/12/2019 17:45	0.63	0.22	0.41	0	443.75	0	
24/12/2019 18:00	0.64	0.22	0.42	0	444	0	
24/12/2019 18:15	0.64	0.22	0.42	0	444.25	0	
24/12/2019 18:30	0.64	0.22	0.42	0	444.5	0	
24/12/2019 18:45	0.64	0.22	0.42	0	444.75	0	
24/12/2019 19:00	0.64	0.22	0.42	0	445	0	
24/12/2019 19:15	0.64	0.22	0.42	0	445.25	0	
24/12/2019 19:30	0.63	0.22	0.41	0	445.5	0	
24/12/2019 19:45	0.63	0.22	0.41	0	445.75	0	
24/12/2019 20:00	0.63	0.22	0.41	0	446	0	
24/12/2019 20:15	0.63	0.22	0.41	0	446.25	0	
24/12/2019 20:30	0.63	0.22	0.41	0	446.5	0	
24/12/2019 20:45	0.63	0.22	0.41	0	446.75	0	
24/12/2019 21:00	0.63	0.22	0.41	0	447	0	
24/12/2019 21:15	0.63	0.22	0.41	0	447.25	0	
24/12/2019 21:30	0.62	0.22	0.40	0	447.5	0	
24/12/2019 21:45	0.62	0.22	0.40	0	447.75	0	
24/12/2019 22:00	0.62	0.22	0.40	0	448	0	
24/12/2019 22:15	0.62	0.22	0.40	0	448.25	0	
24/12/2019 22:30	0.62	0.22	0.40	0	448.5	0	
24/12/2019 22:45	0.62	0.22	0.40	0	448.75	0	
24/12/2019 23:00	0.61	0.22	0.39	0	449	0	
24/12/2019 23:15	0.61	0.22	0.39	0	449.25	0	
24/12/2019 23:30	0.61	0.22	0.39	0	449.5	0	
24/12/2019 23:45	0.61	0.22	0.39	0	449.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
25/12/2019 00:00	0.61	0.22	0.39	0	450	0	
25/12/2019 00:15	0.60	0.22	0.38	0	450.25	0	
25/12/2019 00:30	0.60	0.22	0.38	0	450.5	0	
25/12/2019 00:45	0.60	0.22	0.38	0	450.75	0	
25/12/2019 01:00	0.60	0.22	0.38	0	451	0	
25/12/2019 01:15	0.60	0.22	0.38	0	451.25	0	
25/12/2019 01:30	0.60	0.22	0.38	0	451.5	0	
25/12/2019 01:45	0.59	0.22	0.37	0	451.75	0	
25/12/2019 02:00	0.59	0.22	0.37	0	452	0	
25/12/2019 02:15	0.59	0.22	0.37	0	452.25	0	
25/12/2019 02:30	0.59	0.22	0.37	0	452.5	0	
25/12/2019 02:45	0.58	0.22	0.36	0	452.75	0	
25/12/2019 03:00	0.58	0.22	0.36	0	453	0	
25/12/2019 03:15	0.57	0.22	0.35	0	453.25	0	
25/12/2019 03:30	0.57	0.22	0.35	0	453.5	0	
25/12/2019 03:45	0.57	0.22	0.35	0	453.75	0	
25/12/2019 04:00	0.56	0.22	0.34	0	454	0	
25/12/2019 04:15	0.56	0.22	0.34	0	454.25	0	
25/12/2019 04:30	0.56	0.22	0.34	0	454.5	0	
25/12/2019 04:45	0.56	0.22	0.34	0	454.75	0	
25/12/2019 05:00	0.56	0.22	0.34	0	455	0	
25/12/2019 05:15	0.56	0.22	0.34	0	455.25	0	
25/12/2019 05:30	0.55	0.22	0.33	0	455.5	0	
25/12/2019 05:45	0.55	0.22	0.33	0	455.75	0	
25/12/2019 06:00	0.54	0.22	0.32	0	456	0	
25/12/2019 06:15	0.54	0.22	0.32	0	456.25	0	
25/12/2019 06:30	0.54	0.22	0.32	0	456.5	0	
25/12/2019 06:45	0.53	0.22	0.31	0	456.75	0	
25/12/2019 07:00	0.53	0.22	0.31	0	457	0	
25/12/2019 07:15	0.53	0.22	0.31	0	457.25	0	
25/12/2019 07:30	0.53	0.22	0.31	0	457.5	0	
25/12/2019 07:45	0.52	0.22	0.30	0	457.75	0	
25/12/2019 08:00	0.52	0.22	0.30	0	458	0	
25/12/2019 08:15	0.51	0.22	0.29	0	458.25	0	
25/12/2019 08:30	0.51	0.22	0.29	0	458.5	0	
25/12/2019 08:45	0.50	0.22	0.28	0	458.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
25/12/2019 09:00	0.50	0.22	0.28	0	459	0	
25/12/2019 09:15	0.50	0.22	0.28	0	459.25	0	
25/12/2019 09:30	0.50	0.22	0.28	0	459.5	0	
25/12/2019 09:45	0.49	0.22	0.27	0	459.75	0	
25/12/2019 10:00	0.49	0.22	0.27	0	460	0	
25/12/2019 10:15	0.49	0.22	0.27	0	460.25	0	
25/12/2019 10:30	0.48	0.22	0.26	0	460.5	0	
25/12/2019 10:45	0.48	0.22	0.26	0	460.75	0	
25/12/2019 11:00	0.48	0.22	0.26	0	461	0	
25/12/2019 11:15	0.48	0.22	0.26	0	461.25	0	
25/12/2019 11:30	0.48	0.22	0.26	0	461.5	0	
25/12/2019 11:45	0.47	0.22	0.25	0	461.75	0	
25/12/2019 12:00	0.47	0.22	0.25	0	462	0	
25/12/2019 12:15	0.46	0.22	0.24	0	462.25	0	
25/12/2019 12:30	0.46	0.22	0.24	0	462.5	0	
25/12/2019 12:45	0.46	0.22	0.24	0	462.75	0	
25/12/2019 13:00	0.46	0.22	0.24	0	463	0	
25/12/2019 13:15	0.46	0.22	0.24	0	463.25	0	
25/12/2019 13:30	0.46	0.22	0.24	0	463.5	0	
25/12/2019 13:45	0.45	0.22	0.23	0	463.75	0	
25/12/2019 14:00	0.45	0.22	0.23	0	464	0	
25/12/2019 14:15	0.44	0.22	0.22	0	464.25	0	
25/12/2019 14:30	0.44	0.22	0.22	0	464.5	0	
25/12/2019 14:45	0.44	0.22	0.22	0	464.75	0	
25/12/2019 15:00	0.44	0.22	0.22	0	465	0	
25/12/2019 15:15	0.44	0.22	0.22	0	465.25	0	
25/12/2019 15:30	0.44	0.22	0.22	0	465.5	0	
25/12/2019 15:45	0.43	0.22	0.21	0	465.75	0	
25/12/2019 16:00	0.43	0.22	0.21	0	466	0	
25/12/2019 16:15	0.43	0.22	0.21	0	466.25	0	
25/12/2019 16:30	0.42	0.22	0.20	0	466.5	0	
25/12/2019 16:45	0.42	0.22	0.20	0	466.75	0	
25/12/2019 17:00	0.42	0.22	0.20	0	467	0	
25/12/2019 17:15	0.42	0.22	0.20	0	467.25	0	
25/12/2019 17:30	0.42	0.22	0.20	0	467.5	0	
25/12/2019 17:45	0.41	0.22	0.19	0	467.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
25/12/2019 18:00	0.41	0.22	0.19	0	468	0	
25/12/2019 18:15	0.40	0.22	0.18	0	468.25	0	
25/12/2019 18:30	0.40	0.22	0.18	0	468.5	0	
25/12/2019 18:45	0.40	0.22	0.18	0	468.75	0	
25/12/2019 19:00	0.40	0.22	0.18	0	469	0	
25/12/2019 19:15	0.40	0.22	0.18	0	469.25	0	
25/12/2019 19:30	0.40	0.22	0.18	0	469.5	0	
25/12/2019 19:45	0.40	0.22	0.18	0	469.75	0	
25/12/2019 20:00	0.39	0.22	0.17	0	470	0	
25/12/2019 20:15	0.39	0.22	0.17	0	470.25	0	
25/12/2019 20:30	0.39	0.22	0.17	0	470.5	0	
25/12/2019 20:45	0.39	0.22	0.17	0	470.75	0	
25/12/2019 21:00	0.39	0.22	0.17	0	471	0	
25/12/2019 21:15	0.39	0.22	0.17	0	471.25	0	
25/12/2019 21:30	0.39	0.22	0.17	0	471.5	0	
25/12/2019 21:45	0.38	0.22	0.16	0	471.75	0	
25/12/2019 22:00	0.38	0.22	0.16	0	472	0	
25/12/2019 22:15	0.38	0.22	0.16	0	472.25	0	
25/12/2019 22:30	0.38	0.22	0.16	0	472.5	0	
25/12/2019 22:45	0.37	0.22	0.15	0	472.75	0	
25/12/2019 23:00	0.37	0.22	0.15	0	473	0	
25/12/2019 23:15	0.37	0.22	0.15	0	473.25	0	
25/12/2019 23:30	0.37	0.22	0.15	0	473.5	0	
25/12/2019 23:45	0.37	0.22	0.15	0	473.75	0	
26/12/2019 00:00	0.37	0.22	0.15	0	474	0	
26/12/2019 00:15	0.37	0.22	0.15	0	474.25	0	
26/12/2019 00:30	0.37	0.22	0.15	0	474.5	0	
26/12/2019 00:45	0.37	0.22	0.15	0	474.75	0	
26/12/2019 01:00	0.36	0.22	0.14	0	475	0	
26/12/2019 01:15	0.36	0.22	0.14	0	475.25	0	
26/12/2019 01:30	0.36	0.22	0.14	0	475.5	0	
26/12/2019 01:45	0.36	0.22	0.14	0	475.75	0	
26/12/2019 02:00	0.36	0.22	0.14	0	476	0	
26/12/2019 02:15	0.36	0.22	0.14	0	476.25	0	
26/12/2019 02:30	0.36	0.22	0.14	0	476.5	0	
26/12/2019 02:45	0.36	0.22	0.14	0	476.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
26/12/2019 03:00	0.35	0.22	0.13	0	477	0	
26/12/2019 03:15	0.35	0.22	0.13	0	477.25	0	
26/12/2019 03:30	0.35	0.22	0.13	0	477.5	0	
26/12/2019 03:45	0.35	0.22	0.13	0	477.75	0	
26/12/2019 04:00	0.35	0.22	0.13	0	478	0	
26/12/2019 04:15	0.35	0.22	0.13	0	478.25	0	
26/12/2019 04:30	0.35	0.22	0.13	0	478.5	0	
26/12/2019 04:45	0.35	0.22	0.13	0	478.75	0	
26/12/2019 05:00	0.35	0.22	0.13	0	479	0	
26/12/2019 05:15	0.35	0.22	0.13	0	479.25	0	
26/12/2019 05:30	0.35	0.22	0.13	0	479.5	0	
26/12/2019 05:45	0.34	0.22	0.12	0	479.75	0	
26/12/2019 06:00	0.34	0.22	0.12	0	480	0	
26/12/2019 06:15	0.34	0.22	0.12	0	480.25	0	
26/12/2019 06:30	0.34	0.22	0.12	0	480.5	0	
26/12/2019 06:45	0.34	0.22	0.12	0	480.75	0	
26/12/2019 07:00	0.34	0.22	0.12	0	481	0	
26/12/2019 07:15	0.34	0.22	0.12	0	481.25	0	
26/12/2019 07:30	0.34	0.22	0.12	0	481.5	0	
26/12/2019 07:45	0.34	0.22	0.12	0	481.75	0	
26/12/2019 08:00	0.34	0.22	0.12	0	482	0	
26/12/2019 08:15	0.34	0.22	0.12	0	482.25	0	
26/12/2019 08:30	0.34	0.22	0.12	0	482.5	0	
26/12/2019 08:45	0.34	0.22	0.12	0	482.75	0	
26/12/2019 09:00	0.34	0.22	0.12	0	483	0	
26/12/2019 09:15	0.33	0.22	0.11	0	483.25	0	
26/12/2019 09:30	0.33	0.22	0.11	0	483.5	0	
26/12/2019 09:45	0.33	0.22	0.11	0	483.75	0	
26/12/2019 10:00	0.33	0.22	0.11	0	484	0	
26/12/2019 10:15	0.33	0.22	0.11	0	484.25	0	
26/12/2019 10:30	0.33	0.22	0.11	0	484.5	0	
26/12/2019 10:45	0.33	0.22	0.11	0	484.75	0	
26/12/2019 11:00	0.33	0.22	0.11	0	485	0	
26/12/2019 11:15	0.33	0.22	0.11	0	485.25	0	
26/12/2019 11:30	0.33	0.22	0.11	0	485.5	0	
26/12/2019 11:45	0.33	0.22	0.11	0.4	485.75	0.4	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
26/12/2019 12:00	0.33	0.22	0.11	0.2	486	0.4	
26/12/2019 12:15	0.33	0.22	0.11	0	486.25	0.2	
26/12/2019 12:30	0.33	0.22	0.11	0	486.5	0	
26/12/2019 12:45	0.33	0.22	0.11	0.6	486.75	0	
26/12/2019 13:00	0.33	0.22	0.11	0.2	487	0.4	
26/12/2019 13:15	0.33	0.22	0.11	0	487.25	0.2	
26/12/2019 13:30	0.33	0.22	0.11	0	487.5	0.2	
26/12/2019 13:45	0.33	0.22	0.11	0	487.75	0	
26/12/2019 14:00	0.33	0.22	0.11	0.2	488	0	
26/12/2019 14:15	0.34	0.22	0.12	0	488.25	0	
26/12/2019 14:30	0.34	0.22	0.12	0.4	488.5	0.2	
26/12/2019 14:45	0.34	0.22	0.12	0.2	488.75	0.2	
26/12/2019 15:00	0.34	0.22	0.12	0.6	489	0.4	
26/12/2019 15:15	0.34	0.22	0.12	0.2	489.25	0.4	
26/12/2019 15:30	0.34	0.22	0.12	0.2	489.5	0.2	
26/12/2019 15:45	0.34	0.22	0.12	0.6	489.75	0.6	
26/12/2019 16:00	0.35	0.22	0.13	0.6	490	0.6	
26/12/2019 16:15	0.35	0.22	0.13	0.4	490.25	0.4	
26/12/2019 16:30	0.35	0.22	0.13	0.4	490.5	0.4	
26/12/2019 16:45	0.36	0.22	0.14	0.2	490.75	0.2	
26/12/2019 17:00	0.36	0.22	0.14	0	491	0	
26/12/2019 17:15	0.37	0.22	0.15	0.2	491.25	0	
26/12/2019 17:30	0.37	0.22	0.15	0	491.5	0.2	
26/12/2019 17:45	0.38	0.22	0.16	0	491.75	0	
26/12/2019 18:00	0.39	0.22	0.17	0.2	492	0	
26/12/2019 18:15	0.40	0.22	0.18	0	492.25	0	
26/12/2019 18:30	0.40	0.22	0.18	0	492.5	0	
26/12/2019 18:45	0.42	0.22	0.20	0	492.75	0	
26/12/2019 19:00	0.44	0.22	0.22	0	493	0	
26/12/2019 19:15	0.46	0.22	0.24	0	493.25	0	
26/12/2019 19:30	0.48	0.22	0.26	0	493.5	0	
26/12/2019 19:45	0.51	0.22	0.29	0	493.75	0	
26/12/2019 20:00	0.54	0.22	0.32	0	494	0	
26/12/2019 20:15	0.58	0.22	0.36	0	494.25	0	
26/12/2019 20:30	0.64	0.22	0.42	0	494.5	0	
26/12/2019 20:45	0.68	0.22	0.46	0	494.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
26/12/2019 21:00	0.74	0.22	0.52	0	495	0.2	
26/12/2019 21:15	0.79	0.22	0.57	0	495.25	0	
26/12/2019 21:30	0.86	0.22	0.64	0	495.5	0	
26/12/2019 21:45	0.92	0.22	0.70	0	495.75	0	
26/12/2019 22:00	0.99	0.22	0.77	0	496	0	
26/12/2019 22:15	1.06	0.22	0.84	0.2	496.25	0	
26/12/2019 22:30	1.11	0.22	0.89	0	496.5	0	
26/12/2019 22:45	1.15	0.22	0.93	0.2	496.75	0.4	
26/12/2019 23:00	1.18	0.22	0.96	0	497	0	
26/12/2019 23:15	1.22	0.22	1.00	0	497.25	0.2	
26/12/2019 23:30	1.25	0.22	1.03	0	497.5	0	
26/12/2019 23:45	1.30	0.22	1.08	0	497.75	0	
27/12/2019 00:00	1.32	0.22	1.10	0	498	0	
27/12/2019 00:15	1.36	0.22	1.14	0	498.25	0	
27/12/2019 00:30	1.40	0.22	1.18	0	498.5	0	
27/12/2019 00:45	1.43	0.22	1.21	0	498.75	0	
27/12/2019 01:00	1.46	0.22	1.24	0	499	0	
27/12/2019 01:15	1.49	0.22	1.27	0	499.25	0	
27/12/2019 01:30	1.53	0.22	1.31	0	499.5	0	
27/12/2019 01:45	1.56	0.22	1.34	0	499.75	0	
27/12/2019 02:00	1.59	0.22	1.37	0	500	0	
27/12/2019 02:15	1.63	0.22	1.41	0	500.25	0	
27/12/2019 02:30	1.67	0.22	1.45	0	500.5	0	
27/12/2019 02:45	1.71	0.22	1.49	0	500.75	0	
27/12/2019 03:00	1.76	0.22	1.54	0	501	0	
27/12/2019 03:15	1.79	0.22	1.57	0	501.25	0	
27/12/2019 03:30	1.83	0.22	1.61	0	501.5	0	
27/12/2019 03:45	1.88	0.22	1.66	0	501.75	0	
27/12/2019 04:00	1.91	0.22	1.69	0	502	0	
27/12/2019 04:15	1.94	0.22	1.72	0	502.25	0	
27/12/2019 04:30	1.96	0.22	1.74	0	502.5	0	
27/12/2019 04:45	1.99	0.22	1.77	0	502.75	0	
27/12/2019 05:00	2.01	0.22	1.79	0	503	0	
27/12/2019 05:15	2.03	0.22	1.81	0	503.25	0	
27/12/2019 05:30	2.03	0.22	1.81	0	503.5	0	
27/12/2019 05:45	2.04	0.22	1.82	0	503.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
27/12/2019 06:00	2.04	0.22	1.82	0	504	0	
27/12/2019 06:15	2.04	0.22	1.82	0	504.25	0	
27/12/2019 06:30	2.03	0.22	1.81	0	504.5	0	
27/12/2019 06:45	2.01	0.22	1.79	0	504.75	0	
27/12/2019 07:00	2.00	0.22	1.78	0	505	0	
27/12/2019 07:15	1.97	0.22	1.75	0	505.25	0	
27/12/2019 07:30	1.95	0.22	1.73	0	505.5	0	
27/12/2019 07:45	1.94	0.22	1.72	0	505.75	0	
27/12/2019 08:00	1.90	0.22	1.68	0	506	0	
27/12/2019 08:15	1.88	0.22	1.66	0	506.25	0	
27/12/2019 08:30	1.85	0.22	1.63	0	506.5	0	
27/12/2019 08:45	1.82	0.22	1.60	0	506.75	0	
27/12/2019 09:00	1.78	0.22	1.56	0	507	0	
27/12/2019 09:15	1.75	0.22	1.53	0	507.25	0	
27/12/2019 09:30	1.72	0.22	1.50	0	507.5	0	
27/12/2019 09:45	1.69	0.22	1.47	0	507.75	0	
27/12/2019 10:00	1.66	0.22	1.44	0	508	0	
27/12/2019 10:15	1.63	0.22	1.41	0	508.25	0	
27/12/2019 10:30	1.60	0.22	1.38	0	508.5	0	
27/12/2019 10:45	1.58	0.22	1.36	0	508.75	0	
27/12/2019 11:00	1.55	0.22	1.33	0	509	0	
27/12/2019 11:15	1.54	0.22	1.32	0	509.25	0	
27/12/2019 11:30	1.52	0.22	1.30	0	509.5	0	
27/12/2019 11:45	1.50	0.22	1.28	0	509.75	0	
27/12/2019 12:00	1.48	0.22	1.26	0	510	0	
27/12/2019 12:15	1.47	0.22	1.25	0	510.25	0	
27/12/2019 12:30	1.45	0.22	1.23	0	510.5	0	
27/12/2019 12:45	1.44	0.22	1.22	0	510.75	0	
27/12/2019 13:00	1.42	0.22	1.20	0	511	0	
27/12/2019 13:15	1.41	0.22	1.19	0	511.25	0	
27/12/2019 13:30	1.40	0.22	1.18	0	511.5	0	
27/12/2019 13:45	1.38	0.22	1.16	0	511.75	0	
27/12/2019 14:00	1.37	0.22	1.15	0	512	0	
27/12/2019 14:15	1.36	0.22	1.14	0	512.25	0	
27/12/2019 14:30	1.35	0.22	1.13	0	512.5	0	
27/12/2019 14:45	1.34	0.22	1.12	0	512.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
27/12/2019 15:00	1.32	0.22	1.10	0	513	0	
27/12/2019 15:15	1.32	0.22	1.10	0	513.25	0	
27/12/2019 15:30	1.31	0.22	1.09	0	513.5	0	
27/12/2019 15:45	1.30	0.22	1.08	0	513.75	0	
27/12/2019 16:00	1.29	0.22	1.07	0	514	0	
27/12/2019 16:15	1.27	0.22	1.05	0	514.25	0	
27/12/2019 16:30	1.27	0.22	1.05	0	514.5	0	
27/12/2019 16:45	1.26	0.22	1.04	0	514.75	0	
27/12/2019 17:00	1.25	0.22	1.03	0	515	0	
27/12/2019 17:15	1.24	0.22	1.02	0	515.25	0	
27/12/2019 17:30	1.23	0.22	1.01	0	515.5	0	
27/12/2019 17:45	1.22	0.22	1.00	0	515.75	0	
27/12/2019 18:00	1.21	0.22	0.99	0	516	0	
27/12/2019 18:15	1.20	0.22	0.98	0	516.25	0	
27/12/2019 18:30	1.20	0.22	0.98	0	516.5	0	
27/12/2019 18:45	1.18	0.22	0.96	0	516.75	0	
27/12/2019 19:00	1.17	0.22	0.95	0	517	0	
27/12/2019 19:15	1.17	0.22	0.95	0	517.25	0	
27/12/2019 19:30	1.16	0.22	0.94	0	517.5	0	
27/12/2019 19:45	1.15	0.22	0.93	0	517.75	0	
27/12/2019 20:00	1.14	0.22	0.92	0	518	0	
27/12/2019 20:15	1.13	0.22	0.91	0	518.25	0	
27/12/2019 20:30	1.13	0.22	0.91	0	518.5	0	
27/12/2019 20:45	1.12	0.22	0.90	0	518.75	0	
27/12/2019 21:00	1.11	0.22	0.89	0	519	0	
27/12/2019 21:15	1.11	0.22	0.89	0	519.25	0	
27/12/2019 21:30	1.10	0.22	0.88	0	519.5	0	
27/12/2019 21:45	1.09	0.22	0.87	0	519.75	0	
27/12/2019 22:00	1.07	0.22	0.85	0	520	0	
27/12/2019 22:15	1.06	0.22	0.84	0	520.25	0	
27/12/2019 22:30	1.05	0.22	0.83	0	520.5	0	
27/12/2019 22:45	1.04	0.22	0.82	0	520.75	0	
27/12/2019 23:00	1.03	0.22	0.81	0	521	0	
27/12/2019 23:15	1.01	0.22	0.79	0	521.25	0	
27/12/2019 23:30	1.00	0.22	0.78	0	521.5	0	
27/12/2019 23:45	0.99	0.22	0.77	0	521.75	0	

		Middleton		Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
28/12/2019 00:00	0.98	0.22	0.76	0	522	0	
28/12/2019 00:15	0.97	0.22	0.75	0	522.25	0	
28/12/2019 00:30	0.96	0.22	0.74	0	522.5	0	
28/12/2019 00:45	0.94	0.22	0.72	0	522.75	0	
28/12/2019 01:00	0.93	0.22	0.71	0	523	0	
28/12/2019 01:15	0.92	0.22	0.70	0	523.25	0	
28/12/2019 01:30	0.91	0.22	0.69	0	523.5	0	
28/12/2019 01:45	0.91	0.22	0.69	0	523.75	0	
28/12/2019 02:00	0.90	0.22	0.68	0	524	0	
28/12/2019 02:15	0.89	0.22	0.67	0	524.25	0	
28/12/2019 02:30	0.88	0.22	0.66	0	524.5	0	
28/12/2019 02:45	0.87	0.22	0.65	0	524.75	0	
28/12/2019 03:00	0.86	0.22	0.64	0	525	0	
28/12/2019 03:15	0.86	0.22	0.64	0	525.25	0	
28/12/2019 03:30	0.85	0.22	0.63	0	525.5	0	
28/12/2019 03:45	0.84	0.22	0.62	0	525.75	0	
28/12/2019 04:00	0.82	0.22	0.60	0	526	0	
28/12/2019 04:15	0.81	0.22	0.59	0	526.25	0	
28/12/2019 04:30	0.81	0.22	0.59	0	526.5	0	
28/12/2019 04:45	0.80	0.22	0.58	0	526.75	0	
28/12/2019 05:00	0.79	0.22	0.57	0	527	0	
28/12/2019 05:15	0.78	0.22	0.56	0	527.25	0	
28/12/2019 05:30	0.78	0.22	0.56	0	527.5	0	
28/12/2019 05:45	0.77	0.22	0.55	0	527.75	0	
28/12/2019 06:00	0.76	0.22	0.54	0	528	0	
28/12/2019 06:15	0.76	0.22	0.54	0	528.25	0	
28/12/2019 06:30	0.76	0.22	0.54	0	528.5	0	
28/12/2019 06:45	0.75	0.22	0.53	0	528.75	0	
28/12/2019 07:00	0.74	0.22	0.52	0	529	0	
28/12/2019 07:15	0.74	0.22	0.52	0	529.25	0	
28/12/2019 07:30	0.73	0.22	0.51	0	529.5	0	
28/12/2019 07:45	0.72	0.22	0.50	0	529.75	0	
28/12/2019 08:00	0.72	0.22	0.50	0	530	0	
28/12/2019 08:15	0.71	0.22	0.49	0	530.25	0	
28/12/2019 08:30	0.71	0.22	0.49	0	530.5	0	
28/12/2019 08:45	0.70	0.22	0.48	0	530.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
28/12/2019 09:00	0.69	0.22	0.47	0	531	0	
28/12/2019 09:15	0.69	0.22	0.47	0	531.25	0	
28/12/2019 09:30	0.68	0.22	0.46	0	531.5	0	
28/12/2019 09:45	0.67	0.22	0.45	0	531.75	0	
28/12/2019 10:00	0.67	0.22	0.45	0	532	0	
28/12/2019 10:15	0.66	0.22	0.44	0	532.25	0	
28/12/2019 10:30	0.66	0.22	0.44	0	532.5	0	
28/12/2019 10:45	0.65	0.22	0.43	0	532.75	0	
28/12/2019 11:00	0.65	0.22	0.43	0	533	0	
28/12/2019 11:15	0.65	0.22	0.43	0	533.25	0	
28/12/2019 11:30	0.65	0.22	0.43	0	533.5	0	
28/12/2019 11:45	0.64	0.22	0.42	0	533.75	0	
28/12/2019 12:00	0.63	0.22	0.41	0	534	0	
28/12/2019 12:15	0.63	0.22	0.41	0	534.25	0	
28/12/2019 12:30	0.62	0.22	0.40	0	534.5	0	
28/12/2019 12:45	0.62	0.22	0.40	0	534.75	0	
28/12/2019 13:00	0.61	0.22	0.39	0	535	0	
28/12/2019 13:15	0.61	0.22	0.39	0	535.25	0	
28/12/2019 13:30	0.60	0.22	0.38	0	535.5	0	
28/12/2019 13:45	0.60	0.22	0.38	0	535.75	0	
28/12/2019 14:00	0.60	0.22	0.38	0	536	0	
28/12/2019 14:15	0.60	0.22	0.38	0	536.25	0	
28/12/2019 14:30	0.59	0.22	0.37	0	536.5	0	
28/12/2019 14:45	0.59	0.22	0.37	0	536.75	0	
28/12/2019 15:00	0.58	0.22	0.36	0	537	0	
28/12/2019 15:15	0.58	0.22	0.36	0	537.25	0	
28/12/2019 15:30	0.57	0.22	0.35	0	537.5	0	
28/12/2019 15:45	0.57	0.22	0.35	0	537.75	0	
28/12/2019 16:00	0.57	0.22	0.35	0	538	0	
28/12/2019 16:15	0.56	0.22	0.34	0	538.25	0	
28/12/2019 16:30	0.56	0.22	0.34	0	538.5	0	
28/12/2019 16:45	0.56	0.22	0.34	0	538.75	0	
28/12/2019 17:00	0.56	0.22	0.34	0	539	0	
28/12/2019 17:15	0.55	0.22	0.33	0	539.25	0	
28/12/2019 17:30	0.55	0.22	0.33	0	539.5	0	
28/12/2019 17:45	0.54	0.22	0.32	0	539.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
28/12/2019 18:00	0.54	0.22	0.32	0	540	0	
28/12/2019 18:15	0.54	0.22	0.32	0	540.25	0	
28/12/2019 18:30	0.53	0.22	0.31	0	540.5	0	
28/12/2019 18:45	0.53	0.22	0.31	0	540.75	0	
28/12/2019 19:00	0.53	0.22	0.31	0	541	0	
28/12/2019 19:15	0.53	0.22	0.31	0	541.25	0	
28/12/2019 19:30	0.53	0.22	0.31	0	541.5	0	
28/12/2019 19:45	0.52	0.22	0.30	0	541.75	0	
28/12/2019 20:00	0.52	0.22	0.30	0	542	0	
28/12/2019 20:15	0.52	0.22	0.30	0	542.25	0	
28/12/2019 20:30	0.51	0.22	0.29	0	542.5	0	
28/12/2019 20:45	0.51	0.22	0.29	0	542.75	0	
28/12/2019 21:00	0.51	0.22	0.29	0	543	0	
28/12/2019 21:15	0.50	0.22	0.28	0	543.25	0	
28/12/2019 21:30	0.50	0.22	0.28	0	543.5	0	
28/12/2019 21:45	0.50	0.22	0.28	0	543.75	0	
28/12/2019 22:00	0.50	0.22	0.28	0	544	0	
28/12/2019 22:15	0.50	0.22	0.28	0	544.25	0	
28/12/2019 22:30	0.50	0.22	0.28	0	544.5	0	
28/12/2019 22:45	0.49	0.22	0.27	0	544.75	0	
28/12/2019 23:00	0.49	0.22	0.27	0	545	0	
28/12/2019 23:15	0.49	0.22	0.27	0	545.25	0	
28/12/2019 23:30	0.48	0.22	0.26	0	545.5	0	
28/12/2019 23:45	0.48	0.22	0.26	0	545.75	0	
29/12/2019 00:00	0.48	0.22	0.26	0	546	0	
29/12/2019 00:15	0.48	0.22	0.26	0	546.25	0	
29/12/2019 00:30	0.48	0.22	0.26	0	546.5	0	
29/12/2019 00:45	0.48	0.22	0.26	0	546.75	0	
29/12/2019 01:00	0.47	0.22	0.25	0	547	0	
29/12/2019 01:15	0.47	0.22	0.25	0	547.25	0	
29/12/2019 01:30	0.47	0.22	0.25	0	547.5	0	
29/12/2019 01:45	0.47	0.22	0.25	0	547.75	0	
29/12/2019 02:00	0.46	0.22	0.24	0	548	0	
29/12/2019 02:15	0.46	0.22	0.24	0	548.25	0	
29/12/2019 02:30	0.46	0.22	0.24	0	548.5	0	
29/12/2019 02:45	0.46	0.22	0.24	0	548.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
29/12/2019 03:00	0.46	0.22	0.24	0	549	0	
29/12/2019 03:15	0.46	0.22	0.24	0	549.25	0	
29/12/2019 03:30	0.46	0.22	0.24	0	549.5	0	
29/12/2019 03:45	0.45	0.22	0.23	0	549.75	0	
29/12/2019 04:00	0.45	0.22	0.23	0	550	0	
29/12/2019 04:15	0.45	0.22	0.23	0	550.25	0	
29/12/2019 04:30	0.44	0.22	0.22	0	550.5	0	
29/12/2019 04:45	0.44	0.22	0.22	0	550.75	0	
29/12/2019 05:00	0.44	0.22	0.22	0	551	0	
29/12/2019 05:15	0.44	0.22	0.22	0	551.25	0	
29/12/2019 05:30	0.44	0.22	0.22	0	551.5	0	
29/12/2019 05:45	0.44	0.22	0.22	0	551.75	0	
29/12/2019 06:00	0.43	0.22	0.21	0	552	0	
29/12/2019 06:15	0.43	0.22	0.21	0	552.25	0	
29/12/2019 06:30	0.43	0.22	0.21	0	552.5	0	
29/12/2019 06:45	0.43	0.22	0.21	0	552.75	0	
29/12/2019 07:00	0.42	0.22	0.20	0	553	0	
29/12/2019 07:15	0.42	0.22	0.20	0	553.25	0	
29/12/2019 07:30	0.42	0.22	0.20	0	553.5	0	
29/12/2019 07:45	0.42	0.22	0.20	0	553.75	0	
29/12/2019 08:00	0.42	0.22	0.20	0	554	0	
29/12/2019 08:15	0.42	0.22	0.20	0	554.25	0	
29/12/2019 08:30	0.42	0.22	0.20	0	554.5	0	
29/12/2019 08:45	0.42	0.22	0.20	0	554.75	0	
29/12/2019 09:00	0.41	0.22	0.19	0	555	0	
29/12/2019 09:15	0.41	0.22	0.19	0	555.25	0	
29/12/2019 09:30	0.41	0.22	0.19	0	555.5	0	
29/12/2019 09:45	0.41	0.22	0.19	0	555.75	0	
29/12/2019 10:00	0.41	0.22	0.19	0	556	0	
29/12/2019 10:15	0.40	0.22	0.18	0	556.25	0	
29/12/2019 10:30	0.40	0.22	0.18	0	556.5	0	
29/12/2019 10:45	0.40	0.22	0.18	0	556.75	0	
29/12/2019 11:00	0.40	0.22	0.18	0	557	0	
29/12/2019 11:15	0.40	0.22	0.18	0	557.25	0	
29/12/2019 11:30	0.40	0.22	0.18	0	557.5	0	
29/12/2019 11:45	0.40	0.22	0.18	0	557.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
29/12/2019 12:00	0.40	0.22	0.18	0	558	0	
29/12/2019 12:15	0.40	0.22	0.18	0	558.25	0	
29/12/2019 12:30	0.39	0.22	0.17	0	558.5	0	
29/12/2019 12:45	0.39	0.22	0.17	0	558.75	0	
29/12/2019 13:00	0.39	0.22	0.17	0	559	0	
29/12/2019 13:15	0.39	0.22	0.17	0	559.25	0	
29/12/2019 13:30	0.39	0.22	0.17	0	559.5	0	
29/12/2019 13:45	0.39	0.22	0.17	0	559.75	0	
29/12/2019 14:00	0.39	0.22	0.17	0	560	0	
29/12/2019 14:15	0.39	0.22	0.17	0	560.25	0	
29/12/2019 14:30	0.39	0.22	0.17	0	560.5	0	
29/12/2019 14:45	0.39	0.22	0.17	0	560.75	0	
29/12/2019 15:00	0.39	0.22	0.17	0	561	0	
29/12/2019 15:15	0.38	0.22	0.16	0	561.25	0	
29/12/2019 15:30	0.38	0.22	0.16	0	561.5	0	
29/12/2019 15:45	0.38	0.22	0.16	0	561.75	0	
29/12/2019 16:00	0.38	0.22	0.16	0	562	0	
29/12/2019 16:15	0.38	0.22	0.16	0	562.25	0	
29/12/2019 16:30	0.37	0.22	0.15	0	562.5	0	
29/12/2019 16:45	0.37	0.22	0.15	0	562.75	0	
29/12/2019 17:00	0.37	0.22	0.15	0	563	0	
29/12/2019 17:15	0.37	0.22	0.15	0	563.25	0	
29/12/2019 17:30	0.37	0.22	0.15	0	563.5	0	
29/12/2019 17:45	0.37	0.22	0.15	0	563.75	0	
29/12/2019 18:00	0.37	0.22	0.15	0	564	0	
29/12/2019 18:15	0.37	0.22	0.15	0	564.25	0	
29/12/2019 18:30	0.37	0.22	0.15	0	564.5	0	
29/12/2019 18:45	0.36	0.22	0.14	0	564.75	0	
29/12/2019 19:00	0.36	0.22	0.14	0	565	0	
29/12/2019 19:15	0.36	0.22	0.14	0	565.25	0	
29/12/2019 19:30	0.36	0.22	0.14	0	565.5	0	
29/12/2019 19:45	0.36	0.22	0.14	0	565.75	0	
29/12/2019 20:00	0.36	0.22	0.14	0	566	0	
29/12/2019 20:15	0.36	0.22	0.14	0	566.25	0	
29/12/2019 20:30	0.36	0.22	0.14	0	566.5	0	
29/12/2019 20:45	0.36	0.22	0.14	0	566.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
29/12/2019 21:00	0.36	0.22	0.14	0	567	0	
29/12/2019 21:15	0.35	0.22	0.13	0	567.25	0	
29/12/2019 21:30	0.35	0.22	0.13	0	567.5	0	
29/12/2019 21:45	0.35	0.22	0.13	0	567.75	0	
29/12/2019 22:00	0.35	0.22	0.13	0	568	0	
29/12/2019 22:15	0.35	0.22	0.13	0	568.25	0	
29/12/2019 22:30	0.35	0.22	0.13	0	568.5	0	
29/12/2019 22:45	0.35	0.22	0.13	0	568.75	0	
29/12/2019 23:00	0.35	0.22	0.13	0	569	0	
29/12/2019 23:15	0.35	0.22	0.13	0	569.25	0	
29/12/2019 23:30	0.35	0.22	0.13	0	569.5	0	
29/12/2019 23:45	0.35	0.22	0.13	0	569.75	0	
30/12/2019 00:00	0.35	0.22	0.13	0	570	0	
30/12/2019 00:15	0.35	0.22	0.13	0	570.25	0	
30/12/2019 00:30	0.34	0.22	0.12	0	570.5	0	
30/12/2019 00:45	0.34	0.22	0.12	0	570.75	0	
30/12/2019 01:00	0.34	0.22	0.12	0	571	0	
30/12/2019 01:15	0.34	0.22	0.12	0	571.25	0	
30/12/2019 01:30	0.34	0.22	0.12	0	571.5	0	
30/12/2019 01:45	0.34	0.22	0.12	0	571.75	0	
30/12/2019 02:00	0.34	0.22	0.12	0	572	0	
30/12/2019 02:15	0.34	0.22	0.12	0	572.25	0	
30/12/2019 02:30	0.34	0.22	0.12	0	572.5	0	
30/12/2019 02:45	0.34	0.22	0.12	0	572.75	0	
30/12/2019 03:00	0.34	0.22	0.12	0	573	0	
30/12/2019 03:15	0.33	0.22	0.11	0	573.25	0	
30/12/2019 03:30	0.33	0.22	0.11	0	573.5	0	
30/12/2019 03:45	0.33	0.22	0.11	0	573.75	0	
30/12/2019 04:00	0.33	0.22	0.11	0	574	0	
30/12/2019 04:15	0.33	0.22	0.11	0	574.25	0	
30/12/2019 04:30	0.32	0.22	0.10	0	574.5	0	
30/12/2019 04:45	0.32	0.22	0.10	0	574.75	0	
30/12/2019 05:00	0.32	0.22	0.10	0	575	0	
30/12/2019 05:15	0.32	0.22	0.10	0	575.25	0	
30/12/2019 05:30	0.32	0.22	0.10	0	575.5	0	
30/12/2019 05:45	0.32	0.22	0.10	0	575.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
30/12/2019 06:00	0.32	0.22	0.10	0	576	0	
30/12/2019 06:15	0.32	0.22	0.10	0	576.25	0	
30/12/2019 06:30	0.32	0.22	0.10	0	576.5	0	
30/12/2019 06:45	0.32	0.22	0.10	0	576.75	0	
30/12/2019 07:00	0.32	0.22	0.10	0	577	0	
30/12/2019 07:15	0.31	0.22	0.09	0	577.25	0	
30/12/2019 07:30	0.31	0.22	0.09	0	577.5	0	
30/12/2019 07:45	0.31	0.22	0.09	0	577.75	0	
30/12/2019 08:00	0.31	0.22	0.09	0	578	0	
30/12/2019 08:15	0.31	0.22	0.09	0	578.25	0	
30/12/2019 08:30	0.31	0.22	0.09	0	578.5	0	
30/12/2019 08:45	0.31	0.22	0.09	0	578.75	0	
30/12/2019 09:00	0.31	0.22	0.09	0	579	0	
30/12/2019 09:15	0.31	0.22	0.09	0	579.25	0	
30/12/2019 09:30	0.31	0.22	0.09	0	579.5	0	
30/12/2019 09:45	0.31	0.22	0.09	0	579.75	0	
30/12/2019 10:00	0.31	0.22	0.09	0	580	0	
30/12/2019 10:15	0.30	0.22	0.08	0	580.25	0	
30/12/2019 10:30	0.30	0.22	0.08	0	580.5	0	
30/12/2019 10:45	0.30	0.22	0.08	0	580.75	0	
30/12/2019 11:00	0.30	0.22	0.08	0	581	0	
30/12/2019 11:15	0.30	0.22	0.08	0	581.25	0	
30/12/2019 11:30	0.30	0.22	0.08	0	581.5	0	
30/12/2019 11:45	0.30	0.22	0.08	0	581.75	0	
30/12/2019 12:00	0.30	0.22	0.08	0	582	0	
30/12/2019 12:15	0.30	0.22	0.08	0	582.25	0	
30/12/2019 12:30	0.30	0.22	0.08	0	582.5	0	
30/12/2019 12:45	0.30	0.22	0.08	0	582.75	0	
30/12/2019 13:00	0.30	0.22	0.08	0	583	0	
30/12/2019 13:15	0.30	0.22	0.08	0	583.25	0	
30/12/2019 13:30	0.30	0.22	0.08	0	583.5	0	
30/12/2019 13:45	0.30	0.22	0.08	0	583.75	0	
30/12/2019 14:00	0.30	0.22	0.08	0	584	0	
30/12/2019 14:15	0.30	0.22	0.08	0	584.25	0	
30/12/2019 14:30	0.30	0.22	0.08	0	584.5	0	
30/12/2019 14:45	0.30	0.22	0.08	0	584.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
30/12/2019 15:00	0.29	0.22	0.07	0	585	0	
30/12/2019 15:15	0.29	0.22	0.07	0	585.25	0	
30/12/2019 15:30	0.29	0.22	0.07	0	585.5	0	
30/12/2019 15:45	0.29	0.22	0.07	0	585.75	0	
30/12/2019 16:00	0.29	0.22	0.07	0	586	0	
30/12/2019 16:15	0.29	0.22	0.07	0	586.25	0	
30/12/2019 16:30	0.29	0.22	0.07	0	586.5	0	
30/12/2019 16:45	0.29	0.22	0.07	0	586.75	0	
30/12/2019 17:00	0.29	0.22	0.07	0	587	0	
30/12/2019 17:15	0.29	0.22	0.07	0	587.25	0	
30/12/2019 17:30	0.29	0.22	0.07	0	587.5	0	
30/12/2019 17:45	0.29	0.22	0.07	0	587.75	0	
30/12/2019 18:00	0.29	0.22	0.07	0	588	0	
30/12/2019 18:15	0.29	0.22	0.07	0	588.25	0	
30/12/2019 18:30	0.29	0.22	0.07	0	588.5	0	
30/12/2019 18:45	0.29	0.22	0.07	0	588.75	0	
30/12/2019 19:00	0.29	0.22	0.07	0	589	0	
30/12/2019 19:15	0.29	0.22	0.07	0	589.25	0	
30/12/2019 19:30	0.29	0.22	0.07	0	589.5	0	
30/12/2019 19:45	0.29	0.22	0.07	0	589.75	0	
30/12/2019 20:00	0.29	0.22	0.07	0	590	0	
30/12/2019 20:15	0.29	0.22	0.07	0	590.25	0	
30/12/2019 20:30	0.28	0.22	0.06	0	590.5	0	
30/12/2019 20:45	0.28	0.22	0.06	0	590.75	0	
30/12/2019 21:00	0.28	0.22	0.06	0	591	0	
30/12/2019 21:15	0.28	0.22	0.06	0	591.25	0	
30/12/2019 21:30	0.28	0.22	0.06	0	591.5	0	
30/12/2019 21:45	0.28	0.22	0.06	0	591.75	0	
30/12/2019 22:00	0.28	0.22	0.06	0	592	0	
30/12/2019 22:15	0.28	0.22	0.06	0	592.25	0	
30/12/2019 22:30	0.28	0.22	0.06	0	592.5	0	
30/12/2019 22:45	0.28	0.22	0.06	0	592.75	0	
30/12/2019 23:00	0.28	0.22	0.06	0	593	0	
30/12/2019 23:15	0.28	0.22	0.06	0	593.25	0	
30/12/2019 23:30	0.28	0.22	0.06	0	593.5	0	
30/12/2019 23:45	0.28	0.22	0.06	0	593.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
31/12/2019 00:00	0.28	0.22	0.06	0	594	0	
31/12/2019 00:15	0.28	0.22	0.06	0	594.25	0	
31/12/2019 00:30	0.28	0.22	0.06	0	594.5	0	
31/12/2019 00:45	0.27	0.22	0.05	0	594.75	0	
31/12/2019 01:00	0.27	0.22	0.05	0	595	0	
31/12/2019 01:15	0.27	0.22	0.05	0	595.25	0	
31/12/2019 01:30	0.27	0.22	0.05	0	595.5	0	
31/12/2019 01:45	0.27	0.22	0.05	0	595.75	0	
31/12/2019 02:00	0.27	0.22	0.05	0	596	0	
31/12/2019 02:15	0.27	0.22	0.05	0	596.25	0	
31/12/2019 02:30	0.27	0.22	0.05	0	596.5	0	
31/12/2019 02:45	0.27	0.22	0.05	0	596.75	0	
31/12/2019 03:00	0.27	0.22	0.05	0	597	0	
31/12/2019 03:15	0.26	0.22	0.04	0	597.25	0	
31/12/2019 03:30	0.26	0.22	0.04	0	597.5	0	
31/12/2019 03:45	0.26	0.22	0.04	0	597.75	0	
31/12/2019 04:00	0.26	0.22	0.04	0	598	0	
31/12/2019 04:15	0.26	0.22	0.04	0	598.25	0	
31/12/2019 04:30	0.26	0.22	0.04	0	598.5	0	
31/12/2019 04:45	0.26	0.22	0.04	0	598.75	0	
31/12/2019 05:00	0.26	0.22	0.04	0	599	0	
31/12/2019 05:15	0.26	0.22	0.04	0	599.25	0	
31/12/2019 05:30	0.26	0.22	0.04	0	599.5	0	
31/12/2019 05:45	0.26	0.22	0.04	0	599.75	0	
31/12/2019 06:00	0.25	0.22	0.03	0	600	0	
31/12/2019 06:15	0.25	0.22	0.03	0	600.25	0	
31/12/2019 06:30	0.25	0.22	0.03	0	600.5	0	
31/12/2019 06:45	0.25	0.22	0.03	0	600.75	0	
31/12/2019 07:00	0.25	0.22	0.03	0	601	0	
31/12/2019 07:15	0.25	0.22	0.03	0	601.25	0	
31/12/2019 07:30	0.25	0.22	0.03	0	601.5	0	
31/12/2019 07:45	0.25	0.22	0.03	0	601.75	0	
31/12/2019 08:00	0.25	0.22	0.03	0	602	0	
31/12/2019 08:15	0.25	0.22	0.03	0	602.25	0	
31/12/2019 08:30	0.24	0.22	0.02	0	602.5	0	
31/12/2019 08:45	0.24	0.22	0.02	0	602.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
31/12/2019 09:00	0.24	0.22	0.02	0	603	0	
31/12/2019 09:15	0.24	0.22	0.02	0	603.25	0	
31/12/2019 09:30	0.24	0.22	0.02	0	603.5	0	
31/12/2019 09:45	0.24	0.22	0.02	0	603.75	0	
31/12/2019 10:00	0.24	0.22	0.02	0	604	0	
31/12/2019 10:15	0.24	0.22	0.02	0	604.25	0	
31/12/2019 10:30	0.24	0.22	0.02	0	604.5	0	
31/12/2019 10:45	0.24	0.22	0.02	0	604.75	0	
31/12/2019 11:00	0.24	0.22	0.02	0	605	0	
31/12/2019 11:15	0.24	0.22	0.02	0	605.25	0	
31/12/2019 11:30	0.24	0.22	0.02	0	605.5	0	
31/12/2019 11:45	0.24	0.22	0.02	0	605.75	0	
31/12/2019 12:00	0.24	0.22	0.02	0	606	0	
31/12/2019 12:15	0.24	0.22	0.02	0	606.25	0	
31/12/2019 12:30	0.24	0.22	0.02	0	606.5	0	
31/12/2019 12:45	0.24	0.22	0.02	0	606.75	0	
31/12/2019 13:00	0.24	0.22	0.02	0	607	0	
31/12/2019 13:15	0.23	0.22	0.01	0	607.25	0	
31/12/2019 13:30	0.23	0.22	0.01	0	607.5	0	
31/12/2019 13:45	0.23	0.22	0.01	0	607.75	0	
31/12/2019 14:00	0.23	0.22	0.01	0	608	0	
31/12/2019 14:15	0.23	0.22	0.01	0	608.25	0	
31/12/2019 14:30	0.23	0.22	0.01	0	608.5	0	
31/12/2019 14:45	0.23	0.22	0.01	0	608.75	0	
31/12/2019 15:00	0.23	0.22	0.01	0	609	0	
31/12/2019 15:15	0.23	0.22	0.01	0	609.25	0	
31/12/2019 15:30	0.23	0.22	0.01	0	609.5	0	
31/12/2019 15:45	0.23	0.22	0.01	0	609.75	0	
31/12/2019 16:00	0.23	0.22	0.01	0	610	0	
31/12/2019 16:15	0.23	0.22	0.01	0	610.25	0	
31/12/2019 16:30	0.23	0.22	0.01	0	610.5	0	
31/12/2019 16:45	0.23	0.22	0.01	0	610.75	0	
31/12/2019 17:00	0.23	0.22	0.01	0	611	0	
31/12/2019 17:15	0.23	0.22	0.01	0	611.25	0	
31/12/2019 17:30	0.22	0.22	0.00	0	611.5	0	
31/12/2019 17:45	0.22	0.22	0.00	0	611.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
31/12/2019 18:00	0.22	0.22	0.00	0	612	0	
31/12/2019 18:15	0.22	0.22	0.00	0	612.25	0	
31/12/2019 18:30	0.22	0.22	0.00	0	612.5	0	
31/12/2019 18:45	0.22	0.22	0.00	0	612.75	0	
31/12/2019 19:00	0.22	0.22	0.00	0	613	0	
31/12/2019 19:15	0.22	0.22	0.00	0	613.25	0	
31/12/2019 19:30	0.22	0.22	0.00	0	613.5	0	
31/12/2019 19:45	0.22	0.22	0.00	0	613.75	0	
31/12/2019 20:00	0.22	0.22	0.00	0	614	0	
31/12/2019 20:15	0.22	0.22	0.00	0	614.25	0	
31/12/2019 20:30	0.22	0.22	0.00	0	614.5	0	
31/12/2019 20:45	0.22	0.22	0.00	0	614.75	0	
31/12/2019 21:00	0.22	0.22	0.00	0	615	0	
31/12/2019 21:15	0.22	0.22	0.00	0	615.25	0	
31/12/2019 21:30	0.22	0.22	0.00	0	615.5	0	
31/12/2019 21:45	0.22	0.22	0.00	0	615.75	0	
31/12/2019 22:00	0.22	0.22	0.00	0	616	0	
31/12/2019 22:15	0.22	0.22	0.00	0	616.25	0	
31/12/2019 22:30	0.22	0.22	0.00	0	616.5	0	
31/12/2019 22:45	0.22	0.22	0.00	0	616.75	0	
31/12/2019 23:00	0.22	0.22	0.00	0	617	0	
31/12/2019 23:15	0.22	0.22	0.00	0	617.25	0	
31/12/2019 23:30	0.22	0.22	0.00	0	617.5	0	
31/12/2019 23:45	0.22	0.22	0.00	0	617.75	0	
01/01/2020 00:00	0.22	0.22	0.00	0	618	0	
01/01/2020 00:15	0.22	0.22	0.00	0	618.25	0	
01/01/2020 00:30	0.22	0.22	0.00	0	618.5	0	
01/01/2020 00:45	0.22	0.22	0.00	0	618.75	0	
01/01/2020 01:00	0.22	0.22	0.00	0	619	0	
01/01/2020 01:15	0.22	0.22	0.00	0	619.25	0	
01/01/2020 01:30	0.22	0.22	0.00	0	619.5	0	
01/01/2020 01:45	0.22	0.22	0.00	0	619.75	0	
01/01/2020 02:00	0.22	0.22	0.00	0	620	0	
01/01/2020 02:15	0.22	0.22	0.00	0	620.25	0	
01/01/2020 02:30	0.22	0.22	0.00	0	620.5	0	
01/01/2020 02:45	0.22	0.22	0.00	0	620.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
01/01/2020 03:00	0.21	0.21	0.00	0	621	0	
01/01/2020 03:15	0.21	0.21	0.00	0	621.25	0	
01/01/2020 03:30	0.21	0.21	0.00	0	621.5	0	
01/01/2020 03:45	0.21	0.21	0.00	0	621.75	0	
01/01/2020 04:00	0.21	0.21	0.00	0	622	0	
01/01/2020 04:15	0.21	0.21	0.00	0	622.25	0	
01/01/2020 04:30	0.21	0.21	0.00	0	622.5	0	
01/01/2020 04:45	0.21	0.21	0.00	0	622.75	0	
01/01/2020 05:00	0.21	0.21	0.00	0	623	0	
01/01/2020 05:15	0.21	0.21	0.00	0	623.25	0	
01/01/2020 05:30	0.21	0.21	0.00	0	623.5	0	
01/01/2020 05:45	0.21	0.21	0.00	0	623.75	0	
01/01/2020 06:00	0.21	0.21	0.00	0	624	0	
01/01/2020 06:15	0.21	0.21	0.00	0	624.25	0	
01/01/2020 06:30	0.21	0.21	0.00	0	624.5	0	
01/01/2020 06:45	0.21	0.21	0.00	0	624.75	0	
01/01/2020 07:00	0.21	0.21	0.00	0	625	0	
01/01/2020 07:15	0.21	0.21	0.00	0	625.25	0	
01/01/2020 07:30	0.21	0.21	0.00	0	625.5	0	
01/01/2020 07:45	0.21	0.21	0.00	0	625.75	0	
01/01/2020 08:00	0.21	0.21	0.00	0	626	0	
01/01/2020 08:15	0.21	0.21	0.00	0	626.25	0	
01/01/2020 08:30	0.21	0.21	0.00	0	626.5	0	
01/01/2020 08:45	0.21	0.21	0.00	0	626.75	0	
01/01/2020 09:00	0.21	0.21	0.00	0	627	0	
01/01/2020 09:15	0.21	0.21	0.00	0	627.25	0	
01/01/2020 09:30	0.21	0.21	0.00	0	627.5	0	
01/01/2020 09:45	0.21	0.21	0.00	0	627.75	0	
01/01/2020 10:00	0.21	0.21	0.00	0	628	0	
01/01/2020 10:15	0.21	0.21	0.00	0	628.25	0	
01/01/2020 10:30	0.21	0.21	0.00	0	628.5	0	
01/01/2020 10:45	0.21	0.21	0.00	0	628.75	0	
01/01/2020 11:00	0.21	0.21	0.00	0	629	0	
01/01/2020 11:15	0.21	0.21	0.00	0	629.25	0	
01/01/2020 11:30	0.21	0.21	0.00	0	629.5	0	
01/01/2020 11:45	0.21	0.21	0.00	0	629.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
01/01/2020 12:00	0.21	0.21	0.00	0	630	0	
01/01/2020 12:15	0.21	0.21	0.00	0	630.25	0	
01/01/2020 12:30	0.21	0.21	0.00	0	630.5	0	
01/01/2020 12:45	0.21	0.21	0.00	0	630.75	0	
01/01/2020 13:00	0.21	0.21	0.00	0	631	0	
01/01/2020 13:15	0.21	0.21	0.00	0	631.25	0	
01/01/2020 13:30	0.21	0.21	0.00	0	631.5	0	
01/01/2020 13:45	0.21	0.21	0.00	0	631.75	0	
01/01/2020 14:00	0.21	0.21	0.00	0	632	0	
01/01/2020 14:15	0.21	0.21	0.00	0	632.25	0	
01/01/2020 14:30	0.21	0.21	0.00	0	632.5	0	
01/01/2020 14:45	0.21	0.21	0.00	0	632.75	0	
01/01/2020 15:00	0.21	0.21	0.00	0	633	0	
01/01/2020 15:15	0.21	0.21	0.00	0	633.25	0	
01/01/2020 15:30	0.21	0.21	0.00	0	633.5	0	
01/01/2020 15:45	0.21	0.21	0.00	0	633.75	0	
01/01/2020 16:00	0.21	0.21	0.00	0	634	0	
01/01/2020 16:15	0.21	0.21	0.00	0	634.25	0	
01/01/2020 16:30	0.21	0.21	0.00	0	634.5	0	
01/01/2020 16:45	0.21	0.21	0.00	0	634.75	0	
01/01/2020 17:00	0.21	0.21	0.00	0	635	0	
01/01/2020 17:15	0.21	0.21	0.00	0	635.25	0	
01/01/2020 17:30	0.21	0.21	0.00	0	635.5	0	
01/01/2020 17:45	0.21	0.21	0.00	0	635.75	0	
01/01/2020 18:00	0.21	0.21	0.00	0	636	0	
01/01/2020 18:15	0.21	0.21	0.00	0	636.25	0	
01/01/2020 18:30	0.21	0.21	0.00	0	636.5	0	
01/01/2020 18:45	0.21	0.21	0.00	0	636.75	0	
01/01/2020 19:00	0.21	0.21	0.00	0	637	0	
01/01/2020 19:15	0.21	0.21	0.00	0	637.25	0	
01/01/2020 19:30	0.21	0.21	0.00	0	637.5	0	
01/01/2020 19:45	0.21	0.21	0.00	0	637.75	0	
01/01/2020 20:00	0.21	0.21	0.00	0	638	0	
01/01/2020 20:15	0.21	0.21	0.00	0	638.25	0	
01/01/2020 20:30	0.21	0.21	0.00	0	638.5	0	
01/01/2020 20:45	0.21	0.21	0.00	0	638.75	0	

	Middleton			Benhall		Thorpeness	
Date & Time	Flow (m^3/s)	Baseflow (m^3/s)	NetFlow (m^3/s)	Rainfall (mm)	Hours	Rainfall (mm)	Benhall
01/01/2020 21:00	0.21	0.21	0.00	0	639	0	
01/01/2020 21:15	0.21	0.21	0.00	0	639.25	0	
01/01/2020 21:30	0.21	0.21	0.00	0	639.5	0	
01/01/2020 21:45	0.21	0.21	0.00	0	639.75	0	
01/01/2020 22:00	0.21	0.21	0.00	0	640	0	
01/01/2020 22:15	0.21	0.21	0.00	0	640.25	0	
01/01/2020 22:30	0.21	0.21	0.00	0	640.5	0	
01/01/2020 22:45	0.21	0.21	0.00	0	640.75	0	
01/01/2020 23:00	0.21	0.21	0.00	0	641	0	
01/01/2020 23:15	0.21	0.21	0.00	0	641.25	0	
01/01/2020 23:30	0.21	0.21	0.00	0	641.5	0	
01/01/2020 23:45	0.21	0.21	0.00	0	641.75	0	
02/01/2020 00:00	0.21	0.21	0.00	0	642	0	
02/01/2020 00:15	0.21	0.21	0.00	0	642.25	0	
02/01/2020 00:30	0.20	0.20	0.00	0	642.5	0	
02/01/2020 00:45	0.20	0.20	0.00	0	642.75	0	

APPENDIX C: STANDARD PERCENTAGE RUNOFF CALCULATION RECORDS

Summary of SPR from Observed Events @ Middleton

Event Date	Peak Flow (m^3s^{-1})	PR	SPR	CWI
Jan-03	14.3	70.0	68.5	131.1
Mar-10	9.0	58.0	56.8	129.8
Jan-16	11.4	73.0	71.8	130.0
Apr-18	9.6	59.0	54.0	128.8
Nov-19	10.5	96.0	95.9	125.7
Mean	10.9	71.2	69.4	129.1

Summary of SPR from Observed Events @ G5

Event Date	Peak Flow (m^3s^{-1})	PR	SPR	CWI
Feb-14	0.8	36.0	35.2	127.7
Jul-14	1.0	13.0	39.2	19.6
Oct-14	1.1	20.0	44.5	26.4
Nov-14	1.6	40.0	52.1	76.3
Nov-14	1.1	40.0	45.8	101.5
Jul-15	1.4	24.0	52.1	8.7
Mean	1.2	28.8	44.8	60.0

Summary of SPR derived @ other sub-catchments

Event Date	SPR
Leis Sizewell	26.8
Leis Lovers	33.6
Leis Abbey	51.4
Leiston	38.2
Leis Upper	31.5
Mins_Eastbridge	24.5
Mins Westleton	40.5
Mins Docwra	26.6
Mins Warkburn	25.9
Mins Scott	25.0
Mins Theberton	54.5
Mins Wash	59.9
Mins Potters	46.8

Mean CWI	60.0
High CWI	127.7
Low CWI	8.7

	Middleton		Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)
21/12/2002 21:15	0.48		0 2	0
21/12/2002 21:30	0.48		0 2	0.25
21/12/2002 21:45	0.48		0	0 5
21/12/2002 22:00	0.48		0	0.75
21/12/2002 22:15	0.48		0 2	1
21/12/2002 22:30	0.48		0 2	1.25
21/12/2002 22:45	0.48		0	1 5
21/12/2002 23:00	0.48		0	1.75
21/12/2002 23:15	0.48		0	2
21/12/2002 23:30	0.48		0 2	2.25
21/12/2002 23:45	0.48		0 2	2 5
22/12/2002 00:00	0.48		0.4	2.75
22/12/2002 00:15	0.48		0 8	3
22/12/2002 00:30	0.49		0.6	3.25
22/12/2002 00:45	0.49		0.6	3 5
22/12/2002 01:00	0.49		0.6	3.75
22/12/2002 01:15	0.49		0.4	4
22/12/2002 01:30	0.49		0.6	4.25
22/12/2002 01:45	0.50		0.6	4 5
22/12/2002 02:00	0.50		0 2	4.75
22/12/2002 02:15	0.51		0	5
22/12/2002 02:30	0.51		0	5.25
22/12/2002 02:45	0.52		0.4	5 5
22/12/2002 03:00	0.53		0.6	5.75
22/12/2002 03:15	0.53		0.6	6
22/12/2002 03:30	0.54		0.6	6.25
22/12/2002 03:45	0.55		0.4	6 5
22/12/2002 04:00	0.57		0.4	6.75
22/12/2002 04:15	0.60		0.4	7
22/12/2002 04:30	0.63		0.4	7.25
22/12/2002 04:45	0.68		0.4	7 5
22/12/2002 05:00	0.75		0 8	7.75
22/12/2002 05:15	0.84		0.6	8
22/12/2002 05:30	0.97		0.4	8.25
22/12/2002 05:45	1.12		0.4	8 5
22/12/2002 06:00	1.30		0.4	8.75
22/12/2002 06:15	1.50		0 8	9
22/12/2002 06:30	1.69		0.4	9.25
22/12/2002 06:45	1.89		0.6	9 5
22/12/2002 07:00	2.09		0 8	9.75
22/12/2002 07:15	2.30		0 8	10
22/12/2002 07:30	2.58		0.4	10.25
22/12/2002 07:45	2.99		0.6	10 5
22/12/2002 08:00	3.42		0 2	10.75
22/12/2002 08:15	3.83		0.4	11
22/12/2002 08:30	4.21		0.6	11.25
22/12/2002 08:45	4.55		0.4	11 5
22/12/2002 09:00	4.81		0.6	11.75
22/12/2002 09:15	5.08		0 2	12
22/12/2002 09:30	5.31		0.4	12.25
22/12/2002 09:45	5.51		0 2	12 5
22/12/2002 10:00	5.69		0.4	12.75

Event 01/01/2003 4th peak		
start of event	37622 22917	
end of event	37622.8125	
duration hours	14	
total RF mm	19.2	
SMD W/E AVERAGE	mm	
W/E 31/12/2002	0	
DATE	API5	Daily Totals
37620	d-1	0.6
37619	d-2	14.6
37618	d-3	1.4
37617	d-4	0
37616	d-5	5 8
		22.4

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)
22/12/2002 10:15	5.85	0	2	13
22/12/2002 10:30	6.00	0		13.25
22/12/2002 10:45	6.15	0		13 5
22/12/2002 11:00	6.35	0		13.75
22/12/2002 11:15	6.49	0		14
22/12/2002 11:30	6.62	0		14.25
22/12/2002 11:45	6.74	0		14 5
22/12/2002 12:00	6.86	0		14.75
22/12/2002 12:15	7.02	0		15
22/12/2002 12:30	7.15	0		15.25
22/12/2002 12:45	7.31	0		15 5
22/12/2002 13:00	7.47	0		15.75
22/12/2002 13:15	7.73	0		16
22/12/2002 13:30	7.94	0		16.25
22/12/2002 13:45	8.24	0		16 5
22/12/2002 14:00	8.54	0		16.75
22/12/2002 14:15	8.88	0		17
22/12/2002 14:30	9.26	0		17.25
22/12/2002 14:45	9.54	0		17 5
22/12/2002 15:00	9.88	0		17.75
22/12/2002 15:15	10.20	0		18
22/12/2002 15:30	10.57	0		18.25
22/12/2002 15:45	10.86	0		18 5
22/12/2002 16:00	11.08	0		18.75
22/12/2002 16:15	11.29	0		19
22/12/2002 16:30	11.55	0		19.25
22/12/2002 16:45	11.74	0		19 5
22/12/2002 17:00	11.86	0		19.75
22/12/2002 17:15	11.97	0		20
22/12/2002 17:30	12.09	0		20.25
22/12/2002 17:45	12.17	0		20 5
22/12/2002 18:00	12.23	0		20.75
22/12/2002 18:15	12.32	0		21
22/12/2002 18:30	12.44	0		21.25
22/12/2002 18:45	12.47	0		21 5
22/12/2002 19:00	12.60	0		21.75
22/12/2002 19:15	12.63	0		22
22/12/2002 19:30	12.72	0		22.25
22/12/2002 19:45	12.72	0		22 5
22/12/2002 20:00	12.82	0		22.75
22/12/2002 20:15	12.85	0		23
22/12/2002 20:30	12.98	0		23.25
22/12/2002 20:45	13.01	0		23 5
22/12/2002 21:00	13.11	0		23.75
22/12/2002 21:15	13.17	0		24
22/12/2002 21:30	13.21	0		24.25
22/12/2002 21:45	13.31	0		24 5
22/12/2002 22:00	13.34	0		24.75
22/12/2002 22:15	13.41	0		25
22/12/2002 22:30	13.38	0		25.25
22/12/2002 22:45	13.38	0		25 5
22/12/2002 23:00	13.51	0		25.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)
22/12/2002 23:15	13.44		0	26
22/12/2002 23:30	13.44		0	26.25
22/12/2002 23:45	13.41		0	26 5
23/12/2002 00:00	13.38		0	26.75
23/12/2002 00:15	13.21		0	27
23/12/2002 00:30	13.24		0	27.25
23/12/2002 00:45	13.14		0	27 5
23/12/2002 01:00	13.08		0	27.75
23/12/2002 01:15	12.91		0	28
23/12/2002 01:30	12.82		0	28.25
23/12/2002 01:45	12.66		0	28 5
23/12/2002 02:00	12.50		0	28.75
23/12/2002 02:15	12.35		0	29
23/12/2002 02:30	12.09		0	29.25
23/12/2002 02:45	11.88		0	29 5
23/12/2002 03:00	11.66		0	29.75
23/12/2002 03:15	11.44		0	30
23/12/2002 03:30	11.18		0	30.25
23/12/2002 03:45	10.90		0	30 5
23/12/2002 04:00	10.64		0	30.75
23/12/2002 04:15	10.32		0	31
23/12/2002 04:30	10.03		0	31.25
23/12/2002 04:45	9.74		0	31 5
23/12/2002 05:00	9.44		0	31.75
23/12/2002 05:15	9.11		0	32
23/12/2002 05:30	8.82		0	32.25
23/12/2002 05:45	8.56		0	32 5
23/12/2002 06:00	8.25		0	32.75
23/12/2002 06:15	7.98		0	33
23/12/2002 06:30	7.71		0	33.25
23/12/2002 06:45	7.47		0	33 5
23/12/2002 07:00	7.22		0	33.75
23/12/2002 07:15	7.00		0	34
23/12/2002 07:30	6.79		0	34.25
23/12/2002 07:45	6.60		0	34 5
23/12/2002 08:00	6.41		0	34.75
23/12/2002 08:15	6.24		0	35
23/12/2002 08:30	6.05		0	35.25
23/12/2002 08:45	5.90		0	35 5
23/12/2002 09:00	5.73		0	35.75
23/12/2002 09:15	5.52		0	36
23/12/2002 09:30	5.35		0	36.25
23/12/2002 09:45	5.14		0	36 5
23/12/2002 10:00	4.93		0	36.75
23/12/2002 10:15	4.71		0	37
23/12/2002 10:30	4.48		0	37.25
23/12/2002 10:45	4.21		0	37 5
23/12/2002 11:00	3.94		0	37.75
23/12/2002 11:15	3.71		0	38
23/12/2002 11:30	3.44		0	38.25
23/12/2002 11:45	3.21		0	38 5
23/12/2002 12:00	2.99		0	38.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)
23/12/2002 12:15	2.80		0	39
23/12/2002 12:30	2.64		0	39.25
23/12/2002 12:45	2.48		0	39 5
23/12/2002 13:00	2.35		0	39.75
23/12/2002 13:15	2.25		0	40
23/12/2002 13:30	2.17		0	40.25
23/12/2002 13:45	2.10		0	40 5
23/12/2002 14:00	2.03		0	40.75
23/12/2002 14:15	1.98		0	41
23/12/2002 14:30	1.93		0	41.25
23/12/2002 14:45	1.88		0	41 5
23/12/2002 15:00	1.85		0	41.75
23/12/2002 15:15	1.81		0	42
23/12/2002 15:30	1.78		0	42.25
23/12/2002 15:45	1.75		0	42 5
23/12/2002 16:00	1.72		0	42.75
23/12/2002 16:15	1.69		0	43
23/12/2002 16:30	1.67		0	43.25
23/12/2002 16:45	1.64		0	43 5
23/12/2002 17:00	1.63		0	43.75
23/12/2002 17:15	1.61		0	44
23/12/2002 17:30	1.59		0	44.25
23/12/2002 17:45	1.57		0	44 5
23/12/2002 18:00	1.56		0	44.75
23/12/2002 18:15	1.53		0	45
23/12/2002 18:30	1.53		0	45.25
23/12/2002 18:45	1.51		0	45 5
23/12/2002 19:00	1.49		0	45.75
23/12/2002 19:15	1.48		0	46
23/12/2002 19:30	1.46		0	46.25
23/12/2002 19:45	1.44		0	46 5
23/12/2002 20:00	1.44		0	46.75
23/12/2002 20:15	1.42		0	47
23/12/2002 20:30	1.40		0	47.25
23/12/2002 20:45	1.39		0	47 5
23/12/2002 21:00	1.39		0	47.75
23/12/2002 21:15	1.37		0	48
23/12/2002 21:30	1.36		0	48.25
23/12/2002 21:45	1.35		0	48 5
23/12/2002 22:00	1.34		0	48.75
23/12/2002 22:15	1.33		0	49
23/12/2002 22:30	1.32		0	49.25
23/12/2002 22:45	1.31		0	49 5
23/12/2002 23:00	1.30		0	49.75
23/12/2002 23:15	1.29		0	50
23/12/2002 23:30	1.28		0	50.25
23/12/2002 23:45	1.28		0 2	50 5
24/12/2002 00:00	1.27		0 2	50.75
24/12/2002 00:15	1.25		0 2	51
24/12/2002 00:30	1.25		0	51.25
24/12/2002 00:45	1.24		0	51 5
24/12/2002 01:00	1.23		0 2	51.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)		Duration (hrs)
24/12/2002 01:15	1.23	0	2		52
24/12/2002 01:30	1.22	0			52.25
24/12/2002 01:45	1.22	0			52 5
24/12/2002 02:00	1.21	0			52.75
24/12/2002 02:15	1.20	0			53
24/12/2002 02:30	1.19	0			53.25
24/12/2002 02:45	1.19	0			53 5
24/12/2002 03:00	1.19	0			53.75
24/12/2002 03:15	1.17	0			54
24/12/2002 03:30	1.17	0			54.25
24/12/2002 03:45	1.16	0			54 5
24/12/2002 04:00	1.16	0			54.75
24/12/2002 04:15	1.15	0			55
24/12/2002 04:30	1.14	0			55.25
24/12/2002 04:45	1.14	0			55 5
24/12/2002 05:00	1.13	0			55.75
24/12/2002 05:15	1.13	0			56
24/12/2002 05:30	1.12	0			56.25
24/12/2002 05:45	1.12	0			56 5
24/12/2002 06:00	1.11	0			56.75
24/12/2002 06:15	1.11	0			57
24/12/2002 06:30	1.10	0			57.25
24/12/2002 06:45	1.09	0			57 5
24/12/2002 07:00	1.09	0			57.75
24/12/2002 07:15	1.08	0			58
24/12/2002 07:30	1.08	0			58.25
24/12/2002 07:45	1.08	0			58 5
24/12/2002 08:00	1.07	0			58.75
24/12/2002 08:15	1.07	0			59
24/12/2002 08:30	1.06	0	2		59.25
24/12/2002 08:45	1.06	0			59 5
24/12/2002 09:00	1.06	0		1.2	59.75
24/12/2002 09:15	1.05	0			60
24/12/2002 09:30	1.05	0			60.25
24/12/2002 09:45	1.05	0			60 5
24/12/2002 10:00	1.04	0			60.75
24/12/2002 10:15	1.03	0			61
24/12/2002 10:30	1.03	0			61.25
24/12/2002 10:45	1.03	0			61 5
24/12/2002 11:00	1.03	0			61.75
24/12/2002 11:15	1.02	0			62
24/12/2002 11:30	1.02	0			62.25
24/12/2002 11:45	1.02	0			62 5
24/12/2002 12:00	1.01	0			62.75
24/12/2002 12:15	1.01	0			63
24/12/2002 12:30	1.01	0			63.25
24/12/2002 12:45	1.01	0			63 5
24/12/2002 13:00	1.01	0			63.75
24/12/2002 13:15	1.00	0			64
24/12/2002 13:30	1.00	0			64.25
24/12/2002 13:45	1.01	0			64 5
24/12/2002 14:00	1.00	0			64.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
24/12/2002 14:15	1.00		0	65
24/12/2002 14:30	1.00		0	65.25
24/12/2002 14:45	1.00		0	65 5
24/12/2002 15:00	1.00		0	65.75
24/12/2002 15:15	1.00		0	66
24/12/2002 15:30	1.00		0	66.25
24/12/2002 15:45	1.00		0	66 5
24/12/2002 16:00	1.00		0	66.75
24/12/2002 16:15	1.00		0	67
24/12/2002 16:30	1.00		0	67.25
24/12/2002 16:45	1.00		0	67 5
24/12/2002 17:00	0.99		0	67.75
24/12/2002 17:15	1.00		0	68
24/12/2002 17:30	1.00		0	68.25
24/12/2002 17:45	0.99		0	68 5
24/12/2002 18:00	0.99		0	68.75
24/12/2002 18:15	0.99		0	69
24/12/2002 18:30	0.99		0	69.25
24/12/2002 18:45	0.99		0	69 5
24/12/2002 19:00	0.99		0	69.75
24/12/2002 19:15	0.99		0	70
24/12/2002 19:30	0.99		0	70.25
24/12/2002 19:45	0.99		0	70 5
24/12/2002 20:00	0.99		0	70.75
24/12/2002 20:15	0.99		0	71
24/12/2002 20:30	0.99		0	71.25
24/12/2002 20:45	0.99		0	71 5
24/12/2002 21:00	0.99		0	71.75
24/12/2002 21:15	0.99		0	72
24/12/2002 21:30	0.98		0	72.25
24/12/2002 21:45	0.98		0	72 5
24/12/2002 22:00	0.98		0	72.75
24/12/2002 22:15	0.98		0	73
24/12/2002 22:30	0.97		0	73.25
24/12/2002 22:45	0.97		0	73 5
24/12/2002 23:00	0.97		0	73.75
24/12/2002 23:15	0.97		0	74
24/12/2002 23:30	0.97		0	74.25
24/12/2002 23:45	0.97		0	74 5
25/12/2002 00:00	0.96		0	74.75
25/12/2002 00:15	0.96		0	75
25/12/2002 00:30	0.96		0	75.25
25/12/2002 00:45	0.95		0	75 5
25/12/2002 01:00	0.95		0	75.75
25/12/2002 01:15	0.95		0	76
25/12/2002 01:30	0.95		0	76.25
25/12/2002 01:45	0.95		0	76 5
25/12/2002 02:00	0.94		0	76.75
25/12/2002 02:15	0.94		0	77
25/12/2002 02:30	0.94		0	77.25
25/12/2002 02:45	0.93		0	77 5
25/12/2002 03:00	0.93		0	77.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)		Duration (hrs)
25/12/2002 03:15	0.93		0		78
25/12/2002 03:30	0.93		0		78.25
25/12/2002 03:45	0.93		0		78 5
25/12/2002 04:00	0.92		0		78.75
25/12/2002 04:15	0.92		0		79
25/12/2002 04:30	0.92		0		79.25
25/12/2002 04:45	0.91		0		79 5
25/12/2002 05:00	0.91		0		79.75
25/12/2002 05:15	0.91		0		80
25/12/2002 05:30	0.91		0		80.25
25/12/2002 05:45	0.91		0 2		80 5
25/12/2002 06:00	0.91		0		80.75
25/12/2002 06:15	0.90		0		81
25/12/2002 06:30	0.90		0		81.25
25/12/2002 06:45	0.89		0		81 5
25/12/2002 07:00	0.89		0		81.75
25/12/2002 07:15	0.89		0		82
25/12/2002 07:30	0.89		0		82.25
25/12/2002 07:45	0.89		0		82 5
25/12/2002 08:00	0.89		0		82.75
25/12/2002 08:15	0.88		0		83
25/12/2002 08:30	0.88		0		83.25
25/12/2002 08:45	0.88		0		83 5
25/12/2002 09:00	0.88		0 2	0.4	83.75
25/12/2002 09:15	0.88		0		84
25/12/2002 09:30	0.88		0		84.25
25/12/2002 09:45	0.88		0		84 5
25/12/2002 10:00	0.88		0 2		84.75
25/12/2002 10:15	0.88		0		85
25/12/2002 10:30	0.88		0		85.25
25/12/2002 10:45	0.88		0		85 5
25/12/2002 11:00	0.88		0		85.75
25/12/2002 11:15	0.88		0		86
25/12/2002 11:30	0.88		0		86.25
25/12/2002 11:45	0.88		0		86 5
25/12/2002 12:00	0.88		0		86.75
25/12/2002 12:15	0.89		0		87
25/12/2002 12:30	0.89		0		87.25
25/12/2002 12:45	0.89		0		87 5
25/12/2002 13:00	0.89		0		87.75
25/12/2002 13:15	0.89		0		88
25/12/2002 13:30	0.90		0		88.25
25/12/2002 13:45	0.90		0		88 5
25/12/2002 14:00	0.91		0		88.75
25/12/2002 14:15	0.92		0		89
25/12/2002 14:30	0.93		0		89.25
25/12/2002 14:45	0.93		0		89 5
25/12/2002 15:00	0.95		0		89.75
25/12/2002 15:15	0.95		0		90
25/12/2002 15:30	0.96		0		90.25
25/12/2002 15:45	0.97		0		90 5
25/12/2002 16:00	0.97		0		90.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
25/12/2002 16:15	0.98		0	91
25/12/2002 16:30	0.99		0	91.25
25/12/2002 16:45	1.00		0	91 5
25/12/2002 17:00	1.01		0	91.75
25/12/2002 17:15	1.01		0	92
25/12/2002 17:30	1.03		0	92.25
25/12/2002 17:45	1.03		0	92 5
25/12/2002 18:00	1.05		0	92.75
25/12/2002 18:15	1.06		0	93
25/12/2002 18:30	1.06		0	93.25
25/12/2002 18:45	1.07		0	93 5
25/12/2002 19:00	1.08		0	93.75
25/12/2002 19:15	1.09		0	94
25/12/2002 19:30	1.09		0	94.25
25/12/2002 19:45	1.10		0	94 5
25/12/2002 20:00	1.11		0	94.75
25/12/2002 20:15	1.11		0	95
25/12/2002 20:30	1.11		0	95.25
25/12/2002 20:45	1.12		0	95 5
25/12/2002 21:00	1.13		0	95.75
25/12/2002 21:15	1.13		0	96
25/12/2002 21:30	1.13		0	96.25
25/12/2002 21:45	1.13		0	96 5
25/12/2002 22:00	1.14		0	96.75
25/12/2002 22:15	1.14		0	97
25/12/2002 22:30	1.14		0	97.25
25/12/2002 22:45	1.15		0	97 5
25/12/2002 23:00	1.15		0	97.75
25/12/2002 23:15	1.15		0	98
25/12/2002 23:30	1.15		0	98.25
25/12/2002 23:45	1.15		0	98 5
26/12/2002 00:00	1.15		0	98.75
26/12/2002 00:15	1.15		0	99
26/12/2002 00:30	1.15		0	99.25
26/12/2002 00:45	1.15		0	99 5
26/12/2002 01:00	1.15		0	99.75
26/12/2002 01:15	1.15		0	100
26/12/2002 01:30	1.15		0	100.25
26/12/2002 01:45	1.14		0	100 5
26/12/2002 02:00	1.14		0	100.75
26/12/2002 02:15	1.14		0	101
26/12/2002 02:30	1.13		0	101.25
26/12/2002 02:45	1.13		0	101 5
26/12/2002 03:00	1.13		0	101.75
26/12/2002 03:15	1.13		0	102
26/12/2002 03:30	1.13		0	102.25
26/12/2002 03:45	1.13		0	102 5
26/12/2002 04:00	1.13		0	102.75
26/12/2002 04:15	1.12		0	103
26/12/2002 04:30	1.12		0	103.25
26/12/2002 04:45	1.11		0	103 5
26/12/2002 05:00	1.11		0	103.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)		Duration (hrs)
26/12/2002 05:15	1.11		0		104
26/12/2002 05:30	1.11		0		104.25
26/12/2002 05:45	1.11		0 2		104 5
26/12/2002 06:00	1.10		0 2		104.75
26/12/2002 06:15	1.11		0		105
26/12/2002 06:30	1.10		0		105.25
26/12/2002 06:45	1.11		1 2		105 5
26/12/2002 07:00	1.13		1 2		105.75
26/12/2002 07:15	1.14		1 2		106
26/12/2002 07:30	1.16		0		106.25
26/12/2002 07:45	1.17		0.4		106 5
26/12/2002 08:00	1.18		0		106.75
26/12/2002 08:15	1.19		0		107
26/12/2002 08:30	1.21		0		107.25
26/12/2002 08:45	1.22		0		107 5
26/12/2002 09:00	1.24		0	4.6	107.75
26/12/2002 09:15	1.28		0		108
26/12/2002 09:30	1.34		0		108.25
26/12/2002 09:45	1.39		0		108 5
26/12/2002 10:00	1.46		0		108.75
26/12/2002 10:15	1.54		0		109
26/12/2002 10:30	1.63		0		109.25
26/12/2002 10:45	1.70		0		109 5
26/12/2002 11:00	1.78		0		109.75
26/12/2002 11:15	1.85		0		110
26/12/2002 11:30	1.92		0		110.25
26/12/2002 11:45	2.00		0		110 5
26/12/2002 12:00	2.05		0		110.75
26/12/2002 12:15	2.12		0		111
26/12/2002 12:30	2.17		0		111.25
26/12/2002 12:45	2.24		0		111 5
26/12/2002 13:00	2.30		0		111.75
26/12/2002 13:15	2.33		0		112
26/12/2002 13:30	2.40		0		112.25
26/12/2002 13:45	2.44		0		112 5
26/12/2002 14:00	2.48		0		112.75
26/12/2002 14:15	2.54		0		113
26/12/2002 14:30	2.60		0		113.25
26/12/2002 14:45	2.65		0		113 5
26/12/2002 15:00	2.69		0		113.75
26/12/2002 15:15	2.74		0		114
26/12/2002 15:30	2.79		0		114.25
26/12/2002 15:45	2.85		0		114 5
26/12/2002 16:00	2.92		0		114.75
26/12/2002 16:15	2.95		0		115
26/12/2002 16:30	3.01		0		115.25
26/12/2002 16:45	3.05		0		115 5
26/12/2002 17:00	3.10		0 2		115.75
26/12/2002 17:15	3.14		0		116
26/12/2002 17:30	3.16		0		116.25
26/12/2002 17:45	3.15		0		116 5
26/12/2002 18:00	3.16		0		116.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
26/12/2002 18:15	3.16		0	117
26/12/2002 18:30	3.16		0	117.25
26/12/2002 18:45	3.13		0	117 5
26/12/2002 19:00	3.10		0	117.75
26/12/2002 19:15	3.05		0	118
26/12/2002 19:30	3.00		0	118.25
26/12/2002 19:45	2.95		0	118 5
26/12/2002 20:00	2.91		0	118.75
26/12/2002 20:15	2.85		0	119
26/12/2002 20:30	2.79		0	119.25
26/12/2002 20:45	2.72		0	119 5
26/12/2002 21:00	2.68		0	119.75
26/12/2002 21:15	2.59		0	120
26/12/2002 21:30	2.55		0	120.25
26/12/2002 21:45	2.48		0	120 5
26/12/2002 22:00	2.41		0	120.75
26/12/2002 22:15	2.38		0	121
26/12/2002 22:30	2.31		0	121.25
26/12/2002 22:45	2.27		0	121 5
26/12/2002 23:00	2.23		0	121.75
26/12/2002 23:15	2.19		0	122
26/12/2002 23:30	2.16		0.4	122.25
26/12/2002 23:45	2.12		0 2	122 5
27/12/2002 00:00	2.08		0.4	122.75
27/12/2002 00:15	2.06		0.4	123
27/12/2002 00:30	2.03		0.4	123.25
27/12/2002 00:45	2.00		0.4	123 5
27/12/2002 01:00	1.98		0 2	123.75
27/12/2002 01:15	1.96		0 2	124
27/12/2002 01:30	1.94		0.4	124.25
27/12/2002 01:45	1.92		0.6	124 5
27/12/2002 02:00	1.92		0 2	124.75
27/12/2002 02:15	1.90		0.4	125
27/12/2002 02:30	1.90		0.4	125.25
27/12/2002 02:45	1.89		0 2	125 5
27/12/2002 03:00	1.92		0.4	125.75
27/12/2002 03:15	1.93		0 2	126
27/12/2002 03:30	1.95		0	126.25
27/12/2002 03:45	1.99		0	126 5
27/12/2002 04:00	2.04		0	126.75
27/12/2002 04:15	2.11		0 2	127
27/12/2002 04:30	2.18		0	127.25
27/12/2002 04:45	2.26		0	127 5
27/12/2002 05:00	2.35		0	127.75
27/12/2002 05:15	2.44		0	128
27/12/2002 05:30	2.57		0	128.25
27/12/2002 05:45	2.70		0	128 5
27/12/2002 06:00	2.83		0	128.75
27/12/2002 06:15	2.97		0	129
27/12/2002 06:30	3.10		0	129.25
27/12/2002 06:45	3.24		0	129 5
27/12/2002 07:00	3.36		0	129.75

Event 01/01/2003 4th peak	

	Middleton		Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)		Duration (hrs)
27/12/2002 07:15	3.49		0		130
27/12/2002 07:30	3.62		0		130.25
27/12/2002 07:45	3.71		0		130 5
27/12/2002 08:00	3.81		0		130.75
27/12/2002 08:15	3.92		0		131
27/12/2002 08:30	4.01		0		131.25
27/12/2002 08:45	4.06		0		131 5
27/12/2002 09:00	4.13		0	5.8	131.75
27/12/2002 09:15	4.20		0		132
27/12/2002 09:30	4.24		0		132.25
27/12/2002 09:45	4.31		0		132 5
27/12/2002 10:00	4.36		0		132.75
27/12/2002 10:15	4.37		0		133
27/12/2002 10:30	4.41		0		133.25
27/12/2002 10:45	4.44		0		133 5
27/12/2002 11:00	4.46		0		133.75
27/12/2002 11:15	4.50		0		134
27/12/2002 11:30	4.51		0		134.25
27/12/2002 11:45	4.54		0		134 5
27/12/2002 12:00	4.56		0		134.75
27/12/2002 12:15	4.58		0		135
27/12/2002 12:30	4.60		0		135.25
27/12/2002 12:45	4.60		0		135 5
27/12/2002 13:00	4.62		0		135.75
27/12/2002 13:15	4.64		0		136
27/12/2002 13:30	4.65		0		136.25
27/12/2002 13:45	4.67		0		136 5
27/12/2002 14:00	4.68		0		136.75
27/12/2002 14:15	4.69		0		137
27/12/2002 14:30	4.69		0		137.25
27/12/2002 14:45	4.72		0		137 5
27/12/2002 15:00	4.73		0		137.75
27/12/2002 15:15	4.73		0		138
27/12/2002 15:30	4.74		0		138.25
27/12/2002 15:45	4.75		0		138 5
27/12/2002 16:00	4.75		0		138.75
27/12/2002 16:15	4.74		0		139
27/12/2002 16:30	4.73		0		139.25
27/12/2002 16:45	4.73		0		139 5
27/12/2002 17:00	4.70		0		139.75
27/12/2002 17:15	4.69		0		140
27/12/2002 17:30	4.65		0		140.25
27/12/2002 17:45	4.62		0		140 5
27/12/2002 18:00	4.58		0		140.75
27/12/2002 18:15	4.52		0		141
27/12/2002 18:30	4.46		0		141.25
27/12/2002 18:45	4.35		0		141 5
27/12/2002 19:00	4.24		0		141.75
27/12/2002 19:15	4.13		0		142
27/12/2002 19:30	3.97		0		142.25
27/12/2002 19:45	3.82		0		142 5
27/12/2002 20:00	3.69		0		142.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)		Duration (hrs)
27/12/2002 20:15	3.51		0		143
27/12/2002 20:30	3.34		0		143.25
27/12/2002 20:45	3.18		0		143 5
27/12/2002 21:00	3.04		0		143.75
27/12/2002 21:15	2.88		0		144
27/12/2002 21:30	2.74		0		144.25
27/12/2002 21:45	2.63		0		144 5
27/12/2002 22:00	2.51		0		144.75
27/12/2002 22:15	2.41		0		145
27/12/2002 22:30	2.32		0		145.25
27/12/2002 22:45	2.26		0		145 5
27/12/2002 23:00	2.21		0		145.75
27/12/2002 23:15	2.15		0		146
27/12/2002 23:30	2.11		0		146.25
27/12/2002 23:45	2.06		0		146 5
28/12/2002 00:00	2.01		0		146.75
28/12/2002 00:15	1.97		0		147
28/12/2002 00:30	1.95		0		147.25
28/12/2002 00:45	1.90		0		147 5
28/12/2002 01:00	1.88		0		147.75
28/12/2002 01:15	1.84		0		148
28/12/2002 01:30	1.81		0		148.25
28/12/2002 01:45	1.79		0		148 5
28/12/2002 02:00	1.76		0		148.75
28/12/2002 02:15	1.75		0		149
28/12/2002 02:30	1.73		0		149.25
28/12/2002 02:45	1.69		0		149 5
28/12/2002 03:00	1.68		0		149.75
28/12/2002 03:15	1.65		0		150
28/12/2002 03:30	1.63		0		150.25
28/12/2002 03:45	1.61		0		150 5
28/12/2002 04:00	1.59		0		150.75
28/12/2002 04:15	1.58		0		151
28/12/2002 04:30	1.55		0		151.25
28/12/2002 04:45	1.54		0		151 5
28/12/2002 05:00	1.53		0		151.75
28/12/2002 05:15	1.50		0		152
28/12/2002 05:30	1.49		0		152.25
28/12/2002 05:45	1.48		0		152 5
28/12/2002 06:00	1.46		0		152.75
28/12/2002 06:15	1.44		0		153
28/12/2002 06:30	1.43		0		153.25
28/12/2002 06:45	1.41		0		153 5
28/12/2002 07:00	1.40		0		153.75
28/12/2002 07:15	1.39		0		154
28/12/2002 07:30	1.37		0		154.25
28/12/2002 07:45	1.36		0		154 5
28/12/2002 08:00	1.35		0		154.75
28/12/2002 08:15	1.33		0		155
28/12/2002 08:30	1.32		0		155.25
28/12/2002 08:45	1.31		0		155 5
28/12/2002 09:00	1.30		0	0	155.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
28/12/2002 09:15	1.28		0	156
28/12/2002 09:30	1.27		0	156.25
28/12/2002 09:45	1.26		0	156 5
28/12/2002 10:00	1.25		0	156.75
28/12/2002 10:15	1.24		0	157
28/12/2002 10:30	1.23		0	157.25
28/12/2002 10:45	1.22		0	157 5
28/12/2002 11:00	1.21		0	157.75
28/12/2002 11:15	1.20		0	158
28/12/2002 11:30	1.19		0	158.25
28/12/2002 11:45	1.19		0	158 5
28/12/2002 12:00	1.17		0	158.75
28/12/2002 12:15	1.16		0	159
28/12/2002 12:30	1.15		0	159.25
28/12/2002 12:45	1.14		0	159 5
28/12/2002 13:00	1.13		0	159.75
28/12/2002 13:15	1.12		0	160
28/12/2002 13:30	1.12		0	160.25
28/12/2002 13:45	1.11		0	160 5
28/12/2002 14:00	1.10		0	160.75
28/12/2002 14:15	1.10		0	161
28/12/2002 14:30	1.08		0	161.25
28/12/2002 14:45	1.08		0	161 5
28/12/2002 15:00	1.08		0	161.75
28/12/2002 15:15	1.06		0	162
28/12/2002 15:30	1.06		0	162.25
28/12/2002 15:45	1.05		0	162 5
28/12/2002 16:00	1.04		0	162.75
28/12/2002 16:15	1.03		0	163
28/12/2002 16:30	1.03		0	163.25
28/12/2002 16:45	1.02		0	163 5
28/12/2002 17:00	1.01		0	163.75
28/12/2002 17:15	1.01		0	164
28/12/2002 17:30	1.00		0	164.25
28/12/2002 17:45	0.99		0	164 5
28/12/2002 18:00	0.99		0	164.75
28/12/2002 18:15	0.99		0	165
28/12/2002 18:30	0.97		0	165.25
28/12/2002 18:45	0.97		0	165 5
28/12/2002 19:00	0.97		0	165.75
28/12/2002 19:15	0.96		0	166
28/12/2002 19:30	0.96		0	166.25
28/12/2002 19:45	0.95		0	166 5
28/12/2002 20:00	0.95		0	166.75
28/12/2002 20:15	0.94		0	167
28/12/2002 20:30	0.93		0	167.25
28/12/2002 20:45	0.93		0	167 5
28/12/2002 21:00	0.93		0	167.75
28/12/2002 21:15	0.93		0	168
28/12/2002 21:30	0.91		0	168.25
28/12/2002 21:45	0.91		0	168 5
28/12/2002 22:00	0.91		0	168.75

Event 01/01/2003 4th peak	

	Middleton		Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)	
28/12/2002 22:15	0.90		0	169	
28/12/2002 22:30	0.90		0	169.25	
28/12/2002 22:45	0.89		0	169 5	
28/12/2002 23:00	0.89		0	169.75	
28/12/2002 23:15	0.88		0	170	
28/12/2002 23:30	0.88		0	170.25	
28/12/2002 23:45	0.88		0	170 5	
29/12/2002 00:00	0.87		0	170.75	
29/12/2002 00:15	0.87		0	171	
29/12/2002 00:30	0.86		0	171.25	
29/12/2002 00:45	0.86		0	171 5	
29/12/2002 01:00	0.86		0	171.75	
29/12/2002 01:15	0.85		0	172	
29/12/2002 01:30	0.85		0	172.25	
29/12/2002 01:45	0.84		0	172 5	
29/12/2002 02:00	0.84		0	172.75	
29/12/2002 02:15	0.84		0	173	
29/12/2002 02:30	0.84		0	173.25	
29/12/2002 02:45	0.83		0	173 5	
29/12/2002 03:00	0.83		0	173.75	
29/12/2002 03:15	0.83		0	174	
29/12/2002 03:30	0.82		0	174.25	
29/12/2002 03:45	0.81		0	174 5	
29/12/2002 04:00	0.81		0	174.75	
29/12/2002 04:15	0.81		0	175	
29/12/2002 04:30	0.81		0	175.25	
29/12/2002 04:45	0.81		0	175 5	
29/12/2002 05:00	0.80		0	175.75	
29/12/2002 05:15	0.80		0	176	
29/12/2002 05:30	0.80		0	176.25	
29/12/2002 05:45	0.80		0	176 5	
29/12/2002 06:00	0.79		0	176.75	
29/12/2002 06:15	0.79		0	177	
29/12/2002 06:30	0.79		0	177.25	
29/12/2002 06:45	0.79		0	177 5	
29/12/2002 07:00	0.78		0	177.75	
29/12/2002 07:15	0.78		0	178	
29/12/2002 07:30	0.77		0	178.25	
29/12/2002 07:45	0.77		0	178 5	
29/12/2002 08:00	0.77		0 2	178.75	
29/12/2002 08:15	0.77		0.4	179	
29/12/2002 08:30	0.77		0.4	179.25	
29/12/2002 08:45	0.77		0 2	179 5	
29/12/2002 09:00	0.76		0 2	1.4 179.75	
29/12/2002 09:15	0.76		0 2	180	
29/12/2002 09:30	0.76		0.4	180.25	
29/12/2002 09:45	0.76		0 2	180 5	
29/12/2002 10:00	0.76		0.4	180.75	
29/12/2002 10:15	0.76		0 2	181	
29/12/2002 10:30	0.76		0 2	181.25	
29/12/2002 10:45	0.76		0 2	181 5	
29/12/2002 11:00	0.76		0 2	181.75	

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)
29/12/2002 11:15	0.76		0 2	182
29/12/2002 11:30	0.76		0.4	182.25
29/12/2002 11:45	0.76		0.4	182 5
29/12/2002 12:00	0.76		0.4	182.75
29/12/2002 12:15	0.77		0	183
29/12/2002 12:30	0.77		0	183.25
29/12/2002 12:45	0.77		0 2	183 5
29/12/2002 13:00	0.78		0 2	183.75
29/12/2002 13:15	0.79		0.4	184
29/12/2002 13:30	0.79		0 2	184.25
29/12/2002 13:45	0.80		0	184 5
29/12/2002 14:00	0.81		0 2	184.75
29/12/2002 14:15	0.82		0 2	185
29/12/2002 14:30	0.83		0.6	185.25
29/12/2002 14:45	0.85		0.4	185 5
29/12/2002 15:00	0.87		0.4	185.75
29/12/2002 15:15	0.89		0.4	186
29/12/2002 15:30	0.92		0.6	186.25
29/12/2002 15:45	0.96		0 8	186 5
29/12/2002 16:00	1.01		0 8	186.75
29/12/2002 16:15	1.07		0 8	187
29/12/2002 16:30	1.15		0.4	187.25
29/12/2002 16:45	1.25		0.4	187 5
29/12/2002 17:00	1.37		0.4	187.75
29/12/2002 17:15	1.51		0.4	188
29/12/2002 17:30	1.68		0.6	188.25
29/12/2002 17:45	1.84		0.6	188 5
29/12/2002 18:00	2.01		0.4	188.75
29/12/2002 18:15	2.21		0.6	189
29/12/2002 18:30	2.39		0 2	189.25
29/12/2002 18:45	2.58		0.4	189 5
29/12/2002 19:00	2.84		0 2	189.75
29/12/2002 19:15	3.14		0 2	190
29/12/2002 19:30	3.46		0	190.25
29/12/2002 19:45	3.80		0	190 5
29/12/2002 20:00	4.13		0	190.75
29/12/2002 20:15	4.43		0 2	191
29/12/2002 20:30	4.69		0	191.25
29/12/2002 20:45	4.92		0	191 5
29/12/2002 21:00	5.17		0	191.75
29/12/2002 21:15	5.31		0	192
29/12/2002 21:30	5.48		0	192.25
29/12/2002 21:45	5.61		0	192 5
29/12/2002 22:00	5.71		0	192.75
29/12/2002 22:15	5.82		0	193
29/12/2002 22:30	5.89		0	193.25
29/12/2002 22:45	5.92		0	193 5
29/12/2002 23:00	5.98		0	193.75
29/12/2002 23:15	6.00		0	194
29/12/2002 23:30	6.07		0	194.25
29/12/2002 23:45	6.06		0	194 5
30/12/2002 00:00	6.11		0	194.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)	
30/12/2002 00:15	6.17		0	195	
30/12/2002 00:30	6.24		0	195.25	
30/12/2002 00:45	6.27		0	195 5	
30/12/2002 01:00	6.34		0	195.75	
30/12/2002 01:15	6.42		0	196	
30/12/2002 01:30	6.48		0	196.25	
30/12/2002 01:45	6.58		0	196 5	
30/12/2002 02:00	6.65		0	196.75	
30/12/2002 02:15	6.77		0	197	
30/12/2002 02:30	6.93		0	197.25	
30/12/2002 02:45	7.03		0	197 5	
30/12/2002 03:00	7.19		0	197.75	
30/12/2002 03:15	7.39		0	198	
30/12/2002 03:30	7.55		0	198.25	
30/12/2002 03:45	7.75		0	198 5	
30/12/2002 04:00	7.95		0	198.75	
30/12/2002 04:15	8.13		0	199	
30/12/2002 04:30	8.31		0	199.25	
30/12/2002 04:45	8.43		0	199 5	
30/12/2002 05:00	8.57		0	199.75	
30/12/2002 05:15	8.68		0	200	
30/12/2002 05:30	8.80		0	200.25	
30/12/2002 05:45	8.88		0	200 5	
30/12/2002 06:00	8.99		0	200.75	
30/12/2002 06:15	9.04		0	201	
30/12/2002 06:30	9.08		0	201.25	
30/12/2002 06:45	9.15		0	201 5	
30/12/2002 07:00	9.15		0	201.75	
30/12/2002 07:15	9.17		0	202	
30/12/2002 07:30	9.17		0	202.25	
30/12/2002 07:45	9.17		0	202 5	
30/12/2002 08:00	9.17		0	202.75	
30/12/2002 08:15	9.13		0	203	
30/12/2002 08:30	9.06		0	203.25	
30/12/2002 08:45	9.02		0	203 5	
30/12/2002 09:00	8.97		0	14.6 203.75	
30/12/2002 09:15	8.87		0	204	
30/12/2002 09:30	8.75		0	204.25	
30/12/2002 09:45	8.68		0	204 5	
30/12/2002 10:00	8.57		0	204.75	
30/12/2002 10:15	8.48		0	205	
30/12/2002 10:30	8.31		0	205.25	
30/12/2002 10:45	8.18		0	205 5	
30/12/2002 11:00	8.02		0	205.75	
30/12/2002 11:15	7.86		0	206	
30/12/2002 11:30	7.70		0	206.25	
30/12/2002 11:45	7.55		0	206 5	
30/12/2002 12:00	7.37		0	206.75	
30/12/2002 12:15	7.23		0	207	
30/12/2002 12:30	7.08		0	207.25	
30/12/2002 12:45	6.93		0	207 5	
30/12/2002 13:00	6.76		0	207.75	

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
30/12/2002 13:15	6.63		0	208
30/12/2002 13:30	6.48		0	208.25
30/12/2002 13:45	6.32		0	208 5
30/12/2002 14:00	6.21		0	208.75
30/12/2002 14:15	6.11		0	209
30/12/2002 14:30	5.97		0	209.25
30/12/2002 14:45	5.83		0	209 5
30/12/2002 15:00	5.71		0	209.75
30/12/2002 15:15	5.61		0	210
30/12/2002 15:30	5.47		0	210.25
30/12/2002 15:45	5.33		0	210 5
30/12/2002 16:00	5.14		0	210.75
30/12/2002 16:15	4.98		0	211
30/12/2002 16:30	4.79		0	211.25
30/12/2002 16:45	4.60		0	211 5
30/12/2002 17:00	4.40		0	211.75
30/12/2002 17:15	4.19		0	212
30/12/2002 17:30	3.96		0	212.25
30/12/2002 17:45	3.75		0	212 5
30/12/2002 18:00	3.54		0 2	212.75
30/12/2002 18:15	3.36		0 2	213
30/12/2002 18:30	3.19		0	213.25
30/12/2002 18:45	3.02		0	213 5
30/12/2002 19:00	2.89		0	213.75
30/12/2002 19:15	2.76		0	214
30/12/2002 19:30	2.64		0	214.25
30/12/2002 19:45	2.52		0	214 5
30/12/2002 20:00	2.45		0	214.75
30/12/2002 20:15	2.37		0	215
30/12/2002 20:30	2.30		0	215.25
30/12/2002 20:45	2.23		0	215 5
30/12/2002 21:00	2.20		0	215.75
30/12/2002 21:15	2.12		0	216
30/12/2002 21:30	2.08		0	216.25
30/12/2002 21:45	2.04		0	216 5
30/12/2002 22:00	2.00		0	216.75
30/12/2002 22:15	1.96		0	217
30/12/2002 22:30	1.93		0	217.25
30/12/2002 22:45	1.88		0	217 5
30/12/2002 23:00	1.86		0	217.75
30/12/2002 23:15	1.84		0	218
30/12/2002 23:30	1.82		0	218.25
30/12/2002 23:45	1.78		0	218 5
31/12/2002 00:00	1.75		0	218.75
31/12/2002 00:15	1.75		0	219
31/12/2002 00:30	1.72		0	219.25
31/12/2002 00:45	1.69		0	219 5
31/12/2002 01:00	1.68		0	219.75
31/12/2002 01:15	1.65		0	220
31/12/2002 01:30	1.64		0	220.25
31/12/2002 01:45	1.61		0	220 5
31/12/2002 02:00	1.60		0	220.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)		Duration (hrs)
31/12/2002 02:15	1.58		0		221
31/12/2002 02:30	1.57		0		221.25
31/12/2002 02:45	1.54		0		221 5
31/12/2002 03:00	1.53		0		221.75
31/12/2002 03:15	1.52		0		222
31/12/2002 03:30	1.50		0		222.25
31/12/2002 03:45	1.48		0		222 5
31/12/2002 04:00	1.47		0		222.75
31/12/2002 04:15	1.46		0		223
31/12/2002 04:30	1.44		0		223.25
31/12/2002 04:45	1.42		0		223 5
31/12/2002 05:00	1.41		0		223.75
31/12/2002 05:15	1.39		0		224
31/12/2002 05:30	1.39		0		224.25
31/12/2002 05:45	1.38		0		224 5
31/12/2002 06:00	1.36		0 2		224.75
31/12/2002 06:15	1.35		0		225
31/12/2002 06:30	1.34		0		225.25
31/12/2002 06:45	1.32		0		225 5
31/12/2002 07:00	1.31		0		225.75
31/12/2002 07:15	1.31		0		226
31/12/2002 07:30	1.29		0		226.25
31/12/2002 07:45	1.28		0		226 5
31/12/2002 08:00	1.28		0		226.75
31/12/2002 08:15	1.25		0		227
31/12/2002 08:30	1.25		0		227.25
31/12/2002 08:45	1.24		0		227 5
31/12/2002 09:00	1.23		0	0.6	227.75
31/12/2002 09:15	1.22		0		228
31/12/2002 09:30	1.21		0		228.25
31/12/2002 09:45	1.20		0		228 5
31/12/2002 10:00	1.19		0		228.75
31/12/2002 10:15	1.18		0		229
31/12/2002 10:30	1.17		0		229.25
31/12/2002 10:45	1.16		0		229 5
31/12/2002 11:00	1.16		0		229.75
31/12/2002 11:15	1.14		0		230
31/12/2002 11:30	1.14		0		230.25
31/12/2002 11:45	1.13		0		230 5
31/12/2002 12:00	1.13		0		230.75
31/12/2002 12:15	1.11		0		231
31/12/2002 12:30	1.11		0		231.25
31/12/2002 12:45	1.11		0		231 5
31/12/2002 13:00	1.10		0		231.75
31/12/2002 13:15	1.09		0		232
31/12/2002 13:30	1.09		0		232.25
31/12/2002 13:45	1.08		0		232 5
31/12/2002 14:00	1.08		0		232.75
31/12/2002 14:15	1.07		0		233
31/12/2002 14:30	1.06		0		233.25
31/12/2002 14:45	1.05		0		233 5
31/12/2002 15:00	1.04		0		233.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
31/12/2002 15:15	1.03		0	234
31/12/2002 15:30	1.03		0	234.25
31/12/2002 15:45	1.02		0	234 5
31/12/2002 16:00	1.01		0	234.75
31/12/2002 16:15	1.01		0	235
31/12/2002 16:30	1.00		0	235.25
31/12/2002 16:45	0.99		0	235 5
31/12/2002 17:00	0.99		0	235.75
31/12/2002 17:15	0.98		0	236
31/12/2002 17:30	0.98		0	236.25
31/12/2002 17:45	0.97		0	236 5
31/12/2002 18:00	0.97		0	236.75
31/12/2002 18:15	0.96		0	237
31/12/2002 18:30	0.96		0	237.25
31/12/2002 18:45	0.95		0	237 5
31/12/2002 19:00	0.95		0	237.75
31/12/2002 19:15	0.95		0	238
31/12/2002 19:30	0.94		0	238.25
31/12/2002 19:45	0.94		0	238 5
31/12/2002 20:00	0.93		0	238.75
31/12/2002 20:15	0.93		0	239
31/12/2002 20:30	0.93		0	239.25
31/12/2002 20:45	0.92		0	239 5
31/12/2002 21:00	0.92		0	239.75
31/12/2002 21:15	0.91		0	240
31/12/2002 21:30	0.91		0	240.25
31/12/2002 21:45	0.91		0	240 5
31/12/2002 22:00	0.91		0	240.75
31/12/2002 22:15	0.90		0	241
31/12/2002 22:30	0.90		0	241.25
31/12/2002 22:45	0.89		0	241 5
31/12/2002 23:00	0.89		0	241.75
31/12/2002 23:15	0.89		0	242
31/12/2002 23:30	0.88		0	242.25
31/12/2002 23:45	0.88		0	242 5
01/01/2003 00:00	0.88		0	242.75
01/01/2003 00:15	0.88		0	243
01/01/2003 00:30	0.88		0	243.25
01/01/2003 00:45	0.87		0	243 5
01/01/2003 01:00	0.87		0	243.75
01/01/2003 01:15	0.87		0	244
01/01/2003 01:30	0.86		0	244.25
01/01/2003 01:45	0.86		0	244 5
01/01/2003 02:00	0.86		0	244.75
01/01/2003 02:15	0.85		0	245
01/01/2003 02:30	0.85		0	245.25
01/01/2003 02:45	0.85		0	245 5
01/01/2003 03:00	0.84		0	245.75
01/01/2003 03:15	0.84		0	246
01/01/2003 03:30	0.84		0	246.25
01/01/2003 03:45	0.84		0	246 5
01/01/2003 04:00	0.84		0	246.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
01/01/2003 04:15	0.83		0	247
01/01/2003 04:30	0.83		0	247.25
01/01/2003 04:45	0.83		0	247 5
01/01/2003 05:00	0.83		0	247.75
01/01/2003 05:15	0.83		0	248
01/01/2003 05:30	0.83		0	248.25
01/01/2003 05:45	0.83		0 2	248 5
01/01/2003 06:00	0.82		0 2	248.75
01/01/2003 06:15	0.82		0 2	249
01/01/2003 06:30	0.82		0 2	249.25
01/01/2003 06:45	0.81		0 2	249 5
01/01/2003 07:00	0.81		0.6	249.75
01/01/2003 07:15	0.81		0 8	250
01/01/2003 07:30	0.82		0 8	250.25
01/01/2003 07:45	0.82		0 8	250 5
01/01/2003 08:00	0.83		0 8	250.75
01/01/2003 08:15	0.83		0.4	251
01/01/2003 08:30	0.84		0 8	251.25
01/01/2003 08:45	0.85		0 8	251 5
01/01/2003 09:00	0.87		1	251.75
01/01/2003 09:15	0.89		0 2	252
01/01/2003 09:30	0.93		0.6	252.25
01/01/2003 09:45	0.96		0 2	252 5
01/01/2003 10:00	1.02		0 2	252.75
01/01/2003 10:15	1.10		0 2	253
01/01/2003 10:30	1.20		0	253.25
01/01/2003 10:45	1.34		0	253 5
01/01/2003 11:00	1.52		0.4	253.75
01/01/2003 11:15	1.71		0.4	254
01/01/2003 11:30	1.92		0 2	254.25
01/01/2003 11:45	2.16		0	254 5
01/01/2003 12:00	2.35		0	254.75
01/01/2003 12:15	2.56		0	255
01/01/2003 12:30	2.77		0	255.25
01/01/2003 12:45	3.00		0	255 5
01/01/2003 13:00	3.26		0	255.75
01/01/2003 13:15	3.53		0	256
01/01/2003 13:30	3.80		0	256.25
01/01/2003 13:45	4.01		0	256 5
01/01/2003 14:00	4.22		0	256.75
01/01/2003 14:15	4.41		0 2	257
01/01/2003 14:30	4.57		2	257.25
01/01/2003 14:45	4.69		0	257 5
01/01/2003 15:00	4.79		0	257.75
01/01/2003 15:15	4.93		0	258
01/01/2003 15:30	5.04		1	258.25
01/01/2003 15:45	5.16		1	258 5
01/01/2003 16:00	5.30		1	258.75
01/01/2003 16:15	5.46		1	259
01/01/2003 16:30	5.58		0 8	259.25
01/01/2003 16:45	5.73		0.4	259 5
01/01/2003 17:00	5.87		0 8	259.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Daily Total RF (mm)	Duration (hrs)
01/01/2003 17:15	6.02		0 2	260
01/01/2003 17:30	6.22		0.4	260.25
01/01/2003 17:45	6.37		0 2	260 5
01/01/2003 18:00	6.51		0	260.75
01/01/2003 18:15	6.67		0	261
01/01/2003 18:30	6.89		0	261.25
01/01/2003 18:45	7.09		0	261 5
01/01/2003 19:00	7.32		0	261.75
01/01/2003 19:15	7.65		0	262
01/01/2003 19:30	7.94		0	262.25
01/01/2003 19:45	8.34		0	262 5
01/01/2003 20:00	8.77		0	262.75
01/01/2003 20:15	9.28		0	263
01/01/2003 20:30	9.82		0	263.25
01/01/2003 20:45	10.38		0	263 5
01/01/2003 21:00	10.88		0	263.75
01/01/2003 21:15	11.42		0	264
01/01/2003 21:30	11.86		0	264.25
01/01/2003 21:45	12.20		0	264 5
01/01/2003 22:00	12.47		0	264.75
01/01/2003 22:15	12.79		0	265
01/01/2003 22:30	12.95		0	265.25
01/01/2003 22:45	13.14		0	265 5
01/01/2003 23:00	13.38		0	265.75
01/01/2003 23:15	13.55		0	266
01/01/2003 23:30	13.58		0	266.25
01/01/2003 23:45	13.65		0	266 5
02/01/2003 00:00	13.65		0	266.75
02/01/2003 00:15	13.76		0	267
02/01/2003 00:30	13.79		0	267.25
02/01/2003 00:45	13.72		0	267 5
02/01/2003 01:00	13.83		0 2	267.75
02/01/2003 01:15	13.69		0	268
02/01/2003 01:30	13.65		0	268.25
02/01/2003 01:45	13.76		0	268 5
02/01/2003 02:00	13.79		0	268.75
02/01/2003 02:15	13.69		0	269
02/01/2003 02:30	13.79		0	269.25
02/01/2003 02:45	13.79		0	269 5
02/01/2003 03:00	13.83		0	269.75
02/01/2003 03:15	13.72		0	270
02/01/2003 03:30	13.86		0	270.25
02/01/2003 03:45	13.93		0	270 5
02/01/2003 04:00	13.93		0	270.75
02/01/2003 04:15	13.93		0	271
02/01/2003 04:30	14.12		0	271.25
02/01/2003 04:45	14.04		0	271 5
02/01/2003 05:00	14.12		0	271.75
02/01/2003 05:15	14.12		0	272
02/01/2003 05:30	14.12		0	272.25
02/01/2003 05:45	14.26		0	272 5
02/01/2003 06:00	14.15		0	272.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
02/01/2003 06:15	14.12		0	273
02/01/2003 06:30	14.08		0	273.25
02/01/2003 06:45	14.04		0	273 5
02/01/2003 07:00	14.01		0	273.75
02/01/2003 07:15	13.93		0	274
02/01/2003 07:30	13.93		0	274.25
02/01/2003 07:45	13.79		0 2	274 5
02/01/2003 08:00	13.76		0 2	274.75
02/01/2003 08:15	13.69		0	275
02/01/2003 08:30	13.48		0	275.25
02/01/2003 08:45	13.34		0	275 5
02/01/2003 09:00	13.14		0.4	275.75
02/01/2003 09:15	13.01		1 2	276
02/01/2003 09:30	12.88		1 2	276.25
02/01/2003 09:45	12.69		1	276 5
02/01/2003 10:00	12.54		1.4	276.75
02/01/2003 10:15	12.38		1 2	277
02/01/2003 10:30	12.11		0 2	277.25
02/01/2003 10:45	11.88		0	277 5
02/01/2003 11:00	11.69		0	277.75
02/01/2003 11:15	11.42		0	278
02/01/2003 11:30	11.21		0	278.25
02/01/2003 11:45	10.95		0	278 5
02/01/2003 12:00	10.76		0	278.75
02/01/2003 12:15	10.59		0	279
02/01/2003 12:30	10.38		0	279.25
02/01/2003 12:45	10.23		0	279 5
02/01/2003 13:00	10.01		0	279.75
02/01/2003 13:15	9.86		0	280
02/01/2003 13:30	9.70		0	280.25
02/01/2003 13:45	9.56		0	280 5
02/01/2003 14:00	9.39		0	280.75
02/01/2003 14:15	9.24		0	281
02/01/2003 14:30	9.06		0	281.25
02/01/2003 14:45	8.94		0	281 5
02/01/2003 15:00	8.78		0	281.75
02/01/2003 15:15	8.67		0	282
02/01/2003 15:30	8.56		0	282.25
02/01/2003 15:45	8.45		0	282 5
02/01/2003 16:00	8.34		0	282.75
02/01/2003 16:15	8.22		0	283
02/01/2003 16:30	8.18		0	283.25
02/01/2003 16:45	8.12		0	283 5
02/01/2003 17:00	8.06		0	283.75
02/01/2003 17:15	8.04		0	284
02/01/2003 17:30	8.02		0	284.25
02/01/2003 17:45	8.02		0	284 5
02/01/2003 18:00	8.04		0	284.75
02/01/2003 18:15	8.05		0 2	285
02/01/2003 18:30	8.09		0	285.25
02/01/2003 18:45	8.15		0	285 5
02/01/2003 19:00	8.22		0	285.75

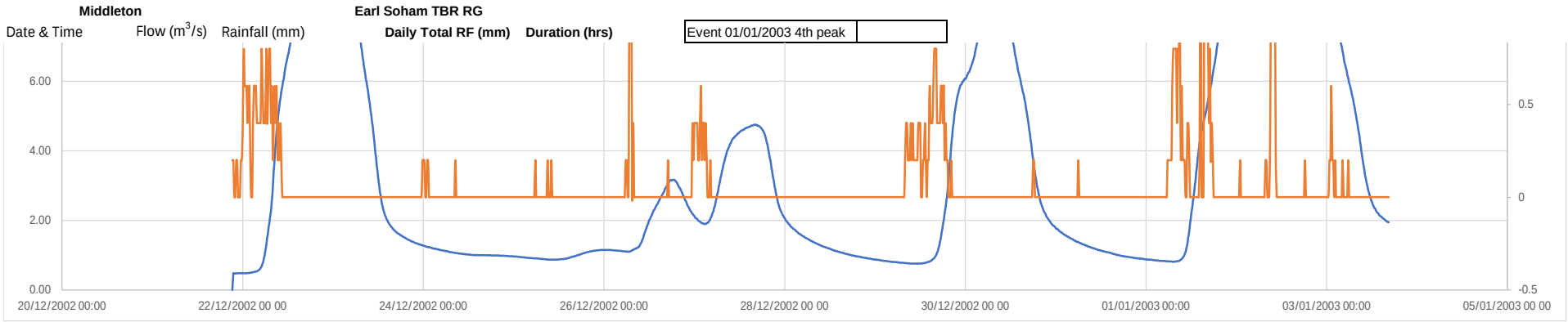
Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
02/01/2003 19:15	8.30		0	286
02/01/2003 19:30	8.36		0	286.25
02/01/2003 19:45	8.40		0	286 5
02/01/2003 20:00	8.48		0	286.75
02/01/2003 20:15	8.52		0	287
02/01/2003 20:30	8.59		0	287.25
02/01/2003 20:45	8.64		0	287 5
02/01/2003 21:00	8.68		0	287.75
02/01/2003 21:15	8.72		0	288
02/01/2003 21:30	8.77		0	288.25
02/01/2003 21:45	8.82		0	288 5
02/01/2003 22:00	8.83		0	288.75
02/01/2003 22:15	8.82		0	289
02/01/2003 22:30	8.85		0	289.25
02/01/2003 22:45	8.87		0	289 5
02/01/2003 23:00	8.83		0	289.75
02/01/2003 23:15	8.85		0	290
02/01/2003 23:30	8.80		0	290.25
02/01/2003 23:45	8.78		0	290 5
03/01/2003 00:00	8.73		0	290.75
03/01/2003 00:15	8.67		0	291
03/01/2003 00:30	8.60		0	291.25
03/01/2003 00:45	8.56		0 2	291 5
03/01/2003 01:00	8.46		0 2	291.75
03/01/2003 01:15	8.36		0.6	292
03/01/2003 01:30	8.25		0 2	292.25
03/01/2003 01:45	8.12		0 2	292 5
03/01/2003 02:00	8.01		0	292.75
03/01/2003 02:15	7.86		0 2	293
03/01/2003 02:30	7.74		0	293.25
03/01/2003 02:45	7.59		0	293 5
03/01/2003 03:00	7.44		0	293.75
03/01/2003 03:15	7.30		0	294
03/01/2003 03:30	7.12		0	294.25
03/01/2003 03:45	6.99		0	294 5
03/01/2003 04:00	6.87		0	294.75
03/01/2003 04:15	6.70		0 2	295
03/01/2003 04:30	6.54		0	295.25
03/01/2003 04:45	6.45		0	295 5
03/01/2003 05:00	6.33		0	295.75
03/01/2003 05:15	6.19		0	296
03/01/2003 05:30	6.07		0	296.25
03/01/2003 05:45	5.95		0 2	296 5
03/01/2003 06:00	5.85		0	296.75
03/01/2003 06:15	5.73		0	297
03/01/2003 06:30	5.60		0	297.25
03/01/2003 06:45	5.49		0	297 5
03/01/2003 07:00	5.34		0	297.75
03/01/2003 07:15	5.21		0	298
03/01/2003 07:30	5.04		0	298.25
03/01/2003 07:45	4.89		0	298 5
03/01/2003 08:00	4.72		0	298.75

Event 01/01/2003 4th peak	

Middleton			Earl Soham TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Total RF (mm)**	**Duration (hrs)**
03/01/2003 08:15	4.56		0	299
03/01/2003 08:30	4.39		0	299.25
03/01/2003 08:45	4.17		0	299 5
03/01/2003 09:00	3.99		0	299.75
03/01/2003 09:15	3.79		0	300
03/01/2003 09:30	3.63		0	300.25
03/01/2003 09:45	3.46		0	300 5
03/01/2003 10:00	3.29		0	300.75
03/01/2003 10:15	3.15		0	301
03/01/2003 10:30	3.02		0	301.25
03/01/2003 10:45	2.90		0	301 5
03/01/2003 11:00	2.79		0	301.75
03/01/2003 11:15	2.71		0	302
03/01/2003 11:30	2.62		0	302.25
03/01/2003 11:45	2.53		0	302 5
03/01/2003 12:00	2.47		0	302.75
03/01/2003 12:15	2.40		0	303
03/01/2003 12:30	2.35		0	303.25
03/01/2003 12:45	2.31		0	303 5
03/01/2003 13:00	2.25		0	303.75
03/01/2003 13:15	2.22		0	304
03/01/2003 13:30	2.20		0	304.25
03/01/2003 13:45	2.15		0	304 5
03/01/2003 14:00	2.12		0	304.75
03/01/2003 14:15	2.12		0	305
03/01/2003 14:30	2.08		0	305.25
03/01/2003 14:45	2.06		0	305 5
03/01/2003 15:00	2.03		0	305.75
03/01/2003 15:15	2.02		0	306
03/01/2003 15:30	1.99		0	306.25
03/01/2003 15:45	1.97		0	306 5
03/01/2003 16:00	1.95		0	306.75
03/01/2003 16:15	1.95		0	307
03/01/2003 16:30	1.91		0	307.25

Event 01/01/2003 4th peak	


Middleton
Earl Soham TBR RG
Date & Time
Flow (m3/s)
Rainfall (mm)
Daily Total RF (mm)
Duration (hrs)
Event 01/01/2003 4th peak
6.00
4.00
2.00
0.00
0.5
0
-0.5
20/12/2002 00:00
22/12/2002 00 00
24/12/2002 00:00
26/12/2002 00:00
28/12/2002 00 00
30/12/2002 00 00
01/01/2003 00:00
03/01/2003 00:00
05/01/2003 00 00

SAAR	592	mm
AREA	50.52	Km2

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capacity in the soil column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
W/E 31/12/2002	0	mm
W/E 07/01/2003	0.4	mm

Source of Rainfa l event data.

Gauge	Easting	Northing	Distance from Catchment Centroid (m)	Reciprocal	Weighting
Benhall	38166	60602			
Soham	23243	62717	15768.0	6.34196E-05	1.0000
Thorpeness	60012	78834			
			Total	6.34196E-05	1.0000

TBR RG

Daily RF totals 9am 9am	**Soham**	
Date	**Total RF (mm)**	**Total RF (mm)**
30/12/2002	d-1	0.6
29/12/2002	d-2	14.6
28/12/2002	d-3	1.4
27/12/2002	d-4	0
26/12/2002	d-5	5.8
		22.4

Rainall Event Depth P (mm)	19.2	
Event duration (hours)	14	

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**30/12/2002**	**29/12/2002**	**28/12/2002**	**27/12/2002**	**26/12/2002**
Benhall	592						
Soham	592	1.0000	0.6	14.6	1.4	0	5.8
Thorpeness	592						
Average Daily rainfall totals			0.6	14.6	1.4	0	5.8

Gauge	**SAAR**	**Weight**	**30/12/2002**	**29/12/2002**	**28/12/2002**	**27/12/2002**	**26/12/2002**
Benhall	592						
Soham	592	1.0000	0.001013514	0.024662162	0.002364865	0	0.009797297
Thorpeness	592						

Gauge	**SAAR**	**Weight**	**30/12/2002**	**29/12/2002**	**28/12/2002**	**27/12/2002**	**26/12/2002**
Benhall	592						
Soham	592	1.0000	0.001013514	0.024662162	0.002364865	0	0.009797297
Thorpeness	592						

Gauge	**SAAR**	**Weight**	**30/12/2002**	**29/12/2002**	**28/12/2002**	**27/12/2002**	**26/12/2002**
Benhall	592						
Soham	592	1.0000	0.6	14.6	1.4	0	5.8
Thorpeness	592						
Catchment Average Antecedent RF mm			0.6	14.6	1.4	0	5.8

Date	**Catchment Average Antecedent Rainfall (mm)**	
26/12/2002	5.80	d-5
27/12/2002	0.00	d-4
28/12/2002	1.40	d-3
29/12/2002	14.60	d-2
30/12/2002	0.60	d-1

API5

6.09	mm	6.089957153	mm / day

CWI Prior to Event January 2003 Event at Middleton
CWI 125 + API15 - SMD

SMD	0	mm
CWI	131.0899572	mm

FEH Parameter								
SPR	68.5	%					**URBEXT2000**	0 0084	As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
PRrural	70.0	%		P=Storm Depth	19.2	mm	**PR**	70	taken from observed PR calculations sheet
DPRrain	0.0	%		SPR	68.47751071	%	**DPRrain**	0	DPRrain is 0, as P<40mm
DPRcwi	1.5	CWI	131.09				**DPRcwi**	1 5	
							SPR	68.47751071	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural							**DPRrain**	0.45(P-40)^0.7	#NUM!
PR	70.0	%					**P**	19 2	
PRrural	70.0	%					**CWI**	131.1	
CWI	131.1	mm					**SPR**	68 5	
BF	0 00001		Baseflow equation taken from FEH				**PR**	70 0	
	-1254								
	1778.5		524 5	0.00525			**SPRHOST**	41.05	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
AREA	50.16			**0.26309** m3s-1			**Duration (hours)**	14	
SPR	68.47751071								
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}								
SPR =	68.5								
PRrural	70.0								

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
01-Jan-03	02-Jan-03	14.00	6.09	0.0	131.1	70.0	1.5	0.00	68.5	70.0	41.05

Middleton		Benhall TBR RG			**Rainfall Event**		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours
21/02/2010 00:00	0.79	0	0		28/02/2010 04:00	0.2	0
21/02/2010 00:15	0.78	0	0.25		28/02/2010 04:15	0	0 25
21/02/2010 00:30	0.78	0	0.5		28/02/2010 04:30	0	0.5
21/02/2010 00:45	0.77	0	0.75		28/02/2010 04:45	0.2	0.75
21/02/2010 01:00	0.77	0	1		28/02/2010 05:00	0.2	1
21/02/2010 01:15	0.77	0	1.25		28/02/2010 05:15	0.2	1 25
21/02/2010 01:30	0.77	0	1.5		28/02/2010 05:30	0.2	1.5
21/02/2010 01:45	0.76	0	1.75		28/02/2010 05:45	0.6	1.75
21/02/2010 02:00	0.76	0	2		28/02/2010 06:00	0.4	2
21/02/2010 02:15	0.76	0	2.25		28/02/2010 06:15	0.6	2 25
21/02/2010 02:30	0.76	0	2.5		28/02/2010 06:30	0.2	2.5
21/02/2010 02:45	0.76	0	2.75		28/02/2010 06:45	0.2	2.75
21/02/2010 03:00	0.75	0	3		28/02/2010 07:00	0.4	3
21/02/2010 03:15	0.75	0	3.25		28/02/2010 07:15	0.4	3 25
21/02/2010 03:30	0.75	0	3.5		28/02/2010 07:30	0.2	3.5
21/02/2010 03:45	0.75	0	3.75		28/02/2010 07:45	0.8	3.75
21/02/2010 04:00	0.74	0	4		28/02/2010 08:00	1	4
21/02/2010 04:15	0.74	0	4.25		28/02/2010 08:15	0.4	4 25
21/02/2010 04:30	0.74	0	4.5		28/02/2010 08:30	0.6	4.5
21/02/2010 04:45	0.74	0	4.75		28/02/2010 08:45	0.6	4.75
21/02/2010 05:00	0.74	0	5		28/02/2010 09:00	0.6	5
21/02/2010 05:15	0.74	0	5.25		28/02/2010 09:15	0.6	5 25
21/02/2010 05:30	0.73	0	5.5		28/02/2010 09:30	1	5.5
21/02/2010 05:45	0.73	0	5.75		28/02/2010 09:45	0.8	5.75
21/02/2010 06:00	0.72	0	6		28/02/2010 10:00	0.6	6
21/02/2010 06:15	0.72	0	6.25		28/02/2010 10:15	0.6	6 25
21/02/2010 06:30	0.72	0	6.5		28/02/2010 10:30	0.8	6.5
21/02/2010 06:45	0.72	0	6.75		28/02/2010 10:45	0.6	6.75
21/02/2010 07:00	0.72	0	7		28/02/2010 11:00	0.4	7
21/02/2010 07:15	0.71	0	7.25		28/02/2010 11:15	0.4	7 25
21/02/2010 07:30	0.71	0	7.5		28/02/2010 11:30	0.4	7.5
21/02/2010 07:45	0.71	0	7.75		28/02/2010 11:45	0.4	7.75
21/02/2010 08:00	0.71	0	8		28/02/2010 12:00	0.4	8
21/02/2010 08:15	0.71	0	8.25		28/02/2010 12:15	0.2	8 25
21/02/2010 08:30	0.70	0	8.5		28/02/2010 12:30	0.4	8.5
21/02/2010 08:45	0.70	0	8.75		28/02/2010 12:45	0.6	8.75
21/02/2010 09:00	0.70	0	9		28/02/2010 13:00	0.6	9
21/02/2010 09:15	0.70	0	9.25		28/02/2010 13:15	0.4	9 25
21/02/2010 09:30	0.70	0	9.5		28/02/2010 13:30	0.4	9.5
21/02/2010 09:45	0.70	0.2	9.75		28/02/2010 13:45	0	9.75
21/02/2010 10:00	0.70	0	10		28/02/2010 14:00	0.2	10
21/02/2010 10:15	0.69	0.6	10.25		28/02/2010 14:15	0	10 25
21/02/2010 10:30	0.70	0.2	10.5		28/02/2010 14:30	0	10.5
21/02/2010 10:45	0.69	0.2	10.75		28/02/2010 14:45	0	10.75
21/02/2010 11:00	0.69	0	11		28/02/2010 15:00	0.2	11
21/02/2010 11:15	0.69	0.2	11.25		28/02/2010 15:15	0	11 25
21/02/2010 11:30	0.70	0.2	11.5		28/02/2010 15:30	0.2	11.5
21/02/2010 11:45	0.69	0.8	11.75		28/02/2010 15:45	0	11.75

start of event	28/02/2010 04:00
end of event	28/02/2010 22:45
duration hours	18.75
total RF mm	19.6
SMD W/E AVERAGE	**mm**
02/03/2010	1.3

DATE	**API5**	Daily Totals
26/02/2010	d-1	3
25/02/2010	d-2	9.4
24/02/2010	d-3	1
23/02/2010	d-4	2.4
22/02/2010	d-5	5.8
		21.6

Middleton		Benhall TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours
21/02/2010 12:00	0.70	0.8	12
21/02/2010 12:15	0.70	0.4	12.25
21/02/2010 12:30	0.70	0.4	12.5
21/02/2010 12:45	0.71	0.4	12.75
21/02/2010 13:00	0.72	0.4	13
21/02/2010 13:15	0.72	0	13.25
21/02/2010 13:30	0.74	0	13.5
21/02/2010 13:45	0.75	0	13.75
21/02/2010 14:00	0.76	0	14
21/02/2010 14:15	0.76	0	14.25
21/02/2010 14:30	0.78	0	14.5
21/02/2010 14:45	0.79	0	14.75
21/02/2010 15:00	0.80	0	15
21/02/2010 15:15	0.83	0	15.25
21/02/2010 15:30	0.85	0	15.5
21/02/2010 15:45	0.89	0	15.75
21/02/2010 16:00	0.93	0	16
21/02/2010 16:15	0.99	0	16.25
21/02/2010 16:30	1.04	0	16.5
21/02/2010 16:45	1.11	0	16.75
21/02/2010 17:00	1.18	0	17
21/02/2010 17:15	1.25	0	17.25
21/02/2010 17:30	1.31	0.2	17.5
21/02/2010 17:45	1.37	0	17.75
21/02/2010 18:00	1.44	0	18
21/02/2010 18:15	1.49	0	18.25
21/02/2010 18:30	1.54	0	18.5
21/02/2010 18:45	1.60	0	18.75
21/02/2010 19:00	1.65	0	19
21/02/2010 19:15	1.71	0	19.25
21/02/2010 19:30	1.76	0	19.5
21/02/2010 19:45	1.80	0	19.75
21/02/2010 20:00	1.84	0	20
21/02/2010 20:15	1.88	0	20.25
21/02/2010 20:30	1.92	0	20.5
21/02/2010 20:45	1.95	0	20.75
21/02/2010 21:00	1.97	0	21
21/02/2010 21:15	1.99	0	21.25
21/02/2010 21:30	2.03	0	21.5
21/02/2010 21:45	2.04	0	21.75
21/02/2010 22:00	2.06	0	22
21/02/2010 22:15	2.07	0	22.25
21/02/2010 22:30	2.09	0	22.5
21/02/2010 22:45	2.10	0	22.75
21/02/2010 23:00	2.12	0	23
21/02/2010 23:15	2.12	0	23.25
21/02/2010 23:30	2.14	0	23.5
21/02/2010 23:45	2.14	0	23.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours
28/02/2010 16:00	0.2	12
28/02/2010 16:15	0.2	12 25
28/02/2010 16:30	0	12.5
28/02/2010 16:45	0	12.75
28/02/2010 17:00	0.2	13
28/02/2010 17:15	0.2	13 25
28/02/2010 17:30	0	13.5
28/02/2010 17:45	0.2	13.75
28/02/2010 18:00	0	14
28/02/2010 18:15	0	14 25
28/02/2010 18:30	0	14.5
28/02/2010 18:45	0	14.75
28/02/2010 19:00	0	15
28/02/2010 19:15	0	15 25
28/02/2010 19:30	0	15.5
28/02/2010 19:45	0	15.75
28/02/2010 20:00	0	16
28/02/2010 20:15	0	16 25
28/02/2010 20:30	0	16.5
28/02/2010 20:45	0	16.75
28/02/2010 21:00	0	17
28/02/2010 21:15	0.2	17 25
28/02/2010 21:30	0	17.5
28/02/2010 21:45	0	17.75
28/02/2010 22:00	0	18
28/02/2010 22:15	0	18 25
28/02/2010 22:30	0	18.5
28/02/2010 22:45	0.2	18.75
Total RF mm	19.6	

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours
22/02/2010 00:00	2.16	0	24
22/02/2010 00:15	2.15	0	24.25
22/02/2010 00:30	2.14	0	24.5
22/02/2010 00:45	2.14	0	24.75
22/02/2010 01:00	2.13	0	25
22/02/2010 01:15	2.12	0	25.25
22/02/2010 01:30	2.11	0	25.5
22/02/2010 01:45	2.09	0	25.75
22/02/2010 02:00	2.08	0	26
22/02/2010 02:15	2.05	0	26.25
22/02/2010 02:30	2.03	0.2	26.5
22/02/2010 02:45	2.01	0.2	26.75
22/02/2010 03:00	2.00	0	27
22/02/2010 03:15	1.97	0.2	27.25
22/02/2010 03:30	1.95	0	27.5
22/02/2010 03:45	1.94	0.2	27.75
22/02/2010 04:00	1.92	0.2	28
22/02/2010 04:15	1.90	0.4	28.25
22/02/2010 04:30	1.88	0	28.5
22/02/2010 04:45	1.86	0.2	28.75
22/02/2010 05:00	1.84	0.4	29
22/02/2010 05:15	1.82	0.2	29.25
22/02/2010 05:30	1.80	0.2	29.5
22/02/2010 05:45	1.78	0.2	29.75
22/02/2010 06:00	1.76	0.2	30
22/02/2010 06:15	1.75	0.4	30.25
22/02/2010 06:30	1.75	0.4	30.5
22/02/2010 06:45	1.72	0.2	30.75
22/02/2010 07:00	1.72	0.2	31
22/02/2010 07:15	1.71	0.4	31.25
22/02/2010 07:30	1.70	0.4	31.5
22/02/2010 07:45	1.71	0.4	31.75
22/02/2010 08:00	1.71	0.8	32
22/02/2010 08:15	1.72	0.8	32.25
22/02/2010 08:30	1.74	0.8	32.5
22/02/2010 08:45	1.76	0.6	32.75
22/02/2010 09:00	1.80	0.6	33
22/02/2010 09:15	1.85	0.4	33.25
22/02/2010 09:30	1.91	0.6	33.5
22/02/2010 09:45	1.97	0.6	33.75
22/02/2010 10:00	2.05	0.4	34
22/02/2010 10:15	2.14	0.2	34.25
22/02/2010 10:30	2.26	0	34.5
22/02/2010 10:45	2.39	0.2	34.75
22/02/2010 11:00	2.57	0	35
22/02/2010 11:15	2.81	0.2	35.25
22/02/2010 11:30	3.04	0.2	35.5
22/02/2010 11:45	3.33	0.4	35.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

Middleton		Benhall TBR RG						**Rainfall Event**	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours	Date & Time	Rainfall (mm)	Duration hours		**start of event**	28/02/2010 04:00
22/02/2010 12:00	3.60	0.2	36						
22/02/2010 12:15	3.95	0	36.25						
22/02/2010 12:30	4.12	0	36.5						
22/02/2010 12:45	4.36	0.2	36.75						
22/02/2010 13:00	4.57	0	37						
22/02/2010 13:15	4.73	0.2	37.25						
22/02/2010 13:30	4.86	0	37.5						
22/02/2010 13:45	5.01	0.2	37.75						
22/02/2010 14:00	5.14	0	38						
22/02/2010 14:15	5.26	0.2	38.25						
22/02/2010 14:30	5.38	0	38.5						
22/02/2010 14:45	5.47	0	38.75						
22/02/2010 15:00	5.55	0	39						
22/02/2010 15:15	5.62	0.2	39.25						
22/02/2010 15:30	5.69	0.4	39.5						
22/02/2010 15:45	5.76	0.2	39.75						
22/02/2010 16:00	5.83	0.2	40						
22/02/2010 16:15	5.88	0.2	40.25						
22/02/2010 16:30	5.94	0	40.5						
22/02/2010 16:45	5.97	0	40.75						
22/02/2010 17:00	6.02	0.2	41						
22/02/2010 17:15	6.06	0	41.25						
22/02/2010 17:30	6.10	0	41.5						
22/02/2010 17:45	6.12	0.2	41.75						
22/02/2010 18:00	6.17	0	42						
22/02/2010 18:15	6.24	0	42.25						
22/02/2010 18:30	6.27	0	42.5						
22/02/2010 18:45	6.32	0	42.75						
22/02/2010 19:00	6.37	0	43						
22/02/2010 19:15	6.45	0	43.25						
22/02/2010 19:30	6.51	0	43.5						
22/02/2010 19:45	6.58	0	43.75						
22/02/2010 20:00	6.63	0	44						
22/02/2010 20:15	6.67	0	44.25						
22/02/2010 20:30	6.73	0	44.5						
22/02/2010 20:45	6.79	0	44.75						
22/02/2010 21:00	6.82	0	45						
22/02/2010 21:15	6.88	0	45.25						
22/02/2010 21:30	6.94	0	45.5						
22/02/2010 21:45	7.00	0	45.75						
22/02/2010 22:00	7.06	0	46						
22/02/2010 22:15	7.09	0	46.25						
22/02/2010 22:30	7.13	0	46.5						
22/02/2010 22:45	7.18	0	46.75						
22/02/2010 23:00	7.20	0	47						
22/02/2010 23:15	7.25	0	47.25						
22/02/2010 23:30	7.28	0	47.5						
22/02/2010 23:45	7.31	0	47.75						

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
23/02/2010 00:00	7.31	0	48					
23/02/2010 00:15	7.35	0	48.25					
23/02/2010 00:30	7.37	0	48.5					
23/02/2010 00:45	7.37	0	48.75					
23/02/2010 01:00	7.37	0	49					
23/02/2010 01:15	7.35	0	49.25					
23/02/2010 01:30	7.36	0	49.5					
23/02/2010 01:45	7.34	0	49.75					
23/02/2010 02:00	7.31	0	50					
23/02/2010 02:15	7.29	0	50.25					
23/02/2010 02:30	7.24	0	50.5					
23/02/2010 02:45	7.21	0	50.75					
23/02/2010 03:00	7.16	0	51					
23/02/2010 03:15	7.13	0	51.25					
23/02/2010 03:30	7.07	0	51.5					
23/02/2010 03:45	7.00	0	51.75					
23/02/2010 04:00	6.95	0	52					
23/02/2010 04:15	6.89	0	52.25					
23/02/2010 04:30	6.80	0	52.5					
23/02/2010 04:45	6.72	0	52.75					
23/02/2010 05:00	6.66	0	53					
23/02/2010 05:15	6.56	0	53.25					
23/02/2010 05:30	6.47	0	53.5					
23/02/2010 05:45	6.36	0	53.75					
23/02/2010 06:00	6.28	0	54					
23/02/2010 06:15	6.19	0	54.25					
23/02/2010 06:30	6.10	0	54.5					
23/02/2010 06:45	5.99	0	54.75					
23/02/2010 07:00	5.89	0	55					
23/02/2010 07:15	5.77	0	55.25					
23/02/2010 07:30	5.63	0	55.5					
23/02/2010 07:45	5.49	0	55.75					
23/02/2010 08:00	5.34	0	56					
23/02/2010 08:15	5.18	0	56.25					
23/02/2010 08:30	5.02	0	56.5					
23/02/2010 08:45	4.83	0	56.75					
23/02/2010 09:00	4.69	0	57		5.8			
23/02/2010 09:15	4.51	0	57.25					
23/02/2010 09:30	4.31	0	57.5					
23/02/2010 09:45	4.11	0	57.75					
23/02/2010 10:00	3.93	0	58					
23/02/2010 10:15	3.73	0	58.25					
23/02/2010 10:30	3.52	0	58.5					
23/02/2010 10:45	3.34	0	58.75					
23/02/2010 11:00	3.13	0	59					
23/02/2010 11:15	2.95	0	59.25					
23/02/2010 11:30	2.75	0	59.5					
23/02/2010 11:45	2.59	0	59.75					

Rainfall Event

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours
23/02/2010 12:00	2.46	0	60
23/02/2010 12:15	2.36	0	60.25
23/02/2010 12:30	2.27	0	60.5
23/02/2010 12:45	2.22	0	60.75
23/02/2010 13:00	2.15	0	61
23/02/2010 13:15	2.10	0	61.25
23/02/2010 13:30	2.06	0	61.5
23/02/2010 13:45	2.03	0	61.75
23/02/2010 14:00	1.99	0	62
23/02/2010 14:15	1.95	0	62.25
23/02/2010 14:30	1.93	0	62.5
23/02/2010 14:45	1.89	0	62.75
23/02/2010 15:00	1.87	0	63
23/02/2010 15:15	1.84	0	63.25
23/02/2010 15:30	1.81	0	63.5
23/02/2010 15:45	1.79	0	63.75
23/02/2010 16:00	1.77	0	64
23/02/2010 16:15	1.75	0.2	64.25
23/02/2010 16:30	1.73	0.2	64.5
23/02/2010 16:45	1.69	0	64.75
23/02/2010 17:00	1.68	0.2	65
23/02/2010 17:15	1.68	0.2	65.25
23/02/2010 17:30	1.64	0.2	65.5
23/02/2010 17:45	1.63	0.2	65.75
23/02/2010 18:00	1.62	0.2	66
23/02/2010 18:15	1.60	0	66.25
23/02/2010 18:30	1.59	0	66.5
23/02/2010 18:45	1.57	0	66.75
23/02/2010 19:00	1.56	0.2	67
23/02/2010 19:15	1.55	0	67.25
23/02/2010 19:30	1.53	0	67.5
23/02/2010 19:45	1.53	0	67.75
23/02/2010 20:00	1.52	0	68
23/02/2010 20:15	1.51	0.2	68.25
23/02/2010 20:30	1.49	0	68.5
23/02/2010 20:45	1.49	0	68.75
23/02/2010 21:00	1.48	0	69
23/02/2010 21:15	1.48	0	69.25
23/02/2010 21:30	1.47	0.2	69.5
23/02/2010 21:45	1.46	0	69.75
23/02/2010 22:00	1.46	0	70
23/02/2010 22:15	1.44	0	70.25
23/02/2010 22:30	1.44	0	70.5
23/02/2010 22:45	1.44	0	70.75
23/02/2010 23:00	1.44	0	71
23/02/2010 23:15	1.43	0	71.25
23/02/2010 23:30	1.43	0	71.5
23/02/2010 23:45	1.42	0	71.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
24/02/2010 00:00	1.42	0	72					
24/02/2010 00:15	1.41	0	72.25					
24/02/2010 00:30	1.41	0	72.5					
24/02/2010 00:45	1.41	0	72.75					
24/02/2010 01:00	1.40	0.2	73					
24/02/2010 01:15	1.40	0	73.25					
24/02/2010 01:30	1.39	0	73.5					
24/02/2010 01:45	1.40	0	73.75					
24/02/2010 02:00	1.39	0	74					
24/02/2010 02:15	1.39	0	74.25					
24/02/2010 02:30	1.39	0	74.5					
24/02/2010 02:45	1.39	0	74.75					
24/02/2010 03:00	1.40	0	75					
24/02/2010 03:15	1.39	0	75.25					
24/02/2010 03:30	1.40	0	75.5					
24/02/2010 03:45	1.39	0	75.75					
24/02/2010 04:00	1.39	0	76					
24/02/2010 04:15	1.39	0.2	76.25					
24/02/2010 04:30	1.39	0	76.5					
24/02/2010 04:45	1.39	0	76.75					
24/02/2010 05:00	1.39	0	77					
24/02/2010 05:15	1.39	0	77.25					
24/02/2010 05:30	1.39	0	77.5					
24/02/2010 05:45	1.39	0	77.75					
24/02/2010 06:00	1.39	0	78					
24/02/2010 06:15	1.39	0	78.25					
24/02/2010 06:30	1.39	0	78.5					
24/02/2010 06:45	1.39	0	78.75					
24/02/2010 07:00	1.39	0	79					
24/02/2010 07:15	1.39	0	79.25					
24/02/2010 07:30	1.39	0	79.5					
24/02/2010 07:45	1.39	0	79.75					
24/02/2010 08:00	1.39	0	80					
24/02/2010 08:15	1.39	0	80.25					
24/02/2010 08:30	1.39	0	80.5					
24/02/2010 08:45	1.39	0	80.75					
24/02/2010 09:00	1.39	0	81		2.4			
24/02/2010 09:15	1.39	0	81.25					
24/02/2010 09:30	1.39	0	81.5					
24/02/2010 09:45	1.38	0	81.75					
24/02/2010 10:00	1.39	0	82					
24/02/2010 10:15	1.38	0	82.25					
24/02/2010 10:30	1.37	0	82.5					
24/02/2010 10:45	1.37	0	82.75					
24/02/2010 11:00	1.37	0	83					
24/02/2010 11:15	1.37	0	83.25					
24/02/2010 11:30	1.36	0	83.5					
24/02/2010 11:45	1.36	0	83.75					

Rainfall Event

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours
24/02/2010 12:00	1.36	0	84
24/02/2010 12:15	1.36	0	84.25
24/02/2010 12:30	1.35	0	84.5
24/02/2010 12:45	1.35	0.2	84.75
24/02/2010 13:00	1.35	0	85
24/02/2010 13:15	1.34	0	85.25
24/02/2010 13:30	1.33	0	85.5
24/02/2010 13:45	1.33	0	85.75
24/02/2010 14:00	1.33	0	86
24/02/2010 14:15	1.32	0	86.25
24/02/2010 14:30	1.32	0	86.5
24/02/2010 14:45	1.32	0	86.75
24/02/2010 15:00	1.32	0	87
24/02/2010 15:15	1.32	0	87.25
24/02/2010 15:30	1.32	0	87.5
24/02/2010 15:45	1.31	0	87.75
24/02/2010 16:00	1.30	0	88
24/02/2010 16:15	1.30	0	88.25
24/02/2010 16:30	1.29	0	88.5
24/02/2010 16:45	1.29	0	88.75
24/02/2010 17:00	1.28	0	89
24/02/2010 17:15	1.28	0	89.25
24/02/2010 17:30	1.28	0	89.5
24/02/2010 17:45	1.28	0	89.75
24/02/2010 18:00	1.27	0	90
24/02/2010 18:15	1.27	0	90.25
24/02/2010 18:30	1.26	0	90.5
24/02/2010 18:45	1.26	0	90.75
24/02/2010 19:00	1.26	0	91
24/02/2010 19:15	1.25	0	91.25
24/02/2010 19:30	1.25	0	91.5
24/02/2010 19:45	1.25	0	91.75
24/02/2010 20:00	1.25	0	92
24/02/2010 20:15	1.24	0	92.25
24/02/2010 20:30	1.24	0	92.5
24/02/2010 20:45	1.24	0	92.75
24/02/2010 21:00	1.23	0	93
24/02/2010 21:15	1.23	0	93.25
24/02/2010 21:30	1.22	0	93.5
24/02/2010 21:45	1.22	0.2	93.75
24/02/2010 22:00	1.21	0	94
24/02/2010 22:15	1.22	0	94.25
24/02/2010 22:30	1.20	0	94.5
24/02/2010 22:45	1.20	0	94.75
24/02/2010 23:00	1.19	0	95
24/02/2010 23:15	1.19	0.2	95.25
24/02/2010 23:30	1.19	0	95.5
24/02/2010 23:45	1.19	0.2	95.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
25/02/2010 00:00	1.19	0	96					
25/02/2010 00:15	1.18	0	96.25					
25/02/2010 00:30	1.17	0	96.5					
25/02/2010 00:45	1.17	0	96.75					
25/02/2010 01:00	1.16	0	97					
25/02/2010 01:15	1.16	0	97.25					
25/02/2010 01:30	1.16	0	97.5					
25/02/2010 01:45	1.16	0	97.75					
25/02/2010 02:00	1.16	0	98					
25/02/2010 02:15	1.15	0	98.25					
25/02/2010 02:30	1.15	0.2	98.5					
25/02/2010 02:45	1.14	0	98.75					
25/02/2010 03:00	1.14	0	99					
25/02/2010 03:15	1.14	0	99.25					
25/02/2010 03:30	1.13	0	99.5					
25/02/2010 03:45	1.13	0	99.75					
25/02/2010 04:00	1.13	0	100					
25/02/2010 04:15	1.12	0	100.25					
25/02/2010 04:30	1.12	0	100.5					
25/02/2010 04:45	1.11	0	100.75					
25/02/2010 05:00	1.11	0	101					
25/02/2010 05:15	1.11	0	101.25					
25/02/2010 05:30	1.11	0	101.5					
25/02/2010 05:45	1.10	0	101.75					
25/02/2010 06:00	1.10	0	102					
25/02/2010 06:15	1.10	0	102.25					
25/02/2010 06:30	1.09	0	102.5					
25/02/2010 06:45	1.09	0	102.75					
25/02/2010 07:00	1.08	0	103					
25/02/2010 07:15	1.08	0	103.25					
25/02/2010 07:30	1.08	0	103.5					
25/02/2010 07:45	1.07	0	103.75					
25/02/2010 08:00	1.07	0	104					
25/02/2010 08:15	1.07	0	104.25					
25/02/2010 08:30	1.06	0	104.5					
25/02/2010 08:45	1.06	0	104.75					
25/02/2010 09:00	1.06	0	105		1			
25/02/2010 09:15	1.05	0	105.25					
25/02/2010 09:30	1.04	0	105.5					
25/02/2010 09:45	1.04	0	105.75					
25/02/2010 10:00	1.03	0	106					
25/02/2010 10:15	1.03	0	106.25					
25/02/2010 10:30	1.03	0	106.5					
25/02/2010 10:45	1.03	0	106.75					
25/02/2010 11:00	1.01	0	107					
25/02/2010 11:15	1.02	0	107.25					
25/02/2010 11:30	1.01	0	107.5					
25/02/2010 11:45	1.01	0	107.75					

Rainfall Event

start of event	28/02/2010 04:00

Middleton		Benhall TBR RG			Rainfall Event			
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours	Date & Time	Rainfall (mm)	Duration hours	**start of event**	28/02/2010 04:00
25/02/2010 12:00	1.00	0	108					
25/02/2010 12:15	1.00	0	108.25					
25/02/2010 12:30	1.00	0	108.5					
25/02/2010 12:45	0.99	0	108.75					
25/02/2010 13:00	0.99	0	109					
25/02/2010 13:15	0.99	0	109.25					
25/02/2010 13:30	0.98	0	109.5					
25/02/2010 13:45	0.98	0	109.75					
25/02/2010 14:00	0.98	0	110					
25/02/2010 14:15	0.97	0	110.25					
25/02/2010 14:30	0.97	0	110.5					
25/02/2010 14:45	0.97	0	110.75					
25/02/2010 15:00	0.97	0	111					
25/02/2010 15:15	0.96	0	111.25					
25/02/2010 15:30	0.96	0	111.5					
25/02/2010 15:45	0.96	0	111.75					
25/02/2010 16:00	0.95	0	112					
25/02/2010 16:15	0.95	0	112.25					
25/02/2010 16:30	0.95	0	112.5					
25/02/2010 16:45	0.95	0	112.75					
25/02/2010 17:00	0.94	0.4	113					
25/02/2010 17:15	0.94	0.2	113.25					
25/02/2010 17:30	0.94	0.2	113.5					
25/02/2010 17:45	0.94	0.4	113.75					
25/02/2010 18:00	0.94	0.4	114					
25/02/2010 18:15	0.94	0.2	114.25					
25/02/2010 18:30	0.94	0.2	114.5					
25/02/2010 18:45	0.94	0.2	114.75					
25/02/2010 19:00	0.95	0.4	115					
25/02/2010 19:15	0.95	0.6	115.25					
25/02/2010 19:30	0.95	0.8	115.5					
25/02/2010 19:45	0.96	0	115.75					
25/02/2010 20:00	0.97	0.2	116					
25/02/2010 20:15	0.97	0.2	116.25					
25/02/2010 20:30	0.98	1.2	116.5					
25/02/2010 20:45	0.99	1.2	116.75					
25/02/2010 21:00	1.01	0.4	117					
25/02/2010 21:15	1.02	0.6	117.25					
25/02/2010 21:30	1.05	0.6	117.5					
25/02/2010 21:45	1.08	0.4	117.75					
25/02/2010 22:00	1.11	0	118					
25/02/2010 22:15	1.16	0	118.25					
25/02/2010 22:30	1.22	0.2	118.5					
25/02/2010 22:45	1.29	0.2	118.75					
25/02/2010 23:00	1.38	0	119					
25/02/2010 23:15	1.48	0	119.25					
25/02/2010 23:30	1.57	0	119.5					
25/02/2010 23:45	1.68	0	119.75					

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
26/02/2010 00:00	1.79	0	120					
26/02/2010 00:15	1.88	0	120.25					
26/02/2010 00:30	1.99	0	120.5					
26/02/2010 00:45	2.07	0	120.75					
26/02/2010 01:00	2.16	0	121					
26/02/2010 01:15	2.23	0	121.25					
26/02/2010 01:30	2.31	0	121.5					
26/02/2010 01:45	2.39	0	121.75					
26/02/2010 02:00	2.47	0	122					
26/02/2010 02:15	2.58	0	122.25					
26/02/2010 02:30	2.68	0	122.5					
26/02/2010 02:45	2.80	0	122.75					
26/02/2010 03:00	2.92	0	123					
26/02/2010 03:15	3.05	0	123.25					
26/02/2010 03:30	3.17	0	123.5					
26/02/2010 03:45	3.28	0	123.75					
26/02/2010 04:00	3.39	0	124					
26/02/2010 04:15	3.48	0	124.25					
26/02/2010 04:30	3.55	0	124.5					
26/02/2010 04:45	3.64	0	124.75					
26/02/2010 05:00	3.70	0	125					
26/02/2010 05:15	3.76	0	125.25					
26/02/2010 05:30	3.81	0	125.5					
26/02/2010 05:45	3.87	0	125.75					
26/02/2010 06:00	3.93	0	126					
26/02/2010 06:15	3.99	0	126.25					
26/02/2010 06:30	4.06	0	126.5					
26/02/2010 06:45	4.11	0	126.75					
26/02/2010 07:00	4.19	0	127					
26/02/2010 07:15	4.24	0	127.25					
26/02/2010 07:30	4.29	0	127.5					
26/02/2010 07:45	4.35	0	127.75					
26/02/2010 08:00	4.38	0	128					
26/02/2010 08:15	4.43	0	128.25					
26/02/2010 08:30	4.47	0	128.5					
26/02/2010 08:45	4.49	0.2	128.75					
26/02/2010 09:00	4.51	0	129		9.4			
26/02/2010 09:15	4.52	0	129.25					
26/02/2010 09:30	4.51	0.2	129.5					
26/02/2010 09:45	4.49	0	129.75					
26/02/2010 10:00	4.46	0	130					
26/02/2010 10:15	4.42	0	130.25					
26/02/2010 10:30	4.37	0	130.5					
26/02/2010 10:45	4.31	0	130.75					
26/02/2010 11:00	4.24	0	131					
26/02/2010 11:15	4.15	0	131.25					
26/02/2010 11:30	4.06	0	131.5					
26/02/2010 11:45	3.96	0	131.75					

Rainfall Event

start of event	28/02/2010 04:00

Middleton		Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)		Hours
26/02/2010 12:00	3.85	0		132
26/02/2010 12:15	3.73	0		132.25
26/02/2010 12:30	3.59	0		132.5
26/02/2010 12:45	3.48	0		132.75
26/02/2010 13:00	3.34	0		133
26/02/2010 13:15	3.18	0		133.25
26/02/2010 13:30	3.03	0		133.5
26/02/2010 13:45	2.88	0		133.75
26/02/2010 14:00	2.74	0		134
26/02/2010 14:15	2.61	0		134.25
26/02/2010 14:30	2.50	0		134.5
26/02/2010 14:45	2.41	0		134.75
26/02/2010 15:00	2.33	0		135
26/02/2010 15:15	2.27	0		135.25
26/02/2010 15:30	2.23	0		135.5
26/02/2010 15:45	2.19	0		135.75
26/02/2010 16:00	2.13	0		136
26/02/2010 16:15	2.10	0		136.25
26/02/2010 16:30	2.07	0		136.5
26/02/2010 16:45	2.03	0		136.75
26/02/2010 17:00	2.01	0		137
26/02/2010 17:15	1.97	0		137.25
26/02/2010 17:30	1.95	0		137.5
26/02/2010 17:45	1.92	0		137.75
26/02/2010 18:00	1.90	0		138
26/02/2010 18:15	1.87	0		138.25
26/02/2010 18:30	1.85	0		138.5
26/02/2010 18:45	1.81	0		138.75
26/02/2010 19:00	1.79	0		139
26/02/2010 19:15	1.78	0		139.25
26/02/2010 19:30	1.75	0		139.5
26/02/2010 19:45	1.73	0		139.75
26/02/2010 20:00	1.71	0		140
26/02/2010 20:15	1.68	0		140.25
26/02/2010 20:30	1.67	0		140.5
26/02/2010 20:45	1.65	0		140.75
26/02/2010 21:00	1.63	0		141
26/02/2010 21:15	1.61	0		141.25
26/02/2010 21:30	1.58	0		141.5
26/02/2010 21:45	1.57	0		141.75
26/02/2010 22:00	1.55	0		142
26/02/2010 22:15	1.53	0		142.25
26/02/2010 22:30	1.52	0		142.5
26/02/2010 22:45	1.51	0		142.75
26/02/2010 23:00	1.49	0		143
26/02/2010 23:15	1.48	0		143.25
26/02/2010 23:30	1.46	0		143.5
26/02/2010 23:45	1.45	0		143.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
27/02/2010 00:00	1.44	0	144					
27/02/2010 00:15	1.42	0	144.25					
27/02/2010 00:30	1.40	0	144.5					
27/02/2010 00:45	1.39	0	144.75					
27/02/2010 01:00	1.38	0	145					
27/02/2010 01:15	1.37	0	145.25					
27/02/2010 01:30	1.36	0	145.5					
27/02/2010 01:45	1.35	0	145.75					
27/02/2010 02:00	1.34	0	146					
27/02/2010 02:15	1.32	0	146.25					
27/02/2010 02:30	1.32	0	146.5					
27/02/2010 02:45	1.30	0	146.75					
27/02/2010 03:00	1.29	0	147					
27/02/2010 03:15	1.28	0	147.25					
27/02/2010 03:30	1.27	0	147.5					
27/02/2010 03:45	1.26	0	147.75					
27/02/2010 04:00	1.25	0	148					
27/02/2010 04:15	1.25	0	148.25					
27/02/2010 04:30	1.24	0	148.5					
27/02/2010 04:45	1.22	0.2	148.75					
27/02/2010 05:00	1.22	0	149					
27/02/2010 05:15	1.21	0	149.25					
27/02/2010 05:30	1.20	0	149.5					
27/02/2010 05:45	1.19	0	149.75					
27/02/2010 06:00	1.18	0.4	150					
27/02/2010 06:15	1.18	0.2	150.25					
27/02/2010 06:30	1.17	0.6	150.5					
27/02/2010 06:45	1.16	0.2	150.75					
27/02/2010 07:00	1.16	0	151					
27/02/2010 07:15	1.15	0.2	151.25					
27/02/2010 07:30	1.15	0.4	151.5					
27/02/2010 07:45	1.15	0.2	151.75					
27/02/2010 08:00	1.14	0.2	152					
27/02/2010 08:15	1.14	0	152.25					
27/02/2010 08:30	1.13	0	152.5					
27/02/2010 08:45	1.13	0.2	152.75					
27/02/2010 09:00	1.13	0	153		3			
27/02/2010 09:15	1.12	0	153.25					
27/02/2010 09:30	1.12	0	153.5					
27/02/2010 09:45	1.12	0	153.75					
27/02/2010 10:00	1.12	0	154					
27/02/2010 10:15	1.11	0	154.25					
27/02/2010 10:30	1.11	0	154.5					
27/02/2010 10:45	1.11	0	154.75					
27/02/2010 11:00	1.11	0	155					
27/02/2010 11:15	1.11	0	155.25					
27/02/2010 11:30	1.11	0	155.5					
27/02/2010 11:45	1.10	0	155.75					

Rainfall Event

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours	
27/02/2010 12:00	1.10	0	156	
27/02/2010 12:15	1.10	0	156.25	
27/02/2010 12:30	1.09	0	156.5	
27/02/2010 12:45	1.09	0	156.75	
27/02/2010 13:00	1.09	0	157	
27/02/2010 13:15	1.10	0	157.25	
27/02/2010 13:30	1.09	0	157.5	
27/02/2010 13:45	1.09	0	157.75	
27/02/2010 14:00	1.09	0	158	
27/02/2010 14:15	1.09	0	158.25	
27/02/2010 14:30	1.09	0	158.5	
27/02/2010 14:45	1.09	0	158.75	
27/02/2010 15:00	1.09	0	159	
27/02/2010 15:15	1.09	0	159.25	
27/02/2010 15:30	1.09	0	159.5	
27/02/2010 15:45	1.09	0	159.75	
27/02/2010 16:00	1.08	0	160	
27/02/2010 16:15	1.08	0	160.25	
27/02/2010 16:30	1.08	0	160.5	
27/02/2010 16:45	1.08	0	160.75	
27/02/2010 17:00	1.09	0	161	
27/02/2010 17:15	1.08	0	161.25	
27/02/2010 17:30	1.08	0	161.5	
27/02/2010 17:45	1.08	0	161.75	
27/02/2010 18:00	1.08	0	162	
27/02/2010 18:15	1.08	0	162.25	
27/02/2010 18:30	1.08	0	162.5	
27/02/2010 18:45	1.08	0	162.75	
27/02/2010 19:00	1.08	0	163	
27/02/2010 19:15	1.08	0	163.25	
27/02/2010 19:30	1.08	0	163.5	
27/02/2010 19:45	1.08	0	163.75	
27/02/2010 20:00	1.08	0	164	
27/02/2010 20:15	1.08	0	164.25	
27/02/2010 20:30	1.08	0	164.5	
27/02/2010 20:45	1.08	0	164.75	
27/02/2010 21:00	1.07	0	165	
27/02/2010 21:15	1.07	0	165.25	
27/02/2010 21:30	1.07	0	165.5	
27/02/2010 21:45	1.07	0	165.75	
27/02/2010 22:00	1.06	0	166	
27/02/2010 22:15	1.06	0	166.25	
27/02/2010 22:30	1.06	0	166.5	
27/02/2010 22:45	1.06	0	166.75	
27/02/2010 23:00	1.06	0	167	
27/02/2010 23:15	1.06	0	167.25	
27/02/2010 23:30	1.06	0	167.5	
27/02/2010 23:45	1.06	0	167.75	

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
28/02/2010 00:00	1.06	0	168					
28/02/2010 00:15	1.05	0	168.25					
28/02/2010 00:30	1.05	0	168.5					
28/02/2010 00:45	1.05	0	168.75					
28/02/2010 01:00	1.04	0	169					
28/02/2010 01:15	1.04	0	169.25					
28/02/2010 01:30	1.04	0	169.5					
28/02/2010 01:45	1.03	0	169.75					
28/02/2010 02:00	1.03	0	170					
28/02/2010 02:15	1.03	0	170.25					
28/02/2010 02:30	1.03	0	170.5					
28/02/2010 02:45	1.03	0	170.75					
28/02/2010 03:00	1.03	0	171					
28/02/2010 03:15	1.03	0	171.25					
28/02/2010 03:30	1.02	0	171.5					
28/02/2010 03:45	1.02	0	171.75					
28/02/2010 04:00	1.02	0.2	172					
28/02/2010 04:15	1.01	0	172.25					
28/02/2010 04:30	1.01	0	172.5					
28/02/2010 04:45	1.01	0.2	172.75					
28/02/2010 05:00	1.01	0.2	173					
28/02/2010 05:15	1.01	0.2	173.25					
28/02/2010 05:30	1.01	0.2	173.5					
28/02/2010 05:45	1.00	0.6	173.75					
28/02/2010 06:00	1.01	0.4	174					
28/02/2010 06:15	1.01	0.6	174.25					
28/02/2010 06:30	1.01	0.2	174.5					
28/02/2010 06:45	1.01	0.2	174.75					
28/02/2010 07:00	1.01	0.4	175					
28/02/2010 07:15	1.01	0.4	175.25					
28/02/2010 07:30	1.01	0.2	175.5					
28/02/2010 07:45	1.03	0.8	175.75					
28/02/2010 08:00	1.03	1	176					
28/02/2010 08:15	1.04	0.4	176.25					
28/02/2010 08:30	1.06	0.6	176.5					
28/02/2010 08:45	1.08	0.6	176.75					
28/02/2010 09:00	1.09	0.6	177		8			
28/02/2010 09:15	1.12	0.6	177.25					
28/02/2010 09:30	1.15	1	177.5					
28/02/2010 09:45	1.19	0.8	177.75					
28/02/2010 10:00	1.26	0.6	178					
28/02/2010 10:15	1.36	0.6	178.25					
28/02/2010 10:30	1.42	0.8	178.5					
28/02/2010 10:45	1.53	0.6	178.75					
28/02/2010 11:00	1.65	0.4	179					
28/02/2010 11:15	1.79	0.4	179.25					
28/02/2010 11:30	1.93	0.4	179.5					
28/02/2010 11:45	2.09	0.4	179.75					

Rainfall Event

start of event	28/02/2010 04:00

Middleton		Benhall TBR RG			Rainfall Event			
Date & Time	Flow (m^3/s)	Rainfall (mm)		Hours	Date & Time	Rainfall (mm)	Duration hours	**start of event**	28/02/2010 04:00
28/02/2010 12:00	2.25	0.4		180				
28/02/2010 12:15	2.44	0.2		180.25				
28/02/2010 12:30	2.69	0.4		180.5				
28/02/2010 12:45	3.03	0.6		180.75				
28/02/2010 13:00	3.42	0.6		181				
28/02/2010 13:15	3.68	0.4		181.25				
28/02/2010 13:30	4.16	0.4		181.5				
28/02/2010 13:45	4.51	0		181.75				
28/02/2010 14:00	4.75	0.2		182				
28/02/2010 14:15	4.97	0		182.25				
28/02/2010 14:30	5.19	0		182.5				
28/02/2010 14:45	5.40	0		182.75				
28/02/2010 15:00	5.57	0.2		183				
28/02/2010 15:15	5.72	0		183.25				
28/02/2010 15:30	5.87	0.2		183.5				
28/02/2010 15:45	6.00	0		183.75				
28/02/2010 16:00	6.10	0.2		184				
28/02/2010 16:15	6.18	0.2		184.25				
28/02/2010 16:30	6.25	0		184.5				
28/02/2010 16:45	6.33	0		184.75				
28/02/2010 17:00	6.40	0.2		185				
28/02/2010 17:15	6.45	0.2		185.25				
28/02/2010 17:30	6.51	0		185.5				
28/02/2010 17:45	6.58	0.2		185.75				
28/02/2010 18:00	6.66	0		186				
28/02/2010 18:15	6.76	0		186.25				
28/02/2010 18:30	6.86	0		186.5				
28/02/2010 18:45	6.94	0		186.75				
28/02/2010 19:00	7.04	0		187				
28/02/2010 19:15	7.14	0		187.25				
28/02/2010 19:30	7.23	0		187.5				
28/02/2010 19:45	7.35	0		187.75				
28/02/2010 20:00	7.44	0		188				
28/02/2010 20:15	7.55	0		188.25				
28/02/2010 20:30	7.65	0		188.5				
28/02/2010 20:45	7.75	0		188.75				
28/02/2010 21:00	7.83	0		189				
28/02/2010 21:15	7.97	0.2		189.25				
28/02/2010 21:30	8.02	0		189.5				
28/02/2010 21:45	8.15	0		189.75				
28/02/2010 22:00	8.24	0		190				
28/02/2010 22:15	8.34	0		190.25				
28/02/2010 22:30	8.40	0		190.5				
28/02/2010 22:45	8.46	0.2		190.75				
28/02/2010 23:00	8.54	0		191				
28/02/2010 23:15	8.62	0		191.25				
28/02/2010 23:30	8.65	0		191.5				
28/02/2010 23:45	8.68	0		191.75				

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)		Hours
01/03/2010 00:00	8.75	0		192
01/03/2010 00:15	8.80	0		192.25
01/03/2010 00:30	8.80	0		192.5
01/03/2010 00:45	8.83	0		192.75
01/03/2010 01:00	8.87	0		193
01/03/2010 01:15	8.88	0		193.25
01/03/2010 01:30	8.90	0		193.5
01/03/2010 01:45	8.95	0		193.75
01/03/2010 02:00	8.97	0		194
01/03/2010 02:15	8.99	0		194.25
01/03/2010 02:30	9.01	0		194.5
01/03/2010 02:45	9.04	0		194.75
01/03/2010 03:00	9.02	0		195
01/03/2010 03:15	9.04	0		195.25
01/03/2010 03:30	9.04	0		195.5
01/03/2010 03:45	9.02	0		195.75
01/03/2010 04:00	9.02	0		196
01/03/2010 04:15	9.01	0		196.25
01/03/2010 04:30	8.95	0		196.5
01/03/2010 04:45	8.94	0		196.75
01/03/2010 05:00	8.87	0		197
01/03/2010 05:15	8.82	0		197.25
01/03/2010 05:30	8.75	0		197.5
01/03/2010 05:45	8.68	0		197.75
01/03/2010 06:00	8.60	0		198
01/03/2010 06:15	8.51	0		198.25
01/03/2010 06:30	8.43	0		198.5
01/03/2010 06:45	8.33	0		198.75
01/03/2010 07:00	8.19	0		199
01/03/2010 07:15	8.06	0		199.25
01/03/2010 07:30	7.94	0		199.5
01/03/2010 07:45	7.82	0		199.75
01/03/2010 08:00	7.66	0		200
01/03/2010 08:15	7.51	0		200.25
01/03/2010 08:30	7.35	0		200.5
01/03/2010 08:45	7.22	0		200.75
01/03/2010 09:00	7.07	0		201
01/03/2010 09:15	6.93	0		201.25
01/03/2010 09:30	6.78	0		201.5
01/03/2010 09:45	6.62	0		201.75
01/03/2010 10:00	6.47	0		202
01/03/2010 10:15	6.32	0		202.25
01/03/2010 10:30	6.20	0		202.5
01/03/2010 10:45	6.04	0		202.75
01/03/2010 11:00	5.87	0		203
01/03/2010 11:15	5.72	0		203.25
01/03/2010 11:30	5.55	0		203.5
01/03/2010 11:45	5.38	0		203.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
01/03/2010 12:00	5.19	0	204					
01/03/2010 12:15	5.00	0	204.25					
01/03/2010 12:30	4.77	0	204.5					
01/03/2010 12:45	4.67	0	204.75					
01/03/2010 13:00	4.49	0	205					
01/03/2010 13:15	4.29	0	205.25					
01/03/2010 13:30	4.10	0	205.5					
01/03/2010 13:45	3.91	0	205.75					
01/03/2010 14:00	3.71	0	206					
01/03/2010 14:15	3.51	0	206.25					
01/03/2010 14:30	3.33	0	206.5					
01/03/2010 14:45	3.15	0	206.75					
01/03/2010 15:00	2.95	0	207					
01/03/2010 15:15	2.79	0	207.25					
01/03/2010 15:30	2.65	0	207.5					
01/03/2010 15:45	2.52	0	207.75					
01/03/2010 16:00	2.42	0	208					
01/03/2010 16:15	2.33	0	208.25					
01/03/2010 16:30	2.27	0	208.5					
01/03/2010 16:45	2.21	0	208.75					
01/03/2010 17:00	2.16	0	209					
01/03/2010 17:15	2.12	0	209.25					
01/03/2010 17:30	2.09	0	209.5					
01/03/2010 17:45	2.04	0	209.75					
01/03/2010 18:00	2.02	0	210					
01/03/2010 18:15	1.98	0	210.25					
01/03/2010 18:30	1.95	0	210.5					
01/03/2010 18:45	1.92	0	210.75					
01/03/2010 19:00	1.90	0	211					
01/03/2010 19:15	1.86	0	211.25					
01/03/2010 19:30	1.83	0	211.5					
01/03/2010 19:45	1.80	0	211.75					
01/03/2010 20:00	1.77	0	212					
01/03/2010 20:15	1.75	0	212.25					
01/03/2010 20:30	1.74	0	212.5					
01/03/2010 20:45	1.71	0	212.75					
01/03/2010 21:00	1.68	0	213					
01/03/2010 21:15	1.66	0	213.25					
01/03/2010 21:30	1.64	0	213.5					
01/03/2010 21:45	1.63	0	213.75					
01/03/2010 22:00	1.60	0	214					
01/03/2010 22:15	1.59	0	214.25					
01/03/2010 22:30	1.58	0	214.5					
01/03/2010 22:45	1.55	0	214.75					
01/03/2010 23:00	1.54	0	215					
01/03/2010 23:15	1.53	0	215.25					
01/03/2010 23:30	1.51	0	215.5					
01/03/2010 23:45	1.49	0	215.75					

Rainfall Event

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours	Date & Time	Rainfall (mm)	Duration hours	**Rainfall Event**	
02/03/2010 00:00	1.48	0	216				**start of event**	28/02/2010 04:00
02/03/2010 00:15	1.47	0	216.25					
02/03/2010 00:30	1.45	0	216.5					
02/03/2010 00:45	1.44	0	216.75					
02/03/2010 01:00	1.43	0	217					
02/03/2010 01:15	1.41	0	217.25					
02/03/2010 01:30	1.39	0	217.5					
02/03/2010 01:45	1.38	0	217.75					
02/03/2010 02:00	1.38	0	218					
02/03/2010 02:15	1.36	0	218.25					
02/03/2010 02:30	1.35	0	218.5					
02/03/2010 02:45	1.34	0	218.75					
02/03/2010 03:00	1.33	0	219					
02/03/2010 03:15	1.32	0	219.25					
02/03/2010 03:30	1.31	0	219.5					
02/03/2010 03:45	1.29	0	219.75					
02/03/2010 04:00	1.28	0	220					
02/03/2010 04:15	1.28	0	220.25					
02/03/2010 04:30	1.27	0	220.5					
02/03/2010 04:45	1.26	0	220.75					
02/03/2010 05:00	1.25	0	221					
02/03/2010 05:15	1.24	0	221.25					
02/03/2010 05:30	1.23	0	221.5					
02/03/2010 05:45	1.22	0	221.75					
02/03/2010 06:00	1.21	0	222					
02/03/2010 06:15	1.20	0	222.25					
02/03/2010 06:30	1.20	0	222.5					
02/03/2010 06:45	1.19	0	222.75					
02/03/2010 07:00	1.18	0	223					
02/03/2010 07:15	1.17	0	223.25					
02/03/2010 07:30	1.16	0	223.5					
02/03/2010 07:45	1.16	0	223.75					
02/03/2010 08:00	1.15	0	224					
02/03/2010 08:15	1.13	0	224.25					
02/03/2010 08:30	1.12	0	224.5					
02/03/2010 08:45	1.12	0.2	224.75					
02/03/2010 09:00	1.11	0	225					
02/03/2010 09:15	1.11	0	225.25					
02/03/2010 09:30	1.10	0	225.5					
02/03/2010 09:45	1.09	0	225.75					
02/03/2010 10:00	1.08	0	226					
02/03/2010 10:15	1.08	0	226.25					
02/03/2010 10:30	1.08	0	226.5					
02/03/2010 10:45	1.07	0	226.75					
02/03/2010 11:00	1.06	0	227					
02/03/2010 11:15	1.06	0	227.25					
02/03/2010 11:30	1.05	0	227.5					
02/03/2010 11:45	1.04	0	227.75					

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)		Hours
02/03/2010 12:00	1.03	0		228
02/03/2010 12:15	1.03	0		228.25
02/03/2010 12:30	1.03	0		228.5
02/03/2010 12:45	1.02	0		228.75
02/03/2010 13:00	1.01	0		229
02/03/2010 13:15	1.01	0		229.25
02/03/2010 13:30	1.00	0		229.5
02/03/2010 13:45	1.00	0		229.75
02/03/2010 14:00	0.99	0		230
02/03/2010 14:15	0.99	0		230.25
02/03/2010 14:30	0.99	0		230.5
02/03/2010 14:45	0.99	0		230.75
02/03/2010 15:00	0.97	0		231
02/03/2010 15:15	0.97	0		231.25
02/03/2010 15:30	0.97	0		231.5
02/03/2010 15:45	0.96	0		231.75
02/03/2010 16:00	0.95	0		232
02/03/2010 16:15	0.95	0		232.25
02/03/2010 16:30	0.94	0		232.5
02/03/2010 16:45	0.93	0		232.75
02/03/2010 17:00	0.93	0		233
02/03/2010 17:15	0.93	0		233.25
02/03/2010 17:30	0.92	0		233.5
02/03/2010 17:45	0.92	0		233.75
02/03/2010 18:00	0.91	0		234
02/03/2010 18:15	0.90	0		234.25
02/03/2010 18:30	0.90	0		234.5
02/03/2010 18:45	0.89	0		234.75
02/03/2010 19:00	0.89	0		235
02/03/2010 19:15	0.89	0		235.25
02/03/2010 19:30	0.88	0		235.5
02/03/2010 19:45	0.88	0		235.75
02/03/2010 20:00	0.88	0		236
02/03/2010 20:15	0.87	0		236.25
02/03/2010 20:30	0.87	0		236.5
02/03/2010 20:45	0.86	0		236.75
02/03/2010 21:00	0.86	0		237
02/03/2010 21:15	0.86	0		237.25
02/03/2010 21:30	0.85	0		237.5
02/03/2010 21:45	0.85	0		237.75
02/03/2010 22:00	0.84	0		238
02/03/2010 22:15	0.84	0		238.25
02/03/2010 22:30	0.84	0		238.5
02/03/2010 22:45	0.84	0		238.75
02/03/2010 23:00	0.83	0		239
02/03/2010 23:15	0.83	0		239.25
02/03/2010 23:30	0.83	0		239.5
02/03/2010 23:45	0.83	0		239.75

Rainfall Event

Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG						
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours		Date & Time	Rainfall (mm)	Duration hours	
03/03/2010 00:00	0.82	0	240					
03/03/2010 00:15	0.81	0	240.25					
03/03/2010 00:30	0.81	0	240.5					
03/03/2010 00:45	0.81	0	240.75					
03/03/2010 01:00	0.81	0	241					
03/03/2010 01:15	0.80	0	241.25					
03/03/2010 01:30	0.80	0	241.5					
03/03/2010 01:45	0.80	0	241.75					
03/03/2010 02:00	0.80	0	242					
03/03/2010 02:15	0.79	0	242.25					
03/03/2010 02:30	0.79	0	242.5					
03/03/2010 02:45	0.79	0	242.75					
03/03/2010 03:00	0.79	0	243					
03/03/2010 03:15	0.79	0	243.25					
03/03/2010 03:30	0.78	0	243.5					
03/03/2010 03:45	0.78	0	243.75					
03/03/2010 04:00	0.78	0	244					
03/03/2010 04:15	0.77	0	244.25					
03/03/2010 04:30	0.77	0	244.5					
03/03/2010 04:45	0.77	0	244.75					
03/03/2010 05:00	0.77	0	245					
03/03/2010 05:15	0.76	0	245.25					
03/03/2010 05:30	0.76	0	245.5					
03/03/2010 05:45	0.76	0	245.75					
03/03/2010 06:00	0.76	0	246					
03/03/2010 06:15	0.76	0	246.25					
03/03/2010 06:30	0.75	0	246.5					
03/03/2010 06:45	0.75	0	246.75					
03/03/2010 07:00	0.75	0	247					
03/03/2010 07:15	0.75	0	247.25					
03/03/2010 07:30	0.75	0	247.5					
03/03/2010 07:45	0.75	0	247.75					
03/03/2010 08:00	0.74	0	248					
03/03/2010 08:15	0.74	0	248.25					
03/03/2010 08:30	0.74	0	248.5					
03/03/2010 08:45	0.74	0	248.75					
03/03/2010 09:00	0.74	0	249					
03/03/2010 09:15	0.74	0	249.25					
03/03/2010 09:30	0.73	0	249.5					
03/03/2010 09:45	0.73	0	249.75					
03/03/2010 10:00	0.72	0	250					
03/03/2010 10:15	0.73	0	250.25					
03/03/2010 10:30	0.72	0	250.5					
03/03/2010 10:45	0.72	0	250.75					
03/03/2010 11:00	0.72	0	251					
03/03/2010 11:15	0.72	0	251.25					
03/03/2010 11:30	0.72	0	251.5					
03/03/2010 11:45	0.72	0	251.75					

Rainfall Event

start of event	28/02/2010 04:00

	Middleton	Benhall TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Hours
03/03/2010 12:00	0.72	0	252
03/03/2010 12:15	0.72	0	252.25
03/03/2010 12:30	0.72	0	252.5
03/03/2010 12:45	0.71	0	252.75
03/03/2010 13:00	0.72	0	253
03/03/2010 13:15	0.71	0	253.25
03/03/2010 13:30	0.71	0	253.5
03/03/2010 13:45	0.71	0	253.75
03/03/2010 14:00	0.71	0	254
03/03/2010 14:15	0.71	0	254.25
03/03/2010 14:30	0.71	0	254.5
03/03/2010 14:45	0.71	0	254.75
03/03/2010 15:00	0.71	0	255
03/03/2010 15:15	0.71	0	255.25
03/03/2010 15:30	0.70	0	255.5
03/03/2010 15:45	0.70	0	255.75
03/03/2010 16:00	0.70	0	256
03/03/2010 16:15	0.70	0	256.25
03/03/2010 16:30	0.70	0	256.5
03/03/2010 16:45	0.70	0	256.75
03/03/2010 17:00	0.70	0	257
03/03/2010 17:15	0.70	0	257.25
03/03/2010 17:30	0.70	0	257.5
03/03/2010 17:45	0.69	0	257.75
03/03/2010 18:00	0.69	0	258
03/03/2010 18:15	0.69	0	258.25
03/03/2010 18:30	0.69	0	258.5
03/03/2010 18:45	0.69	0	258.75
03/03/2010 19:00	0.69	0	259
03/03/2010 19:15	0.69	0	259.25
03/03/2010 19:30	0.69	0	259.5
03/03/2010 19:45	0.69	0	259.75
03/03/2010 20:00	0.68	0	260
03/03/2010 20:15	0.68	0	260.25
03/03/2010 20:30	0.68	0	260.5
03/03/2010 20:45	0.68	0	260.75
03/03/2010 21:00	0.68	0	261
03/03/2010 21:15	0.68	0	261.25
03/03/2010 21:30	0.68	0	261.5
03/03/2010 21:45	0.68	0	261.75
03/03/2010 22:00	0.68	0	262
03/03/2010 22:15	0.68	0	262.25
03/03/2010 22:30	0.67	0	262.5
03/03/2010 22:45	0.67	0	262.75
03/03/2010 23:00	0.67	0	263
03/03/2010 23:15	0.67	0	263.25
03/03/2010 23:30	0.67	0	263.5
03/03/2010 23:45	0.67	0	263.75

Rainfall Event

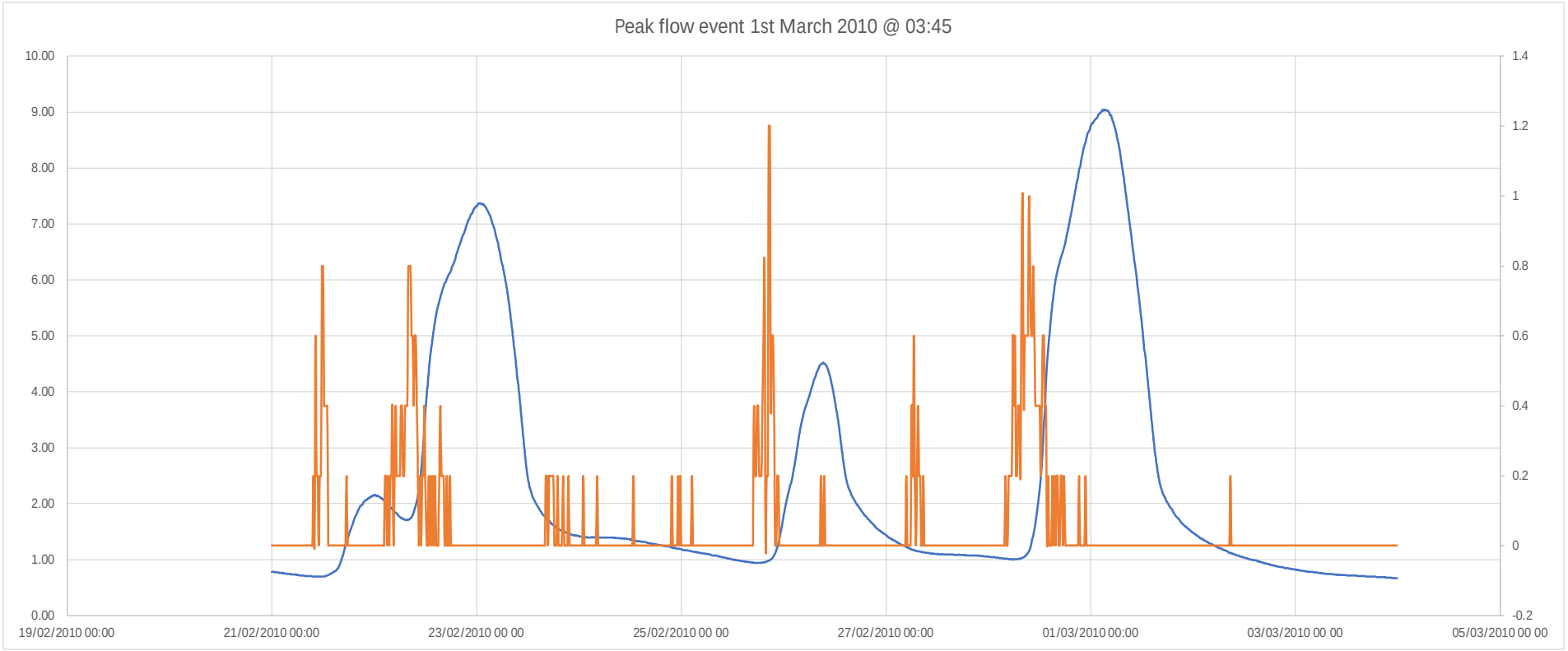
Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00

Date & Time	Middleton Flow (m^3/s)	Benhall TBR RG Rainfall (mm)	Hours

Rainfall Event		
Date & Time	Rainfall (mm)	Duration hours

start of event	28/02/2010 04:00



SAAR	592	mm
AREA	50.52	Km2

SMD on the first day of the event 1.3 mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capac ty in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**
W/E 02/03/2010	1.3
W/E 09/03/2010	7.1

Source of Rainfall event data.

Gauge	**Easting**	**Northing**	**Distance from Catchment Centroid (m)**	**Reciprocal**	**Weighting**
Benhall	38166	60602	8878.0	0.000112638	1.0000
Soham	23243	62717	15768.0		
Thorpeness	60012	78834			
			Total	0.000112638	1.0000

TBR RG

Daily RF totals 9am 9am	**Benhall**	**Soham**	
Date	**Total RF (mm)**	**Total RF (mm)**	
26/02/2010	3	N/A	0.005067568
25/02/2010	9.4	N/A	0.015878378
24/02/2010	1	N/A	0.001689189
23/02/2010	2.4	N/A	0.004054054
22/02/2010	5.8	N/A	0.009797297

Rainall Event Depth P (mm)	19.6
Event duration (hours)	18.75

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**22/02/2010**	**23/02/2010**	**24/02/2010**	**25/02/2010**	**26/02/2010**
Benhall	592	1.0000	5.8	2.4	1	9.4	3
Soham	592	N/A	N/A	N/A	N/A	N/A	N/A
Thorpeness	592						
Average Daily rainfall totals			5.8	2.4	1	9.4	3

Gauge	**SAAR**	**Weight**	**Standardised daily rainfall totals**				
Benhall	592	1.0000	0.009797297	0.004054054	0.001689189	0.015878378	0.005067568
Soham	592						
Thorpeness	592						

Gauge	**SAAR**	**Weight**	**Catchment average standardised daily rainfall**				
Benhall	592	1.0000	0.009797297	0.004054054	0.001689189	0.015878378	0.005067568
Soham	592		0	0	0	0	0
Thorpeness	592						

Gauge	**SAAR**	**Weight**	**Catchment Average Antecedent Rainfall totals (mm)**				
Benhall	592	1.0000	5.8	2.4	1	9.4	3
Soham	592		0	0	0	0	0
Thorpeness	592						
Catchment Average Antecedent RF mm			5.8	2.4	1	9.4	3

Date	**Catchment Average Antecedent Rainfall (mm)**	
22/02/2010	5.80	d-5
23/02/2010	2.40	d-4
24/02/2010	1.00	d-3
25/02/2010	9.40	d-2
26/02/2010	3.00	d-1

API5

6.09	mm	6.089957153	mm / day

March 2010 Event at Middleton

CWI Prior to Event
CWI 125 + API15 - SMD

SMD	1.3	mm
CWI	129.79	mm

FEH Parameter										
SPR	56.8	%					**URBEXT2000**	0 0084	As URBEXT2000 value is essentially rural the PR is the same as the PRrural value	
PRrural	58.0	%		P=Storm Depth	19.6	mm	**PR**	58	taken from PR calculations sheet using Benhall TBR RG record	
DPRrain	0.0	%		SPR	56.77219431		**DPRrain**	0	DPRrain is 0, as P<40mm	
DPRcwi	1.2	CWI	129.79				**DPRcwi**	1 2		
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural							**SPR**	56.77219431		
PR	58.0	%					**DPRrain**	0.45(P-40)^0.7	#NUM!	
PRrural	58.0	%					**P**	19.6	mm	57.9696836
CWI	129.8	mm					**CWI**	129 8		
BF	0.0		Baseflow equation taken from FEH				**SPR**	56 8		
	-1254.0						**PR**	58 0		
	1778.5		524 5 0.00525							
AREA	50.2		**0.26309** m3s-1				**SPRHOST**	41.05	from FEH Catchment descriptors & SPRHOST is the same as SPRcds	
SPR	56.8						**Duration (hours)**	18.75		
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	56.8									
PRrural	58.0									

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
07-Jan-16	07-Jan-16	18.75	6.09	1.3	129.8	58.0	1.2	0 0	56.8	58	41.05

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
30/12/2015 00:00	0.52	0		0
30/12/2015 00:15	0.52	0		0.25
30/12/2015 00:30	0.52	0		0.5
30/12/2015 00:45	0.51	0		0.75
30/12/2015 01:00	0.51	0		1
30/12/2015 01:15	0.51	0		1.25
30/12/2015 01:30	0.51	0		1.5
30/12/2015 01:45	0.51	0		1.75
30/12/2015 02:00	0.51	0		2
30/12/2015 02:15	0.51	0		2.25
30/12/2015 02:30	0.51	0		2.5
30/12/2015 02:45	0.51	0		2.75
30/12/2015 03:00	0.51	0		3
30/12/2015 03:15	0.51	0		3.25
30/12/2015 03:30	0.51	0		3.5
30/12/2015 03:45	0.51	0		3.75
30/12/2015 04:00	0.50	0		4
30/12/2015 04:15	0.50	0		4.25
30/12/2015 04:30	0.50	0		4.5
30/12/2015 04:45	0.50	0		4.75
30/12/2015 05:00	0.50	0		5
30/12/2015 05:15	0.50	0		5.25
30/12/2015 05:30	0.50	0		5.5
30/12/2015 05:45	0.50	0		5.75
30/12/2015 06:00	0.50	0		6
30/12/2015 06:15	0.50	0		6.25
30/12/2015 06:30	0.50	0		6.5
30/12/2015 06:45	0.50	0		6.75
30/12/2015 07:00	0.50	0		7
30/12/2015 07:15	0.50	0		7.25
30/12/2015 07:30	0.50	0		7.5
30/12/2015 07:45	0.50	0		7.75
30/12/2015 08:00	0.50	0		8
30/12/2015 08:15	0.50	0		8.25

start of event	07/01/2016 02:30
end of event	07/01/2016 15:00
duration hours	12.5
total RF mm	17.2
SMD W/E AVERAGE	**mm**

DATE	**API5**	**Daily Totals**
05/01/2016	d-1	2.8
04/01/2016	d-2	3
03/01/2016	d-3	10.8
02/01/2016	d-4	2.8
01/01/2016	d-5	2.4
		21.8

Thorpeness RG data not availabe

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
30/12/2015 08:30	0.49	0		8.5
30/12/2015 08:45	0.50	0		8.75
30/12/2015 09:00	0.50	0		9
30/12/2015 09:15	0.49	0		9.25
30/12/2015 09:30	0.49	0		9.5
30/12/2015 09:45	0.49	0		9.75
30/12/2015 10:00	0.49	0		10
30/12/2015 10:15	0.49	0		10.25
30/12/2015 10:30	0.49	0		10.5
30/12/2015 10:45	0.49	0		10.75
30/12/2015 11:00	0.49	0		11
30/12/2015 11:15	0.49	0		11.25
30/12/2015 11:30	0.49	0		11.5
30/12/2015 11:45	0.49	0		11.75
30/12/2015 12:00	0.49	0		12
30/12/2015 12:15	0.49	0		12.25
30/12/2015 12:30	0.49	0		12.5
30/12/2015 12:45	0.49	0		12.75
30/12/2015 13:00	0.49	0		13
30/12/2015 13:15	0.49	0		13.25
30/12/2015 13:30	0.49	0		13.5
30/12/2015 13:45	0.49	0		13.75
30/12/2015 14:00	0.49	0		14
30/12/2015 14:15	0.49	0		14.25
30/12/2015 14:30	0.49	0		14.5
30/12/2015 14:45	0.49	0		14.75
30/12/2015 15:00	0.49	0		15
30/12/2015 15:15	0.49	0		15.25
30/12/2015 15:30	0.49	0		15.5
30/12/2015 15:45	0.49	0		15.75
30/12/2015 16:00	0.49	0		16
30/12/2015 16:15	0.49	0		16.25
30/12/2015 16:30	0.49	0		16.5
30/12/2015 16:45	0.49	0		16.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
30/12/2015 17:00	0.49	0		17
30/12/2015 17:15	0.49	0		17.25
30/12/2015 17:30	0.49	0		17.5
30/12/2015 17:45	0.49	0		17.75
30/12/2015 18:00	0.49	0		18
30/12/2015 18:15	0.49	0		18.25
30/12/2015 18:30	0.49	0		18.5
30/12/2015 18:45	0.49	0		18.75
30/12/2015 19:00	0.49	0.2		19
30/12/2015 19:15	0.49	0.2		19.25
30/12/2015 19:30	0.49	0		19.5
30/12/2015 19:45	0.49	0		19.75
30/12/2015 20:00	0.49	0		20
30/12/2015 20:15	0.49	0		20.25
30/12/2015 20:30	0.49	0		20.5
30/12/2015 20:45	0.49	0		20.75
30/12/2015 21:00	0.49	0		21
30/12/2015 21:15	0.49	0		21.25
30/12/2015 21:30	0.49	0.2		21.5
30/12/2015 21:45	0.49	0.6		21.75
30/12/2015 22:00	0.49	0		22
30/12/2015 22:15	0.49	0.2		22.25
30/12/2015 22:30	0.49	0		22.5
30/12/2015 22:45	0.49	0.4		22.75
30/12/2015 23:00	0.49	0.6		23
30/12/2015 23:15	0.49	0		23.25
30/12/2015 23:30	0.49	0.2		23.5
30/12/2015 23:45	0.49	0		23.75
31/12/2015 00:00	0.49	0		24
31/12/2015 00:15	0.49	0		24.25
31/12/2015 00:30	0.49	0		24.5
31/12/2015 00:45	0.49	0		24.75
31/12/2015 01:00	0.49	0		25
31/12/2015 01:15	0.49	0		25.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
31/12/2015 01:30	0.49	0.2		25.5
31/12/2015 01:45	0.50	0.2		25.75
31/12/2015 02:00	0.49	0		26
31/12/2015 02:15	0.49	0		26.25
31/12/2015 02:30	0.50	0		26.5
31/12/2015 02:45	0.49	0		26.75
31/12/2015 03:00	0.49	0		27
31/12/2015 03:15	0.50	0		27.25
31/12/2015 03:30	0.50	0		27.5
31/12/2015 03:45	0.50	0		27.75
31/12/2015 04:00	0.50	0		28
31/12/2015 04:15	0.50	0		28.25
31/12/2015 04:30	0.50	0		28.5
31/12/2015 04:45	0.50	0		28.75
31/12/2015 05:00	0.50	0		29
31/12/2015 05:15	0.50	0		29.25
31/12/2015 05:30	0.50	0		29.5
31/12/2015 05:45	0.50	0		29.75
31/12/2015 06:00	0.50	0		30
31/12/2015 06:15	0.50	0		30.25
31/12/2015 06:30	0.50	0		30.5
31/12/2015 06:45	0.50	0		30.75
31/12/2015 07:00	0.50	0		31
31/12/2015 07:15	0.51	0		31.25
31/12/2015 07:30	0.51	0		31.5
31/12/2015 07:45	0.51	0		31.75
31/12/2015 08:00	0.51	0		32
31/12/2015 08:15	0.51	0		32.25
31/12/2015 08:30	0.51	0		32.5
31/12/2015 08:45	0.51	0		32.75
31/12/2015 09:00	0.51	0		33
31/12/2015 09:15	0.52	0		33.25
31/12/2015 09:30	0.52	0		33.5
31/12/2015 09:45	0.52	0		33.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
31/12/2015 10:00	0.52	0		34
31/12/2015 10:15	0.52	0		34.25
31/12/2015 10:30	0.52	0		34.5
31/12/2015 10:45	0.52	0		34.75
31/12/2015 11:00	0.52	0		35
31/12/2015 11:15	0.53	0		35.25
31/12/2015 11:30	0.53	0		35.5
31/12/2015 11:45	0.53	0		35.75
31/12/2015 12:00	0.53	0		36
31/12/2015 12:15	0.53	0		36.25
31/12/2015 12:30	0.53	0		36.5
31/12/2015 12:45	0.53	0		36.75
31/12/2015 13:00	0.53	0		37
31/12/2015 13:15	0.53	0		37.25
31/12/2015 13:30	0.53	0		37.5
31/12/2015 13:45	0.54	0		37.75
31/12/2015 14:00	0.54	0		38
31/12/2015 14:15	0.54	0		38.25
31/12/2015 14:30	0.54	0		38.5
31/12/2015 14:45	0.55	0		38.75
31/12/2015 15:00	0.55	0		39
31/12/2015 15:15	0.55	0		39.25
31/12/2015 15:30	0.55	0		39.5
31/12/2015 15:45	0.55	0		39.75
31/12/2015 16:00	0.55	0		40
31/12/2015 16:15	0.56	0		40.25
31/12/2015 16:30	0.56	0		40.5
31/12/2015 16:45	0.56	0		40.75
31/12/2015 17:00	0.56	0		41
31/12/2015 17:15	0.56	0		41.25
31/12/2015 17:30	0.56	0		41.5
31/12/2015 17:45	0.56	0		41.75
31/12/2015 18:00	0.56	0		42
31/12/2015 18:15	0.56	0		42.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
31/12/2015 18:30	0.56	0		42.5
31/12/2015 18:45	0.56	0		42.75
31/12/2015 19:00	0.56	0		43
31/12/2015 19:15	0.56	0.6		43.25
31/12/2015 19:30	0.56	2		43.5
31/12/2015 19:45	0.56	0.6		43.75
31/12/2015 20:00	0.56	0		44
31/12/2015 20:15	0.56	0		44.25
31/12/2015 20:30	0.56	0		44.5
31/12/2015 20:45	0.56	0		44.75
31/12/2015 21:00	0.56	0		45
31/12/2015 21:15	0.56	0		45.25
31/12/2015 21:30	0.56	0		45.5
31/12/2015 21:45	0.56	0		45.75
31/12/2015 22:00	0.56	0		46
31/12/2015 22:15	0.56	0		46.25
31/12/2015 22:30	0.56	0		46.5
31/12/2015 22:45	0.56	0		46.75
31/12/2015 23:00	0.56	0		47
31/12/2015 23:15	0.56	0		47.25
31/12/2015 23:30	0.56	0		47.5
31/12/2015 23:45	0.57	0		47.75
01/01/2016 00:00	0.57	0		48
01/01/2016 00:15	0.57	0		48.25
01/01/2016 00:30	0.57	0		48.5
01/01/2016 00:45	0.57	0		48.75
01/01/2016 01:00	0.57	0		49
01/01/2016 01:15	0.58	0		49.25
01/01/2016 01:30	0.58	0		49.5
01/01/2016 01:45	0.58	0		49.75
01/01/2016 02:00	0.58	0		50
01/01/2016 02:15	0.59	0		50.25
01/01/2016 02:30	0.59	0		50.5
01/01/2016 02:45	0.59	0		50.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
01/01/2016 03:00	0.60	0		51
01/01/2016 03:15	0.60	0		51.25
01/01/2016 03:30	0.60	0		51.5
01/01/2016 03:45	0.61	0		51.75
01/01/2016 04:00	0.61	0		52
01/01/2016 04:15	0.61	0		52.25
01/01/2016 04:30	0.62	0		52.5
01/01/2016 04:45	0.62	0		52.75
01/01/2016 05:00	0.62	0		53
01/01/2016 05:15	0.62	0		53.25
01/01/2016 05:30	0.62	0		53.5
01/01/2016 05:45	0.62	0		53.75
01/01/2016 06:00	0.62	0		54
01/01/2016 06:15	0.63	0		54.25
01/01/2016 06:30	0.63	0		54.5
01/01/2016 06:45	0.63	0		54.75
01/01/2016 07:00	0.63	0		55
01/01/2016 07:15	0.63	0		55.25
01/01/2016 07:30	0.63	0		55.5
01/01/2016 07:45	0.64	0		55.75
01/01/2016 08:00	0.64	0		56
01/01/2016 08:15	0.64	0		56.25
01/01/2016 08:30	0.64	0		56.5
01/01/2016 08:45	0.64	0		56.75
01/01/2016 09:00	0.64	0		57
01/01/2016 09:15	0.64	0		57.25
01/01/2016 09:30	0.64	0		57.5
01/01/2016 09:45	0.64	0.2		57.75
01/01/2016 10:00	0.64	0		58
01/01/2016 10:15	0.64	0		58.25
01/01/2016 10:30	0.64	0		58.5
01/01/2016 10:45	0.63	0		58.75
01/01/2016 11:00	0.63	0		59
01/01/2016 11:15	0.63	0		59.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
01/01/2016 11:30	0.63	0		59.5
01/01/2016 11:45	0.63	0		59.75
01/01/2016 12:00	0.63	0		60
01/01/2016 12:15	0.63	0		60.25
01/01/2016 12:30	0.63	0		60.5
01/01/2016 12:45	0.62	0		60.75
01/01/2016 13:00	0.62	0		61
01/01/2016 13:15	0.62	0		61.25
01/01/2016 13:30	0.62	0		61.5
01/01/2016 13:45	0.62	0		61.75
01/01/2016 14:00	0.62	0		62
01/01/2016 14:15	0.62	0		62.25
01/01/2016 14:30	0.62	0		62.5
01/01/2016 14:45	0.62	0		62.75
01/01/2016 15:00	0.62	0		63
01/01/2016 15:15	0.62	0		63.25
01/01/2016 15:30	0.62	0		63.5
01/01/2016 15:45	0.62	0		63.75
01/01/2016 16:00	0.62	0		64
01/01/2016 16:15	0.61	0		64.25
01/01/2016 16:30	0.62	0		64.5
01/01/2016 16:45	0.61	0		64.75
01/01/2016 17:00	0.61	0		65
01/01/2016 17:15	0.61	0		65.25
01/01/2016 17:30	0.61	0		65.5
01/01/2016 17:45	0.61	0		65.75
01/01/2016 18:00	0.61	0		66
01/01/2016 18:15	0.61	0		66.25
01/01/2016 18:30	0.61	0		66.5
01/01/2016 18:45	0.61	0		66.75
01/01/2016 19:00	0.61	0		67
01/01/2016 19:15	0.60	0		67.25
01/01/2016 19:30	0.60	0		67.5
01/01/2016 19:45	0.60	0		67.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
01/01/2016 20:00	0.60	0		68
01/01/2016 20:15	0.60	0		68.25
01/01/2016 20:30	0.59	0		68.5
01/01/2016 20:45	0.60	0		68.75
01/01/2016 21:00	0.60	0		69
01/01/2016 21:15	0.60	0		69.25
01/01/2016 21:30	0.60	0		69.5
01/01/2016 21:45	0.60	0		69.75
01/01/2016 22:00	0.60	0		70
01/01/2016 22:15	0.60	0		70.25
01/01/2016 22:30	0.59	0		70.5
01/01/2016 22:45	0.59	0		70.75
01/01/2016 23:00	0.59	0		71
01/01/2016 23:15	0.59	0		71.25
01/01/2016 23:30	0.59	0		71.5
01/01/2016 23:45	0.59	0		71.75
02/01/2016 00:00	0.59	0		72
02/01/2016 00:15	0.59	0		72.25
02/01/2016 00:30	0.60	0		72.5
02/01/2016 00:45	0.59	0		72.75
02/01/2016 01:00	0.59	0.2		73
02/01/2016 01:15	0.59	0.2		73.25
02/01/2016 01:30	0.59	0		73.5
02/01/2016 01:45	0.59	0.4		73.75
02/01/2016 02:00	0.59	0.4		74
02/01/2016 02:15	0.59	0.2		74.25
02/01/2016 02:30	0.59	0		74.5
02/01/2016 02:45	0.59	0		74.75
02/01/2016 03:00	0.59	0.2		75
02/01/2016 03:15	0.59	0.2		75.25
02/01/2016 03:30	0.59	0		75.5
02/01/2016 03:45	0.59	0		75.75
02/01/2016 04:00	0.59	0		76
02/01/2016 04:15	0.60	0		76.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
02/01/2016 04:30	0.59	0.2		76.5
02/01/2016 04:45	0.60	0		76.75
02/01/2016 05:00	0.60	0		77
02/01/2016 05:15	0.60	0.2		77.25
02/01/2016 05:30	0.60	0		77.5
02/01/2016 05:45	0.60	0		77.75
02/01/2016 06:00	0.60	0		78
02/01/2016 06:15	0.60	0		78.25
02/01/2016 06:30	0.60	0		78.5
02/01/2016 06:45	0.60	0		78.75
02/01/2016 07:00	0.61	0		79
02/01/2016 07:15	0.61	0		79.25
02/01/2016 07:30	0.61	0		79.5
02/01/2016 07:45	0.61	0		79.75
02/01/2016 08:00	0.62	0		80
02/01/2016 08:15	0.62	0		80.25
02/01/2016 08:30	0.62	0		80.5
02/01/2016 08:45	0.63	0		80.75
02/01/2016 09:00	0.63	0	2.4	81
02/01/2016 09:15	0.64	0		81.25
02/01/2016 09:30	0.65	0		81.5
02/01/2016 09:45	0.66	0		81.75
02/01/2016 10:00	0.66	0		82
02/01/2016 10:15	0.67	0		82.25
02/01/2016 10:30	0.68	0		82.5
02/01/2016 10:45	0.68	0		82.75
02/01/2016 11:00	0.69	0		83
02/01/2016 11:15	0.70	0		83.25
02/01/2016 11:30	0.70	0		83.5
02/01/2016 11:45	0.71	0		83.75
02/01/2016 12:00	0.71	0		84
02/01/2016 12:15	0.72	0		84.25
02/01/2016 12:30	0.72	0		84.5
02/01/2016 12:45	0.73	0		84.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
02/01/2016 13:00	0.74	0		85
02/01/2016 13:15	0.74	0		85.25
02/01/2016 13:30	0.74	0		85.5
02/01/2016 13:45	0.74	0		85.75
02/01/2016 14:00	0.75	0		86
02/01/2016 14:15	0.75	0		86.25
02/01/2016 14:30	0.75	0		86.5
02/01/2016 14:45	0.75	0		86.75
02/01/2016 15:00	0.75	0		87
02/01/2016 15:15	0.76	0		87.25
02/01/2016 15:30	0.76	0		87.5
02/01/2016 15:45	0.76	0		87.75
02/01/2016 16:00	0.76	0		88
02/01/2016 16:15	0.76	0		88.25
02/01/2016 16:30	0.76	0		88.5
02/01/2016 16:45	0.76	0		88.75
02/01/2016 17:00	0.76	0		89
02/01/2016 17:15	0.76	0		89.25
02/01/2016 17:30	0.76	0		89.5
02/01/2016 17:45	0.76	0.4		89.75
02/01/2016 18:00	0.76	0.2		90
02/01/2016 18:15	0.76	0.4		90.25
02/01/2016 18:30	0.76	0.2		90.5
02/01/2016 18:45	0.76	0		90.75
02/01/2016 19:00	0.76	0		91
02/01/2016 19:15	0.76	0		91.25
02/01/2016 19:30	0.76	0		91.5
02/01/2016 19:45	0.76	0		91.75
02/01/2016 20:00	0.76	0		92
02/01/2016 20:15	0.76	0.2		92.25
02/01/2016 20:30	0.76	0.2		92.5
02/01/2016 20:45	0.76	0.2		92.75
02/01/2016 21:00	0.76	0		93
02/01/2016 21:15	0.76	0		93.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
02/01/2016 21:30	0.76	0.2		93.5
02/01/2016 21:45	0.76	0		93.75
02/01/2016 22:00	0.76	0		94
02/01/2016 22:15	0.76	0		94.25
02/01/2016 22:30	0.76	0		94.5
02/01/2016 22:45	0.77	0		94.75
02/01/2016 23:00	0.77	0		95
02/01/2016 23:15	0.78	0		95.25
02/01/2016 23:30	0.79	0		95.5
02/01/2016 23:45	0.79	0		95.75
03/01/2016 00:00	0.80	0		96
03/01/2016 00:15	0.81	0.2		96.25
03/01/2016 00:30	0.83	0		96.5
03/01/2016 00:45	0.84	0		96.75
03/01/2016 01:00	0.86	0		97
03/01/2016 01:15	0.88	0		97.25
03/01/2016 01:30	0.89	0.4		97.5
03/01/2016 01:45	0.91	0		97.75
03/01/2016 02:00	0.92	0.2		98
03/01/2016 02:15	0.94	0		98.25
03/01/2016 02:30	0.95	0		98.5
03/01/2016 02:45	0.97	0		98.75
03/01/2016 03:00	0.97	0		99
03/01/2016 03:15	0.99	0		99.25
03/01/2016 03:30	1.00	0		99.5
03/01/2016 03:45	1.01	0		99.75
03/01/2016 04:00	1.02	0		100
03/01/2016 04:15	1.03	0		100.25
03/01/2016 04:30	1.04	0		100.5
03/01/2016 04:45	1.06	0		100.75
03/01/2016 05:00	1.06	0		101
03/01/2016 05:15	1.08	0		101.25
03/01/2016 05:30	1.08	0		101.5
03/01/2016 05:45	1.10	0		101.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
03/01/2016 06:00	1.11	0		102
03/01/2016 06:15	1.12	0		102.25
03/01/2016 06:30	1.13	0		102.5
03/01/2016 06:45	1.13	0		102.75
03/01/2016 07:00	1.15	0		103
03/01/2016 07:15	1.16	0		103.25
03/01/2016 07:30	1.16	0		103.5
03/01/2016 07:45	1.17	0		103.75
03/01/2016 08:00	1.18	0		104
03/01/2016 08:15	1.19	0		104.25
03/01/2016 08:30	1.19	0		104.5
03/01/2016 08:45	1.19	0		104.75
03/01/2016 09:00	1.20	0	2.8	105
03/01/2016 09:15	1.21	0		105.25
03/01/2016 09:30	1.21	0		105.5
03/01/2016 09:45	1.21	0		105.75
03/01/2016 10:00	1.21	0		106
03/01/2016 10:15	1.22	0		106.25
03/01/2016 10:30	1.22	0		106.5
03/01/2016 10:45	1.21	0		106.75
03/01/2016 11:00	1.22	0		107
03/01/2016 11:15	1.22	0		107.25
03/01/2016 11:30	1.22	0		107.5
03/01/2016 11:45	1.22	0		107.75
03/01/2016 12:00	1.21	0		108
03/01/2016 12:15	1.21	0.2		108.25
03/01/2016 12:30	1.21	0		108.5
03/01/2016 12:45	1.20	0.2		108.75
03/01/2016 13:00	1.20	0.2		109
03/01/2016 13:15	1.19	0.4		109.25
03/01/2016 13:30	1.19	0		109.5
03/01/2016 13:45	1.19	0.4		109.75
03/01/2016 14:00	1.19	0.2		110
03/01/2016 14:15	1.19	0.4		110.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
03/01/2016 14:30	1.19	0.4		110.5
03/01/2016 14:45	1.19	0.4		110.75
03/01/2016 15:00	1.18	0.6		111
03/01/2016 15:15	1.18	0.8		111.25
03/01/2016 15:30	1.18	0.8		111.5
03/01/2016 15:45	1.18	0.4		111.75
03/01/2016 16:00	1.19	0.6		112
03/01/2016 16:15	1.19	0.6		112.25
03/01/2016 16:30	1.19	0.4		112.5
03/01/2016 16:45	1.21	0.4		112.75
03/01/2016 17:00	1.22	0.6		113
03/01/2016 17:15	1.23	0.6		113.25
03/01/2016 17:30	1.26	0.2		113.5
03/01/2016 17:45	1.30	0.2		113.75
03/01/2016 18:00	1.36	0.2		114
03/01/2016 18:15	1.44	0.4		114.25
03/01/2016 18:30	1.53	0.4		114.5
03/01/2016 18:45	1.65	0.2		114.75
03/01/2016 19:00	1.80	0.4		115
03/01/2016 19:15	2.03	0		115.25
03/01/2016 19:30	2.33	0		115.5
03/01/2016 19:45	2.70	0		115.75
03/01/2016 20:00	3.01	0		116
03/01/2016 20:15	3.32	0		116.25
03/01/2016 20:30	3.58	0		116.5
03/01/2016 20:45	3.84	0		116.75
03/01/2016 21:00	4.09	0		117
03/01/2016 21:15	4.31	0		117.25
03/01/2016 21:30	4.53	0		117.5
03/01/2016 21:45	4.71	0		117.75
03/01/2016 22:00	4.83	0		118
03/01/2016 22:15	4.94	0		118.25
03/01/2016 22:30	5.06	0		118.5
03/01/2016 22:45	5.26	0		118.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
03/01/2016 23:00	5.35	0		119
03/01/2016 23:15	5.44	0		119.25
03/01/2016 23:30	5.50	0		119.5
03/01/2016 23:45	5.56	0		119.75
04/01/2016 00:00	5.62	0		120
04/01/2016 00:15	5.66	0		120.25
04/01/2016 00:30	5.69	0		120.5
04/01/2016 00:45	5.72	0		120.75
04/01/2016 01:00	5.75	0		121
04/01/2016 01:15	5.77	0		121.25
04/01/2016 01:30	5.78	0		121.5
04/01/2016 01:45	5.79	0		121.75
04/01/2016 02:00	5.80	0		122
04/01/2016 02:15	5.80	0		122.25
04/01/2016 02:30	5.81	0		122.5
04/01/2016 02:45	5.82	0		122.75
04/01/2016 03:00	5.82	0		123
04/01/2016 03:15	5.82	0		123.25
04/01/2016 03:30	5.82	0		123.5
04/01/2016 03:45	5.83	0		123.75
04/01/2016 04:00	5.84	0		124
04/01/2016 04:15	5.85	0		124.25
04/01/2016 04:30	5.87	0		124.5
04/01/2016 04:45	5.87	0.2		124.75
04/01/2016 05:00	5.90	0		125
04/01/2016 05:15	5.92	0		125.25
04/01/2016 05:30	5.94	0		125.5
04/01/2016 05:45	5.97	0		125.75
04/01/2016 06:00	5.99	0		126
04/01/2016 06:15	6.03	0		126.25
04/01/2016 06:30	6.07	0		126.5
04/01/2016 06:45	6.10	0		126.75
04/01/2016 07:00	6.14	0		127
04/01/2016 07:15	6.18	0		127.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
04/01/2016 07:30	6.22	0		127.5
04/01/2016 07:45	6.25	0		127.75
04/01/2016 08:00	6.30	0		128
04/01/2016 08:15	6.34	0		128.25
04/01/2016 08:30	6.38	0		128.5
04/01/2016 08:45	6.42	0		128.75
04/01/2016 09:00	6.45	0	10.8	129
04/01/2016 09:15	6.49	0		129.25
04/01/2016 09:30	6.53	0		129.5
04/01/2016 09:45	6.56	0		129.75
04/01/2016 10:00	6.60	0		130
04/01/2016 10:15	6.62	0		130.25
04/01/2016 10:30	6.64	0		130.5
04/01/2016 10:45	6.64	0		130.75
04/01/2016 11:00	6.65	0		131
04/01/2016 11:15	6.64	0		131.25
04/01/2016 11:30	6.64	0		131.5
04/01/2016 11:45	6.64	0		131.75
04/01/2016 12:00	6.62	0		132
04/01/2016 12:15	6.59	0		132.25
04/01/2016 12:30	6.57	0		132.5
04/01/2016 12:45	6.54	0		132.75
04/01/2016 13:00	6.49	0		133
04/01/2016 13:15	6.45	0		133.25
04/01/2016 13:30	6.40	0		133.5
04/01/2016 13:45	6.35	0		133.75
04/01/2016 14:00	6.30	0		134
04/01/2016 14:15	6.24	0		134.25
04/01/2016 14:30	6.17	0		134.5
04/01/2016 14:45	6.10	0		134.75
04/01/2016 15:00	6.04	0		135
04/01/2016 15:15	5.95	0		135.25
04/01/2016 15:30	5.86	0		135.5
04/01/2016 15:45	5.77	0		135.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
04/01/2016 16:00	5.66	0		136
04/01/2016 16:15	5.55	0		136.25
04/01/2016 16:30	5.42	0		136.5
04/01/2016 16:45	5.30	0		136.75
04/01/2016 17:00	5.15	0		137
04/01/2016 17:15	4.99	0		137.25
04/01/2016 17:30	4.85	0		137.5
04/01/2016 17:45	4.69	0		137.75
04/01/2016 18:00	4.51	0		138
04/01/2016 18:15	4.30	0		138.25
04/01/2016 18:30	4.10	0		138.5
04/01/2016 18:45	3.90	0		138.75
04/01/2016 19:00	3.71	0		139
04/01/2016 19:15	3.51	0		139.25
04/01/2016 19:30	3.32	0		139.5
04/01/2016 19:45	3.13	0		139.75
04/01/2016 20:00	2.95	0		140
04/01/2016 20:15	2.76	0		140.25
04/01/2016 20:30	2.59	0		140.5
04/01/2016 20:45	2.41	0		140.75
04/01/2016 21:00	2.24	0		141
04/01/2016 21:15	2.08	0		141.25
04/01/2016 21:30	1.94	0		141.5
04/01/2016 21:45	1.81	0		141.75
04/01/2016 22:00	1.70	0		142
04/01/2016 22:15	1.62	0		142.25
04/01/2016 22:30	1.56	0		142.5
04/01/2016 22:45	1.52	0		142.75
04/01/2016 23:00	1.48	0		143
04/01/2016 23:15	1.44	0		143.25
04/01/2016 23:30	1.42	0		143.5
04/01/2016 23:45	1.39	0		143.75
05/01/2016 00:00	1.36	0		144
05/01/2016 00:15	1.35	0		144.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
05/01/2016 00:30	1.32	0		144.5
05/01/2016 00:45	1.30	0		144.75
05/01/2016 01:00	1.28	0		145
05/01/2016 01:15	1.26	0		145.25
05/01/2016 01:30	1.25	0		145.5
05/01/2016 01:45	1.23	0		145.75
05/01/2016 02:00	1.22	0		146
05/01/2016 02:15	1.20	0		146.25
05/01/2016 02:30	1.19	0		146.5
05/01/2016 02:45	1.17	0		146.75
05/01/2016 03:00	1.16	0		147
05/01/2016 03:15	1.15	0		147.25
05/01/2016 03:30	1.13	0		147.5
05/01/2016 03:45	1.13	0		147.75
05/01/2016 04:00	1.12	0.2		148
05/01/2016 04:15	1.11	0		148.25
05/01/2016 04:30	1.10	0		148.5
05/01/2016 04:45	1.08	0		148.75
05/01/2016 05:00	1.08	0		149
05/01/2016 05:15	1.07	0		149.25
05/01/2016 05:30	1.06	0		149.5
05/01/2016 05:45	1.06	0		149.75
05/01/2016 06:00	1.04	0		150
05/01/2016 06:15	1.03	0		150.25
05/01/2016 06:30	1.03	0		150.5
05/01/2016 06:45	1.02	0		150.75
05/01/2016 07:00	1.01	0.8		151
05/01/2016 07:15	1.01	0.2		151.25
05/01/2016 07:30	1.00	0.8		151.5
05/01/2016 07:45	0.99	0.2		151.75
05/01/2016 08:00	0.99	0.2		152
05/01/2016 08:15	0.98	0.2		152.25
05/01/2016 08:30	0.97	0.2		152.5
05/01/2016 08:45	0.97	0.2		152.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
05/01/2016 09:00	0.97	0	3	153
05/01/2016 09:15	0.97	0.2		153.25
05/01/2016 09:30	0.96	0.2		153.5
05/01/2016 09:45	0.96	0		153.75
05/01/2016 10:00	0.96	0.4		154
05/01/2016 10:15	0.96	0.8		154.25
05/01/2016 10:30	0.97	0.6		154.5
05/01/2016 10:45	0.97	0.2		154.75
05/01/2016 11:00	0.98	0		155
05/01/2016 11:15	0.99	0		155.25
05/01/2016 11:30	0.99	0.2		155.5
05/01/2016 11:45	1.01	0		155.75
05/01/2016 12:00	1.03	0		156
05/01/2016 12:15	1.05	0		156.25
05/01/2016 12:30	1.08	0		156.5
05/01/2016 12:45	1.13	0		156.75
05/01/2016 13:00	1.18	0		157
05/01/2016 13:15	1.24	0		157.25
05/01/2016 13:30	1.31	0		157.5
05/01/2016 13:45	1.38	0		157.75
05/01/2016 14:00	1.46	0		158
05/01/2016 14:15	1.54	0		158.25
05/01/2016 14:30	1.61	0		158.5
05/01/2016 14:45	1.68	0		158.75
05/01/2016 15:00	1.75	0		159
05/01/2016 15:15	1.83	0		159.25
05/01/2016 15:30	1.91	0		159.5
05/01/2016 15:45	2.00	0		159.75
05/01/2016 16:00	2.09	0		160
05/01/2016 16:15	2.18	0		160.25
05/01/2016 16:30	2.26	0		160.5
05/01/2016 16:45	2.34	0		160.75
05/01/2016 17:00	2.41	0		161
05/01/2016 17:15	2.48	0		161.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
05/01/2016 17:30	2.54	0		161.5
05/01/2016 17:45	2.59	0		161.75
05/01/2016 18:00	2.64	0		162
05/01/2016 18:15	2.68	0		162.25
05/01/2016 18:30	2.72	0		162.5
05/01/2016 18:45	2.74	0		162.75
05/01/2016 19:00	2.76	0		163
05/01/2016 19:15	2.79	0		163.25
05/01/2016 19:30	2.81	0		163.5
05/01/2016 19:45	2.83	0		163.75
05/01/2016 20:00	2.84	0		164
05/01/2016 20:15	2.85	0		164.25
05/01/2016 20:30	2.85	0		164.5
05/01/2016 20:45	2.85	0		164.75
05/01/2016 21:00	2.85	0		165
05/01/2016 21:15	2.84	0		165.25
05/01/2016 21:30	2.83	0		165.5
05/01/2016 21:45	2.81	0		165.75
05/01/2016 22:00	2.78	0.2		166
05/01/2016 22:15	2.76	0		166.25
05/01/2016 22:30	2.73	0		166.5
05/01/2016 22:45	2.69	0		166.75
05/01/2016 23:00	2.65	0		167
05/01/2016 23:15	2.62	0		167.25
05/01/2016 23:30	2.57	0		167.5
05/01/2016 23:45	2.52	0		167.75
06/01/2016 00:00	2.47	0		168
06/01/2016 00:15	2.41	0		168.25
06/01/2016 00:30	2.35	0		168.5
06/01/2016 00:45	2.30	0		168.75
06/01/2016 01:00	2.24	0		169
06/01/2016 01:15	2.18	0		169.25
06/01/2016 01:30	2.11	0		169.5
06/01/2016 01:45	2.04	0		169.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
06/01/2016 02:00	1.98	0		170
06/01/2016 02:15	1.93	0		170.25
06/01/2016 02:30	1.87	0		170.5
06/01/2016 02:45	1.81	0		170.75
06/01/2016 03:00	1.77	0		171
06/01/2016 03:15	1.74	0		171.25
06/01/2016 03:30	1.70	0		171.5
06/01/2016 03:45	1.67	0		171.75
06/01/2016 04:00	1.64	0		172
06/01/2016 04:15	1.62	0		172.25
06/01/2016 04:30	1.59	0		172.5
06/01/2016 04:45	1.57	0		172.75
06/01/2016 05:00	1.54	0		173
06/01/2016 05:15	1.53	0		173.25
06/01/2016 05:30	1.51	0		173.5
06/01/2016 05:45	1.48	0		173.75
06/01/2016 06:00	1.47	0		174
06/01/2016 06:15	1.45	0		174.25
06/01/2016 06:30	1.44	0		174.5
06/01/2016 06:45	1.42	0		174.75
06/01/2016 07:00	1.40	0		175
06/01/2016 07:15	1.38	0		175.25
06/01/2016 07:30	1.36	0		175.5
06/01/2016 07:45	1.36	0		175.75
06/01/2016 08:00	1.34	0		176
06/01/2016 08:15	1.32	0		176.25
06/01/2016 08:30	1.31	0		176.5
06/01/2016 08:45	1.30	0		176.75
06/01/2016 09:00	1.28	0	2.8	177
06/01/2016 09:15	1.27	0		177.25
06/01/2016 09:30	1.25	0		177.5
06/01/2016 09:45	1.25	0		177.75
06/01/2016 10:00	1.23	0		178
06/01/2016 10:15	1.22	0.2		178.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
06/01/2016 10:30	1.21	0.2		178.5
06/01/2016 10:45	1.19	0.2		178.75
06/01/2016 11:00	1.18	0		179
06/01/2016 11:15	1.17	0		179.25
06/01/2016 11:30	1.16	0		179.5
06/01/2016 11:45	1.15	0		179.75
06/01/2016 12:00	1.14	0		180
06/01/2016 12:15	1.13	0		180.25
06/01/2016 12:30	1.12	0		180.5
06/01/2016 12:45	1.11	0		180.75
06/01/2016 13:00	1.11	0		181
06/01/2016 13:15	1.10	0		181.25
06/01/2016 13:30	1.09	0		181.5
06/01/2016 13:45	1.08	0		181.75
06/01/2016 14:00	1.07	0		182
06/01/2016 14:15	1.06	0		182.25
06/01/2016 14:30	1.06	0		182.5
06/01/2016 14:45	1.05	0		182.75
06/01/2016 15:00	1.04	0		183
06/01/2016 15:15	1.03	0		183.25
06/01/2016 15:30	1.02	0		183.5
06/01/2016 15:45	1.01	0		183.75
06/01/2016 16:00	1.01	0		184
06/01/2016 16:15	1.00	0		184.25
06/01/2016 16:30	0.99	0		184.5
06/01/2016 16:45	0.99	0		184.75
06/01/2016 17:00	0.98	0		185
06/01/2016 17:15	0.97	0		185.25
06/01/2016 17:30	0.97	0		185.5
06/01/2016 17:45	0.96	0		185.75
06/01/2016 18:00	0.95	0		186
06/01/2016 18:15	0.95	0		186.25
06/01/2016 18:30	0.94	0		186.5
06/01/2016 18:45	0.93	0		186.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
06/01/2016 19:00	0.93	0		187
06/01/2016 19:15	0.92	0		187.25
06/01/2016 19:30	0.92	0		187.5
06/01/2016 19:45	0.91	0		187.75
06/01/2016 20:00	0.91	0		188
06/01/2016 20:15	0.90	0		188.25
06/01/2016 20:30	0.89	0		188.5
06/01/2016 20:45	0.89	0		188.75
06/01/2016 21:00	0.89	0		189
06/01/2016 21:15	0.88	0		189.25
06/01/2016 21:30	0.88	0		189.5
06/01/2016 21:45	0.87	0		189.75
06/01/2016 22:00	0.86	0		190
06/01/2016 22:15	0.86	0		190.25
06/01/2016 22:30	0.86	0		190.5
06/01/2016 22:45	0.86	0		190.75
06/01/2016 23:00	0.85	0		191
06/01/2016 23:15	0.85	0		191.25
06/01/2016 23:30	0.84	0		191.5
06/01/2016 23:45	0.84	0		191.75
07/01/2016 00:00	0.84	0		192
07/01/2016 00:15	0.83	0		192.25
07/01/2016 00:30	0.83	0		192.5
07/01/2016 00:45	0.83	0		192.75
07/01/2016 01:00	0.82	0		193
07/01/2016 01:15	0.82	0		193.25
07/01/2016 01:30	0.81	0		193.5
07/01/2016 01:45	0.81	0		193.75
07/01/2016 02:00	0.81	0		194
07/01/2016 02:15	0.81	0		194.25
07/01/2016 02:30	0.80	0.6		194.5
07/01/2016 02:45	0.80	0.2		194.75
07/01/2016 03:00	0.80	0		195
07/01/2016 03:15	0.80	0		195.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
07/01/2016 03:30	0.79	0		195.5
07/01/2016 03:45	0.79	0		195.75
07/01/2016 04:00	0.79	0		196
07/01/2016 04:15	0.79	0		196.25
07/01/2016 04:30	0.78	0		196.5
07/01/2016 04:45	0.78	0		196.75
07/01/2016 05:00	0.78	0		197
07/01/2016 05:15	0.77	0		197.25
07/01/2016 05:30	0.77	0		197.5
07/01/2016 05:45	0.77	0		197.75
07/01/2016 06:00	0.77	0.2		198
07/01/2016 06:15	0.77	0.2		198.25
07/01/2016 06:30	0.76	0.6		198.5
07/01/2016 06:45	0.76	0.6		198.75
07/01/2016 07:00	0.76	0.6		199
07/01/2016 07:15	0.76	0.8		199.25
07/01/2016 07:30	0.77	0.8		199.5
07/01/2016 07:45	0.77	0.8		199.75
07/01/2016 08:00	0.77	1.2		200
07/01/2016 08:15	0.78	1.4		200.25
07/01/2016 08:30	0.79	1.4		200.5
07/01/2016 08:45	0.81	1.2		200.75
07/01/2016 09:00	0.84	1.2		201
07/01/2016 09:15	0.88	1		201.25
07/01/2016 09:30	0.92	0.8		201.5
07/01/2016 09:45	0.98	1		201.75
07/01/2016 10:00	1.06	0.6		202
07/01/2016 10:15	1.16	0.4		202.25
07/01/2016 10:30	1.31	0.4		202.5
07/01/2016 10:45	1.49	0.2		202.75
07/01/2016 11:00	1.71	0.2		203
07/01/2016 11:15	1.99	0		203.25
07/01/2016 11:30	2.45	0		203.5
07/01/2016 11:45	2.99	0		203.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
07/01/2016 12:00	3.53	0		204
07/01/2016 12:15	4.00	0.6		204.25
07/01/2016 12:30	4.39	0		204.5
07/01/2016 12:45	4.73	0		204.75
07/01/2016 13:00	4.97	0		205
07/01/2016 13:15	5.18	0		205.25
07/01/2016 13:30	5.40	0		205.5
07/01/2016 13:45	5.59	0		205.75
07/01/2016 14:00	5.76	0		206
07/01/2016 14:15	5.91	0		206.25
07/01/2016 14:30	6.03	0		206.5
07/01/2016 14:45	6.12	0		206.75
07/01/2016 15:00	6.22	0.2		207
07/01/2016 15:15	6.31	0		207.25
07/01/2016 15:30	6.39	0		207.5
07/01/2016 15:45	6.46	0		207.75
07/01/2016 16:00	6.53	0		208
07/01/2016 16:15	6.61	0		208.25
07/01/2016 16:30	6.67	0		208.5
07/01/2016 16:45	6.74	0		208.75
07/01/2016 17:00	6.81	0		209
07/01/2016 17:15	6.88	0		209.25
07/01/2016 17:30	6.95	0		209.5
07/01/2016 17:45	7.01	0		209.75
07/01/2016 18:00	7.09	0		210
07/01/2016 18:15	7.15	0		210.25
07/01/2016 18:30	7.22	0		210.5
07/01/2016 18:45	7.30	0		210.75
07/01/2016 19:00	7.38	0		211
07/01/2016 19:15	7.44	0		211.25
07/01/2016 19:30	7.54	0		211.5
07/01/2016 19:45	7.63	0		211.75
07/01/2016 20:00	7.71	0		212
07/01/2016 20:15	7.78	0		212.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
07/01/2016 20:30	7.86	0		212.5
07/01/2016 20:45	7.94	0		212.75
07/01/2016 21:00	8.02	0		213
07/01/2016 21:15	8.13	0		213.25
07/01/2016 21:30	8.22	0		213.5
07/01/2016 21:45	8.31	0		213.75
07/01/2016 22:00	8.42	0		214
07/01/2016 22:15	8.56	0		214.25
07/01/2016 22:30	8.70	0		214.5
07/01/2016 22:45	8.83	0		214.75
07/01/2016 23:00	8.99	0		215
07/01/2016 23:15	9.15	0		215.25
07/01/2016 23:30	9.33	0		215.5
07/01/2016 23:45	9.50	0		215.75
08/01/2016 00:00	9.70	0		216
08/01/2016 00:15	9.93	0		216.25
08/01/2016 00:30	10.12	0		216.5
08/01/2016 00:45	10.34	0		216.75
08/01/2016 01:00	10.52	0		217
08/01/2016 01:15	10.71	0		217.25
08/01/2016 01:30	10.83	0		217.5
08/01/2016 01:45	10.95	0		217.75
08/01/2016 02:00	11.08	0		218
08/01/2016 02:15	11.21	0		218.25
08/01/2016 02:30	11.26	0		218.5
08/01/2016 02:45	11.29	0		218.75
08/01/2016 03:00	11.36	0		219
08/01/2016 03:15	11.34	0		219.25
08/01/2016 03:30	11.34	0		219.5
08/01/2016 03:45	11.31	0		219.75
08/01/2016 04:00	11.23	0		220
08/01/2016 04:15	11.16	0		220.25
08/01/2016 04:30	11.05	0		220.5
08/01/2016 04:45	10.98	0		220.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
08/01/2016 05:00	10.88	0		221
08/01/2016 05:15	10.76	0		221.25
08/01/2016 05:30	10.61	0		221.5
08/01/2016 05:45	10.43	0		221.75
08/01/2016 06:00	10.27	0		222
08/01/2016 06:15	10.10	0		222.25
08/01/2016 06:30	9.93	0		222.5
08/01/2016 06:45	9.74	0		222.75
08/01/2016 07:00	9.54	0		223
08/01/2016 07:15	9.35	0		223.25
08/01/2016 07:30	9.15	0		223.5
08/01/2016 07:45	8.95	0		223.75
08/01/2016 08:00	8.73	0		224
08/01/2016 08:15	8.54	0		224.25
08/01/2016 08:30	8.33	0		224.5
08/01/2016 08:45	8.15	0		224.75
08/01/2016 09:00	7.94	0		225
08/01/2016 09:15	7.77	0		225.25
08/01/2016 09:30	7.60	0		225.5
08/01/2016 09:45	7.41	0.2		225.75
08/01/2016 10:00	7.21	0		226
08/01/2016 10:15	7.04	0		226.25
08/01/2016 10:30	6.88	0		226.5
08/01/2016 10:45	6.71	0		226.75
08/01/2016 11:00	6.55	0		227
08/01/2016 11:15	6.38	0		227.25
08/01/2016 11:30	6.22	0		227.5
08/01/2016 11:45	6.05	0		227.75
08/01/2016 12:00	5.88	0		228
08/01/2016 12:15	5.71	0		228.25
08/01/2016 12:30	5.52	0		228.5
08/01/2016 12:45	5.33	0		228.75
08/01/2016 13:00	5.13	0		229
08/01/2016 13:15	4.93	0		229.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
08/01/2016 13:30	4.73	0		229.5
08/01/2016 13:45	4.51	0		229.75
08/01/2016 14:00	4.26	0		230
08/01/2016 14:15	4.03	0		230.25
08/01/2016 14:30	3.80	0		230.5
08/01/2016 14:45	3.57	0		230.75
08/01/2016 15:00	3.35	0		231
08/01/2016 15:15	3.15	0		231.25
08/01/2016 15:30	2.95	0		231.5
08/01/2016 15:45	2.75	0		231.75
08/01/2016 16:00	2.58	0		232
08/01/2016 16:15	2.41	0		232.25
08/01/2016 16:30	2.25	0		232.5
08/01/2016 16:45	2.10	0		232.75
08/01/2016 17:00	1.96	0		233
08/01/2016 17:15	1.84	0		233.25
08/01/2016 17:30	1.73	0		233.5
08/01/2016 17:45	1.64	0		233.75
08/01/2016 18:00	1.58	0		234
08/01/2016 18:15	1.52	0		234.25
08/01/2016 18:30	1.48	0		234.5
08/01/2016 18:45	1.44	0		234.75
08/01/2016 19:00	1.41	0		235
08/01/2016 19:15	1.39	0		235.25
08/01/2016 19:30	1.36	0		235.5
08/01/2016 19:45	1.35	0		235.75
08/01/2016 20:00	1.32	0		236
08/01/2016 20:15	1.30	0		236.25
08/01/2016 20:30	1.28	0		236.5
08/01/2016 20:45	1.27	0		236.75
08/01/2016 21:00	1.25	0		237
08/01/2016 21:15	1.24	0		237.25
08/01/2016 21:30	1.22	0		237.5
08/01/2016 21:45	1.21	0		237.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
08/01/2016 22:00	1.19	0		238
08/01/2016 22:15	1.18	0		238.25
08/01/2016 22:30	1.17	0		238.5
08/01/2016 22:45	1.16	0		238.75
08/01/2016 23:00	1.15	0		239
08/01/2016 23:15	1.14	0		239.25
08/01/2016 23:30	1.13	0		239.5
08/01/2016 23:45	1.12	0		239.75
09/01/2016 00:00	1.11	0		240
09/01/2016 00:15	1.10	0		240.25
09/01/2016 00:30	1.09	0		240.5
09/01/2016 00:45	1.08	0		240.75
09/01/2016 01:00	1.07	0		241
09/01/2016 01:15	1.06	0		241.25
09/01/2016 01:30	1.06	0		241.5
09/01/2016 01:45	1.05	0		241.75
09/01/2016 02:00	1.03	0		242
09/01/2016 02:15	1.03	0		242.25
09/01/2016 02:30	1.02	0		242.5
09/01/2016 02:45	1.01	0.2		242.75
09/01/2016 03:00	1.01	0		243
09/01/2016 03:15	1.00	0		243.25
09/01/2016 03:30	0.99	0.2		243.5
09/01/2016 03:45	0.99	0		243.75
09/01/2016 04:00	0.98	0		244
09/01/2016 04:15	0.97	0		244.25
09/01/2016 04:30	0.97	0		244.5
09/01/2016 04:45	0.97	0.2		244.75
09/01/2016 05:00	0.96	0		245
09/01/2016 05:15	0.95	0.2		245.25
09/01/2016 05:30	0.95	0		245.5
09/01/2016 05:45	0.95	0		245.75
09/01/2016 06:00	0.94	0.2		246
09/01/2016 06:15	0.93	0		246.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
09/01/2016 06:30	0.93	0		246.5
09/01/2016 06:45	0.93	0		246.75
09/01/2016 07:00	0.92	0		247
09/01/2016 07:15	0.92	0		247.25
09/01/2016 07:30	0.91	0		247.5
09/01/2016 07:45	0.91	0		247.75
09/01/2016 08:00	0.91	0		248
09/01/2016 08:15	0.90	0		248.25
09/01/2016 08:30	0.90	0		248.5
09/01/2016 08:45	0.89	0		248.75
09/01/2016 09:00	0.89	0		249
09/01/2016 09:15	0.89	0		249.25
09/01/2016 09:30	0.88	0		249.5
09/01/2016 09:45	0.88	0		249.75
09/01/2016 10:00	0.88	0		250
09/01/2016 10:15	0.88	0		250.25
09/01/2016 10:30	0.87	0		250.5
09/01/2016 10:45	0.87	0		250.75
09/01/2016 11:00	0.86	0		251
09/01/2016 11:15	0.86	0		251.25
09/01/2016 11:30	0.86	0		251.5
09/01/2016 11:45	0.86	0		251.75
09/01/2016 12:00	0.85	0		252
09/01/2016 12:15	0.85	0		252.25
09/01/2016 12:30	0.84	0		252.5
09/01/2016 12:45	0.84	0		252.75
09/01/2016 13:00	0.84	0		253
09/01/2016 13:15	0.84	0		253.25
09/01/2016 13:30	0.84	0		253.5
09/01/2016 13:45	0.83	0		253.75
09/01/2016 14:00	0.83	0		254
09/01/2016 14:15	0.83	0		254.25
09/01/2016 14:30	0.83	0		254.5
09/01/2016 14:45	0.83	0		254.75

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
09/01/2016 15:00	0.82	0		255
09/01/2016 15:15	0.82	0		255.25
09/01/2016 15:30	0.81	0		255.5
09/01/2016 15:45	0.81	0		255.75
09/01/2016 16:00	0.81	0		256
09/01/2016 16:15	0.81	0		256.25
09/01/2016 16:30	0.81	0		256.5
09/01/2016 16:45	0.80	0		256.75
09/01/2016 17:00	0.80	0		257
09/01/2016 17:15	0.80	0		257.25
09/01/2016 17:30	0.80	0		257.5
09/01/2016 17:45	0.80	0		257.75
09/01/2016 18:00	0.79	0		258
09/01/2016 18:15	0.79	0		258.25
09/01/2016 18:30	0.79	0		258.5
09/01/2016 18:45	0.79	0		258.75
09/01/2016 19:00	0.79	0		259
09/01/2016 19:15	0.78	0.2		259.25
09/01/2016 19:30	0.78	0.6		259.5
09/01/2016 19:45	0.78	0.2		259.75
09/01/2016 20:00	0.77	0.2		260
09/01/2016 20:15	0.77	0.2		260.25
09/01/2016 20:30	0.77	0		260.5
09/01/2016 20:45	0.77	0		260.75
09/01/2016 21:00	0.77	0		261
09/01/2016 21:15	0.77	0		261.25
09/01/2016 21:30	0.77	0		261.5
09/01/2016 21:45	0.77	0		261.75
09/01/2016 22:00	0.77	0		262
09/01/2016 22:15	0.77	0		262.25
09/01/2016 22:30	0.77	0		262.5
09/01/2016 22:45	0.77	0.2		262.75
09/01/2016 23:00	0.77	0.2		263
09/01/2016 23:15	0.77	0		263.25

start of event	07/01/2016 02:30

	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
09/01/2016 23:30	0.78	0.4		263.5
09/01/2016 23:45	0.78	0		263.75
10/01/2016 00:00	0.78	0.2		264
10/01/2016 00:15	0.78	0		264.25
10/01/2016 00:30	0.79	0		264.5
10/01/2016 00:45	0.79	0		264.75
10/01/2016 01:00	0.79	0		265
10/01/2016 01:15	0.79	0		265.25
10/01/2016 01:30	0.79	0		265.5
10/01/2016 01:45	0.80	0.2		265.75
10/01/2016 02:00	0.80	0		266
10/01/2016 02:15	0.80	0		266.25
10/01/2016 02:30	0.81	0		266.5
10/01/2016 02:45	0.81	0		266.75
10/01/2016 03:00	0.82	0		267
10/01/2016 03:15	0.83	0		267.25
10/01/2016 03:30	0.83	0		267.5
10/01/2016 03:45	0.84	0		267.75
10/01/2016 04:00	0.85	0		268
10/01/2016 04:15	0.86	0		268.25
10/01/2016 04:30	0.88	0		268.5
10/01/2016 04:45	0.89	0		268.75
10/01/2016 05:00	0.90	0		269
10/01/2016 05:15	0.91	0		269.25
10/01/2016 05:30	0.93	0		269.5
10/01/2016 05:45	0.95	0		269.75
10/01/2016 06:00	0.97	0		270
10/01/2016 06:15	0.99	0		270.25
10/01/2016 06:30	1.00	0		270.5
10/01/2016 06:45	1.02	0		270.75
10/01/2016 07:00	1.03	0		271
10/01/2016 07:15	1.05	0		271.25
10/01/2016 07:30	1.07	0		271.5
10/01/2016 07:45	1.08	0		271.75

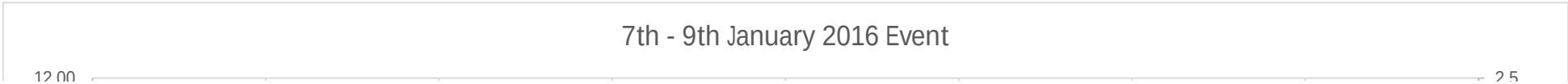
start of event	07/01/2016 02:30

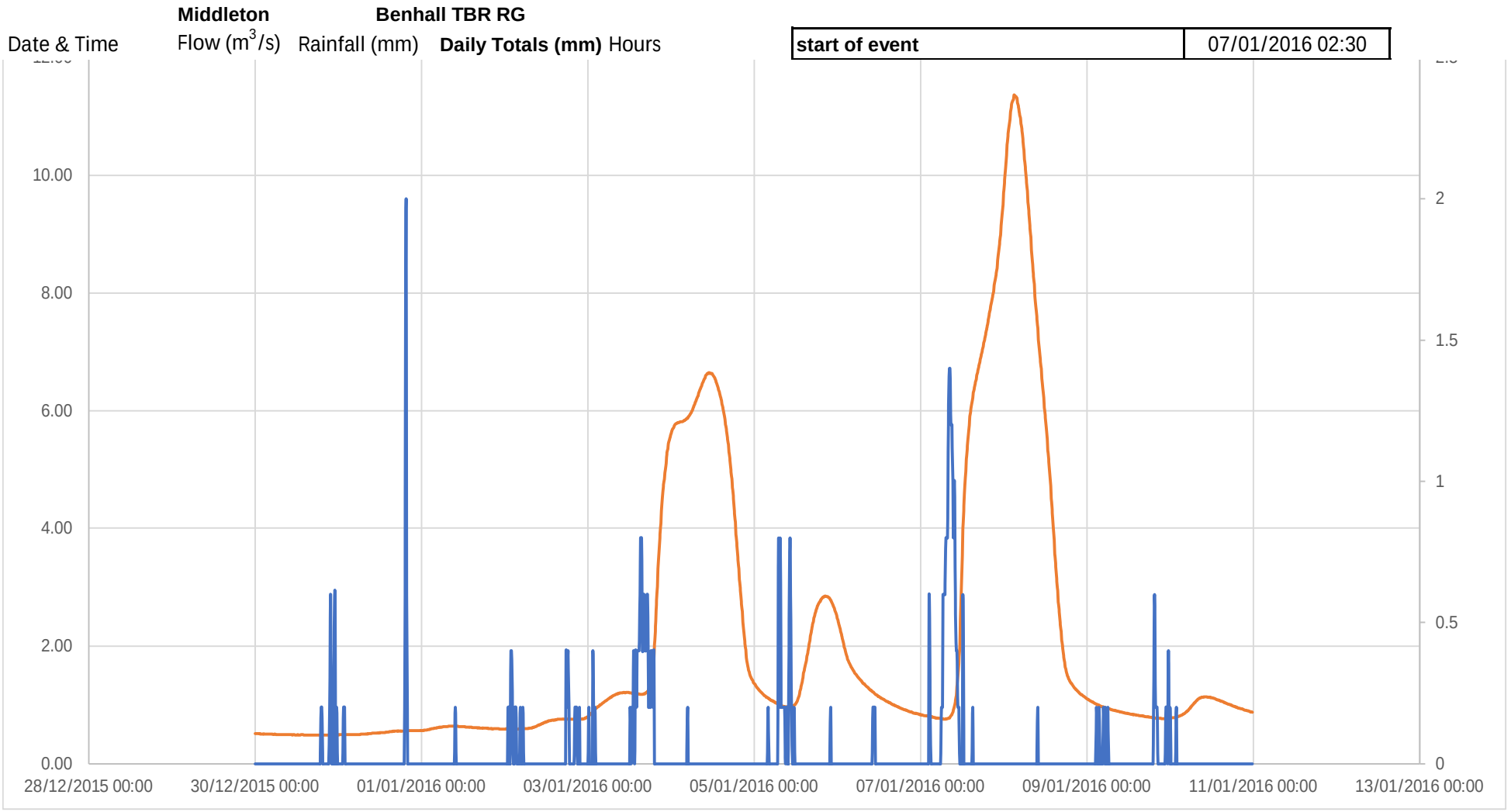
	Middleton	Benhall TBR RG		
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
10/01/2016 08:00	1.10	0		272
10/01/2016 08:15	1.11	0		272.25
10/01/2016 08:30	1.12	0		272.5
10/01/2016 08:45	1.12	0		272.75
10/01/2016 09:00	1.13	0		273
10/01/2016 09:15	1.13	0		273.25
10/01/2016 09:30	1.13	0		273.5
10/01/2016 09:45	1.14	0		273.75
10/01/2016 10:00	1.14	0		274
10/01/2016 10:15	1.14	0		274.25
10/01/2016 10:30	1.14	0		274.5
10/01/2016 10:45	1.13	0		274.75
10/01/2016 11:00	1.13	0		275
10/01/2016 11:15	1.13	0		275.25
10/01/2016 11:30	1.13	0		275.5
10/01/2016 11:45	1.13	0		275.75
10/01/2016 12:00	1.12	0		276
10/01/2016 12:15	1.12	0		276.25
10/01/2016 12:30	1.11	0		276.5
10/01/2016 12:45	1.11	0		276.75
10/01/2016 13:00	1.11	0		277
10/01/2016 13:15	1.10	0		277.25
10/01/2016 13:30	1.09	0		277.5
10/01/2016 13:45	1.09	0		277.75
10/01/2016 14:00	1.08	0		278
10/01/2016 14:15	1.08	0		278.25
10/01/2016 14:30	1.07	0		278.5
10/01/2016 14:45	1.06	0		278.75
10/01/2016 15:00	1.06	0		279
10/01/2016 15:15	1.06	0		279.25
10/01/2016 15:30	1.05	0		279.5
10/01/2016 15:45	1.04	0		279.75
10/01/2016 16:00	1.03	0		280
10/01/2016 16:15	1.03	0		280.25

start of event	07/01/2016 02:30

	Middleton		Benhall TBR RG	
Date & Time	Flow (m^3/s)	Rainfall (mm)	**Daily Totals (mm)**	Hours
10/01/2016 16:30	1.02	0		280.5
10/01/2016 16:45	1.01	0		280.75
10/01/2016 17:00	1.01	0		281
10/01/2016 17:15	1.01	0		281.25
10/01/2016 17:30	1.00	0		281.5
10/01/2016 17:45	0.99	0		281.75
10/01/2016 18:00	0.99	0		282
10/01/2016 18:15	0.98	0		282.25
10/01/2016 18:30	0.98	0		282.5
10/01/2016 18:45	0.97	0		282.75
10/01/2016 19:00	0.97	0		283
10/01/2016 19:15	0.96	0		283.25
10/01/2016 19:30	0.95	0		283.5
10/01/2016 19:45	0.95	0		283.75
10/01/2016 20:00	0.95	0		284
10/01/2016 20:15	0.94	0		284.25
10/01/2016 20:30	0.93	0		284.5
10/01/2016 20:45	0.93	0		284.75
10/01/2016 21:00	0.93	0		285
10/01/2016 21:15	0.92	0		285.25
10/01/2016 21:30	0.91	0		285.5
10/01/2016 21:45	0.91	0		285.75
10/01/2016 22:00	0.91	0		286
10/01/2016 22:15	0.90	0		286.25
10/01/2016 22:30	0.90	0		286.5
10/01/2016 22:45	0.89	0		286.75
10/01/2016 23:00	0.89	0		287
10/01/2016 23:15	0.88	0		287.25
10/01/2016 23:30	0.88	0		287.5
10/01/2016 23:45	0.88	0		287.75

start of event	07/01/2016 02:30




Middleton
Benhall TBR RG
Date & Time
Flow (m3/s)
Rainfall (mm)
Daily Totals (mm)
Hours
start of event
07/01/2016 02:30
10.00
8.00
6.00
4.00
2.00
0.00
2
1.5
1
0.5
0
28/12/2015 00:00
30/12/2015 00:00
01/01/2016 00:00
03/01/2016 00:00
05/01/2016 00:00
07/01/2016 00:00
09/01/2016 00:00
11/01/2016 00:00
13/01/2016 00:00

SAAR	592	mm
AREA	50.16	Km2

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capac ty in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**
W/E ??/12/2015	0
W/E ??/01/2016	0

Source of Rainfall event data.

Gauge	Easting	Northing	Distance from Catchment Centroid (m)	Reciprocal	Weighting
Benhall	38166	60602	8878.0	0.000112638	1.0000
Soham	23243	62717	15768.0		0.0000
Thorpeness	60012	78834			
			Total	0.000112638	1.0000

TBR RG

Daily RF totals 9am 9am	Benhall	Soham
Date	Total RF (mm)	Total RF (mm)
05/01/2016	2.4	
04/01/2016	3	
03/01/2016	10.8	
02/01/2016	2.8	
01/01/2016	2.4	

Rainall Event Depth P (mm)	17.2
Event duration (hours)	12.5

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**01/01/2016**	**02/01/2016**	**03/01/2016**	**04/01/2016**	**05/01/2016**
Benhall	592	1.0000	2.4	3	10.8	2.8	2.4
Soham	592	0.0000	N/A	N/A	N/A	N/A	N/A
Thorpeness	592		N/A	N/A	N/A	N/A	N/A
Average Daily rainfall totals			2.4	3	10.8	2.8	2.4

Gauge	**SAAR**	**Weight**	**02/01/2016**	**03/01/2016**	**04/01/2016**	**05/01/2016**	**06/01/2016**
Benhall	592	1.0000	0.004054054	0.005067568	0.018243243	0.00472973	0.004054054
Soham	592	0.0000	N/A	N/A	N/A	N/A	N/A
Thorpeness	592		N/A	N/A	N/A	N/A	N/A

Gauge	**SAAR**	**Weight**	**02/01/2016**	**03/01/2016**	**04/01/2016**	**05/01/2016**	**06/01/2016**
Benhall	592	1.0000	0.004054054	0.005067568	0.018243243	0.00472973	0.004054054
Soham	592	0.0000	N/A	N/A	N/A	N/A	N/A
Thorpeness	592		N/A	N/A	N/A	N/A	N/A

Gauge	**SAAR**	**Weight**	**02/01/2016**	**03/01/2016**	**04/01/2016**	**05/01/2016**	**06/01/2016**
Benhall	592	1.0000	2.4	3	10.8	2.8	2.4
Soham	592	0.0000	N/A	N/A	N/A	N/A	N/A
Thorpeness	592		N/A	N/A	N/A	N/A	N/A
Catchment Average Antecedent RF mm			2.4	3	10.8	2.8	2.4

Date	**Catchment Average Antecedent Rainfall (mm)**	
01/01/2016	2.40	d-5
02/01/2016	3.00	d-4
03/01/2016	10.80	d-3
04/01/2016	2.80	d-2
05/01/2016	2.40	d-1

API5	mm		
4.97		4.967425138	mm / day

January 2016 Event at Middleton

CWI Prior to Event		
CWI 125 + API15 - SMD	0	mm
SMD	129.9674251	mm
CWI		

FEH Parameter										
SPR	71.8	%						**URBEXT2000**	0 0084	As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
PRrural	73.0	%			P=Storm Depth	17.2	mm	**PR**	73	taken from PR calculations sheet using Benhall TBR RG record
DPRrain	0.0	%			SPR	71.76572281		**DPRrain**	0	DPRrain is 0, as P<40mm
DPRcwi	1.2	CWI	129.967					**DPRcwi**	1.241856284	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural								**SPR**	71.76572281	
PR	73.0	%						**DPRrain**	0.45(P-40)^0.7	#NUM!
PRrural	73.0	%						**P**	17 2	
CWI	130.0	mm						**CWI**	129 9674251	
BF	0 00001		Baseflow equation taken from FEH					**SPR**	71.76572281	
	-1254							**PR**	72.99204195	
	1778.5		524 5	0.00525						
AREA	50.16			**0.26309** m3s-1				**SPRHOST**	41.05	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
SPR	71.8							**Duration (hours)**	12 5	
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	71.76572281									
PRrural	73.0075791									

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
07-Jan-16	07-Jan-16	12.50	5.0	0.0	130.0	73.0	1.2	0 0	71.8	73	41.05

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
25/03/2018 21 00		0.18	0		0	0		0	
25/03/2018 21 15		0.18	0		0.25	0		0	
25/03/2018 21 30		0.18	0		0.5	0		0	
25/03/2018 21 45		0.18	0		0.75	0		0	
25/03/2018 22 00		0.18	0		1	0		0	
25/03/2018 22 15		0.18	0		1.25	0		0	
25/03/2018 22 30		0.18	0		1.5	0		0	
25/03/2018 22 45		0.18	0		1.75	0		0	
25/03/2018 23 00		0.18	0		2	0		0	
25/03/2018 23 15		0.18	0		2.25	0		0	
25/03/2018 23 30		0.18	0		2.5	0		0	
25/03/2018 23 45		0.18	0		2.75	0		0	
26/03/2018 00 00		0.18	0		3	0		0	
26/03/2018 00 15		0.18	0		3.25	0		0	
26/03/2018 00 30		0.18	0		3.5	0		0	
26/03/2018 00 45		0.18	0		3.75	0		0	
26/03/2018 01 00		0.18	0		4	0		0	
26/03/2018 01 15		0.18	0		4.25	0		0	
26/03/2018 01 30		0.18	0		4.5	0		0	
26/03/2018 01 45		0.18	0		4.75	0		0	
26/03/2018 02 00		0.18	0		5	0		0	
26/03/2018 02 15		0.18	0		5.25	0		0	
26/03/2018 02 30		0.18	0		5.5	0		0	
26/03/2018 02 45		0.18	0		5.75	0		0	
26/03/2018 03 00		0.18	0		6	0		0	
26/03/2018 03 15		0.18	0		6.25	0		0	
26/03/2018 03 30		0.18	0		6.5	0		0	
26/03/2018 03 45		0.18	0		6.75	0		0	
26/03/2018 04 00		0.18	0		7	0		0	
26/03/2018 04 15		0.18	0		7.25	0		0	
26/03/2018 04 30		0.18	0		7.5	0		0	
26/03/2018 04 45		0.18	0		7.75	0		0	
26/03/2018 05 00		0.18	0		8	0		0	
26/03/2018 05 15		0.18	0		8.25	0		0	
26/03/2018 05 30		0.18	0		8.5	0		0	
26/03/2018 05 45		0.18	0		8.75	0		0	
26/03/2018 06 00		0.18	0		9	0		0	
26/03/2018 06 15		0.18	0		9.25	0		0	
26/03/2018 06 30		0.18	0		9.5	0		0	
26/03/2018 06 45		0.18	0		9.75	0		0	
26/03/2018 07 00		0.18	0		10	0		0	
26/03/2018 07 15		0.18	0		10.25	0		0	
26/03/2018 07 30		0.18	0		10.5	0		0	
26/03/2018 07 45		0.18	0		10.75	0		0	
26/03/2018 08 00		0.18	0		11	0		0	
26/03/2018 08 15		0.18	0		11.25	0		0	
26/03/2018 08 30		0.18	0		11.5	0		0	
26/03/2018 08 45		0.18	0		11.75	0		0	
26/03/2018 09 00		0.18	0	0	12	0	0	0	0
26/03/2018 09 15		0.18	0		12.25	0		0	
26/03/2018 09 30		0.18	0		12.5	0		0	
26/03/2018 09 45		0.18	0		12.75	0		0	
26/03/2018 10 00		0.18	0		13	0		0	
26/03/2018 10 15		0.18	0		13.25	0		0	
26/03/2018 10 30		0.18	0		13.5	0		0	
26/03/2018 10 45		0.18	0		13.75	0		0	
26/03/2018 11 00		0.18	0		14	0		0	
26/03/2018 11 15		0.18	0		14.25	0		0	
26/03/2018 11 30		0.18	0		14.5	0		0	
26/03/2018 11 45		0.18	0		14.75	0		0	
26/03/2018 12 00		0.18	0		15	0		0	
26/03/2018 12 15		0.18	0		15.25	0		0	
26/03/2018 12 30		0.18	0		15.5	0		0	
26/03/2018 12 45		0.18	0		15.75	0		0	
26/03/2018 13 00		0.18	0		16	0		0	
26/03/2018 13 15		0.18	0		16.25	0		0	
26/03/2018 13 30		0.18	0		16.5	0		0	
26/03/2018 13 45		0.18	0		16.75	0		0	
26/03/2018 14 00		0.18	0		17	0		0	
26/03/2018 14 15		0.18	0		17.25	0		0	
26/03/2018 14 30		0.18	0		17.5	0		0	
26/03/2018 14 45		0.18	0		17.75	0		0	
26/03/2018 15 00		0.18	0		18	0		0	
26/03/2018 15 15		0.18	0		18.25	0		0	
26/03/2018 15 30		0.18	0		18.5	0		0	
26/03/2018 15 45		0.18	0		18.75	0		0	
26/03/2018 16 00		0.18	0		19	0		0	
26/03/2018 16 15		0.18	0		19.25	0		0	
26/03/2018 16 30		0.18	0		19.5	0		0	

start of event	30/03/2018 14 00
end of event	02/04/2018 19 00
duration hours	77
total RF mm	31
SMD W/E AVERAGE	**mm**
03/04/2018	1.4

DATE	API5	Benhall Daily Totals	Soham Daily Totals	Thorpeness Daily Totals
29/03/2018	d-1	3.6	3.6	4.6
28/03/2018	d-2	5.2	6.6	7.2
27/03/2018	d-3	1.6	1.4	1
26/03/2018	d-4	0.2	0.4	0.2
25/03/2018	d-5	0	0	0
		10.6	12	13

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
26/03/2018 16 45		0.18	0		19.75	0		0	
26/03/2018 17 00		0.18	0		20	0		0	
26/03/2018 17 15		0.18	0		20.25	0		0	
26/03/2018 17 30		0.18	0		20.5	0		0	
26/03/2018 17 45		0.18	0		20.75	0		0	
26/03/2018 18 00		0.18	0		21	0		0	
26/03/2018 18 15		0.18	0		21.25	0		0	
26/03/2018 18 30		0.18	0		21.5	0		0	
26/03/2018 18 45		0.18	0		21.75	0		0	
26/03/2018 19 00		0.18	0		22	0		0	
26/03/2018 19 15		0.18	0		22.25	0		0	
26/03/2018 19 30		0.18	0		22.5	0		0	
26/03/2018 19 45		0.18	0		22.75	0		0	
26/03/2018 20 00		0.18	0		23	0		0	
26/03/2018 20 15		0.18	0		23.25	0		0	
26/03/2018 20 30		0.18	0		23.5	0		0	
26/03/2018 20 45		0.18	0		23.75	0		0	
26/03/2018 21 00		0.18	0		24	0		0	
26/03/2018 21 15		0.18	0		24.25	0		0	
26/03/2018 21 30		0.18	0		24.5	0		0	
26/03/2018 21 45		0.18	0		24.75	0		0	
26/03/2018 22 00		0.18	0		25	0		0	
26/03/2018 22 15		0.18	0		25.25	0		0	
26/03/2018 22 30		0.18	0		25.5	0		0	
26/03/2018 22 45		0.18	0		25.75	0		0	
26/03/2018 23 00		0.18	0		26	0		0	
26/03/2018 23 15		0.18	0		26.25	0		0	
26/03/2018 23 30		0.18	0		26.5	0		0	
26/03/2018 23 45		0.18	0		26.75	0		0	
27/03/2018 00 00		0.18	0		27	0		0	
27/03/2018 00 15		0.18	0		27.25	0		0	
27/03/2018 00 30		0.18	0		27.5	0		0	
27/03/2018 00 45		0.18	0		27.75	0		0	
27/03/2018 01 00		0.18	0		28	0		0	
27/03/2018 01 15		0.18	0		28.25	0		0	
27/03/2018 01 30		0.18	0		28.5	0		0	
27/03/2018 01 45		0.18	0		28.75	0		0	
27/03/2018 02 00		0.18	0		29	0		0	
27/03/2018 02 15		0.18	0		29.25	0		0	
27/03/2018 02 30		0.18	0		29.5	0		0	
27/03/2018 02 45		0.18	0		29.75	0		0	
27/03/2018 03 00		0.18	0		30	0		0	
27/03/2018 03 15		0.18	0		30.25	0		0	
27/03/2018 03 30		0.18	0		30.5	0		0	
27/03/2018 03 45		0.18	0		30.75	0		0	
27/03/2018 04 00		0.18	0		31	0		0	
27/03/2018 04 15		0.18	0		31.25	0		0	
27/03/2018 04 30		0.18	0		31.5	0		0	
27/03/2018 04 45		0.18	0		31.75	0		0	
27/03/2018 05 00		0.18	0		32	0		0	
27/03/2018 05 15		0.18	0		32.25	0		0	
27/03/2018 05 30		0.18	0		32.5	0		0	
27/03/2018 05 45		0.18	0		32.75	0		0	
27/03/2018 06 00		0.18	0		33	0		0	
27/03/2018 06 15		0.18	0		33.25	0		0	
27/03/2018 06 30		0.18	0		33.5	0		0	
27/03/2018 06 45		0.18	0		33.75	0.2		0	
27/03/2018 07 00		0.18	0		34	0		0	
27/03/2018 07 15		0.18	0.2		34.25	0		0	
27/03/2018 07 30		0.18	0		34.5	0		0.2	
27/03/2018 07 45		0.18	0		34.75	0		0	
27/03/2018 08 00		0.18	0		35	0.2		0	
27/03/2018 08 15		0.18	0		35.25	0		0	
27/03/2018 08 30		0.18	0		35.5	0		0	
27/03/2018 08 45		0.18	0		35.75	0		0	
27/03/2018 09 00		0.18	0	0.2	36	0	0.4	0	0.2
27/03/2018 09 15		0.18	0		36.25	0		0	
27/03/2018 09 30		0.18	0		36.5	0		0	
27/03/2018 09 45		0.18	0		36.75	0		0	
27/03/2018 10 00		0.18	0		37	0		0	
27/03/2018 10 15		0.18	0		37.25	0.2		0	
27/03/2018 10 30		0.18	0.2		37.5	0		0.2	
27/03/2018 10 45		0.18	0		37.75	0		0	
27/03/2018 11 00		0.18	0		38	0		0	
27/03/2018 11 15		0.18	0		38.25	0		0	
27/03/2018 11 30		0.18	0		38.5	0		0	
27/03/2018 11 45		0.18	0		38.75	0		0	
27/03/2018 12 00		0.18	0.2		39	0		0	
27/03/2018 12 15		0.18	0		39.25	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
27/03/2018 12 30		0.18	0		39.5	0		0	
27/03/2018 12 45		0.18	0		39.75	0		0	
27/03/2018 13 00		0.18	0		40	0		0	
27/03/2018 13 15		0.18	0		40.25	0		0	
27/03/2018 13 30		0.19	0		40.5	0		0	
27/03/2018 13 45		0.19	0		40.75	0		0	
27/03/2018 14 00		0.19	0		41	0		0	
27/03/2018 14 15		0.19	0		41.25	0		0	
27/03/2018 14 30		0.19	0		41.5	0		0	
27/03/2018 14 45		0.19	0		41.75	0		0	
27/03/2018 15 00		0.19	0		42	0		0	
27/03/2018 15 15		0.19	0		42.25	0		0	
27/03/2018 15 30		0.19	0		42.5	0		0	
27/03/2018 15 45		0.19	0		42.75	0		0	
27/03/2018 16 00		0.19	0		43	0		0	
27/03/2018 16 15		0.19	0		43.25	0		0	
27/03/2018 16 30		0.19	0		43.5	0		0	
27/03/2018 16 45		0.19	0		43.75	0		0	
27/03/2018 17 00		0.18	0		44	0.2		0	
27/03/2018 17 15		0.18	0		44.25	0		0	
27/03/2018 17 30		0.18	0		44.5	0		0	
27/03/2018 17 45		0.18	0		44.75	0		0	
27/03/2018 18 00		0.18	0		45	0.4		0	
27/03/2018 18 15		0.18	0.2		45.25	0		0	
27/03/2018 18 30		0.18	0.2		45.5	0		0.2	
27/03/2018 18 45		0.18	0		45.75	0		0	
27/03/2018 19 00		0.18	0		46	0		0	
27/03/2018 19 15		0.18	0		46.25	0		0	
27/03/2018 19 30		0.18	0		46.5	0		0	
27/03/2018 19 45		0.18	0		46.75	0		0	
27/03/2018 20 00		0.19	0		47	0		0	
27/03/2018 20 15		0.19	0		47.25	0		0	
27/03/2018 20 30		0.19	0		47.5	0		0	
27/03/2018 20 45		0.19	0		47.75	0		0	
27/03/2018 21 00		0.19	0		48	0		0	
27/03/2018 21 15		0.19	0		48.25	0		0	
27/03/2018 21 30		0.19	0		48.5	0		0	
27/03/2018 21 45		0.19	0		48.75	0		0	
27/03/2018 22 00		0.19	0		49	0		0	
27/03/2018 22 15		0.19	0		49.25	0		0	
27/03/2018 22 30		0.19	0		49.5	0		0	
27/03/2018 22 45		0.19	0		49.75	0		0	
27/03/2018 23 00		0.19	0		50	0		0	
27/03/2018 23 15		0.19	0		50.25	0		0	
27/03/2018 23 30		0.19	0		50.5	0		0	
27/03/2018 23 45		0.19	0		50.75	0		0	
28/03/2018 00 00		0.19	0		51	0		0	
28/03/2018 00 15		0.19	0		51.25	0		0	
28/03/2018 00 30		0.19	0		51.5	0		0	
28/03/2018 00 45		0.19	0		51.75	0		0	
28/03/2018 01 00		0.19	0		52	0		0	
28/03/2018 01 15		0.19	0		52.25	0		0	
28/03/2018 01 30		0.19	0		52.5	0		0	
28/03/2018 01 45		0.19	0		52.75	0		0	
28/03/2018 02 00		0.19	0		53	0		0	
28/03/2018 02 15		0.19	0		53.25	0		0	
28/03/2018 02 30		0.19	0		53.5	0		0	
28/03/2018 02 45		0.19	0		53.75	0		0	
28/03/2018 03 00		0.19	0		54	0		0	
28/03/2018 03 15		0.19	0		54.25	0		0	
28/03/2018 03 30		0.19	0		54.5	0		0	
28/03/2018 03 45		0.19	0		54.75	0		0	
28/03/2018 04 00		0.19	0		55	0		0	
28/03/2018 04 15		0.19	0		55.25	0		0	
28/03/2018 04 30		0.19	0		55.5	0		0	
28/03/2018 04 45		0.19	0		55.75	0		0	
28/03/2018 05 00		0.19	0		56	0		0	
28/03/2018 05 15		0.19	0		56.25	0		0	
28/03/2018 05 30		0.19	0		56.5	0		0	
28/03/2018 05 45		0.19	0		56.75	0		0	
28/03/2018 06 00		0.19	0		57	0		0	
28/03/2018 06 15		0.19	0		57.25	0		0	
28/03/2018 06 30		0.19	0		57.5	0		0	
28/03/2018 06 45		0.19	0		57.75	0		0	
28/03/2018 07 00		0.19	0		58	0		0	
28/03/2018 07 15		0.19	0		58.25	0		0	
28/03/2018 07 30		0.19	0		58.5	0		0	
28/03/2018 07 45		0.19	0		58.75	0		0	
28/03/2018 08 00		0.19	0.2		59	0.2		0.2	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
28/03/2018 08 15		0.19	0.2		59.25	0.2		0	
28/03/2018 08 30		0.19	0.2		59.5	0.2		0.2	
28/03/2018 08 45		0.19	0		59.75	0		0.2	
28/03/2018 09 00		0.19	0.2	1.6	60	0	1.4	0	1
28/03/2018 09 15		0.19	0		60.25	0.2		0.4	
28/03/2018 09 30		0.19	0		60.5	0		0.2	
28/03/2018 09 45		0.19	0.2		60.75	0		0.2	
28/03/2018 10 00		0.19	0		61	0.2		0.2	
28/03/2018 10 15		0.19	0		61.25	0.2		0	
28/03/2018 10 30		0.19	0.2		61.5	0.4		0.2	
28/03/2018 10 45		0.19	0.4		61.75	0.2		0.2	
28/03/2018 11 00		0.19	0.4		62	0.2		0.4	
28/03/2018 11 15		0.19	0.2		62.25	0.2		0.4	
28/03/2018 11 30		0.19	0.2		62.5	0.2		0.2	
28/03/2018 11 45		0.19	0.2		62.75	0.2		0.4	
28/03/2018 12 00		0.19	0.2		63	0.2		0.2	
28/03/2018 12 15		0.19	0.2		63.25	0.4		0.4	
28/03/2018 12 30		0.20	0.2		63.5	0.2		0.4	
28/03/2018 12 45		0.20	0.4		63.75	0.2		0.4	
28/03/2018 13 00		0.20	0.2		64	0.4		0.2	
28/03/2018 13 15		0.20	0.2		64.25	0.4		0.2	
28/03/2018 13 30		0.20	0.2		64.5	0.2		0.2	
28/03/2018 13 45		0.20	0.2		64.75	0.4		0.4	
28/03/2018 14 00		0.20	0.2		65	0.4		0.2	
28/03/2018 14 15		0.21	0.4		65.25	0.2		0.2	
28/03/2018 14 30		0.21	0.2		65.5	0.4		0.6	
28/03/2018 14 45		0.21	0.4		65.75	0.2		0.4	
28/03/2018 15 00		0.21	0.2		66	0.2		0.2	
28/03/2018 15 15		0.22	0		66.25	0.2		0.2	
28/03/2018 15 30		0.22	0.2		66.5	0		0	
28/03/2018 15 45		0.22	0		66.75	0		0	
28/03/2018 16 00		0.22	0		67	0		0	
28/03/2018 16 15		0.22	0		67.25	0		0	
28/03/2018 16 30		0.22	0		67.5	0		0	
28/03/2018 16 45		0.22	0		67.75	0		0	
28/03/2018 17 00		0.23	0		68	0		0	
28/03/2018 17 15		0.23	0		68.25	0		0	
28/03/2018 17 30		0.23	0		68.5	0		0	
28/03/2018 17 45		0.23	0		68.75	0		0	
28/03/2018 18 00		0.23	0		69	0		0	
28/03/2018 18 15		0.23	0		69.25	0		0	
28/03/2018 18 30		0.23	0		69.5	0.2		0	
28/03/2018 18 45		0.23	0		69.75	0.4		0	
28/03/2018 19 00		0.23	0		70	0		0	
28/03/2018 19 15		0.23	0		70.25	0		0	
28/03/2018 19 30		0.23	0		70.5	0		0	
28/03/2018 19 45		0.23	0		70.75	0		0	
28/03/2018 20 00		0.23	0		71	0		0	
28/03/2018 20 15		0.23	0		71.25	0		0	
28/03/2018 20 30		0.23	0		71.5	0		0	
28/03/2018 20 45		0.24	0		71.75	0		0	
28/03/2018 21 00		0.24	0		72	0		0	
28/03/2018 21 15		0.24	0		72.25	0		0	
28/03/2018 21 30		0.24	0		72.5	0		0	
28/03/2018 21 45		0.24	0		72.75	0		0	
28/03/2018 22 00		0.24	0		73	0		0	
28/03/2018 22 15		0.24	0		73.25	0		0	
28/03/2018 22 30		0.24	0		73.5	0		0	
28/03/2018 22 45		0.25	0		73.75	0		0	
28/03/2018 23 00		0.25	0		74	0		0	
28/03/2018 23 15		0.26	0		74.25	0		0	
28/03/2018 23 30		0.26	0		74.5	0		0	
28/03/2018 23 45		0.27	0		74.75	0		0	
29/03/2018 00 00		0.27	0		75	0		0	
29/03/2018 00 15		0.28	0		75.25	0		0	
29/03/2018 00 30		0.28	0		75.5	0		0	
29/03/2018 00 45		0.29	0		75.75	0		0	
29/03/2018 01 00		0.29	0		76	0		0	
29/03/2018 01 15		0.29	0		76.25	0		0	
29/03/2018 01 30		0.29	0		76.5	0		0.2	
29/03/2018 01 45		0.30	0		76.75	0		0	
29/03/2018 02 00		0.30	0		77	0		0	
29/03/2018 02 15		0.30	0		77.25	0		0	
29/03/2018 02 30		0.30	0		77.5	0		0	
29/03/2018 02 45		0.31	0		77.75	0		0	
29/03/2018 03 00		0.31	0		78	0		0	
29/03/2018 03 15		0.31	0		78.25	0		0	
29/03/2018 03 30		0.31	0		78.5	0		0	
29/03/2018 03 45		0.31	0		78.75	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
29/03/2018 04 00		0.31	0		79	0		0	
29/03/2018 04 15		0.31	0		79.25	0		0	
29/03/2018 04 30		0.31	0		79.5	0		0	
29/03/2018 04 45		0.31	0		79.75	0		0	
29/03/2018 05 00		0.31	0		80	0		0	
29/03/2018 05 15		0.31	0		80.25	0		0	
29/03/2018 05 30		0.31	0		80.5	0		0	
29/03/2018 05 45		0.31	0		80.75	0		0	
29/03/2018 06 00		0.31	0		81	0		0	
29/03/2018 06 15		0.31	0		81.25	0		0	
29/03/2018 06 30		0.30	0		81.5	0		0	
29/03/2018 06 45		0.30	0		81.75	0		0	
29/03/2018 07 00		0.30	0		82	0		0	
29/03/2018 07 15		0.30	0		82.25	0		0	
29/03/2018 07 30		0.30	0		82.5	0		0	
29/03/2018 07 45		0.30	0		82.75	0		0	
29/03/2018 08 00		0.30	0		83	0		0	
29/03/2018 08 15		0.30	0		83.25	0		0	
29/03/2018 08 30		0.30	0		83.5	0		0	
29/03/2018 08 45		0.30	0		83.75	0		0	
29/03/2018 09 00		0.30	0	5.2	84	0	6.6	0	7.2
29/03/2018 09 15		0.30	0		84.25	0		0	
29/03/2018 09 30		0.30	0		84.5	0		0	
29/03/2018 09 45		0.30	0		84.75	0		0	
29/03/2018 10 00		0.30	0		85	0		0	
29/03/2018 10 15		0.30	0		85.25	0		0	
29/03/2018 10 30		0.30	0		85.5	0		0	
29/03/2018 10 45		0.30	0		85.75	0		0	
29/03/2018 11 00		0.29	0		86	0		0	
29/03/2018 11 15		0.29	0		86.25	0		0	
29/03/2018 11 30		0.29	0		86.5	0		0	
29/03/2018 11 45		0.29	0		86.75	0		0	
29/03/2018 12 00		0.29	0		87	0		0	
29/03/2018 12 15		0.29	0		87.25	0		0	
29/03/2018 12 30		0.29	0		87.5	0		0	
29/03/2018 12 45		0.29	0		87.75	0		0	
29/03/2018 13 00		0.29	0		88	0		0	
29/03/2018 13 15		0.29	0		88.25	0		0	
29/03/2018 13 30		0.29	0		88.5	0		0	
29/03/2018 13 45		0.29	0		88.75	0		0	
29/03/2018 14 00		0.29	0		89	0		0	
29/03/2018 14 15		0.29	0		89.25	0		0	
29/03/2018 14 30		0.29	0		89.5	0		0	
29/03/2018 14 45		0.29	0		89.75	0		0	
29/03/2018 15 00		0.29	0		90	0		0	
29/03/2018 15 15		0.29	0		90.25	0		0	
29/03/2018 15 30		0.29	0		90.5	0		0	
29/03/2018 15 45		0.29	0		90.75	0		0	
29/03/2018 16 00		0.29	0		91	0		0	
29/03/2018 16 15		0.29	0		91.25	0.2		0	
29/03/2018 16 30		0.29	0.2		91.5	0.2		0	
29/03/2018 16 45		0.29	0.2		91.75	0.2		0.2	
29/03/2018 17 00		0.29	0		92	0.4		0	
29/03/2018 17 15		0.29	0.2		92.25	0.6		0.2	
29/03/2018 17 30		0.29	0.2		92.5	0.8		0.2	
29/03/2018 17 45		0.29	0.2		92.75	0.4		0	
29/03/2018 18 00		0.29	0		93	0.4		0	
29/03/2018 18 15		0.29	0.2		93.25	0		0.4	
29/03/2018 18 30		0.29	0.8		93.5	0		0.8	
29/03/2018 18 45		0.29	0.6		93.75	0		0.6	
29/03/2018 19 00		0.29	0.4		94	0.2		0.4	
29/03/2018 19 15		0.29	0.2		94.25	0.2		0.6	
29/03/2018 19 30		0.29	0.2		94.5	0		0	
29/03/2018 19 45		0.29	0		94.75	0		0	
29/03/2018 20 00		0.29	0		95	0		0	
29/03/2018 20 15		0.29	0		95.25	0		0	
29/03/2018 20 30		0.29	0		95.5	0		0	
29/03/2018 20 45		0.29	0		95.75	0		0	
29/03/2018 21 00		0.29	0		96	0		0	
29/03/2018 21 15		0.29	0		96.25	0		0	
29/03/2018 21 30		0.29	0		96.5	0		0	
29/03/2018 21 45		0.29	0		96.75	0		0	
29/03/2018 22 00		0.30	0		97	0		0	
29/03/2018 22 15		0.30	0		97.25	0		0	
29/03/2018 22 30		0.30	0		97.5	0		0	
29/03/2018 22 45		0.30	0		97.75	0		0.4	
29/03/2018 23 00		0.31	0		98	0		0.4	
29/03/2018 23 15		0.31	0		98.25	0		0	
29/03/2018 23 30		0.31	0		98.5	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
29/03/2018 23 45	0.31		0		98.75	0		0.2	
30/03/2018 00 00	0.31		0		99	0		0	
30/03/2018 00 15	0.31		0		99.25	0		0	
30/03/2018 00 30	0.31		0.2		99.5	0		0	
30/03/2018 00 45	0.31		0		99.75	0		0	
30/03/2018 01 00	0.31		0		100	0		0	
30/03/2018 01 15	0.31		0		100.25	0		0	
30/03/2018 01 30	0.31		0		100.5	0		0	
30/03/2018 01 45	0.31		0		100.75	0		0	
30/03/2018 02 00	0.31		0		101	0		0	
30/03/2018 02 15	0.31		0		101.25	0		0	
30/03/2018 02 30	0.31		0		101.5	0		0	
30/03/2018 02 45	0.32		0		101.75	0		0	
30/03/2018 03 00	0.32		0		102	0		0	
30/03/2018 03 15	0.33		0		102.25	0		0	
30/03/2018 03 30	0.33		0		102.5	0		0	
30/03/2018 03 45	0.34		0		102.75	0		0	
30/03/2018 04 00	0.34		0		103	0		0	
30/03/2018 04 15	0.34		0		103.25	0		0	
30/03/2018 04 30	0.34		0		103.5	0		0	
30/03/2018 04 45	0.35		0		103.75	0		0.2	
30/03/2018 05 00	0.35		0		104	0		0	
30/03/2018 05 15	0.35		0		104.25	0		0	
30/03/2018 05 30	0.35		0		104.5	0		0	
30/03/2018 05 45	0.36		0		104.75	0		0	
30/03/2018 06 00	0.36		0		105	0		0	
30/03/2018 06 15	0.36		0		105.25	0		0	
30/03/2018 06 30	0.36		0		105.5	0		0	
30/03/2018 06 45	0.36		0		105.75	0		0	
30/03/2018 07 00	0.36		0		106	0		0	
30/03/2018 07 15	0.36		0		106.25	0		0	
30/03/2018 07 30	0.36		0		106.5	0		0	
30/03/2018 07 45	0.36		0		106.75	0		0	
30/03/2018 08 00	0.36		0		107	0		0	
30/03/2018 08 15	0.36		0		107.25	0		0	
30/03/2018 08 30	0.36		0		107.5	0		0	
30/03/2018 08 45	0.36		0		107.75	0		0	
30/03/2018 09 00	0.36		0	3.6	108	0	3.6	0	4.6
30/03/2018 09 15	0.36		0		108.25	0		0	
30/03/2018 09 30	0.36		0		108.5	0		0	
30/03/2018 09 45	0.36		0		108.75	0		0	
30/03/2018 10 00	0.36		0		109	0		0	
30/03/2018 10 15	0.36		0		109.25	0		0	
30/03/2018 10 30	0.36		0		109.5	0		0	
30/03/2018 10 45	0.36		0		109.75	0		0	
30/03/2018 11 00	0.36		0		110	0		0	
30/03/2018 11 15	0.36		0		110.25	0		0	
30/03/2018 11 30	0.36		0		110.5	0		0	
30/03/2018 11 45	0.36		0		110.75	0		0	
30/03/2018 12 00	0.36		0		111	0		0	
30/03/2018 12 15	0.36		0		111.25	0		0	
30/03/2018 12 30	0.36		0		111.5	0		0	
30/03/2018 12 45	0.36		0		111.75	0		0	
30/03/2018 13 00	0.36		0		112	0		0	
30/03/2018 13 15	0.36		0		112.25	0		0	
30/03/2018 13 30	0.36		0		112.5	0		0	
30/03/2018 13 45	0.36		0		112.75	0		0	
30/03/2018 14 00	0.36		0.2		113	0.2		0.2	
30/03/2018 14 15	0.36		0.2		113.25	0.2		0.2	
30/03/2018 14 30	0.36		0.6		113.5	0.6		0.6	
30/03/2018 14 45	0.36		0.6		113.75	1		0	
30/03/2018 15 00	0.36		0		114	0.8		0.2	
30/03/2018 15 15	0.36		0.4		114.25	0		0	
30/03/2018 15 30	0.36		0.2		114.5	0.6		0.2	
30/03/2018 15 45	0.36		0		114.75	0.4		0	
30/03/2018 16 00	0.36		0.4		115	0.2		0	
30/03/2018 16 15	0.36		0.2		115.25	0.2		0.2	
30/03/2018 16 30	0.36		0		115.5	0.4		0	
30/03/2018 16 45	0.36		0.4		115.75	0.6		0.2	
30/03/2018 17 00	0.37		1		116	1.2		0.6	
30/03/2018 17 15	0.37		2		116.25	1.6		1.2	
30/03/2018 17 30	0.37		1.2		116.5	0.4		0.8	
30/03/2018 17 45	0.38		0.2		116.75	0.2		0.4	
30/03/2018 18 00	0.39		0		117	0		0.2	
30/03/2018 18 15	0.40		0		117.25	0		0	
30/03/2018 18 30	0.41		0		117.5	0		0	
30/03/2018 18 45	0.42		0		117.75	0		0	
30/03/2018 19 00	0.42		0		118	0.2		0	
30/03/2018 19 15	0.43		0.4		118.25	0.4		0.2	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
30/03/2018 19 30		0.44	0		118.5	0.4		0.2	
30/03/2018 19 45		0.45	0.6		118.75	0		0.2	
30/03/2018 20 00		0.47	0.4		119	0.2		0.4	
30/03/2018 20 15		0.50	0.6		119.25	0.4		0.6	
30/03/2018 20 30		0.53	0.2		119.5	0.6		0	
30/03/2018 20 45		0.59	0.2		119.75	0.4		0.2	
30/03/2018 21 00		0.67	0		120	0		0	
30/03/2018 21 15		0.78	0		120.25	0		0	
30/03/2018 21 30		0.89	0		120.5	0		0	
30/03/2018 21 45		1.04	0		120.75	0		0	
30/03/2018 22 00		1.15	0		121	0		0	
30/03/2018 22 15		1.22	0		121.25	0		0	
30/03/2018 22 30		1.32	0		121.5	0		0	
30/03/2018 22 45		1.41	0		121.75	0		0	
30/03/2018 23 00		1.50	0		122	0		0	
30/03/2018 23 15		1.58	0		122.25	0		0	
30/03/2018 23 30		1.67	0		122.5	0		0	
30/03/2018 23 45		1.77	0		122.75	0		0	
31/03/2018 00 00		1.86	0		123	0		0	
31/03/2018 00 15		1.95	0		123.25	0		0	
31/03/2018 00 30		2.04	0		123.5	0		0	
31/03/2018 00 45		2.12	0		123.75	0		0	
31/03/2018 01 00		2.21	0		124	0		0	
31/03/2018 01 15		2.31	0		124.25	0		0	
31/03/2018 01 30		2.42	0		124.5	0		0	
31/03/2018 01 45		2.53	0		124.75	0		0	
31/03/2018 02 00		2.65	0		125	0		0	
31/03/2018 02 15		2.77	0		125.25	0		0	
31/03/2018 02 30		2.88	0		125.5	0		0	
31/03/2018 02 45		3.00	0		125.75	0		0	
31/03/2018 03 00		3.11	0		126	0		0	
31/03/2018 03 15		3.21	0		126.25	0		0	
31/03/2018 03 30		3.30	0		126.5	0		0	
31/03/2018 03 45		3.41	0		126.75	0		0	
31/03/2018 04 00		3.48	0.2		127	0		0.2	
31/03/2018 04 15		3.54	0.2		127.25	0		0	
31/03/2018 04 30		3.58	0.2		127.5	0		0	
31/03/2018 04 45		3.63	0		127.75	0		0	
31/03/2018 05 00		3.66	0		128	0		0	
31/03/2018 05 15		3.69	0		128.25	0		0	
31/03/2018 05 30		3.71	0		128.5	0		0	
31/03/2018 05 45		3.73	0		128.75	0		0.2	
31/03/2018 06 00		3.75	0		129	0.4		0	
31/03/2018 06 15		3.76	0		129.25	0		0	
31/03/2018 06 30		3.77	0		129.5	0		0	
31/03/2018 06 45		3.78	0		129.75	0		0	
31/03/2018 07 00		3.79	0		130	0		0	
31/03/2018 07 15		3.80	0		130.25	0		0	
31/03/2018 07 30		3.80	0		130.5	0		0	
31/03/2018 07 45		3.80	0		130.75	0		0	
31/03/2018 08 00		3.80	0		131	0		0	
31/03/2018 08 15		3.79	0		131.25	0		0	
31/03/2018 08 30		3.77	0		131.5	0		0	
31/03/2018 08 45		3.76	0		131.75	0		0	
31/03/2018 09 00		3.75	0	10.6	132	0	11.6	0	7.2
31/03/2018 09 15		3.73	0		132.25	0		0	
31/03/2018 09 30		3.70	0		132.5	0		0	
31/03/2018 09 45		3.66	0		132.75	0		0	
31/03/2018 10 00		3.63	0		133	0		0	
31/03/2018 10 15		3.59	0		133.25	0		0	
31/03/2018 10 30		3.54	0		133.5	0		0	
31/03/2018 10 45		3.48	0		133.75	0		0	
31/03/2018 11 00		3.39	0		134	0		0	
31/03/2018 11 15		3.31	0		134.25	0		0	
31/03/2018 11 30		3.21	0		134.5	0		0	
31/03/2018 11 45		3.11	0		134.75	0		0	
31/03/2018 12 00		2.99	0		135	0		0	
31/03/2018 12 15		2.87	0		135.25	0		0	
31/03/2018 12 30		2.76	0		135.5	0		0	
31/03/2018 12 45		2.63	0		135.75	0.2		0	
31/03/2018 13 00		2.50	0		136	0.2		0	
31/03/2018 13 15		2.38	0		136.25	0		0	
31/03/2018 13 30		2.27	0		136.5	0		0	
31/03/2018 13 45		2.15	0		136.75	0		0	
31/03/2018 14 00		2.06	0		137	0		0	
31/03/2018 14 15		1.99	0		137.25	0.4		0	
31/03/2018 14 30		1.92	0		137.5	0.2		0	
31/03/2018 14 45		1.88	0		137.75	0		0	
31/03/2018 15 00		1.82	0		138	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
31/03/2018 15 15		1.78	0		138.25	0.2		0	
31/03/2018 15 30		1.75	0		138.5	0.6		0	
31/03/2018 15 45		1.71	0		138.75	0.6		0	
31/03/2018 16 00		1.67	0		139	1.4		0	
31/03/2018 16 15		1.64	0		139.25	1.6		0	
31/03/2018 16 30		1.62	0.2		139.5	0.8		0	
31/03/2018 16 45		1.59	0.2		139.75	0.2		0	
31/03/2018 17 00		1.57	0.4		140	0.2		0.2	
31/03/2018 17 15		1.54	0.6		140.25	0.4		0	
31/03/2018 17 30		1.52	0.8		140.5	0.2		0	
31/03/2018 17 45		1.50	1		140.75	0.2		0	
31/03/2018 18 00		1.48	0.6		141	0.2		0.4	
31/03/2018 18 15		1.47	0.8		141.25	0		0.4	
31/03/2018 18 30		1.45	0.4		141.5	0		0.8	
31/03/2018 18 45		1.44	0.2		141.75	0		1.2	
31/03/2018 19 00		1.42	0		142	0		0.4	
31/03/2018 19 15		1.41	0		142.25	0		0.4	
31/03/2018 19 30		1.41	0		142.5	0		0	
31/03/2018 19 45		1.40	0.2		142.75	0		0	
31/03/2018 20 00		1.39	0		143	0		0	
31/03/2018 20 15		1.38	0		143.25	0		0	
31/03/2018 20 30		1.38	0		143.5	0		0	
31/03/2018 20 45		1.38	0		143.75	0		0.2	
31/03/2018 21 00		1.38	0		144	0		0	
31/03/2018 21 15		1.38	0		144.25	0		0	
31/03/2018 21 30		1.38	0		144.5	0		0	
31/03/2018 21 45		1.39	0		144.75	0		0	
31/03/2018 22 00		1.41	0		145	0		0	
31/03/2018 22 15		1.42	0		145.25	0		0	
31/03/2018 22 30		1.45	0		145.5	0.2		0	
31/03/2018 22 45		1.48	0.2		145.75	0		0	
31/03/2018 23 00		1.52	0		146	0		0	
31/03/2018 23 15		1.56	0.4		146.25	0		0.2	
31/03/2018 23 30		1.61	0		146.5	0		0	
31/03/2018 23 45		1.66	0.2		146.75	0		0	
01/04/2018 00 00		1.71	0		147	0		0	
01/04/2018 00 15		1.76	0		147.25	0		0	
01/04/2018 00 30		1.80	0		147.5	0		0	
01/04/2018 00 45		1.85	0.2		147.75	0		0	
01/04/2018 01 00		1.90	0		148	0		0	
01/04/2018 01 15		1.95	0		148.25	0		0	
01/04/2018 01 30		2.01	0		148.5	0		0	
01/04/2018 01 45		2.06	0		148.75	0		0	
01/04/2018 02 00		2.12	0		149	0		0	
01/04/2018 02 15		2.18	0		149.25	0		0	
01/04/2018 02 30		2.24	0		149.5	0		0	
01/04/2018 02 45		2.31	0		149.75	0		0	
01/04/2018 03 00		2.38	0		150	0		0	
01/04/2018 03 15		2.46	0		150.25	0		0	
01/04/2018 03 30		2.54	0		150.5	0		0	
01/04/2018 03 45		2.61	0		150.75	0		0	
01/04/2018 04 00		2.69	0		151	0		0	
01/04/2018 04 15		2.77	0		151.25	0		0	
01/04/2018 04 30		2.84	0		151.5	0		0	
01/04/2018 04 45		2.90	0		151.75	0		0	
01/04/2018 05 00		2.97	0		152	0		0	
01/04/2018 05 15		3.02	0		152.25	0		0	
01/04/2018 05 30		3.08	0		152.5	0		0	
01/04/2018 05 45		3.13	0		152.75	0		0	
01/04/2018 06 00		3.18	0		153	0		0	
01/04/2018 06 15		3.22	0		153.25	0		0	
01/04/2018 06 30		3.26	0		153.5	0		0	
01/04/2018 06 45		3.28	0		153.75	0		0	
01/04/2018 07 00		3.31	0		154	0		0	
01/04/2018 07 15		3.34	0		154.25	0		0	
01/04/2018 07 30		3.35	0		154.5	0		0	
01/04/2018 07 45		3.36	0		154.75	0		0	
01/04/2018 08 00		3.36	0		155	0		0	
01/04/2018 08 15		3.36	0		155.25	0		0	
01/04/2018 08 30		3.35	0		155.5	0		0	
01/04/2018 08 45		3.33	0		155.75	0		0	
01/04/2018 09 00		3.30	0		156	0		0	
01/04/2018 09 15		3.27	0		156.25	0		0	
01/04/2018 09 30		3.25	0		156.5	0		0	
01/04/2018 09 45		3.20	0		156.75	0		0	
01/04/2018 10 00		3.17	0		157	0		0	
01/04/2018 10 15		3.12	0		157.25	0		0	
01/04/2018 10 30		3.07	0		157.5	0		0	
01/04/2018 10 45		3.01	0		157.75	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
01/04/2018 11 00	2.95		0		158	0		0	
01/04/2018 11 15	2.87		0		158.25	0		0	
01/04/2018 11 30	2.81		0		158.5	0		0	
01/04/2018 11 45	2.74		0		158.75	0		0	
01/04/2018 12 00	2.65		0		159	0		0	
01/04/2018 12 15	2.58		0		159.25	0		0	
01/04/2018 12 30	2.50		0		159.5	0		0	
01/04/2018 12 45	2.41		0		159.75	0		0	
01/04/2018 13 00	2.33		0		160	0		0	
01/04/2018 13 15	2.27		0		160.25	0		0	
01/04/2018 13 30	2.19		0		160.5	0		0	
01/04/2018 13 45	2.13		0		160.75	0		0	
01/04/2018 14 00	2.06		0		161	0		0	
01/04/2018 14 15	2.01		0		161.25	0		0	
01/04/2018 14 30	1.95		0		161.5	0		0	
01/04/2018 14 45	1.92		0		161.75	0		0	
01/04/2018 15 00	1.88		0		162	0		0	
01/04/2018 15 15	1.84		0		162.25	0.2		0.2	
01/04/2018 15 30	1.81		0		162.5	0.2		0	
01/04/2018 15 45	1.77		0		162.75	0		0	
01/04/2018 16 00	1.75		0		163	0		0	
01/04/2018 16 15	1.72		0		163.25	0		0	
01/04/2018 16 30	1.70		0		163.5	0		0	
01/04/2018 16 45	1.67		0		163.75	0		0	
01/04/2018 17 00	1.65		0		164	0		0	
01/04/2018 17 15	1.63		0		164.25	0		0	
01/04/2018 17 30	1.61		0		164.5	0		0	
01/04/2018 17 45	1.59		0		164.75	0		0	
01/04/2018 18 00	1.58		0		165	0		0	
01/04/2018 18 15	1.56		0		165.25	0		0	
01/04/2018 18 30	1.54		0		165.5	0		0	
01/04/2018 18 45	1.53		0		165.75	0		0	
01/04/2018 19 00	1.51		0		166	0		0	
01/04/2018 19 15	1.51		0		166.25	0		0	
01/04/2018 19 30	1.49		0		166.5	0		0	
01/04/2018 19 45	1.49		0		166.75	0		0	
01/04/2018 20 00	1.48		0		167	0		0	
01/04/2018 20 15	1.47		0		167.25	0		0	
01/04/2018 20 30	1.47		0		167.5	0		0	
01/04/2018 20 45	1.47		0		167.75	0		0	
01/04/2018 21 00	1.47		0		168	0		0	
01/04/2018 21 15	1.48		0		168.25	0		0	
01/04/2018 21 30	1.49		0		168.5	0		0	
01/04/2018 21 45	1.50		0		168.75	0		0	
01/04/2018 22 00	1.51		0		169	0		0	
01/04/2018 22 15	1.52		0		169.25	0		0	
01/04/2018 22 30	1.54		0		169.5	0		0	
01/04/2018 22 45	1.55		0		169.75	0		0	
01/04/2018 23 00	1.56		0		170	0		0	
01/04/2018 23 15	1.58		0		170.25	0		0	
01/04/2018 23 30	1.59		0		170.5	0		0	
01/04/2018 23 45	1.61		0		170.75	0		0	
02/04/2018 00 00	1.62		0		171	0		0	
02/04/2018 00 15	1.63		0		171.25	0		0	
02/04/2018 00 30	1.65		0.2		171.5	0.2		0	
02/04/2018 00 45	1.66		0		171.75	0.2		0.2	
02/04/2018 01 00	1.67		0.2		172	0		0	
02/04/2018 01 15	1.67		0.2		172.25	0.4		0	
02/04/2018 01 30	1.68		0.2		172.5	0.2		0.2	
02/04/2018 01 45	1.68		0.4		172.75	0.6		0.4	
02/04/2018 02 00	1.69		0.4		173	0.2		0.4	
02/04/2018 02 15	1.69		0.4		173.25	0.4		0.2	
02/04/2018 02 30	1.70		0.4		173.5	0.4		0.4	
02/04/2018 02 45	1.70		0.4		173.75	0.4		0.2	
02/04/2018 03 00	1.70		0.2		174	0.2		0.2	
02/04/2018 03 15	1.70		0.2		174.25	0.4		0.4	
02/04/2018 03 30	1.70		0.4		174.5	0.4		0.2	
02/04/2018 03 45	1.69		0.4		174.75	0.8		0.2	
02/04/2018 04 00	1.69		0.6		175	0.8		0.4	
02/04/2018 04 15	1.69		0.8		175.25	1		0.8	
02/04/2018 04 30	1.69		0.8		175.5	0.8		0.6	
02/04/2018 04 45	1.70		0.6		175.75	0.8		0.6	
02/04/2018 05 00	1.71		0.6		176	0.6		0.6	
02/04/2018 05 15	1.71		0.6		176.25	0.8		0.6	
02/04/2018 05 30	1.73		0.6		176.5	0.4		0.6	
02/04/2018 05 45	1.75		0.6		176.75	0.4		0.4	
02/04/2018 06 00	1.77		0.2		177	0.2		0.2	
02/04/2018 06 15	1.81		0.2		177.25	0.2		0.2	
02/04/2018 06 30	1.85		0.2		177.5	0.2		0.2	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
02/04/2018 06 45		1.91	0.2		177.75	0.4		0	
02/04/2018 07 00		2.00	0.2		178	0.2		0.2	
02/04/2018 07 15		2.11	0.4		178.25	0.6		0.2	
02/04/2018 07 30		2.27	0.2		178.5	0.2		0.2	
02/04/2018 07 45		2.49	0.4		178.75	0.2		0.4	
02/04/2018 08 00		2.81	0.2		179	0		0.2	
02/04/2018 08 15		3.18	0		179.25	0		0.2	
02/04/2018 08 30		3.57	0.2		179.5	0.2		0	
02/04/2018 08 45		3.86	0.2		179.75	0.2		0.2	
02/04/2018 09 00		4.13	0		180	0.2		0.2	
02/04/2018 09 15		4.38	0.2		180.25	0.2		0.2	
02/04/2018 09 30		4.60	0		180.5	0		0	
02/04/2018 09 45		4.78	0.2		180.75	0.2		0.2	
02/04/2018 10 00		4.93	0.2		181	0.2		0.2	
02/04/2018 10 15		5.07	0.2		181.25	0.2		0.2	
02/04/2018 10 30		5.21	0		181.5	0		0	
02/04/2018 10 45		5.37	0		181.75	0		0	
02/04/2018 11 00		5.52	0		182	0		0	
02/04/2018 11 15		5.67	0		182.25	0		0.2	
02/04/2018 11 30		5.81	0		182.5	0		0	
02/04/2018 11 45		5.93	0		182.75	0		0	
02/04/2018 12 00		6.05	0		183	0		0	
02/04/2018 12 15		6.16	0		183.25	0		0	
02/04/2018 12 30		6.28	0		183.5	0		0	
02/04/2018 12 45		6.38	0		183.75	0		0	
02/04/2018 13 00		6.49	0		184	0		0	
02/04/2018 13 15		6.57	0		184.25	0.2		0	
02/04/2018 13 30		6.65	0.2		184.5	0		0	
02/04/2018 13 45		6.71	0		184.75	0		0	
02/04/2018 14 00		6.78	0		185	0		0	
02/04/2018 14 15		6.85	0		185.25	0		0	
02/04/2018 14 30		6.93	0		185.5	0		0	
02/04/2018 14 45		7.00	0.2		185.75	0.2		0.2	
02/04/2018 15 00		7.08	0		186	0		0	
02/04/2018 15 15		7.17	0		186.25	0		0	
02/04/2018 15 30		7.25	0		186.5	0		0	
02/04/2018 15 45		7.34	0		186.75	0		0	
02/04/2018 16 00		7.41	0		187	0		0	
02/04/2018 16 15		7.49	0		187.25	0		0.2	
02/04/2018 16 30		7.58	0.2		187.5	0		0.2	
02/04/2018 16 45		7.66	0		187.75	0.4		0.2	
02/04/2018 17 00		7.76	0.2		188	0.2		0	
02/04/2018 17 15		7.84	0.2		188.25	0		0.2	
02/04/2018 17 30		7.90	0.2		188.5	0		0.2	
02/04/2018 17 45		7.97	0		188.75	0.2		0	
02/04/2018 18 00		8.04	0		189	0		0.2	
02/04/2018 18 15		8.11	0		189.25	0		0	
02/04/2018 18 30		8.16	0		189.5	0		0	
02/04/2018 18 45		8.23	0		189.75	0		0	
02/04/2018 19 00		8.25	0.2		190	0.2		0	
02/04/2018 19 15		8.30	0		190.25	0		0	
02/04/2018 19 30		8.36	0		190.5	0		0	
02/04/2018 19 45		8.39	0		190.75	0		0	
02/04/2018 20 00		8.43	0		191	0		0	
02/04/2018 20 15		8.48	0		191.25	0		0	
02/04/2018 20 30		8.51	0		191.5	0		0	
02/04/2018 20 45		8.55	0		191.75	0		0	
02/04/2018 21 00		8.61	0		192	0		0	
02/04/2018 21 15		8.64	0		192.25	0		0	
02/04/2018 21 30		8.70	0		192.5	0		0	
02/04/2018 21 45		8.75	0		192.75	0		0	
02/04/2018 22 00		8.80	0		193	0		0	
02/04/2018 22 15		8.85	0		193.25	0		0	
02/04/2018 22 30		8.89	0		193.5	0		0	
02/04/2018 22 45		9.00	0		193.75	0		0	
02/04/2018 23 00		9.08	0		194	0		0	
02/04/2018 23 15		9.19	0		194.25	0		0.2	
02/04/2018 23 30		9.29	0		194.5	0		0	
02/04/2018 23 45		9.38	0		194.75	0		0	
03/04/2018 00 00		9.46	0		195	0		0	
03/04/2018 00 15		9.51	0		195.25	0		0	
03/04/2018 00 30		9.54	0		195.5	0		0	
03/04/2018 00 45		9.56	0		195.75	0		0	
03/04/2018 01 00		9.56	0		196	0		0	
03/04/2018 01 15		9.56	0		196.25	0		0	
03/04/2018 01 30		9.54	0		196.5	0		0	
03/04/2018 01 45		9.46	0		196.75	0		0	
03/04/2018 02 00		9.43	0		197	0		0	
03/04/2018 02 15		9.35	0.2		197.25	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
03/04/2018 02 30		9.27	0		197.5	0		0	
03/04/2018 02 45		9.14	0		197.75	0		0	
03/04/2018 03 00		9.03	0		198	0		0	
03/04/2018 03 15		8.90	0		198.25	0		0	
03/04/2018 03 30		8.84	0		198.5	0		0.2	
03/04/2018 03 45		8.78	0		198.75	0		0	
03/04/2018 04 00		8.71	0		199	0		0	
03/04/2018 04 15		8.62	0		199.25	0		0	
03/04/2018 04 30		8.56	0		199.5	0		0	
03/04/2018 04 45		8.47	0		199.75	0		0	
03/04/2018 05 00		8.38	0		200	0		0	
03/04/2018 05 15		8.29	0		200.25	0		0	
03/04/2018 05 30		8.17	0		200.5	0		0	
03/04/2018 05 45		8.08	0		200.75	0		0	
03/04/2018 06 00		7.97	0		201	0		0	
03/04/2018 06 15		7.86	0		201.25	0		0	
03/04/2018 06 30		7.75	0		201.5	0		0	
03/04/2018 06 45		7.64	0		201.75	0		0	
03/04/2018 07 00		7.53	0		202	0		0	
03/04/2018 07 15		7.42	0		202.25	0		0	
03/04/2018 07 30		7.30	0		202.5	0		0	
03/04/2018 07 45		7.19	0		202.75	0		0	
03/04/2018 08 00		7.06	0		203	0		0	
03/04/2018 08 15		6.93	0		203.25	0		0	
03/04/2018 08 30		6.80	0		203.5	0		0	
03/04/2018 08 45		6.67	0		203.75	0		0	
03/04/2018 09 00		6.54	0		204	0		0	
03/04/2018 09 15		6.41	0		204.25	0		0	
03/04/2018 09 30		6.27	0		204.5	0		0	
03/04/2018 09 45		6.14	0		204.75	0		0	
03/04/2018 10 00		6.00	0		205	0		0	
03/04/2018 10 15		5.86	0		205.25	0		0	
03/04/2018 10 30		5.73	0		205.5	0		0	
03/04/2018 10 45		5.59	0		205.75	0		0	
03/04/2018 11 00		5.44	0		206	0		0	
03/04/2018 11 15		5.29	0		206.25	0		0	
03/04/2018 11 30		5.13	0		206.5	0		0	
03/04/2018 11 45		4.97	0		206.75	0		0	
03/04/2018 12 00		4.82	0		207	0		0	
03/04/2018 12 15		4.64	0		207.25	0		0	
03/04/2018 12 30		4.46	0		207.5	0		0	
03/04/2018 12 45		4.26	0		207.75	0		0	
03/04/2018 13 00		4.06	0		208	0		0.2	
03/04/2018 13 15		3.89	0		208.25	0		0	
03/04/2018 13 30		3.70	0		208.5	0		0	
03/04/2018 13 45		3.54	0		208.75	0		0	
03/04/2018 14 00		3.33	0		209	0		0	
03/04/2018 14 15		3.11	0		209.25	0		0	
03/04/2018 14 30		2.90	0		209.5	0		0	
03/04/2018 14 45		2.70	0		209.75	0		0	
03/04/2018 15 00		2.53	0		210	0		0	
03/04/2018 15 15		2.36	0		210.25	0		0	
03/04/2018 15 30		2.23	0		210.5	0		0	
03/04/2018 15 45		2.12	0		210.75	0		0	
03/04/2018 16 00		2.03	0		211	0		0	
03/04/2018 16 15		1.96	0		211.25	0		0	
03/04/2018 16 30		1.90	0		211.5	0		0	
03/04/2018 16 45		1.86	0		211.75	0		0	
03/04/2018 17 00		1.82	0		212	0		0	
03/04/2018 17 15		1.78	0		212.25	0		0	
03/04/2018 17 30		1.75	0		212.5	0		0	
03/04/2018 17 45		1.71	0		212.75	0		0	
03/04/2018 18 00		1.69	0		213	0		0	
03/04/2018 18 15		1.66	0		213.25	0		0	
03/04/2018 18 30		1.64	0		213.5	0		0	
03/04/2018 18 45		1.62	0		213.75	0		0	
03/04/2018 19 00		1.60	0		214	0		0	
03/04/2018 19 15		1.58	0		214.25	0		0	
03/04/2018 19 30		1.55	0		214.5	0		0	
03/04/2018 19 45		1.54	0		214.75	0		0	
03/04/2018 20 00		1.52	0		215	0		0	
03/04/2018 20 15		1.50	0		215.25	0		0	
03/04/2018 20 30		1.48	0		215.5	0		0	
03/04/2018 20 45		1.47	0		215.75	0		0	
03/04/2018 21 00		1.45	0		216	0		0	
03/04/2018 21 15		1.44	0		216.25	0		0	
03/04/2018 21 30		1.42	0		216.5	0		0	
03/04/2018 21 45		1.41	0		216.75	0		0	
03/04/2018 22 00		1.39	0		217	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
03/04/2018 22 15		1.38	0		217.25	0		0	
03/04/2018 22 30		1.36	0		217.5	0		0	
03/04/2018 22 45		1.35	0		217.75	0		0	
03/04/2018 23 00		1.34	0		218	0		0	
03/04/2018 23 15		1.32	0		218.25	0		0	
03/04/2018 23 30		1.31	0		218.5	0		0	
03/04/2018 23 45		1.30	0		218.75	0		0	
04/04/2018 00 00		1.29	0		219	0		0	
04/04/2018 00 15		1.28	0		219.25	0		0	
04/04/2018 00 30		1.27	0		219.5	0		0	
04/04/2018 00 45		1.26	0		219.75	0		0	
04/04/2018 01 00		1.24	0		220	0		0	
04/04/2018 01 15		1.24	0		220.25	0		0	
04/04/2018 01 30		1.23	0		220.5	0		0	
04/04/2018 01 45		1.22	0		220.75	0		0	
04/04/2018 02 00		1.21	0		221	0		0	
04/04/2018 02 15		1.20	0		221.25	0		0	
04/04/2018 02 30		1.19	0		221.5	0		0	
04/04/2018 02 45		1.18	0		221.75	0		0	
04/04/2018 03 00		1.17	0		222	0		0	
04/04/2018 03 15		1.16	0		222.25	0		0	
04/04/2018 03 30		1.15	0		222.5	0		0	
04/04/2018 03 45		1.14	0		222.75	0		0	
04/04/2018 04 00		1.13	0		223	0		0	
04/04/2018 04 15		1.13	0		223.25	0		0	
04/04/2018 04 30		1.12	0		223.5	0		0	
04/04/2018 04 45		1.11	0		223.75	0		0	
04/04/2018 05 00		1.11	0		224	0		0	
04/04/2018 05 15		1.10	0		224.25	0		0	
04/04/2018 05 30		1.07	0		224.5	0		0	
04/04/2018 05 45		1.06	0		224.75	0		0	
04/04/2018 06 00		1.05	0		225	0		0	
04/04/2018 06 15		1.04	0		225.25	0		0	
04/04/2018 06 30		1.03	0		225.5	0		0	
04/04/2018 06 45		1.01	0		225.75	0		0	
04/04/2018 07 00		1.00	0		226	0		0	
04/04/2018 07 15		0.99	0		226.25	0		0	
04/04/2018 07 30		0.98	0		226.5	0		0	
04/04/2018 07 45		0.97	0		226.75	0		0	
04/04/2018 08 00		0.96	0		227	0		0	
04/04/2018 08 15		0.94	0		227.25	0		0	
04/04/2018 08 30		0.93	0		227.5	0		0	
04/04/2018 08 45		0.93	0		227.75	0		0	
04/04/2018 09 00		0.92	0		228	0		0	
04/04/2018 09 15		0.91	0		228.25	0		0	
04/04/2018 09 30		0.90	0		228.5	0		0	
04/04/2018 09 45		0.90	0		228.75	0		0	
04/04/2018 10 00		0.89	0		229	0		0	
04/04/2018 10 15		0.88	0		229.25	0		0	
04/04/2018 10 30		0.87	0		229.5	0		0	
04/04/2018 10 45		0.87	0		229.75	0		0	
04/04/2018 11 00		0.86	0		230	0		0	
04/04/2018 11 15		0.86	0		230.25	0		0	
04/04/2018 11 30		0.85	0		230.5	0		0	
04/04/2018 11 45		0.84	0		230.75	0		0	
04/04/2018 12 00		0.84	0		231	0		0	
04/04/2018 12 15		0.82	0		231.25	0		0	
04/04/2018 12 30		0.82	0		231.5	0		0	
04/04/2018 12 45		0.81	0		231.75	0		0	
04/04/2018 13 00		0.80	0		232	0		0	
04/04/2018 13 15		0.80	0		232.25	0		0	
04/04/2018 13 30		0.79	0		232.5	0		0	
04/04/2018 13 45		0.78	0		232.75	0		0	
04/04/2018 14 00		0.78	0		233	0		0	
04/04/2018 14 15		0.77	0		233.25	0		0	
04/04/2018 14 30		0.76	0		233.5	0		0	
04/04/2018 14 45		0.76	0		233.75	0		0	
04/04/2018 15 00		0.76	0		234	0		0	
04/04/2018 15 15		0.76	0		234.25	0		0	
04/04/2018 15 30		0.75	0		234.5	0		0	
04/04/2018 15 45		0.74	0		234.75	0		0	
04/04/2018 16 00		0.74	0		235	0		0	
04/04/2018 16 15		0.73	0		235.25	0		0	
04/04/2018 16 30		0.72	0		235.5	0		0	
04/04/2018 16 45		0.72	0		235.75	0		0	
04/04/2018 17 00		0.71	0		236	0		0	
04/04/2018 17 15		0.70	0		236.25	0		0	
04/04/2018 17 30		0.70	0		236.5	0		0	
04/04/2018 17 45		0.69	0		236.75	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
04/04/2018 18 00		0.68	0		237	0		0	
04/04/2018 18 15		0.68	0		237.25	0		0	
04/04/2018 18 30		0.67	0		237.5	0		0	
04/04/2018 18 45		0.67	0		237.75	0		0	
04/04/2018 19 00		0.66	0		238	0		0	
04/04/2018 19 15		0.65	0		238.25	0		0	
04/04/2018 19 30		0.65	0		238.5	0		0	
04/04/2018 19 45		0.65	0		238.75	0		0	
04/04/2018 20 00		0.64	0		239	0.2		0	
04/04/2018 20 15		0.64	0		239.25	0		0	
04/04/2018 20 30		0.63	0		239.5	0		0	
04/04/2018 20 45		0.62	0		239.75	0		0	
04/04/2018 21 00		0.62	0		240	0		0	
04/04/2018 21 15		0.61	0		240.25	0		0	
04/04/2018 21 30		0.61	0		240.5	0		0	
04/04/2018 21 45		0.60	0		240.75	0		0	
04/04/2018 22 00		0.60	0.2		241	0.2		0.2	
04/04/2018 22 15		0.60	0		241.25	0		0	
04/04/2018 22 30		0.59	0		241.5	0		0	
04/04/2018 22 45		0.59	0		241.75	0		0	
04/04/2018 23 00		0.58	0		242	0		0	
04/04/2018 23 15		0.58	0		242.25	0		0	
04/04/2018 23 30		0.57	0		242.5	0		0	
04/04/2018 23 45		0.56	0		242.75	0		0	
05/04/2018 00 00		0.56	0		243	0		0	
05/04/2018 00 15		0.56	0		243.25	0		0	
05/04/2018 00 30		0.56	0		243.5	0		0	
05/04/2018 00 45		0.55	0		243.75	0		0	
05/04/2018 01 00		0.55	0		244	0		0	
05/04/2018 01 15		0.54	0		244.25	0		0	
05/04/2018 01 30		0.54	0		244.5	0		0	
05/04/2018 01 45		0.53	0		244.75	0		0	
05/04/2018 02 00		0.53	0		245	0		0	
05/04/2018 02 15		0.53	0		245.25	0		0	
05/04/2018 02 30		0.53	0		245.5	0		0	
05/04/2018 02 45		0.52	0		245.75	0		0	
05/04/2018 03 00		0.52	0		246	0		0	
05/04/2018 03 15		0.51	0		246.25	0		0	
05/04/2018 03 30		0.51	0		246.5	0		0	
05/04/2018 03 45		0.50	0		246.75	0		0	
05/04/2018 04 00		0.50	0		247	0		0	
05/04/2018 04 15		0.50	0		247.25	0		0	
05/04/2018 04 30		0.50	0		247.5	0		0	
05/04/2018 04 45		0.49	0		247.75	0		0	
05/04/2018 05 00		0.49	0		248	0		0	
05/04/2018 05 15		0.48	0		248.25	0		0	
05/04/2018 05 30		0.48	0		248.5	0		0	
05/04/2018 05 45		0.48	0		248.75	0		0	
05/04/2018 06 00		0.48	0		249	0		0	
05/04/2018 06 15		0.47	0		249.25	0		0	
05/04/2018 06 30		0.47	0		249.5	0		0	
05/04/2018 06 45		0.46	0		249.75	0		0	
05/04/2018 07 00		0.46	0		250	0		0	
05/04/2018 07 15		0.46	0		250.25	0		0	
05/04/2018 07 30		0.45	0		250.5	0		0	
05/04/2018 07 45		0.45	0		250.75	0		0	
05/04/2018 08 00		0.44	0		251	0		0	
05/04/2018 08 15		0.44	0		251.25	0		0	
05/04/2018 08 30		0.44	0		251.5	0		0	
05/04/2018 08 45		0.43	0		251.75	0		0	
05/04/2018 09 00		0.43	0		252	0		0	
05/04/2018 09 15		0.42	0		252.25	0		0	
05/04/2018 09 30		0.42	0		252.5	0		0	
05/04/2018 09 45		0.42	0		252.75	0		0	
05/04/2018 10 00		0.42	0		253	0		0	
05/04/2018 10 15		0.41	0		253.25	0		0	
05/04/2018 10 30		0.41	0		253.5	0		0	
05/04/2018 10 45		0.40	0		253.75	0		0	
05/04/2018 11 00		0.40	0		254	0		0	
05/04/2018 11 15		0.40	0		254.25	0		0	
05/04/2018 11 30		0.39	0		254.5	0		0	
05/04/2018 11 45		0.39	0		254.75	0		0	
05/04/2018 12 00		0.39	0		255	0		0	
05/04/2018 12 15		0.39	0		255.25	0		0	
05/04/2018 12 30		0.38	0		255.5	0		0	
05/04/2018 12 45		0.38	0		255.75	0		0	
05/04/2018 13 00		0.37	0		256	0		0	
05/04/2018 13 15		0.37	0		256.25	0		0	
05/04/2018 13 30		0.37	0		256.5	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
05/04/2018 13 45		0.37	0		256.75	0		0	
05/04/2018 14 00		0.36	0		257	0		0	
05/04/2018 14 15		0.36	0		257.25	0		0	
05/04/2018 14 30		0.36	0		257.5	0		0	
05/04/2018 14 45		0.36	0		257.75	0		0	
05/04/2018 15 00		0.36	0		258	0		0	
05/04/2018 15 15		0.35	0		258.25	0		0	
05/04/2018 15 30		0.35	0		258.5	0		0	
05/04/2018 15 45		0.35	0		258.75	0		0	
05/04/2018 16 00		0.35	0		259	0		0	
05/04/2018 16 15		0.35	0		259.25	0		0	
05/04/2018 16 30		0.35	0		259.5	0		0	
05/04/2018 16 45		0.34	0		259.75	0		0	
05/04/2018 17 00		0.34	0		260	0		0	
05/04/2018 17 15		0.34	0		260.25	0		0	
05/04/2018 17 30		0.34	0		260.5	0		0	
05/04/2018 17 45		0.34	0		260.75	0		0	
05/04/2018 18 00		0.34	0		261	0		0	
05/04/2018 18 15		0.33	0		261.25	0		0	
05/04/2018 18 30		0.33	0		261.5	0		0	
05/04/2018 18 45		0.33	0		261.75	0		0	
05/04/2018 19 00		0.32	0		262	0		0	
05/04/2018 19 15		0.32	0		262.25	0		0	
05/04/2018 19 30		0.32	0		262.5	0		0	
05/04/2018 19 45		0.32	0		262.75	0		0	
05/04/2018 20 00		0.32	0		263	0		0	
05/04/2018 20 15		0.32	0		263.25	0		0	
05/04/2018 20 30		0.32	0		263.5	0		0	
05/04/2018 20 45		0.32	0		263.75	0		0	
05/04/2018 21 00		0.31	0		264	0		0	
05/04/2018 21 15		0.31	0		264.25	0		0	
05/04/2018 21 30		0.31	0		264.5	0		0	
05/04/2018 21 45		0.31	0		264.75	0		0	
05/04/2018 22 00		0.31	0		265	0		0	
05/04/2018 22 15		0.30	0		265.25	0		0	
05/04/2018 22 30		0.30	0		265.5	0		0	
05/04/2018 22 45		0.30	0		265.75	0		0	
05/04/2018 23 00		0.30	0		266	0		0	
05/04/2018 23 15		0.30	0		266.25	0		0	
05/04/2018 23 30		0.30	0		266.5	0		0	
05/04/2018 23 45		0.29	0		266.75	0		0	
06/04/2018 00 00		0.29	0		267	0		0	
06/04/2018 00 15		0.29	0		267.25	0		0	
06/04/2018 00 30		0.29	0		267.5	0		0	
06/04/2018 00 45		0.29	0		267.75	0		0	
06/04/2018 01 00		0.29	0		268	0		0	
06/04/2018 01 15		0.29	0		268.25	0		0	
06/04/2018 01 30		0.29	0		268.5	0		0	
06/04/2018 01 45		0.29	0		268.75	0		0	
06/04/2018 02 00		0.29	0		269	0		0	
06/04/2018 02 15		0.29	0		269.25	0		0	
06/04/2018 02 30		0.29	0		269.5	0		0	
06/04/2018 02 45		0.28	0		269.75	0		0	
06/04/2018 03 00		0.28	0		270	0		0	
06/04/2018 03 15		0.28	0		270.25	0		0	
06/04/2018 03 30		0.28	0		270.5	0		0	
06/04/2018 03 45		0.28	0		270.75	0		0	
06/04/2018 04 00		0.28	0		271	0		0	
06/04/2018 04 15		0.28	0		271.25	0		0	
06/04/2018 04 30		0.28	0		271.5	0		0	
06/04/2018 04 45		0.28	0		271.75	0		0	
06/04/2018 05 00		0.28	0		272	0		0	
06/04/2018 05 15		0.27	0		272.25	0		0	
06/04/2018 05 30		0.27	0		272.5	0		0	
06/04/2018 05 45		0.27	0		272.75	0		0	
06/04/2018 06 00		0.27	0		273	0		0	
06/04/2018 06 15		0.27	0		273.25	0		0	
06/04/2018 06 30		0.27	0		273.5	0		0	
06/04/2018 06 45		0.27	0		273.75	0		0	
06/04/2018 07 00		0.27	0		274	0		0	
06/04/2018 07 15		0.27	0		274.25	0		0	
06/04/2018 07 30		0.27	0		274.5	0		0	
06/04/2018 07 45		0.27	0		274.75	0		0	
06/04/2018 08 00		0.27	0		275	0		0	
06/04/2018 08 15		0.27	0		275.25	0		0	
06/04/2018 08 30		0.27	0		275.5	0		0	
06/04/2018 08 45		0.27	0		275.75	0		0	
06/04/2018 09 00		0.26	0		276	0		0	
06/04/2018 09 15		0.26	0		276.25	0		0	

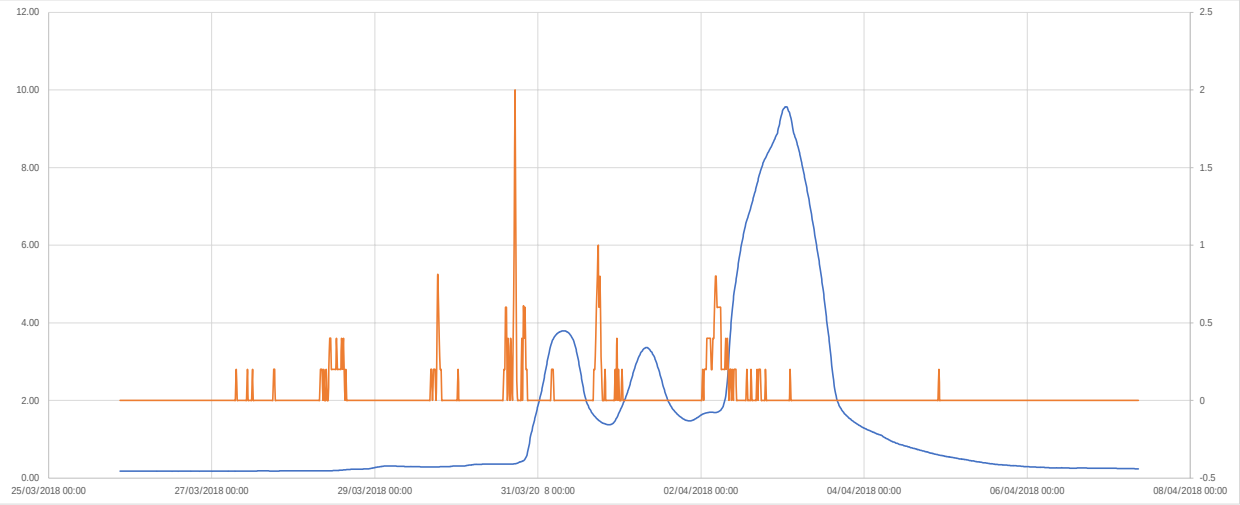
start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
06/04/2018 09 30		0.26	0		276.5	0		0	
06/04/2018 09 45		0.26	0		276.75	0		0	
06/04/2018 10 00		0.27	0		277	0		0	
06/04/2018 10 15		0.27	0		277.25	0		0	
06/04/2018 10 30		0.26	0		277.5	0		0	
06/04/2018 10 45		0.26	0		277.75	0		0	
06/04/2018 11 00		0.26	0		278	0		0	
06/04/2018 11 15		0.26	0		278.25	0		0	
06/04/2018 11 30		0.26	0		278.5	0		0	
06/04/2018 11 45		0.26	0		278.75	0		0	
06/04/2018 12 00		0.26	0		279	0		0	
06/04/2018 12 15		0.26	0		279.25	0		0	
06/04/2018 12 30		0.26	0		279.5	0		0	
06/04/2018 12 45		0.26	0		279.75	0		0	
06/04/2018 13 00		0.26	0		280	0		0	
06/04/2018 13 15		0.26	0		280.25	0		0	
06/04/2018 13 30		0.26	0		280.5	0		0	
06/04/2018 13 45		0.26	0		280.75	0		0	
06/04/2018 14 00		0.26	0		281	0		0	
06/04/2018 14 15		0.26	0		281.25	0		0	
06/04/2018 14 30		0.26	0		281.5	0		0	
06/04/2018 14 45		0.26	0		281.75	0		0	
06/04/2018 15 00		0.26	0		282	0		0	
06/04/2018 15 15		0.26	0		282.25	0		0	
06/04/2018 15 30		0.26	0		282.5	0		0	
06/04/2018 15 45		0.26	0		282.75	0		0	
06/04/2018 16 00		0.26	0		283	0		0	
06/04/2018 16 15		0.26	0		283.25	0		0	
06/04/2018 16 30		0.26	0		283.5	0		0	
06/04/2018 16 45		0.26	0		283.75	0		0	
06/04/2018 17 00		0.26	0		284	0		0	
06/04/2018 17 15		0.26	0		284.25	0		0	
06/04/2018 17 30		0.26	0		284.5	0		0	
06/04/2018 17 45		0.26	0		284.75	0		0	
06/04/2018 18 00		0.26	0		285	0		0	
06/04/2018 18 15		0.26	0		285.25	0		0	
06/04/2018 18 30		0.26	0		285.5	0		0	
06/04/2018 18 45		0.26	0		285.75	0		0	
06/04/2018 19 00		0.26	0		286	0		0	
06/04/2018 19 15		0.26	0		286.25	0		0	
06/04/2018 19 30		0.26	0		286.5	0		0	
06/04/2018 19 45		0.26	0		286.75	0		0	
06/04/2018 20 00		0.26	0		287	0		0	
06/04/2018 20 15		0.26	0		287.25	0		0	
06/04/2018 20 30		0.26	0		287.5	0		0	
06/04/2018 20 45		0.26	0		287.75	0		0	
06/04/2018 21 00		0.26	0		288	0		0	
06/04/2018 21 15		0.26	0		288.25	0		0	
06/04/2018 21 30		0.26	0		288.5	0		0	
06/04/2018 21 45		0.26	0		288.75	0		0	
06/04/2018 22 00		0.26	0		289	0		0	
06/04/2018 22 15		0.26	0		289.25	0		0	
06/04/2018 22 30		0.26	0		289.5	0		0	
06/04/2018 22 45		0.26	0		289.75	0		0	
06/04/2018 23 00		0.25	0		290	0		0	
06/04/2018 23 15		0.25	0		290.25	0		0	
06/04/2018 23 30		0.25	0		290.5	0		0	
06/04/2018 23 45		0.25	0		290.75	0		0	
07/04/2018 00 00		0.25	0		291	0		0	
07/04/2018 00 15		0.25	0		291.25	0		0	
07/04/2018 00 30		0.25	0		291.5	0		0	
07/04/2018 00 45		0.25	0		291.75	0		0	
07/04/2018 01 00		0.25	0		292	0		0	
07/04/2018 01 15		0.25	0		292.25	0		0	
07/04/2018 01 30		0.25	0		292.5	0		0	
07/04/2018 01 45		0.25	0		292.75	0		0	
07/04/2018 02 00		0.25	0		293	0		0	
07/04/2018 02 15		0.25	0		293.25	0		0	
07/04/2018 02 30		0.25	0		293.5	0		0	
07/04/2018 02 45		0.25	0		293.75	0		0	
07/04/2018 03 00		0.25	0		294	0		0	
07/04/2018 03 15		0.25	0		294.25	0		0	
07/04/2018 03 30		0.25	0		294.5	0		0	
07/04/2018 03 45		0.25	0		294.75	0		0	
07/04/2018 04 00		0.25	0		295	0		0	
07/04/2018 04 15		0.25	0		295.25	0		0	
07/04/2018 04 30		0.25	0		295.5	0		0	
07/04/2018 04 45		0.25	0		295.75	0		0	
07/04/2018 05 00		0.25	0		296	0		0	

start of event	30/03/2018 14 00

	Middleton		Benhall	Daily Total		Earl Soham	Daily Total	Thorpeness	Daily Total
Date & Time	Flow (m^3/s)		Rainfall (mm)	Rainfall (mm)	Hours	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
07/04/2018 05 15		0.24	0		296.25	0		0	
07/04/2018 05 30		0.24	0		296.5	0		0	
07/04/2018 05 45		0.24	0		296.75	0		0	
07/04/2018 06 00		0.24	0		297	0		0	
07/04/2018 06 15		0.24	0		297.25	0		0	
07/04/2018 06 30		0.24	0		297.5	0		0	
07/04/2018 06 45		0.24	0		297.75	0		0	
07/04/2018 07 00		0.24	0		298	0		0	
07/04/2018 07 15		0.24	0		298.25	0		0	
07/04/2018 07 30		0.24	0		298.5	0		0	
07/04/2018 07 45		0.24	0		298.75	0		0	
07/04/2018 08 00		0.24	0		299	0		0	
07/04/2018 08 15		0.24	0		299.25	0		0	
07/04/2018 08 30		0.24	0		299.5	0		0	
07/04/2018 08 45		0.24	0		299.75	0		0	

start of event	30/03/2018 14 00



SAAR	592	mm
AREA	50.16	Km2

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capac ty in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
W/E 03/04/2018	1.4	mm
W/E 10/04/2018	0	mm

Source of Rainfall event data.

Gauge	Easting	Northing	Distance from Catchment Centroid (m)	Reciprocal	Weighting
Benhall	38166	60602	8878	0.000112638	0.4462
Soham	23243	62717	15768	6.34196E-05	0.2512
Thorpeness	60012	78834	13088	7.64059E-05	0.3026
			Total	0.000252463	1.0000

TBR RG

Antecedent Daily RF totals 9am 9am	**Benhall**	**Soham**	**Thorpeness**
Date	**Total RF (mm)**	**Total RF (mm)**	**Total RF (mm)**
25/03/2018	0	0	0
26/03/2018	0.2	0.4	0.2
27/03/2018	1.6	1.6	1
28/03/2018	5.2	6.6	7.2
29/03/2018	3.6	3.6	4.6

Rainall Event Depth P (mm)	31
Event duration (hours)	77

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**25/03/2018**	**26/03/2018**	**27/03/2018**	**28 03/2018**	**29/03/2018**
Benhall	592	0.4462	0	0.2	1.6	5.2	3.6
Soham	592	0.2512	0	0.4	1.6	6.6	3.6
Thorpeness	592	0.3026	0	0.2	1	7.2	4.6
Average Daily rainfall totals			0	0.266666667	1.4	6.333333333	3.933333333

Gauge	**SAAR**	**Weight**	**25/03/2018**	**26/03/2018**	**27/03/2018**	**28 03/2018**	**29/03/2018**
Benhall	592	0.4462	0	0.000337838	0.002702703	0.008783784	0.006081081
Soham	592	0.2512	0	0.000675676	0.002702703	0.011148649	0.006081081
Thorpeness	592	0.3026	0	0.000337838	0.001689189	0.012162162	0.00777027

Gauge	**SAAR**	**Weight**	**25/03/2018**	**26/03/2018**	**27/03/2018**	**28 03/2018**	**29/03/2018**
Benhall	592	0.4462	0	0.000150728	0.001205826	0.003918935	0.002713109
Soham	592	0.2512	0	0.000169732	0.000678927	0.002800575	0.001527586
Thorpeness	592	0.3026	0	0.000102244	0.000511218	0.003680773	0.002351605

Gauge	**SAAR**	**Weight**	**25/03/2018**	**26/03/2018**	**27/03/2018**	**28 03/2018**	**29/03/2018**
Benhall	592	0.4462	0	0.089231125	0.713849004	2.320009262	1.606160258
Soham	592	0.2512	0	0.100481219	0.401924877	1.657940116	0.904330972
Thorpeness	592	0.3026	0	0.060528265	0.302641325	2.179017539	1.392150094
Catchment Average Antecedent RF mm			0	0.25024061	1.418415205	6.156966917	3.902641325

Date	**Catchment Average Antecedent Rainfall (mm)**	
25/03/2018	0.00	d-5
26/03/2018	0.25	d-4
27/03/2018	1.42	d-3
28/03/2018	6.16	d-2
29/03/2018	3.90	d-1

API5
5.21 mm 5.209261781 mm / day

CWI Prior to Event April 2018 Event at Middleton
CWI 125 + API15 - SMD
SMD 1.4 mm
CWI 128.8092618 mm

FEH Parameter										
SPR	54.0	%					**URBEXT2000**	0.0084	As URBEXT2000 value is essentially rural the PR is the same as the PRrural value	
PRrural	55.0	%		P=Storm Depth	31	mm	**PR**	59	taken from PR calculations sheet using Benhall TBR RG record	
DPRrain	0	%		SPR	54.00978906		**DPRrain**	0	DPRrain is 0, as P<40mm	
DPRcwi	0.95	CWI	128.809				**DPRcwi**	1.0		
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural							**SPR**	54 0		
PR	55.0	%					**DPRrain**	0.45(P-40)^0.7	#NUM!	
PRrural	55.0	%					**P**	31		54.9621045
CWI	128.8	mm					**CWI**	128.8		
BF	0.00001		Baseflow equation taken from FEH				**SPR**	54 0		
	-1254						**PR**	55 0		
	1778 5		524 5 0.00525							
AREA	50.16		**0.26309** m3s-1				**SPRHOST**	41.05	from FEH Catchment descriptors & SPRHOST is the same as SPRcds	
SPR	54.0						**Duration (hours)**	77		
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	54 0									
PRrural	55 0									

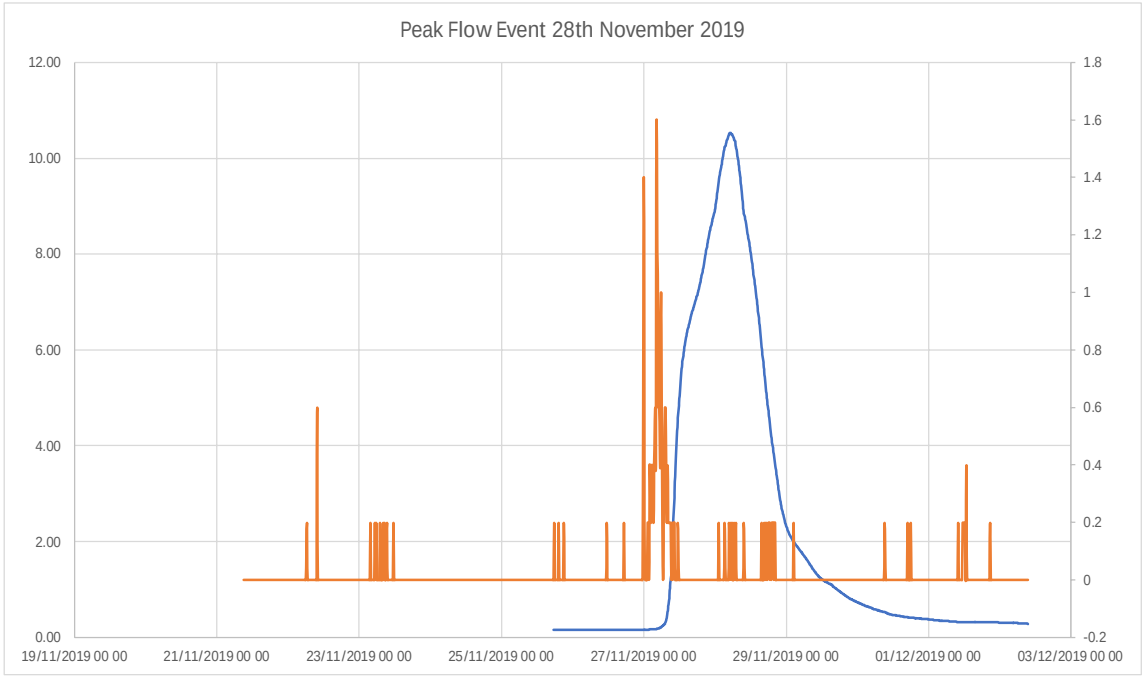
Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
30-Mar-18	02-Apr-18	77.00	5.2	1.4	128.8	55.0	1.0	0.0	54.0	59	41.05

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
21/11/2019 09:00		0						
21/11/2019 09:15		0						
21/11/2019 09:30		0						
21/11/2019 09:45		0						
21/11/2019 10:00		0						
21/11/2019 10:15		0						
21/11/2019 10:30		0						
21/11/2019 10:45		0						
21/11/2019 11:00		0						
21/11/2019 11:15		0						
21/11/2019 11:30		0						
21/11/2019 11:45		0						
21/11/2019 12:00		0						
21/11/2019 12:15		0						
21/11/2019 12:30		0						
21/11/2019 12:45		0						
21/11/2019 13:00		0						
21/11/2019 13:15		0						
21/11/2019 13:30		0						
21/11/2019 13:45		0						
21/11/2019 14:00		0						
21/11/2019 14:15		0						
21/11/2019 14:30		0						
21/11/2019 14:45		0						
21/11/2019 15:00		0						
21/11/2019 15:15		0						
21/11/2019 15:30		0						
21/11/2019 15:45		0						
21/11/2019 16:00		0						
21/11/2019 16:15		0						
21/11/2019 16:30		0						
21/11/2019 16:45		0						
21/11/2019 17:00		0						
21/11/2019 17:15		0						
21/11/2019 17:30		0						
21/11/2019 17:45		0						
21/11/2019 18:00		0						
21/11/2019 18:15		0						
21/11/2019 18:30		0						
21/11/2019 18:45		0						
21/11/2019 19:00		0						
21/11/2019 19:15		0						
21/11/2019 19:30		0						
21/11/2019 19:45		0						
21/11/2019 20:00		0						
21/11/2019 20:15		0						
21/11/2019 20:30		0						
21/11/2019 20:45		0						
21/11/2019 21:00		0						
21/11/2019 21:15		0						
21/11/2019 21:30		0						
21/11/2019 21:45		0						
21/11/2019 22:00		0						
21/11/2019 22:15		0						

	DATE TIME
start of event	26/11/2019 23:45
end of event	27/11/2019 11:30
duration hours	11.75
total RF mm	17 2
SMD W/E AVERAGE	**mm**
26/11/2019	0

DATE	API5	Benhall Daily Totals
25/11/2019	d-1	0.6
24/11/2019	d-2	0
23/11/2019	d-3	0.4
22/11/2019	d-4	1.8
21/11/2019	d-5	0.2
		3



Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
21/11/2019 22:30		0						
21/11/2019 22:45		0						
21/11/2019 23:00		0						
21/11/2019 23:15		0						
21/11/2019 23:30		0						
21/11/2019 23:45		0						
22/11/2019 00:00		0						
22/11/2019 00:15		0						
22/11/2019 00:30		0						
22/11/2019 00:45		0						
22/11/2019 01:00		0						
22/11/2019 01:15		0						
22/11/2019 01:30		0						
22/11/2019 01:45		0						
22/11/2019 02:00		0						
22/11/2019 02:15		0						
22/11/2019 02:30		0						
22/11/2019 02:45		0						
22/11/2019 03:00		0						
22/11/2019 03:15		0						
22/11/2019 03:30		0						
22/11/2019 03:45		0						
22/11/2019 04:00		0						
22/11/2019 04:15		0						
22/11/2019 04:30		0						
22/11/2019 04:45		0						
22/11/2019 05:00		0						
22/11/2019 05:15		0						
22/11/2019 05:30		0						
22/11/2019 05:45		0						
22/11/2019 06:00		0						
22/11/2019 06:15		0.2						
22/11/2019 06:30		0						
22/11/2019 06:45		0						
22/11/2019 07:00		0						
22/11/2019 07:15		0						
22/11/2019 07:30		0						
22/11/2019 07:45		0						
22/11/2019 08:00		0						
22/11/2019 08:15		0						
22/11/2019 08:30		0						
22/11/2019 08:45		0						
22/11/2019 09:00		0		0 2				
22/11/2019 09:15		0						
22/11/2019 09:30		0						
22/11/2019 09:45		0.6						
22/11/2019 10:00		0						
22/11/2019 10:15		0						
22/11/2019 10:30		0						
22/11/2019 10:45		0						
22/11/2019 11:00		0						
22/11/2019 11:15		0						
22/11/2019 11:30		0						
22/11/2019 11:45		0						

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
22/11/2019 12:00		0						
22/11/2019 12:15		0						
22/11/2019 12:30		0						
22/11/2019 12:45		0						
22/11/2019 13:00		0						
22/11/2019 13:15		0						
22/11/2019 13:30		0						
22/11/2019 13:45		0						
22/11/2019 14:00		0						
22/11/2019 14:15		0						
22/11/2019 14:30		0						
22/11/2019 14:45		0						
22/11/2019 15:00		0						
22/11/2019 15:15		0						
22/11/2019 15:30		0						
22/11/2019 15:45		0						
22/11/2019 16:00		0						
22/11/2019 16:15		0						
22/11/2019 16:30		0						
22/11/2019 16:45		0						
22/11/2019 17:00		0						
22/11/2019 17:15		0						
22/11/2019 17:30		0						
22/11/2019 17:45		0						
22/11/2019 18:00		0						
22/11/2019 18:15		0						
22/11/2019 18:30		0						
22/11/2019 18:45		0						
22/11/2019 19:00		0						
22/11/2019 19:15		0						
22/11/2019 19:30		0						
22/11/2019 19:45		0						
22/11/2019 20:00		0						
22/11/2019 20:15		0						
22/11/2019 20:30		0						
22/11/2019 20:45		0						
22/11/2019 21:00		0						
22/11/2019 21:15		0						
22/11/2019 21:30		0						
22/11/2019 21:45		0						
22/11/2019 22:00		0						
22/11/2019 22:15		0						
22/11/2019 22:30		0						
22/11/2019 22:45		0						
22/11/2019 23:00		0						
22/11/2019 23:15		0						
22/11/2019 23:30		0						
22/11/2019 23:45		0						
23/11/2019 00:00		0						
23/11/2019 00:15		0						
23/11/2019 00:30		0						
23/11/2019 00:45		0						
23/11/2019 01:00		0						
23/11/2019 01:15		0						

	DATE TIME

0

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
23/11/2019 01:30		0						
23/11/2019 01:45		0						
23/11/2019 02:00		0						
23/11/2019 02:15		0						
23/11/2019 02:30		0						
23/11/2019 02:45		0						
23/11/2019 03:00		0						
23/11/2019 03:15		0						
23/11/2019 03:30		0						
23/11/2019 03:45		0.2						
23/11/2019 04:00		0						
23/11/2019 04:15		0						
23/11/2019 04:30		0						
23/11/2019 04:45		0						
23/11/2019 05:00		0						
23/11/2019 05:15		0.2						
23/11/2019 05:30		0						
23/11/2019 05:45		0.2						
23/11/2019 06:00		0						
23/11/2019 06:15		0						
23/11/2019 06:30		0						
23/11/2019 06:45		0						
23/11/2019 07:00		0.2						
23/11/2019 07:15		0						
23/11/2019 07:30		0						
23/11/2019 07:45		0						
23/11/2019 08:00		0.2						
23/11/2019 08:15		0						
23/11/2019 08:30		0.2						
23/11/2019 08:45		0						
23/11/2019 09:00		0		1 8				
23/11/2019 09:15		0.2						
23/11/2019 09:30		0						
23/11/2019 09:45		0						
23/11/2019 10:00		0						
23/11/2019 10:15		0						
23/11/2019 10:30		0						
23/11/2019 10:45		0						
23/11/2019 11:00		0						
23/11/2019 11:15		0						
23/11/2019 11:30		0.2						
23/11/2019 11:45		0						
23/11/2019 12:00		0						
23/11/2019 12:15		0						
23/11/2019 12:30		0						
23/11/2019 12:45		0						
23/11/2019 13:00		0						
23/11/2019 13:15		0						
23/11/2019 13:30		0						
23/11/2019 13:45		0						
23/11/2019 14:00		0						
23/11/2019 14:15		0						
23/11/2019 14:30		0						
23/11/2019 14:45		0						

	DATE TIME

0

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
23/11/2019 15:00		0						
23/11/2019 15:15		0						
23/11/2019 15:30		0						
23/11/2019 15:45		0						
23/11/2019 16:00		0						
23/11/2019 16:15		0						
23/11/2019 16:30		0						
23/11/2019 16:45		0						
23/11/2019 17:00		0						
23/11/2019 17:15		0						
23/11/2019 17:30		0						
23/11/2019 17:45		0						
23/11/2019 18:00		0						
23/11/2019 18:15		0						
23/11/2019 18:30		0						
23/11/2019 18:45		0						
23/11/2019 19:00		0						
23/11/2019 19:15		0						
23/11/2019 19:30		0						
23/11/2019 19:45		0						
23/11/2019 20:00		0						
23/11/2019 20:15		0						
23/11/2019 20:30		0						
23/11/2019 20:45		0						
23/11/2019 21:00		0						
23/11/2019 21:15		0						
23/11/2019 21:30		0						
23/11/2019 21:45		0						
23/11/2019 22:00		0						
23/11/2019 22:15		0						
23/11/2019 22:30		0						
23/11/2019 22:45		0						
23/11/2019 23:00		0						
23/11/2019 23:15		0						
23/11/2019 23:30		0						
23/11/2019 23:45		0						
24/11/2019 00:00		0						
24/11/2019 00:15		0						
24/11/2019 00:30		0						
24/11/2019 00:45		0						
24/11/2019 01:00		0						
24/11/2019 01:15		0						
24/11/2019 01:30		0						
24/11/2019 01:45		0						
24/11/2019 02:00		0						
24/11/2019 02:15		0						
24/11/2019 02:30		0						
24/11/2019 02:45		0						
24/11/2019 03:00		0						
24/11/2019 03:15		0						
24/11/2019 03:30		0						
24/11/2019 03:45		0						
24/11/2019 04:00		0						
24/11/2019 04:15		0						

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
24/11/2019 04:30		0						
24/11/2019 04:45		0						
24/11/2019 05:00		0						
24/11/2019 05:15		0						
24/11/2019 05:30		0						
24/11/2019 05:45		0						
24/11/2019 06:00		0						
24/11/2019 06:15		0						
24/11/2019 06:30		0						
24/11/2019 06:45		0						
24/11/2019 07:00		0						
24/11/2019 07:15		0						
24/11/2019 07:30		0						
24/11/2019 07:45		0						
24/11/2019 08:00		0						
24/11/2019 08:15		0						
24/11/2019 08:30		0						
24/11/2019 08:45		0						
24/11/2019 09:00		0		0.4				
24/11/2019 09:15		0						
24/11/2019 09:30		0						
24/11/2019 09:45		0						
24/11/2019 10:00		0						
24/11/2019 10:15		0						
24/11/2019 10:30		0						
24/11/2019 10:45		0						
24/11/2019 11:00		0						
24/11/2019 11:15		0						
24/11/2019 11:30		0						
24/11/2019 11:45		0						
24/11/2019 12:00		0						
24/11/2019 12:15		0						
24/11/2019 12:30		0						
24/11/2019 12:45		0						
24/11/2019 13:00		0						
24/11/2019 13:15		0						
24/11/2019 13:30		0						
24/11/2019 13:45		0						
24/11/2019 14:00		0						
24/11/2019 14:15		0						
24/11/2019 14:30		0						
24/11/2019 14:45		0						
24/11/2019 15:00		0						
24/11/2019 15:15		0						
24/11/2019 15:30		0						
24/11/2019 15:45		0						
24/11/2019 16:00		0						
24/11/2019 16:15		0						
24/11/2019 16:30		0						
24/11/2019 16:45		0						
24/11/2019 17:00		0						
24/11/2019 17:15		0						
24/11/2019 17:30		0						
24/11/2019 17:45		0						

	DATE TIME

0

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
24/11/2019 18:00		0						
24/11/2019 18:15		0						
24/11/2019 18:30		0						
24/11/2019 18:45		0						
24/11/2019 19:00		0						
24/11/2019 19:15		0						
24/11/2019 19:30		0						
24/11/2019 19:45		0						
24/11/2019 20:00		0						
24/11/2019 20:15		0						
24/11/2019 20:30		0						
24/11/2019 20:45		0						
24/11/2019 21:00		0						
24/11/2019 21:15		0						
24/11/2019 21:30		0						
24/11/2019 21:45		0						
24/11/2019 22:00		0						
24/11/2019 22:15		0						
24/11/2019 22:30		0						
24/11/2019 22:45		0						
24/11/2019 23:00		0						
24/11/2019 23:15		0						
24/11/2019 23:30		0						
24/11/2019 23:45		0						
25/11/2019 00:00		0						
25/11/2019 00:15		0						
25/11/2019 00:30		0						
25/11/2019 00:45		0						
25/11/2019 01:00		0						
25/11/2019 01:15		0						
25/11/2019 01:30		0						
25/11/2019 01:45		0						
25/11/2019 02:00		0						
25/11/2019 02:15		0						
25/11/2019 02:30		0						
25/11/2019 02:45		0						
25/11/2019 03:00		0						
25/11/2019 03:15		0						
25/11/2019 03:30		0						
25/11/2019 03:45		0						
25/11/2019 04:00		0						
25/11/2019 04:15		0						
25/11/2019 04:30		0						
25/11/2019 04:45		0						
25/11/2019 05:00		0						
25/11/2019 05:15		0						
25/11/2019 05:30		0						
25/11/2019 05:45		0						
25/11/2019 06:00		0						
25/11/2019 06:15		0						
25/11/2019 06:30		0						
25/11/2019 06:45		0						
25/11/2019 07:00		0						
25/11/2019 07:15		0						

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
25/11/2019 07:30		0						
25/11/2019 07:45		0						
25/11/2019 08:00		0						
25/11/2019 08:15		0						
25/11/2019 08:30		0						
25/11/2019 08:45		0						
25/11/2019 09:00		0		0				
25/11/2019 09:15		0						
25/11/2019 09:30		0						
25/11/2019 09:45		0						
25/11/2019 10:00		0						
25/11/2019 10:15		0						
25/11/2019 10:30		0						
25/11/2019 10:45		0						
25/11/2019 11:00		0						
25/11/2019 11:15		0						
25/11/2019 11:30		0						
25/11/2019 11:45		0						
25/11/2019 12:00		0						
25/11/2019 12:15		0						
25/11/2019 12:30		0						
25/11/2019 12:45		0						
25/11/2019 13:00		0						
25/11/2019 13:15		0						
25/11/2019 13:30		0						
25/11/2019 13:45		0						
25/11/2019 14:00		0						
25/11/2019 14:15		0						
25/11/2019 14:30		0						
25/11/2019 14:45		0						
25/11/2019 15:00		0						
25/11/2019 15:15		0						
25/11/2019 15:30		0						
25/11/2019 15:45		0						
25/11/2019 16:00		0						
25/11/2019 16:15		0						
25/11/2019 16:30		0						
25/11/2019 16:45		0						
25/11/2019 17:00		0						
25/11/2019 17:15		0						
25/11/2019 17:30	0.17	0	0		0		0.2	
25/11/2019 17:45	0.17	0.2	0.25		0		0	
25/11/2019 18:00	0.17	0	0.5		0		0	
25/11/2019 18:15	0.17	0	0.75		0		0	
25/11/2019 18:30	0.17	0	1		0		0	
25/11/2019 18:45	0.17	0	1.25		0		0	
25/11/2019 19:00	0.17	0	1.5		0		0	
25/11/2019 19:15	0.17	0.2	1.75		0		0	
25/11/2019 19:30	0.17	0	2		0		0	
25/11/2019 19:45	0.17	0	2.25		0		0	
25/11/2019 20:00	0.17	0	2.5		0		0	
25/11/2019 20:15	0.17	0	2.75		0		0	
25/11/2019 20:30	0.17	0	3		0		0	
25/11/2019 20:45	0.17	0	3.25		0		0	

	DATE TIME
	0

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
25/11/2019 21:00	0.17	0.2	3.5		0		0	
25/11/2019 21:15	0.17	0	3.75		0		0	
25/11/2019 21:30	0.17	0	4		0		0	
25/11/2019 21:45	0.17	0	4.25		0		0	
25/11/2019 22:00	0.17	0	4.5		0		0	
25/11/2019 22:15	0.17	0	4.75		0		0	
25/11/2019 22:30	0.17	0	5		0		0	
25/11/2019 22:45	0.17	0	5.25		0		0	
25/11/2019 23:00	0.17	0	5.5		0		0	
25/11/2019 23:15	0.17	0	5.75		0		0	
25/11/2019 23:30	0.17	0	6		0		0	
25/11/2019 23:45	0.17	0	6.25		0		0	
26/11/2019 00:00	0.17	0	6.5		0		0	
26/11/2019 00:15	0.17	0	6.75		0		0	
26/11/2019 00:30	0.17	0	7		0		0	
26/11/2019 00:45	0.17	0	7.25		0		0	
26/11/2019 01:00	0.17	0	7.5		0		0	
26/11/2019 01:15	0.17	0	7.75		0		0	
26/11/2019 01:30	0.17	0	8		0		0	
26/11/2019 01:45	0.17	0	8.25		0		0	
26/11/2019 02:00	0.17	0	8.5		0		0	
26/11/2019 02:15	0.17	0	8.75		0		0	
26/11/2019 02:30	0.17	0	9		0		0	
26/11/2019 02:45	0.17	0	9.25		0		0	
26/11/2019 03:00	0.17	0	9.5		0 2		0	
26/11/2019 03:15	0.17	0	9.75		0		0	
26/11/2019 03:30	0.17	0	10		0		0	
26/11/2019 03:45	0.17	0	10.25		0		0	
26/11/2019 04:00	0.17	0	10.5		0		0	
26/11/2019 04:15	0.17	0	10.75		0		0	
26/11/2019 04:30	0.17	0	11		0		0	
26/11/2019 04:45	0.17	0	11.25		0 2		0	
26/11/2019 05:00	0.17	0	11.5		0		0	
26/11/2019 05:15	0.17	0	11.75		0		0	
26/11/2019 05:30	0.17	0	12		0 2		0	
26/11/2019 05:45	0.17	0	12.25		0		0	
26/11/2019 06:00	0.17	0	12.5		0		0	
26/11/2019 06:15	0.17	0	12.75		0 2		0	
26/11/2019 06:30	0.17	0	13		0		0	
26/11/2019 06:45	0.17	0	13.25		0		0	
26/11/2019 07:00	0.17	0	13.5		0		0	
26/11/2019 07:15	0.17	0	13.75		0		0	
26/11/2019 07:30	0.17	0	14		0		0	
26/11/2019 07:45	0.16	0	14.25		0 2		0	
26/11/2019 08:00	0.16	0	14.5		0		0.2	
26/11/2019 08:15	0.16	0	14.75		0		0	
26/11/2019 08:30	0.16	0	15		0 2		0	
26/11/2019 08:45	0.16	0	15.25		0.4		0	
26/11/2019 09:00	0.16	0	15.5	0.6	0.4		0	
26/11/2019 09:15	0.16	0	15.75		0		0	
26/11/2019 09:30	0.16	0	16		0		0	
26/11/2019 09:45	0.16	0	16.25		0 2		0	
26/11/2019 10:00	0.16	0	16.5		0		0	
26/11/2019 10:15	0.16	0	16.75		0 2		0	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
26/11/2019 10:30	0.16	0	17		0		0	
26/11/2019 10:45	0.16	0	17.25		0		0	
26/11/2019 11:00	0.16	0	17.5		0		0	
26/11/2019 11:15	0.16	0	17.75		0		0	
26/11/2019 11:30	0.16	0.2	18		0		0.2	
26/11/2019 11:45	0.16	0	18.25		0		0.2	
26/11/2019 12:00	0.16	0	18.5		0		0	
26/11/2019 12:15	0.16	0	18.75		0		0	
26/11/2019 12:30	0.16	0	19		0		0	
26/11/2019 12:45	0.16	0	19.25		0 2		0	
26/11/2019 13:00	0.16	0	19.5		0		0	
26/11/2019 13:15	0.16	0	19.75		0		0	
26/11/2019 13:30	0.16	0	20		0		0	
26/11/2019 13:45	0.16	0	20.25		0		0	
26/11/2019 14:00	0.16	0	20.5		0		0	
26/11/2019 14:15	0.16	0	20.75		0		0	
26/11/2019 14:30	0.16	0	21		0		0	
26/11/2019 14:45	0.16	0	21.25		0		0	
26/11/2019 15:00	0.16	0	21.5		0		0	
26/11/2019 15:15	0.16	0	21.75		0		0	
26/11/2019 15:30	0.16	0	22		0		0	
26/11/2019 15:45	0.16	0	22.25		0		0	
26/11/2019 16:00	0.16	0	22.5		0		0	
26/11/2019 16:15	0.17	0	22.75		0		0	
26/11/2019 16:30	0.17	0	23		0		0	
26/11/2019 16:45	0.17	0	23.25		0		0	
26/11/2019 17:00	0.17	0	23.5		0		0	
26/11/2019 17:15	0.17	0.2	23.75		0		0	
26/11/2019 17:30	0.17	0	24		0		0	
26/11/2019 17:45	0.17	0	24.25		0		0	
26/11/2019 18:00	0.17	0	24.5		0		0	
26/11/2019 18:15	0.17	0	24.75		0		0	
26/11/2019 18:30	0.17	0	25		0		0	
26/11/2019 18:45	0.17	0	25.25		0		0	
26/11/2019 19:00	0.17	0	25.5		0		0	
26/11/2019 19:15	0.17	0	25.75		0		0	
26/11/2019 19:30	0.17	0	26		0		0	
26/11/2019 19:45	0.17	0	26.25		0		0	
26/11/2019 20:00	0.17	0	26.5		0		0	
26/11/2019 20:15	0.17	0	26.75		0		0	
26/11/2019 20:30	0.17	0	27		0		0	
26/11/2019 20:45	0.17	0	27.25		0		0	
26/11/2019 21:00	0.17	0	27.5		0		0	
26/11/2019 21:15	0.17	0	27.75		0		0	
26/11/2019 21:30	0.17	0	28		0		0	
26/11/2019 21:45	0.17	0	28.25		0		0	
26/11/2019 22:00	0.17	0	28.5		0		0	
26/11/2019 22:15	0.17	0	28.75		0		0	
26/11/2019 22:30	0.17	0	29		0		0	
26/11/2019 22:45	0.17	0	29.25		0		0	
26/11/2019 23:00	0.17	0	29.5		0		0	
26/11/2019 23:15	0.17	0	29.75		0		0	
26/11/2019 23:30	0.17	0	30		0		0.2	
26/11/2019 23:45	0.17	0.6	30.25		0		0.2	

	DATE TIME

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Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
27/11/2019 00:00	0.17	1.4	30.5		0		0.2	
27/11/2019 00:15	0.17	0.2	30.75		0		0	
27/11/2019 00:30	0.17	0	31		0		0.2	
27/11/2019 00:45	0.17	0	31.25		0		0	
27/11/2019 01:00	0.17	0	31.5		0		0	
27/11/2019 01:15	0.17	0.2	31.75		0		0	
27/11/2019 01:30	0.17	0.2	32		0		0	
27/11/2019 01:45	0.17	0	32.25		0		0.2	
27/11/2019 02:00	0.17	0.4	32.5		0		0	
27/11/2019 02:15	0.17	0.2	32.75		0		0.4	
27/11/2019 02:30	0.17	0.4	33		0		0.2	
27/11/2019 02:45	0.17	0.4	33.25		0		0.4	
27/11/2019 03:00	0.17	0.4	33.5		0		0.6	
27/11/2019 03:15	0.18	0.2	33.75		0		0.2	
27/11/2019 03:30	0.18	0.4	34		0		0.4	
27/11/2019 03:45	0.18	0.6	34.25		0		0.6	
27/11/2019 04:00	0.18	0.4	34.5		0		0.8	
27/11/2019 04:15	0.18	1.6	34.75		0		1.2	
27/11/2019 04:30	0.19	1.2	35		0		0.8	
27/11/2019 04:45	0.19	1	35.25		0		0.4	
27/11/2019 05:00	0.19	0.6	35.5		0		0.4	
27/11/2019 05:15	0.20	0.6	35.75		0		0.8	
27/11/2019 05:30	0.21	0.4	36		0		0.2	
27/11/2019 05:45	0.22	1	36.25		0		0.8	
27/11/2019 06:00	0.23	0.6	36.5		0		0.2	
27/11/2019 06:15	0.24	0.2	36.75		0		0.2	
27/11/2019 06:30	0.25	0	37		0		0	
27/11/2019 06:45	0.27	0.2	37.25		0		0.2	
27/11/2019 07:00	0.29	0.6	37.5		0		0	
27/11/2019 07:15	0.32	0.6	37.75		0		0.4	
27/11/2019 07:30	0.37	0.4	38		0		0.8	
27/11/2019 07:45	0.44	0.2	38.25		0		0.4	
27/11/2019 08:00	0.53	0.4	38.5		0		0.4	
27/11/2019 08:15	0.65	0.2	38.75		0		0.2	
27/11/2019 08:30	0.82	0.2	39		0		0.2	
27/11/2019 08:45	1.04	0.2	39.25		0		0.2	
27/11/2019 09:00	1.19	0.2	39.5		0 2		0.2	
27/11/2019 09:15	1.35	0	39.75		0 2		0.2	
27/11/2019 09:30	1.61	0.2	40		0		0	
27/11/2019 09:45	2.02	0	40.25		0 2		0.2	
27/11/2019 10:00	2.46	0.2	40.5		0		0	
27/11/2019 10:15	2.92	0.2	40.75		0		0.2	
27/11/2019 10:30	3.36	0	41		0		0	
27/11/2019 10:45	3.73	0	41.25		0		0	
27/11/2019 11:00	4.03	0	41.5		0		0	
27/11/2019 11:15	4.32	0	41.75		0		0.2	
27/11/2019 11:30	4.58	0.2	42		0		0	
27/11/2019 11:45	4.83	0	42.25		0		0	
27/11/2019 12:00	5.04	0	42.5		0		0	
27/11/2019 12:15	5.24	0	42.75		0		0	
27/11/2019 12:30	5.44	0	43		0		0	
27/11/2019 12:45	5.61	0	43.25		0		0	
27/11/2019 13:00	5.75	0	43.5		0		0	
27/11/2019 13:15	5.87	0	43.75		0		0	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
27/11/2019 13:30	5.99	0	44		0		0	
27/11/2019 13:45	6.10	0	44.25		0		0	
27/11/2019 14:00	6.18	0	44.5		0		0	
27/11/2019 14:15	6.27	0	44.75		0		0	
27/11/2019 14:30	6.35	0	45		0		0	
27/11/2019 14:45	6.42	0	45.25		0		0	
27/11/2019 15:00	6.49	0	45.5		0		0	
27/11/2019 15:15	6.54	0	45.75		0		0	
27/11/2019 15:30	6.61	0	46		0		0	
27/11/2019 15:45	6.67	0	46.25		0		0	
27/11/2019 16:00	6.73	0	46.5		0		0	
27/11/2019 16:15	6.79	0	46.75		0		0	
27/11/2019 16:30	6.84	0	47		0		0	
27/11/2019 16:45	6.90	0	47.25		0		0	
27/11/2019 17:00	6.95	0	47.5		0		0	
27/11/2019 17:15	7.00	0	47.75		0 2		0	
27/11/2019 17:30	7.04	0	48		0 2		0	
27/11/2019 17:45	7.10	0	48.25		0		0	
27/11/2019 18:00	7.15	0	48.5		0		0	
27/11/2019 18:15	7.21	0	48.75		0 2		0	
27/11/2019 18:30	7.27	0	49		0.4		0	
27/11/2019 18:45	7.34	0	49.25		0.4		0	
27/11/2019 19:00	7.40	0	49.5		0 2		0	
27/11/2019 19:15	7.48	0	49.75		0.4		0	
27/11/2019 19:30	7.55	0	50		0 2		0	
27/11/2019 19:45	7.63	0	50.25		0.4		0	
27/11/2019 20:00	7.71	0	50.5		0 2		0	
27/11/2019 20:15	7.79	0	50.75		0 2		0	
27/11/2019 20:30	7.88	0	51		0 2		0	
27/11/2019 20:45	7.97	0	51.25		0 2		0	
27/11/2019 21:00	8.07	0	51.5		0.4		0	
27/11/2019 21:15	8.15	0	51.75		0		0	
27/11/2019 21:30	8.25	0	52		0.4		0	
27/11/2019 21:45	8.33	0	52.25		0		0	
27/11/2019 22:00	8.41	0	52.5		0		0	
27/11/2019 22:15	8.48	0	52.75		0		0	
27/11/2019 22:30	8.55	0	53		0		0	
27/11/2019 22:45	8.61	0	53.25		0 2		0	
27/11/2019 23:00	8.68	0	53.5		0		0	
27/11/2019 23:15	8.76	0	53.75		0		0	
27/11/2019 23:30	8.81	0	54		0		0	
27/11/2019 23:45	8.86	0	54.25		0		0	
28/11/2019 00:00	8.93	0	54.5		0		0	
28/11/2019 00:15	9.03	0	54.75		0		0	
28/11/2019 00:30	9.16	0	55		0		0	
28/11/2019 00:45	9.29	0	55.25		0		0	
28/11/2019 01:00	9.40	0	55.5		0		0.2	
28/11/2019 01:15	9.51	0.2	55.75		0		0.2	
28/11/2019 01:30	9.62	0	56		0		0	
28/11/2019 01:45	9.70	0	56.25		0		0	
28/11/2019 02:00	9.81	0	56.5		0		0	
28/11/2019 02:15	9.87	0	56.75		0		0	
28/11/2019 02:30	9.98	0	57		0		0	
28/11/2019 02:45	10.06	0	57.25		0		0	

	DATE TIME

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Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
28/11/2019 03:00	10.15	0	57.5		0		0	
28/11/2019 03:15	10.24	0.2	57.75		0		0	
28/11/2019 03:30	10.26	0	58		0		0	
28/11/2019 03:45	10.32	0	58.25		0		0	
28/11/2019 04:00	10.38	0	58.5		0		0	
28/11/2019 04:15	10.41	0	58.75		0		0	
28/11/2019 04:30	10.47	0	59		0		0	
28/11/2019 04:45	10.49	0.2	59.25		0		0.2	
28/11/2019 05:00	10.52	0	59.5		0		0.2	
28/11/2019 05:15	10.52	0.2	59.75		0		0	
28/11/2019 05:30	10.49	0	60		0 2		0	
28/11/2019 05:45	10.49	0.2	60.25		0.4		0	
28/11/2019 06:00	10.47	0	60.5		0.4		0	
28/11/2019 06:15	10.44	0	60.75		0.6		0	
28/11/2019 06:30	10.38	0.2	61		0.6		0.2	
28/11/2019 06:45	10.35	0	61.25		0.6		0	
28/11/2019 07:00	10.24	0.2	61.5		0 2		0.2	
28/11/2019 07:15	10.18	0	61.75		0.4		0	
28/11/2019 07:30	10.06	0	62		0 2		0	
28/11/2019 07:45	9.98	0	62.25		0		0	
28/11/2019 08:00	9.87	0	62.5		0 2		0	
28/11/2019 08:15	9.76	0	62.75		0		0	
28/11/2019 08:30	9.59	0	63		0 2		0	
28/11/2019 08:45	9.43	0	63.25		0 2		0	
28/11/2019 09:00	9.29	0	63.5		0		0	
28/11/2019 09:15	9.14	0	63.75		0		0	
28/11/2019 09:30	8.95	0	64		0 2		0.2	
28/11/2019 09:45	8.85	0.2	64.25		0		0	
28/11/2019 10:00	8.78	0	64.5		0		0	
28/11/2019 10:15	8.69	0	64.75		0		0	
28/11/2019 10:30	8.61	0	65		0		0	
28/11/2019 10:45	8.52	0	65.25		0		0	
28/11/2019 11:00	8.42	0	65.5		0		0	
28/11/2019 11:15	8.34	0	65.75		0		0	
28/11/2019 11:30	8.24	0	66		0		0	
28/11/2019 11:45	8.13	0	66.25		0		0	
28/11/2019 12:00	8.03	0	66.5		0		0	
28/11/2019 12:15	7.92	0	66.75		0		0	
28/11/2019 12:30	7.82	0	67		0		0	
28/11/2019 12:45	7.70	0	67.25		0		0	
28/11/2019 13:00	7.57	0	67.5		0		0	
28/11/2019 13:15	7.46	0	67.75		0		0	
28/11/2019 13:30	7.34	0	68		0		0	
28/11/2019 13:45	7.20	0	68.25		0		0	
28/11/2019 14:00	7.08	0	68.5		0		0	
28/11/2019 14:15	6.96	0	68.75		0		0	
28/11/2019 14:30	6.81	0	69		0		0	
28/11/2019 14:45	6.67	0	69.25		0		0	
28/11/2019 15:00	6.51	0	69.5		0		0	
28/11/2019 15:15	6.36	0	69.75		0		0	
28/11/2019 15:30	6.21	0	70		0		0	
28/11/2019 15:45	6.05	0.2	70.25		0		0	
28/11/2019 16:00	5.90	0	70.5		0		0	
28/11/2019 16:15	5.74	0	70.75		0		0	

	DATE TIME

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Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
28/11/2019 16:30	5.60	0.2	71		0		0	
28/11/2019 16:45	5.44	0	71.25		0		0.2	
28/11/2019 17:00	5.29	0.2	71.5		0		0	
28/11/2019 17:15	5.13	0	71.75		0		0.2	
28/11/2019 17:30	5.00	0.2	72		0		0	
28/11/2019 17:45	4.87	0	72.25		0		0.2	
28/11/2019 18:00	4.73	0.2	72.5		0		0.2	
28/11/2019 18:15	4.59	0.2	72.75		0 2		0	
28/11/2019 18:30	4.45	0	73		0		0	
28/11/2019 18:45	4.32	0.2	73.25		0		0.2	
28/11/2019 19:00	4.20	0	73.5		0		0.2	
28/11/2019 19:15	4.07	0.2	73.75		0		0	
28/11/2019 19:30	3.95	0.2	74		0		0	
28/11/2019 19:45	3.84	0	74.25		0 2		0	
28/11/2019 20:00	3.73	0.2	74.5		0		0	
28/11/2019 20:15	3.62	0.2	74.75		0		0	
28/11/2019 20:30	3.52	0	75		0		0.2	
28/11/2019 20:45	3.41	0	75.25		0		0	
28/11/2019 21:00	3.28	0	75.5		0		0	
28/11/2019 21:15	3.17	0	75.75		0		0	
28/11/2019 21:30	3.06	0	76		0		0	
28/11/2019 21:45	2.96	0	76.25		0		0	
28/11/2019 22:00	2.86	0	76.5		0		0	
28/11/2019 22:15	2.78	0	76.75		0		0	
28/11/2019 22:30	2.70	0	77		0		0	
28/11/2019 22:45	2.62	0	77.25		0		0	
28/11/2019 23:00	2.56	0	77.5		0		0	
28/11/2019 23:15	2.50	0	77.75		0		0	
28/11/2019 23:30	2.44	0	78		0		0	
28/11/2019 23:45	2.38	0	78.25		0		0	
29/11/2019 00:00	2.33	0	78.5		0		0	
29/11/2019 00:15	2.29	0	78.75		0		0	
29/11/2019 00:30	2.24	0	79		0		0	
29/11/2019 00:45	2.20	0	79.25		0		0	
29/11/2019 01:00	2.16	0	79.5		0		0	
29/11/2019 01:15	2.14	0	79.75		0		0	
29/11/2019 01:30	2.11	0	80		0		0	
29/11/2019 01:45	2.07	0	80.25		0		0	
29/11/2019 02:00	2.05	0	80.5		0		0	
29/11/2019 02:15	2.03	0	80.75		0		0	
29/11/2019 02:30	2.00	0.2	81		0		0	
29/11/2019 02:45	1.98	0	81.25		0		0	
29/11/2019 03:00	1.95	0	81.5		0		0	
29/11/2019 03:15	1.94	0	81.75		0		0	
29/11/2019 03:30	1.92	0	82		0		0	
29/11/2019 03:45	1.89	0	82.25		0		0	
29/11/2019 04:00	1.88	0	82.5		0		0	
29/11/2019 04:15	1.86	0	82.75		0 2		0	
29/11/2019 04:30	1.83	0	83		0		0	
29/11/2019 04:45	1.82	0	83.25		0		0	
29/11/2019 05:00	1.79	0	83.5		0		0	
29/11/2019 05:15	1.77	0	83.75		0		0	
29/11/2019 05:30	1.75	0	84		0		0	
29/11/2019 05:45	1.73	0	84.25		0 2		0	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
29/11/2019 06:00	1.71	0	84.5		0		0	
29/11/2019 06:15	1.69	0	84.75		0		0	
29/11/2019 06:30	1.67	0	85		0		0	
29/11/2019 06:45	1.64	0	85.25		0		0	
29/11/2019 07:00	1.62	0	85.5		0	2	0	
29/11/2019 07:15	1.60	0	85.75		0		0	
29/11/2019 07:30	1.58	0	86		0		0	
29/11/2019 07:45	1.55	0	86.25		0		0	
29/11/2019 08:00	1.53	0	86.5		0		0	
29/11/2019 08:15	1.51	0	86.75		0		0	
29/11/2019 08:30	1.48	0	87		0		0	
29/11/2019 08:45	1.45	0	87.25		0		0	
29/11/2019 09:00	1.44	0	87.5		0		0	
29/11/2019 09:15	1.41	0	87.75		0		0	
29/11/2019 09:30	1.39	0	88		0		0	
29/11/2019 09:45	1.37	0	88.25		0		0	
29/11/2019 10:00	1.35	0	88.5		0		0	
29/11/2019 10:15	1.33	0	88.75		0		0	
29/11/2019 10:30	1.31	0	89		0		0	
29/11/2019 10:45	1.30	0	89.25		0		0	
29/11/2019 11:00	1.27	0	89.5		0		0	
29/11/2019 11:15	1.26	0	89.75		0		0	
29/11/2019 11:30	1.24	0	90		0		0	
29/11/2019 11:45	1.24	0	90.25		0		0	
29/11/2019 12:00	1.22	0	90.5		0		0	
29/11/2019 12:15	1.21	0	90.75		0		0	
29/11/2019 12:30	1.20	0	91		0		0	
29/11/2019 12:45	1.19	0	91.25		0		0	
29/11/2019 13:00	1.18	0	91.5		0		0	
29/11/2019 13:15	1.17	0	91.75		0		0	
29/11/2019 13:30	1.16	0	92		0		0	
29/11/2019 13:45	1.15	0	92.25		0		0	
29/11/2019 14:00	1.15	0	92.5		0		0	
29/11/2019 14:15	1.13	0	92.75		0		0	
29/11/2019 14:30	1.13	0	93		0		0	
29/11/2019 14:45	1.12	0	93.25		0		0	
29/11/2019 15:00	1.11	0	93.5		0		0.4	
29/11/2019 15:15	1.11	0	93.75		0		0	
29/11/2019 15:30	1.10	0	94		0		0	
29/11/2019 15:45	1.07	0	94.25		0		0	
29/11/2019 16:00	1.06	0	94.5		0		0	
29/11/2019 16:15	1.05	0	94.75		0		0	
29/11/2019 16:30	1.04	0	95		0		0	
29/11/2019 16:45	1.03	0	95.25		0		0	
29/11/2019 17:00	1.01	0	95.5		0		0	
29/11/2019 17:15	1.00	0	95.75		0		0	
29/11/2019 17:30	0.99	0	96		0		0	
29/11/2019 17:45	0.98	0	96.25		0		0	
29/11/2019 18:00	0.97	0	96.5		0		0	
29/11/2019 18:15	0.96	0	96.75		0		0	
29/11/2019 18:30	0.94	0	97		0		0	
29/11/2019 18:45	0.93	0	97.25		0		0	
29/11/2019 19:00	0.92	0	97.5		0	2	0	
29/11/2019 19:15	0.91	0	97.75		0		0	

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Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
29/11/2019 19:30	0.90	0	98		0		0	
29/11/2019 19:45	0.89	0	98.25		0		0	
29/11/2019 20:00	0.88	0	98.5		0		0	
29/11/2019 20:15	0.87	0	98.75		0		0	
29/11/2019 20:30	0.86	0	99		0		0	
29/11/2019 20:45	0.85	0	99.25		0		0	
29/11/2019 21:00	0.84	0	99.5		0		0	
29/11/2019 21:15	0.82	0	99.75		0		0	
29/11/2019 21:30	0.81	0	100		0		0	
29/11/2019 21:45	0.80	0	100.25		0		0	
29/11/2019 22:00	0.80	0	100.5		0		0.2	
29/11/2019 22:15	0.79	0	100.75		0		0	
29/11/2019 22:30	0.78	0	101		0		0	
29/11/2019 22:45	0.77	0	101.25		0		0	
29/11/2019 23:00	0.76	0	101.5		0		0	
29/11/2019 23:15	0.76	0	101.75		0		0	
29/11/2019 23:30	0.76	0	102		0		0	
29/11/2019 23:45	0.75	0	102.25		0		0	
30/11/2019 00:00	0.74	0	102.5		0		0	
30/11/2019 00:15	0.74	0	102.75		0		0	
30/11/2019 00:30	0.73	0	103		0		0	
30/11/2019 00:45	0.72	0	103.25		0		0	
30/11/2019 01:00	0.71	0	103.5		0		0	
30/11/2019 01:15	0.71	0	103.75		0		0	
30/11/2019 01:30	0.70	0	104		0		0	
30/11/2019 01:45	0.69	0	104.25		0		0	
30/11/2019 02:00	0.69	0	104.5		0		0	
30/11/2019 02:15	0.68	0	104.75		0		0	
30/11/2019 02:30	0.67	0	105		0		0	
30/11/2019 02:45	0.66	0	105.25		0		0	
30/11/2019 03:00	0.66	0	105.5		0		0	
30/11/2019 03:15	0.65	0	105.75		0		0	
30/11/2019 03:30	0.65	0	106		0		0	
30/11/2019 03:45	0.65	0	106.25		0		0	
30/11/2019 04:00	0.64	0	106.5		0		0	
30/11/2019 04:15	0.63	0	106.75		0		0	
30/11/2019 04:30	0.63	0	107		0		0	
30/11/2019 04:45	0.62	0	107.25		0		0	
30/11/2019 05:00	0.61	0	107.5		0		0	
30/11/2019 05:15	0.60	0	107.75		0		0	
30/11/2019 05:30	0.60	0	108		0		0	
30/11/2019 05:45	0.60	0	108.25		0		0	
30/11/2019 06:00	0.59	0	108.5		0		0	
30/11/2019 06:15	0.59	0	108.75		0		0	
30/11/2019 06:30	0.58	0	109		0		0	
30/11/2019 06:45	0.57	0	109.25		0		0	
30/11/2019 07:00	0.57	0	109.5		0		0	
30/11/2019 07:15	0.56	0	109.75		0		0	
30/11/2019 07:30	0.56	0	110		0		0	
30/11/2019 07:45	0.56	0	110.25		0		0	
30/11/2019 08:00	0.55	0	110.5		0		0	
30/11/2019 08:15	0.55	0	110.75		0		0	
30/11/2019 08:30	0.54	0	111		0		0	
30/11/2019 08:45	0.54	0	111.25		0		0	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
30/11/2019 09:00	0.53	0	111.5		0		0	
30/11/2019 09:15	0.53	0.2	111.75		0		0	
30/11/2019 09:30	0.53	0	112		0		0	
30/11/2019 09:45	0.52	0	112.25		0		0	
30/11/2019 10:00	0.51	0	112.5		0		0	
30/11/2019 10:15	0.50	0	112.75		0		0	
30/11/2019 10:30	0.50	0	113		0		0	
30/11/2019 10:45	0.50	0	113.25		0		0	
30/11/2019 11:00	0.49	0	113.5		0		0	
30/11/2019 11:15	0.49	0	113.75		0		0	
30/11/2019 11:30	0.48	0	114		0		0	
30/11/2019 11:45	0.48	0	114.25		0		0	
30/11/2019 12:00	0.48	0	114.5		0		0	
30/11/2019 12:15	0.48	0	114.75		0		0	
30/11/2019 12:30	0.47	0	115		0		0	
30/11/2019 12:45	0.47	0	115.25		0		0	
30/11/2019 13:00	0.47	0	115.5		0		0	
30/11/2019 13:15	0.46	0	115.75		0		0	
30/11/2019 13:30	0.46	0	116		0		0	
30/11/2019 13:45	0.46	0	116.25		0		0	
30/11/2019 14:00	0.46	0	116.5		0		0	
30/11/2019 14:15	0.46	0	116.75		0		0	
30/11/2019 14:30	0.45	0	117		0		0.2	
30/11/2019 14:45	0.45	0	117.25		0		0	
30/11/2019 15:00	0.45	0	117.5		0		0	
30/11/2019 15:15	0.44	0	117.75		0		0	
30/11/2019 15:30	0.44	0	118		0		0	
30/11/2019 15:45	0.44	0	118.25		0		0	
30/11/2019 16:00	0.44	0	118.5		0		0	
30/11/2019 16:15	0.44	0	118.75		0		0	
30/11/2019 16:30	0.44	0	119		0		0	
30/11/2019 16:45	0.43	0	119.25		0		0.2	
30/11/2019 17:00	0.43	0.2	119.5		0		0	
30/11/2019 17:15	0.42	0	119.75		0		0	
30/11/2019 17:30	0.42	0	120		0		0	
30/11/2019 17:45	0.42	0	120.25		0		0	
30/11/2019 18:00	0.42	0.2	120.5		0		0	
30/11/2019 18:15	0.42	0	120.75		0		0	
30/11/2019 18:30	0.42	0	121		0		0	
30/11/2019 18:45	0.42	0	121.25		0		0	
30/11/2019 19:00	0.42	0	121.5		0		0	
30/11/2019 19:15	0.41	0	121.75		0		0	
30/11/2019 19:30	0.41	0	122		0		0	
30/11/2019 19:45	0.41	0	122.25		0		0	
30/11/2019 20:00	0.40	0	122.5		0		0	
30/11/2019 20:15	0.40	0	122.75		0		0	
30/11/2019 20:30	0.40	0	123		0		0	
30/11/2019 20:45	0.40	0	123.25		0		0	
30/11/2019 21:00	0.40	0	123.5		0		0	
30/11/2019 21:15	0.40	0	123.75		0		0	
30/11/2019 21:30	0.40	0	124		0		0	
30/11/2019 21:45	0.39	0	124.25		0		0	
30/11/2019 22:00	0.39	0	124.5		0		0	
30/11/2019 22:15	0.39	0	124.75		0		0	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
30/11/2019 22:30	0.39	0	125		0		0	
30/11/2019 22:45	0.39	0	125.25		0		0	
30/11/2019 23:00	0.39	0	125.5		0		0	
30/11/2019 23:15	0.39	0	125.75		0		0	
30/11/2019 23:30	0.39	0	126		0		0	
30/11/2019 23:45	0.39	0	126.25		0		0	
01/12/2019 00:00	0.38	0	126.5		0		0	
01/12/2019 00:15	0.38	0	126.75		0		0	
01/12/2019 00:30	0.38	0	127		0		0	
01/12/2019 00:45	0.37	0	127.25		0		0	
01/12/2019 01:00	0.37	0	127.5		0		0	
01/12/2019 01:15	0.37	0	127.75		0		0	
01/12/2019 01:30	0.37	0	128		0		0	
01/12/2019 01:45	0.37	0	128.25		0		0	
01/12/2019 02:00	0.37	0	128.5		0		0	
01/12/2019 02:15	0.37	0	128.75		0		0	
01/12/2019 02:30	0.37	0	129		0		0	
01/12/2019 02:45	0.36	0	129.25		0		0	
01/12/2019 03:00	0.36	0	129.5		0		0	
01/12/2019 03:15	0.36	0	129.75		0		0	
01/12/2019 03:30	0.36	0	130		0		0	
01/12/2019 03:45	0.36	0	130.25		0		0	
01/12/2019 04:00	0.36	0	130.5		0		0	
01/12/2019 04:15	0.36	0	130.75		0		0	
01/12/2019 04:30	0.36	0	131		0		0	
01/12/2019 04:45	0.35	0	131.25		0		0	
01/12/2019 05:00	0.35	0	131.5		0		0	
01/12/2019 05:15	0.35	0	131.75		0		0	
01/12/2019 05:30	0.35	0	132		0		0	
01/12/2019 05:45	0.35	0	132.25		0		0	
01/12/2019 06:00	0.35	0	132.5		0		0	
01/12/2019 06:15	0.35	0	132.75		0		0	
01/12/2019 06:30	0.35	0	133		0		0	
01/12/2019 06:45	0.35	0	133.25		0		0	
01/12/2019 07:00	0.34	0	133.5		0		0	
01/12/2019 07:15	0.34	0	133.75		0		0	
01/12/2019 07:30	0.34	0	134		0		0	
01/12/2019 07:45	0.34	0	134.25		0		0	
01/12/2019 08:00	0.34	0	134.5		0		0	
01/12/2019 08:15	0.34	0	134.75		0		0	
01/12/2019 08:30	0.34	0	135		0		0	
01/12/2019 08:45	0.34	0	135.25		0		0	
01/12/2019 09:00	0.34	0	135.5		0		0	
01/12/2019 09:15	0.34	0	135.75		0		0	
01/12/2019 09:30	0.33	0	136		0		0	
01/12/2019 09:45	0.33	0	136.25		0		0	
01/12/2019 10:00	0.33	0.2	136.5		0		0	
01/12/2019 10:15	0.33	0	136.75		0		0	
01/12/2019 10:30	0.33	0	137		0 2		0	
01/12/2019 10:45	0.33	0	137.25		0		0	
01/12/2019 11:00	0.33	0	137.5		0		0	
01/12/2019 11:15	0.33	0	137.75		0		0	
01/12/2019 11:30	0.33	0.2	138		0		0	
01/12/2019 11:45	0.33	0.2	138.25		0		0.2	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
01/12/2019 12:00	0.33	0.2	138.5		0		0	
01/12/2019 12:15	0.33	0.2	138.75		0		0	
01/12/2019 12:30	0.33	0	139		0		0	
01/12/2019 12:45	0.33	0.4	139.25		0.4		0.2	
01/12/2019 13:00	0.33	0	139.5		0 2		0	
01/12/2019 13:15	0.33	0	139.75		0.4		0	
01/12/2019 13:30	0.33	0	140		0		0	
01/12/2019 13:45	0.33	0	140.25		0 2		0	
01/12/2019 14:00	0.33	0	140.5		0		0.6	
01/12/2019 14:15	0.33	0	140.75		0		0	
01/12/2019 14:30	0.33	0	141		0		0	
01/12/2019 14:45	0.33	0	141.25		0		0	
01/12/2019 15:00	0.33	0	141.5		0		0	
01/12/2019 15:15	0.33	0	141.75		0 2		0	
01/12/2019 15:30	0.33	0	142		0		0	
01/12/2019 15:45	0.33	0	142.25		0		0	
01/12/2019 16:00	0.32	0	142.5		0		0	
01/12/2019 16:15	0.32	0	142.75		0		0	
01/12/2019 16:30	0.32	0	143		0		0	
01/12/2019 16:45	0.32	0	143.25		0		0	
01/12/2019 17:00	0.32	0	143.5		0		0	
01/12/2019 17:15	0.32	0	143.75		0		0	
01/12/2019 17:30	0.32	0	144		0		0	
01/12/2019 17:45	0.32	0	144.25		0		0	
01/12/2019 18:00	0.32	0	144.5		0		0	
01/12/2019 18:15	0.32	0	144.75		0		0	
01/12/2019 18:30	0.32	0	145		0		0	
01/12/2019 18:45	0.32	0	145.25		0		0	
01/12/2019 19:00	0.32	0	145.5		0		0	
01/12/2019 19:15	0.32	0	145.75		0		0.2	
01/12/2019 19:30	0.32	0	146		0		0	
01/12/2019 19:45	0.32	0	146.25		0		0	
01/12/2019 20:00	0.32	0	146.5		0		0	
01/12/2019 20:15	0.32	0	146.75		0		0	
01/12/2019 20:30	0.32	0	147		0		0	
01/12/2019 20:45	0.32	0.2	147.25		0		0	
01/12/2019 21:00	0.32	0	147.5		0		0	
01/12/2019 21:15	0.32	0	147.75		0		0	
01/12/2019 21:30	0.32	0	148		0		0	
01/12/2019 21:45	0.32	0	148.25		0		0	
01/12/2019 22:00	0.32	0	148.5		0		0	
01/12/2019 22:15	0.32	0	148.75		0		0	
01/12/2019 22:30	0.32	0	149		0		0	
01/12/2019 22:45	0.32	0	149.25		0		0	
01/12/2019 23:00	0.32	0	149.5		0		0	
01/12/2019 23:15	0.32	0	149.75		0		0	
01/12/2019 23:30	0.32	0	150		0		0	
01/12/2019 23:45	0.31	0	150.25		0		0	
02/12/2019 00:00	0.31	0	150.5		0		0	
02/12/2019 00:15	0.31	0	150.75		0 2		0	
02/12/2019 00:30	0.31	0	151		0		0	
02/12/2019 00:45	0.31	0	151.25		0 2		0	
02/12/2019 01:00	0.31	0	151.5		0.4		0	
02/12/2019 01:15	0.31	0	151.75		0.4		0	

	DATE TIME

Middleton		Benhall			Earl Soham		Thorpeness	
Date & Time	Flow (m^3/s)	Rainfall (mm)	Duration hours	Daily totals mm	Rainfall (mm)	Daily totals mm	Rainfall (mm)	Daily totals mm
02/12/2019 01:30	0.31	0	152		0	2	0	
02/12/2019 01:45	0.31	0	152.25		0	2	0	
02/12/2019 02:00	0.31	0	152.5		0		0	
02/12/2019 02:15	0.31	0	152.75		0		0	
02/12/2019 02:30	0.31	0	153		0	2	0	
02/12/2019 02:45	0.31	0	153.25		0		0	
02/12/2019 03:00	0.31	0	153.5		0		0	
02/12/2019 03:15	0.31	0	153.75		0		0	
02/12/2019 03:30	0.31	0	154		0		0	
02/12/2019 03:45	0.31	0	154.25		0		0	
02/12/2019 04:00	0.31	0	154.5		0	2	0	
02/12/2019 04:15	0.31	0	154.75		0		0.2	
02/12/2019 04:30	0.30	0	155		0		0	
02/12/2019 04:45	0.30	0	155.25		0		0	
02/12/2019 05:00	0.30	0	155.5		0		0	
02/12/2019 05:15	0.30	0	155.75		0		0	
02/12/2019 05:30	0.30	0	156		0		0	
02/12/2019 05:45	0.30	0	156.25		0		0	
02/12/2019 06:00	0.30	0	156.5		0		0	
02/12/2019 06:15	0.30	0	156.75		0		0	
02/12/2019 06:30	0.30	0	157		0		0	
02/12/2019 06:45	0.30	0	157.25		0		0	
02/12/2019 07:00	0.30	0	157.5		0		0	
02/12/2019 07:15	0.30	0	157.75		0		0	
02/12/2019 07:30	0.30	0	158		0		0	
02/12/2019 07:45	0.30	0	158.25		0		0	
02/12/2019 08:00	0.29	0	158.5		0		0	
02/12/2019 08:15	0.29	0	158.75		0		0	
02/12/2019 08:30	0.29	0	159		0		0	
02/12/2019 08:45	0.29	0	159.25		0		0	
02/12/2019 09:00	0.29	0	159.5		0		0	
02/12/2019 09:15	0.29	0	159.75		0		0	
02/12/2019 09:30	0.29	0	160		0		0	

	DATE TIME

SAAR	592	mm
AREA	50.16	Km2

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capacity in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
W/E 26/11/2019	0	mm
W/E	0	mm

Source of Rainfall event data.

Gauge	Easting	Northing	Distance from Catchment Centroid (m)	Reciprocal	Weighting
Benhall	38166	60602	8878	0.000112638	1
Soham	23243	62717			
Thorpeness	60012	78834			
			Total	0.000112638	1

TBR RG

Daily RF totals 9am 9am	**Benhall**	**Soham**	Thorpeness
Date	**Total RF (mm)**	**Total RF (mm)**	**Total RF (mm)**
25/11/2019	0.6		
24/11/2019	0		
23/11/2019	0.4		
22/11/2019	1.8		
21/11/2019	0.2		

Rainall Event Depth P (mm)	17.2
Event duration (hours)	11.75

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**21/11/2019**	**22/11/2019**	**23/11/2019**	**24/11/2019**	**25/11/2019**
Benhall	592	1.0000	0.2	1.8	0.4	0	0.6
Soham	592		0	0	0	0	0
Thorpeness	592						
Average Daily rainfall totals			0.2	1.8	0.4	0	0.6

Gauge	**SAAR**	**Weight**	**21/11/2019**	**22/11/2019**	**23/11/2019**	**24/11/2019**	**25/11/2019**
Benhall	592	1.0000	0.000337838	0.003040541	0.000675676	0	0.001013514
Soham	592		0	0	0	0	0
Thorpeness	592						

Gauge	**SAAR**	**Weight**	**21/11/2019**	**22/11/2019**	**23/11/2019**	**24/11/2019**	**25/11/2019**
Benhall	592	1.0000	0.000337838	0.003040541	0.000675676	0	0.001013514
Soham	592		0	0	0	0	0
Thorpeness	592						

Gauge	**SAAR**	**Weight**	**21/11/2019**	**22/11/2019**	**23/11/2019**	**24/11/2019**	**25/11/2019**
Benhall	592	1.0000	0.2	1.8	0.4	0	0.6
Soham	592		0	0	0	0	0
Thorpeness	592						
Catchment Average Antecedent RF mm			0.2	1.8	0.4	0	0.6

Date	**Catchment Average Antecedent Rainfall (mm)**	
21/11/2019	0.20	d-5
22/11/2019	1.80	d-4
23/11/2019	0.40	d-3
24/11/2019	0.00	d-2
25/11/2019	0.60	d-1

API5

0.66	mm	0.662912607	mm / day

CWI Prior to Event November 2019 Event at Middleton
CWI 125 + API15 - SMD

SMD	0	mm
CWI	125.6629126	mm

FEH Parameter										
SPR	95.9	%						**URBEXT2000**	0.0084	As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
PRrural	96.1	%			P=Storm Depth	17.2	mm	**PR**	96	taken from PR calculations sheet using Benhall TBR RG record
DPRrain	0.0	%			SPR	95.89995738		**DPRrain**	0	DPRrain is 0, as P<40mm
DPRcwi	0.2	CWI	125.6629					**DPRcwi**	0.2	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural								**SPR**	95.9	
PR	95.9	%						**DPRrain**	0.45(P-40)^0.7	#NUM!
PRrural	96.1	%						**P**	17.2	
CWI	125.7	mm						**CWI**	125.7	
BF	0.00001		Baseflow equation taken from FEH					**SPR**	95.9	
	-1254							**PR**	95.9	
	1778.5		524.5	0.005245						
AREA	50.16		**0.263089**	m3s-1				**SPRHOST**	41.05	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
SPR	95.9							**Duration (hours)**	11.75	
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	95.9									
PRrural	96.1									

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
26-Nov-19	27-Nov-19	11.75	0.66	0.00	125.66	96.07	0.17	0.00	95.90	96.00	41.05

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)		Date & Time	Rainfall (mm)	Rainfall (mm)
31/01/2014 08 45	0.040053362	31/01/2014 08 45	.		31/01/2014 08 45	0.845	31/01/2014 08 45	M		04/02/2014 00 00	.	.
31/01/2014 09 00	0.045705812	31/01/2014 09 00	.		31/01/2014 09 00	0.837	31/01/2014 09 00	M		04/02/2014 00 15	.	.
31/01/2014 09 15	0.052843244	31/01/2014 09 15	.		31/01/2014 09 15	0.829	31/01/2014 09 15	M		04/02/2014 00 30	.	.
31/01/2014 09 30	0.043858078	31/01/2014 09 30	.		31/01/2014 09 30	0.829	31/01/2014 09 30	M		04/02/2014 00 45	.	.
31/01/2014 09 45	0.052468096	31/01/2014 09 45	.		31/01/2014 09 45	0.829	31/01/2014 09 45	M		04/02/2014 01 00	.	.
31/01/2014 10 00	0.052926154	31/01/2014 10 00	.		31/01/2014 10 00	0.821	31/01/2014 10 00	M		04/02/2014 01 15	.	.
31/01/2014 10 15	0.052956816	31/01/2014 10 15	.		31/01/2014 10 15	0.821	31/01/2014 10 15	M		04/02/2014 01 30	.	.
31/01/2014 10 30	0.054840272	31/01/2014 10 30	.		31/01/2014 10 30	0.814	31/01/2014 10 30	M		04/02/2014 01 45	.	.
31/01/2014 10 45	0.061945703	31/01/2014 10 45	.		31/01/2014 10 45	0.814	31/01/2014 10 45	M		04/02/2014 02 00	.	.
31/01/2014 11 00	0.062012765	31/01/2014 11 00	.		31/01/2014 11 00	0.806	31/01/2014 11 00	M		04/02/2014 02 15	.	.
31/01/2014 11 15	0.053441438	31/01/2014 11 15	.		31/01/2014 11 15	0.798	31/01/2014 11 15	M		04/02/2014 02 30	.	.
31/01/2014 11 30	0.045346295	31/01/2014 11 30	.		31/01/2014 11 30	0.798	31/01/2014 11 30	M		04/02/2014 02 45	.	.
31/01/2014 11 45	0.04772722	31/01/2014 11 45	.		31/01/2014 11 45	0.798	31/01/2014 11 45	M		04/02/2014 03 00	.	.
31/01/2014 12 00	0.050604804	31/01/2014 12 00	.		31/01/2014 12 00	0.791	31/01/2014 12 00	M		04/02/2014 03 15	.	.
31/01/2014 12 15	0.041242143	31/01/2014 12 15	.		31/01/2014 12 15	0.783	31/01/2014 12 15	M		04/02/2014 03 30	.	.
31/01/2014 12 30	0.047838785	31/01/2014 12 30	.		31/01/2014 12 30	0.783	31/01/2014 12 30	M		04/02/2014 03 45	.	.
31/01/2014 12 45	0.045512408	31/01/2014 12 45	.		31/01/2014 12 45	0.776	31/01/2014 12 45	M		04/02/2014 04 00	.	.
31/01/2014 13 00	0.054385103	31/01/2014 13 00	.		31/01/2014 13 00	0.776	31/01/2014 13 00	M		04/02/2014 04 15	.	.
31/01/2014 13 15	0.057276511	31/01/2014 13 15	.		31/01/2014 13 15	0.768	31/01/2014 13 15	M		04/02/2014 04 30	.	.
31/01/2014 13 30	0.057276511	31/01/2014 13 30	.		31/01/2014 13 30	0.768	31/01/2014 13 30	M		04/02/2014 04 45	.	.
31/01/2014 13 45	0.054869992	31/01/2014 13 45	.		31/01/2014 13 45	0.768	31/01/2014 13 45	M		04/02/2014 05 00	.	.
31/01/2014 14 00	0.051077341	31/01/2014 14 00	.		31/01/2014 14 00	0.768	31/01/2014 14 00	M		04/02/2014 05 15	.	.
31/01/2014 14 15	0.055330178	31/01/2014 14 15	.		31/01/2014 14 15	0.76	31/01/2014 14 15	M		04/02/2014 05 30	.	.
31/01/2014 14 30	0.051089064	31/01/2014 14 30	.		31/01/2014 14 30	0.76	31/01/2014 14 30	M		04/02/2014 05 45	.	.
31/01/2014 14 45	0.055309173	31/01/2014 14 45	.		31/01/2014 14 45	0.76	31/01/2014 14 45	M		04/02/2014 06 00	.	.
31/01/2014 15 00	0.042255479	31/01/2014 15 00	.		31/01/2014 15 00	0.753	31/01/2014 15 00	M		04/02/2014 06 15	.	.
31/01/2014 15 15	0.053422092	31/01/2014 15 15	.		31/01/2014 15 15	0.753	31/01/2014 15 15	M		04/02/2014 06 30	.	.
31/01/2014 15 30	0.036206897	31/01/2014 15 30	.		31/01/2014 15 30	0.753	31/01/2014 15 30	M		04/02/2014 06 45	.	.
31/01/2014 15 45	0.053422092	31/01/2014 15 45	.		31/01/2014 15 45	0.746	31/01/2014 15 45	M		04/02/2014 07 00	.	.
31/01/2014 16 00	0.057144296	31/01/2014 16 00	.		31/01/2014 16 00	0.746	31/01/2014 16 00	M		04/02/2014 07 15	.	.
31/01/2014 16 15	0.045095729	31/01/2014 16 15		0.2	31/01/2014 16 15	0.738	31/01/2014 16 15	M		04/02/2014 07 30	.	.
31/01/2014 16 30	0.04555739	31/01/2014 16 30		0.2	31/01/2014 16 30	0.738	31/01/2014 16 30	M		04/02/2014 07 45	.	.
31/01/2014 16 45	0.037709152	31/01/2014 16 45		0.2	31/01/2014 16 45	0.731	31/01/2014 16 45	M		04/02/2014 08 00	.	.
31/01/2014 17 00	0.052020645	31/01/2014 17 00		0.4	31/01/2014 17 00	0.731	31/01/2014 17 00	M		04/02/2014 08 15	.	.
31/01/2014 17 15	0.052020645	31/01/2014 17 15		0.4	31/01/2014 17 15	0.731	31/01/2014 17 15	M		04/02/2014 08 30	.	.
31/01/2014 17 30	0.049250679	31/01/2014 17 30		0.2	31/01/2014 17 30	0.723	31/01/2014 17 30	M		04/02/2014 08 45	.	.
31/01/2014 17 45	0.053422092	31/01/2014 17 45		0.4	31/01/2014 17 45	0.723	31/01/2014 17 45	M		04/02/2014 09 00	.	.
31/01/2014 18 00	0.057813894	31/01/2014 18 00		0.2	31/01/2014 18 00	0.723	31/01/2014 18 00	M		04/02/2014 09 15	.	.
31/01/2014 18 15	0.075187224	31/01/2014 18 15		0.2	31/01/2014 18 15	0.723	31/01/2014 18 15	M		04/02/2014 09 30	.	.
31/01/2014 18 30	0.088278359	31/01/2014 18 30		0.4	31/01/2014 18 30	0.723	31/01/2014 18 30	M		04/02/2014 09 45	.	.
31/01/2014 18 45	0.075781657	31/01/2014 18 45		0.4	31/01/2014 18 45	0.723	31/01/2014 18 45	M		04/02/2014 10 00	.	.
31/01/2014 19 00	0.095858212	31/01/2014 19 00		0.6	31/01/2014 19 00	0.723	31/01/2014 19 00	M		04/02/2014 10 15	.	.
31/01/2014 19 15	0.095677868	31/01/2014 19 15		0.4	31/01/2014 19 15	0.723	31/01/2014 19 15	M		04/02/2014 10 30	.	.
31/01/2014 19 30	0.084248504	31/01/2014 19 30		0.4	31/01/2014 19 30	0.723	31/01/2014 19 30	M		04/02/2014 10 45	.	.
31/01/2014 19 45	0.095412923	31/01/2014 19 45		0.4	31/01/2014 19 45	0.731	31/01/2014 19 45	M		04/02/2014 11 00	.	.
31/01/2014 20 00	0.116670487	31/01/2014 20 00		0.4	31/01/2014 20 00	0.731	31/01/2014 20 00	M		04/02/2014 11 15	.	.
31/01/2014 20 15	0.115716734	31/01/2014 20 15		0.4	31/01/2014 20 15	0.731	31/01/2014 20 15	M		04/02/2014 11 30	.	.
31/01/2014 20 30	0.105258331	31/01/2014 20 30		0.4	31/01/2014 20 30	0.738	31/01/2014 20 30	M		04/02/2014 11 45	.	.
31/01/2014 20 45	0.104502682	31/01/2014 20 45		0.6	31/01/2014 20 45	0.746	31/01/2014 20 45	M		04/02/2014 12 00	.	.
31/01/2014 21 00	0.110390468	31/01/2014 21 00		0.2	31/01/2014 21 00	0.753	31/01/2014 21 00	M		04/02/2014 12 15	.	.
31/01/2014 21 15	0.122596148	31/01/2014 21 15		0.2	31/01/2014 21 15	0.76	31/01/2014 21 15	M		04/02/2014 12 30	.	.
31/01/2014 21 30	0.119529822	31/01/2014 21 30	.		31/01/2014 21 30	0.775	31/01/2014 21 30	M		04/02/2014 12 45	.	.
31/01/2014 21 45	0.131335845	31/01/2014 21 45	.		31/01/2014 21 45	0.783	31/01/2014 21 45	M		04/02/2014 13 00	.	.
31/01/2014 22 00	0.124247505	31/01/2014 22 00	.		31/01/2014 22 00	0.798	31/01/2014 22 00	M		04/02/2014 13 15	.	.
31/01/2014 22 15	0.09928276	31/01/2014 22 15		0.2	31/01/2014 22 15	0.821	31/01/2014 22 15	M		04/02/2014 13 30	.	.
31/01/2014 22 30	0.103420071	31/01/2014 22 30		0.2	31/01/2014 22 30	0.844	31/01/2014 22 30	M		04/02/2014 13 45	.	.
31/01/2014 22 45	0.109606209	31/01/2014 22 45		0.2	31/01/2014 22 45	0.868	31/01/2014 22 45	M		04/02/2014 14 00	.	.
31/01/2014 23 00	0.108122063	31/01/2014 23 00		0.4	31/01/2014 23 00	0.916	31/01/2014 23 00	M		04/02/2014 14 15	.	.
31/01/2014 23 15	0.106482729	31/01/2014 23 15		0.4	31/01/2014 23 15	0.973	31/01/2014 23 15	M		04/02/2014 14 30	.	.
31/01/2014 23 30	0.117159164	31/01/2014 23 30		0.6	31/01/2014 23 30	1.04	31/01/2014 23 30	M		04/02/2014 14 45	.	.
31/01/2014 23 45	0.123253721	31/01/2014 23 45		0.8	31/01/2014 23 45	1.14	31/01/2014 23 45	M		04/02/2014 15 00	.	.
01/02/2014 00 00	0.147855461	01/02/2014 00 00	.		01/02/2014 00 00	1.24	01/02/2014 00 00	M		04/02/2014 15 15	.	.
01/02/2014 00 15	0.155866832	01/02/2014 00 15		0.2	01/02/2014 00 15	---	01/02/2014 00 15			04/02/2014 15 30	.	.
01/02/2014 00 30	0.179847948	01/02/2014 00 30		0.2	01/02/2014 00 30	---	01/02/2014 00 30			04/02/2014 15 45	.	.
01/02/2014 00 45	0.15178107	01/02/2014 00 45	.		01/02/2014 00 45	---	01/02/2014 00 45			04/02/2014 16 00	.	.
01/02/2014 01 00	0.192024165	01/02/2014 01 00	.		01/02/2014 01 00	---	01/02/2014 01 00			04/02/2014 16 15	.	.
01/02/2014 01 15	0.199340463	01/02/2014 01 15	.		01/02/2014 01 15	---	01/02/2014 01 15			04/02/2014 16 30	.	.
01/02/2014 01 30	0.15506281	01/02/2014 01 30		0.2	01/02/2014 01 30	---	01/02/2014 01 30			04/02/2014 16 45	.	.
01/02/2014 01 45	0.168952895	01/02/2014 01 45	.		01/02/2014 01 45	---	01/02/2014 01 45			04/02/2014 17 00	.	.
01/02/2014 02 00	0.203638919	01/02/2014 02 00	.		01/02/2014 02 00	---	01/02/2014 02 00			04/02/2014 17 15	.	.
01/02/2014 02 15	0.179712829	01/02/2014 02 15		0.4	01/02/2014 02 15	---	01/02/2014 02 15			04/02/2014 17 30	.	.
01/02/2014 02 30	0.224782172	01/02/2014 02 30		0.2	01/02/2014 02 30	---	01/02/2014 02 30			04/02/2014 17 45	.	.
01/02/2014 02 45	0.224745332	01/02/2014 02 45	.		01/02/2014 02 45	---	01/02/2014 02 45			04/02/2014 18 00	.	.
01/02/2014 03 00	0.206027897	01/02/2014 03 00	.		01/02/2014 03 00	---	01/02/2014 03 00			04/02/2014 18 15	.	.
01/02/2014 03 15	0.210589984	01/02/2014 03 15	.		01/02/2014 03 15	---	01/02/2014 03 15			04/02/2014 18 30	.	.

	DATE TIME
start of event	06/02/2014 13 30
end of event	07/02/2014 08 15
duration hours	18.75
total RF mm	20.4
SMD W/E AVERAGE	mm
04-Feb-14	0

DATE	API5	Daily Totals
05/02/2014	d-1	1.6
04/02/2014	d-2	4.4
03/02/2014	d-3	0
02/02/2014	d-4	0.2
01/02/2014	d-5	0
		6.2

incomplete dataset at Thorpeness RG & Earl Soham

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG		Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Rainfall (mm)	Rainfall (mm)
01/02/2014 03 30	0.249417928	01/02/2014 03 30	0.4		01/02/2014 03 30	---	01/02/2014 03 30		04/02/2014 18 45	.	.
01/02/2014 03 45	0.195812259	01/02/2014 03 45	0.4		01/02/2014 03 45	---	01/02/2014 03 45		04/02/2014 19 00	.	.
01/02/2014 04 00	0.230304661	01/02/2014 04 00	0.6		01/02/2014 04 00	---	01/02/2014 04 00		04/02/2014 19 15	.	.
01/02/2014 04 15	0.214936878	01/02/2014 04 15	.		01/02/2014 04 15	---	01/02/2014 04 15		04/02/2014 19 30	.	.
01/02/2014 04 30	0.244060987	01/02/2014 04 30	0.6		01/02/2014 04 30	---	01/02/2014 04 30		04/02/2014 19 45	.	.
01/02/2014 04 45	0.370496193	01/02/2014 04 45	0.2		01/02/2014 04 45	---	01/02/2014 04 45		04/02/2014 20 00	.	.
01/02/2014 05 00	0.35030077	01/02/2014 05 00	1		01/02/2014 05 00	---	01/02/2014 05 00		04/02/2014 20 15	.	.
01/02/2014 05 15	0.3619913	01/02/2014 05 15	0.8		01/02/2014 05 15	---	01/02/2014 05 15		04/02/2014 20 30	.	.
01/02/2014 05 30	0.387197267	01/02/2014 05 30	0.4		01/02/2014 05 30	---	01/02/2014 05 30		04/02/2014 20 45	.	.
01/02/2014 05 45	0.573876012	01/02/2014 05 45	.		01/02/2014 05 45	---	01/02/2014 05 45		04/02/2014 21 00	.	.
01/02/2014 06 00	0.466547352	01/02/2014 06 00	.		01/02/2014 06 00	---	01/02/2014 06 00		04/02/2014 21 15	.	.
01/02/2014 06 15	0.546502447	01/02/2014 06 15	.		01/02/2014 06 15	---	01/02/2014 06 15		04/02/2014 21 30	.	.
01/02/2014 06 30	0.441953199	01/02/2014 06 30	.		01/02/2014 06 30	---	01/02/2014 06 30		04/02/2014 21 45	.	.
01/02/2014 06 45	0.410704329	01/02/2014 06 45	.		01/02/2014 06 45	---	01/02/2014 06 45		04/02/2014 22 00	.	.
01/02/2014 07 00	0.33431251	01/02/2014 07 00	.		01/02/2014 07 00	---	01/02/2014 07 00		04/02/2014 22 15	.	.
01/02/2014 07 15	0.398475929	01/02/2014 07 15	.		01/02/2014 07 15	---	01/02/2014 07 15		04/02/2014 22 30	.	.
01/02/2014 07 30	0.323520941	01/02/2014 07 30	.		01/02/2014 07 30	---	01/02/2014 07 30		04/02/2014 22 45	.	.
01/02/2014 07 45	0.35204716	01/02/2014 07 45	.		01/02/2014 07 45	---	01/02/2014 07 45		04/02/2014 23 00	.	.
01/02/2014 08 00	0.418625207	01/02/2014 08 00	.		01/02/2014 08 00	---	01/02/2014 08 00		04/02/2014 23 15	.	.
01/02/2014 08 15	0.408173133	01/02/2014 08 15	.		01/02/2014 08 15	---	01/02/2014 08 15		04/02/2014 23 30	.	.
01/02/2014 08 30	0.394108829	01/02/2014 08 30	.		01/02/2014 08 30	---	01/02/2014 08 30		04/02/2014 23 45	.	.
01/02/2014 08 45	0.394108829	01/02/2014 08 45	.		01/02/2014 08 45	---	01/02/2014 08 45		05/02/2014 00 00	.	.
01/02/2014 09 00	0.382057239	01/02/2014 09 00	.	15.6	01/02/2014 09 00	---	01/02/2014 09 00		05/02/2014 00 15	.	.
01/02/2014 09 15	0.376892271	01/02/2014 09 15	.		01/02/2014 09 15	---	01/02/2014 09 15		05/02/2014 00 30	.	.
01/02/2014 09 30	0.342822551	01/02/2014 09 30	.		01/02/2014 09 30	---	01/02/2014 09 30		05/02/2014 00 45	.	.
01/02/2014 09 45	0.360571201	01/02/2014 09 45	.		01/02/2014 09 45	---	01/02/2014 09 45		05/02/2014 01 00	.	.
01/02/2014 10 00	0.374445958	01/02/2014 10 00	.		01/02/2014 10 00	---	01/02/2014 10 00		05/02/2014 01 15	.	.
01/02/2014 10 15	0.385197699	01/02/2014 10 15	.		01/02/2014 10 15	---	01/02/2014 10 15		05/02/2014 01 30	.	.
01/02/2014 10 30	0.367142348	01/02/2014 10 30	.		01/02/2014 10 30	---	01/02/2014 10 30		05/02/2014 01 45	.	.
01/02/2014 10 45	0.345978092	01/02/2014 10 45	.		01/02/2014 10 45	---	01/02/2014 10 45		05/02/2014 02 00	.	.
01/02/2014 11 00	0.325392307	01/02/2014 11 00	.		01/02/2014 11 00	---	01/02/2014 11 00		05/02/2014 02 15	.	.
01/02/2014 11 15	0.294999053	01/02/2014 11 15	.		01/02/2014 11 15	---	01/02/2014 11 15		05/02/2014 02 30	.	.
01/02/2014 11 30	0.328495279	01/02/2014 11 30	.		01/02/2014 11 30	---	01/02/2014 11 30		05/02/2014 02 45	0.2	.
01/02/2014 11 45	0.332466998	01/02/2014 11 45	.		01/02/2014 11 45	---	01/02/2014 11 45		05/02/2014 03 00	0.2	.
01/02/2014 12 00	0.356992599	01/02/2014 12 00	.		01/02/2014 12 00	---	01/02/2014 12 00		05/02/2014 03 15	0.2	.
01/02/2014 12 15	0.319853511	01/02/2014 12 15	.		01/02/2014 12 15	---	01/02/2014 12 15		05/02/2014 03 30	0.4	.
01/02/2014 12 30	0.332843799	01/02/2014 12 30	.		01/02/2014 12 30	---	01/02/2014 12 30		05/02/2014 03 45	0.2	.
01/02/2014 12 45	0.30904217	01/02/2014 12 45	.		01/02/2014 12 45	---	01/02/2014 12 45		05/02/2014 04 00	0.4	.
01/02/2014 13 00	0.341188578	01/02/2014 13 00	.		01/02/2014 13 00	---	01/02/2014 13 00		05/02/2014 04 15	.	.
01/02/2014 13 15	0.29823397	01/02/2014 13 15	.		01/02/2014 13 15	---	01/02/2014 13 15		05/02/2014 04 30	.	.
01/02/2014 13 30	0.325334917	01/02/2014 13 30	.		01/02/2014 13 30	---	01/02/2014 13 30		05/02/2014 04 45	.	.
01/02/2014 13 45	0.24759231	01/02/2014 13 45	.		01/02/2014 13 45	---	01/02/2014 13 45		05/02/2014 05 00	.	.
01/02/2014 14 00	0.344501071	01/02/2014 14 00	.		01/02/2014 14 00	---	01/02/2014 14 00		05/02/2014 05 15	.	.
01/02/2014 14 15	0.249752095	01/02/2014 14 15	.		01/02/2014 14 15	---	01/02/2014 14 15		05/02/2014 05 30	.	.
01/02/2014 14 30	0.204600339	01/02/2014 14 30	.		01/02/2014 14 30	---	01/02/2014 14 30		05/02/2014 05 45	.	.
01/02/2014 14 45	0.219249577	01/02/2014 14 45	.		01/02/2014 14 45	---	01/02/2014 14 45		05/02/2014 06 00	.	.
01/02/2014 15 00	0.282470607	01/02/2014 15 00	.		01/02/2014 15 00	---	01/02/2014 15 00		05/02/2014 06 15	.	.
01/02/2014 15 15	0.245865062	01/02/2014 15 15	.		01/02/2014 15 15	---	01/02/2014 15 15		05/02/2014 06 30	.	.
01/02/2014 15 30	0.229459285	01/02/2014 15 30	.		01/02/2014 15 30	---	01/02/2014 15 30		05/02/2014 06 45	.	.
01/02/2014 15 45	0.231312038	01/02/2014 15 45	.		01/02/2014 15 45	---	01/02/2014 15 45		05/02/2014 07 00	.	.
01/02/2014 16 00	0.206936374	01/02/2014 16 00	.		01/02/2014 16 00	---	01/02/2014 16 00		05/02/2014 07 15	0.4	.
01/02/2014 16 15	0.184773848	01/02/2014 16 15	.		01/02/2014 16 15	---	01/02/2014 16 15		05/02/2014 07 30	1	.
01/02/2014 16 30	0.235936385	01/02/2014 16 30	.		01/02/2014 16 30	---	01/02/2014 16 30		05/02/2014 07 45	.	.
01/02/2014 16 45	0.181850606	01/02/2014 16 45	.		01/02/2014 16 45	---	01/02/2014 16 45		05/02/2014 08 00	.	0.4
01/02/2014 17 00	0.250453447	01/02/2014 17 00	.		01/02/2014 17 00	---	01/02/2014 17 00		05/02/2014 08 15	.	.
01/02/2014 17 15	0.214578765	01/02/2014 17 15	.		01/02/2014 17 15	---	01/02/2014 17 15		05/02/2014 08 30	.	.
01/02/2014 17 30	0.242094523	01/02/2014 17 30	.		01/02/2014 17 30	---	01/02/2014 17 30		05/02/2014 08 45	.	.
01/02/2014 17 45	0.154585224	01/02/2014 17 45	.		01/02/2014 17 45	---	01/02/2014 17 45		05/02/2014 09 00	.	.
01/02/2014 18 00	0.197601166	01/02/2014 18 00	.		01/02/2014 18 00	---	01/02/2014 18 00		05/02/2014 09 15	.	.
01/02/2014 18 15	0.20757494	01/02/2014 18 15	.		01/02/2014 18 15	---	01/02/2014 18 15		05/02/2014 09 30	.	.
01/02/2014 18 30	0.140254504	01/02/2014 18 30	.		01/02/2014 18 30	---	01/02/2014 18 30		05/02/2014 09 45	.	.
01/02/2014 18 45	0.184378735	01/02/2014 18 45	.		01/02/2014 18 45	---	01/02/2014 18 45		05/02/2014 10 00	.	.
01/02/2014 19 00	0.239866185	01/02/2014 19 00	.		01/02/2014 19 00	---	01/02/2014 19 00		05/02/2014 10 15	.	.
01/02/2014 19 15	0.193688787	01/02/2014 19 15	.		01/02/2014 19 15	---	01/02/2014 19 15		05/02/2014 10 30	.	.
01/02/2014 19 30	0.193688787	01/02/2014 19 30	.		01/02/2014 19 30	---	01/02/2014 19 30		05/02/2014 10 45	.	.
01/02/2014 19 45	0.191694094	01/02/2014 19 45	.		01/02/2014 19 45	---	01/02/2014 19 45		05/02/2014 11 00	.	.
01/02/2014 20 00	0.199788367	01/02/2014 20 00	.		01/02/2014 20 00	---	01/02/2014 20 00		05/02/2014 11 15	.	.
01/02/2014 20 15	0.14185344	01/02/2014 20 15	.		01/02/2014 20 15	---	01/02/2014 20 15		05/02/2014 11 30	.	.
01/02/2014 20 30	0.178586808	01/02/2014 20 30	.		01/02/2014 20 30	---	01/02/2014 20 30		05/02/2014 11 45	.	.
01/02/2014 20 45	0.181171121	01/02/2014 20 45	.		01/02/2014 20 45	---	01/02/2014 20 45		05/02/2014 12 00	.	.
01/02/2014 21 00	0.173730383	01/02/2014 21 00	.		01/02/2014 21 00	---	01/02/2014 21 00		05/02/2014 12 15	.	.
01/02/2014 21 15	0.156285192	01/02/2014 21 15	.		01/02/2014 21 15	---	01/02/2014 21 15		05/02/2014 12 30	.	.
01/02/2014 21 30	0.201517352	01/02/2014 21 30	.		01/02/2014 21 30	---	01/02/2014 21 30		05/02/2014 12 45	.	.
01/02/2014 21 45	0.176558194	01/02/2014 21 45	.		01/02/2014 21 45	---	01/02/2014 21 45		05/02/2014 13 00	.	.
01/02/2014 22 00	0.17236745	01/02/2014 22 00	.		01/02/2014 22 00	---	01/02/2014 22 00		05/02/2014 13 15	.	.

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
01/02/2014 22 15	0.166225221	01/02/2014 22 15	.		01/02/2014 22 15	---	01/02/2014 22 15		05/02/2014 13 30	.	.
01/02/2014 22 30	0.180257058	01/02/2014 22 30	.		01/02/2014 22 30	---	01/02/2014 22 30		05/02/2014 13 45	.	.
01/02/2014 22 45	0.15104811	01/02/2014 22 45	.		01/02/2014 22 45	---	01/02/2014 22 45		05/02/2014 14 00	.	.
01/02/2014 23 00	0.176301882	01/02/2014 23 00	.		01/02/2014 23 00	---	01/02/2014 23 00		05/02/2014 14 15	0.4	.
01/02/2014 23 15	0.169059948	01/02/2014 23 15	.		01/02/2014 23 15	---	01/02/2014 23 15		05/02/2014 14 30	0.2	.
01/02/2014 23 30	0.183847853	01/02/2014 23 30	.		01/02/2014 23 30	---	01/02/2014 23 30		05/02/2014 14 45	0.2	.
01/02/2014 23 45	0.144810948	01/02/2014 23 45	.		01/02/2014 23 45	---	01/02/2014 23 45		05/02/2014 15 00	.	.
02/02/2014 00 00	0.164658061	02/02/2014 00 00	.		02/02/2014 00 00	---	02/02/2014 00 00		05/02/2014 15 15	0.2	.
02/02/2014 00 15	0.162630942	02/02/2014 00 15	.		02/02/2014 00 15	---	02/02/2014 00 15		05/02/2014 15 30	.	.
02/02/2014 00 30	0.117947979	02/02/2014 00 30	.		02/02/2014 00 30	---	02/02/2014 00 30		05/02/2014 15 45	.	.
02/02/2014 00 45	0.116253498	02/02/2014 00 45	.		02/02/2014 00 45	---	02/02/2014 00 45		05/02/2014 16 00	.	.
02/02/2014 01 00	0.152404942	02/02/2014 01 00	.		02/02/2014 01 00	---	02/02/2014 01 00		05/02/2014 16 15	.	.
02/02/2014 01 15	0.140957829	02/02/2014 01 15	.		02/02/2014 01 15	---	02/02/2014 01 15		05/02/2014 16 30	.	.
02/02/2014 01 30	0.149984217	02/02/2014 01 30	.		02/02/2014 01 30	---	02/02/2014 01 30		05/02/2014 16 45	.	.
02/02/2014 01 45	0.126654364	02/02/2014 01 45	.		02/02/2014 01 45	---	02/02/2014 01 45		05/02/2014 17 00	.	.
02/02/2014 02 00	0.107010785	02/02/2014 02 00	.		02/02/2014 02 00	---	02/02/2014 02 00		05/02/2014 17 15	.	.
02/02/2014 02 15	0.148688436	02/02/2014 02 15	.		02/02/2014 02 15	---	02/02/2014 02 15		05/02/2014 17 30	.	.
02/02/2014 02 30	0.079762721	02/02/2014 02 30	.		02/02/2014 02 30	---	02/02/2014 02 30		05/02/2014 17 45	.	.
02/02/2014 02 45	0.110112866	02/02/2014 02 45	.		02/02/2014 02 45	---	02/02/2014 02 45		05/02/2014 18 00	.	.
02/02/2014 03 00	0.138271825	02/02/2014 03 00	.		02/02/2014 03 00	---	02/02/2014 03 00		05/02/2014 18 15	.	.
02/02/2014 03 15	0.069792015	02/02/2014 03 15	.		02/02/2014 03 15	---	02/02/2014 03 15		05/02/2014 18 30	.	.
02/02/2014 03 30	0.085809077	02/02/2014 03 30	.		02/02/2014 03 30	---	02/02/2014 03 30		05/02/2014 18 45	.	.
02/02/2014 03 45	0.101278853	02/02/2014 03 45	.		02/02/2014 03 45	---	02/02/2014 03 45		05/02/2014 19 00	.	.
02/02/2014 04 00	0.100100278	02/02/2014 04 00	.		02/02/2014 04 00	---	02/02/2014 04 00		05/02/2014 19 15	.	.
02/02/2014 04 15	0.083648131	02/02/2014 04 15	.		02/02/2014 04 15	---	02/02/2014 04 15		05/02/2014 19 30	.	.
02/02/2014 04 30	0.074887991	02/02/2014 04 30	.		02/02/2014 04 30	---	02/02/2014 04 30		05/02/2014 19 45	.	.
02/02/2014 04 45	0.075918897	02/02/2014 04 45	.		02/02/2014 04 45	---	02/02/2014 04 45		05/02/2014 20 00	.	.
02/02/2014 05 00	0.101805265	02/02/2014 05 00	.		02/02/2014 05 00	---	02/02/2014 05 00		05/02/2014 20 15	.	.
02/02/2014 05 15	0.098159338	02/02/2014 05 15	.		02/02/2014 05 15	---	02/02/2014 05 15		05/02/2014 20 30	.	.
02/02/2014 05 30	0.102853768	02/02/2014 05 30	.		02/02/2014 05 30	---	02/02/2014 05 30		05/02/2014 20 45	.	.
02/02/2014 05 45	0.086588243	02/02/2014 05 45	.		02/02/2014 05 45	---	02/02/2014 05 45		05/02/2014 21 00	.	.
02/02/2014 06 00	0.088203889	02/02/2014 06 00	.		02/02/2014 06 00	---	02/02/2014 06 00		05/02/2014 21 15	.	.
02/02/2014 06 15	0.086978201	02/02/2014 06 15	.		02/02/2014 06 15	---	02/02/2014 06 15		05/02/2014 21 30	.	.
02/02/2014 06 30	0.079827955	02/02/2014 06 30	.		02/02/2014 06 30	---	02/02/2014 06 30		05/02/2014 21 45	.	.
02/02/2014 06 45	0.095929677	02/02/2014 06 45	.		02/02/2014 06 45	---	02/02/2014 06 45		05/02/2014 22 00	.	.
02/02/2014 07 00	0.080404949	02/02/2014 07 00	.		02/02/2014 07 00	---	02/02/2014 07 00		05/02/2014 22 15	.	.
02/02/2014 07 15	0.093179476	02/02/2014 07 15	.		02/02/2014 07 15	---	02/02/2014 07 15		05/02/2014 22 30	.	.
02/02/2014 07 30	0.097404917	02/02/2014 07 30	.		02/02/2014 07 30	---	02/02/2014 07 30		05/02/2014 22 45	.	.
02/02/2014 07 45	0.070792446	02/02/2014 07 45	.		02/02/2014 07 45	---	02/02/2014 07 45		05/02/2014 23 00	.	.
02/02/2014 08 00	0.082871629	02/02/2014 08 00	.		02/02/2014 08 00	---	02/02/2014 08 00		05/02/2014 23 15	.	.
02/02/2014 08 15	0.086695717	02/02/2014 08 15	.		02/02/2014 08 15	---	02/02/2014 08 15		05/02/2014 23 30	.	.
02/02/2014 08 30	0.068033619	02/02/2014 08 30	.		02/02/2014 08 30	---	02/02/2014 08 30		05/02/2014 23 45	.	.
02/02/2014 08 45	0.067025649	02/02/2014 08 45	.		02/02/2014 08 45	1.27	02/02/2014 08 45		06/02/2014 00 00	.	.
02/02/2014 09 00	0.080296373	02/02/2014 09 00	.	0	02/02/2014 09 00	1.25	02/02/2014 09 00		06/02/2014 00 15	.	.
02/02/2014 09 15	0.074371705	02/02/2014 09 15	.		02/02/2014 09 15	1.23	02/02/2014 09 15		06/02/2014 00 30	.	.
02/02/2014 09 30	0.083963035	02/02/2014 09 30	.		02/02/2014 09 30	1.22	02/02/2014 09 30		06/02/2014 00 45	.	.
02/02/2014 09 45	0.082681808	02/02/2014 09 45	.		02/02/2014 09 45	1.2	02/02/2014 09 45		06/02/2014 01 00	.	.
02/02/2014 10 00	0.087420514	02/02/2014 10 00	.		02/02/2014 10 00	1.18	02/02/2014 10 00		06/02/2014 01 15	.	.
02/02/2014 10 15	0.078072705	02/02/2014 10 15	.		02/02/2014 10 15	1.17	02/02/2014 10 15		06/02/2014 01 30	.	.
02/02/2014 10 30	0.081411208	02/02/2014 10 30	.		02/02/2014 10 30	1.15	02/02/2014 10 30		06/02/2014 01 45	0.2	.
02/02/2014 10 45	0.066880148	02/02/2014 10 45	.		02/02/2014 10 45	1.13	02/02/2014 10 45		06/02/2014 02 00	.	.
02/02/2014 11 00	0.063562384	02/02/2014 11 00	.		02/02/2014 11 00	1.13	02/02/2014 11 00		06/02/2014 02 15	.	.
02/02/2014 11 15	0.076833442	02/02/2014 11 15	.		02/02/2014 11 15	1.11	02/02/2014 11 15		06/02/2014 02 30	.	.
02/02/2014 11 30	0.047358474	02/02/2014 11 30	.		02/02/2014 11 30	1.1	02/02/2014 11 30		06/02/2014 02 45	.	.
02/02/2014 11 45	0.063562384	02/02/2014 11 45	.		02/02/2014 11 45	1.08	02/02/2014 11 45		06/02/2014 03 00	.	.
02/02/2014 12 00	0.094727727	02/02/2014 12 00	.		02/02/2014 12 00	1.07	02/02/2014 12 00		06/02/2014 03 15	.	.
02/02/2014 12 15	0.080939313	02/02/2014 12 15	.		02/02/2014 12 15	1.06	02/02/2014 12 15		06/02/2014 03 30	.	.
02/02/2014 12 30		02/02/2014 12 30	.		02/02/2014 12 30	1.05	02/02/2014 12 30		06/02/2014 03 45	.	.
02/02/2014 12 45	0.094583796	02/02/2014 12 45	.		02/02/2014 12 45	1.03	02/02/2014 12 45		06/02/2014 04 00	.	.
02/02/2014 13 00	0.070794367	02/02/2014 13 00	.		02/02/2014 13 00	1.02	02/02/2014 13 00		06/02/2014 04 15	.	.
02/02/2014 13 15	0.073450996	02/02/2014 13 15	.		02/02/2014 13 15	1.01	02/02/2014 13 15		06/02/2014 04 30	.	.
02/02/2014 13 30	0.051947103	02/02/2014 13 30	.		02/02/2014 13 30	0.997	02/02/2014 13 30		06/02/2014 04 45	.	.
02/02/2014 13 45	0.054681323	02/02/2014 13 45	.		02/02/2014 13 45	0.989	02/02/2014 13 45		06/02/2014 05 00	.	.
02/02/2014 14 00	0.071163252	02/02/2014 14 00	.		02/02/2014 14 00	0.981	02/02/2014 14 00		06/02/2014 05 15	.	.
02/02/2014 14 15	0.083069698	02/02/2014 14 15	.		02/02/2014 14 15	0.964	02/02/2014 14 15		06/02/2014 05 30	.	.
02/02/2014 14 30	0.0762215	02/02/2014 14 30	.		02/02/2014 14 30	0.956	02/02/2014 14 30		06/02/2014 05 45	.	.
02/02/2014 14 45	0.065745163	02/02/2014 14 45	.		02/02/2014 14 45	0.94	02/02/2014 14 45		06/02/2014 06 00	.	.
02/02/2014 15 00	0.072607003	02/02/2014 15 00	.		02/02/2014 15 00	0.931	02/02/2014 15 00		06/02/2014 06 15	.	.
02/02/2014 15 15	0.052690576	02/02/2014 15 15	.		02/02/2014 15 15	0.923	02/02/2014 15 15		06/02/2014 06 30	.	.
02/02/2014 15 30	0.064400997	02/02/2014 15 30	.		02/02/2014 15 30	0.915	02/02/2014 15 30		06/02/2014 06 45	.	.
02/02/2014 15 45	0.057012323	02/02/2014 15 45	.		02/02/2014 15 45	0.899	02/02/2014 15 45		06/02/2014 07 00	.	.
02/02/2014 16 00	0.05898033	02/02/2014 16 00	.		02/02/2014 16 00	0.891	02/02/2014 16 00		06/02/2014 07 15	.	.
02/02/2014 16 15	0.065444755	02/02/2014 16 15	.		02/02/2014 16 15	0.883	02/02/2014 16 15		06/02/2014 07 30	.	.
02/02/2014 16 30	0.04074796	02/02/2014 16 30	.		02/02/2014 16 30	0.875	02/02/2014 16 30		06/02/2014 07 45	.	.
02/02/2014 16 45	0.063873652	02/02/2014 16 45	.		02/02/2014 16 45	0.86	02/02/2014 16 45		06/02/2014 08 00	.	.

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G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
02/02/2014 17 00	0.05002828	02/02/2014 17 00	.		02/02/2014 17 00	0.852	02/02/2014 17 00		06/02/2014 08 15	.	.
02/02/2014 17 15	0.05684741	02/02/2014 17 15	.		02/02/2014 17 15	0.844	02/02/2014 17 15		06/02/2014 08 30	.	.
02/02/2014 17 30	0.047539477	02/02/2014 17 30	.		02/02/2014 17 30	0.836	02/02/2014 17 30		06/02/2014 08 45	.	.
02/02/2014 17 45	0.053111323	02/02/2014 17 45	.		02/02/2014 17 45	0.828	02/02/2014 17 45		06/02/2014 09 00	.	.
02/02/2014 18 00	0.059091756	02/02/2014 18 00	.		02/02/2014 18 00	0.821	02/02/2014 18 00		06/02/2014 09 15	.	.
02/02/2014 18 15	0.046184417	02/02/2014 18 15	.		02/02/2014 18 15	0.813	02/02/2014 18 15		06/02/2014 09 30	.	.
02/02/2014 18 30	0.054281963	02/02/2014 18 30	.		02/02/2014 18 30	0.805	02/02/2014 18 30		06/02/2014 09 45	.	.
02/02/2014 18 45	0.060255762	02/02/2014 18 45	.		02/02/2014 18 45	0.79	02/02/2014 18 45		06/02/2014 10 00	.	.
02/02/2014 19 00	0.054359679	02/02/2014 19 00	.		02/02/2014 19 00	0.782	02/02/2014 19 00		06/02/2014 10 15	.	.
02/02/2014 19 15	0.050706529	02/02/2014 19 15	.		02/02/2014 19 15	0.775	02/02/2014 19 15		06/02/2014 10 30	.	.
02/02/2014 19 30	0.066140011	02/02/2014 19 30	.		02/02/2014 19 30	0.767	02/02/2014 19 30		06/02/2014 10 45	.	.
02/02/2014 19 45	0.056560608	02/02/2014 19 45	.		02/02/2014 19 45	0.767	02/02/2014 19 45		06/02/2014 11 00	.	.
02/02/2014 20 00	0.056560608	02/02/2014 20 00	.		02/02/2014 20 00	0.76	02/02/2014 20 00		06/02/2014 11 15	.	.
02/02/2014 20 15	0.054964041	02/02/2014 20 15	.		02/02/2014 20 15	0.752	02/02/2014 20 15		06/02/2014 11 30	.	.
02/02/2014 20 30	0.06081812	02/02/2014 20 30	.		02/02/2014 20 30	0.745	02/02/2014 20 30		06/02/2014 11 45	.	.
02/02/2014 20 45	0.061882498	02/02/2014 20 45	.		02/02/2014 20 45	0.737	02/02/2014 20 45		06/02/2014 12 00	.	.
02/02/2014 21 00	0.040594937	02/02/2014 21 00	.		02/02/2014 21 00	0.737	02/02/2014 21 00		06/02/2014 12 15	.	.
02/02/2014 21 15	0.056028419	02/02/2014 21 15	.		02/02/2014 21 15	0.73	02/02/2014 21 15		06/02/2014 12 30	.	.
02/02/2014 21 30	0.058197179	02/02/2014 21 30	.		02/02/2014 21 30	0.723	02/02/2014 21 30		06/02/2014 12 45	.	.
02/02/2014 21 45	0.047740104	02/02/2014 21 45	.		02/02/2014 21 45	0.715	02/02/2014 21 45		06/02/2014 13 00	0.2	.
02/02/2014 22 00	0.055657007	02/02/2014 22 00	.		02/02/2014 22 00	0.708	02/02/2014 22 00		06/02/2014 13 15	0.2	.
02/02/2014 22 15	0.054665717	02/02/2014 22 15	.		02/02/2014 22 15	0.701	02/02/2014 22 15		06/02/2014 13 30	.	.
02/02/2014 22 30	0.053170865	02/02/2014 22 30	.		02/02/2014 22 30	0.694	02/02/2014 22 30		06/02/2014 13 45	0.2	.
02/02/2014 22 45	0.060864167	02/02/2014 22 45	.		02/02/2014 22 45	0.686	02/02/2014 22 45		06/02/2014 14 00	0.4	.
02/02/2014 23 00	0.047107692	02/02/2014 23 00	.		02/02/2014 23 00	0.686	02/02/2014 23 00		06/02/2014 14 15	0.2	.
02/02/2014 23 15	0.046186572	02/02/2014 23 15	.		02/02/2014 23 15	0.679	02/02/2014 23 15		06/02/2014 14 30	0.4	.
02/02/2014 23 30	0.052303216	02/02/2014 23 30	.		02/02/2014 23 30	0.672	02/02/2014 23 30		06/02/2014 14 45	0.4	.
02/02/2014 23 45	0.051847186	02/02/2014 23 45	.		02/02/2014 23 45	0.665	02/02/2014 23 45		06/02/2014 15 00	0.2	.
03/02/2014 00 00	0.054338673	03/02/2014 00 00	.		03/02/2014 00 00	0.658	03/02/2014 00 00		06/02/2014 15 15	0.4	.
03/02/2014 00 15	0.051393291	03/02/2014 00 15	.		03/02/2014 00 15	0.658	03/02/2014 00 15		06/02/2014 15 30	0.4	0.2
03/02/2014 00 30	0.049959761	03/02/2014 00 30	.		03/02/2014 00 30	0.651	03/02/2014 00 30		06/02/2014 15 45	0.6	.
03/02/2014 00 45	0.048543126	03/02/2014 00 45	.		03/02/2014 00 45	0.644	03/02/2014 00 45		06/02/2014 16 00	0.6	0.2
03/02/2014 01 00	0.059231128	03/02/2014 01 00	.		03/02/2014 01 00	0.637	03/02/2014 01 00		06/02/2014 16 15	0.4	.
03/02/2014 01 15	0.051494931	03/02/2014 01 15	.		03/02/2014 01 15	0.63	03/02/2014 01 15		06/02/2014 16 30	0.4	0.4
03/02/2014 01 30	0.052489068	03/02/2014 01 30	.		03/02/2014 01 30	0.63	03/02/2014 01 30		06/02/2014 16 45	0.4	0.2
03/02/2014 01 45	0.034870229	03/02/2014 01 45	.		03/02/2014 01 45	0.623	03/02/2014 01 45		06/02/2014 17 00	0.4	0.2
03/02/2014 02 00	0.048714654	03/02/2014 02 00	.		03/02/2014 02 00	0.623	03/02/2014 02 00		06/02/2014 17 15	0.8	0.4
03/02/2014 02 15	0.045931153	03/02/2014 02 15	.		03/02/2014 02 15	0.616	03/02/2014 02 15		06/02/2014 17 30	0.6	0.2
03/02/2014 02 30	0.04737351	03/02/2014 02 30	.		03/02/2014 02 30	0.609	03/02/2014 02 30		06/02/2014 17 45	0.6	0.2
03/02/2014 02 45	0.045095729	03/02/2014 02 45	.		03/02/2014 02 45	0.609	03/02/2014 02 45		06/02/2014 18 00	0.6	0.2
03/02/2014 03 00	0.037810251	03/02/2014 03 00	.		03/02/2014 03 00	0.602	03/02/2014 03 00		06/02/2014 18 15	0.2	0.2
03/02/2014 03 15	0.041474712	03/02/2014 03 15	.		03/02/2014 03 15	0.596	03/02/2014 03 15		06/02/2014 18 30	0.4	.
03/02/2014 03 30	0.048358754	03/02/2014 03 30	.		03/02/2014 03 30	0.596	03/02/2014 03 30		06/02/2014 18 45	.	0.2
03/02/2014 03 45	0.040251006	03/02/2014 03 45	.		03/02/2014 03 45	0.589	03/02/2014 03 45		06/02/2014 19 00	0.2	0.4
03/02/2014 04 00	0.035398	03/02/2014 04 00	.		03/02/2014 04 00	0.582	03/02/2014 04 00		06/02/2014 19 15	.	0.4
03/02/2014 04 15	0.043487037	03/02/2014 04 15	.		03/02/2014 04 15	0.582	03/02/2014 04 15		06/02/2014 19 30	0.2	0.2
03/02/2014 04 30	0.040380752	03/02/2014 04 30	.		03/02/2014 04 30	0.575	03/02/2014 04 30		06/02/2014 19 45	.	.
03/02/2014 04 45	0.030618142	03/02/2014 04 45	.		03/02/2014 04 45	0.575	03/02/2014 04 45		06/02/2014 20 00	.	.
03/02/2014 05 00	0.03647607	03/02/2014 05 00	.		03/02/2014 05 00	0.569	03/02/2014 05 00		06/02/2014 20 15	.	.
03/02/2014 05 15	0.030009936	03/02/2014 05 15		0.2	03/02/2014 05 15	0.562	03/02/2014 05 15		06/02/2014 20 30	.	.
03/02/2014 05 30	0.024769888	03/02/2014 05 30	.		03/02/2014 05 30	0.562	03/02/2014 05 30		06/02/2014 20 45	.	.
03/02/2014 05 45	0.020179243	03/02/2014 05 45	.		03/02/2014 05 45	0.556	03/02/2014 05 45		06/02/2014 21 00	.	.
03/02/2014 06 00	0.036205624	03/02/2014 06 00	.		03/02/2014 06 00	0.556	03/02/2014 06 00		06/02/2014 21 15	.	.
03/02/2014 06 15	0.038804496	03/02/2014 06 15	.		03/02/2014 06 15	0.556	03/02/2014 06 15		06/02/2014 21 30	.	.
03/02/2014 06 30	0.044002241	03/02/2014 06 30	.		03/02/2014 06 30	0.549	03/02/2014 06 30		06/02/2014 21 45	.	.
03/02/2014 06 45	0.034039897	03/02/2014 06 45	.		03/02/2014 06 45	0.549	03/02/2014 06 45		06/02/2014 22 00	.	.
03/02/2014 07 00	0.039719839	03/02/2014 07 00	.		03/02/2014 07 00	0.542	03/02/2014 07 00		06/02/2014 22 15	.	.
03/02/2014 07 15	0.038371351	03/02/2014 07 15	.		03/02/2014 07 15	0.542	03/02/2014 07 15		06/02/2014 22 30	.	.
03/02/2014 07 30	0.037938205	03/02/2014 07 30	.		03/02/2014 07 30	0.536	03/02/2014 07 30		06/02/2014 22 45	0.2	.
03/02/2014 07 45	0.039237642	03/02/2014 07 45	.		03/02/2014 07 45	0.536	03/02/2014 07 45		06/02/2014 23 00	0.2	.
03/02/2014 08 00	0.044435387	03/02/2014 08 00	.		03/02/2014 08 00	0.529	03/02/2014 08 00		06/02/2014 23 15	.	0.2
03/02/2014 08 15	0.039180021	03/02/2014 08 15	.		03/02/2014 08 15	0.529	03/02/2014 08 15		06/02/2014 23 30	.	.
03/02/2014 08 30	0.031193583	03/02/2014 08 30	.		03/02/2014 08 30	0.529	03/02/2014 08 30		06/02/2014 23 45	.	.
03/02/2014 08 45	0.043896965	03/02/2014 08 45	.		03/02/2014 08 45	0.523	03/02/2014 08 45		07/02/2014 00 00	.	.
03/02/2014 09 00	0.038360517	03/02/2014 09 00	.	0.2	03/02/2014 09 00	0.523	03/02/2014 09 00		07/02/2014 00 15	.	.
03/02/2014 09 15	0.050635662	03/02/2014 09 15	.		03/02/2014 09 15	0.523	03/02/2014 09 15		07/02/2014 00 30	.	.
03/02/2014 09 30	0.045931153	03/02/2014 09 30	.		03/02/2014 09 30	0.517	03/02/2014 09 30		07/02/2014 00 45	.	.
03/02/2014 09 45	0.052022416	03/02/2014 09 45	.		03/02/2014 09 45	0.517	03/02/2014 09 45		07/02/2014 01 00	.	.
03/02/2014 10 00	0.056774732	03/02/2014 10 00	.		03/02/2014 10 00	0.517	03/02/2014 10 00		07/02/2014 01 15	.	.
03/02/2014 10 15	0.055357138	03/02/2014 10 15	.		03/02/2014 10 15	0.51	03/02/2014 10 15		07/02/2014 01 30	.	.
03/02/2014 10 30	0.057297079	03/02/2014 10 30	.		03/02/2014 10 30	0.51	03/02/2014 10 30		07/02/2014 01 45	0.2	.
03/02/2014 10 45	0.04520927	03/02/2014 10 45	.		03/02/2014 10 45	0.51	03/02/2014 10 45		07/02/2014 02 00	.	.
03/02/2014 11 00	0.057780591	03/02/2014 11 00	.		03/02/2014 11 00	0.51	03/02/2014 11 00		07/02/2014 02 15	.	.
03/02/2014 11 15	0.049517511	03/02/2014 11 15	.		03/02/2014 11 15	0.504	03/02/2014 11 15		07/02/2014 02 30	0.2	.
03/02/2014 11 30	0.062809729	03/02/2014 11 30	.		03/02/2014 11 30	0.504	03/02/2014 11 30		07/02/2014 02 45	0.2	.

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
03/02/2014 11 45	0.056788174	03/02/2014 11 45	.		03/02/2014 11 45	0.504	03/02/2014 11 45		07/02/2014 03 00	0.6	.
03/02/2014 12 00	0.058816662	03/02/2014 12 00	.		03/02/2014 12 00	0.504	03/02/2014 12 00		07/02/2014 03 15	0.4	0.2
03/02/2014 12 15	0.054240679	03/02/2014 12 15	.		03/02/2014 12 15	0.497	03/02/2014 12 15		07/02/2014 03 30	0.2	.
03/02/2014 12 30	0.054813319	03/02/2014 12 30	.		03/02/2014 12 30	0.497	03/02/2014 12 30		07/02/2014 03 45	.	.
03/02/2014 12 45	0.047860807	03/02/2014 12 45	.		03/02/2014 12 45	0.497	03/02/2014 12 45		07/02/2014 04 00	.	0.2
03/02/2014 13 00	0.043578278	03/02/2014 13 00	.		03/02/2014 13 00	0.497	03/02/2014 13 00		07/02/2014 04 15	.	0.6
03/02/2014 13 15	0.057312589	03/02/2014 13 15	.		03/02/2014 13 15	0.491	03/02/2014 13 15		07/02/2014 04 30	.	0.2
03/02/2014 13 30	0.036363316	03/02/2014 13 30	.		03/02/2014 13 30	0.491	03/02/2014 13 30		07/02/2014 04 45	.	0.2
03/02/2014 13 45	0.054389435	03/02/2014 13 45	.		03/02/2014 13 45	0.491	03/02/2014 13 45		07/02/2014 05 00	.	0.2
03/02/2014 14 00	0.041824684	03/02/2014 14 00	.		03/02/2014 14 00	0.491	03/02/2014 14 00		07/02/2014 05 15	0.2	0.4
03/02/2014 14 15	0.04959902	03/02/2014 14 15	.		03/02/2014 14 15	0.491	03/02/2014 14 15		07/02/2014 05 30	0.2	0.8
03/02/2014 14 30	0.051518393	03/02/2014 14 30	.		03/02/2014 14 30	0.485	03/02/2014 14 30		07/02/2014 05 45	0.4	1
03/02/2014 14 45	0.049631959	03/02/2014 14 45	.		03/02/2014 14 45	0.485	03/02/2014 14 45		07/02/2014 06 00	0.2	3
03/02/2014 15 00	0.04677485	03/02/2014 15 00	.		03/02/2014 15 00	0.479	03/02/2014 15 00		07/02/2014 06 15	1.6	0.8
03/02/2014 15 15	0.050108144	03/02/2014 15 15	.		03/02/2014 15 15	0.479	03/02/2014 15 15		07/02/2014 06 30	0.2	0.6
03/02/2014 15 30	0.040681517	03/02/2014 15 30	.		03/02/2014 15 30	0.479	03/02/2014 15 30		07/02/2014 06 45	0.4	0.4
03/02/2014 15 45	0.040773242	03/02/2014 15 45	.		03/02/2014 15 45	0.479	03/02/2014 15 45		07/02/2014 07 00	0.4	0.2
03/02/2014 16 00	0.045462252	03/02/2014 16 00	.		03/02/2014 16 00	0.472	03/02/2014 16 00		07/02/2014 07 15	0.4	0.6
03/02/2014 16 15	0.043044204	03/02/2014 16 15	.		03/02/2014 16 15	0.472	03/02/2014 16 15		07/02/2014 07 30	0.2	0.2
03/02/2014 16 30	0.043117747	03/02/2014 16 30	.		03/02/2014 16 30	0.466	03/02/2014 16 30		07/02/2014 07 45	.	0.2
03/02/2014 16 45	0.042648846	03/02/2014 16 45	.		03/02/2014 16 45	0.466	03/02/2014 16 45		07/02/2014 08 00	.	.
03/02/2014 17 00	0.047838785	03/02/2014 17 00	.		03/02/2014 17 00	0.466	03/02/2014 17 00		07/02/2014 08 15	.	.
03/02/2014 17 15	0.037137448	03/02/2014 17 15	.		03/02/2014 17 15	0.46	03/02/2014 17 15		07/02/2014 08 30	.	.
03/02/2014 17 30	0.054817919	03/02/2014 17 30	.		03/02/2014 17 30	0.46	03/02/2014 17 30		07/02/2014 08 45	.	.
03/02/2014 17 45	0.048275658	03/02/2014 17 45	.		03/02/2014 17 45	0.46	03/02/2014 17 45		07/02/2014 09 00	0.2	.
03/02/2014 18 00	0.036206897	03/02/2014 18 00	.		03/02/2014 18 00	0.454	03/02/2014 18 00		07/02/2014 09 15	.	0.2
03/02/2014 18 15	0.049682361	03/02/2014 18 15	.		03/02/2014 18 15	0.454	03/02/2014 18 15		07/02/2014 09 30	.	.
03/02/2014 18 30	0.051089064	03/02/2014 18 30	.		03/02/2014 18 30	0.454	03/02/2014 18 30		07/02/2014 09 45	.	.
03/02/2014 18 45	0.041154055	03/02/2014 18 45	.		03/02/2014 18 45	0.454	03/02/2014 18 45		07/02/2014 10 00	.	.
03/02/2014 19 00	0.052022416	03/02/2014 19 00	.		03/02/2014 19 00	0.454	03/02/2014 19 00		07/02/2014 10 15	.	.
03/02/2014 19 15	0.046824504	03/02/2014 19 15	.		03/02/2014 19 15	0.448	03/02/2014 19 15		07/02/2014 10 30	.	.
03/02/2014 19 30	0.054877295	03/02/2014 19 30	.		03/02/2014 19 30	0.448	03/02/2014 19 30		07/02/2014 10 45	.	.
03/02/2014 19 45	0.055357138	03/02/2014 19 45	.		03/02/2014 19 45	0.448	03/02/2014 19 45		07/02/2014 11 00	.	.
03/02/2014 20 00	0.052478079	03/02/2014 20 00	.		03/02/2014 20 00	0.442	03/02/2014 20 00		07/02/2014 11 15	.	.
03/02/2014 20 15	0.048110344	03/02/2014 20 15	.		03/02/2014 20 15	0.442	03/02/2014 20 15		07/02/2014 11 30	.	.
03/02/2014 20 30	0.049077369	03/02/2014 20 30	.		03/02/2014 20 30	0.442	03/02/2014 20 30		07/02/2014 11 45	.	.
03/02/2014 20 45	0.05536382	03/02/2014 20 45	.		03/02/2014 20 45	0.442	03/02/2014 20 45		07/02/2014 12 00	.	.
03/02/2014 21 00	0.05341505	03/02/2014 21 00	.		03/02/2014 21 00	0.442	03/02/2014 21 00		07/02/2014 12 15	.	.
03/02/2014 21 15	0.049030319	03/02/2014 21 15	.		03/02/2014 21 15	0.442	03/02/2014 21 15		07/02/2014 12 30	.	.
03/02/2014 21 30	0.051011418	03/02/2014 21 30	.		03/02/2014 21 30	0.436	03/02/2014 21 30		07/02/2014 12 45	.	.
03/02/2014 21 45	0.05536303	03/02/2014 21 45	.		03/02/2014 21 45	0.436	03/02/2014 21 45		07/02/2014 13 00	.	.
03/02/2014 22 00	0.050527906	03/02/2014 22 00	.		03/02/2014 22 00	0.436	03/02/2014 22 00		07/02/2014 13 15	.	.
03/02/2014 22 15	0.041341171	03/02/2014 22 15	.		03/02/2014 22 15	0.436	03/02/2014 22 15		07/02/2014 13 30	.	.
03/02/2014 22 30	0.038440097	03/02/2014 22 30	.		03/02/2014 22 30	0.436	03/02/2014 22 30		07/02/2014 13 45	.	.
03/02/2014 22 45	0.049119177	03/02/2014 22 45	.		03/02/2014 22 45	0.436	03/02/2014 22 45		07/02/2014 14 00	.	.
03/02/2014 23 00	0.041060632	03/02/2014 23 00	.		03/02/2014 23 00	0.436	03/02/2014 23 00		07/02/2014 14 15	.	.
03/02/2014 23 15	0.043441556	03/02/2014 23 15	.		03/02/2014 23 15	0.43	03/02/2014 23 15		07/02/2014 14 30	.	.
03/02/2014 23 30	0.04772722	03/02/2014 23 30	.		03/02/2014 23 30	0.43	03/02/2014 23 30		07/02/2014 14 45	.	.
03/02/2014 23 45	0.054869992	03/02/2014 23 45	.		03/02/2014 23 45	0.43	03/02/2014 23 45		07/02/2014 15 00	.	.
04/02/2014 00 00	0.050604804	04/02/2014 00 00	.		04/02/2014 00 00	0.43	04/02/2014 00 00		07/02/2014 15 15	.	.
04/02/2014 00 15	0.049659729	04/02/2014 00 15	.		04/02/2014 00 15	0.43	04/02/2014 00 15	.	07/02/2014 15 30	.	.
04/02/2014 00 30	0.036553133	04/02/2014 00 30	.		04/02/2014 00 30	0.43	04/02/2014 00 30	.	07/02/2014 15 45	.	.
04/02/2014 00 45	0.03899855	04/02/2014 00 45	.		04/02/2014 00 45	0.43	04/02/2014 00 45	.	07/02/2014 16 00	.	.
04/02/2014 01 00	0.041790203	04/02/2014 01 00	.		04/02/2014 01 00	0.43	04/02/2014 01 00	.	07/02/2014 16 15	.	.
04/02/2014 01 15	0.04140244	04/02/2014 01 15	.		04/02/2014 01 15	0.43	04/02/2014 01 15	.	07/02/2014 16 30	.	.
04/02/2014 01 30	0.035519962	04/02/2014 01 30	.		04/02/2014 01 30	0.43	04/02/2014 01 30	.	07/02/2014 16 45	.	.
04/02/2014 01 45	0.047904289	04/02/2014 01 45	.		04/02/2014 01 45	0.43	04/02/2014 01 45	.	07/02/2014 17 00	.	.
04/02/2014 02 00	0.044759846	04/02/2014 02 00	.		04/02/2014 02 00	0.424	04/02/2014 02 00	.	07/02/2014 17 15	.	.
04/02/2014 02 15	0.037187255	04/02/2014 02 15	.		04/02/2014 02 15	0.424	04/02/2014 02 15	.	07/02/2014 17 30	.	.
04/02/2014 02 30	0.038605732	04/02/2014 02 30	.		04/02/2014 02 30	0.424	04/02/2014 02 30	.	07/02/2014 17 45	.	.
04/02/2014 02 45	0.037356484	04/02/2014 02 45	.		04/02/2014 02 45	0.424	04/02/2014 02 45	.	07/02/2014 18 00	.	.
04/02/2014 03 00	0.033834826	04/02/2014 03 00	.		04/02/2014 03 00	0.424	04/02/2014 03 00	.	07/02/2014 18 15	.	.
04/02/2014 03 15	0.036996667	04/02/2014 03 15	.		04/02/2014 03 15	0.424	04/02/2014 03 15	.	07/02/2014 18 30	.	.
04/02/2014 03 30	0.035772478	04/02/2014 03 30	.		04/02/2014 03 30	0.418	04/02/2014 03 30	.	07/02/2014 18 45	.	.
04/02/2014 03 45	0.038804496	04/02/2014 03 45	.		04/02/2014 03 45	0.418	04/02/2014 03 45	.	07/02/2014 19 00	.	.
04/02/2014 04 00	0.036712419	04/02/2014 04 00	.		04/02/2014 04 00	0.418	04/02/2014 04 00	.	07/02/2014 19 15	.	.
04/02/2014 04 15	0.035502593	04/02/2014 04 15	.		04/02/2014 04 15	0.418	04/02/2014 04 15	.	07/02/2014 19 30	.	.
04/02/2014 04 30	0.042297628	04/02/2014 04 30	.		04/02/2014 04 30	0.418	04/02/2014 04 30	.	07/02/2014 19 45	.	.
04/02/2014 04 45	0.032945821	04/02/2014 04 45	.		04/02/2014 04 45	0.418	04/02/2014 04 45	.	07/02/2014 20 00	.	.
04/02/2014 05 00	0.030815177	04/02/2014 05 00	.		04/02/2014 05 00	0.412	04/02/2014 05 00	.	07/02/2014 20 15	.	.
04/02/2014 05 15	0.039337752	04/02/2014 05 15	.		04/02/2014 05 15	0.412	04/02/2014 05 15	.	07/02/2014 20 30	.	.
04/02/2014 05 30	0.04022558	04/02/2014 05 30	.		04/02/2014 05 30	0.412	04/02/2014 05 30	.	07/02/2014 20 45	.	.
04/02/2014 05 45	0.031350195	04/02/2014 05 45	.		04/02/2014 05 45	0.412	04/02/2014 05 45	.	07/02/2014 21 00	.	.
04/02/2014 06 00	0.041493492	04/02/2014 06 00	.		04/02/2014 06 00	0.412	04/02/2014 06 00	.	07/02/2014 21 15	.	.
04/02/2014 06 15	0.031453909	04/02/2014 06 15	.		04/02/2014 06 15	0.412	04/02/2014 06 15	.	07/02/2014 21 30	.	.

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G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
04/02/2014 06 30	0.033130539	04/02/2014 06 30	.		04/02/2014 06 30	0.412	04/02/2014 06 30	.	07/02/2014 21 45	.	.
04/02/2014 06 45	0.032711381	04/02/2014 06 45	.		04/02/2014 06 45	0.406	04/02/2014 06 45	.	07/02/2014 22 00	.	.
04/02/2014 07 00	0.032711381	04/02/2014 07 00	.		04/02/2014 07 00	0.406	04/02/2014 07 00	.	07/02/2014 22 15	.	.
04/02/2014 07 15	0.034807169	04/02/2014 07 15	.		04/02/2014 07 15	0.406	04/02/2014 07 15	.	07/02/2014 22 30	.	.
04/02/2014 07 30	0.034388011	04/02/2014 07 30	.		04/02/2014 07 30	0.406	04/02/2014 07 30	.	07/02/2014 22 45	.	.
04/02/2014 07 45	0.038579585	04/02/2014 07 45	.		04/02/2014 07 45	0.406	04/02/2014 07 45	.	07/02/2014 23 00	.	.
04/02/2014 08 00	0.045297228	04/02/2014 08 00	.		04/02/2014 08 00	0.401	04/02/2014 08 00	.	07/02/2014 23 15	.	.
04/02/2014 08 15	0.042338767	04/02/2014 08 15	.		04/02/2014 08 15	0.401	04/02/2014 08 15	.	07/02/2014 23 30	.	.
04/02/2014 08 30	0.036712419	04/02/2014 08 30	.		04/02/2014 08 30	0.401	04/02/2014 08 30	.	07/02/2014 23 45	.	.
04/02/2014 08 45	0.040537078	04/02/2014 08 45	.		04/02/2014 08 45	0.401	04/02/2014 08 45	.	08/02/2014 00 00	.	.
04/02/2014 09 00	0.047037077	04/02/2014 09 00	.	0	04/02/2014 09 00	0.401	04/02/2014 09 00	.	08/02/2014 00 15	0.2	.
04/02/2014 09 15	0.047475476	04/02/2014 09 15	.		04/02/2014 09 15	0.395	04/02/2014 09 15	.	08/02/2014 00 30	.	.
04/02/2014 09 30	0.056084664	04/02/2014 09 30	.		04/02/2014 09 30	0.395	04/02/2014 09 30	.	08/02/2014 00 45	.	.
04/02/2014 09 45	0.041864102	04/02/2014 09 45	.		04/02/2014 09 45	0.395	04/02/2014 09 45	.	08/02/2014 01 00	.	.
04/02/2014 10 00	0.046019051	04/02/2014 10 00	.		04/02/2014 10 00	0.395	04/02/2014 10 00	.	08/02/2014 01 15	0.2	.
04/02/2014 10 15	0.057653678	04/02/2014 10 15	.		04/02/2014 10 15	0.389	04/02/2014 10 15	.	08/02/2014 01 30	.	.
04/02/2014 10 30	0.040394377	04/02/2014 10 30	.		04/02/2014 10 30	0.389	04/02/2014 10 30	.	08/02/2014 01 45	0.2	.
04/02/2014 10 45	0.047337856	04/02/2014 10 45	.		04/02/2014 10 45	0.389	04/02/2014 10 45	.	08/02/2014 02 00	0.2	0.2
04/02/2014 11 00	0.042179945	04/02/2014 11 00	.		04/02/2014 11 00	0.389	04/02/2014 11 00	.	08/02/2014 02 15	0.4	.
04/02/2014 11 15	0.042787424	04/02/2014 11 15	.		04/02/2014 11 15	0.389	04/02/2014 11 15	.	08/02/2014 02 30	0.4	0.2
04/02/2014 11 30	0.050635865	04/02/2014 11 30	.		04/02/2014 11 30	0.389	04/02/2014 11 30	.	08/02/2014 02 45	0.2	.
04/02/2014 11 45	0.045139173	04/02/2014 11 45	.		04/02/2014 11 45	0.383	04/02/2014 11 45	.	08/02/2014 03 00	.	0.2
04/02/2014 12 00	0.054790612	04/02/2014 12 00	.		04/02/2014 12 00	0.383	04/02/2014 12 00	.	08/02/2014 03 15	.	.
04/02/2014 12 15	0.047887519	04/02/2014 12 15	.		04/02/2014 12 15	0.383	04/02/2014 12 15	.	08/02/2014 03 30	.	.
04/02/2014 12 30	0.039463826	04/02/2014 12 30	.		04/02/2014 12 30	0.383	04/02/2014 12 30	.	08/02/2014 03 45	.	0.2
04/02/2014 12 45	0.029156011	04/02/2014 12 45	.		04/02/2014 12 45	0.378	04/02/2014 12 45	.	08/02/2014 04 00	0.2	.
04/02/2014 13 00	0.050044394	04/02/2014 13 00	.		04/02/2014 13 00	0.378	04/02/2014 13 00	.	08/02/2014 04 15	.	.
04/02/2014 13 15	0.049560881	04/02/2014 13 15	.		04/02/2014 13 15	0.378	04/02/2014 13 15	.	08/02/2014 04 30	.	.
04/02/2014 13 30	0.047679648	04/02/2014 13 30	.		04/02/2014 13 30	0.372	04/02/2014 13 30	.	08/02/2014 04 45	.	.
04/02/2014 13 45	0.038679708	04/02/2014 13 45	.		04/02/2014 13 45	0.372	04/02/2014 13 45	.	08/02/2014 05 00	.	.
04/02/2014 14 00	0.036901218	04/02/2014 14 00	.		04/02/2014 14 00	0.372	04/02/2014 14 00	.	08/02/2014 05 15	.	.
04/02/2014 14 15	0.04452445	04/02/2014 14 15	.		04/02/2014 14 15	0.372	04/02/2014 14 15	.	08/02/2014 05 30	.	.
04/02/2014 14 30	0.048789018	04/02/2014 14 30	.		04/02/2014 14 30	0.367	04/02/2014 14 30	.	08/02/2014 05 45	.	.
04/02/2014 14 45	0.035179259	04/02/2014 14 45	.		04/02/2014 14 45	0.367	04/02/2014 14 45	.	08/02/2014 06 00	.	.
04/02/2014 15 00	0.035633725	04/02/2014 15 00	.		04/02/2014 15 00	0.361	04/02/2014 15 00	.	08/02/2014 06 15	0.4	.
04/02/2014 15 15	0.041996239	04/02/2014 15 15	.		04/02/2014 15 15	0.361	04/02/2014 15 15	.	08/02/2014 06 30	1.4	.
04/02/2014 15 30	0.027453349	04/02/2014 15 30	.		04/02/2014 15 30	0.361	04/02/2014 15 30	.	08/02/2014 06 45	0.2	.
04/02/2014 15 45	0.042054542	04/02/2014 15 45	.		04/02/2014 15 45	0.361	04/02/2014 15 45	.	08/02/2014 07 00	0.2	.
04/02/2014 16 00	0.041603658	04/02/2014 16 00	.		04/02/2014 16 00	0.356	04/02/2014 16 00	.	08/02/2014 07 15	.	.
04/02/2014 16 15	0.04070189	04/02/2014 16 15	.		04/02/2014 16 15	0.356	04/02/2014 16 15	.	08/02/2014 07 30	.	.
04/02/2014 16 30	0.048370104	04/02/2014 16 30	.		04/02/2014 16 30	0.35	04/02/2014 16 30	.	08/02/2014 07 45	.	.
04/02/2014 16 45	0.038447469	04/02/2014 16 45	.		04/02/2014 16 45	0.35	04/02/2014 16 45	.	08/02/2014 08 00	.	.
04/02/2014 17 00	0.036292628	04/02/2014 17 00	.		04/02/2014 17 00	0.35	04/02/2014 17 00	.	08/02/2014 08 15	.	.
04/02/2014 17 15	0.031372174	04/02/2014 17 15	.		04/02/2014 17 15	0.345	04/02/2014 17 15	.	08/02/2014 08 30	.	0.2
04/02/2014 17 30	0.037718222	04/02/2014 17 30	.		04/02/2014 17 30	0.345	04/02/2014 17 30	.	08/02/2014 08 45	0.2	0.2
04/02/2014 17 45	0.036386957	04/02/2014 17 45	.		04/02/2014 17 45	0.345	04/02/2014 17 45	.	08/02/2014 09 00	.	0.2
04/02/2014 18 00	0.039049487	04/02/2014 18 00	.		04/02/2014 18 00	0.345	04/02/2014 18 00	.	08/02/2014 09 15	.	.
04/02/2014 18 15	0.043896965	04/02/2014 18 15	.		04/02/2014 18 15	0.339	04/02/2014 18 15	.	08/02/2014 09 30	.	.
04/02/2014 18 30	0.034056058	04/02/2014 18 30	.		04/02/2014 18 30	0.339	04/02/2014 18 30	.	08/02/2014 09 45	.	.
04/02/2014 18 45	0.038447469	04/02/2014 18 45	.		04/02/2014 18 45	0.339	04/02/2014 18 45	.	08/02/2014 10 00	.	.
04/02/2014 19 00	0.04070189	04/02/2014 19 00	.		04/02/2014 19 00	0.339	04/02/2014 19 00	.	08/02/2014 10 15	.	.
04/02/2014 19 15	0.056993595	04/02/2014 19 15	.		04/02/2014 19 15	0.339	04/02/2014 19 15	.	08/02/2014 10 30	.	.
04/02/2014 19 30	0.034603847	04/02/2014 19 30	.		04/02/2014 19 30	0.334	04/02/2014 19 30	.	08/02/2014 10 45	.	.
04/02/2014 19 45	0.045095729	04/02/2014 19 45	.		04/02/2014 19 45	0.334	04/02/2014 19 45	.	08/02/2014 11 00	.	.
04/02/2014 20 00	0.04737351	04/02/2014 20 00	.		04/02/2014 20 00	0.334	04/02/2014 20 00	.	08/02/2014 11 15	.	.
04/02/2014 20 15	0.051089064	04/02/2014 20 15	.		04/02/2014 20 15	0.334	04/02/2014 20 15	.	08/02/2014 11 30	.	.
04/02/2014 20 30	0.052026866	04/02/2014 20 30	.		04/02/2014 20 30	0.334	04/02/2014 20 30	.	08/02/2014 11 45	.	.
04/02/2014 20 45	0.031864123	04/02/2014 20 45	.		04/02/2014 20 45	0.328	04/02/2014 20 45	.	08/02/2014 12 00	.	.
04/02/2014 21 00	0.043651306	04/02/2014 21 00	.		04/02/2014 21 00	0.328	04/02/2014 21 00	.	08/02/2014 12 15	.	.
04/02/2014 21 15	0.039555796	04/02/2014 21 15	.		04/02/2014 21 15	0.328	04/02/2014 21 15	.	08/02/2014 12 30	.	.
04/02/2014 21 30	0.045512408	04/02/2014 21 30	.		04/02/2014 21 30	0.328	04/02/2014 21 30	.	08/02/2014 12 45	.	.
04/02/2014 21 45	0.038170813	04/02/2014 21 45	.		04/02/2014 21 45	0.328	04/02/2014 21 45	.	08/02/2014 13 00	.	.
04/02/2014 22 00	0.03062359	04/02/2014 22 00	.		04/02/2014 22 00	0.328	04/02/2014 22 00	.	08/02/2014 13 15	.	.
04/02/2014 22 15	0.039929101	04/02/2014 22 15	.		04/02/2014 22 15	0.328	04/02/2014 22 15	.	08/02/2014 13 30	.	.
04/02/2014 22 30	0.039463826	04/02/2014 22 30	.		04/02/2014 22 30	0.323	04/02/2014 22 30	.	08/02/2014 13 45	.	.
04/02/2014 22 45	0.038170813	04/02/2014 22 45	.		04/02/2014 22 45	0.323	04/02/2014 22 45	.	08/02/2014 14 00	.	.
04/02/2014 23 00	0.04971975	04/02/2014 23 00	.		04/02/2014 23 00	0.323	04/02/2014 23 00	.	08/02/2014 14 15	.	.
04/02/2014 23 15	0.044681116	04/02/2014 23 15	.		04/02/2014 23 15	0.323	04/02/2014 23 15	.	08/02/2014 14 30	.	.
04/02/2014 23 30	0.042390827	04/02/2014 23 30	.		04/02/2014 23 30	0.323	04/02/2014 23 30	.	08/02/2014 14 45	.	.
04/02/2014 23 45	0.043814101	04/02/2014 23 45	.		04/02/2014 23 45	0.323	04/02/2014 23 45	.	08/02/2014 15 00	.	.
05/02/2014 00 00	0.044723031	05/02/2014 00 00	.		05/02/2014 00 00	0.323	05/02/2014 00 00	.	08/02/2014 15 15	.	.
05/02/2014 00 15	0.034270329	05/02/2014 00 15	.		05/02/2014 00 15	0.318	05/02/2014 00 15	.	08/02/2014 15 30	.	.
05/02/2014 00 30	0.039349237	05/02/2014 00 30	.		05/02/2014 00 30	0.318	05/02/2014 00 30	.	08/02/2014 15 45	.	.
05/02/2014 00 45	0.037187255	05/02/2014 00 45	.		05/02/2014 00 45	0.323	05/02/2014 00 45	.	08/02/2014 16 00	.	.
05/02/2014 01 00	0.043487037	05/02/2014 01 00	.		05/02/2014 01 00	0.318	05/02/2014 01 00	.	08/02/2014 16 15	.	.

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
05/02/2014 01 15	0.037356484	05/02/2014 01 15	.		05/02/2014 01 15	0.318	05/02/2014 01 15	.	08/02/2014 16 30	.	.
05/02/2014 01 30	0.033066631	05/02/2014 01 30	.		05/02/2014 01 30	0.318	05/02/2014 01 30	.	08/02/2014 16 45	.	.
05/02/2014 01 45	0.039180021	05/02/2014 01 45	0.2		05/02/2014 01 45	0.318	05/02/2014 01 45	.	08/02/2014 17 00	.	.
05/02/2014 02 00	0.033503302	05/02/2014 02 00	0.2		05/02/2014 02 00	0.318	05/02/2014 02 00	.	08/02/2014 17 15	.	.
05/02/2014 02 15	0.031007879	05/02/2014 02 15	0.4		05/02/2014 02 15	0.318	05/02/2014 02 15	.	08/02/2014 17 30	.	.
05/02/2014 02 30	0.039670787	05/02/2014 02 30	0.2		05/02/2014 02 30	0.318	05/02/2014 02 30	.	08/02/2014 17 45	.	.
05/02/2014 02 45	0.042727259	05/02/2014 02 45	0.4		05/02/2014 02 45	0.323	05/02/2014 02 45	.	08/02/2014 18 00	.	.
05/02/2014 03 00	0.034993894	05/02/2014 03 00	0.4		05/02/2014 03 00	0.323	05/02/2014 03 00	.	08/02/2014 18 15	.	.
05/02/2014 03 15	0.043043282	05/02/2014 03 15	0.4		05/02/2014 03 15	0.323	05/02/2014 03 15	.	08/02/2014 18 30	.	.
05/02/2014 03 30	0.061813135	05/02/2014 03 30	0.4		05/02/2014 03 30	0.323	05/02/2014 03 30	0.2	08/02/2014 18 45	.	.
05/02/2014 03 45	0.077033056	05/02/2014 03 45	0.4		05/02/2014 03 45	0.328	05/02/2014 03 45	0.2	08/02/2014 19 00	.	.
05/02/2014 04 00	0.083215781	05/02/2014 04 00	0.4		05/02/2014 04 00	0.334	05/02/2014 04 00	0.2	08/02/2014 19 15	.	.
05/02/2014 04 15	0.090050164	05/02/2014 04 15	0.4		05/02/2014 04 15	0.339	05/02/2014 04 15	0.4	08/02/2014 19 30	.	.
05/02/2014 04 30	0.112510042	05/02/2014 04 30	0.4		05/02/2014 04 30	0.344	05/02/2014 04 30	0.2	08/02/2014 19 45	.	.
05/02/2014 04 45	0.107020724	05/02/2014 04 45	0.2		05/02/2014 04 45	0.35	05/02/2014 04 45	0.4	08/02/2014 20 00	.	.
05/02/2014 05 00	0.107808346	05/02/2014 05 00	.		05/02/2014 05 00	0.355	05/02/2014 05 00	.	08/02/2014 20 15	.	.
05/02/2014 05 15	0.087510693	05/02/2014 05 15	.		05/02/2014 05 15	0.361	05/02/2014 05 15	.	08/02/2014 20 30	.	.
05/02/2014 05 30	0.10834168	05/02/2014 05 30	.		05/02/2014 05 30	0.366	05/02/2014 05 30	.	08/02/2014 20 45	.	.
05/02/2014 05 45	0.101178844	05/02/2014 05 45	.		05/02/2014 05 45	0.372	05/02/2014 05 45	.	08/02/2014 21 00	.	.
05/02/2014 06 00	0.106799989	05/02/2014 06 00	.		05/02/2014 06 00	0.383	05/02/2014 06 00	.	08/02/2014 21 15	.	.
05/02/2014 06 15	0.079936423	05/02/2014 06 15	.		05/02/2014 06 15	0.395	05/02/2014 06 15	.	08/02/2014 21 30	.	.
05/02/2014 06 30	0.068385308	05/02/2014 06 30	.		05/02/2014 06 30	0.406	05/02/2014 06 30	.	08/02/2014 21 45	.	.
05/02/2014 06 45	0.065598003	05/02/2014 06 45	.		05/02/2014 06 45	0.412	05/02/2014 06 45	.	08/02/2014 22 00	.	.
05/02/2014 07 00	0.061118433	05/02/2014 07 00	.		05/02/2014 07 00	0.424	05/02/2014 07 00	.	08/02/2014 22 15	.	.
05/02/2014 07 15	0.06170502	05/02/2014 07 15	.		05/02/2014 07 15	0.43	05/02/2014 07 15	.	08/02/2014 22 30	.	.
05/02/2014 07 30	0.074592614	05/02/2014 07 30	.		05/02/2014 07 30	0.442	05/02/2014 07 30	.	08/02/2014 22 45	.	.
05/02/2014 07 45	0.078765073	05/02/2014 07 45	.		05/02/2014 07 45	0.454	05/02/2014 07 45	.	08/02/2014 23 00	.	.
05/02/2014 08 00	0.086047917	05/02/2014 08 00	.		05/02/2014 08 00	0.472	05/02/2014 08 00	0.4	08/02/2014 23 15	.	.
05/02/2014 08 15	0.073950351	05/02/2014 08 15	.		05/02/2014 08 15	0.491	05/02/2014 08 15	1	08/02/2014 23 30	.	.
05/02/2014 08 30	0.074575551	05/02/2014 08 30	.		05/02/2014 08 30	0.516	05/02/2014 08 30	.	08/02/2014 23 45	.	.
05/02/2014 08 45	0.167259827	05/02/2014 08 45	.		05/02/2014 08 45	0.548	05/02/2014 08 45	.	09/02/2014 00 00	.	.
05/02/2014 09 00	0.140364973	05/02/2014 09 00	.	4.4	05/02/2014 09 00	0.582	05/02/2014 09 00	.	09/02/2014 00 15	.	.
05/02/2014 09 15	0.116397062	05/02/2014 09 15	0.2		05/02/2014 09 15	0.615	05/02/2014 09 15	.	09/02/2014 00 30	.	.
05/02/2014 09 30	0.114131873	05/02/2014 09 30	.		05/02/2014 09 30	0.65	05/02/2014 09 30	.	09/02/2014 00 45	.	.
05/02/2014 09 45	0.092909524	05/02/2014 09 45	.		05/02/2014 09 45	0.693	05/02/2014 09 45	.	09/02/2014 01 00	.	.
05/02/2014 10 00	0.109457049	05/02/2014 10 00	.		05/02/2014 10 00	0.737	05/02/2014 10 00	.	09/02/2014 01 15	.	.
05/02/2014 10 15	0.086493605	05/02/2014 10 15	.		05/02/2014 10 15	0.781	05/02/2014 10 15	.	09/02/2014 01 30	.	.
05/02/2014 10 30	0.083353666	05/02/2014 10 30	.		05/02/2014 10 30	0.827	05/02/2014 10 30	.	09/02/2014 01 45	.	.
05/02/2014 10 45	0.081539433	05/02/2014 10 45	.		05/02/2014 10 45	0.874	05/02/2014 10 45	.	09/02/2014 02 00	.	.
05/02/2014 11 00	0.078451889	05/02/2014 11 00	.		05/02/2014 11 00	0.922	05/02/2014 11 00	.	09/02/2014 02 15	.	.
05/02/2014 11 15	0.085590806	05/02/2014 11 15	.		05/02/2014 11 15	0.963	05/02/2014 11 15	.	09/02/2014 02 30	.	.
05/02/2014 11 30	0.079309768	05/02/2014 11 30	.		05/02/2014 11 30	0.996	05/02/2014 11 30	.	09/02/2014 02 45	.	.
05/02/2014 11 45	0.0762215	05/02/2014 11 45	.		05/02/2014 11 45	1.02	05/02/2014 11 45	.	09/02/2014 03 00	.	.
05/02/2014 12 00	0.074405036	05/02/2014 12 00	.		05/02/2014 12 00	1.05	05/02/2014 12 00	.	09/02/2014 03 15	.	.
05/02/2014 12 15	0.070885489	05/02/2014 12 15	.		05/02/2014 12 15	1.07	05/02/2014 12 15	.	09/02/2014 03 30	.	.
05/02/2014 12 30	0.081802437	05/02/2014 12 30	.		05/02/2014 12 30	1.09	05/02/2014 12 30	.	09/02/2014 03 45	.	.
05/02/2014 12 45	0.090899894	05/02/2014 12 45	.		05/02/2014 12 45	1.1	05/02/2014 12 45	.	09/02/2014 04 00	.	.
05/02/2014 13 00	0.081802437	05/02/2014 13 00	.		05/02/2014 13 00	1.11	05/02/2014 13 00	.	09/02/2014 04 15	.	.
05/02/2014 13 15	0.066117914	05/02/2014 13 15	.		05/02/2014 13 15	1.12	05/02/2014 13 15	.	09/02/2014 04 30	.	.
05/02/2014 13 30	0.073347856	05/02/2014 13 30	.		05/02/2014 13 30	1.12	05/02/2014 13 30	.	09/02/2014 04 45	.	.
05/02/2014 13 45	0.071540371	05/02/2014 13 45	.		05/02/2014 13 45	1.12	05/02/2014 13 45	.	09/02/2014 05 00	.	.
05/02/2014 14 00	0.075174054	05/02/2014 14 00	.		05/02/2014 14 00	1.12	05/02/2014 14 00	.	09/02/2014 05 15	.	.
05/02/2014 14 15	0.080537826	05/02/2014 14 15	.		05/02/2014 14 15	1.12	05/02/2014 14 15	.	09/02/2014 05 30	.	.
05/02/2014 14 30	0.081159086	05/02/2014 14 30	.		05/02/2014 14 30	1.12	05/02/2014 14 30	.	09/02/2014 05 45	.	.
05/02/2014 14 45	0.060324107	05/02/2014 14 45	.		05/02/2014 14 45	1.11	05/02/2014 14 45	.	09/02/2014 06 00	.	.
05/02/2014 15 00	0.060324107	05/02/2014 15 00	0.4		05/02/2014 15 00	1.11	05/02/2014 15 00	0.4	09/02/2014 06 15	.	.
05/02/2014 15 15	0.069241924	05/02/2014 15 15	0.6		05/02/2014 15 15	1.11	05/02/2014 15 15	0.2	09/02/2014 06 30	.	0.2
05/02/2014 15 30	0.073998093	05/02/2014 15 30	0.2		05/02/2014 15 30	1.1	05/02/2014 15 30	0.2	09/02/2014 06 45	.	.
05/02/2014 15 45	0.066720409	05/02/2014 15 45	.		05/02/2014 15 45	1.09	05/02/2014 15 45	.	09/02/2014 07 00	.	.
05/02/2014 16 00	0.066196506	05/02/2014 16 00	0.2		05/02/2014 16 00	1.09	05/02/2014 16 00	0.2	09/02/2014 07 15	.	.
05/02/2014 16 15	0.070763411	05/02/2014 16 15	.		05/02/2014 16 15	1.09	05/02/2014 16 15	.	09/02/2014 07 30	.	.
05/02/2014 16 30	0.089370707	05/02/2014 16 30	.		05/02/2014 16 30	1.08	05/02/2014 16 30	.	09/02/2014 07 45	.	.
05/02/2014 16 45	0.094349489	05/02/2014 16 45	.		05/02/2014 16 45	1.07	05/02/2014 16 45	.	09/02/2014 08 00	.	.
05/02/2014 17 00	0.082432831	05/02/2014 17 00	.		05/02/2014 17 00	1.06	05/02/2014 17 00	.	09/02/2014 08 15	.	.
05/02/2014 17 15	0.081171398	05/02/2014 17 15	.		05/02/2014 17 15	1.06	05/02/2014 17 15	.	09/02/2014 08 30	.	.
05/02/2014 17 30	0.094976144	05/02/2014 17 30	.		05/02/2014 17 30	1.06	05/02/2014 17 30	.	09/02/2014 08 45	.	.
05/02/2014 17 45	0.093580468	05/02/2014 17 45	.		05/02/2014 17 45	1.06	05/02/2014 17 45	.	09/02/2014 09 00	.	.
05/02/2014 18 00	0.076294188	05/02/2014 18 00	.		05/02/2014 18 00	1.05	05/02/2014 18 00	.	09/02/2014 09 15	.	.
05/02/2014 18 15	0.084258541	05/02/2014 18 15	.		05/02/2014 18 15	1.04	05/02/2014 18 15	.	09/02/2014 09 30	.	.
05/02/2014 18 30	0.083037524	05/02/2014 18 30	.		05/02/2014 18 30	1.04	05/02/2014 18 30	.	09/02/2014 09 45	.	.
05/02/2014 18 45	0.075737466	05/02/2014 18 45	.		05/02/2014 18 45	1.03	05/02/2014 18 45	.	09/02/2014 10 00	.	.
05/02/2014 19 00	0.07695046	05/02/2014 19 00	.		05/02/2014 19 00	1.03	05/02/2014 19 00	.	09/02/2014 10 15	.	.
05/02/2014 19 15	0.081782788	05/02/2014 19 15	.		05/02/2014 19 15	1.02	05/02/2014 19 15	.	09/02/2014 10 30	.	.
05/02/2014 19 30	0.086000254	05/02/2014 19 30	.		05/02/2014 19 30	1.02	05/02/2014 19 30	.	09/02/2014 10 45	.	.
05/02/2014 19 45	0.082987779	05/02/2014 19 45	.		05/02/2014 19 45	1.01	05/02/2014 19 45	.	09/02/2014 11 00	.	.

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG		Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
05/02/2014 20 00	0.073950351	05/02/2014 20 00	.		05/02/2014 20 00	1.01	05/02/2014 20 00	.	09/02/2014 11 15	.	.
05/02/2014 20 15	0.082987779	05/02/2014 20 15	.		05/02/2014 20 15	1.01	05/02/2014 20 15	.	09/02/2014 11 30	.	.
05/02/2014 20 30	0.084795264	05/02/2014 20 30	.		05/02/2014 20 30	1.01	05/02/2014 20 30	.	09/02/2014 11 45	.	.
05/02/2014 20 45	0.08774262	05/02/2014 20 45	.		05/02/2014 20 45	1.01	05/02/2014 20 45	.	09/02/2014 12 00	.	.
05/02/2014 21 00	0.081180293	05/02/2014 21 00	.		05/02/2014 21 00	1.01	05/02/2014 21 00	.	09/02/2014 12 15	.	.
05/02/2014 21 15	0.073977048	05/02/2014 21 15	.		05/02/2014 21 15	1.01	05/02/2014 21 15	.	09/02/2014 12 30	.	.
05/02/2014 21 30	0.083510432	05/02/2014 21 30	.		05/02/2014 21 30	1.01	05/02/2014 21 30	.	09/02/2014 12 45	.	.
05/02/2014 21 45	0.0858245	05/02/2014 21 45	.		05/02/2014 21 45	1.01	05/02/2014 21 45	.	09/02/2014 13 00	.	.
05/02/2014 22 00	0.061021437	05/02/2014 22 00	.		05/02/2014 22 00	1	05/02/2014 22 00	.	09/02/2014 13 15	.	.
05/02/2014 22 15	0.075194616	05/02/2014 22 15	.		05/02/2014 22 15	1.01	05/02/2014 22 15	.	09/02/2014 13 30	.	.
05/02/2014 22 30	0.085233951	05/02/2014 22 30	.		05/02/2014 22 30	1	05/02/2014 22 30	.	09/02/2014 13 45	.	.
05/02/2014 22 45	0.068157479	05/02/2014 22 45	.		05/02/2014 22 45	1	05/02/2014 22 45	.	09/02/2014 14 00	.	.
05/02/2014 23 00	0.071060772	05/02/2014 23 00	.		05/02/2014 23 00	1	05/02/2014 23 00	.	09/02/2014 14 15	.	.
05/02/2014 23 15	0.091034377	05/02/2014 23 15	.		05/02/2014 23 15	1	05/02/2014 23 15	.	09/02/2014 14 30	.	.
05/02/2014 23 30	0.089274616	05/02/2014 23 30	.		05/02/2014 23 30	1	05/02/2014 23 30	.	09/02/2014 14 45	.	.
05/02/2014 23 45	0.079271337	05/02/2014 23 45	.		05/02/2014 23 45	1	05/02/2014 23 45	.	09/02/2014 15 00	.	.
06/02/2014 00 00	0.066453363	06/02/2014 00 00	.		06/02/2014 00 00	0.996	06/02/2014 00 00	.	09/02/2014 15 15	.	.
06/02/2014 00 15	0.082184514	06/02/2014 00 15	.		06/02/2014 00 15	0.996	06/02/2014 00 15	.	09/02/2014 15 30	.	.
06/02/2014 00 30	0.078655906	06/02/2014 00 30	.		06/02/2014 00 30	0.988	06/02/2014 00 30	.	09/02/2014 15 45	.	.
06/02/2014 00 45	0.064188571	06/02/2014 00 45	.		06/02/2014 00 45	0.988	06/02/2014 00 45	.	09/02/2014 16 00	.	.
06/02/2014 01 00	0.060225314	06/02/2014 01 00	.		06/02/2014 01 00	0.988	06/02/2014 01 00	.	09/02/2014 16 15	.	.
06/02/2014 01 15	0.066015595	06/02/2014 01 15	.		06/02/2014 01 15	0.979	06/02/2014 01 15	.	09/02/2014 16 30	.	.
06/02/2014 01 30	0.072294836	06/02/2014 01 30	.		06/02/2014 01 30	0.979	06/02/2014 01 30	.	09/02/2014 16 45	.	.
06/02/2014 01 45	0.066052675	06/02/2014 01 45	.		06/02/2014 01 45	0.971	06/02/2014 01 45	.	09/02/2014 17 00	.	.
06/02/2014 02 00	0.078470805	06/02/2014 02 00	.		06/02/2014 02 00	0.963	06/02/2014 02 00	.	09/02/2014 17 15	.	.
06/02/2014 02 15	0.067796469	06/02/2014 02 15	.		06/02/2014 02 15	0.955	06/02/2014 02 15	.	09/02/2014 17 30	.	.
06/02/2014 02 30	0.061227614	06/02/2014 02 30	.		06/02/2014 02 30	0.955	06/02/2014 02 30	0.2	09/02/2014 17 45	.	.
06/02/2014 02 45	0.053367474	06/02/2014 02 45	.		06/02/2014 02 45	0.947	06/02/2014 02 45	.	09/02/2014 18 00	.	.
06/02/2014 03 00	0.050449042	06/02/2014 03 00	.		06/02/2014 03 00	0.938	06/02/2014 03 00	.	09/02/2014 18 15	.	.
06/02/2014 03 15	0.064975713	06/02/2014 03 15	.		06/02/2014 03 15	0.93	06/02/2014 03 15	.	09/02/2014 18 30	.	.
06/02/2014 03 30	0.046186572	06/02/2014 03 30	.		06/02/2014 03 30	0.922	06/02/2014 03 30	.	09/02/2014 18 45	.	.
06/02/2014 03 45	0.046365915	06/02/2014 03 45	.		06/02/2014 03 45	0.922	06/02/2014 03 45	.	09/02/2014 19 00	.	.
06/02/2014 04 00	0.055844555	06/02/2014 04 00	.		06/02/2014 04 00	0.914	06/02/2014 04 00	.	09/02/2014 19 15	.	.
06/02/2014 04 15	0.048487111	06/02/2014 04 15	.		06/02/2014 04 15	0.906	06/02/2014 04 15	.	09/02/2014 19 30	.	.
06/02/2014 04 30	0.056813567	06/02/2014 04 30	.		06/02/2014 04 30	0.898	06/02/2014 04 30	.	09/02/2014 19 45	.	.
06/02/2014 04 45	0.06248895	06/02/2014 04 45	.		06/02/2014 04 45	0.89	06/02/2014 04 45	.	09/02/2014 20 00	.	.
06/02/2014 05 00	0.050132266	06/02/2014 05 00	.		06/02/2014 05 00	0.882	06/02/2014 05 00	.	09/02/2014 20 15	.	.
06/02/2014 05 15	0.050151262	06/02/2014 05 15	.		06/02/2014 05 15	0.874	06/02/2014 05 15	.	09/02/2014 20 30	.	.
06/02/2014 05 30	0.045047132	06/02/2014 05 30	.		06/02/2014 05 30	0.866	06/02/2014 05 30	.	09/02/2014 20 45	.	.
06/02/2014 05 45	0.046442959	06/02/2014 05 45	.		06/02/2014 05 45	0.858	06/02/2014 05 45	.	09/02/2014 21 00	.	.
06/02/2014 06 00	0.050635865	06/02/2014 06 00	.		06/02/2014 06 00	0.858	06/02/2014 06 00	.	09/02/2014 21 15	.	.
06/02/2014 06 15	0.048358754	06/02/2014 06 15	.		06/02/2014 06 15	0.85	06/02/2014 06 15	.	09/02/2014 21 30	.	.
06/02/2014 06 30	0.047449823	06/02/2014 06 30	.		06/02/2014 06 30	0.843	06/02/2014 06 30	.	09/02/2014 21 45	.	.
06/02/2014 06 45	0.042505426	06/02/2014 06 45	.		06/02/2014 06 45	0.835	06/02/2014 06 45	.	09/02/2014 22 00	.	.
06/02/2014 07 00	0.047465151	06/02/2014 07 00	.		06/02/2014 07 00	0.827	06/02/2014 07 00	.	09/02/2014 22 15	.	.
06/02/2014 07 15	0.046563383	06/02/2014 07 15	.		06/02/2014 07 15	0.819	06/02/2014 07 15	.	09/02/2014 22 30	.	.
06/02/2014 07 30	0.041152774	06/02/2014 07 30	.		06/02/2014 07 30	0.819	06/02/2014 07 30	.	09/02/2014 22 45	.	.
06/02/2014 07 45	0.048817803	06/02/2014 07 45	.		06/02/2014 07 45	0.812	06/02/2014 07 45	.	09/02/2014 23 00	.	.
06/02/2014 08 00	0.053326644	06/02/2014 08 00	.		06/02/2014 08 00	0.804	06/02/2014 08 00	.	09/02/2014 23 15	.	.
06/02/2014 08 15	0.054266803	06/02/2014 08 15	.		06/02/2014 08 15	0.796	06/02/2014 08 15	.	09/02/2014 23 30	.	.
06/02/2014 08 30	0.052468096	06/02/2014 08 30	.		06/02/2014 08 30	0.789	06/02/2014 08 30	.	09/02/2014 23 45	.	.
06/02/2014 08 45	0.057653678	06/02/2014 08 45	.		06/02/2014 08 45	0.789	06/02/2014 08 45	.	10/02/2014 00 00	.	.
06/02/2014 09 00	0.064780927	06/02/2014 09 00	.	1.6	06/02/2014 09 00	0.781	06/02/2014 09 00	.	10/02/2014 00 15	.	.
06/02/2014 09 15	0.057297079	06/02/2014 09 15	.		06/02/2014 09 15	0.774	06/02/2014 09 15	.	10/02/2014 00 30	.	.
06/02/2014 09 30	0.063646091	06/02/2014 09 30	.		06/02/2014 09 30	0.766	06/02/2014 09 30	.	10/02/2014 00 45	.	.
06/02/2014 09 45	0.060759193	06/02/2014 09 45	.		06/02/2014 09 45	0.766	06/02/2014 09 45	.	10/02/2014 01 00	.	.
06/02/2014 10 00	0.06227416	06/02/2014 10 00	.		06/02/2014 10 00	0.759	06/02/2014 10 00	.	10/02/2014 01 15	.	.
06/02/2014 10 15	0.052414177	06/02/2014 10 15	.		06/02/2014 10 15	0.751	06/02/2014 10 15	.	10/02/2014 01 30	.	.
06/02/2014 10 30	0.050898706	06/02/2014 10 30	.		06/02/2014 10 30	0.751	06/02/2014 10 30	.	10/02/2014 01 45	.	.
06/02/2014 10 45	0.061779575	06/02/2014 10 45	.		06/02/2014 10 45	0.744	06/02/2014 10 45	.	10/02/2014 02 00	.	.
06/02/2014 11 00	0.057813894	06/02/2014 11 00	.		06/02/2014 11 00	0.744	06/02/2014 11 00	.	10/02/2014 02 15	.	.
06/02/2014 11 15	0.049468878	06/02/2014 11 15	.		06/02/2014 11 15	0.736	06/02/2014 11 15	.	10/02/2014 02 30	.	.
06/02/2014 11 30	0.048977994	06/02/2014 11 30	.		06/02/2014 11 30	0.729	06/02/2014 11 30	.	10/02/2014 02 45	0.2	.
06/02/2014 11 45	0.060759193	06/02/2014 11 45	.		06/02/2014 11 45	0.722	06/02/2014 11 45	.	10/02/2014 03 00	.	.
06/02/2014 12 00	0.05536382	06/02/2014 12 00	.		06/02/2014 12 00	0.722	06/02/2014 12 00	.	10/02/2014 03 15	.	.
06/02/2014 12 15	0.054879517	06/02/2014 12 15	.		06/02/2014 12 15	0.714	06/02/2014 12 15	.	10/02/2014 03 30	.	.
06/02/2014 12 30	0.052945468	06/02/2014 12 30	.		06/02/2014 12 30	0.714	06/02/2014 12 30	.	10/02/2014 03 45	.	.
06/02/2014 12 45	0.044800589	06/02/2014 12 45	.		06/02/2014 12 45	0.707	06/02/2014 12 45	.	10/02/2014 04 00	.	.
06/02/2014 13 00	0.051518393	06/02/2014 13 00	.		06/02/2014 13 00	0.7	06/02/2014 13 00	.	10/02/2014 04 15	.	.
06/02/2014 13 15	0.050584329	06/02/2014 13 15	.		06/02/2014 13 15	0.7	06/02/2014 13 15	.	10/02/2014 04 30	.	.
06/02/2014 13 30	0.052489068	06/02/2014 13 30		0.2	06/02/2014 13 30	0.692	06/02/2014 13 30	.	10/02/2014 04 45	.	.
06/02/2014 13 45	0.053917623	06/02/2014 13 45		0.2	06/02/2014 13 45	0.692	06/02/2014 13 45	0.2	10/02/2014 05 00	.	.
06/02/2014 14 00	0.046298665	06/02/2014 14 00	.		06/02/2014 14 00	0.685	06/02/2014 14 00	0.2	10/02/2014 05 15	.	.
06/02/2014 14 15	0.042013002	06/02/2014 14 15		0.2	06/02/2014 14 15	0.685	06/02/2014 14 15	.	10/02/2014 05 30	.	.
06/02/2014 14 30	0.050132266	06/02/2014 14 30		0.2	06/02/2014 14 30	0.678	06/02/2014 14 30	0.2	10/02/2014 05 45	.	.

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
06/02/2014 14 45	0.043989279	06/02/2014 14 45	0.4		06/02/2014 14 45	0.678	06/02/2014 14 45	0.4	10/02/2014 06 00	.	.
06/02/2014 15 00	0.061060395	06/02/2014 15 00	0.2		06/02/2014 15 00	0.671	06/02/2014 15 00	0.2			
06/02/2014 15 15	0.050527906	06/02/2014 15 15	0.4		06/02/2014 15 15	0.671	06/02/2014 15 15	0.4			
06/02/2014 15 30	0.066978155	06/02/2014 15 30	0.4		06/02/2014 15 30	0.671	06/02/2014 15 30	0.4			
06/02/2014 15 45	0.090561962	06/02/2014 15 45	0.4		06/02/2014 15 45	0.664	06/02/2014 15 45	0.2			
06/02/2014 16 00	0.091239206	06/02/2014 16 00	0.4		06/02/2014 16 00	0.664	06/02/2014 16 00	0.4			
06/02/2014 16 15	0.100503048	06/02/2014 16 15	0.2		06/02/2014 16 15	0.664	06/02/2014 16 15	0.4			
06/02/2014 16 30	0.113392989	06/02/2014 16 30	0.6		06/02/2014 16 30	0.664	06/02/2014 16 30	0.6			
06/02/2014 16 45	0.124144051	06/02/2014 16 45	0.6		06/02/2014 16 45	0.664	06/02/2014 16 45	0.6			
06/02/2014 17 00	0.108651567	06/02/2014 17 00	0.4		06/02/2014 17 00	0.671	06/02/2014 17 00	0.4			
06/02/2014 17 15	0.133322114	06/02/2014 17 15	0.6		06/02/2014 17 15	0.671	06/02/2014 17 15	0.4			
06/02/2014 17 30	0.14338703	06/02/2014 17 30	0.6		06/02/2014 17 30	0.678	06/02/2014 17 30	0.4			
06/02/2014 17 45	0.115505181	06/02/2014 17 45	0.6		06/02/2014 17 45	0.685	06/02/2014 17 45	0.4			
06/02/2014 18 00	0.173601744	06/02/2014 18 00	0.6		06/02/2014 18 00	0.7	06/02/2014 18 00	0.8			
06/02/2014 18 15	0.162760521	06/02/2014 18 15	0.4		06/02/2014 18 15	0.714	06/02/2014 18 15	0.6			
06/02/2014 18 30	0.1550522	06/02/2014 18 30	0.6		06/02/2014 18 30	0.729	06/02/2014 18 30	0.6			
06/02/2014 18 45	0.146158445	06/02/2014 18 45	0.6		06/02/2014 18 45	0.751	06/02/2014 18 45	0.6			
06/02/2014 19 00	0.176820774	06/02/2014 19 00	0.2		06/02/2014 19 00	0.789	06/02/2014 19 00	0.2			
06/02/2014 19 15	0.178406363	06/02/2014 19 15	0.6		06/02/2014 19 15	0.835	06/02/2014 19 15	0.4			
06/02/2014 19 30	0.198132672	06/02/2014 19 30	0.2		06/02/2014 19 30	0.89	06/02/2014 19 30	.			
06/02/2014 19 45	0.273054415	06/02/2014 19 45	.		06/02/2014 19 45	0.971	06/02/2014 19 45	0.2			
06/02/2014 20 00	0.349087878	06/02/2014 20 00	0.2		06/02/2014 20 00	1.07	06/02/2014 20 00	.			
06/02/2014 20 15	0.250491221	06/02/2014 20 15	.		06/02/2014 20 15	1.2	06/02/2014 20 15	0.2			
06/02/2014 20 30	0.30721861	06/02/2014 20 30	.		06/02/2014 20 30	---	06/02/2014 20 30	.			
06/02/2014 20 45	0.28599309	06/02/2014 20 45	.		06/02/2014 20 45	---	06/02/2014 20 45	.			
06/02/2014 21 00	0.31434567	06/02/2014 21 00	.		06/02/2014 21 00	---	06/02/2014 21 00	.			
06/02/2014 21 15	0.24794263	06/02/2014 21 15	.		06/02/2014 21 15	---	06/02/2014 21 15	.			
06/02/2014 21 30	0.308877416	06/02/2014 21 30	.		06/02/2014 21 30	---	06/02/2014 21 30	.			
06/02/2014 21 45	0.342486785	06/02/2014 21 45	.		06/02/2014 21 45	---	06/02/2014 21 45	.			
06/02/2014 22 00	0.246754971	06/02/2014 22 00	.		06/02/2014 22 00	---	06/02/2014 22 00	.			
06/02/2014 22 15	0.281544916	06/02/2014 22 15	.		06/02/2014 22 15	---	06/02/2014 22 15	.			
06/02/2014 22 30	0.30624849	06/02/2014 22 30	.		06/02/2014 22 30	---	06/02/2014 22 30	.			
06/02/2014 22 45	0.226961127	06/02/2014 22 45	.		06/02/2014 22 45	---	06/02/2014 22 45	.			
06/02/2014 23 00	0.272072902	06/02/2014 23 00	.		06/02/2014 23 00	---	06/02/2014 23 00	.			
06/02/2014 23 15	0.288406427	06/02/2014 23 15	0.2		06/02/2014 23 15	---	06/02/2014 23 15	.			
06/02/2014 23 30	0.328277813	06/02/2014 23 30	.		06/02/2014 23 30	---	06/02/2014 23 30	0.2			
06/02/2014 23 45	0.268712432	06/02/2014 23 45	0.2		06/02/2014 23 45	---	06/02/2014 23 45	0.2			
07/02/2014 00 00	0.282339076	07/02/2014 00 00	.		07/02/2014 00 00	---	07/02/2014 00 00	.			
07/02/2014 00 15	0.299048731	07/02/2014 00 15	.		07/02/2014 00 15	---	07/02/2014 00 15	.			
07/02/2014 00 30	0.294629159	07/02/2014 00 30	0.2		07/02/2014 00 30	---	07/02/2014 00 30	.			
07/02/2014 00 45	0.301613912	07/02/2014 00 45	.		07/02/2014 00 45	---	07/02/2014 00 45	.			
07/02/2014 01 00	0.328596351	07/02/2014 01 00	.		07/02/2014 01 00	---	07/02/2014 01 00	.			
07/02/2014 01 15	0.32424134	07/02/2014 01 15	.		07/02/2014 01 15	---	07/02/2014 01 15	.			
07/02/2014 01 30	0.294936299	07/02/2014 01 30	.		07/02/2014 01 30	---	07/02/2014 01 30	.			
07/02/2014 01 45	0.303388263	07/02/2014 01 45	.		07/02/2014 01 45	---	07/02/2014 01 45	.			
07/02/2014 02 00	0.325412982	07/02/2014 02 00	.		07/02/2014 02 00	---	07/02/2014 02 00	.			
07/02/2014 02 15	0.301755673	07/02/2014 02 15	.		07/02/2014 02 15	---	07/02/2014 02 15	.			
07/02/2014 02 30	0.294761416	07/02/2014 02 30	.		07/02/2014 02 30	---	07/02/2014 02 30	0.2			
07/02/2014 02 45	0.212793044	07/02/2014 02 45	.		07/02/2014 02 45	---	07/02/2014 02 45	.			
07/02/2014 03 00	0.292964491	07/02/2014 03 00	.		07/02/2014 03 00	---	07/02/2014 03 00	.			
07/02/2014 03 15	0.231652031	07/02/2014 03 15	.		07/02/2014 03 15	---	07/02/2014 03 15	0.2			
07/02/2014 03 30	0.258781519	07/02/2014 03 30	.		07/02/2014 03 30	---	07/02/2014 03 30	0.2			
07/02/2014 03 45	0.249755374	07/02/2014 03 45	0.2		07/02/2014 03 45	---	07/02/2014 03 45	0.6			
07/02/2014 04 00	0.321285748	07/02/2014 04 00	0.4		07/02/2014 04 00	---	07/02/2014 04 00	0.4			
07/02/2014 04 15	0.23026635	07/02/2014 04 15	0.2		07/02/2014 04 15	---	07/02/2014 04 15	0.2			
07/02/2014 04 30	0.276284335	07/02/2014 04 30	.		07/02/2014 04 30	---	07/02/2014 04 30	.			
07/02/2014 04 45	0.267664	07/02/2014 04 45	.		07/02/2014 04 45	---	07/02/2014 04 45	.			
07/02/2014 05 00	0.295087729	07/02/2014 05 00	0.2		07/02/2014 05 00	---	07/02/2014 05 00	.			
07/02/2014 05 15	0.246754971	07/02/2014 05 15	.		07/02/2014 05 15	---	07/02/2014 05 15	.			
07/02/2014 05 30	0.285743137	07/02/2014 05 30	0.2		07/02/2014 05 30	---	07/02/2014 05 30	.			
07/02/2014 05 45	0.21061572	07/02/2014 05 45	0.2		07/02/2014 05 45	---	07/02/2014 05 45	.			
07/02/2014 06 00	0.235544158	07/02/2014 06 00	1.4		07/02/2014 06 00	---	07/02/2014 06 00	0.2			
07/02/2014 06 15	0.248004694	07/02/2014 06 15	0.6		07/02/2014 06 15	---	07/02/2014 06 15	0.2			
07/02/2014 06 30	0.280535099	07/02/2014 06 30	2.4		07/02/2014 06 30	---	07/02/2014 06 30	0.4			
07/02/2014 06 45	0.361815286	07/02/2014 06 45	1.6		07/02/2014 06 45	---	07/02/2014 06 45	0.2			
07/02/2014 07 00	0.239605509	07/02/2014 07 00	0.6		07/02/2014 07 00	---	07/02/2014 07 00	1.6			
07/02/2014 07 15	0.754985812	07/02/2014 07 15	0.4		07/02/2014 07 15	---	07/02/2014 07 15	0.2			
07/02/2014 07 30	0.814109528	07/02/2014 07 30	0.4		07/02/2014 07 30	---	07/02/2014 07 30	0.4			
07/02/2014 07 45	0.757228335	07/02/2014 07 45	0.6		07/02/2014 07 45	---	07/02/2014 07 45	0.4			
07/02/2014 08 00	0.720623719	07/02/2014 08 00	0.2		07/02/2014 08 00	---	07/02/2014 08 00	0.4			
07/02/2014 08 15	0.764158797	07/02/2014 08 15	0.2		07/02/2014 08 15	---	07/02/2014 08 15	0.2			
07/02/2014 08 30	0.643594692	07/02/2014 08 30	.		07/02/2014 08 30	---	07/02/2014 08 30	.			
07/02/2014 08 45	0.733301621	07/02/2014 08 45	.		07/02/2014 08 45	---	07/02/2014 08 45	.			
07/02/2014 09 00	0.604187601	07/02/2014 09 00	.		07/02/2014 09 00	---	07/02/2014 09 00	.			
07/02/2014 09 15	0.555253279	07/02/2014 09 15	.		07/02/2014 09 15	---	07/02/2014 09 15	.			

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
07/02/2014 09 30	0.597329007	07/02/2014 09 30	.		07/02/2014 09 30	---	07/02/2014 09 30	.			
07/02/2014 09 45	0.471955535	07/02/2014 09 45		0.2	07/02/2014 09 45	---	07/02/2014 09 45	0.2			
07/02/2014 10 00	0.528395726	07/02/2014 10 00	.		07/02/2014 10 00	---	07/02/2014 10 00	.			
07/02/2014 10 15	0.513234177	07/02/2014 10 15	.		07/02/2014 10 15	---	07/02/2014 10 15	.			
07/02/2014 10 30	0.540666961	07/02/2014 10 30	.		07/02/2014 10 30	---	07/02/2014 10 30	.			
07/02/2014 10 45	0.536080316	07/02/2014 10 45	.		07/02/2014 10 45	---	07/02/2014 10 45	.			
07/02/2014 11 00	0.553490945	07/02/2014 11 00	.		07/02/2014 11 00	---	07/02/2014 11 00	.			
07/02/2014 11 15	0.493489775	07/02/2014 11 15	.		07/02/2014 11 15	---	07/02/2014 11 15	.			
07/02/2014 11 30	0.52125341	07/02/2014 11 30	.		07/02/2014 11 30	---	07/02/2014 11 30	.			
07/02/2014 11 45	0.553047251	07/02/2014 11 45	.		07/02/2014 11 45	---	07/02/2014 11 45	.			
07/02/2014 12 00	0.40969358	07/02/2014 12 00	.		07/02/2014 12 00	---	07/02/2014 12 00	.			
07/02/2014 12 15	0.502876026	07/02/2014 12 15	.		07/02/2014 12 15	---	07/02/2014 12 15	.			
07/02/2014 12 30	0.451205953	07/02/2014 12 30	.		07/02/2014 12 30	---	07/02/2014 12 30	.			
07/02/2014 12 45	0.427287974	07/02/2014 12 45	.		07/02/2014 12 45	---	07/02/2014 12 45	.			
07/02/2014 13 00	0.439104397	07/02/2014 13 00	.		07/02/2014 13 00	---	07/02/2014 13 00	.			
07/02/2014 13 15	0.426999381	07/02/2014 13 15	.		07/02/2014 13 15	---	07/02/2014 13 15	.			
07/02/2014 13 30	0.372980132	07/02/2014 13 30	.		07/02/2014 13 30	---	07/02/2014 13 30	.			
07/02/2014 13 45	0.367474584	07/02/2014 13 45	.		07/02/2014 13 45	---	07/02/2014 13 45	.			
07/02/2014 14 00	0.406896045	07/02/2014 14 00	.		07/02/2014 14 00	---	07/02/2014 14 00	.			
07/02/2014 14 15	0.416539166	07/02/2014 14 15	.		07/02/2014 14 15	---	07/02/2014 14 15	.			
07/02/2014 14 30	0.408567681	07/02/2014 14 30	.		07/02/2014 14 30	---	07/02/2014 14 30	.			
07/02/2014 14 45	0.400983113	07/02/2014 14 45	.		07/02/2014 14 45	---	07/02/2014 14 45	.			
07/02/2014 15 00	0.391393899	07/02/2014 15 00	.		07/02/2014 15 00	---	07/02/2014 15 00	.			
07/02/2014 15 15	0.35551937	07/02/2014 15 15	.		07/02/2014 15 15	---	07/02/2014 15 15	.			
07/02/2014 15 30	0.36423391	07/02/2014 15 30	.		07/02/2014 15 30	---	07/02/2014 15 30	.			
07/02/2014 15 45	0.348308458	07/02/2014 15 45	.		07/02/2014 15 45	---	07/02/2014 15 45	.			
07/02/2014 16 00	0.336407748	07/02/2014 16 00	.		07/02/2014 16 00	---	07/02/2014 16 00	.			
07/02/2014 16 15	0.32439687	07/02/2014 16 15	.		07/02/2014 16 15	---	07/02/2014 16 15	.			
07/02/2014 16 30	0.314241911	07/02/2014 16 30	.		07/02/2014 16 30	---	07/02/2014 16 30	.			
07/02/2014 16 45	0.348083622	07/02/2014 16 45	.		07/02/2014 16 45	---	07/02/2014 16 45	.			
07/02/2014 17 00	0.302744119	07/02/2014 17 00	.		07/02/2014 17 00	---	07/02/2014 17 00	.			
07/02/2014 17 15	0.288301899	07/02/2014 17 15	.		07/02/2014 17 15	---	07/02/2014 17 15	.			
07/02/2014 17 30	0.276894062	07/02/2014 17 30	.		07/02/2014 17 30	---	07/02/2014 17 30	.			
07/02/2014 17 45	0.30730018	07/02/2014 17 45	.		07/02/2014 17 45	---	07/02/2014 17 45	.			
07/02/2014 18 00	0.249388834	07/02/2014 18 00	.		07/02/2014 18 00	---	07/02/2014 18 00	.			
07/02/2014 18 15	0.27737536	07/02/2014 18 15	.		07/02/2014 18 15	---	07/02/2014 18 15	.			
07/02/2014 18 30	0.282597537	07/02/2014 18 30	.		07/02/2014 18 30	---	07/02/2014 18 30	.			
07/02/2014 18 45	0.284937756	07/02/2014 18 45	.		07/02/2014 18 45	---	07/02/2014 18 45	.			
07/02/2014 19 00	0.267073893	07/02/2014 19 00	.		07/02/2014 19 00	---	07/02/2014 19 00	.			
07/02/2014 19 15	0.300288133	07/02/2014 19 15	.		07/02/2014 19 15	---	07/02/2014 19 15	.			
07/02/2014 19 30	0.229185287	07/02/2014 19 30	.		07/02/2014 19 30	---	07/02/2014 19 30	.			
07/02/2014 19 45	0.22324606	07/02/2014 19 45	.		07/02/2014 19 45	---	07/02/2014 19 45	.			
07/02/2014 20 00	0.270705879	07/02/2014 20 00	.		07/02/2014 20 00	---	07/02/2014 20 00	.			
07/02/2014 20 15	0.258915522	07/02/2014 20 15	.		07/02/2014 20 15	---	07/02/2014 20 15	.			
07/02/2014 20 30	0.241995861	07/02/2014 20 30	.		07/02/2014 20 30	---	07/02/2014 20 30	.			
07/02/2014 20 45	0.228052967	07/02/2014 20 45	.		07/02/2014 20 45	---	07/02/2014 20 45	.			
07/02/2014 21 00	0.210470644	07/02/2014 21 00	.		07/02/2014 21 00	---	07/02/2014 21 00	.			
07/02/2014 21 15	0.238353536	07/02/2014 21 15	.		07/02/2014 21 15	---	07/02/2014 21 15	.			
07/02/2014 21 30	0.236088597	07/02/2014 21 30	.		07/02/2014 21 30	---	07/02/2014 21 30	.			
07/02/2014 21 45	0.228922354	07/02/2014 21 45	.		07/02/2014 21 45	---	07/02/2014 21 45	.			
07/02/2014 22 00	0.236733644	07/02/2014 22 00	.		07/02/2014 22 00	---	07/02/2014 22 00	.			
07/02/2014 22 15	0.223421038	07/02/2014 22 15	.		07/02/2014 22 15	---	07/02/2014 22 15	.			
07/02/2014 22 30	0.212820779	07/02/2014 22 30	.		07/02/2014 22 30	---	07/02/2014 22 30	.			
07/02/2014 22 45	0.205868694	07/02/2014 22 45	.		07/02/2014 22 45	---	07/02/2014 22 45	.			
07/02/2014 23 00	0.160564157	07/02/2014 23 00	.		07/02/2014 23 00	---	07/02/2014 23 00	.			
07/02/2014 23 15	0.21606329	07/02/2014 23 15	.		07/02/2014 23 15	---	07/02/2014 23 15	.			
07/02/2014 23 30	0.223355996	07/02/2014 23 30	.		07/02/2014 23 30	---	07/02/2014 23 30	.			
07/02/2014 23 45	0.210589984	07/02/2014 23 45	.		07/02/2014 23 45	---	07/02/2014 23 45	.			
08/02/2014 00 00	0.213024003	08/02/2014 00 00	.		08/02/2014 00 00	---	08/02/2014 00 00	.			
08/02/2014 00 15	0.178506238	08/02/2014 00 15	.		08/02/2014 00 15	---	08/02/2014 00 15	.			
08/02/2014 00 30	0.175500712	08/02/2014 00 30	.		08/02/2014 00 30	---	08/02/2014 00 30	.			
08/02/2014 00 45	0.21337249	08/02/2014 00 45	.		08/02/2014 00 45	---	08/02/2014 00 45	.			
08/02/2014 01 00	0.183884661	08/02/2014 01 00		0.2	08/02/2014 01 00	---	08/02/2014 01 00	0.2			
08/02/2014 01 15	0.179530534	08/02/2014 01 15	.		08/02/2014 01 15	---	08/02/2014 01 15	.			
08/02/2014 01 30	0.195116998	08/02/2014 01 30	.		08/02/2014 01 30	---	08/02/2014 01 30	.			
08/02/2014 01 45	0.17457957	08/02/2014 01 45		0.2	08/02/2014 01 45	---	08/02/2014 01 45	.			
08/02/2014 02 00	0.185814392	08/02/2014 02 00	.		08/02/2014 02 00	---	08/02/2014 02 00	0.2			
08/02/2014 02 15	0.20652668	08/02/2014 02 15		0.2	08/02/2014 02 15	---	08/02/2014 02 15	.			
08/02/2014 02 30	0.176524496	08/02/2014 02 30		0.2	08/02/2014 02 30	---	08/02/2014 02 30	0.2			
08/02/2014 02 45	0.163547922	08/02/2014 02 45		0.2	08/02/2014 02 45	---	08/02/2014 02 45	0.2			
08/02/2014 03 00	0.200278936	08/02/2014 03 00		0.4	08/02/2014 03 00	---	08/02/2014 03 00	0.4			
08/02/2014 03 15	0.167093244	08/02/2014 03 15		0.6	08/02/2014 03 15	---	08/02/2014 03 15	0.4			
08/02/2014 03 30	0.170919232	08/02/2014 03 30	.		08/02/2014 03 30	---	08/02/2014 03 30	0.2			
08/02/2014 03 45	0.173379402	08/02/2014 03 45	.		08/02/2014 03 45	---	08/02/2014 03 45	.			
08/02/2014 04 00	0.21745035	08/02/2014 04 00		0.2	08/02/2014 04 00	---	08/02/2014 04 00	.			

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
08/02/2014 04 15	0.185329334	08/02/2014 04 15	.		08/02/2014 04 15	---	08/02/2014 04 15	.			
08/02/2014 04 30	0.215184868	08/02/2014 04 30	.		08/02/2014 04 30	---	08/02/2014 04 30	.			
08/02/2014 04 45	0.198015565	08/02/2014 04 45	.		08/02/2014 04 45	---	08/02/2014 04 45	0.2			
08/02/2014 05 00	0.184848284	08/02/2014 05 00	.		08/02/2014 05 00	---	08/02/2014 05 00	.			
08/02/2014 05 15	0.177460787	08/02/2014 05 15	.		08/02/2014 05 15	---	08/02/2014 05 15	.			
08/02/2014 05 30	0.180214978	08/02/2014 05 30	.		08/02/2014 05 30	---	08/02/2014 05 30	.			
08/02/2014 05 45	0.179411431	08/02/2014 05 45		0.2	08/02/2014 05 45	---	08/02/2014 05 45	.			
08/02/2014 06 00	0.203700132	08/02/2014 06 00	.		08/02/2014 06 00	---	08/02/2014 06 00	.			
08/02/2014 06 15	0.201517352	08/02/2014 06 15	.		08/02/2014 06 15	---	08/02/2014 06 15	.			
08/02/2014 06 30	0.191947402	08/02/2014 06 30	.		08/02/2014 06 30	---	08/02/2014 06 30	.			
08/02/2014 06 45	0.156985176	08/02/2014 06 45	.		08/02/2014 06 45	---	08/02/2014 06 45	.			
08/02/2014 07 00	0.141320395	08/02/2014 07 00	.		08/02/2014 07 00	---	08/02/2014 07 00	0.4			
08/02/2014 07 15	0.153538609	08/02/2014 07 15		0.2	08/02/2014 07 15	---	08/02/2014 07 15	1.4			
08/02/2014 07 30	0.156833713	08/02/2014 07 30	.		08/02/2014 07 30	---	08/02/2014 07 30	0.2			
08/02/2014 07 45	0.182847287	08/02/2014 07 45	.		08/02/2014 07 45	---	08/02/2014 07 45	0.2			
08/02/2014 08 00	0.156413241	08/02/2014 08 00	.		08/02/2014 08 00	---	08/02/2014 08 00	.			
08/02/2014 08 15	0.165578557	08/02/2014 08 15	.		08/02/2014 08 15	---	08/02/2014 08 15	.			
08/02/2014 08 30	0.177707241	08/02/2014 08 30	.		08/02/2014 08 30	---	08/02/2014 08 30	.			
08/02/2014 08 45	0.172486606	08/02/2014 08 45	.		08/02/2014 08 45	---	08/02/2014 08 45	.			
08/02/2014 09 00	0.175710253	08/02/2014 09 00	.		08/02/2014 09 00	---	08/02/2014 09 00	.			
08/02/2014 09 15	0.114310965	08/02/2014 09 15		0.2	08/02/2014 09 15	---	08/02/2014 09 15	.			
08/02/2014 09 30	0.148769179	08/02/2014 09 30	.		08/02/2014 09 30	---	08/02/2014 09 30	0.2			
08/02/2014 09 45	0.143102254	08/02/2014 09 45	.		08/02/2014 09 45	---	08/02/2014 09 45	.			
08/02/2014 10 00	0.170979505	08/02/2014 10 00	.		08/02/2014 10 00	---	08/02/2014 10 00	.			
08/02/2014 10 15	0.156325371	08/02/2014 10 15	.		08/02/2014 10 15	---	08/02/2014 10 15	.			
08/02/2014 10 30	0.170065052	08/02/2014 10 30	.		08/02/2014 10 30	---	08/02/2014 10 30	.			
08/02/2014 10 45	0.127369172	08/02/2014 10 45	.		08/02/2014 10 45	---	08/02/2014 10 45	.			
08/02/2014 11 00	0.165223289	08/02/2014 11 00	.		08/02/2014 11 00	---	08/02/2014 11 00	.			
08/02/2014 11 15	0.15763576	08/02/2014 11 15	.		08/02/2014 11 15	---	08/02/2014 11 15	.			
08/02/2014 11 30	0.120563563	08/02/2014 11 30	.		08/02/2014 11 30	---	08/02/2014 11 30	.			
08/02/2014 11 45	0.124573632	08/02/2014 11 45	.		08/02/2014 11 45	---	08/02/2014 11 45	.			
08/02/2014 12 00	0.118173325	08/02/2014 12 00	.		08/02/2014 12 00	---	08/02/2014 12 00	.			
08/02/2014 12 15	0.146524679	08/02/2014 12 15		0.4	08/02/2014 12 15	---	08/02/2014 12 15	.			
08/02/2014 12 30	0.156772705	08/02/2014 12 30	.		08/02/2014 12 30	---	08/02/2014 12 30	.			
08/02/2014 12 45	0.139598229	08/02/2014 12 45	.		08/02/2014 12 45	---	08/02/2014 12 45	.			
08/02/2014 13 00	0.138360299	08/02/2014 13 00	.		08/02/2014 13 00	---	08/02/2014 13 00	.			
08/02/2014 13 15	0.147212096	08/02/2014 13 15	.		08/02/2014 13 15	---	08/02/2014 13 15	.			
08/02/2014 13 30	0.134335207	08/02/2014 13 30	.		08/02/2014 13 30	---	08/02/2014 13 30	.			
08/02/2014 13 45	0.124559964	08/02/2014 13 45	.		08/02/2014 13 45	---	08/02/2014 13 45	.			
08/02/2014 14 00	0.125644625	08/02/2014 14 00	.		08/02/2014 14 00	---	08/02/2014 14 00	.			
08/02/2014 14 15	0.10775184	08/02/2014 14 15	.		08/02/2014 14 15	---	08/02/2014 14 15	.			
08/02/2014 14 30	0.126219592	08/02/2014 14 30	.		08/02/2014 14 30	---	08/02/2014 14 30	.			
08/02/2014 14 45	0.139834394	08/02/2014 14 45	.		08/02/2014 14 45	---	08/02/2014 14 45	.			
08/02/2014 15 00	0.131012089	08/02/2014 15 00	.		08/02/2014 15 00	---	08/02/2014 15 00	.			
08/02/2014 15 15	0.14344395	08/02/2014 15 15	.		08/02/2014 15 15	---	08/02/2014 15 15	.			
08/02/2014 15 30	0.118010014	08/02/2014 15 30	.		08/02/2014 15 30	---	08/02/2014 15 30	.			
08/02/2014 15 45	0.139119977	08/02/2014 15 45	.		08/02/2014 15 45	---	08/02/2014 15 45	.			
08/02/2014 16 00	0.119148553	08/02/2014 16 00	.		08/02/2014 16 00	---	08/02/2014 16 00	.			
08/02/2014 16 15	0.1261791	08/02/2014 16 15	.		08/02/2014 16 15	---	08/02/2014 16 15	.			
08/02/2014 16 30	0.122053722	08/02/2014 16 30	.		08/02/2014 16 30	---	08/02/2014 16 30	.			
08/02/2014 16 45	0.103437266	08/02/2014 16 45	.		08/02/2014 16 45	---	08/02/2014 16 45	.			
08/02/2014 17 00	0.116301261	08/02/2014 17 00	.		08/02/2014 17 00	---	08/02/2014 17 00	.			
08/02/2014 17 15	0.137441827	08/02/2014 17 15	.		08/02/2014 17 15	---	08/02/2014 17 15	.			
08/02/2014 17 30	0.108836449	08/02/2014 17 30	.		08/02/2014 17 30	---	08/02/2014 17 30	.			
08/02/2014 17 45	0.133228573	08/02/2014 17 45	.		08/02/2014 17 45	---	08/02/2014 17 45	.			
08/02/2014 18 00	0.109812145	08/02/2014 18 00	.		08/02/2014 18 00	---	08/02/2014 18 00	.			
08/02/2014 18 15	0.134071062	08/02/2014 18 15	.		08/02/2014 18 15	---	08/02/2014 18 15	.			
08/02/2014 18 30	0.097647151	08/02/2014 18 30	.		08/02/2014 18 30	---	08/02/2014 18 30	.			
08/02/2014 18 45	0.132400607	08/02/2014 18 45	.		08/02/2014 18 45	---	08/02/2014 18 45	.			
08/02/2014 19 00	0.115196073	08/02/2014 19 00	.		08/02/2014 19 00	---	08/02/2014 19 00	.			
08/02/2014 19 15	0.101429479	08/02/2014 19 15	.		08/02/2014 19 15	---	08/02/2014 19 15	.			
08/02/2014 19 30	0.059466961	08/02/2014 19 30	.		08/02/2014 19 30	---	08/02/2014 19 30	.			
08/02/2014 19 45	0.117816744	08/02/2014 19 45	.		08/02/2014 19 45	---	08/02/2014 19 45	.			
08/02/2014 20 00	0.123464782	08/02/2014 20 00	.		08/02/2014 20 00	---	08/02/2014 20 00	.			
08/02/2014 20 15	0.127469061	08/02/2014 20 15	.		08/02/2014 20 15	---	08/02/2014 20 15	.			
08/02/2014 20 30	0.091787593	08/02/2014 20 30	.		08/02/2014 20 30	---	08/02/2014 20 30	.			
08/02/2014 20 45	0.099707647	08/02/2014 20 45	.		08/02/2014 20 45	---	08/02/2014 20 45	.			
08/02/2014 21 00	0.128219843	08/02/2014 21 00	.		08/02/2014 21 00	---	08/02/2014 21 00	.			
08/02/2014 21 15	0.085852651	08/02/2014 21 15	.		08/02/2014 21 15	---	08/02/2014 21 15	.			
08/02/2014 21 30	0.066573352	08/02/2014 21 30	.		08/02/2014 21 30	---	08/02/2014 21 30	.			
08/02/2014 21 45	0.101619146	08/02/2014 21 45	.		08/02/2014 21 45	---	08/02/2014 21 45	.			
08/02/2014 22 00	0.09939218	08/02/2014 22 00	.		08/02/2014 22 00	---	08/02/2014 22 00	.			
08/02/2014 22 15	0.103420071	08/02/2014 22 15	.		08/02/2014 22 15	---	08/02/2014 22 15	.			
08/02/2014 22 30	0.094352811	08/02/2014 22 30	.		08/02/2014 22 30	---	08/02/2014 22 30	.			
08/02/2014 22 45	0.114147939	08/02/2014 22 45	.		08/02/2014 22 45	---	08/02/2014 22 45	.			

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG		Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
08/02/2014 23 00	0.113390358	08/02/2014 23 00	.		08/02/2014 23 00	---	08/02/2014 23 00	.			
08/02/2014 23 15	0.102101155	08/02/2014 23 15	.		08/02/2014 23 15	---	08/02/2014 23 15	.			
08/02/2014 23 30	0.089564073	08/02/2014 23 30	.		08/02/2014 23 30	---	08/02/2014 23 30	.			
08/02/2014 23 45	0.097003649	08/02/2014 23 45	.		08/02/2014 23 45	---	08/02/2014 23 45	.			
09/02/2014 00 00	0.088203889	09/02/2014 00 00	.		09/02/2014 00 00	---	09/02/2014 00 00	.			
09/02/2014 00 15	0.099298534	09/02/2014 00 15	.		09/02/2014 00 15	---	09/02/2014 00 15	.			
09/02/2014 00 30	0.101561331	09/02/2014 00 30	.		09/02/2014 00 30	1.28	09/02/2014 00 30	.			
09/02/2014 00 45	0.089171325	09/02/2014 00 45	.		09/02/2014 00 45	1.26	09/02/2014 00 45	.			
09/02/2014 01 00	0.079101201	09/02/2014 01 00	.		09/02/2014 01 00	1.25	09/02/2014 01 00	.			
09/02/2014 01 15	0.092909524	09/02/2014 01 15	.		09/02/2014 01 15	1.24	09/02/2014 01 15	.			
09/02/2014 01 30	0.092095489	09/02/2014 01 30	.		09/02/2014 01 30	1.23	09/02/2014 01 30	.			
09/02/2014 01 45	0.088943532	09/02/2014 01 45	.		09/02/2014 01 45	1.22	09/02/2014 01 45	.			
09/02/2014 02 00	0.092431723	09/02/2014 02 00	.		09/02/2014 02 00	1.2	09/02/2014 02 00	.			
09/02/2014 02 15	0.099235521	09/02/2014 02 15	.		09/02/2014 02 15	1.19	09/02/2014 02 15	.			
09/02/2014 02 30	0.09273728	09/02/2014 02 30	.		09/02/2014 02 30	1.19	09/02/2014 02 30	.			
09/02/2014 02 45	0.112493131	09/02/2014 02 45	.		09/02/2014 02 45	1.17	09/02/2014 02 45	.			
09/02/2014 03 00	0.105268374	09/02/2014 03 00	.		09/02/2014 03 00	1.16	09/02/2014 03 00	.			
09/02/2014 03 15	0.08617705	09/02/2014 03 15	.		09/02/2014 03 15	1.15	09/02/2014 03 15	.			
09/02/2014 03 30	0.069967652	09/02/2014 03 30	.		09/02/2014 03 30	1.13	09/02/2014 03 30	.			
09/02/2014 03 45	0.069392596	09/02/2014 03 45	.		09/02/2014 03 45	1.12	09/02/2014 03 45	.			
09/02/2014 04 00	0.069669969	09/02/2014 04 00	.		09/02/2014 04 00	1.11	09/02/2014 04 00	.			
09/02/2014 04 15	0.070256659	09/02/2014 04 15	.		09/02/2014 04 15	1.11	09/02/2014 04 15	.			
09/02/2014 04 30	0.06464284	09/02/2014 04 30	.		09/02/2014 04 30	1.09	09/02/2014 04 30	.			
09/02/2014 04 45	0.063769425	09/02/2014 04 45	.		09/02/2014 04 45	1.09	09/02/2014 04 45	.			
09/02/2014 05 00	0.067690757	09/02/2014 05 00	.		09/02/2014 05 00	1.07	09/02/2014 05 00	.			
09/02/2014 05 15	0.075737466	09/02/2014 05 15	.		09/02/2014 05 15	1.06	09/02/2014 05 15	.			
09/02/2014 05 30	0.0649995	09/02/2014 05 30	.		09/02/2014 05 30	1.05	09/02/2014 05 30	.			
09/02/2014 05 45	0.055115946	09/02/2014 05 45	.		09/02/2014 05 45	1.05	09/02/2014 05 45	.			
09/02/2014 06 00	0.064637956	09/02/2014 06 00	.		09/02/2014 06 00	1.04	09/02/2014 06 00	.			
09/02/2014 06 15	0.052470117	09/02/2014 06 15	.		09/02/2014 06 15	1.02	09/02/2014 06 15	.			
09/02/2014 06 30	0.046607031	09/02/2014 06 30	.		09/02/2014 06 30	1.01	09/02/2014 06 30	.			
09/02/2014 06 45	0.055847958	09/02/2014 06 45	.		09/02/2014 06 45	1	09/02/2014 06 45	.			
09/02/2014 07 00	0.066052675	09/02/2014 07 00		0.2	09/02/2014 07 00	0.995	09/02/2014 07 00	.			
09/02/2014 07 15	0.051445483	09/02/2014 07 15	.		09/02/2014 07 15	0.987	09/02/2014 07 15	.			
09/02/2014 07 30	0.035357685	09/02/2014 07 30	.		09/02/2014 07 30	0.978	09/02/2014 07 30	.			
09/02/2014 07 45	0.072210981	09/02/2014 07 45	.		09/02/2014 07 45	0.97	09/02/2014 07 45	.			
09/02/2014 08 00	0.059585037	09/02/2014 08 00	.		09/02/2014 08 00	0.962	09/02/2014 08 00	.			
09/02/2014 08 15	0.066702868	09/02/2014 08 15	.		09/02/2014 08 15	0.954	09/02/2014 08 15	.			
09/02/2014 08 30	0.058489986	09/02/2014 08 30	.		09/02/2014 08 30	0.945	09/02/2014 08 30	.			
09/02/2014 08 45	0.074858353	09/02/2014 08 45	.		09/02/2014 08 45	0.937	09/02/2014 08 45	.			
09/02/2014 09 00	0.06076	09/02/2014 09 00	.		09/02/2014 09 00	0.929	09/02/2014 09 00	.			
09/02/2014 09 15	0.062399792	09/02/2014 09 15	.		09/02/2014 09 15	0.921	09/02/2014 09 15	.			
09/02/2014 09 30	0.04726409	09/02/2014 09 30	.		09/02/2014 09 30	0.913	09/02/2014 09 30	.			
09/02/2014 09 45	0.05093662	09/02/2014 09 45	.		09/02/2014 09 45	0.905	09/02/2014 09 45	.			
09/02/2014 10 00	0.065072189	09/02/2014 10 00	.		09/02/2014 10 00	0.897	09/02/2014 10 00	.			
09/02/2014 10 15	0.055118029	09/02/2014 10 15	.		09/02/2014 10 15	0.889	09/02/2014 10 15	.			
09/02/2014 10 30	0.064991925	09/02/2014 10 30	.		09/02/2014 10 30	0.881	09/02/2014 10 30	.			
09/02/2014 10 45	0.041107811	09/02/2014 10 45	.		09/02/2014 10 45	0.873	09/02/2014 10 45	.			
09/02/2014 11 00	0.075690463	09/02/2014 11 00	.		09/02/2014 11 00	0.865	09/02/2014 11 00	.			
09/02/2014 11 15	0.049611742	09/02/2014 11 15	.		09/02/2014 11 15	0.857	09/02/2014 11 15	.			
09/02/2014 11 30	0.065398169	09/02/2014 11 30	.		09/02/2014 11 30	0.849	09/02/2014 11 30	.			
09/02/2014 11 45	0.03838437	09/02/2014 11 45	.		09/02/2014 11 45	0.842	09/02/2014 11 45	.			
09/02/2014 12 00	0.088278359	09/02/2014 12 00	.		09/02/2014 12 00	0.834	09/02/2014 12 00	.			
09/02/2014 12 15	0.078042926	09/02/2014 12 15	.		09/02/2014 12 15	0.834	09/02/2014 12 15	.			
09/02/2014 12 30	0.078617687	09/02/2014 12 30	.		09/02/2014 12 30	0.826	09/02/2014 12 30	.			
09/02/2014 12 45	0.063161395	09/02/2014 12 45	.		09/02/2014 12 45	0.818	09/02/2014 12 45	.			
09/02/2014 13 00	0.068869796	09/02/2014 13 00	.		09/02/2014 13 00	0.811	09/02/2014 13 00	.			
09/02/2014 13 15	0.069454247	09/02/2014 13 15	.		09/02/2014 13 15	0.803	09/02/2014 13 15	.			
09/02/2014 13 30	0.047910956	09/02/2014 13 30	.		09/02/2014 13 30	0.795	09/02/2014 13 30	.			
09/02/2014 13 45	0.04167474	09/02/2014 13 45	.		09/02/2014 13 45	0.788	09/02/2014 13 45	.			
09/02/2014 14 00	0.067228471	09/02/2014 14 00	.		09/02/2014 14 00	0.78	09/02/2014 14 00	.			
09/02/2014 14 15	0.062196242	09/02/2014 14 15	.		09/02/2014 14 15	0.773	09/02/2014 14 15	.			
09/02/2014 14 30	0.05002828	09/02/2014 14 30	.		09/02/2014 14 30	0.773	09/02/2014 14 30	.			
09/02/2014 14 45	0.055669415	09/02/2014 14 45	.		09/02/2014 14 45	0.765	09/02/2014 14 45	.			
09/02/2014 15 00	0.076622065	09/02/2014 15 00	.		09/02/2014 15 00	0.758	09/02/2014 15 00	.			
09/02/2014 15 15	0.061775139	09/02/2014 15 15	.		09/02/2014 15 15	0.75	09/02/2014 15 15	.			
09/02/2014 15 30	0.056917053	09/02/2014 15 30	.		09/02/2014 15 30	0.743	09/02/2014 15 30	.			
09/02/2014 15 45	0.060220164	09/02/2014 15 45	.		09/02/2014 15 45	0.735	09/02/2014 15 45	.			
09/02/2014 16 00	0.066698201	09/02/2014 16 00	.		09/02/2014 16 00	0.728	09/02/2014 16 00	.			
09/02/2014 16 15	0.053287664	09/02/2014 16 15	.		09/02/2014 16 15	0.721	09/02/2014 16 15	.			
09/02/2014 16 30	0.057624986	09/02/2014 16 30	.		09/02/2014 16 30	0.721	09/02/2014 16 30	.			
09/02/2014 16 45	0.048045584	09/02/2014 16 45	.		09/02/2014 16 45	0.706	09/02/2014 16 45	.			
09/02/2014 17 00	0.055555274	09/02/2014 17 00	.		09/02/2014 17 00	0.699	09/02/2014 17 00	.			
09/02/2014 17 15	0.055026893	09/02/2014 17 15	.		09/02/2014 17 15	0.691	09/02/2014 17 15	.			
09/02/2014 17 30	0.053510522	09/02/2014 17 30	.		09/02/2014 17 30	0.684	09/02/2014 17 30	.			

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
09/02/2014 17 45	0.064510548	09/02/2014 17 45	.		09/02/2014 17 45	0.677	09/02/2014 17 45	.			
09/02/2014 18 00	0.054148697	09/02/2014 18 00	.		09/02/2014 18 00	0.677	09/02/2014 18 00	.			
09/02/2014 18 15	0.054148697	09/02/2014 18 15	.		09/02/2014 18 15	0.67	09/02/2014 18 15	.			
09/02/2014 18 30	0.042774254	09/02/2014 18 30	.		09/02/2014 18 30	0.663	09/02/2014 18 30	.			
09/02/2014 18 45	0.07017632	09/02/2014 18 45	.		09/02/2014 18 45	0.656	09/02/2014 18 45	.			
09/02/2014 19 00	0.059318898	09/02/2014 19 00	.		09/02/2014 19 00	0.649	09/02/2014 19 00	.			
09/02/2014 19 15	0.067591219	09/02/2014 19 15	.		09/02/2014 19 15	0.642	09/02/2014 19 15	.			
09/02/2014 19 30	0.046803466	09/02/2014 19 30	.		09/02/2014 19 30	0.642	09/02/2014 19 30	.			
09/02/2014 19 45	0.059302583	09/02/2014 19 45	.		09/02/2014 19 45	0.635	09/02/2014 19 45	.			
09/02/2014 20 00	0.047324263	09/02/2014 20 00	.		09/02/2014 20 00	0.628	09/02/2014 20 00	.			
09/02/2014 20 15	0.053573821	09/02/2014 20 15	.		09/02/2014 20 15	0.621	09/02/2014 20 15	.			
09/02/2014 20 30	0.063468955	09/02/2014 20 30	.		09/02/2014 20 30	0.621	09/02/2014 20 30	.			
09/02/2014 20 45	0.043678687	09/02/2014 20 45	.		09/02/2014 20 45	0.614	09/02/2014 20 45	.			
09/02/2014 21 00	0.048978496	09/02/2014 21 00	.		09/02/2014 21 00	0.607	09/02/2014 21 00	.			
09/02/2014 21 15	0.048461475	09/02/2014 21 15	.		09/02/2014 21 15	0.607	09/02/2014 21 15	.			
09/02/2014 21 30	0.053114656	09/02/2014 21 30	.		09/02/2014 21 30	0.6	09/02/2014 21 30	.			
09/02/2014 21 45	0.060352938	09/02/2014 21 45	.		09/02/2014 21 45	0.594	09/02/2014 21 45	.			
09/02/2014 22 00	0.071134765	09/02/2014 22 00	.		09/02/2014 22 00	0.594	09/02/2014 22 00	.			
09/02/2014 22 15	0.048636189	09/02/2014 22 15	.		09/02/2014 22 15	0.587	09/02/2014 22 15	.			
09/02/2014 22 30	0.062392664	09/02/2014 22 30	.		09/02/2014 22 30	0.58	09/02/2014 22 30	.			
09/02/2014 22 45	0.060853452	09/02/2014 22 45	.		09/02/2014 22 45	0.58	09/02/2014 22 45	.			
09/02/2014 23 00	0.05581736	09/02/2014 23 00	.		09/02/2014 23 00	0.573	09/02/2014 23 00	.			
09/02/2014 23 15	0.049853997	09/02/2014 23 15	.		09/02/2014 23 15	0.567	09/02/2014 23 15	.			
09/02/2014 23 30	0.052843781	09/02/2014 23 30	.		09/02/2014 23 30	0.567	09/02/2014 23 30	.			
09/02/2014 23 45	0.043874428	09/02/2014 23 45	.		09/02/2014 23 45	0.56	09/02/2014 23 45	.			
10/02/2014 00 00	0.05831748	10/02/2014 00 00	.		10/02/2014 00 00	0.554	10/02/2014 00 00	.			
10/02/2014 00 15	0.047014461	10/02/2014 00 15	.		10/02/2014 00 15	0.554	10/02/2014 00 15	.			
10/02/2014 00 30	0.045541811	10/02/2014 00 30	.		10/02/2014 00 30	0.547	10/02/2014 00 30	.			
10/02/2014 00 45	0.059748551	10/02/2014 00 45	.		10/02/2014 00 45	0.547	10/02/2014 00 45	.			
10/02/2014 01 00	0.048110344	10/02/2014 01 00	.		10/02/2014 01 00	0.54	10/02/2014 01 00	.			
10/02/2014 01 15	0.051011418	10/02/2014 01 15	.		10/02/2014 01 15	0.534	10/02/2014 01 15	.			
10/02/2014 01 30	0.050979088	10/02/2014 01 30	.		10/02/2014 01 30	0.534	10/02/2014 01 30	.			
10/02/2014 01 45	0.05534997	10/02/2014 01 45	.		10/02/2014 01 45	0.528	10/02/2014 01 45	.			
10/02/2014 02 00	0.054338673	10/02/2014 02 00	.		10/02/2014 02 00	0.528	10/02/2014 02 00	.			
10/02/2014 02 15	0.052345484	10/02/2014 02 15	.		10/02/2014 02 15	0.521	10/02/2014 02 15	.			
10/02/2014 02 30	0.044469101	10/02/2014 02 30	.		10/02/2014 02 30	0.515	10/02/2014 02 30	.			
10/02/2014 02 45	0.054396005	10/02/2014 02 45	.		10/02/2014 02 45	0.515	10/02/2014 02 45	.			
10/02/2014 03 00	0.051536698	10/02/2014 03 00	.		10/02/2014 03 00	0.515	10/02/2014 03 00	.			
10/02/2014 03 15	0.045462252	10/02/2014 03 15	.		10/02/2014 03 15	0.508	10/02/2014 03 15	.			
10/02/2014 03 30	0.053422092	10/02/2014 03 30		0.2	10/02/2014 03 30	0.508	10/02/2014 03 30		0.2		
10/02/2014 03 45	0.047865696	10/02/2014 03 45	.		10/02/2014 03 45	0.502	10/02/2014 03 45	.			
10/02/2014 04 00	0.054300327	10/02/2014 04 00	.		10/02/2014 04 00	0.502	10/02/2014 04 00	.			
10/02/2014 04 15	0.043814101	10/02/2014 04 15	.		10/02/2014 04 15	0.502	10/02/2014 04 15	.			
10/02/2014 04 30	0.045661614	10/02/2014 04 30	.		10/02/2014 04 30	0.496	10/02/2014 04 30	.			
10/02/2014 04 45	0.039871139	10/02/2014 04 45	.		10/02/2014 04 45	0.496	10/02/2014 04 45	.			
10/02/2014 05 00	0.036386957	10/02/2014 05 00	.		10/02/2014 05 00	0.489	10/02/2014 05 00	.			
10/02/2014 05 15	0.038605732	10/02/2014 05 15	.		10/02/2014 05 15	0.489	10/02/2014 05 15	.			
10/02/2014 05 30	0.043519386	10/02/2014 05 30	.		10/02/2014 05 30	0.489	10/02/2014 05 30	.			
10/02/2014 05 45	0.041318349	10/02/2014 05 45	.		10/02/2014 05 45	0.483	10/02/2014 05 45	.			
10/02/2014 06 00	0.045730081	10/02/2014 06 00	.		10/02/2014 06 00	0.483	10/02/2014 06 00	.			
10/02/2014 06 15	0.037433338	10/02/2014 06 15	.		10/02/2014 06 15	0.483	10/02/2014 06 15	.			
10/02/2014 06 30	0.038371351	10/02/2014 06 30	.		10/02/2014 06 30	0.477	10/02/2014 06 30	.			
10/02/2014 06 45	0.039237642	10/02/2014 06 45	.		10/02/2014 06 45	0.477	10/02/2014 06 45	.			
10/02/2014 07 00	0.049199986	10/02/2014 07 00	.		10/02/2014 07 00	0.477	10/02/2014 07 00	.			
10/02/2014 07 15	0.04226966	10/02/2014 07 15	.		10/02/2014 07 15	0.477	10/02/2014 07 15	.			
10/02/2014 07 30	0.038371351	10/02/2014 07 30	.		10/02/2014 07 30	0.471	10/02/2014 07 30	.			
10/02/2014 07 45	0.035249984	10/02/2014 07 45	.		10/02/2014 07 45	0.471	10/02/2014 07 45	.			
10/02/2014 08 00	0.047913435	10/02/2014 08 00	.		10/02/2014 08 00	0.465	10/02/2014 08 00	.			
10/02/2014 08 15	0.043079178	10/02/2014 08 15	.		10/02/2014 08 15	0.465	10/02/2014 08 15	.			
10/02/2014 08 30	0.041712017	10/02/2014 08 30	.		10/02/2014 08 30	0.465	10/02/2014 08 30	.			
10/02/2014 08 45	0.047916035	10/02/2014 08 45		0.4	10/02/2014 08 45	0.465	10/02/2014 08 45		0.2		
10/02/2014 09 00	0.055216442	10/02/2014 09 00		0.4	10/02/2014 09 00	0.465	10/02/2014 09 00		0.2		
10/02/2014 09 15	0.05859148	10/02/2014 09 15	.		10/02/2014 09 15	0.465	10/02/2014 09 15		0.2		
10/02/2014 09 30	0.054393807	10/02/2014 09 30		0.2	10/02/2014 09 30	0.458	10/02/2014 09 30		0.2		
10/02/2014 09 45	0.040374147	10/02/2014 09 45	.		10/02/2014 09 45	0.458	10/02/2014 09 45		0.2		
10/02/2014 10 00	0.064304622	10/02/2014 10 00		0.2	10/02/2014 10 00	0.458	10/02/2014 10 00	.			
10/02/2014 10 15	0.05549623	10/02/2014 10 15	.		10/02/2014 10 15	0.458	10/02/2014 10 15	.			
10/02/2014 10 30	0.063873652	10/02/2014 10 30	.		10/02/2014 10 30	0.458	10/02/2014 10 30		0.2		
10/02/2014 10 45	0.087813874	10/02/2014 10 45	.		10/02/2014 10 45	0.458	10/02/2014 10 45	.			
10/02/2014 11 00	0.087915	10/02/2014 11 00	.		10/02/2014 11 00	0.458	10/02/2014 11 00	.			
10/02/2014 11 15	0.071145785	10/02/2014 11 15	.		10/02/2014 11 15	0.458	10/02/2014 11 15	.			
10/02/2014 11 30	0.076257392	10/02/2014 11 30		0.2	10/02/2014 11 30	0.458	10/02/2014 11 30	.			
10/02/2014 11 45	0.069465018	10/02/2014 11 45	.		10/02/2014 11 45	0.458	10/02/2014 11 45		0.2		
10/02/2014 12 00	0.070017493	10/02/2014 12 00	.		10/02/2014 12 00	0.464	10/02/2014 12 00		0.4		
10/02/2014 12 15	0.06889297	10/02/2014 12 15	.		10/02/2014 12 15	0.464	10/02/2014 12 15	.			

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
10/02/2014 12 30	0.067248511	10/02/2014 12 30		0.2	10/02/2014 12 30	0.464	10/02/2014 12 30		0.2		
10/02/2014 12 45	0.085293995	10/02/2014 12 45		0.4	10/02/2014 12 45	0.464	10/02/2014 12 45		0.2		
10/02/2014 13 00	0.102993463	10/02/2014 13 00	.		10/02/2014 13 00	0.464	10/02/2014 13 00		0.4		
10/02/2014 13 15	0.087495167	10/02/2014 13 15	.		10/02/2014 13 15	0.464	10/02/2014 13 15	.			
10/02/2014 13 30	0.087478559	10/02/2014 13 30	.		10/02/2014 13 30	0.464	10/02/2014 13 30	.			
10/02/2014 13 45	0.098441541	10/02/2014 13 45		0.2	10/02/2014 13 45	0.464	10/02/2014 13 45	.			
10/02/2014 14 00	0.100597893	10/02/2014 14 00	.		10/02/2014 14 00	0.464	10/02/2014 14 00		0.2		
10/02/2014 14 15	0.088147459	10/02/2014 14 15	.		10/02/2014 14 15	0.458	10/02/2014 14 15	.			
10/02/2014 14 30	0.093297881	10/02/2014 14 30	.		10/02/2014 14 30	0.464	10/02/2014 14 30	.			
10/02/2014 14 45	0.075549837	10/02/2014 14 45	.		10/02/2014 14 45	0.464	10/02/2014 14 45	.			
10/02/2014 15 00	0.0651266	10/02/2014 15 00	.		10/02/2014 15 00	0.464	10/02/2014 15 00	.			
10/02/2014 15 15	0.065847165	10/02/2014 15 15	.		10/02/2014 15 15	0.464	10/02/2014 15 15	.			
10/02/2014 15 30	0.083037524	10/02/2014 15 30	.		10/02/2014 15 30	0.464	10/02/2014 15 30	.			
10/02/2014 15 45	0.093031803	10/02/2014 15 45	.		10/02/2014 15 45	0.458	10/02/2014 15 45	.			
10/02/2014 16 00	0.086829628	10/02/2014 16 00	.		10/02/2014 16 00	0.458	10/02/2014 16 00	.			
10/02/2014 16 15	0.089962903	10/02/2014 16 15	.		10/02/2014 16 15	0.458	10/02/2014 16 15	.			
10/02/2014 16 30	0.065014632	10/02/2014 16 30	.		10/02/2014 16 30	0.458	10/02/2014 16 30	.			
10/02/2014 16 45	0.080595488	10/02/2014 16 45	.		10/02/2014 16 45	0.458	10/02/2014 16 45	.			
10/02/2014 17 00	0.076962827	10/02/2014 17 00	.		10/02/2014 17 00	0.458	10/02/2014 17 00	.			
10/02/2014 17 15	0.074592614	10/02/2014 17 15	.		10/02/2014 17 15	0.458	10/02/2014 17 15	.			
10/02/2014 17 30	0.065224543	10/02/2014 17 30	.		10/02/2014 17 30	0.458	10/02/2014 17 30	.			
10/02/2014 17 45	0.05550817	10/02/2014 17 45	.		10/02/2014 17 45	0.458	10/02/2014 17 45	.			
10/02/2014 18 00	0.074578197	10/02/2014 18 00	.		10/02/2014 18 00	0.458	10/02/2014 18 00	.			
10/02/2014 18 15	0.060518832	10/02/2014 18 15	.		10/02/2014 18 15	0.458	10/02/2014 18 15	.			
10/02/2014 18 30	0.047950017	10/02/2014 18 30	.		10/02/2014 18 30	0.452	10/02/2014 18 30	.			
10/02/2014 18 45	0.065072189	10/02/2014 18 45		0.4	10/02/2014 18 45	0.452	10/02/2014 18 45	.			
10/02/2014 19 00	0.057520982	10/02/2014 19 00		0.8	10/02/2014 19 00	0.452	10/02/2014 19 00		0.6		
10/02/2014 19 15	0.058600655	10/02/2014 19 15		0.6	10/02/2014 19 15	0.452	10/02/2014 19 15		1.2		
10/02/2014 19 30	0.06993722	10/02/2014 19 30	.		10/02/2014 19 30	0.452	10/02/2014 19 30	.			
10/02/2014 19 45	0.067122454	10/02/2014 19 45	.		10/02/2014 19 45	0.452	10/02/2014 19 45	.			
10/02/2014 20 00	0.112665299	10/02/2014 20 00	.		10/02/2014 20 00	0.452	10/02/2014 20 00		0.2		
10/02/2014 20 15	0.124198737	10/02/2014 20 15		0.2	10/02/2014 20 15	0.452	10/02/2014 20 15	.			
10/02/2014 20 30	0.108299922	10/02/2014 20 30	.		10/02/2014 20 30	0.452	10/02/2014 20 30		0.6		
10/02/2014 20 45	0.082746609	10/02/2014 20 45	.		10/02/2014 20 45	0.452	10/02/2014 20 45	.			
10/02/2014 21 00	0.074945287	10/02/2014 21 00	.		10/02/2014 21 00	0.452	10/02/2014 21 00	.			
10/02/2014 21 15	0.076264116	10/02/2014 21 15	.		10/02/2014 21 15	0.458	10/02/2014 21 15	.			
10/02/2014 21 30	0.091415961	10/02/2014 21 30	.		10/02/2014 21 30	0.452	10/02/2014 21 30	.			
10/02/2014 21 45	0.098178733	10/02/2014 21 45	.		10/02/2014 21 45	0.458	10/02/2014 21 45	.			
10/02/2014 22 00	0.10430054	10/02/2014 22 00		0.4	10/02/2014 22 00	0.458	10/02/2014 22 00		0.2		
10/02/2014 22 15	0.104853119	10/02/2014 22 15		0.2	10/02/2014 22 15	0.458	10/02/2014 22 15		0.2		
10/02/2014 22 30	0.074842783	10/02/2014 22 30	.		10/02/2014 22 30	0.464	10/02/2014 22 30	.			
10/02/2014 22 45	0.098684215	10/02/2014 22 45	.		10/02/2014 22 45	0.464	10/02/2014 22 45	.			
10/02/2014 23 00	0.09813454	10/02/2014 23 00	.		10/02/2014 23 00	0.464	10/02/2014 23 00	.			
10/02/2014 23 15	0.099586576	10/02/2014 23 15		0.2	10/02/2014 23 15	0.471	10/02/2014 23 15	.			
10/02/2014 23 30	0.079377595	10/02/2014 23 30	.		10/02/2014 23 30	0.471	10/02/2014 23 30	.			
10/02/2014 23 45	0.096122647	10/02/2014 23 45	.		10/02/2014 23 45	0.477	10/02/2014 23 45	.			
11/02/2014 00 00	0.094770123	11/02/2014 00 00	.		11/02/2014 00 00	0.477	11/02/2014 00 00	.			
11/02/2014 00 15	0.090696524	11/02/2014 00 15	.		11/02/2014 00 15	0.483	11/02/2014 00 15	.			
11/02/2014 00 30	0.091376725	11/02/2014 00 30	.		11/02/2014 00 30	0.489	11/02/2014 00 30	.			
11/02/2014 00 45	0.107623897	11/02/2014 00 45	.		11/02/2014 00 45	0.489	11/02/2014 00 45		0.2		
11/02/2014 01 00	0.083963035	11/02/2014 01 00	.		11/02/2014 01 00	0.495	11/02/2014 01 00	.			
11/02/2014 01 15	0.085991109	11/02/2014 01 15	.		11/02/2014 01 15	0.502	11/02/2014 01 15	.			
11/02/2014 01 30	0.086667133	11/02/2014 01 30	.		11/02/2014 01 30	0.508	11/02/2014 01 30	.			
11/02/2014 01 45	0.081853914	11/02/2014 01 45	.		11/02/2014 01 45	0.508	11/02/2014 01 45	.			
11/02/2014 02 00	0.083214315	11/02/2014 02 00	.		11/02/2014 02 00	0.514	11/02/2014 02 00	.			
11/02/2014 02 15	0.098178733	11/02/2014 02 15	.		11/02/2014 02 15	0.521	11/02/2014 02 15	.			
11/02/2014 02 30	0.091376725	11/02/2014 02 30	.		11/02/2014 02 30	0.527	11/02/2014 02 30	.			
11/02/2014 02 45	0.096138131	11/02/2014 02 45	.		11/02/2014 02 45	0.54	11/02/2014 02 45	.			
11/02/2014 03 00	0.102259938	11/02/2014 03 00	.		11/02/2014 03 00	0.547	11/02/2014 03 00	.			
11/02/2014 03 15	0.087975721	11/02/2014 03 15	.		11/02/2014 03 15	0.56	11/02/2014 03 15	.			
11/02/2014 03 30	0.087926259	11/02/2014 03 30	.		11/02/2014 03 30	0.566	11/02/2014 03 30	.			
11/02/2014 03 45	0.083135554	11/02/2014 03 45	.		11/02/2014 03 45	0.573	11/02/2014 03 45	.			
11/02/2014 04 00	0.092032577	11/02/2014 04 00	.		11/02/2014 04 00	0.587	11/02/2014 04 00	.			
11/02/2014 04 15	0.105720305	11/02/2014 04 15	.		11/02/2014 04 15	0.593	11/02/2014 04 15	.			
11/02/2014 04 30	0.101613986	11/02/2014 04 30	.		11/02/2014 04 30	0.6	11/02/2014 04 30	.			
11/02/2014 04 45	0.099560827	11/02/2014 04 45	.		11/02/2014 04 45	0.607	11/02/2014 04 45	.			
11/02/2014 05 00	0.089979418	11/02/2014 05 00	.		11/02/2014 05 00	0.614	11/02/2014 05 00	.			
11/02/2014 05 15	0.096138895	11/02/2014 05 15	.		11/02/2014 05 15	0.621	11/02/2014 05 15	.			
11/02/2014 05 30	0.069916507	11/02/2014 05 30	.		11/02/2014 05 30	0.627	11/02/2014 05 30	.			
11/02/2014 05 45	0.087492173	11/02/2014 05 45	.		11/02/2014 05 45	0.634	11/02/2014 05 45	.			
11/02/2014 06 00	0.082334233	11/02/2014 06 00	.		11/02/2014 06 00	0.641	11/02/2014 06 00	.			
11/02/2014 06 15	0.079200802	11/02/2014 06 15	.		11/02/2014 06 15	0.648	11/02/2014 06 15	.			
11/02/2014 06 30	0.069187793	11/02/2014 06 30	.		11/02/2014 06 30	0.648	11/02/2014 06 30	.			
11/02/2014 06 45	0.067403322	11/02/2014 06 45	.		11/02/2014 06 45	0.648	11/02/2014 06 45	.			
11/02/2014 07 00	0.082447538	11/02/2014 07 00	.		11/02/2014 07 00	0.655	11/02/2014 07 00	.			

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G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
11/02/2014 07 15	0.077466708	11/02/2014 07 15	.		11/02/2014 07 15	0.655	11/02/2014 07 15	.			
11/02/2014 07 30	0.086217127	11/02/2014 07 30	.		11/02/2014 07 30	0.655	11/02/2014 07 30	.			
11/02/2014 07 45	0.084939433	11/02/2014 07 45	.		11/02/2014 07 45	0.662	11/02/2014 07 45	.			
11/02/2014 08 00	0.085550838	11/02/2014 08 00	.		11/02/2014 08 00	0.655	11/02/2014 08 00	.			
11/02/2014 08 15	0.084871029	11/02/2014 08 15	.		11/02/2014 08 15	0.662	11/02/2014 08 15	.			
11/02/2014 08 30	0.090113317	11/02/2014 08 30	.		11/02/2014 08 30	0.662	11/02/2014 08 30	.			
11/02/2014 08 45	0.096010891	11/02/2014 08 45	.		11/02/2014 08 45	0.662	11/02/2014 08 45	.			
11/02/2014 09 00	0.084836507	11/02/2014 09 00		0.2	11/02/2014 09 00	0.662	11/02/2014 09 00				
11/02/2014 09 15	0.094749371	11/02/2014 09 15		0.2	11/02/2014 09 15	0.662	11/02/2014 09 15	.			
11/02/2014 09 30	0.080151207	11/02/2014 09 30	.		11/02/2014 09 30	0.662	11/02/2014 09 30	.			
11/02/2014 09 45	0.092762119	11/02/2014 09 45		0.2	11/02/2014 09 45	0.662	11/02/2014 09 45				
11/02/2014 10 00	0.067738443	11/02/2014 10 00		0.2	11/02/2014 10 00	0.662	11/02/2014 10 00				
11/02/2014 10 15	0.092737127	11/02/2014 10 15		0.2	11/02/2014 10 15	0.662	11/02/2014 10 15	.			
11/02/2014 10 30	0.109348566	11/02/2014 10 30	.		11/02/2014 10 30	0.662	11/02/2014 10 30				
11/02/2014 10 45	0.126220168	11/02/2014 10 45		0.4	11/02/2014 10 45	0.662	11/02/2014 10 45				
11/02/2014 11 00	0.09018688	11/02/2014 11 00		0.2	11/02/2014 11 00	0.669	11/02/2014 11 00				
11/02/2014 11 15	0.143234627	11/02/2014 11 15		0.2	11/02/2014 11 15	0.669	11/02/2014 11 15				
11/02/2014 11 30	0.126578532	11/02/2014 11 30		0.2	11/02/2014 11 30	0.677	11/02/2014 11 30				
11/02/2014 11 45	0.140441027	11/02/2014 11 45		0.4	11/02/2014 11 45	0.677	11/02/2014 11 45				
11/02/2014 12 00	0.158740849	11/02/2014 12 00		0.2	11/02/2014 12 00	0.677	11/02/2014 12 00				
11/02/2014 12 15	0.13827522	11/02/2014 12 15	.		11/02/2014 12 15	0.684	11/02/2014 12 15	.			
11/02/2014 12 30	0.140863118	11/02/2014 12 30	.		11/02/2014 12 30	0.691	11/02/2014 12 30	.			
11/02/2014 12 45	0.114086375	11/02/2014 12 45		0.4	11/02/2014 12 45	0.698	11/02/2014 12 45	.			
11/02/2014 13 00	0.097440484	11/02/2014 13 00	.		11/02/2014 13 00	0.705	11/02/2014 13 00				
11/02/2014 13 15	0.148721146	11/02/2014 13 15	.		11/02/2014 13 15	0.713	11/02/2014 13 15				
11/02/2014 13 30	0.129496049	11/02/2014 13 30	.		11/02/2014 13 30	0.72	11/02/2014 13 30	.			
11/02/2014 13 45	0.106800968	11/02/2014 13 45		0.4	11/02/2014 13 45	0.735	11/02/2014 13 45				
11/02/2014 14 00	0.118887475	11/02/2014 14 00	.		11/02/2014 14 00	0.742	11/02/2014 14 00				
11/02/2014 14 15	0.100690754	11/02/2014 14 15	.		11/02/2014 14 15	0.749	11/02/2014 14 15	.			
11/02/2014 14 30	0.120767171	11/02/2014 14 30	.		11/02/2014 14 30	0.764	11/02/2014 14 30	.			
11/02/2014 14 45	0.105076434	11/02/2014 14 45	.		11/02/2014 14 45	0.779	11/02/2014 14 45	.			
11/02/2014 15 00	0.148730836	11/02/2014 15 00	.		11/02/2014 15 00	0.802	11/02/2014 15 00	.			
11/02/2014 15 15	0.142508083	11/02/2014 15 15	.		11/02/2014 15 15	0.818	11/02/2014 15 15	.			
11/02/2014 15 30	0.119485873	11/02/2014 15 30	.		11/02/2014 15 30	0.849	11/02/2014 15 30	.			
11/02/2014 15 45	0.135559232	11/02/2014 15 45	.		11/02/2014 15 45	0.872	11/02/2014 15 45	.			
11/02/2014 16 00	0.137314154	11/02/2014 16 00	.		11/02/2014 16 00	0.904	11/02/2014 16 00	.			
11/02/2014 16 15	0.092563647	11/02/2014 16 15	.		11/02/2014 16 15	0.936	11/02/2014 16 15	.			
11/02/2014 16 30	0.121519858	11/02/2014 16 30	.		11/02/2014 16 30	0.969	11/02/2014 16 30	.			
11/02/2014 16 45	0.145208035	11/02/2014 16 45	.		11/02/2014 16 45	1.01	11/02/2014 16 45	.			
11/02/2014 17 00	0.133741485	11/02/2014 17 00	.		11/02/2014 17 00	1.05	11/02/2014 17 00	.			
11/02/2014 17 15	0.12051085	11/02/2014 17 15	.		11/02/2014 17 15	1.1	11/02/2014 17 15	.			
11/02/2014 17 30	0.151382331	11/02/2014 17 30	.		11/02/2014 17 30	1.14	11/02/2014 17 30	.			
11/02/2014 17 45	0.110619554	11/02/2014 17 45	.		11/02/2014 17 45	1.18	11/02/2014 17 45	.			
11/02/2014 18 00	0.134558617	11/02/2014 18 00	.		11/02/2014 18 00	1.23	11/02/2014 18 00	.			
11/02/2014 18 15	0.122009799	11/02/2014 18 15	.		11/02/2014 18 15	1.28	11/02/2014 18 15	.			
11/02/2014 18 30	0.163897597	11/02/2014 18 30	.		11/02/2014 18 30	---	11/02/2014 18 30	.			
11/02/2014 18 45	0.153221247	11/02/2014 18 45	.		11/02/2014 18 45	---	11/02/2014 18 45	.			
11/02/2014 19 00	0.132617026	11/02/2014 19 00	.		11/02/2014 19 00	---	11/02/2014 19 00	.			
11/02/2014 19 15	0.129033684	11/02/2014 19 15	.		11/02/2014 19 15	---	11/02/2014 19 15	.			
11/02/2014 19 30	0.142471219	11/02/2014 19 30	.		11/02/2014 19 30	---	11/02/2014 19 30	.			
11/02/2014 19 45	0.113804477	11/02/2014 19 45	.		11/02/2014 19 45	---	11/02/2014 19 45	.			
11/02/2014 20 00	0.129929519	11/02/2014 20 00	.		11/02/2014 20 00	---	11/02/2014 20 00	.			
11/02/2014 20 15	0.138051934	11/02/2014 20 15	.		11/02/2014 20 15	---	11/02/2014 20 15	.			
11/02/2014 20 30	0.119336109	11/02/2014 20 30	.		11/02/2014 20 30	---	11/02/2014 20 30	.			
11/02/2014 20 45	0.137218512	11/02/2014 20 45	.		11/02/2014 20 45	---	11/02/2014 20 45	.			
11/02/2014 21 00	0.138105144	11/02/2014 21 00	.		11/02/2014 21 00	---	11/02/2014 21 00	.			
11/02/2014 21 15	0.145208035	11/02/2014 21 15	.		11/02/2014 21 15	---	11/02/2014 21 15	.			
11/02/2014 21 30	0.14257892	11/02/2014 21 30	.		11/02/2014 21 30	---	11/02/2014 21 30	.			
11/02/2014 21 45	0.124258722	11/02/2014 21 45	.		11/02/2014 21 45	---	11/02/2014 21 45	.			
11/02/2014 22 00	0.093355988	11/02/2014 22 00	.		11/02/2014 22 00	---	11/02/2014 22 00	.			
11/02/2014 22 15	0.133192375	11/02/2014 22 15	.		11/02/2014 22 15	---	11/02/2014 22 15	.			
11/02/2014 22 30	0.097060941	11/02/2014 22 30	.		11/02/2014 22 30	---	11/02/2014 22 30	.			
11/02/2014 22 45	0.103283244	11/02/2014 22 45	.		11/02/2014 22 45	---	11/02/2014 22 45	.			
11/02/2014 23 00	0.095548233	11/02/2014 23 00	.		11/02/2014 23 00	---	11/02/2014 23 00	.			
11/02/2014 23 15	0.129112145	11/02/2014 23 15	.		11/02/2014 23 15	---	11/02/2014 23 15	.			
11/02/2014 23 30	0.117858792	11/02/2014 23 30	.		11/02/2014 23 30	---	11/02/2014 23 30	.			
11/02/2014 23 45	0.110795723	11/02/2014 23 45	.		11/02/2014 23 45	---	11/02/2014 23 45	.			
12/02/2014 00 00	0.104557671	12/02/2014 00 00	.		12/02/2014 00 00	---	12/02/2014 00 00	.			
12/02/2014 00 15	0.114880373	12/02/2014 00 15	.		12/02/2014 00 15	---	12/02/2014 00 15	.			
12/02/2014 00 30	0.106482729	12/02/2014 00 30	.		12/02/2014 00 30	---	12/02/2014 00 30	.			
12/02/2014 00 45	0.10203666	12/02/2014 00 45	.		12/02/2014 00 45	---	12/02/2014 00 45	.			
12/02/2014 01 00	0.067738449	12/02/2014 01 00	.		12/02/2014 01 00	---	12/02/2014 01 00	.			
12/02/2014 01 15	0.094027818	12/02/2014 01 15	.		12/02/2014 01 15	---	12/02/2014 01 15	.			
12/02/2014 01 30	0.098417971	12/02/2014 01 30	.		12/02/2014 01 30	---	12/02/2014 01 30	.			
12/02/2014 01 45	0.106616836	12/02/2014 01 45	.		12/02/2014 01 45	---	12/02/2014 01 45	.			

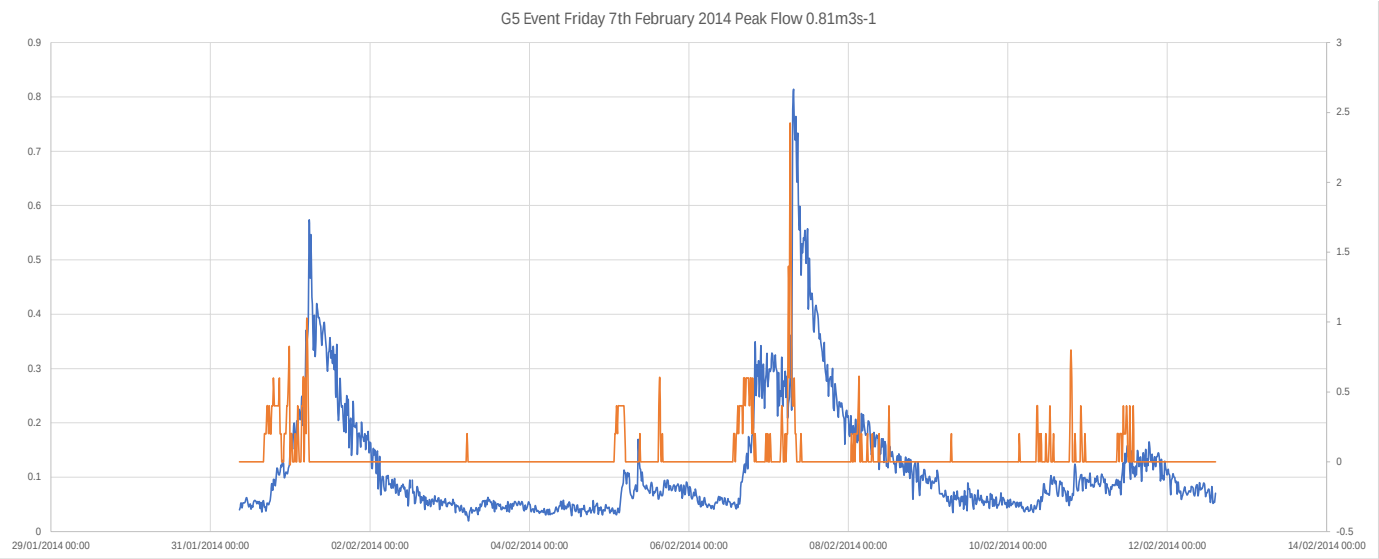
	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)
12/02/2014 02 00	0.100662814	12/02/2014 02 00	.		12/02/2014 02 00	---	12/02/2014 02 00	.			
12/02/2014 02 15	0.099298534	12/02/2014 02 15	.		12/02/2014 02 15	---	12/02/2014 02 15	.			
12/02/2014 02 30	0.090002509	12/02/2014 02 30	.		12/02/2014 02 30	---	12/02/2014 02 30	.			
12/02/2014 02 45	0.092407291	12/02/2014 02 45	.		12/02/2014 02 45	---	12/02/2014 02 45	.			
12/02/2014 03 00	0.068734841	12/02/2014 03 00	.		12/02/2014 03 00	---	12/02/2014 03 00	.			
12/02/2014 03 15	0.091313674	12/02/2014 03 15	.		12/02/2014 03 15	---	12/02/2014 03 15	.			
12/02/2014 03 30	0.077772709	12/02/2014 03 30	.		12/02/2014 03 30	---	12/02/2014 03 30	.			
12/02/2014 03 45	0.071260223	12/02/2014 03 45	.		12/02/2014 03 45	---	12/02/2014 03 45	.			
12/02/2014 04 00	0.07417923	12/02/2014 04 00	.		12/02/2014 04 00	---	12/02/2014 04 00	.			
12/02/2014 04 15	0.059314875	12/02/2014 04 15	.		12/02/2014 04 15	---	12/02/2014 04 15	.			
12/02/2014 04 30	0.064863684	12/02/2014 04 30	.		12/02/2014 04 30	1.28	12/02/2014 04 30	.			
12/02/2014 04 45	0.068865494	12/02/2014 04 45	.		12/02/2014 04 45	1.27	12/02/2014 04 45	.			
12/02/2014 05 00	0.076069004	12/02/2014 05 00	.		12/02/2014 05 00	1.25	12/02/2014 05 00	.			
12/02/2014 05 15	0.082432831	12/02/2014 05 15	.		12/02/2014 05 15	1.24	12/02/2014 05 15	.			
12/02/2014 05 30	0.074976293	12/02/2014 05 30	.		12/02/2014 05 30	1.22	12/02/2014 05 30	.			
12/02/2014 05 45	0.07014888	12/02/2014 05 45	.		12/02/2014 05 45	1.21	12/02/2014 05 45	.			
12/02/2014 06 00	0.06716429	12/02/2014 06 00	.		12/02/2014 06 00	1.2	12/02/2014 06 00	.			
12/02/2014 06 15	0.070216835	12/02/2014 06 15	.		12/02/2014 06 15	1.18	12/02/2014 06 15	.			
12/02/2014 06 30	0.074575551	12/02/2014 06 30	.		12/02/2014 06 30	1.18	12/02/2014 06 30	.			
12/02/2014 06 45	0.074592614	12/02/2014 06 45	.		12/02/2014 06 45	1.16	12/02/2014 06 45	.			
12/02/2014 07 00	0.072809051	12/02/2014 07 00	.		12/02/2014 07 00	1.15	12/02/2014 07 00	.			
12/02/2014 07 15	0.082871754	12/02/2014 07 15	.		12/02/2014 07 15	1.14	12/02/2014 07 15	.			
12/02/2014 07 30	0.082281205	12/02/2014 07 30	.		12/02/2014 07 30	1.13	12/02/2014 07 30	.			
12/02/2014 07 45	0.079919009	12/02/2014 07 45	.		12/02/2014 07 45	1.11	12/02/2014 07 45	.			
12/02/2014 08 00	0.068744066	12/02/2014 08 00	.		12/02/2014 08 00	1.1	12/02/2014 08 00	.			
12/02/2014 08 15	0.06574583	12/02/2014 08 15	.		12/02/2014 08 15	1.1	12/02/2014 08 15	.			
12/02/2014 08 30	0.076970699	12/02/2014 08 30	.		12/02/2014 08 30	1.08	12/02/2014 08 30	.			
12/02/2014 08 45	0.084750105	12/02/2014 08 45	.		12/02/2014 08 45	1.07	12/02/2014 08 45	.			
12/02/2014 09 00	0.086047917	12/02/2014 09 00	.		12/02/2014 09 00	1.06	12/02/2014 09 00	.			
12/02/2014 09 15	0.065943272	12/02/2014 09 15	.		12/02/2014 09 15	1.05	12/02/2014 09 15	.			
12/02/2014 09 30	0.075679657	12/02/2014 09 30	.		12/02/2014 09 30	1.04	12/02/2014 09 30	.			
12/02/2014 09 45	0.089869094	12/02/2014 09 45	.		12/02/2014 09 45	1.04	12/02/2014 09 45	.			
12/02/2014 10 00	0.076879285	12/02/2014 10 00	.		12/02/2014 10 00	1.03	12/02/2014 10 00	.			
12/02/2014 10 15	0.079795772	12/02/2014 10 15	.		12/02/2014 10 15	1.02	12/02/2014 10 15	.			
12/02/2014 10 30	0.079098946	12/02/2014 10 30	.		12/02/2014 10 30	1.01	12/02/2014 10 30	.			
12/02/2014 10 45	0.084296475	12/02/2014 10 45	.		12/02/2014 10 45	1	12/02/2014 10 45	.			
12/02/2014 11 00	0.08942268	12/02/2014 11 00	.		12/02/2014 11 00	0.994	12/02/2014 11 00	.			
12/02/2014 11 15	0.086217127	12/02/2014 11 15	.		12/02/2014 11 15	0.985	12/02/2014 11 15	.			
12/02/2014 11 30	0.064392028	12/02/2014 11 30	.		12/02/2014 11 30	0.977	12/02/2014 11 30	.			
12/02/2014 11 45	0.071312224	12/02/2014 11 45	.		12/02/2014 11 45	0.969	12/02/2014 11 45	.			
12/02/2014 12 00	0.071437853	12/02/2014 12 00	.		12/02/2014 12 00	0.961	12/02/2014 12 00	.			
12/02/2014 12 15	0.075737466	12/02/2014 12 15	.		12/02/2014 12 15	0.952	12/02/2014 12 15	.			
12/02/2014 12 30	0.078163454	12/02/2014 12 30	.		12/02/2014 12 30	0.944	12/02/2014 12 30	.			
12/02/2014 12 45	0.070386029	12/02/2014 12 45	.		12/02/2014 12 45	0.944	12/02/2014 12 45	.			
12/02/2014 13 00	0.053784374	12/02/2014 13 00	.		12/02/2014 13 00	0.936	12/02/2014 13 00	.			
12/02/2014 13 15	0.069241924	12/02/2014 13 15	.		12/02/2014 13 15	0.928	12/02/2014 13 15	.			
12/02/2014 13 30	0.082321389	12/02/2014 13 30	.		12/02/2014 13 30	0.92	12/02/2014 13 30	.			
12/02/2014 13 45	0.051733039	12/02/2014 13 45	.		12/02/2014 13 45	0.912	12/02/2014 13 45	.			
12/02/2014 14 00	0.055252562	12/02/2014 14 00	.		12/02/2014 14 00	0.912	12/02/2014 14 00	.			
12/02/2014 14 15	0.05377209	12/02/2014 14 15	.		12/02/2014 14 15	0.896	12/02/2014 14 15	.			
12/02/2014 14 30	0.070554198	12/02/2014 14 30	.		12/02/2014 14 30	0.896	12/02/2014 14 30	.			

	DATE TIME

G5 Flow		Benhall TBR RG			Middleton Flow		Thorpeness TBR RG			Thorpeness	Earl Soham
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Date & Time	Rainfall (mm)	Rainfall (mm)

	DATE TIME



SAAR	592	mm
AREA	5.04	Km2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

SMD on the first day of the event 0mm
So I conditions were saturated prior to the event
approx. 0 mm of free capacity in the soil column
Weekly Soil Moisture Def cit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
04-Feb-14	0	mm
11-Feb-14	0	mm

Source of Rainfall event data.

Gauge	Easting	Northing	Distance from Catchment Centroid (m)	Reciprocal	Weighting
Benhall	38166	60602	20912.0	0.00005	1.00000
Soham	23243	62717			0.00000
Thorpeness	60012	78834			0.00000
			Total	0.00005	1.00000

BR RG

Daily RF totals 9am 9am	**Benhall**	**Soham**	**horpeness**
Date	**otal RF (mm)**	**otal RF (mm)**	**otal RF (mm)**
05/02/201	1.6	0	
0 /02/201	4.4	0	
03/02/201	0	0	
02/02/201	0.2	0	
01/02/201	0	0	
Total API5 RF	6.2		

Rainall Event Depth P (mm)	20.4
Event duration (hours)	18.75

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**We ght**	**01/02/2014**	**02/02/2014**	**03/02/2014**	**04/02 2014**	**05/02/2014**
Benhall	592	1.0000	0	0.2	0	4.4	1.6
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	0.00000					
Average Daily rainfall to als			0	0.2	0	4.4	1.6

Gauge	**SAAR**	**We ght**	**01/02/2014**	**02/02/2014**	**03/02/2014**	**04/02 2014**	**05/02/2014**
Benhall	592	1.0000	0	0.000337838	0	0.007432432	0.002702703
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	0.00000					

Gauge	**SAAR**	**We ght**	**01/02/2014**	**02/02/2014**	**03/02/2014**	**04/02 2014**	**05/02/2014**
Benhall	592	1.0000	0	0.000337838	0	0.007432432	0.002702703
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592						

Gauge	**SAAR**	**We ght**	**01/02/2014**	**02/02/2014**	**03/02/2014**	**04/02 2014**	**05/02/2014**
Benhall	592	1.0000	0	0.2	0	4.4	1.6
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	0.00000					
Catchment Average Antecedent RF mm			0	0.2	0	4.4	1.6

Date	**Catchment Average Antecedent Rainfall (mm)**	
01/02/2014	0.00	d-5
02/02/2014	0.20	d-
03/02/2014	0.00	d-3
04/02/2014	. 0	d-2
05/02/2014	1.60	d-1

API5

2.70	mm	2.704683438	mm / day

CWI Prior to Event February 201 Event at G5
CWI = 125 API15 - SMD

SMD	0	mm
CWI	127.7046834	mm

FEH Parameter						
SPR	35.2	%				
PRrural	35.9	%		P=Storm Depth	20.4	mm
DPRrain	0.0	%		SPR	35.23793268	
DPRcwi	0.7	CWI	127.705			

As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural

PR	36.1	%		
PRrural	35.9	%		
CWI	127.7	mm		
BF	0.00001		Baseflow equation taken from FEH	
	-1254			
	1778.5	524.5	0.00525	
AREA	5.04		**0.02643**	m3s-1
SPR	35.2			

SPR = PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}

SPR =	35.2
PRrural	35.9

URBEXT2000		As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
PR	36	taken from PR calculations sheet using Benhall TBR RG record
DPRrain	0	DPRrain is 0, as P<40mm
DPRcwi	0.7	
SPR	35.2	
DPRrain	0.45(P-40)^0.7	#NUM!
P	20.4	
CWI	127.7	
SPR	35.2	
PR	36.1	
SPRHOST	24.27	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
Duration (hours)	18.75	

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
06-Feb-14	07-Feb-14	18.75	2.7	0.0	127.7	35.9	0.7	0.0	35.2	36.00	24.27

Site	Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Leis Sizewell	Leis Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	Leis Abbey	24.3	44.8	27.8	51.4
Leiston	Leiston	24.3	44.8	20.7	38.2
Leis Upper	Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	Mins Potters	24.3	44.8	25.3	46.8
				Mean	37.3

NOTES

The FEH SPRHOST catchment descriptor underestimates the SPR thoughout all of the upland sub-catchments

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
07/07/2014 08:45	0.036163412	05/07/2014 09:15	.	
07/07/2014 09:00	0.033269729	05/07/2014 09:30	.	
07/07/2014 09:15	0.037396561	05/07/2014 09:45	.	
07/07/2014 09:30	0.03121835	05/07/2014 10 00	.	
07/07/2014 09:45	0.033984912	05/07/2014 10:15	.	
07/07/2014 10:00	0.034308015	05/07/2014 10:30	.	
07/07/2014 10:15	0.037257394	05/07/2014 10:45	.	
07/07/2014 10:30	0.048477884	05/07/2014 11 00	.	
07/07/2014 10:45	0.060307194	05/07/2014 11:15	.	
07/07/2014 11:00	0.050745599	05/07/2014 11:30	.	
07/07/2014 11:15	0.038153368	05/07/2014 11:45	.	
07/07/2014 11:30	0.045499862	05/07/2014 12 00	.	
07/07/2014 11:45	0.034740858	05/07/2014 12:15	.	
07/07/2014 12:00	0.027533994	05/07/2014 12:30	.	
07/07/2014 12:15	0.033351218	05/07/2014 12:45	.	
07/07/2014 12:30	0.036740577	05/07/2014 13 00	.	
07/07/2014 12:45	0.031609892	05/07/2014 13:15	.	
07/07/2014 13:00	0.033121461	05/07/2014 13:30	.	
07/07/2014 13:15	0.044870111	05/07/2014 13:45	.	
07/07/2014 13:30	0.026237311	05/07/2014 14 00	.	
07/07/2014 13:45	0.028297213	05/07/2014 14:15	.	
07/07/2014 14:00	0.03678583	05/07/2014 14:30	.	
07/07/2014 14:15	0.033229674	05/07/2014 14:45	.	
07/07/2014 14:30	0.036997121	05/07/2014 15 00	.	
07/07/2014 14:45	0.030174387	05/07/2014 15:15	.	
07/07/2014 15:00	0.043569096	05/07/2014 15:30	.	
07/07/2014 15:15	0.023570989	05/07/2014 15:45	.	
07/07/2014 15:30	0.033040744	05/07/2014 16 00	.	
07/07/2014 15:45	0.028519807	05/07/2014 16:15	.	
07/07/2014 16:00	0.025317148	05/07/2014 16:30	.	
07/07/2014 16:15	0.026148526	05/07/2014 16:45	.	
07/07/2014 16:30	0.032470407	05/07/2014 17 00	.	
07/07/2014 16:45	0.026420107	05/07/2014 17:15	.	
07/07/2014 17:00	0.025737384	05/07/2014 17:30	.	
07/07/2014 17:15	0.027072834	05/07/2014 17:45	.	
07/07/2014 17:30	0.030099182	05/07/2014 18 00	.	
07/07/2014 17:45	0.028760321	05/07/2014 18:15	.	
07/07/2014 18:00	0.024901459	05/07/2014 18:30	.	
07/07/2014 18:15	0.034388011	05/07/2014 18:45	.	
07/07/2014 18:30	0.031772832	05/07/2014 19 00	.	
07/07/2014 18:45	0.030927557	05/07/2014 19:15	.	
07/07/2014 19:00	0.032519692	05/07/2014 19:30	.	
07/07/2014 19:15	0.034993894	05/07/2014 19:45	.	
07/07/2014 19:30	0.027975861	05/07/2014 20 00	.	
07/07/2014 19:45	0.034813314	05/07/2014 20:15	.	
07/07/2014 20:00	0.03163379	05/07/2014 20:30	.	
07/07/2014 20:15	0.029872961	05/07/2014 20:45	.	
07/07/2014 20:30	0.029432754	05/07/2014 21 00	.	
07/07/2014 20:45	0.027826583	05/07/2014 21:15	.	
07/07/2014 21:00	0.023459876	05/07/2014 21:30	0 2	
07/07/2014 21:15	0.025206558	05/07/2014 21:45	.	
07/07/2014 21:30	0.030883277	05/07/2014 22 00	.	
07/07/2014 21:45	0.030574733	05/07/2014 22:15	.	
07/07/2014 22:00	0.03069758	05/07/2014 22:30	.	
07/07/2014 22:15	0.026676425	05/07/2014 22:45	.	
07/07/2014 22:30	0.029573265	05/07/2014 23 00	.	
07/07/2014 22:45	0.031193583	05/07/2014 23:15	.	

	DATE TIME
start of event	12/07/2014 05:15
end of event	12/07/2014 06:15
duration hours	1
total RF mm	7.4
SMD W/E AVERAGE	**mm**
08-Jul-14	112.6

DATE	API5	Daily Totals
10/07/2014	d-1	9.2
09/07/2014	d-2	0.4
08/07/2014	d-3	1.8
07/07/2014	d-4	0
06/07/2014	d-5	4.2
		15.6

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
07/07/2014 23:00	0.026791511	05/07/2014 23:30	.	
07/07/2014 23:15	0.032514205	05/07/2014 23:45	.	
07/07/2014 23:30	0.030753376	06/07/2014 00 00	.	
07/07/2014 23:45	0.033938629	06/07/2014 00:15	0 2	
08/07/2014 00:00	0.036206897	06/07/2014 00:30	0 6	
08/07/2014 00:15	0.035203726	06/07/2014 00:45	0 2	
08/07/2014 00:30	0.038312086	06/07/2014 01 00	.	
08/07/2014 00:45	0.032465777	06/07/2014 01:15	.	
08/07/2014 01:00	0.02905543	06/07/2014 01:30	.	
08/07/2014 01:15	0.033121461	06/07/2014 01:45	.	
08/07/2014 01:30	0.034394044	06/07/2014 02 00	0 2	
08/07/2014 01:45	0.024575008	06/07/2014 02:15	0 2	
08/07/2014 02:00	0.025557093	06/07/2014 02:30	.	
08/07/2014 02:15	0.031319948	06/07/2014 02:45	.	
08/07/2014 02:30	0.019309701	06/07/2014 03 00	.	
08/07/2014 02:45	0.026564215	06/07/2014 03:15	.	
08/07/2014 03:00	0.025737384	06/07/2014 03:30	.	
08/07/2014 03:15	0.023201925	06/07/2014 03:45	.	
08/07/2014 03:30	0.025833499	06/07/2014 04 00	.	
08/07/2014 03:45	0.022203778	06/07/2014 04:15	.	
08/07/2014 04:00	0.023484785	06/07/2014 04:30	0 2	
08/07/2014 04:15	0.031928292	06/07/2014 04:45	.	
08/07/2014 04:30	0.023461041	06/07/2014 05 00	.	
08/07/2014 04:45	0.027549192	06/07/2014 05:15	.	
08/07/2014 05:00	0.020623601	06/07/2014 05:30	.	
08/07/2014 05:15	0.018564024	06/07/2014 05:45	.	
08/07/2014 05:30	0.023412441	06/07/2014 06 00	.	
08/07/2014 05:45	0.018491325	06/07/2014 06:15	.	
08/07/2014 06:00	0.021116649	06/07/2014 06:30	.	
08/07/2014 06:15	0.024669063	06/07/2014 06:45	.	
08/07/2014 06:30	0.020050925	06/07/2014 07 00	.	
08/07/2014 06:45	0.022434817	06/07/2014 07:15	.	
08/07/2014 07:00	0.02549999	06/07/2014 07:30	0 2	
08/07/2014 07:15	0.023461041	06/07/2014 07:45	.	
08/07/2014 07:30	0.027767029	06/07/2014 08 00	0 2	
08/07/2014 07:45	0.025441768	06/07/2014 08:15	0 2	
08/07/2014 08:00	0.029082481	06/07/2014 08:30	.	
08/07/2014 08:15	0.029777279	06/07/2014 08:45	.	
08/07/2014 08:30	0.036712419	06/07/2014 09 00	.	
08/07/2014 08:45	0.027389912	06/07/2014 09:15	.	
08/07/2014 09:00	0.025911096	06/07/2014 09:30	0 2	
08/07/2014 09:15	0.026180592	06/07/2014 09:45	.	
08/07/2014 09:30	0.038447469	06/07/2014 10 00	0 2	
08/07/2014 09:45	0.032585976	06/07/2014 10:15	0.4	
08/07/2014 10:00	0.025371831	06/07/2014 10:30	0 2	
08/07/2014 10:15	0.032135092	06/07/2014 10:45	0.4	
08/07/2014 10:30	0.031855501	06/07/2014 11 00	0.4	
08/07/2014 10:45	0.033739727	06/07/2014 11:15	0 2	
08/07/2014 11:00	0.032324667	06/07/2014 11:30	0 2	
08/07/2014 11:15	0.046594356	06/07/2014 11:45	.	
08/07/2014 11:30	0.039651212	06/07/2014 12 00	0 2	
08/07/2014 11:45	0.032952969	06/07/2014 12:15	0.4	
08/07/2014 12:00	0.033441674	06/07/2014 12:30	0.4	
08/07/2014 12:15	0.037602724	06/07/2014 12:45	0 2	
08/07/2014 12:30	0.040178378	06/07/2014 13 00	0 2	
08/07/2014 12:45	0.026351303	06/07/2014 13:15	.	
08/07/2014 13:00	0.025275504	06/07/2014 13:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
08/07/2014 13:15	0.02810065	06/07/2014 13:45	.	
08/07/2014 13:30	0.030721104	06/07/2014 14 00	.	
08/07/2014 13:45	0.030409248	06/07/2014 14:15	.	
08/07/2014 14:00	0.028872823	06/07/2014 14:30	.	
08/07/2014 14:15	0.029777279	06/07/2014 14:45	.	
08/07/2014 14:30	0.039929101	06/07/2014 15 00	.	
08/07/2014 14:45	0.049655187	06/07/2014 15:15	.	
08/07/2014 15:00	0.039166543	06/07/2014 15:30	.	
08/07/2014 15:15	0.047748712	06/07/2014 15:45	.	
08/07/2014 15:30	0.044650393	06/07/2014 16 00	.	
08/07/2014 15:45	0.045796476	06/07/2014 16:15	.	
08/07/2014 16:00	0.042986622	06/07/2014 16:30	.	
08/07/2014 16:15	0.053189853	06/07/2014 16:45	.	
08/07/2014 16:30	0.043934302	06/07/2014 17 00	.	
08/07/2014 16:45	0.03713931	06/07/2014 17:15	.	
08/07/2014 17:00	0.036041442	06/07/2014 17:30	.	
08/07/2014 17:15	0.033363271	06/07/2014 17:45	.	
08/07/2014 17:30	0.031916832	06/07/2014 18 00	.	
08/07/2014 17:45	0.028990919	06/07/2014 18:15	.	
08/07/2014 18:00	0.028147797	06/07/2014 18:30	.	
08/07/2014 18:15	0.049030319	06/07/2014 18:45	.	
08/07/2014 18:30	0.034571998	06/07/2014 19 00	.	
08/07/2014 18:45	0.043917741	06/07/2014 19:15	.	
08/07/2014 19:00	0.033593455	06/07/2014 19:30	.	
08/07/2014 19:15	0.035615331	06/07/2014 19:45	0	2
08/07/2014 19:30	0.024361707	06/07/2014 20 00	.	
08/07/2014 19:45	0.038897638	06/07/2014 20:15	.	
08/07/2014 20:00	0.029988519	06/07/2014 20:30	.	
08/07/2014 20:15	0.034065993	06/07/2014 20:45	.	
08/07/2014 20:30	0.039736442	06/07/2014 21 00	.	
08/07/2014 20:45	0.031864123	06/07/2014 21:15	.	
08/07/2014 21:00	0.034345795	06/07/2014 21:30	.	
08/07/2014 21:15	0.041324928	06/07/2014 21:45	.	
08/07/2014 21:30	0.035741621	06/07/2014 22 00	.	
08/07/2014 21:45	0.032949968	06/07/2014 22:15	.	
08/07/2014 22:00	0.032169219	06/07/2014 22:30	.	
08/07/2014 22:15	0.030481328	06/07/2014 22:45	.	
08/07/2014 22:30	0.035061905	06/07/2014 23 00	.	
08/07/2014 22:45	0.031089072	06/07/2014 23:15	.	
08/07/2014 23:00	0.034503372	06/07/2014 23:30	.	
08/07/2014 23:15	0.028112132	06/07/2014 23:45	.	
08/07/2014 23:30	0.032514205	07/07/2014 00 00	.	
08/07/2014 23:45	0.029135604	07/07/2014 00:15	.	
09/07/2014 00:00	0.038632474	07/07/2014 00:30	.	
09/07/2014 00:15	0.036774968	07/07/2014 00:45	.	
09/07/2014 00:30	0.033440161	07/07/2014 01 00	.	
09/07/2014 00:45	0.037687679	07/07/2014 01:15	.	
09/07/2014 01:00	0.030126137	07/07/2014 01:30	.	
09/07/2014 01:15	0.034577402	07/07/2014 01:45	.	
09/07/2014 01:30	0.037687679	07/07/2014 02 00	.	
09/07/2014 01:45	0.032489305	07/07/2014 02:15	.	
09/07/2014 02:00	0.027090947	07/07/2014 02:30	.	
09/07/2014 02:15	0.027793662	07/07/2014 02:45	0	2
09/07/2014 02:30	0.026676425	07/07/2014 03 00	.	
09/07/2014 02:45	0.021813288	07/07/2014 03:15	0	2
09/07/2014 03:00	0.02381354	07/07/2014 03:30	.	
09/07/2014 03:15	0.025867046	07/07/2014 03:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
09/07/2014 03:30	0.027984144	07/07/2014 04 00	.	
09/07/2014 03:45	0.025050037	07/07/2014 04:15	.	
09/07/2014 04:00	0.028664593	07/07/2014 04:30	.	
09/07/2014 04:15	0.030673567	07/07/2014 04:45	.	
09/07/2014 04:30	0.028064437	07/07/2014 05 00	.	
09/07/2014 04:45	0.019444502	07/07/2014 05:15	.	
09/07/2014 05:00	0.024846626	07/07/2014 05:30	.	
09/07/2014 05:15	0.019744541	07/07/2014 05:45	.	
09/07/2014 05:30	0.019744541	07/07/2014 06 00	.	
09/07/2014 05:45	0.024575991	07/07/2014 06:15	.	
09/07/2014 06:00	0.023938701	07/07/2014 06:30	.	
09/07/2014 06:15	0.023938701	07/07/2014 06:45	.	
09/07/2014 06:30	0.03609407	07/07/2014 07 00	.	
09/07/2014 06:45	0.02136029	07/07/2014 07:15	.	
09/07/2014 07:00	0.020116191	07/07/2014 07:30	.	
09/07/2014 07:15	0.022849172	07/07/2014 07:45	.	
09/07/2014 07:30	0.026722819	07/07/2014 08 00	.	
09/07/2014 07:45	0.037121068	07/07/2014 08:15	.	
09/07/2014 08:00	0.03570937	07/07/2014 08:30	.	
09/07/2014 08:15	0.035928722	07/07/2014 08:45	.	
09/07/2014 08:30	0.034275034	07/07/2014 09 00	.	4.2
09/07/2014 08:45	0.042325763	07/07/2014 09:15	.	
09/07/2014 09:00	0.03106075	07/07/2014 09:30	.	
09/07/2014 09:15	0.050979088	07/07/2014 09:45	.	
09/07/2014 09:30	0.031491392	07/07/2014 10 00	.	
09/07/2014 09:45	0.038669445	07/07/2014 10:15	.	
09/07/2014 10:00	0.034048464	07/07/2014 10:30	.	
09/07/2014 10:15	0.03572022	07/07/2014 10:45	.	
09/07/2014 10:30	0.048886652	07/07/2014 11 00	.	
09/07/2014 10:45	0.041288987	07/07/2014 11:15	.	
09/07/2014 11:00	0.039175462	07/07/2014 11:30	.	
09/07/2014 11:15	0.039155113	07/07/2014 11:45	.	
09/07/2014 11:30	0.036071482	07/07/2014 12 00	.	
09/07/2014 11:45	0.02590648	07/07/2014 12:15	.	
09/07/2014 12:00	0.038679708	07/07/2014 12:30	.	
09/07/2014 12:15	0.030926321	07/07/2014 12:45	.	
09/07/2014 12:30	0.034477524	07/07/2014 13 00	.	
09/07/2014 12:45	0.026998884	07/07/2014 13:15	.	
09/07/2014 13:00	0.026899034	07/07/2014 13:30	.	
09/07/2014 13:15	0.033724427	07/07/2014 13:45	.	
09/07/2014 13:30	0 0443998	07/07/2014 14 00	.	
09/07/2014 13:45	0.029136595	07/07/2014 14:15	.	
09/07/2014 14:00	0.028263253	07/07/2014 14:30	.	
09/07/2014 14:15	0.031441024	07/07/2014 14:45	.	
09/07/2014 14:30	0.034993894	07/07/2014 15 00	.	
09/07/2014 14:45	0.036844481	07/07/2014 15:15	.	
09/07/2014 15:00	0.027681492	07/07/2014 15:30	.	
09/07/2014 15:15	0.035249984	07/07/2014 15:45	.	
09/07/2014 15:30	0.037906051	07/07/2014 16 00	.	
09/07/2014 15:45	0.039642481	07/07/2014 16:15	.	
09/07/2014 16:00	0.034724794	07/07/2014 16:30	.	
09/07/2014 16:15	0.031505652	07/07/2014 16:45	.	
09/07/2014 16:30	0.026953241	07/07/2014 17 00	.	
09/07/2014 16:45	0.031241306	07/07/2014 17:15	.	
09/07/2014 17:00	0.031552481	07/07/2014 17:30	.	
09/07/2014 17:15	0.024638003	07/07/2014 17:45	.	
09/07/2014 17:30	0.03329487	07/07/2014 18 00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
09/07/2014 17:45	0.029997016	07/07/2014 18:15	.	
09/07/2014 18:00	0.023238704	07/07/2014 18:30	.	
09/07/2014 18:15	0.026701183	07/07/2014 18:45	.	
09/07/2014 18:30	0.033463382	07/07/2014 19 00	.	
09/07/2014 18:45	0.031772832	07/07/2014 19:15	.	
09/07/2014 19:00	0.032618107	07/07/2014 19:30	.	
09/07/2014 19:15	0.03635485	07/07/2014 19:45	.	
09/07/2014 19:30	0.038430945	07/07/2014 20 00	.	
09/07/2014 19:45	0.03069758	07/07/2014 20:15	.	
09/07/2014 20:00	0.024769888	07/07/2014 20:30	.	
09/07/2014 20:15	0.031319948	07/07/2014 20:45	.	
09/07/2014 20:30	0.035155448	07/07/2014 21 00	.	
09/07/2014 20:45	0.02855234	07/07/2014 21:15	.	
09/07/2014 21:00	0.037356484	07/07/2014 21:30	.	
09/07/2014 21:15	0.026791511	07/07/2014 21:45	.	
09/07/2014 21:30	0.030883277	07/07/2014 22 00	.	
09/07/2014 21:45	0.033394619	07/07/2014 22:15	.	
09/07/2014 22:00	0.035155448	07/07/2014 22:30	.	
09/07/2014 22:15	0.033939972	07/07/2014 22:45	.	
09/07/2014 22:30	0.03274046	07/07/2014 23 00	.	
09/07/2014 22:45	0.030574733	07/07/2014 23:15	.	
09/07/2014 23:00	0 033705	07/07/2014 23:30	.	
09/07/2014 23:15	0.038911623	07/07/2014 23:45	.	
09/07/2014 23:30	0.030815177	08/07/2014 00 00	.	
09/07/2014 23:45	0.029275297	08/07/2014 00:15	.	
10/07/2014 00:00	0.034840397	08/07/2014 00:30	.	
10/07/2014 00:15	0.041864102	08/07/2014 00:45	.	
10/07/2014 00:30	0.039736442	08/07/2014 01 00	.	
10/07/2014 00:45	0.033284353	08/07/2014 01:15	.	
10/07/2014 01:00	0.034088486	08/07/2014 01:30	.	
10/07/2014 01:15	0.036022536	08/07/2014 01:45	.	
10/07/2014 01:30	0.034244039	08/07/2014 02 00	.	
10/07/2014 01:45	0.045879429	08/07/2014 02:15	.	
10/07/2014 02:00	0.031707558	08/07/2014 02:30	.	
10/07/2014 02:15	0.031819488	08/07/2014 02:45	.	
10/07/2014 02:30	0.028409006	08/07/2014 03 00	.	
10/07/2014 02:45	0.028938965	08/07/2014 03:15	.	
10/07/2014 03:00	0.030305415	08/07/2014 03:30	.	
10/07/2014 03:15	0.028980199	08/07/2014 03:45	.	
10/07/2014 03:30	0.021607851	08/07/2014 04 00	.	
10/07/2014 03:45	0.027400423	08/07/2014 04:15	.	
10/07/2014 04:00	0.018567366	08/07/2014 04:30	.	
10/07/2014 04:15	0.034552277	08/07/2014 04:45	.	
10/07/2014 04:30	0.022092579	08/07/2014 05 00	.	
10/07/2014 04:45	0.022971789	08/07/2014 05:15	.	
10/07/2014 05:00	0.020116191	08/07/2014 05:30	.	
10/07/2014 05:15	0.023202012	08/07/2014 05:45	.	
10/07/2014 05:30	0.029562516	08/07/2014 06 00	.	
10/07/2014 05:45	0.019566823	08/07/2014 06:15	.	
10/07/2014 06:00	0.020642321	08/07/2014 06:30	.	
10/07/2014 06:15	0.018985201	08/07/2014 06:45	.	
10/07/2014 06:30	0.02100082	08/07/2014 07 00	.	
10/07/2014 06:45	0.017985905	08/07/2014 07:15	.	
10/07/2014 07:00	0.026668363	08/07/2014 07:30	.	
10/07/2014 07:15	0.024307046	08/07/2014 07:45	.	
10/07/2014 07:30	0.023721724	08/07/2014 08 00	.	
10/07/2014 07:45	0.025557754	08/07/2014 08:15	.	

G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
10/07/2014 08:00	0.02948441	08/07/2014 08:30	.		
10/07/2014 08:15	0.027395593	08/07/2014 08:45	.		
10/07/2014 08:30	0.02655389	08/07/2014 09 00	.		0
10/07/2014 08:45	0.029432754	08/07/2014 09:15	.		
10/07/2014 09:00	0.027175367	08/07/2014 09:30	.		
10/07/2014 09:15	0.027831937	08/07/2014 09:45	.		
10/07/2014 09:30	0.028485922	08/07/2014 10 00	.		
10/07/2014 09:45	0.033269729	08/07/2014 10:15	.		
10/07/2014 10:00	0.036408212	08/07/2014 10:30	.		
10/07/2014 10:15	0.034100932	08/07/2014 10:45	.		
10/07/2014 10:30	0.042191504	08/07/2014 11 00	.		
10/07/2014 10:45	0.039166543	08/07/2014 11:15	.		
10/07/2014 11:00	0.037007198	08/07/2014 11:30	.		
10/07/2014 11:15	0.035273047	08/07/2014 11:45	.		
10/07/2014 11:30	0.033576349	08/07/2014 12 00	.		
10/07/2014 11:45	0.026994897	08/07/2014 12:15	.		
10/07/2014 12:00	0.02792891	08/07/2014 12:30	.		
10/07/2014 12:15	0.030517007	08/07/2014 12:45	.		
10/07/2014 12:30	0.029156011	08/07/2014 13 00	.		
10/07/2014 12:45	0.032484693	08/07/2014 13:15	.		
10/07/2014 13:00	0.027907814	08/07/2014 13:30	.		
10/07/2014 13:15	0.026004406	08/07/2014 13:45	.		
10/07/2014 13:30	0.037433338	08/07/2014 14 00	.		
10/07/2014 13:45	0.028409006	08/07/2014 14:15	.		
10/07/2014 14:00	0.024849375	08/07/2014 14:30	0 6		
10/07/2014 14:15	0.029536791	08/07/2014 14:45	0 2		
10/07/2014 14:30	0.033040744	08/07/2014 15 00	.		
10/07/2014 14:45	0.022651603	08/07/2014 15:15	.		
10/07/2014 15:00	0.022989076	08/07/2014 15:30	.		
10/07/2014 15:15	0.028872823	08/07/2014 15:45	.		
10/07/2014 15:30	0.02305354	08/07/2014 16 00	.		
10/07/2014 15:45	0.027585626	08/07/2014 16:15	0 2		
10/07/2014 16:00	0.022803406	08/07/2014 16:30	.		
10/07/2014 16:15	0.025715818	08/07/2014 16:45	.		
10/07/2014 16:30	0.037947102	08/07/2014 17 00	.		
10/07/2014 16:45	0.02439748	08/07/2014 17:15	.		
10/07/2014 17:00	0.039541176	08/07/2014 17:30	.		
10/07/2014 17:15	0.033618195	08/07/2014 17:45	.		
10/07/2014 17:30	0.02439748	08/07/2014 18 00	.		
10/07/2014 17:45	0.029385551	08/07/2014 18:15	.		
10/07/2014 18:00	0.029997016	08/07/2014 18:30	.		
10/07/2014 18:15	0.030721104	08/07/2014 18:45	.		
10/07/2014 18:30	0.026278546	08/07/2014 19 00	.		
10/07/2014 18:45	0.034993894	08/07/2014 19:15	.		
10/07/2014 19:00	0.03274046	08/07/2014 19:30	.		
10/07/2014 19:15	0.028263253	08/07/2014 19:45	0 2		
10/07/2014 19:30	0.032073997	08/07/2014 20 00	.		
10/07/2014 19:45	0.033724427	08/07/2014 20:15	.		
10/07/2014 20:00	0.03078244	08/07/2014 20:30	.		
10/07/2014 20:15	0.034840397	08/07/2014 20:45	0 2		
10/07/2014 20:30	0.032135092	08/07/2014 21 00	0 2		
10/07/2014 20:45	0.033487744	08/07/2014 21:15	.		
10/07/2014 21:00	0.034145789	08/07/2014 21:30	.		
10/07/2014 21:15	0.039773663	08/07/2014 21:45	.		
10/07/2014 21:30	0.059358672	08/07/2014 22 00	.		
10/07/2014 21:45	0.097884643	08/07/2014 22:15	.		
10/07/2014 22:00	0.105151639	08/07/2014 22:30	.		

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
10/07/2014 22:15	0.108836449	08/07/2014 22:45	.	
10/07/2014 22:30	0.111333648	08/07/2014 23 00	.	
10/07/2014 22:45	0.115218596	08/07/2014 23:15	.	
10/07/2014 23:00	0.107280214	08/07/2014 23:30	.	
10/07/2014 23:15	0.1048481	08/07/2014 23:45	.	
10/07/2014 23:30	0.103752045	09/07/2014 00 00	.	
10/07/2014 23:45	0.10441313	09/07/2014 00:15	.	
11/07/2014 00:00	0.107310147	09/07/2014 00:30	.	
11/07/2014 00:15	0.111390649	09/07/2014 00:45	.	
11/07/2014 00:30	0.107079659	09/07/2014 01 00	.	
11/07/2014 00:45	0.105741956	09/07/2014 01:15	.	
11/07/2014 01:00	0.099341833	09/07/2014 01:30	.	
11/07/2014 01:15	0.09508352	09/07/2014 01:45	.	
11/07/2014 01:30	0.09369651	09/07/2014 02 00	.	
11/07/2014 01:45	0.075375206	09/07/2014 02:15	.	
11/07/2014 02:00	0.080142276	09/07/2014 02:30	.	
11/07/2014 02:15	0.066184515	09/07/2014 02:45	.	
11/07/2014 02:30	0.069712813	09/07/2014 03 00	0 2	
11/07/2014 02:45	0.059301141	09/07/2014 03:15	.	
11/07/2014 03:00	0.075892599	09/07/2014 03:30	.	
11/07/2014 03:15	0.053965681	09/07/2014 03:45	.	
11/07/2014 03:30	0.052700079	09/07/2014 04 00	.	
11/07/2014 03:45	0.075041739	09/07/2014 04:15	.	
11/07/2014 04:00	0.053863708	09/07/2014 04:30	.	
11/07/2014 04:15	0.041218319	09/07/2014 04:45	.	
11/07/2014 04:30	0.053851464	09/07/2014 05 00	.	
11/07/2014 04:45	0.054050607	09/07/2014 05:15	.	
11/07/2014 05:00	0.053807764	09/07/2014 05:30	.	
11/07/2014 05:15	0.048025774	09/07/2014 05:45	.	
11/07/2014 05:30	0.047411244	09/07/2014 06 00	.	
11/07/2014 05:45	0.060510116	09/07/2014 06:15	.	
11/07/2014 06:00	0.049334306	09/07/2014 06:30	.	
11/07/2014 06:15	0.054703181	09/07/2014 06:45	.	
11/07/2014 06:30	0.069447826	09/07/2014 07 00	.	
11/07/2014 06:45	0.061919576	09/07/2014 07:15	.	
11/07/2014 07:00	0.056922049	09/07/2014 07:30	.	
11/07/2014 07:15	0.060044787	09/07/2014 07:45	.	
11/07/2014 07:30	0.085495921	09/07/2014 08 00	.	
11/07/2014 07:45	0.057349017	09/07/2014 08:15	.	
11/07/2014 08:00	0.05169016	09/07/2014 08:30	.	
11/07/2014 08:15	0.048434325	09/07/2014 08:45	.	
11/07/2014 08:30	0.058201829	09/07/2014 09 00	.	1.8
11/07/2014 08:45	0.057098995	09/07/2014 09:15	.	
11/07/2014 09:00	0.068098971	09/07/2014 09:30	.	
11/07/2014 09:15	0.05580488	09/07/2014 09:45	.	
11/07/2014 09:30	0.046746076	09/07/2014 10 00	.	
11/07/2014 09:45	0.060438164	09/07/2014 10:15	.	
11/07/2014 10:00	0.056922049	09/07/2014 10:30	.	
11/07/2014 10:15	0.051375956	09/07/2014 10:45	.	
11/07/2014 10:30	0.056884607	09/07/2014 11 00	.	
11/07/2014 10:45	0.048524074	09/07/2014 11:15	.	
11/07/2014 11:00	0.055807491	09/07/2014 11:30	.	
11/07/2014 11:15	0.05360909	09/07/2014 11:45	.	
11/07/2014 11:30	0.057349017	09/07/2014 12 00	.	
11/07/2014 11:45	0.055363385	09/07/2014 12:15	.	
11/07/2014 12:00	0.053807764	09/07/2014 12:30	.	
11/07/2014 12:15	0.075130969	09/07/2014 12:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
11/07/2014 12:30	0.047040342	09/07/2014 13 00	.	
11/07/2014 12:45	0.03713931	09/07/2014 13:15	.	
11/07/2014 13:00	0.024240439	09/07/2014 13:30	.	
11/07/2014 13:15	0.035599416	09/07/2014 13:45	.	
11/07/2014 13:30	0.028330514	09/07/2014 14 00	.	
11/07/2014 13:45	0.035206965	09/07/2014 14:15	.	
11/07/2014 14:00	0.031313221	09/07/2014 14:30	.	
11/07/2014 14:15	0.045175063	09/07/2014 14:45	.	
11/07/2014 14:30	0.033226433	09/07/2014 15 00	.	
11/07/2014 14:45	0.028642382	09/07/2014 15:15	.	
11/07/2014 15:00	0.033927354	09/07/2014 15:30	.	
11/07/2014 15:15	0.031670924	09/07/2014 15:45	.	
11/07/2014 15:30	0.036643255	09/07/2014 16 00	.	
11/07/2014 15:45	0.032489305	09/07/2014 16:15	.	
11/07/2014 16:00	0.03106075	09/07/2014 16:30	.	
11/07/2014 16:15	0.033284353	09/07/2014 16:45	.	
11/07/2014 16:30	0.03201312	09/07/2014 17 00	.	
11/07/2014 16:45	0.033441674	09/07/2014 17:15	.	
11/07/2014 17:00	0.041626592	09/07/2014 17:30	.	
11/07/2014 17:15	0.032333024	09/07/2014 17:45	.	
11/07/2014 17:30	0.037022034	09/07/2014 18 00	.	
11/07/2014 17:45	0.03514643	09/07/2014 18:15	.	
11/07/2014 18:00	0.037959836	09/07/2014 18:30	.	
11/07/2014 18:15	0.03453853	09/07/2014 18:45	.	
11/07/2014 18:30	0.040108262	09/07/2014 19 00	.	
11/07/2014 18:45	0.034394044	09/07/2014 19:15	.	
11/07/2014 19:00	0.038562628	09/07/2014 19:30	.	
11/07/2014 19:15	0.035539023	09/07/2014 19:45	0	2
11/07/2014 19:30	0.034251496	09/07/2014 20 00	.	
11/07/2014 19:45	0.028360896	09/07/2014 20:15	.	
11/07/2014 20:00	0.047931196	09/07/2014 20:30	.	
11/07/2014 20:15	0.031115307	09/07/2014 20:45	.	
11/07/2014 20:30	0.032599062	09/07/2014 21 00	.	
11/07/2014 20:45	0.030126137	09/07/2014 21:15	.	
11/07/2014 21:00	0.035901669	09/07/2014 21:30	.	
11/07/2014 21:15	0.042490761	09/07/2014 21:45	.	
11/07/2014 21:30	0.032778846	09/07/2014 22 00	.	
11/07/2014 21:45	0.038312086	09/07/2014 22:15	.	
11/07/2014 22:00	0.027593853	09/07/2014 22:30	.	
11/07/2014 22:15	0.038312086	09/07/2014 22:45	.	
11/07/2014 22:30	0.030220387	09/07/2014 23 00	.	
11/07/2014 22:45	0.027319313	09/07/2014 23:15	.	
11/07/2014 23:00	0.037956585	09/07/2014 23:30	.	
11/07/2014 23:15	0.041341171	09/07/2014 23:45	.	
11/07/2014 23:30	0.041824684	10/07/2014 00 00	.	
11/07/2014 23:45	0.039523251	10/07/2014 00:15	.	
12/07/2014 00:00	0.03572022	10/07/2014 00:30	.	
12/07/2014 00:15	0.045916828	10/07/2014 00:45	.	
12/07/2014 00:30	0.038231544	10/07/2014 01 00	.	
12/07/2014 00:45	0.044641704	10/07/2014 01:15	.	
12/07/2014 01:00	0.04023062	10/07/2014 01:30	.	
12/07/2014 01:15	0.037136493	10/07/2014 01:45	.	
12/07/2014 01:30	0.043103521	10/07/2014 02 00	0	2
12/07/2014 01:45	0.037087033	10/07/2014 02:15	.	
12/07/2014 02:00	0.036399966	10/07/2014 02:30	.	
12/07/2014 02:15	0.039522314	10/07/2014 02:45	.	
12/07/2014 02:30	0.033880519	10/07/2014 03 00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
12/07/2014 02:45	0.038814982	10/07/2014 03:15	.	
12/07/2014 03:00	0.035499447	10/07/2014 03:30	.	
12/07/2014 03:15	0.043569096	10/07/2014 03:45	.	
12/07/2014 03:30	0.035928722	10/07/2014 04 00	.	
12/07/2014 03:45	0.034308656	10/07/2014 04:15	.	
12/07/2014 04:00	0.031453909	10/07/2014 04:30	.	
12/07/2014 04:15	0.025874698	10/07/2014 04:45	.	
12/07/2014 04:30	0.03132554	10/07/2014 05 00	.	
12/07/2014 04:45	0.031006959	10/07/2014 05:15	.	
12/07/2014 05:00	0.035768261	10/07/2014 05:30	.	
12/07/2014 05:15	0.035179259	10/07/2014 05:45	.	
12/07/2014 05:30	0.906191578	10/07/2014 06 00	.	
12/07/2014 05:45	0.7660085	10/07/2014 06:15	.	
12/07/2014 06:00	0.520778947	10/07/2014 06:30	.	
12/07/2014 06:15	0.428351947	10/07/2014 06:45	.	
12/07/2014 06:30	0.356427667	10/07/2014 07 00	.	
12/07/2014 06:45	0.332629844	10/07/2014 07:15	.	
12/07/2014 07:00	0.299915222	10/07/2014 07:30	.	
12/07/2014 07:15	0.271674993	10/07/2014 07:45	.	
12/07/2014 07:30	0.248813811	10/07/2014 08 00	.	
12/07/2014 07:45	0.241132891	10/07/2014 08:15	.	
12/07/2014 08:00	0.227303215	10/07/2014 08:30	.	
12/07/2014 08:15	0.202483763	10/07/2014 08:45	.	
12/07/2014 08:30	0.19701187	10/07/2014 09 00	.	0.4
12/07/2014 08:45	0.187770529	10/07/2014 09:15	.	
12/07/2014 09:00	0.183993273	10/07/2014 09:30	.	
12/07/2014 09:15	0.174624883	10/07/2014 09:45	.	
12/07/2014 09:30	0.166395391	10/07/2014 10 00	.	
12/07/2014 09:45	0.159362785	10/07/2014 10:15	.	
12/07/2014 10:00	0.161937282	10/07/2014 10:30	.	
12/07/2014 10:15	0.15938719	10/07/2014 10:45	.	
12/07/2014 10:30	0.154873354	10/07/2014 11 00	.	
12/07/2014 10:45	0.157192405	10/07/2014 11:15	.	
12/07/2014 11:00	0.148576446	10/07/2014 11:30	.	
12/07/2014 11:15	0.149396412	10/07/2014 11:45	.	
12/07/2014 11:30	0.136515495	10/07/2014 12 00	.	
12/07/2014 11:45	0.130306906	10/07/2014 12:15	.	
12/07/2014 12:00	0.13117298	10/07/2014 12:30	.	
12/07/2014 12:15	0.115949625	10/07/2014 12:45	.	
12/07/2014 12:30	0.124961935	10/07/2014 13 00	.	
12/07/2014 12:45	0.115552272	10/07/2014 13:15	.	
12/07/2014 13:00	0.107414166	10/07/2014 13:30	.	
12/07/2014 13:15	0.105509248	10/07/2014 13:45	.	
12/07/2014 13:30	0.103970639	10/07/2014 14 00	.	
12/07/2014 13:45	0.107353627	10/07/2014 14:15	.	
12/07/2014 14:00	0.098543185	10/07/2014 14:30	.	
12/07/2014 14:15	0.090198629	10/07/2014 14:45	.	
12/07/2014 14:30	0.092473323	10/07/2014 15 00	.	
12/07/2014 14:45	0.093032264	10/07/2014 15:15	.	
12/07/2014 15:00	0.088826164	10/07/2014 15:30	.	
12/07/2014 15:15	0.094915911	10/07/2014 15:45	.	
12/07/2014 15:30	0.099475305	10/07/2014 16 00	.	
12/07/2014 15:45	0.095905291	10/07/2014 16:15	.	
12/07/2014 16:00	0.089223114	10/07/2014 16:30	.	
12/07/2014 16:15	0.092118171	10/07/2014 16:45	.	
12/07/2014 16:30	0.094874971	10/07/2014 17 00	.	
12/07/2014 16:45	0.084455842	10/07/2014 17:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
12/07/2014 17:00	0.077264909	10/07/2014 17:30	.	
12/07/2014 17:15	0.074684922	10/07/2014 17:45	.	
12/07/2014 17:30	0.069941815	10/07/2014 18 00	.	
12/07/2014 17:45	0.070380155	10/07/2014 18:15	.	
12/07/2014 18:00	0.079259251	10/07/2014 18:30	.	
12/07/2014 18:15	0.079981727	10/07/2014 18:45	.	
12/07/2014 18:30	0.088549001	10/07/2014 19 00	.	
12/07/2014 18:45	0.074013924	10/07/2014 19:15	.	
12/07/2014 19:00	0.083594105	10/07/2014 19:30	.	
12/07/2014 19:15	0.073479446	10/07/2014 19:45	.	
12/07/2014 19:30	0.080847338	10/07/2014 20 00	0 2	
12/07/2014 19:45	0.074383479	10/07/2014 20:15	3 2	
12/07/2014 20:00	0.071312019	10/07/2014 20:30	1 6	
12/07/2014 20:15	0.074740678	10/07/2014 20:45	0 8	
12/07/2014 20:30	0.075467432	10/07/2014 21 00	0 6	
12/07/2014 20:45	0.071626336	10/07/2014 21:15	0 6	
12/07/2014 21:00	0.072357378	10/07/2014 21:30	0 8	
12/07/2014 21:15	0.077647693	10/07/2014 21:45	0 2	
12/07/2014 21:30	0.074383479	10/07/2014 22 00	0 2	
12/07/2014 21:45	0.07313073	10/07/2014 22:15	0 2	
12/07/2014 22:00	0.073844677	10/07/2014 22:30	.	
12/07/2014 22:15	0.07741441	10/07/2014 22:45	0 2	
12/07/2014 22:30	0.073844677	10/07/2014 23 00	.	
12/07/2014 22:45	0.078842303	10/07/2014 23:15	.	
12/07/2014 23:00	0.080129132	10/07/2014 23:30	.	
12/07/2014 23:15	0.077256305	10/07/2014 23:45	.	
12/07/2014 23:30	0.084438371	11/07/2014 00 00	0 2	
12/07/2014 23:45	0.08624716	11/07/2014 00:15	.	
13/07/2014 00:00	0.086588243	11/07/2014 00:30	0 2	
13/07/2014 00:15	0.085383651	11/07/2014 00:45	.	
13/07/2014 00:30	0.082171926	11/07/2014 01 00	.	
13/07/2014 00:45	0.085044121	11/07/2014 01:15	.	
13/07/2014 01:00	0.086404612	11/07/2014 01:30	.	
13/07/2014 01:15	0.085634579	11/07/2014 01:45	.	
13/07/2014 01:30	0.086739758	11/07/2014 02 00	.	
13/07/2014 01:45	0.070965135	11/07/2014 02:15	.	
13/07/2014 02:00	0.079101201	11/07/2014 02:30	.	
13/07/2014 02:15	0.07098889	11/07/2014 02:45	.	
13/07/2014 02:30	0.064527508	11/07/2014 03 00	.	
13/07/2014 02:45	0.063561721	11/07/2014 03:15	.	
13/07/2014 03:00	0.064657122	11/07/2014 03:30	.	
13/07/2014 03:15	0.074371705	11/07/2014 03:45	.	
13/07/2014 03:30	0.063682295	11/07/2014 04 00	.	
13/07/2014 03:45	0.056038583	11/07/2014 04:15	.	
13/07/2014 04:00	0.071395698	11/07/2014 04:30	.	
13/07/2014 04:15	0.06488949	11/07/2014 04:45	.	
13/07/2014 04:30	0.055162846	11/07/2014 05 00	0 2	
13/07/2014 04:45	0.058004303	11/07/2014 05:15	.	
13/07/2014 05:00	0.065867735	11/07/2014 05:30	.	
13/07/2014 05:15	0.067389494	11/07/2014 05:45	.	
13/07/2014 05:30	0.087654516	11/07/2014 06 00	.	
13/07/2014 05:45	0.105372153	11/07/2014 06:15	.	
13/07/2014 06:00	0.108212844	11/07/2014 06:30	.	
13/07/2014 06:15	0.121519858	11/07/2014 06:45	.	
13/07/2014 06:30	0.109732922	11/07/2014 07 00	.	
13/07/2014 06:45	0.107176246	11/07/2014 07:15	.	
13/07/2014 07:00	0.100425372	11/07/2014 07:30	.	

G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
13/07/2014 07:15	0.088402342	11/07/2014 07:45	.		
13/07/2014 07:30	0.090815967	11/07/2014 08 00	.		
13/07/2014 07:45	0.089158419	11/07/2014 08:15	.		
13/07/2014 08:00	0.089638109	11/07/2014 08:30	.		
13/07/2014 08:15	0.083112786	11/07/2014 08:45	.		
13/07/2014 08:30	0.081955788	11/07/2014 09 00	.		9.2
13/07/2014 08:45	0.071709092	11/07/2014 09:15	.		
13/07/2014 09:00	0.080067815	11/07/2014 09:30	.		
13/07/2014 09:15	0.072147828	11/07/2014 09:45	.		
13/07/2014 09:30	0.080236541	11/07/2014 10 00	.		
13/07/2014 09:45	0.078962664	11/07/2014 10:15	.		
13/07/2014 10:00	0.085634579	11/07/2014 10:30	.		
13/07/2014 10:15	0.094955614	11/07/2014 10:45	.		
13/07/2014 10:30	0.09383312	11/07/2014 11 00	0 2		
13/07/2014 10:45	0.097837398	11/07/2014 11:15	.		
13/07/2014 11:00	0.087630262	11/07/2014 11:30	.		
13/07/2014 11:15	0.086822033	11/07/2014 11:45	.		
13/07/2014 11:30	0.071996614	11/07/2014 12 00	.		
13/07/2014 11:45	0.073088419	11/07/2014 12:15	.		
13/07/2014 12:00	0.056547961	11/07/2014 12:30	.		
13/07/2014 12:15	0.071500986	11/07/2014 12:45	.		
13/07/2014 12:30	0.062715589	11/07/2014 13 00	.		
13/07/2014 12:45	0.060155329	11/07/2014 13:15	.		
13/07/2014 13:00	0.063867986	11/07/2014 13:30	.		
13/07/2014 13:15	0.054243566	11/07/2014 13:45	.		
13/07/2014 13:30	0.048238512	11/07/2014 14 00	.		
13/07/2014 13:45	0.046650121	11/07/2014 14:15	.		
13/07/2014 14:00	0.056297044	11/07/2014 14:30	.		
13/07/2014 14:15	0.143924463	11/07/2014 14:45	.		
13/07/2014 14:30	0.960306874	11/07/2014 15 00	.		
13/07/2014 14:45	0.502715012	11/07/2014 15:15	.		
13/07/2014 15:00	0.396464856	11/07/2014 15:30	.		
13/07/2014 15:15	0.342391982	11/07/2014 15:45	.		
13/07/2014 15:30	0.295290829	11/07/2014 16 00	.		
13/07/2014 15:45	0.268427955	11/07/2014 16:15	.		
13/07/2014 16:00	0.243973073	11/07/2014 16:30	.		
13/07/2014 16:15	0.205710533	11/07/2014 16:45	.		
13/07/2014 16:30	0.200788606	11/07/2014 17 00	.		
13/07/2014 16:45	0.197544641	11/07/2014 17:15	.		
13/07/2014 17:00	0.180218894	11/07/2014 17:30	.		
13/07/2014 17:15	0.16467657	11/07/2014 17:45	.		
13/07/2014 17:30	0.148450827	11/07/2014 18 00	.		
13/07/2014 17:45	0.139102907	11/07/2014 18:15	.		
13/07/2014 18:00	0.148576446	11/07/2014 18:30	.		
13/07/2014 18:15	0.224658089	11/07/2014 18:45	.		
13/07/2014 18:30	0.26280571	11/07/2014 19 00	.		
13/07/2014 18:45	0.430544028	11/07/2014 19:15	.		
13/07/2014 19:00	0.723970762	11/07/2014 19:30	.		
13/07/2014 19:15	0.570542857	11/07/2014 19:45	.		
13/07/2014 19:30	0.429232874	11/07/2014 20 00	.		
13/07/2014 19:45	0.388375126	11/07/2014 20:15	.		
13/07/2014 20:00	0.335656003	11/07/2014 20:30	0 2		
13/07/2014 20:15	0.296241314	11/07/2014 20:45	.		
13/07/2014 20:30	0.271630547	11/07/2014 21 00	.		
13/07/2014 20:45	0.25086571	11/07/2014 21:15	.		
13/07/2014 21:00	0.22621398	11/07/2014 21:30	.		
13/07/2014 21:15	0.220759133	11/07/2014 21:45	.		

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
13/07/2014 21:30	0.19276764	11/07/2014 22 00	.	
13/07/2014 21:45	0.19000312	11/07/2014 22:15	.	
13/07/2014 22:00	0.174382231	11/07/2014 22:30	.	
13/07/2014 22:15	0.168237861	11/07/2014 22:45	.	
13/07/2014 22:30	0.152962549	11/07/2014 23 00	.	
13/07/2014 22:45	0.153557101	11/07/2014 23:15	.	
13/07/2014 23:00	0.145600635	11/07/2014 23:30	.	
13/07/2014 23:15	0.138216719	11/07/2014 23:45	.	
13/07/2014 23:30	0.137582362	12/07/2014 00 00	.	
13/07/2014 23:45	0.137638563	12/07/2014 00:15	.	
14/07/2014 00:00	0.136080122	12/07/2014 00:30	.	
14/07/2014 00:15	0.134782849	12/07/2014 00:45	.	
14/07/2014 00:30	0.128433575	12/07/2014 01 00	.	
14/07/2014 00:45	0.129415168	12/07/2014 01:15	.	
14/07/2014 01:00	0.13084258	12/07/2014 01:30	.	
14/07/2014 01:15	0.117214773	12/07/2014 01:45	.	
14/07/2014 01:30	0.116997379	12/07/2014 02 00	.	
14/07/2014 01:45	0.110940838	12/07/2014 02:15	.	
14/07/2014 02:00	0.108641353	12/07/2014 02:30	.	
14/07/2014 02:15	0.100913775	12/07/2014 02:45	.	
14/07/2014 02:30	0.100886828	12/07/2014 03 00	.	
14/07/2014 02:45	0.099122728	12/07/2014 03:15	.	
14/07/2014 03:00	0.094915911	12/07/2014 03:30	.	
14/07/2014 03:15	0.091242046	12/07/2014 03:45	.	
14/07/2014 03:30	0.089411576	12/07/2014 04 00	.	
14/07/2014 03:45	0.093831192	12/07/2014 04:15	.	
14/07/2014 04:00	0.083324481	12/07/2014 04:30	.	
14/07/2014 04:15	0.080841921	12/07/2014 04:45	.	
14/07/2014 04:30	0.079710945	12/07/2014 05 00	.	
14/07/2014 04:45	0 0763696	12/07/2014 05:15	5 8	
14/07/2014 05:00	0.073618503	12/07/2014 05:30	0.4	
14/07/2014 05:15	0.078374447	12/07/2014 05:45	0.4	
14/07/2014 05:30	0.084188478	12/07/2014 06 00	0 2	
14/07/2014 05:45	0.082442554	12/07/2014 06:15	0 6	
14/07/2014 06:00	0.079522749	12/07/2014 06:30	.	
14/07/2014 06:15	0.093591506	12/07/2014 06:45	.	
14/07/2014 06:30	0.088872444	12/07/2014 07 00	.	
14/07/2014 06:45	0.089023674	12/07/2014 07:15	.	
14/07/2014 07:00	0.093928285	12/07/2014 07:30	.	
14/07/2014 07:15	0.08598496	12/07/2014 07:45	.	
14/07/2014 07:30	0.076559854	12/07/2014 08 00	.	
14/07/2014 07:45	0.085516119	12/07/2014 08:15	.	
14/07/2014 08:00	0.085641986	12/07/2014 08:30	.	
14/07/2014 08:15	0.081129872	12/07/2014 08:45	.	
14/07/2014 08:30	0.081129872	12/07/2014 09 00	.	7.8
14/07/2014 08:45	0.078936748	12/07/2014 09:15	.	
14/07/2014 09:00	0.086978201	12/07/2014 09:30	.	
14/07/2014 09:15	0.088440283	12/07/2014 09:45	.	
14/07/2014 09:30	0.089171325	12/07/2014 10 00	.	
14/07/2014 09:45	0.080067815	12/07/2014 10:15	.	
14/07/2014 10:00	0.098251885	12/07/2014 10:30	.	
14/07/2014 10:15	0.095645004	12/07/2014 10:45	.	
14/07/2014 10:30	0.100840351	12/07/2014 11 00	.	
14/07/2014 10:45	0.098383691	12/07/2014 11:15	.	
14/07/2014 11:00	0.091956177	12/07/2014 11:30	.	
14/07/2014 11:15	0.09510655	12/07/2014 11:45	.	
14/07/2014 11:30	0.096034121	12/07/2014 12 00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
14/07/2014 11:45	0.083512792	12/07/2014 12:15	.	
14/07/2014 12:00	0.080459226	12/07/2014 12:30	.	
14/07/2014 12:15	0.073088419	12/07/2014 12:45	0 2	
14/07/2014 12:30	0.075819892	12/07/2014 13 00	.	
14/07/2014 12:45	0.076300687	12/07/2014 13:15	.	
14/07/2014 13:00	0 0744986	12/07/2014 13:30	.	
14/07/2014 13:15	0.067394667	12/07/2014 13:45	.	
14/07/2014 13:30	0.060767689	12/07/2014 14 00	.	
14/07/2014 13:45	0.063488492	12/07/2014 14:15	.	
14/07/2014 14:00	0.071875149	12/07/2014 14:30	.	
14/07/2014 14:15	0.078551953	12/07/2014 14:45	.	
14/07/2014 14:30	0.074889778	12/07/2014 15 00	.	
14/07/2014 14:45	0.085471596	12/07/2014 15:15	.	
14/07/2014 15:00	0.076031863	12/07/2014 15:30	.	
14/07/2014 15:15	0 0858731	12/07/2014 15:45	.	
14/07/2014 15:30	0.064541644	12/07/2014 16 00	.	
14/07/2014 15:45	0.072188572	12/07/2014 16:15	.	
14/07/2014 16:00	0.063411164	12/07/2014 16:30	.	
14/07/2014 16:15	0.060334282	12/07/2014 16:45	.	
14/07/2014 16:30	0.073450996	12/07/2014 17 00	.	
14/07/2014 16:45	0.057660185	12/07/2014 17:15	.	
14/07/2014 17:00	0.068451561	12/07/2014 17:30	.	
14/07/2014 17:15	0.067181988	12/07/2014 17:45	.	
14/07/2014 17:30	0.065277627	12/07/2014 18 00	.	
14/07/2014 17:45	0.074864238	12/07/2014 18:15	.	
14/07/2014 18:00	0.063643392	12/07/2014 18:30	.	
14/07/2014 18:15	0.060510116	12/07/2014 18:45	.	
14/07/2014 18:30	0.059256806	12/07/2014 19 00	.	
14/07/2014 18:45	0.060510116	12/07/2014 19:15	.	
14/07/2014 19:00	0.065403496	12/07/2014 19:30	0.4	
14/07/2014 19:15	0.063511348	12/07/2014 19:45	.	
14/07/2014 19:30	0.057834904	12/07/2014 20 00	.	
14/07/2014 19:45	0.066034213	12/07/2014 20:15	.	
14/07/2014 20:00	0.065277627	12/07/2014 20:30	0 2	
14/07/2014 20:15	0.068340057	12/07/2014 20:45	0 2	
14/07/2014 20:30	0.059395914	12/07/2014 21 00	.	
14/07/2014 20:45	0.061468906	12/07/2014 21:15	.	
14/07/2014 21:00	0.061468906	12/07/2014 21:30	.	
14/07/2014 21:15	0.066547201	12/07/2014 21:45	.	
14/07/2014 21:30	0.074864238	12/07/2014 22 00	.	
14/07/2014 21:45	0.059727052	12/07/2014 22:15	.	
14/07/2014 22:00	0.058630151	12/07/2014 22:30	.	
14/07/2014 22:15	0.060988484	12/07/2014 22:45	.	
14/07/2014 22:30	0.06273848	12/07/2014 23 00	.	
14/07/2014 22:45	0.06770119	12/07/2014 23:15	.	
14/07/2014 23:00	0.066423455	12/07/2014 23:30	.	
14/07/2014 23:15	0.061312516	12/07/2014 23:45	.	
14/07/2014 23:30	0.06514572	13/07/2014 00 00	.	
14/07/2014 23:45	0.06835114	13/07/2014 00:15	.	
15/07/2014 00:00	0.075607304	13/07/2014 00:30	.	
15/07/2014 00:15	0.075892599	13/07/2014 00:45	.	
15/07/2014 00:30	0.080074595	13/07/2014 01 00	.	
15/07/2014 00:45	0.065341508	13/07/2014 01:15	.	
15/07/2014 01:00	0.070861466	13/07/2014 01:30	.	
15/07/2014 01:15	0.067816775	13/07/2014 01:45	.	
15/07/2014 01:30	0.052430934	13/07/2014 02 00	.	
15/07/2014 01:45	0.044894511	13/07/2014 02:15	0.4	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
15/07/2014 02:00	0.042237808	13/07/2014 02:30	0 2	
15/07/2014 02:15	0.044325315	13/07/2014 02:45	0 2	
15/07/2014 02:30	0.039389751	13/07/2014 03 00	.	
15/07/2014 02:45	0.038082785	13/07/2014 03:15	2.4	
15/07/2014 03:00	0.037959836	13/07/2014 03:30	0 8	
15/07/2014 03:15	0.041474712	13/07/2014 03:45	0 2	
15/07/2014 03:30	0.036193049	13/07/2014 04 00	.	
15/07/2014 03:45	0.037718222	13/07/2014 04:15	.	
15/07/2014 04:00	0.033606751	13/07/2014 04:30	0 2	
15/07/2014 04:15	0.034650336	13/07/2014 04:45	2.4	
15/07/2014 04:30	0.030196437	13/07/2014 05 00	0 2	
15/07/2014 04:45	0.032882638	13/07/2014 05:15	.	
15/07/2014 05:00	0.030601607	13/07/2014 05:30	.	
15/07/2014 05:15	0.027474763	13/07/2014 05:45	.	
15/07/2014 05:30	0.032766364	13/07/2014 06 00	.	
15/07/2014 05:45	0.025715818	13/07/2014 06:15	.	
15/07/2014 06:00	0.025441768	13/07/2014 06:30	.	
15/07/2014 06:15	0.023874844	13/07/2014 06:45	0 2	
15/07/2014 06:30	0.027792154	13/07/2014 07 00	.	
15/07/2014 06:45	0.026788589	13/07/2014 07:15	0 2	
15/07/2014 07:00	0.030690198	13/07/2014 07:30	.	
15/07/2014 07:15	0.031233711	13/07/2014 07:45	0 2	
15/07/2014 07:30	0.034224207	13/07/2014 08 00	.	
15/07/2014 07:45	0.035155448	13/07/2014 08:15	.	
15/07/2014 08:00	0.039269447	13/07/2014 08:30	.	
15/07/2014 08:15	0.041154055	13/07/2014 08:45	.	
15/07/2014 08:30	0.045050928	13/07/2014 09 00	.	
15/07/2014 08:45	0.043266845	13/07/2014 09:15	.	
15/07/2014 09:00	0.040189154	13/07/2014 09:30	.	
15/07/2014 09:15	0.046044416	13/07/2014 09:45	.	
15/07/2014 09:30	0.043103521	13/07/2014 10 00	.	
15/07/2014 09:45	0.045384639	13/07/2014 10:15	.	
15/07/2014 10:00	0.049838438	13/07/2014 10:30	.	
15/07/2014 10:15	0.046910415	13/07/2014 10:45	.	
15/07/2014 10:30	0.044445542	13/07/2014 11 00	.	
15/07/2014 10:45	0.040993703	13/07/2014 11:15	.	
15/07/2014 11:00	0.046598193	13/07/2014 11:30	.	
15/07/2014 11:15	0.048264687	13/07/2014 11:45	.	
15/07/2014 11:30	0.057942461	13/07/2014 12 00	0.4	
15/07/2014 11:45	0.046941263	13/07/2014 12:15	0 6	
15/07/2014 12:00	0.058282286	13/07/2014 12:30	.	
15/07/2014 12:15	0.043706799	13/07/2014 12:45	.	
15/07/2014 12:30	0.041127126	13/07/2014 13 00	.	
15/07/2014 12:45	0.045876375	13/07/2014 13:15	.	
15/07/2014 13:00	0.044050698	13/07/2014 13:30	.	
15/07/2014 13:15	0.040756742	13/07/2014 13:45	.	
15/07/2014 13:30	0.042985346	13/07/2014 14 00	.	
15/07/2014 13:45	0.042209625	13/07/2014 14:15	5	
15/07/2014 14:00	0.046719961	13/07/2014 14:30	.	
15/07/2014 14:15	0.04209913	13/07/2014 14:45	.	
15/07/2014 14:30	0.038067999	13/07/2014 15 00	.	
15/07/2014 14:45	0.037247491	13/07/2014 15:15	.	
15/07/2014 15:00	0.040558597	13/07/2014 15:30	.	
15/07/2014 15:15	0.040178378	13/07/2014 15:45	.	
15/07/2014 15:30	0.039723913	13/07/2014 16 00	.	
15/07/2014 15:45	0.036643933	13/07/2014 16:15	.	
15/07/2014 16:00	0.036739941	13/07/2014 16:30	.	

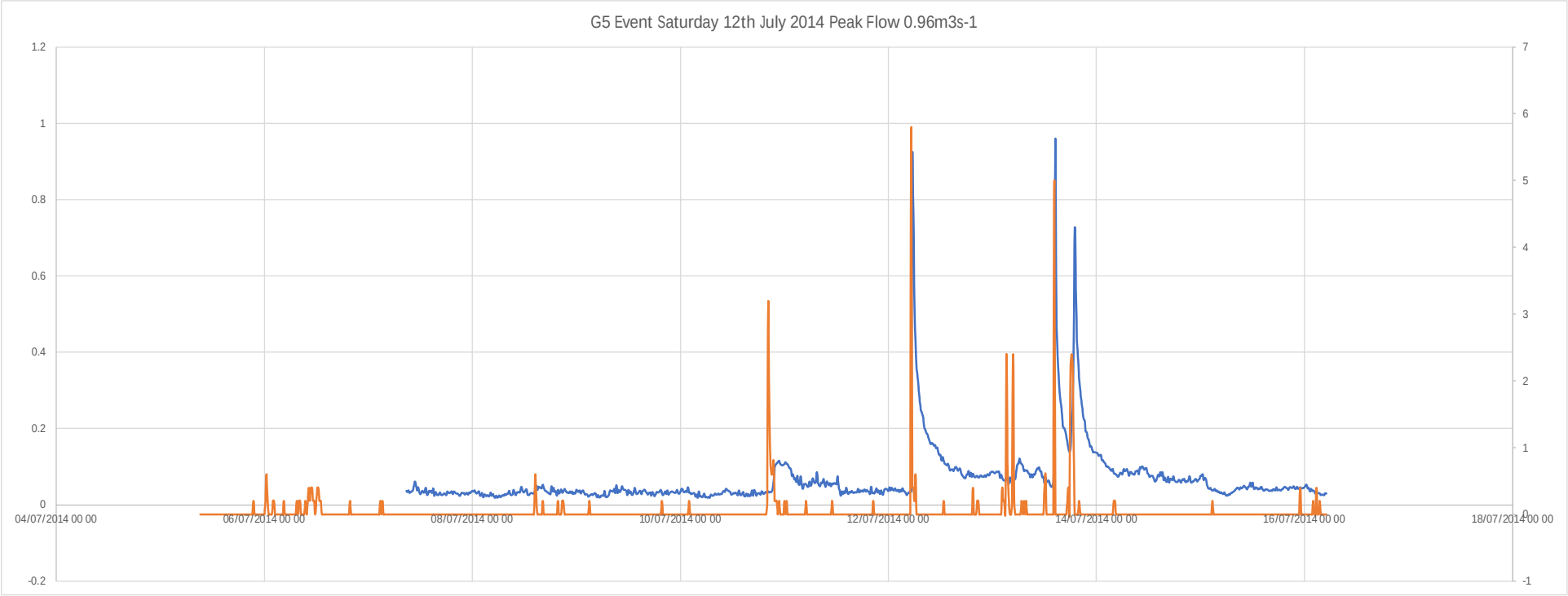
G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
15/07/2014 16:15	0.038081883	13/07/2014 16:45	.	
15/07/2014 16:30	0.036739941	13/07/2014 17 00	.	
15/07/2014 16:45	0.04070189	13/07/2014 17:15	0 2	
15/07/2014 17:00	0.040251006	13/07/2014 17:30	0.4	
15/07/2014 17:15	0.037545701	13/07/2014 17:45	.	
15/07/2014 17:30	0.045631962	13/07/2014 18 00	2 2	
15/07/2014 17:45	0.038170813	13/07/2014 18:15	2.4	
15/07/2014 18:00	0.038632474	13/07/2014 18:30	2 2	
15/07/2014 18:15	0.039555796	13/07/2014 18:45	1	
15/07/2014 18:30	0.037137448	13/07/2014 19 00	.	
15/07/2014 18:45	0.041060632	13/07/2014 19:15	.	
15/07/2014 19:00	0.041824684	13/07/2014 19:30	.	
15/07/2014 19:15	0.045541811	13/07/2014 19:45	.	
15/07/2014 19:30	0.046864212	13/07/2014 20 00	0 2	
15/07/2014 19:45	0.044270886	13/07/2014 20:15	.	
15/07/2014 20:00	0.043152045	13/07/2014 20:30	.	
15/07/2014 20:15	0.039465206	13/07/2014 20:45	.	
15/07/2014 20:30	0.044560197	13/07/2014 21 00	.	
15/07/2014 20:45	0.046498559	13/07/2014 21:15	.	
15/07/2014 21:00	0.043932288	13/07/2014 21:30	.	
15/07/2014 21:15	0.044958797	13/07/2014 21:45	.	
15/07/2014 21:30	0.048636189	13/07/2014 22 00	.	
15/07/2014 21:45	0.04264629	13/07/2014 22:15	.	
15/07/2014 22:00	0.041258762	13/07/2014 22:30	.	
15/07/2014 22:15	0.046864212	13/07/2014 22:45	.	
15/07/2014 22:30	0.042379535	13/07/2014 23 00	.	
15/07/2014 22:45	0.042877833	13/07/2014 23:15	.	
15/07/2014 23:00	0.045867617	13/07/2014 23:30	.	
15/07/2014 23:15	0.042985346	13/07/2014 23:45	.	
15/07/2014 23:30	0.043087395	14/07/2014 00 00	.	
15/07/2014 23:45	0.044669308	14/07/2014 00:15	.	
16/07/2014 00:00	0.04564177	14/07/2014 00:30	.	
16/07/2014 00:15	0.051582781	14/07/2014 00:45	.	
16/07/2014 00:30	0.052122617	14/07/2014 01 00	.	
16/07/2014 00:45	0.042637094	14/07/2014 01:15	.	
16/07/2014 01:00	0.043874428	14/07/2014 01:30	.	
16/07/2014 01:15	0.035055511	14/07/2014 01:45	.	
16/07/2014 01:30	0.041790203	14/07/2014 02 00	.	
16/07/2014 01:45	0.03608819	14/07/2014 02:15	.	
16/07/2014 02:00	0.037718222	14/07/2014 02:30	.	
16/07/2014 02:15	0.035339333	14/07/2014 02:45	.	
16/07/2014 02:30	0.02881437	14/07/2014 03 00	.	
16/07/2014 02:45	0.029058348	14/07/2014 03:15	.	
16/07/2014 03:00	0.030099182	14/07/2014 03:30	.	
16/07/2014 03:15	0.031006959	14/07/2014 03:45	.	
16/07/2014 03:30	0.029886339	14/07/2014 04 00	0 2	
16/07/2014 03:45	0.025194516	14/07/2014 04:15	0 2	
16/07/2014 04:00	0.027008692	14/07/2014 04:30	.	
16/07/2014 04:15	0.026722819	14/07/2014 04:45	.	
16/07/2014 04:30	0.02489871	14/07/2014 05 00	.	
16/07/2014 04:45	0.030354263	14/07/2014 05:15	.	
16/07/2014 05:00	0.030036809	14/07/2014 05:30	.	
		14/07/2014 05:45	.	
		14/07/2014 06 00	.	
		14/07/2014 06:15	.	
		14/07/2014 06:30	.	
		14/07/2014 06:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
		14/07/2014 07 00	.	
		14/07/2014 07:15	.	
		14/07/2014 07:30	.	
		14/07/2014 07:45	.	
		14/07/2014 08 00	.	
		14/07/2014 08:15	.	
		14/07/2014 08:30	.	
		14/07/2014 08:45	.	
		14/07/2014 09 00	.	
		14/07/2014 09:15	.	
		14/07/2014 09:30	.	
		14/07/2014 09:45	.	
		14/07/2014 10 00	.	
		14/07/2014 10:15	.	
		14/07/2014 10:30	.	
		14/07/2014 10:45	.	
		14/07/2014 11 00	.	
		14/07/2014 11:15	.	
		14/07/2014 11:30	.	
		14/07/2014 11:45	.	
		14/07/2014 12 00	.	
		14/07/2014 12:15	.	
		14/07/2014 12:30	.	
		14/07/2014 12:45	.	
		14/07/2014 13 00	.	
		14/07/2014 13:15	.	
		14/07/2014 13:30	.	
		14/07/2014 13:45	.	
		14/07/2014 14 00	.	
		14/07/2014 14:15	.	
		14/07/2014 14:30	.	
		14/07/2014 14:45	.	
		14/07/2014 15 00	.	
		14/07/2014 15:15	.	
		14/07/2014 15:30	.	
		14/07/2014 15:45	.	
		14/07/2014 16 00	.	
		14/07/2014 16:15	.	
		14/07/2014 16:30	.	
		14/07/2014 16:45	.	
		14/07/2014 17 00	.	
		14/07/2014 17:15	.	
		14/07/2014 17:30	.	
		14/07/2014 17:45	.	
		14/07/2014 18 00	.	
		14/07/2014 18:15	.	
		14/07/2014 18:30	.	
		14/07/2014 18:45	.	
		14/07/2014 19 00	.	
		14/07/2014 19:15	.	
		14/07/2014 19:30	.	
		14/07/2014 19:45	.	
		14/07/2014 20 00	.	
		14/07/2014 20:15	.	
		14/07/2014 20:30	.	
		14/07/2014 20:45	.	
		14/07/2014 21 00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
		14/07/2014 21:15	.	
		14/07/2014 21:30	.	
		14/07/2014 21:45	.	
		14/07/2014 22 00	.	
		14/07/2014 22:15	.	
		14/07/2014 22:30	.	
		14/07/2014 22:45	.	
		14/07/2014 23 00	.	
		14/07/2014 23:15	.	
		14/07/2014 23:30	.	
		14/07/2014 23:45	.	
		15/07/2014 00 00	.	
		15/07/2014 00:15	.	
		15/07/2014 00:30	.	
		15/07/2014 00:45	.	
		15/07/2014 01 00	.	
		15/07/2014 01:15	.	
		15/07/2014 01:30	.	
		15/07/2014 01:45	.	
		15/07/2014 02 00	.	
		15/07/2014 02:15	.	
		15/07/2014 02:30	.	
		15/07/2014 02:45	0 2	
		15/07/2014 03 00	.	
		15/07/2014 03:15	.	
		15/07/2014 03:30	.	
		15/07/2014 03:45	.	
		15/07/2014 04 00	.	
		15/07/2014 04:15	.	
		15/07/2014 04:30	.	
		15/07/2014 04:45	.	
		15/07/2014 05 00	.	
		15/07/2014 05:15	.	
		15/07/2014 05:30	.	
		15/07/2014 05:45	.	
		15/07/2014 06 00	.	
		15/07/2014 06:15	.	
		15/07/2014 06:30	.	
		15/07/2014 06:45	.	
		15/07/2014 07 00	.	
		15/07/2014 07:15	.	
		15/07/2014 07:30	.	
		15/07/2014 07:45	.	
		15/07/2014 08 00	.	
		15/07/2014 08:15	.	
		15/07/2014 08:30	.	
		15/07/2014 08:45	.	
		15/07/2014 09 00	.	
		15/07/2014 09:15	.	
		15/07/2014 09:30	.	
		15/07/2014 09:45	.	
		15/07/2014 10 00	.	
		15/07/2014 10:15	.	
		15/07/2014 10:30	.	
		15/07/2014 10:45	.	
		15/07/2014 11 00	.	
		15/07/2014 11:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
		15/07/2014 11:30	.	
		15/07/2014 11:45	.	
		15/07/2014 12 00	.	
		15/07/2014 12:15	.	
		15/07/2014 12:30	.	
		15/07/2014 12:45	.	
		15/07/2014 13 00	.	
		15/07/2014 13:15	.	
		15/07/2014 13:30	.	
		15/07/2014 13:45	.	
		15/07/2014 14 00	.	
		15/07/2014 14:15	.	
		15/07/2014 14:30	.	
		15/07/2014 14:45	.	
		15/07/2014 15 00	.	
		15/07/2014 15:15	.	
		15/07/2014 15:30	.	
		15/07/2014 15:45	.	
		15/07/2014 16 00	.	
		15/07/2014 16:15	.	
		15/07/2014 16:30	.	
		15/07/2014 16:45	.	
		15/07/2014 17 00	.	
		15/07/2014 17:15	.	
		15/07/2014 17:30	.	
		15/07/2014 17:45	.	
		15/07/2014 18 00	.	
		15/07/2014 18:15	.	
		15/07/2014 18:30	.	
		15/07/2014 18:45	.	
		15/07/2014 19 00	.	
		15/07/2014 19:15	.	
		15/07/2014 19:30	.	
		15/07/2014 19:45	.	
		15/07/2014 20 00	.	
		15/07/2014 20:15	.	
		15/07/2014 20:30	.	
		15/07/2014 20:45	.	
		15/07/2014 21 00	.	
		15/07/2014 21:15	.	
		15/07/2014 21:30	.	
		15/07/2014 21:45	.	
		15/07/2014 22 00	.	
		15/07/2014 22:15	.	
		15/07/2014 22:30	.	
		15/07/2014 22:45	.	
		15/07/2014 23 00	0.4	
		15/07/2014 23:15	.	
		15/07/2014 23:30	.	
		15/07/2014 23:45	.	
		16/07/2014 00 00	.	
		16/07/2014 00:15	.	
		16/07/2014 00:30	.	
		16/07/2014 00:45	.	
		16/07/2014 01 00	.	
		16/07/2014 01:15	.	
		16/07/2014 01:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
		16/07/2014 01:45	.	
		16/07/2014 02 00	0 2	
		16/07/2014 02:15	.	
		16/07/2014 02:30	.	
		16/07/2014 02:45	0.4	
		16/07/2014 03 00	.	
		16/07/2014 03:15	.	
		16/07/2014 03:30	0 2	
		16/07/2014 03:45	.	
		16/07/2014 04 00	.	
		16/07/2014 04:15	.	
		16/07/2014 04:30	.	
		16/07/2014 04:45	.	
		16/07/2014 05 00	.	



SAAR	592	mm
AREA	5.04	Km2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capacity in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
08-Jul-14	112.6	mm
15-Jul-14	76.6	mm

Source of Rainfall event data.

Gauge	**Easting**	**Northing**	**Distance from Catchment Centroid (m)**	**Reciprocal**	**Weighting**
Benhall	38166	60602	20912.0		
Soham	23243	62717	6550.0		
Thorpeness	60012	78834	3636.0	0.00028	1.00000
			Total	0.00028	1.00000

TBR RG

Daily RF totals 9am 9am	**Benhall**	**Soham**	**Thorpeness**
Date	**Total RF (mm)**	**Total RF (mm)**	**Total RF (mm)**
10/07/2014			9.2
09/07/2014			0.4
08/07/2014			1.8
07/07/2014			0
06/07/2014			4.2
Total API5 RF			15.6

Rainall Event Depth P (mm)	7.4
Event duration (hours)	1

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**06/07/2014**	**07/07/2014**	**08/07/2014**	**09/07/2014**	**10/07/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.00000	4.2	0	1.8	0.4	9.2
Average Da ly rainfall totals			4.2	0	1.8	0.4	9.2

Gauge	**SAAR**	**Weight**	**06/07/2014**	**07/07/2014**	**08/07/2014**	**09/07/2014**	**10/07/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.00000	0.007094595	0	0.003040541	0.000675676	0.015540541

Gauge	**SAAR**	**Weight**	**06/07/2014**	**07/07/2014**	**08/07/2014**	**09/07/2014**	**10/07/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.0000	0.007094595	0	0.003040541	0.000675676	0.015540541

Gauge	**SAAR**	**Weight**	**06/07/2014**	**07/07/2014**	**08/07/2014**	**09/07/2014**	**10/07/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.00000	4.2	0	1.8	0.4	9.2
Catchment Average Antecedent RF mm			4.2	0	1.8	0.4	9.2

Date	**Catchment Average Antecedent Rainfall (mm)**	
06/07/2014	4.20	d-5
07/07/2014	0.00	d-4
08/07/2014	1.80	d-3
09/07/2014	0.40	d-2
10/07/2014	9.20	d-1

AP 5

7.15	mm	7.150617325	mm / day

CWI Prior to Event July 2014 Event at G5
CWI 125 + API15 - SMD

SMD	112.6	mm
CWI	19.55061732	mm

FEH Parameter									
SPR	39.2	%			P=Storm Depth	0	mm	**URBEXT2000**	
PRrural	12.9	%			SPR	39.21834278		**PR**	13
DPRrain	0.0	%						**DPRrain**	0
DPRcwi	-26.4	CWI	19.55061732					**DPRcwi**	-26.4
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural								**SPR**	39.2
PR	13.2	%						**DPRrain**	0.45(P-40)^0.7
PRrural	12.9	%						**P**	
CWI	19.6	mm						**CWI**	19.6
BF	0.00001		Baseflow equation taken from FEH					**SPR**	39.2
	-1254							**PR**	13.2
	1778.5	524.5	0.005245						
AREA	50.52		**0.2649774**	m3s-1				**SPRHOST**	24.3
SPR	39.2							**Duration (hours)**	1
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}								
SPR =	39.2								
PRrural	12.9								

As URBEXT2000 value is essentially rural the PR is the same as the PRrural value

taken from PR calculations sheet using Thorpeness TBR RG record

DPRrain is 0, as P<40mm

#NUM!

from FEH Catchment descriptors & SPRHOST is the same as SPRcds

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
12/07/2014 05:15	12/07/2014 06:15	1.00	7.2	112.6	19.6	12.9	-26.4	0.0	39.2	13.0	24.3

Site	Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Sizewell	Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	Leis Abbey	24.3	44.8	27.8	51.4
Leiston	Leiston	24.3	44.8	20.7	38.2
Leis Upper	Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	Mins Potters	24.3	44.8	25.3	46.8
				Mean	37.3

SPRHOST is the average of both Leiston and Leiston Abbey catchments 27.8

20.7

24.3

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
02/10/2014 05:30	0.020347017	02/10/2014 05:30	.	
02/10/2014 05:45	0.01119659	02/10/2014 05:45	.	
02/10/2014 06:00	0.038304137	02/10/2014 06:00	.	
02/10/2014 06:15	0.008836577	02/10/2014 06:15	.	
02/10/2014 06:30	0.011046644	02/10/2014 06:30	.	
02/10/2014 06:45	0.01156824	02/10/2014 06:45	.	
02/10/2014 07:00	0.018309612	02/10/2014 07:00	.	
02/10/2014 07:15	0.006528365	02/10/2014 07:15	.	
02/10/2014 07:30	0.010995659	02/10/2014 07:30	.	
02/10/2014 07:45	0.016587682	02/10/2014 07:45	.	
02/10/2014 08:00	0.030389048	02/10/2014 08:00	.	
02/10/2014 08:15	0.009049742	02/10/2014 08:15	.	
02/10/2014 08:30	0.018157686	02/10/2014 08:30	.	
02/10/2014 08:45	0.018944794	02/10/2014 08:45	.	
02/10/2014 09:00	0.02710666	02/10/2014 09:00	.	
02/10/2014 09:15	0.023942531	02/10/2014 09:15	.	
02/10/2014 09:30	0.036238556	02/10/2014 09:30	.	
02/10/2014 09:45	0.035565727	02/10/2014 09:45	.	
02/10/2014 10:00	0.028708247	02/10/2014 10:00	.	
02/10/2014 10:15	0.03191529	02/10/2014 10:15	.	
02/10/2014 10:30	0.02792891	02/10/2014 10:30	.	
02/10/2014 10:45	0.024440828	02/10/2014 10:45	.	
02/10/2014 11:00	0.029136967	02/10/2014 11:00	.	
02/10/2014 11:15	0.028642382	02/10/2014 11:15	.	
02/10/2014 11:30	0.036215029	02/10/2014 11:30	.	
02/10/2014 11:45	0.019311582	02/10/2014 11:45	.	
02/10/2014 12:00	0.027319313	02/10/2014 12:00	.	
02/10/2014 12:15	0.033441674	02/10/2014 12:15	.	
02/10/2014 12:30	0.022725094	02/10/2014 12:30	.	
02/10/2014 12:45	0.023179182	02/10/2014 12:45	.	
02/10/2014 13:00	0.025505559	02/10/2014 13:00	.	
02/10/2014 13:15	0.028937591	02/10/2014 13:15	.	
02/10/2014 13:30	0.024984636	02/10/2014 13:30	.	
02/10/2014 13:45	0.019487944	02/10/2014 13:45	.	
02/10/2014 14:00	0.023568295	02/10/2014 14:00	.	
02/10/2014 14:15	0.019748195	02/10/2014 14:15	.	
02/10/2014 14:30	0.029408685	02/10/2014 14:30	.	
02/10/2014 14:45	0.018248436	02/10/2014 14:45	.	
02/10/2014 15:00	0.022651603	02/10/2014 15:00	.	
02/10/2014 15:15	0.022651603	02/10/2014 15:15	.	
02/10/2014 15:30	0.024165359	02/10/2014 15:30	.	
02/10/2014 15:45	0.021045534	02/10/2014 15:45	.	
02/10/2014 16:00	0.040824507	02/10/2014 16:00	.	
02/10/2014 16:15	0.029582918	02/10/2014 16:15	.	
02/10/2014 16:30	0.027511857	02/10/2014 16:30	.	
02/10/2014 16:45	0.031193583	02/10/2014 16:45	.	
02/10/2014 17:00	0.019307987	02/10/2014 17:00	.	

	DATE TIME
start of event	08/10/2014 08:45
end of event	08/10/2014 12:30
duration hours	3.75
total RF mm	17
SMD W/E AVERAG	**mm**
07-Oct-14	103.0

DATE	API5	Daily Totals
06/10/2014	d-1	5
05/10/2014	d-2	0.2
04/10/2014	d-3	4.2
03/10/2014	d-4	0.4
02/10/2014	d-5	0

SMD data required for w/c 01/10/2014 & w/c 8/10/2014

Event starts	08/10/2014	08:45
Event ends	08/10/2014	12:30

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
02/10/2014 17:15	0.020839851	02/10/2014 17:15	.	
02/10/2014 17:30	0.027389912	02/10/2014 17:30	.	
02/10/2014 17:45	0.02371006	02/10/2014 17:45	.	
02/10/2014 18:00	0.020855532	02/10/2014 18:00	.	
02/10/2014 18:15	0.023961817	02/10/2014 18:15	.	
02/10/2014 18:30	0.027068102	02/10/2014 18:30	.	
02/10/2014 18:45	0.019510338	02/10/2014 18:45	.	
02/10/2014 19:00	0.023568295	02/10/2014 19:00	.	
02/10/2014 19:15	0.020181904	02/10/2014 19:15	.	
02/10/2014 19:30	0.022935997	02/10/2014 19:30	.	
02/10/2014 19:45	0.026706212	02/10/2014 19:45	.	
02/10/2014 20:00	0.028868081	02/10/2014 20:00	.	
02/10/2014 20:15	0.033441674	02/10/2014 20:15	.	
02/10/2014 20:30	0.020328588	02/10/2014 20:30	.	
02/10/2014 20:45	0.032637949	02/10/2014 20:45	.	
02/10/2014 21:00	0.031306196	02/10/2014 21:00	.	
02/10/2014 21:15	0.026169457	02/10/2014 21:15	.	
02/10/2014 21:30	0.025674872	02/10/2014 21:30	.	
02/10/2014 21:45	0.030420397	02/10/2014 21:45	.	
02/10/2014 22:00	0.035403371	02/10/2014 22:00	.	
02/10/2014 22:15	0.027202186	02/10/2014 22:15	.	
02/10/2014 22:30	0.033908479	02/10/2014 22:30	.	
02/10/2014 22:45	0.026932315	02/10/2014 22:45	.	
02/10/2014 23:00	0.031115307	02/10/2014 23:00	.	
02/10/2014 23:15	0.023452063	02/10/2014 23:15	.	
02/10/2014 23:30	0.02590648	02/10/2014 23:30	.	
02/10/2014 23:45	0.032287963	02/10/2014 23:45	.	
03/10/2014 00:00	0.028206227	03/10/2014 00:00	.	
03/10/2014 00:15	0.030365772	03/10/2014 00:15	.	
03/10/2014 00:30	0.030953431	03/10/2014 00:30	.	
03/10/2014 00:45	0.040232224	03/10/2014 00:45	.	
03/10/2014 01:00	0.029848751	03/10/2014 01:00	.	
03/10/2014 01:15	0.029210268	03/10/2014 01:15	.	
03/10/2014 01:30	0.025157891	03/10/2014 01:30	.	
03/10/2014 01:45	0.039263905	03/10/2014 01:45	.	
03/10/2014 02:00	0.02847593	03/10/2014 02:00	.	
03/10/2014 02:15	0.014550613	03/10/2014 02:15	.	
03/10/2014 02:30	0.028112132	03/10/2014 02:30	.	
03/10/2014 02:45	0.020816057	03/10/2014 02:45	.	
03/10/2014 03:00	0.017825798	03/10/2014 03:00	.	
03/10/2014 03:15	0.014093549	03/10/2014 03:15	.	
03/10/2014 03:30	0.018244385	03/10/2014 03:30	.	
03/10/2014 03:45	0.016825632	03/10/2014 03:45	.	
03/10/2014 04:00	0.017607147	03/10/2014 04:00	.	
03/10/2014 04:15	0.020740995	03/10/2014 04:15	.	
03/10/2014 04:30	0.018567366	03/10/2014 04:30	.	
03/10/2014 04:45	0.018353873	03/10/2014 04:45	.	

	DATE TIME

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
03/10/2014 05:00	0.016428921	03/10/2014 05:00	.			
03/10/2014 05:15	0.017378582	03/10/2014 05:15	.			
03/10/2014 05:30	0.012798931	03/10/2014 05:30	.			
03/10/2014 05:45	0.018523495	03/10/2014 05:45	.			
03/10/2014 06:00	0.016233669	03/10/2014 06:00	.			
03/10/2014 06:15	0.013562206	03/10/2014 06:15	.			
03/10/2014 06:30	0.01488896	03/10/2014 06:30	.			
03/10/2014 06:45	0.015072173	03/10/2014 06:45	.			
03/10/2014 07:00	0.020579273	03/10/2014 07:00	.			
03/10/2014 07:15	0.019034247	03/10/2014 07:15	.			
03/10/2014 07:30	0.017834749	03/10/2014 07:30	.			
03/10/2014 07:45	0.06392693	03/10/2014 07:45	.			
03/10/2014 08:00	0.027346348	03/10/2014 08:00	.			
03/10/2014 08:15	0.0215453	03/10/2014 08:15	.			
03/10/2014 08:30	0.027831937	03/10/2014 08:30	.			
03/10/2014 08:45	0.031844824	03/10/2014 08:45	.			
03/10/2014 09:00	0.023201947	03/10/2014 09:00	.	0		
03/10/2014 09:15	0.028990919	03/10/2014 09:15	.			
03/10/2014 09:30	0.029561168	03/10/2014 09:30	.			
03/10/2014 09:45	0.022326029	03/10/2014 09:45	.			
03/10/2014 10:00	0.034948414	03/10/2014 10:00	.			
03/10/2014 10:15	0.026758023	03/10/2014 10:15	.			
03/10/2014 10:30	0.023032699	03/10/2014 10:30	.			
03/10/2014 10:45	0.028095311	03/10/2014 10:45	.			
03/10/2014 11:00	0.030483346	03/10/2014 11:00	.			
03/10/2014 11:15	0.032306509	03/10/2014 11:15	.			
03/10/2014 11:30	0.032527182	03/10/2014 11:30	.			
03/10/2014 11:45	0.028855097	03/10/2014 11:45	.			
03/10/2014 12:00	0.036908332	03/10/2014 12:00	.			
03/10/2014 12:15	0.030137977	03/10/2014 12:15	.			
03/10/2014 12:30	0.041740214	03/10/2014 12:30	.			
03/10/2014 12:45	0.033153948	03/10/2014 12:45	.			
03/10/2014 13:00	0.020393093	03/10/2014 13:00	.			
03/10/2014 13:15	0.018667835	03/10/2014 13:15	.			
03/10/2014 13:30	0.025180287	03/10/2014 13:30	.			
03/10/2014 13:45	0.067140676	03/10/2014 13:45	.			
03/10/2014 14:00	0.026619468	03/10/2014 14:00	.			
03/10/2014 14:15	0.025385264	03/10/2014 14:15	.			
03/10/2014 14:30	0.025606863	03/10/2014 14:30	.			
03/10/2014 14:45	0.022489423	03/10/2014 14:45	.			
03/10/2014 15:00	0.023917977	03/10/2014 15:00	.			
03/10/2014 15:15	0.025560319	03/10/2014 15:15	.			
03/10/2014 15:30	0.024830608	03/10/2014 15:30	.			
03/10/2014 15:45	0.025244302	03/10/2014 15:45	.			
03/10/2014 16:00	0.021764758	03/10/2014 16:00	.			
03/10/2014 16:15	0.044759846	03/10/2014 16:15	.			
03/10/2014 16:30	0.027090947	03/10/2014 16:30	.			

G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
03/10/2014 16:45	0.031703306	03/10/2014 16:45	.		
03/10/2014 17:00	0.026835801	03/10/2014 17:00	.		
03/10/2014 17:15	0.023696313	03/10/2014 17:15	.		
03/10/2014 17:30	0.031115307	03/10/2014 17:30	.		
03/10/2014 17:45	0.034577402	03/10/2014 17:45	.		
03/10/2014 18:00	0.024191117	03/10/2014 18:00	.		
03/10/2014 18:15	0.029423803	03/10/2014 18:15	.		
03/10/2014 18:30	0.025194103	03/10/2014 18:30	.		
03/10/2014 18:45	0.028485165	03/10/2014 18:45	.		
03/10/2014 19:00	0.023933374	03/10/2014 19:00	.		
03/10/2014 19:15	0.038955707	03/10/2014 19:15	.		
03/10/2014 19:30	0.023915371	03/10/2014 19:30	.		
03/10/2014 19:45	0.033984912	03/10/2014 19:45	.		
03/10/2014 20:00	0.023888419	03/10/2014 20:00	.		
03/10/2014 20:15	0.030428848	03/10/2014 20:15	.		
03/10/2014 20:30	0.025437556	03/10/2014 20:30		0 2	
03/10/2014 20:45	0.024879266	03/10/2014 20:45	.		
03/10/2014 21:00	0.028369815	03/10/2014 21:00	.		
03/10/2014 21:15	0.034847852	03/10/2014 21:15	.		
03/10/2014 21:30	0.037007198	03/10/2014 21:30	.		
03/10/2014 21:45	0.032688506	03/10/2014 21:45	.		
03/10/2014 22:00	0.037007198	03/10/2014 22:00	.		
03/10/2014 22:15	0.03214867	03/10/2014 22:15	.		
03/10/2014 22:30	0.031547724	03/10/2014 22:30	.		
03/10/2014 22:45	0.031249747	03/10/2014 22:45	.		
03/10/2014 23:00	0.032002598	03/10/2014 23:00	.		
03/10/2014 23:15	0.024409215	03/10/2014 23:15	.		
03/10/2014 23:30	0.027263651	03/10/2014 23:30	.		
03/10/2014 23:45	0.026229611	03/10/2014 23:45	.		
04/10/2014 00:00	0.036005176	04/10/2014 00:00	.		
04/10/2014 00:15	0.032919379	04/10/2014 00:15	.		
04/10/2014 00:30	0.033538995	04/10/2014 00:30	.		
04/10/2014 00:45	0.041694132	04/10/2014 00:45	.		
04/10/2014 01:00	0.030721366	04/10/2014 01:00	.		
04/10/2014 01:15	0.025195571	04/10/2014 01:15	.		
04/10/2014 01:30	0.035059973	04/10/2014 01:30	.		
04/10/2014 01:45	0.028147797	04/10/2014 01:45	.		
04/10/2014 02:00	0.025868776	04/10/2014 02:00	.		
04/10/2014 02:15	0.031230768	04/10/2014 02:15	.		
04/10/2014 02:30	0.029860913	04/10/2014 02:30	.		
04/10/2014 02:45	0.026089953	04/10/2014 02:45	.		
04/10/2014 03:00	0.018400069	04/10/2014 03:00	.		
04/10/2014 03:15	0.01996651	04/10/2014 03:15	.		
04/10/2014 03:30	0.018238269	04/10/2014 03:30	.		
04/10/2014 03:45	0.015048414	04/10/2014 03:45	.		
04/10/2014 04:00	0.017621714	04/10/2014 04:00	.		
04/10/2014 04:15	0.020515686	04/10/2014 04:15		0 2	

	DATE TIME

G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
04/10/2014 04:30	0.015382882	04/10/2014 04:30	.		
04/10/2014 04:45	0.018441048	04/10/2014 04:45	.		
04/10/2014 05:00	0.018818223	04/10/2014 05:00	.		
04/10/2014 05:15	0.021209333	04/10/2014 05:15	.		
04/10/2014 05:30	0.020974392	04/10/2014 05:30	.		
04/10/2014 05:45	0.017215416	04/10/2014 05:45	.		
04/10/2014 06:00	0.015256761	04/10/2014 06:00	.		
04/10/2014 06:15	0.013298105	04/10/2014 06:15	.		
04/10/2014 06:30	0.016823685	04/10/2014 06:30	.		
04/10/2014 06:45	0.019393916	04/10/2014 06:45	.		
04/10/2014 07:00	0.020974392	04/10/2014 07:00	.		
04/10/2014 07:15	0.021847752	04/10/2014 07:15	.		
04/10/2014 07:30	0.039519351	04/10/2014 07:30	.		
04/10/2014 07:45	0.022823015	04/10/2014 07:45	.		
04/10/2014 08:00	0.018671073	04/10/2014 08:00	.		
04/10/2014 08:15	0.011516335	04/10/2014 08:15	.		
04/10/2014 08:30	0.022630552	04/10/2014 08:30	.		
04/10/2014 08:45	0.017000647	04/10/2014 08:45	.		
04/10/2014 09:00	0.019922253	04/10/2014 09:00	.		0.4
04/10/2014 09:15	0.020584683	04/10/2014 09:15	.		
04/10/2014 09:30	0.022234736	04/10/2014 09:30	.		
04/10/2014 09:45	0.03121835	04/10/2014 09:45	.		
04/10/2014 10:00	0.028575587	04/10/2014 10:00	.		
04/10/2014 10:15	0.026487289	04/10/2014 10:15	.		
04/10/2014 10:30	0.030566187	04/10/2014 10:30	.		
04/10/2014 10:45	0.031443729	04/10/2014 10:45	.		
04/10/2014 11:00	0.030903094	04/10/2014 11:00	.		
04/10/2014 11:15	0.014819142	04/10/2014 11:15	.		
04/10/2014 11:30	0.03148723	04/10/2014 11:30	.		
04/10/2014 11:45	0.042611151	04/10/2014 11:45	.		
04/10/2014 12:00	0.034048549	04/10/2014 12:00	.		
04/10/2014 12:15	0.02806845	04/10/2014 12:15	.		
04/10/2014 12:30	0.033428602	04/10/2014 12:30	.		
04/10/2014 12:45	0.030325456	04/10/2014 12:45	.		
04/10/2014 13:00	0.040949051	04/10/2014 13:00	.		
04/10/2014 13:15	0.029202909	04/10/2014 13:15	.		
04/10/2014 13:30	0.048362512	04/10/2014 13:30	.		
04/10/2014 13:45	0.031149579	04/10/2014 13:45	.		
04/10/2014 14:00	0.033370602	04/10/2014 14:00	.		
04/10/2014 14:15	0.031408451	04/10/2014 14:15	.		
04/10/2014 14:30	0.030566187	04/10/2014 14:30	.		
04/10/2014 14:45	0.027559304	04/10/2014 14:45	0 2		
04/10/2014 15:00	0.030483346	04/10/2014 15:00	.		
04/10/2014 15:15	0.027022699	04/10/2014 15:15	0.4		
04/10/2014 15:30	0.024658429	04/10/2014 15:30	0.4		
04/10/2014 15:45	0.029379681	04/10/2014 15:45	0.4		
04/10/2014 16:00	0.02623218	04/10/2014 16:00	0.6		

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G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
04/10/2014 16:15	0.030953431	04/10/2014 16:15		0.4	
04/10/2014 16:30	0.030820617	04/10/2014 16:30		0.4	
04/10/2014 16:45	0.034807315	04/10/2014 16:45		0.6	
04/10/2014 17:00	0.049888021	04/10/2014 17:00		0 2	
04/10/2014 17:15	0.066754627	04/10/2014 17:15	.		
04/10/2014 17:30	0.07902243	04/10/2014 17:30	.		
04/10/2014 17:45	0.096499559	04/10/2014 17:45	.		
04/10/2014 18:00	0.095215653	04/10/2014 18:00	.		
04/10/2014 18:15	0.080357935	04/10/2014 18:15	.		
04/10/2014 18:30	0.082280181	04/10/2014 18:30	.		
04/10/2014 18:45	0.079587435	04/10/2014 18:45	.		
04/10/2014 19:00	0.074703353	04/10/2014 19:00		0 2	
04/10/2014 19:15	0.064635679	04/10/2014 19:15	.		
04/10/2014 19:30	0.065604853	04/10/2014 19:30	.		
04/10/2014 19:45	0.05816249	04/10/2014 19:45	.		
04/10/2014 20:00	0.05765781	04/10/2014 20:00	.		
04/10/2014 20:15	0.055183204	04/10/2014 20:15	.		
04/10/2014 20:30	0.052834588	04/10/2014 20:30		0 2	
04/10/2014 20:45	0.050878281	04/10/2014 20:45	.		
04/10/2014 21:00	0.052619266	04/10/2014 21:00	.		
04/10/2014 21:15	0.050360225	04/10/2014 21:15	.		
04/10/2014 21:30	0.045286809	04/10/2014 21:30	.		
04/10/2014 21:45	0.040322507	04/10/2014 21:45	.		
04/10/2014 22:00	0.047698173	04/10/2014 22:00	.		
04/10/2014 22:15	0.050800623	04/10/2014 22:15	.		
04/10/2014 22:30	0.042424399	04/10/2014 22:30	.		
04/10/2014 22:45	0.038292911	04/10/2014 22:45	.		
04/10/2014 23:00	0.046178689	04/10/2014 23:00	.		
04/10/2014 23:15	0.047843874	04/10/2014 23:15	.		
04/10/2014 23:30	0.060767689	04/10/2014 23:30	.		
04/10/2014 23:45	0.055679618	04/10/2014 23:45	.		
05/10/2014 00:00	0.05614003	05/10/2014 00:00	.		
05/10/2014 00:15	0.056829942	05/10/2014 00:15	.		
05/10/2014 00:30	0.055105453	05/10/2014 00:30	.		
05/10/2014 00:45	0.055526241	05/10/2014 00:45	.		
05/10/2014 01:00	0.057696957	05/10/2014 01:00	.		
05/10/2014 01:15	0.04896406	05/10/2014 01:15	.		
05/10/2014 01:30	0.053436501	05/10/2014 01:30	.		
05/10/2014 01:45	0.044809917	05/10/2014 01:45	.		
05/10/2014 02:00	0.041622153	05/10/2014 02:00	.		
05/10/2014 02:15	0.033563949	05/10/2014 02:15	.		
05/10/2014 02:30	0.03177569	05/10/2014 02:30	.		
05/10/2014 02:45	0.030045661	05/10/2014 02:45	.		
05/10/2014 03:00	0.034554657	05/10/2014 03:00	.		
05/10/2014 03:15	0.029189589	05/10/2014 03:15	.		
05/10/2014 03:30	0.028607842	05/10/2014 03:30	.		
05/10/2014 03:45	0.026994897	05/10/2014 03:45	.		

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G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
05/10/2014 04:00	0.022447639	05/10/2014 04:00	.		
05/10/2014 04:15	0.02710666	05/10/2014 04:15	.		
05/10/2014 04:30	0.021060868	05/10/2014 04:30	.		
05/10/2014 04:45	0.029227764	05/10/2014 04:45	.		
05/10/2014 05:00	0.023817626	05/10/2014 05:00	.		
05/10/2014 05:15	0.017952755	05/10/2014 05:15	0 2		
05/10/2014 05:30	0.020628609	05/10/2014 05:30	.		
05/10/2014 05:45	0.015847789	05/10/2014 05:45	.		
05/10/2014 06:00	0.023997117	05/10/2014 06:00	.		
05/10/2014 06:15	0.016980523	05/10/2014 06:15	.		
05/10/2014 06:30	0.015945084	05/10/2014 06:30	.		
05/10/2014 06:45	0.015945084	05/10/2014 06:45	.		
05/10/2014 07:00	0.014924927	05/10/2014 07:00	.		
05/10/2014 07:15	0.009238566	05/10/2014 07:15	.		
05/10/2014 07:30	0.022474809	05/10/2014 07:30	.		
05/10/2014 07:45	0.015900672	05/10/2014 07:45	.		
05/10/2014 08:00	0.022778116	05/10/2014 08:00	.		
05/10/2014 08:15	0.023269853	05/10/2014 08:15	.		
05/10/2014 08:30	0.019294697	05/10/2014 08:30	.		
05/10/2014 08:45	0.02223629	05/10/2014 08:45	.		
05/10/2014 09:00	0.02576841	05/10/2014 09:00	.	4.2	
05/10/2014 09:15	0.029156011	05/10/2014 09:15	.		
05/10/2014 09:30	0.027802826	05/10/2014 09:30	.		
05/10/2014 09:45	0.028925505	05/10/2014 09:45	.		
05/10/2014 10:00	0.025195571	05/10/2014 10:00	.		
05/10/2014 10:15	0.028909651	05/10/2014 10:15	.		
05/10/2014 10:30	0.024240439	05/10/2014 10:30	.		
05/10/2014 10:45	0.028361354	05/10/2014 10:45	.		
05/10/2014 11:00	0.035761069	05/10/2014 11:00	.		
05/10/2014 11:15	0.029188183	05/10/2014 11:15	.		
05/10/2014 11:30	0.021943954	05/10/2014 11:30	.		
05/10/2014 11:45	0.028582074	05/10/2014 11:45	.		
05/10/2014 12:00	0.032077885	05/10/2014 12:00	.		
05/10/2014 12:15	0.039304755	05/10/2014 12:15	.		
05/10/2014 12:30	0.051603889	05/10/2014 12:30	.		
05/10/2014 12:45	0.033477709	05/10/2014 12:45	.		
05/10/2014 13:00	0.033170809	05/10/2014 13:00	.		
05/10/2014 13:15	0.024666878	05/10/2014 13:15	.		
05/10/2014 13:30	0.027798326	05/10/2014 13:30	.		
05/10/2014 13:45	0.036243739	05/10/2014 13:45	.		
05/10/2014 14:00	0.015787904	05/10/2014 14:00	.		
05/10/2014 14:15	0.032260091	05/10/2014 14:15	.		
05/10/2014 14:30	0.032511222	05/10/2014 14:30	.		
05/10/2014 14:45	0.025383859	05/10/2014 14:45	.		
05/10/2014 15:00	0.027559304	05/10/2014 15:00	.		
05/10/2014 15:15	0.016114242	05/10/2014 15:15	.		
05/10/2014 15:30	0.025693644	05/10/2014 15:30	.		

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G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
05/10/2014 15:45	0.023852413	05/10/2014 15:45	.			
05/10/2014 16:00	0.02623218	05/10/2014 16:00	.			
05/10/2014 16:15	0.050449042	05/10/2014 16:15	.			
05/10/2014 16:30	0.02467855	05/10/2014 16:30	.			
05/10/2014 16:45	0.033667203	05/10/2014 16:45	.			
05/10/2014 17:00	0.026481643	05/10/2014 17:00	.			
05/10/2014 17:15	0.026481643	05/10/2014 17:15	.			
05/10/2014 17:30	0.028297691	05/10/2014 17:30	.			
05/10/2014 17:45	0.035018953	05/10/2014 17:45	.			
05/10/2014 18:00	0.045241076	05/10/2014 18:00	.			
05/10/2014 18:15	0.028855097	05/10/2014 18:15	.			
05/10/2014 18:30	0.031478015	05/10/2014 18:30	.			
05/10/2014 18:45	0.027281347	05/10/2014 18:45	.			
05/10/2014 19:00	0.02780593	05/10/2014 19:00	.			
05/10/2014 19:15	0.027022699	05/10/2014 19:15	.			
05/10/2014 19:30	0.025693644	05/10/2014 19:30	.			
05/10/2014 19:45	0.029449488	05/10/2014 19:45	.			
05/10/2014 20:00	0.031364292	05/10/2014 20:00	.			
05/10/2014 20:15	0.027281035	05/10/2014 20:15	.			
05/10/2014 20:30	0.023689054	05/10/2014 20:30	.			
05/10/2014 20:45	0.026707531	05/10/2014 20:45	.			
05/10/2014 21:00	0.028373299	05/10/2014 21:00	.			
05/10/2014 21:15	0.026970636	05/10/2014 21:15	.			
05/10/2014 21:30	0.035357685	05/10/2014 21:30	.			
05/10/2014 21:45	0.029766319	05/10/2014 21:45	.			
05/10/2014 22:00	0.033121139	05/10/2014 22:00	.			
05/10/2014 22:15	0.03030568	05/10/2014 22:15	.			
05/10/2014 22:30	0.030775349	05/10/2014 22:30	.			
05/10/2014 22:45	0.025450808	05/10/2014 22:45	.			
05/10/2014 23:00	0.026994897	05/10/2014 23:00	.			
05/10/2014 23:15	0.026218231	05/10/2014 23:15	.			
05/10/2014 23:30	0.029275225	05/10/2014 23:30	.			
05/10/2014 23:45	0.022888863	05/10/2014 23:45	.			
06/10/2014 00:00	0.031249747	06/10/2014 00:00	.			
06/10/2014 00:15	0.037136493	06/10/2014 00:15	.			
06/10/2014 00:30	0.036475958	06/10/2014 00:30	.			
06/10/2014 00:45	0.032906869	06/10/2014 00:45	.			
06/10/2014 01:00	0.034871595	06/10/2014 01:00	.			
06/10/2014 01:15	0.030594323	06/10/2014 01:15	.			
06/10/2014 01:30	0.025130796	06/10/2014 01:30	.			
06/10/2014 01:45	0.022326029	06/10/2014 01:45	.			
06/10/2014 02:00	0.025450638	06/10/2014 02:00	.			
06/10/2014 02:15	0.033269729	06/10/2014 02:15	.			
06/10/2014 02:30	0.027046392	06/10/2014 02:30	.			
06/10/2014 02:45	0.025299509	06/10/2014 02:45	.			
06/10/2014 03:00	0.021320175	06/10/2014 03:00		0 2		
06/10/2014 03:15	0.021531267	06/10/2014 03:15	.			

G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
06/10/2014 03:30	0.019307987	06/10/2014 03:30	.		
06/10/2014 03:45	0.019312953	06/10/2014 03:45	.		
06/10/2014 04:00	0.01973583	06/10/2014 04:00	.		
06/10/2014 04:15	0.020361623	06/10/2014 04:15	.		
06/10/2014 04:30	0.018666126	06/10/2014 04:30	.		
06/10/2014 04:45	0.018454527	06/10/2014 04:45	.		
06/10/2014 05:00	0.015791668	06/10/2014 05:00	.		
06/10/2014 05:15	0.01681964	06/10/2014 05:15	.		
06/10/2014 05:30	0.016622671	06/10/2014 05:30	.		
06/10/2014 05:45	0.013637485	06/10/2014 05:45	.		
06/10/2014 06:00	0.018021187	06/10/2014 06:00	.		
06/10/2014 06:15	0.013637485	06/10/2014 06:15	.		
06/10/2014 06:30	0.018818223	06/10/2014 06:30	.		
06/10/2014 06:45	0.015416882	06/10/2014 06:45	.		
06/10/2014 07:00	0.015198233	06/10/2014 07:00	.		
06/10/2014 07:15	0.018454527	06/10/2014 07:15	.		
06/10/2014 07:30	0.018666126	06/10/2014 07:30	.		
06/10/2014 07:45	0.020974974	06/10/2014 07:45	.		
06/10/2014 08:00	0.024769888	06/10/2014 08:00	.		
06/10/2014 08:15	0.014273855	06/10/2014 08:15	.		
06/10/2014 08:30	0.025560319	06/10/2014 08:30	.		
06/10/2014 08:45	0.022470297	06/10/2014 08:45	.		
06/10/2014 09:00	0.025199233	06/10/2014 09:00	.		0.2
06/10/2014 09:15	0.024930012	06/10/2014 09:15	.		
06/10/2014 09:30	0.027022699	06/10/2014 09:30	.		
06/10/2014 09:45	0.027822401	06/10/2014 09:45	.		
06/10/2014 10:00	0.027022699	06/10/2014 10:00	.		
06/10/2014 10:15	0.031778128	06/10/2014 10:15	.		
06/10/2014 10:30	0.029136223	06/10/2014 10:30	.		
06/10/2014 10:45	0.029664604	06/10/2014 10:45	.		
06/10/2014 11:00	0.030820617	06/10/2014 11:00	.		
06/10/2014 11:15	0.035117684	06/10/2014 11:15	.		
06/10/2014 11:30	0.025923205	06/10/2014 11:30	.		
06/10/2014 11:45	0.032976134	06/10/2014 11:45	.		
06/10/2014 12:00	0.027416803	06/10/2014 12:00	.		
06/10/2014 12:15	0.021490067	06/10/2014 12:15	.		
06/10/2014 12:30	0.030325456	06/10/2014 12:30	.		
06/10/2014 12:45	0.03526815	06/10/2014 12:45	.		
06/10/2014 13:00	0.024051123	06/10/2014 13:00	.		
06/10/2014 13:15	0.020371754	06/10/2014 13:15	.		
06/10/2014 13:30	0.02755108	06/10/2014 13:30	.		
06/10/2014 13:45	0.027290212	06/10/2014 13:45	0 2		
06/10/2014 14:00	0.020932126	06/10/2014 14:00	.		
06/10/2014 14:15	0.02803866	06/10/2014 14:15	.		
06/10/2014 14:30	0.030912614	06/10/2014 14:30	.		
06/10/2014 14:45	0.032636753	06/10/2014 14:45	.		
06/10/2014 15:00	0.027529773	06/10/2014 15:00	.		

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G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
06/10/2014 15:15	0.06237951	06/10/2014 15:15		0 2	
06/10/2014 15:30	0.02226727	06/10/2014 15:30	.		
06/10/2014 15:45	0.024930012	06/10/2014 15:45	.		
06/10/2014 16:00	0.026492401	06/10/2014 16:00	.		
06/10/2014 16:15	0.023888419	06/10/2014 16:15	.		
06/10/2014 16:30	0.031100931	06/10/2014 16:30	.		
06/10/2014 16:45	0.02209345	06/10/2014 16:45		0.4	
06/10/2014 17:00	0.022035512	06/10/2014 17:00	.		
06/10/2014 17:15	0.027290212	06/10/2014 17:15	.		
06/10/2014 17:30	0.028909651	06/10/2014 17:30		0 2	
06/10/2014 17:45	0.025130796	06/10/2014 17:45		0 2	
06/10/2014 18:00	0.030018662	06/10/2014 18:00	.		
06/10/2014 18:15	0.030052668	06/10/2014 18:15	.		
06/10/2014 18:30	0.031192571	06/10/2014 18:30		0 2	
06/10/2014 18:45	0.02553861	06/10/2014 18:45		0 2	
06/10/2014 19:00	0.036712219	06/10/2014 19:00	.		
06/10/2014 19:15	0.036393158	06/10/2014 19:15		0 2	
06/10/2014 19:30	0.036393158	06/10/2014 19:30	.		
06/10/2014 19:45	0.028899318	06/10/2014 19:45		0 2	
06/10/2014 20:00	0.041315138	06/10/2014 20:00		0 2	
06/10/2014 20:15	0.042725532	06/10/2014 20:15		0 2	
06/10/2014 20:30	0.045224629	06/10/2014 20:30		0.4	
06/10/2014 20:45	0.048233019	06/10/2014 20:45	.		
06/10/2014 21:00	0.056373337	06/10/2014 21:00		0 2	
06/10/2014 21:15	0.064325405	06/10/2014 21:15	.		
06/10/2014 21:30	0.074674894	06/10/2014 21:30	.		
06/10/2014 21:45	0.071483261	06/10/2014 21:45	.		
06/10/2014 22:00	0.072328883	06/10/2014 22:00	.		
06/10/2014 22:15	0.065838601	06/10/2014 22:15	.		
06/10/2014 22:30	0.065604853	06/10/2014 22:30	.		
06/10/2014 22:45	0.056147347	06/10/2014 22:45	.		
06/10/2014 23:00	0.056799649	06/10/2014 23:00	.		
06/10/2014 23:15	0.059647183	06/10/2014 23:15	.		
06/10/2014 23:30	0.053440666	06/10/2014 23:30	.		
06/10/2014 23:45	0.046411013	06/10/2014 23:45	.		
07/10/2014 00:00	0.050878281	07/10/2014 00:00	.		
07/10/2014 00:15	0.052772828	07/10/2014 00:15	.		
07/10/2014 00:30	0.050527985	07/10/2014 00:30	.		
07/10/2014 00:45	0.045675675	07/10/2014 00:45	.		
07/10/2014 01:00	0.046000756	07/10/2014 01:00	.		
07/10/2014 01:15	0.049706008	07/10/2014 01:15	.		
07/10/2014 01:30	0.048524074	07/10/2014 01:30	.		
07/10/2014 01:45	0.035724579	07/10/2014 01:45	.		
07/10/2014 02:00	0.042697718	07/10/2014 02:00	.		
07/10/2014 02:15	0.03085668	07/10/2014 02:15	.		
07/10/2014 02:30	0.029747344	07/10/2014 02:30	.		
07/10/2014 02:45	0.028924381	07/10/2014 02:45	.		

	DATE TIME

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
07/10/2014 03:00	0.017772399	07/10/2014 03:00	.			
07/10/2014 03:15	0.024380794	07/10/2014 03:15	.			
07/10/2014 03:30	0.02157643	07/10/2014 03:30	.			
07/10/2014 03:45	0.023933374	07/10/2014 03:45	.			
07/10/2014 04:00	0.02148853	07/10/2014 04:00	.			
07/10/2014 04:15	0.016198529	07/10/2014 04:15	.			
07/10/2014 04:30	0.025560319	07/10/2014 04:30	.			
07/10/2014 04:45	0.016200048	07/10/2014 04:45		0 2		
07/10/2014 05:00	0.01628154	07/10/2014 05:00	.			
07/10/2014 05:15	0.017255918	07/10/2014 05:15	.			
07/10/2014 05:30	0.017952755	07/10/2014 05:30	.			
07/10/2014 05:45	0.015530472	07/10/2014 05:45	.			
07/10/2014 06:00	0.014289791	07/10/2014 06:00	.			
07/10/2014 06:15	0.01671408	07/10/2014 06:15	.			
07/10/2014 06:30	0.015847789	07/10/2014 06:30	.			
07/10/2014 06:45	0.017987366	07/10/2014 06:45		0 2		
07/10/2014 07:00	0.018734895	07/10/2014 07:00		0 8		
07/10/2014 07:15	0.029047914	07/10/2014 07:15		0.6		
07/10/2014 07:30	0.029202909	07/10/2014 07:30	.			
07/10/2014 07:45	0.031202489	07/10/2014 07:45		0 2		
07/10/2014 08:00	0.038646489	07/10/2014 08:00	.			
07/10/2014 08:15	0.045549294	07/10/2014 08:15	.			
07/10/2014 08:30	0.057146521	07/10/2014 08:30	.			
07/10/2014 08:45	0.05554343	07/10/2014 08:45	.			
07/10/2014 09:00	0.050087701	07/10/2014 09:00	.		5	
07/10/2014 09:15	0.050031047	07/10/2014 09:15	.			
07/10/2014 09:30	0.054695079	07/10/2014 09:30	.			
07/10/2014 09:45	0.042782389	07/10/2014 09:45	.			
07/10/2014 10:00	0.045655216	07/10/2014 10:00	.			
07/10/2014 10:15	0.050998382	07/10/2014 10:15	.			
07/10/2014 10:30	0.045302895	07/10/2014 10:30	.			
07/10/2014 10:45	0.050426142	07/10/2014 10:45	.			
07/10/2014 11:00	0.053764389	07/10/2014 11:00	.			
07/10/2014 11:15	0.053764389	07/10/2014 11:15	.			
07/10/2014 11:30	0.048617026	07/10/2014 11:30	.			
07/10/2014 11:45	0.048577539	07/10/2014 11:45	.			
07/10/2014 12:00	0.044572862	07/10/2014 12:00	.			
07/10/2014 12:15	0.044856508	07/10/2014 12:15	.			
07/10/2014 12:30	0.041698475	07/10/2014 12:30	.			
07/10/2014 12:45	0.037687273	07/10/2014 12:45	.			
07/10/2014 13:00	0.035129125	07/10/2014 13:00	.			
07/10/2014 13:15	0.031433445	07/10/2014 13:15	.			
07/10/2014 13:30	0.049438418	07/10/2014 13:30	.			
07/10/2014 13:45	0.04117447	07/10/2014 13:45	.			
07/10/2014 14:00	0.02803866	07/10/2014 14:00	.			
07/10/2014 14:15	0.030594323	07/10/2014 14:15	.			
07/10/2014 14:30	0.033991394	07/10/2014 14:30	.			

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
07/10/2014 14:45	0.023852413	07/10/2014 14:45	.			
07/10/2014 15:00	0.022888863	07/10/2014 15:00	.			
07/10/2014 15:15	0.025696124	07/10/2014 15:15	.			
07/10/2014 15:30	0.017464665	07/10/2014 15:30	.			
07/10/2014 15:45	0.030620722	07/10/2014 15:45	.			
07/10/2014 16:00	0.016772343	07/10/2014 16:00	.			
07/10/2014 16:15	0.020234438	07/10/2014 16:15	.			
07/10/2014 16:30	0.040142095	07/10/2014 16:30	.			
07/10/2014 16:45	0.026619468	07/10/2014 16:45	.			
07/10/2014 17:00	0.030029815	07/10/2014 17:00	.			
07/10/2014 17:15	0.02443383	07/10/2014 17:15	.			
07/10/2014 17:30	0.022470297	07/10/2014 17:30	.			
07/10/2014 17:45	0.026169457	07/10/2014 17:45	.			
07/10/2014 18:00	0.028925505	07/10/2014 18:00	.			
07/10/2014 18:15	0.019887338	07/10/2014 18:15	.			
07/10/2014 18:30	0.02853466	07/10/2014 18:30	.			
07/10/2014 18:45	0.025971605	07/10/2014 18:45	.			
07/10/2014 19:00	0.025971605	07/10/2014 19:00	.			
07/10/2014 19:15	0.025183013	07/10/2014 19:15	.			
07/10/2014 19:30	0.034740858	07/10/2014 19:30	.			
07/10/2014 19:45	0.032919379	07/10/2014 19:45	.			
07/10/2014 20:00	0.029989324	07/10/2014 20:00	.			
07/10/2014 20:15	0.032688506	07/10/2014 20:15	.			
07/10/2014 20:30	0.029449488	07/10/2014 20:30	.			
07/10/2014 20:45	0.03214867	07/10/2014 20:45	.			
07/10/2014 21:00	0.029703334	07/10/2014 21:00	.			
07/10/2014 21:15	0.025415274	07/10/2014 21:15	.			
07/10/2014 21:30	0.040423484	07/10/2014 21:30	.			
07/10/2014 21:45	0.035063409	07/10/2014 21:45	.			
07/10/2014 22:00	0.031015535	07/10/2014 22:00	.			
07/10/2014 22:15	0.033891652	07/10/2014 22:15	.			
07/10/2014 22:30	0.028855097	07/10/2014 22:30	.			
07/10/2014 22:45	0.02780593	07/10/2014 22:45	.			
07/10/2014 23:00	0.034100932	07/10/2014 23:00	.			
07/10/2014 23:15	0.03117957	07/10/2014 23:15	.			
07/10/2014 23:30	0.029275225	07/10/2014 23:30	.			
07/10/2014 23:45	0.026700165	07/10/2014 23:45	.			
08/10/2014 00:00	0.0213491	08/10/2014 00:00	.			
08/10/2014 00:15	0.031778128	08/10/2014 00:15	.			
08/10/2014 00:30	0.031364292	08/10/2014 00:30	.			
08/10/2014 00:45	0.02782856	08/10/2014 00:45	.			
08/10/2014 01:00	0.034740858	08/10/2014 01:00	.			
08/10/2014 01:15	0.028765726	08/10/2014 01:15	.			
08/10/2014 01:30	0.02443383	08/10/2014 01:30	.			
08/10/2014 01:45	0.028679826	08/10/2014 01:45	.			
08/10/2014 02:00	0.027366662	08/10/2014 02:00	.			
08/10/2014 02:15	0.023817626	08/10/2014 02:15	.			

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
08/10/2014 02:30	0.022630552	08/10/2014 02:30	.			
08/10/2014 02:45	0.019529839	08/10/2014 02:45	.			
08/10/2014 03:00	0.017403161	08/10/2014 03:00	.			
08/10/2014 03:15	0.014093549	08/10/2014 03:15	.			
08/10/2014 03:30	0.022989076	08/10/2014 03:30	.			
08/10/2014 03:45	0.015603584	08/10/2014 03:45	.			
08/10/2014 04:00	0.018230388	08/10/2014 04:00	.			
08/10/2014 04:15	0.016427113	08/10/2014 04:15	.			
08/10/2014 04:30	0.013467133	08/10/2014 04:30	.			
08/10/2014 04:45	0.012514643	08/10/2014 04:45	.			
08/10/2014 05:00	0.021674206	08/10/2014 05:00	.			
08/10/2014 05:15	0.017968883	08/10/2014 05:15	.			
08/10/2014 05:30	0.017378582	08/10/2014 05:30	.			
08/10/2014 05:45	0.015283239	08/10/2014 05:45	.			
08/10/2014 06:00	0.016039833	08/10/2014 06:00	.			
08/10/2014 06:15	0.028221333	08/10/2014 06:15	.			
08/10/2014 06:30	0.009230493	08/10/2014 06:30	.			
08/10/2014 06:45	0.017198902	08/10/2014 06:45	.			
08/10/2014 07:00	0.017607147	08/10/2014 07:00	.			
08/10/2014 07:15	0.011955417	08/10/2014 07:15	.			
08/10/2014 07:30	0.016980523	08/10/2014 07:30	.			
08/10/2014 07:45	0.021949231	08/10/2014 07:45	.			
08/10/2014 08:00	0.023363161	08/10/2014 08:00	.			
08/10/2014 08:15	0.020610499	08/10/2014 08:15	.			
08/10/2014 08:30	0.033764196	08/10/2014 08:30	.			
08/10/2014 08:45	0.029136967	08/10/2014 08:45	0 2			
08/10/2014 09:00	0.033467892	08/10/2014 09:00	0 2	0.4		
08/10/2014 09:15	0.038779069	08/10/2014 09:15	0 2			
08/10/2014 09:30	0.039973953	08/10/2014 09:30	0 2			
08/10/2014 09:45	0.036921651	08/10/2014 09:45	0.4			
08/10/2014 10:00	0.049088912	08/10/2014 10:00	1			
08/10/2014 10:15	0.063605514	08/10/2014 10:15	1.6			
08/10/2014 10:30	0.099003779	08/10/2014 10:30	2.4			
08/10/2014 10:45	0.290224196	08/10/2014 10:45	3			
08/10/2014 11:00	0.481444614	08/10/2014 11:00	1 2			
08/10/2014 11:15	0.427030223	08/10/2014 11:15	1 2			
08/10/2014 11:30	0.488056565	08/10/2014 11:30	1 8			
08/10/2014 11:45	0.806410977	08/10/2014 11:45	0.6			
08/10/2014 12:00	0.935619966	08/10/2014 12:00	0.6			
08/10/2014 12:15	0.820299355	08/10/2014 12:15	1.4			
08/10/2014 12:30	0.693528456	08/10/2014 12:30	1			
08/10/2014 12:45	1.049828228	08/10/2014 12:45	.			
08/10/2014 13:00	0.855735256	08/10/2014 13:00	.			
08/10/2014 13:15	0.675560948	08/10/2014 13:15	.			
08/10/2014 13:30	0.601380048	08/10/2014 13:30	.			
08/10/2014 13:45	0.491483171	08/10/2014 13:45	.			
08/10/2014 14:00	0.426560681	08/10/2014 14:00	.			

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
08/10/2014 14:15	0.4128086	08/10/2014 14:15	.			
08/10/2014 14:30	0.331165378	08/10/2014 14:30	.			
08/10/2014 14:45	0.301346834	08/10/2014 14:45	.			
08/10/2014 15:00	0.280467213	08/10/2014 15:00	.			
08/10/2014 15:15	0.250365561	08/10/2014 15:15	.			
08/10/2014 15:30	0.24066813	08/10/2014 15:30	.			
08/10/2014 15:45	0.247180983	08/10/2014 15:45	.			
08/10/2014 16:00	0.189141562	08/10/2014 16:00	.			
08/10/2014 16:15	0.197086845	08/10/2014 16:15	.			
08/10/2014 16:30	0.152022906	08/10/2014 16:30	.			
08/10/2014 16:45	0.157692673	08/10/2014 16:45	.			
08/10/2014 17:00	0.15321323	08/10/2014 17:00		0 2		
08/10/2014 17:15	0.153496182	08/10/2014 17:15	.			
08/10/2014 17:30	0.127898818	08/10/2014 17:30	.			
08/10/2014 17:45	0.135264838	08/10/2014 17:45	.			
08/10/2014 18:00	0.122021613	08/10/2014 18:00	.			
08/10/2014 18:15	0.127029587	08/10/2014 18:15	.			
08/10/2014 18:30	0.116743901	08/10/2014 18:30	.			
08/10/2014 18:45	0.108661543	08/10/2014 18:45	.			
08/10/2014 19:00	0.109532582	08/10/2014 19:00	.			
08/10/2014 19:15	0.098072091	08/10/2014 19:15	.			
08/10/2014 19:30	0.105814847	08/10/2014 19:30	.			
08/10/2014 19:45	0.10126648	08/10/2014 19:45	.			
08/10/2014 20:00	0.1044141	08/10/2014 20:00	.			
08/10/2014 20:15	0.107943048	08/10/2014 20:15	.			
08/10/2014 20:30	0.094633975	08/10/2014 20:30	.			
08/10/2014 20:45	0.102875669	08/10/2014 20:45	.			
08/10/2014 21:00	0.094467741	08/10/2014 21:00	.			
08/10/2014 21:15	0.093196903	08/10/2014 21:15	.			
08/10/2014 21:30	0.083694537	08/10/2014 21:30	.			
08/10/2014 21:45	0.088554112	08/10/2014 21:45	.			
08/10/2014 22:00	0.084505673	08/10/2014 22:00	.			
08/10/2014 22:15	0.081707217	08/10/2014 22:15	.			
08/10/2014 22:30	0.087709242	08/10/2014 22:30	.			
08/10/2014 22:45	0.088549001	08/10/2014 22:45	.			
08/10/2014 23:00	0.084915232	08/10/2014 23:00	.			
08/10/2014 23:15	0.081565545	08/10/2014 23:15	.			
08/10/2014 23:30	0.083001958	08/10/2014 23:30	.			
08/10/2014 23:45	0.086119242	08/10/2014 23:45	.			
09/10/2014 00:00	0.102101155	09/10/2014 00:00	.			
09/10/2014 00:15	0.092700767	09/10/2014 00:15	.			
09/10/2014 00:30	0.093196903	09/10/2014 00:30	.			
09/10/2014 00:45	0.09130759	09/10/2014 00:45	.			
09/10/2014 01:00	0.090935161	09/10/2014 01:00	.			
09/10/2014 01:15	0.084054036	09/10/2014 01:15	.			
09/10/2014 01:30	0.08812361	09/10/2014 01:30	.			
09/10/2014 01:45	0.089070287	09/10/2014 01:45	.			

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
09/10/2014 02:00	0.085116442	09/10/2014 02:00	.			
09/10/2014 02:15	0.078554838	09/10/2014 02:15	.			
09/10/2014 02:30	0.09342982	09/10/2014 02:30	.			
09/10/2014 02:45	0.075604701	09/10/2014 02:45	.			
09/10/2014 03:00	0.073731167	09/10/2014 03:00	.			
09/10/2014 03:15	0.0725275	09/10/2014 03:15	.			
09/10/2014 03:30	0.071981315	09/10/2014 03:30	.			
09/10/2014 03:45	0.080478537	09/10/2014 03:45	.			
09/10/2014 04:00	0.079242938	09/10/2014 04:00	.			
09/10/2014 04:15	0.087478559	09/10/2014 04:15	.			
09/10/2014 04:30	0.07612567	09/10/2014 04:30	.			
09/10/2014 04:45	0.071163252	09/10/2014 04:45	.			
09/10/2014 05:00	0.071863274	09/10/2014 05:00	.			
09/10/2014 05:15	0.074405036	09/10/2014 05:15	.			
09/10/2014 05:30	0.071930786	09/10/2014 05:30	.			
09/10/2014 05:45	0.069456537	09/10/2014 05:45	.			
09/10/2014 06:00	0.077523249	09/10/2014 06:00	.			
09/10/2014 06:15	0.068305288	09/10/2014 06:15	.			
09/10/2014 06:30	0.069672495	09/10/2014 06:30	.			
09/10/2014 06:45	0.0679254	09/10/2014 06:45	.			
09/10/2014 07:00	0.081782788	09/10/2014 07:00	.			
09/10/2014 07:15	0.08119594	09/10/2014 07:15	.			
09/10/2014 07:30	0.069606326	09/10/2014 07:30	.			
09/10/2014 07:45	0.075679657	09/10/2014 07:45	.			
09/10/2014 08:00	0.07813778	09/10/2014 08:00	.			
09/10/2014 08:15	0.084920595	09/10/2014 08:15	.			
09/10/2014 08:30	0.083064908	09/10/2014 08:30	.			
09/10/2014 08:45	0.086776282	09/10/2014 08:45	.			
09/10/2014 09:00	0.075679657	09/10/2014 09:00	.			
09/10/2014 09:15	0.070763411	09/10/2014 09:15	.			
09/10/2014 09:30	0.080590659	09/10/2014 09:30	.			
09/10/2014 09:45	0.094533619	09/10/2014 09:45	.			
09/10/2014 10:00	0.091431606	09/10/2014 10:00	.			
09/10/2014 10:15	0.093431534	09/10/2014 10:15	.			
09/10/2014 10:30	0.085417412	09/10/2014 10:30	.			
09/10/2014 10:45	0.096010891	09/10/2014 10:45	.			
09/10/2014 11:00	0.083628348	09/10/2014 11:00	.			
09/10/2014 11:15	0.088144945	09/10/2014 11:15	.			
09/10/2014 11:30	0.081802114	09/10/2014 11:30	.			
09/10/2014 11:45	0.078089312	09/10/2014 11:45	.			
09/10/2014 12:00	0.087970271	09/10/2014 12:00	.			
09/10/2014 12:15	0.086700577	09/10/2014 12:15	.			
09/10/2014 12:30	0.077556957	09/10/2014 12:30		0.6		
09/10/2014 12:45	0.078769952	09/10/2014 12:45	.			
09/10/2014 13:00	0.117310169	09/10/2014 13:00	.			
09/10/2014 13:15	0.104813048	09/10/2014 13:15	.			
09/10/2014 13:30	0.110284113	09/10/2014 13:30	.			

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
09/10/2014 13:45	0.126674977	09/10/2014 13:45	.			
09/10/2014 14:00	0.113221198	09/10/2014 14:00	.			
09/10/2014 14:15	0.08657545	09/10/2014 14:15	.			
09/10/2014 14:30	0.097079605	09/10/2014 14:30	.			
09/10/2014 14:45	0.09736609	09/10/2014 14:45	.			
09/10/2014 15:00	0.083652505	09/10/2014 15:00	.			
09/10/2014 15:15	0.090016324	09/10/2014 15:15	.			
09/10/2014 15:30	0.077496995	09/10/2014 15:30	.			
09/10/2014 15:45	0.086836887	09/10/2014 15:45	.			
09/10/2014 16:00	0.079746004	09/10/2014 16:00	.			
09/10/2014 16:15	0.073529856	09/10/2014 16:15	.			
09/10/2014 16:30	0.079309768	09/10/2014 16:30	.			
09/10/2014 16:45	0.086776282	09/10/2014 16:45	.			
09/10/2014 17:00	0.074450595	09/10/2014 17:00	.			
09/10/2014 17:15	0.073836065	09/10/2014 17:15	.			
09/10/2014 17:30	0.076321925	09/10/2014 17:30	.			
09/10/2014 17:45	0.084258541	09/10/2014 17:45	.			
09/10/2014 18:00	0.078763961	09/10/2014 18:00	.			
09/10/2014 18:15	0.073917975	09/10/2014 18:15	.			
09/10/2014 18:30	0.070885489	09/10/2014 18:30	.			
09/10/2014 18:45	0.078153452	09/10/2014 18:45	.			
09/10/2014 19:00	0.076343963	09/10/2014 19:00	.			
09/10/2014 19:15	0.081180293	09/10/2014 19:15	.			
09/10/2014 19:30	0.084151601	09/10/2014 19:30	.			
09/10/2014 19:45	0.072780041	09/10/2014 19:45	.			
09/10/2014 20:00	0.05362794	09/10/2014 20:00	.			
09/10/2014 20:15	0.073950351	09/10/2014 20:15	.			
09/10/2014 20:30	0.03177569	09/10/2014 20:30	.			
09/10/2014 20:45	0.065598003	09/10/2014 20:45	.			
09/10/2014 21:00	0.032381613	09/10/2014 21:00	.			
09/10/2014 21:15	0.068108026	09/10/2014 21:15	.			
09/10/2014 21:30	0.069289125	09/10/2014 21:30	.			
09/10/2014 21:45	0.073422968	09/10/2014 21:45	.			
09/10/2014 22:00	0.074609937	09/10/2014 22:00	.			
09/10/2014 22:15	0.088101441	09/10/2014 22:15	.			
09/10/2014 22:30	0.081601878	09/10/2014 22:30	.			
09/10/2014 22:45	0.078688702	09/10/2014 22:45	.			
09/10/2014 23:00	0.067082038	09/10/2014 23:00	.			
09/10/2014 23:15	0.076318641	09/10/2014 23:15	.			
09/10/2014 23:30	0.069996262	09/10/2014 23:30	.			
09/10/2014 23:45	0.081100107	09/10/2014 23:45	.			
10/10/2014 00:00	0.075174054	10/10/2014 00:00	.			
10/10/2014 00:15	0.08660275	10/10/2014 00:15	.			
10/10/2014 00:30	0.07756522	10/10/2014 00:30	.			
10/10/2014 00:45	0.079889222	10/10/2014 00:45	.			
10/10/2014 01:00	0.070588419	10/10/2014 01:00	.			
10/10/2014 01:15	0.056981145	10/10/2014 01:15	.			

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
10/10/2014 01:30	0.058284857	10/10/2014 01:30	.			
10/10/2014 01:45	0.06029582	10/10/2014 01:45	.			
10/10/2014 02:00	0.050584329	10/10/2014 02:00	.			
10/10/2014 02:15	0.051551981	10/10/2014 02:15	.			
10/10/2014 02:30	0.056355933	10/10/2014 02:30	.			
10/10/2014 02:45	0.041438365	10/10/2014 02:45	.			
10/10/2014 03:00	0.042776081	10/10/2014 03:00	.			
10/10/2014 03:15	0.039113999	10/10/2014 03:15	.			
10/10/2014 03:30	0.031247482	10/10/2014 03:30	.			
10/10/2014 03:45	0.038758365	10/10/2014 03:45	.			
10/10/2014 04:00	0.037595519	10/10/2014 04:00	.			
10/10/2014 04:15	0.0298806	10/10/2014 04:15	.			
10/10/2014 04:30	0.037850286	10/10/2014 04:30	.			
10/10/2014 04:45	0.038475362	10/10/2014 04:45	.			
10/10/2014 05:00	0.03144773	10/10/2014 05:00	.			
10/10/2014 05:15	0.036293088	10/10/2014 05:15	.			
10/10/2014 05:30	0.03659383	10/10/2014 05:30	.			
10/10/2014 05:45	0.03891873	10/10/2014 05:45	.			
10/10/2014 06:00	0.034811829	10/10/2014 06:00	.			
10/10/2014 06:15	0.038171306	10/10/2014 06:15	.			
10/10/2014 06:30	0.038171306	10/10/2014 06:30	.			
10/10/2014 06:45	0.037223064	10/10/2014 06:45	.			
10/10/2014 07:00	0.037163463	10/10/2014 07:00	.			
10/10/2014 07:15	0.033132091	10/10/2014 07:15	.			
10/10/2014 07:30	0.040094029	10/10/2014 07:30	.			
10/10/2014 07:45	0.041793778	10/10/2014 07:45	.			
10/10/2014 08:00	0.039070343	10/10/2014 08:00	.			
10/10/2014 08:15	0.050800822	10/10/2014 08:15	.			
10/10/2014 08:30	0.050384737	10/10/2014 08:30	.			
10/10/2014 08:45	0.048595725	10/10/2014 08:45	.			
10/10/2014 09:00	0.054252257	10/10/2014 09:00	.			
10/10/2014 09:15	0.049633132	10/10/2014 09:15	.			
10/10/2014 09:30	0.04924208	10/10/2014 09:30	.			
10/10/2014 09:45	0.051474627	10/10/2014 09:45	.			
10/10/2014 10:00	0.053737872	10/10/2014 10:00	.			
10/10/2014 10:15	0.053290558	10/10/2014 10:15	.			
10/10/2014 10:30	0.053326644	10/10/2014 10:30	.			
10/10/2014 10:45	0.054228412	10/10/2014 10:45	.			
10/10/2014 11:00	0.054228412	10/10/2014 11:00	.			
10/10/2014 11:15	0.048366919	10/10/2014 11:15	.			
10/10/2014 11:30	0.049268687	10/10/2014 11:30	.			
10/10/2014 11:45	0.049719571	10/10/2014 11:45	.			
10/10/2014 12:00	0.051501302	10/10/2014 12:00	.			
10/10/2014 12:15	0.052362137	10/10/2014 12:15	.			
10/10/2014 12:30	0.053590154	10/10/2014 12:30	.			
10/10/2014 12:45	0.047882836	10/10/2014 12:45	.			
10/10/2014 13:00	0.046155811	10/10/2014 13:00	.			

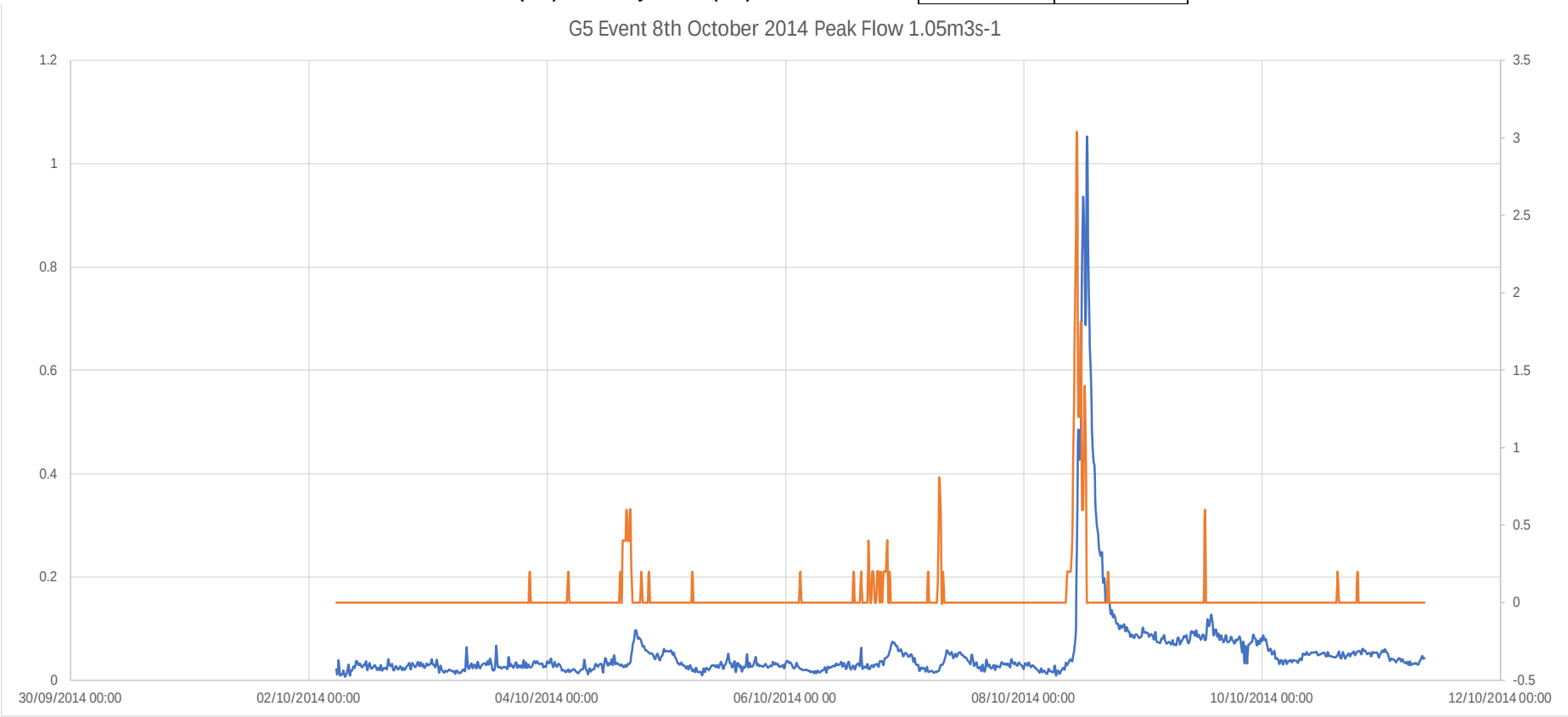
G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
10/10/2014 13:15	0.05408841	10/10/2014 13:15	.		
10/10/2014 13:30	0.046543576	10/10/2014 13:30	.		
10/10/2014 13:45	0.046517281	10/10/2014 13:45	.		
10/10/2014 14:00	0.046101592	10/10/2014 14:00	.		
10/10/2014 14:15	0.044837359	10/10/2014 14:15	.		
10/10/2014 14:30	0.045249591	10/10/2014 14:30	.		
10/10/2014 14:45	0.04399791	10/10/2014 14:45	.		
10/10/2014 15:00	0.04604184	10/10/2014 15:00	.		
10/10/2014 15:15	0.048437094	10/10/2014 15:15		0 2	
10/10/2014 15:30	0.055609818	10/10/2014 15:30	.		
10/10/2014 15:45	0.044355796	10/10/2014 15:45	.		
10/10/2014 16:00	0.04194422	10/10/2014 16:00	.		
10/10/2014 16:15	0.054684872	10/10/2014 16:15	.		
10/10/2014 16:30	0.048308579	10/10/2014 16:30	.		
10/10/2014 16:45	0.041932285	10/10/2014 16:45	.		
10/10/2014 17:00	0.04551895	10/10/2014 17:00	.		
10/10/2014 17:15	0.049178949	10/10/2014 17:15	.		
10/10/2014 17:30	0.051274558	10/10/2014 17:30	.		
10/10/2014 17:45	0.046074054	10/10/2014 17:45	.		
10/10/2014 18:00	0.051845299	10/10/2014 18:00	.		
10/10/2014 18:15	0.051921236	10/10/2014 18:15	.		
10/10/2014 18:30	0.055345882	10/10/2014 18:30	.		
10/10/2014 18:45	0.048220206	10/10/2014 18:45	.		
10/10/2014 19:00	0.052904701	10/10/2014 19:00	.		
10/10/2014 19:15	0.05518657	10/10/2014 19:15		0 2	
10/10/2014 19:30	0.056210178	10/10/2014 19:30	.		
10/10/2014 19:45	0.055845188	10/10/2014 19:45	.		
10/10/2014 20:00	0.049699607	10/10/2014 20:00	.		
10/10/2014 20:15	0.060447581	10/10/2014 20:15	.		
10/10/2014 20:30	0.05686907	10/10/2014 20:30	.		
10/10/2014 20:45	0.057316384	10/10/2014 20:45	.		
10/10/2014 21:00	0.053737872	10/10/2014 21:00	.		
10/10/2014 21:15	0.050170455	10/10/2014 21:15	.		
10/10/2014 21:30	0.05239593	10/10/2014 21:30	.		
10/10/2014 21:45	0.05232353	10/10/2014 21:45	.		
10/10/2014 22:00	0.046167968	10/10/2014 22:00	.		
10/10/2014 22:15	0.054327307	10/10/2014 22:15	.		
10/10/2014 22:30	0.05217915	10/10/2014 22:30	.		
10/10/2014 22:45	0.0534	10/10/2014 22:45	.		
10/10/2014 23:00	0.052904701	10/10/2014 23:00	.		
10/10/2014 23:15	0.053583991	10/10/2014 23:15	.		
10/10/2014 23:30	0.044012896	10/10/2014 23:30	.		
10/10/2014 23:45	0.049011414	10/10/2014 23:45	.		
11/10/2014 00:00	0.053468045	11/10/2014 00:00	.		
11/10/2014 00:15	0.057243443	11/10/2014 00:15	.		
11/10/2014 00:30	0.054266803	11/10/2014 00:30	.		
11/10/2014 00:45	0.060089905	11/10/2014 00:45	.		

	DATE TIME

G5 flow		Thorpeness TBR RG				
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)		DATE TIME
11/10/2014 01:00	0.054964774	11/10/2014 01:00	.			
11/10/2014 01:15	0.052547742	11/10/2014 01:15	.			
11/10/2014 01:30	0.04604184	11/10/2014 01:30	.			
11/10/2014 01:45	0.037150066	11/10/2014 01:45	.			
11/10/2014 02:00	0.041480305	11/10/2014 02:00	.			
11/10/2014 02:15	0.041007412	11/10/2014 02:15	.			
11/10/2014 02:30	0.039813643	11/10/2014 02:30	.			
11/10/2014 02:45	0.03864182	11/10/2014 02:45	.			
11/10/2014 03:00	0.034615823	11/10/2014 03:00	.			
11/10/2014 03:15	0.038422967	11/10/2014 03:15	.			
11/10/2014 03:30	0.041728788	11/10/2014 03:30	.			
11/10/2014 03:45	0.042202679	11/10/2014 03:45	.			
11/10/2014 04:00	0.036101399	11/10/2014 04:00	.			
11/10/2014 04:15	0.040551081	11/10/2014 04:15	.			
11/10/2014 04:30	0.03623736	11/10/2014 04:30	.			
11/10/2014 04:45	0.03392223	11/10/2014 04:45	.			
11/10/2014 05:00	0.032236418	11/10/2014 05:00	.			
11/10/2014 05:15	0.035918797	11/10/2014 05:15	.			
11/10/2014 05:30	0.029335905	11/10/2014 05:30	.			
11/10/2014 05:45	0.036242463	11/10/2014 05:45	.			
11/10/2014 06:00	0.029604584	11/10/2014 06:00	.			
11/10/2014 06:15	0.03075921	11/10/2014 06:15	.			
11/10/2014 06:30	0.03195395	11/10/2014 06:30	.			
11/10/2014 06:45	0.031113193	11/10/2014 06:45	.			
11/10/2014 07:00	0.032993158	11/10/2014 07:00	.			
11/10/2014 07:15	0.030288377	11/10/2014 07:15	.			
11/10/2014 07:30	0.03003846	11/10/2014 07:30	.			
11/10/2014 07:45	0.036804073	11/10/2014 07:45	.			
11/10/2014 08:00	0.03924522	11/10/2014 08:00	.			
11/10/2014 08:15	0.046718789	11/10/2014 08:15	.			
11/10/2014 08:30	0.041561823	11/10/2014 08:30	.			
11/10/2014 08:45	0.042869276	11/10/2014 08:45	.			

G5 flow		Thorpeness TBR RG			
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)	

	DATE TIME



SAAR	592	mm
AREA	5.04	Km2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

SMD on the irst day of the event 0mm
So l condit ons were saturated prior to the event
approx. 0 mm of free capacity in the soil column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
07-Oct-14	103.0	mm
14-Oct-14	60.7	mm

Source of Rainfall event data.

Gauge	East ng	Northing	Distance from Catchment Centroid (m)	Reciprocal	Weighting
Benhall	38 66	60602			
Soham	23243	62717			
Thorpeness	60012	78834	3636.0	0.00028	1.00000
			Total	0.00028	1.00000

BR RG

Daily RF totals 9am 9am	**Benhall**	**Soham**	**horpeness**
Date	**otal RF (mm)**	**otal RF (mm)**	**otal RF (mm)**
06/10/201		0	5
05/10/201		0	0.2
0 /10/201		0	.2
03/10/201		0	0.
02/10/201		0	0
Total API5 RF			9.8

Rainall Event Depth P (mm)	17
Event duration (hours)	3.75

Daily Rainfall totals mm

RF Gauge	**SAAR**	**Weight**	**02/10/2014**	**03/10 2014**	**04 10/2014**	**05/10/2014**	**06/10/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.00000	0	0.4	4.2	0.2	5
Average Daily rainfall tota s			0	0.4	4.2	0.2	5

Gauge	**SAAR**	**Weight**	**02/10/2014**	**03/10 2014**	**04 10/2014**	**05/10/2014**	**06/10/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.00000	0	0.000675676	0.007094595	0 000337838	0.008445946

Gauge	**SAAR**	**Weight**	**02/10/2014**	**03/10 2014**	**04 10/2014**	**05/10/2014**	**06/10/2014**
Benhall	592						
Soham	592						
Thorpeness	592	1.0000	0	0.000675676	0.007094595	0 000337838	0.008445946

Gauge	**SAAR**	**Weight**	**02/10/2014**	**03/10 2014**	**04 10/2014**	**05/10/2014**	**06/10/2014**
Benhall	592		0	0	0	0	0
Soham	592		0	0	0	0	0
Thorpeness	592	1.00000	0	0.4	4.2	0.2	5
Catchment Average Antecedent RF mm			0	0.4	4.2	0.2	5

Date	**Catchment Average Antecedent Rainfall (mm)**	
02/10/2014	0.00	d-5
03/10/2014	0. 0	d-
04/10/2014	.20	d-3
05/10/2014	0.20	d-2
06/10/2014	5.00	d-1

API5

4.38	mm	4.384062043	mm / day

CWI Prior to Event October 201 Event at G5
CWI = 125 API15 - SMD

SMD	103	mm
CWI	26.38406204	mm

FEH Parameter										
SPR	44.52766617	%						**URBEXT2000**		As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
PRrural	19.87	%			P=Storm Depth	17	mm	**PR**	20	taken from PR calculations sheet using Benhall TBR RG record
DPRrain	0	%			SPR	44.52766617		**DPRrain**	0	DPRrain is 0, as P<40mm
DPRcwi	-24.65398449	CWI	26.3841					**DPRcwi**	-24.65398449	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural								**SPR**	44.52766617	
PR	20.13263424	%						**DPRrain**	0.45(P-40)^0.7	#NUM!
PRrural	19.87368168	%						**P**	17	
CWI	26.38406204	mm						**CWI**	26.38406204	
BF	0.00001		Baseflow equation taken from FEH					**SPR**	44.52766617	
	-1254							**PR**	20.13263424	
										from FEH Catchment descriptors & SPRHOST is the same as SPRcds.
	1778.5	524.5	0.00525					**SPRHOST**	24.27	Average SPRHOST value of both Leiston and Leiston Abbey catchments
AREA	50.52		**0.26498** m3s-1					**Duration (hours)**	3.75	
SPR	44.52766617									
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	44.52766617									
PRrural	19.87368168									

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
08-Oct-14	08-Oct-14	3.75	4.38	103.00	26.38	19.87	-24.65	0.00	44.53	20.00	24.27

Site **Sub-catchment** **SPRg.cds** **SPRg.obs** **SPRs.cds** **SPRs.adj**

Site	Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Sizewell	Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	Leis Abbey	24.3	44.8	27.8	51.4
Leiston	Leiston	24.3	44.8	20.7	38.2
Leis Upper	Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	Mins Potters	24.3	44.8	25.3	46.8
				Mean	37.3

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
30/10/2014 08:45	0.04442076	30/10/2014 08:45	.	
30/10/2014 09:00	0.04309811	30/10/2014 09:00	.	
30/10/2014 09:15	0.04354943	30/10/2014 09:15	.	
30/10/2014 09:30	0.03702792	30/10/2014 09:30	.	
30/10/2014 09:45	0.04243113	30/10/2014 09:45	.	
30/10/2014 10:00	0.04222443	30/10/2014 10:00	.	
30/10/2014 10:15	0.0321143	30/10/2014 10:15	.	
30/10/2014 10:30	0.04847024	30/10/2014 10:30	.	
30/10/2014 10:45	0.04504944	30/10/2014 10:45	.	
30/10/2014 11:00	0.04631375	30/10/2014 11:00	.	
30/10/2014 11:15	0.05524798	30/10/2014 11:15	.	
30/10/2014 11:30	0.0614728	30/10/2014 11:30	.	
30/10/2014 11:45	0.04322003	30/10/2014 11:45	.	
30/10/2014 12:00	0.04198758	30/10/2014 12:00	.	
30/10/2014 12:15	0.03316606	30/10/2014 12:15	.	
30/10/2014 12:30	0.03495541	30/10/2014 12:30	.	
30/10/2014 12:45	0.02972783	30/10/2014 12:45	.	
30/10/2014 13:00	0.03682752	30/10/2014 13:00	.	
30/10/2014 13:15	0.04522621	30/10/2014 13:15	.	
30/10/2014 13:30	0.03682752	30/10/2014 13:30	.	
30/10/2014 13:45	0.0388432	30/10/2014 13:45	.	
30/10/2014 14:00	0.03909637	30/10/2014 14:00	.	
30/10/2014 14:15	0.04085889	30/10/2014 14:15	0.2	
30/10/2014 14:30	0.04095353	30/10/2014 14:30	.	
30/10/2014 14:45	0.03985104	30/10/2014 14:45	.	
30/10/2014 15:00	0.03543585	30/10/2014 15:00	.	
30/10/2014 15:15	0.03532764	30/10/2014 15:15	.	
30/10/2014 15:30	0.03304238	30/10/2014 15:30	.	
30/10/2014 15:45	0.03924522	30/10/2014 15:45	.	
30/10/2014 16:00	0.03826583	30/10/2014 16:00	.	
30/10/2014 16:15	0.02520722	30/10/2014 16:15	.	
30/10/2014 16:30	0.03365073	30/10/2014 16:30	.	
30/10/2014 16:45	0.03656069	30/10/2014 16:45	.	
30/10/2014 17:00	0.02977078	30/10/2014 17:00	.	
30/10/2014 17:15	0.02879834	30/10/2014 17:15	.	
30/10/2014 17:30	0.03532764	30/10/2014 17:30	.	
30/10/2014 17:45	0.03942914	30/10/2014 17:45	.	
30/10/2014 18:00	0.03891873	30/10/2014 18:00	.	
30/10/2014 18:15	0.03586653	30/10/2014 18:15	.	
30/10/2014 18:30	0.04909272	30/10/2014 18:30	.	
30/10/2014 18:45	0.03824046	30/10/2014 18:45	.	
30/10/2014 19:00	0.03722306	30/10/2014 19:00	.	
30/10/2014 19:15	0.04378277	30/10/2014 19:15	.	
30/10/2014 19:30	0.04207112	30/10/2014 19:30	.	
30/10/2014 19:45	0.03912049	30/10/2014 19:45	.	

	DATE TIME
start of event	05/11/2014 00:45
end of event	05/11/2014 10:15
duration hours	9.5
total RF mm	28.8
SMD W/E AVERAGE	**mm**
04-Nov-14	56.2

DATE	API5	Daily Totals
03/11/2014	d-1	7.2
02/11/2014	d-2	6.8
01/11/2014	d-3	0
31/10/2014	d-4	0
30/10/2014	d-5	0.2
		14.2

05/11/2014

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
30/10/2014 20:00	0.03847536	30/10/2014 20:00	.	
30/10/2014 20:15	0.04234731	30/10/2014 20:15	.	
30/10/2014 20:30	0.04164332	30/10/2014 20:30	.	
30/10/2014 20:45	0.04322777	30/10/2014 20:45	.	
30/10/2014 21:00	0.03969205	30/10/2014 21:00	.	
30/10/2014 21:15	0.04511859	30/10/2014 21:15	.	
30/10/2014 21:30	0.04186266	30/10/2014 21:30	.	
30/10/2014 21:45	0.03896851	30/10/2014 21:45	.	
30/10/2014 22:00	0.04083212	30/10/2014 22:00	.	
30/10/2014 22:15	0.03791172	30/10/2014 22:15	.	
30/10/2014 22:30	0.03864182	30/10/2014 22:30	.	
30/10/2014 22:45	0.04113913	30/10/2014 22:45	.	
30/10/2014 23:00	0.03892578	30/10/2014 23:00	.	
30/10/2014 23:15	0.04065493	30/10/2014 23:15	.	
30/10/2014 23:30	0.02967547	30/10/2014 23:30	.	
30/10/2014 23:45	0.0434033	30/10/2014 23:45	.	
31/10/2014 00:00	0.03777137	31/10/2014 00:00	.	
31/10/2014 00:15	0.04551527	31/10/2014 00:15	.	
31/10/2014 00:30	0.04551527	31/10/2014 00:30	.	
31/10/2014 00:45	0.03802079	31/10/2014 00:45	.	
31/10/2014 01:00	0.03620567	31/10/2014 01:00	.	
31/10/2014 01:15	0.04055108	31/10/2014 01:15	.	
31/10/2014 01:30	0.03223642	31/10/2014 01:30	.	
31/10/2014 01:45	0.03329793	31/10/2014 01:45	.	
31/10/2014 02:00	0.03020803	31/10/2014 02:00	.	
31/10/2014 02:15	0.03543359	31/10/2014 02:15	.	
31/10/2014 02:30	0.02976497	31/10/2014 02:30	.	
31/10/2014 02:45	0.02855141	31/10/2014 02:45	.	
31/10/2014 03:00	0.02533316	31/10/2014 03:00	.	
31/10/2014 03:15	0.02834075	31/10/2014 03:15	.	
31/10/2014 03:30	0.02772887	31/10/2014 03:30	.	
31/10/2014 03:45	0.02250223	31/10/2014 03:45	.	
31/10/2014 04:00	0.03244729	31/10/2014 04:00	.	
31/10/2014 04:15	0.03152932	31/10/2014 04:15	.	
31/10/2014 04:30	0.03472275	31/10/2014 04:30	.	
31/10/2014 04:45	0.02904582	31/10/2014 04:45	.	
31/10/2014 05:00	0.02930905	31/10/2014 05:00	.	
31/10/2014 05:15	0.02947458	31/10/2014 05:15	.	
31/10/2014 05:30	0.02504837	31/10/2014 05:30	.	
31/10/2014 05:45	0.02843312	31/10/2014 05:45	.	
31/10/2014 06:00	0.02860089	31/10/2014 06:00	.	
31/10/2014 06:15	0.02190568	31/10/2014 06:15	.	
31/10/2014 06:30	0.02595818	31/10/2014 06:30	.	
31/10/2014 06:45	0.03156078	31/10/2014 06:45	.	
31/10/2014 07:00	0.02799549	31/10/2014 07:00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
31/10/2014 07:15	0.02519419	31/10/2014 07:15	.	
31/10/2014 07:30	0.0257683	31/10/2014 07:30	.	
31/10/2014 07:45	0.03416116	31/10/2014 07:45	.	
31/10/2014 08:00	0.02868107	31/10/2014 08:00	.	
31/10/2014 08:15	0.02695184	31/10/2014 08:15	.	
31/10/2014 08:30	0.02535122	31/10/2014 08:30	.	
31/10/2014 08:45	0.03613554	31/10/2014 08:45	.	
31/10/2014 09:00	0.03685152	31/10/2014 09:00	.	0.2
31/10/2014 09:15	0.04108729	31/10/2014 09:15	.	
31/10/2014 09:30	0.03917915	31/10/2014 09:30	.	
31/10/2014 09:45	0.05080577	31/10/2014 09:45	.	
31/10/2014 10:00	0.04775976	31/10/2014 10:00	.	
31/10/2014 10:15	0.04667294	31/10/2014 10:15	.	
31/10/2014 10:30	0.04984819	31/10/2014 10:30	.	
31/10/2014 10:45	0.05046483	31/10/2014 10:45	.	
31/10/2014 11:00	0.04668186	31/10/2014 11:00	.	
31/10/2014 11:15	0.04857335	31/10/2014 11:15	.	
31/10/2014 11:30	0.04659474	31/10/2014 11:30	.	
31/10/2014 11:45	0.05071938	31/10/2014 11:45	.	
31/10/2014 12:00	0.0428989	31/10/2014 12:00	.	
31/10/2014 12:15	0.05034441	31/10/2014 12:15	.	
31/10/2014 12:30	0.04659474	31/10/2014 12:30	.	
31/10/2014 12:45	0.04022029	31/10/2014 12:45	.	
31/10/2014 13:00	0.03795539	31/10/2014 13:00	.	
31/10/2014 13:15	0.04813314	31/10/2014 13:15	.	
31/10/2014 13:30	0.03718162	31/10/2014 13:30	.	
31/10/2014 13:45	0.03933028	31/10/2014 13:45	.	
31/10/2014 14:00	0.04286928	31/10/2014 14:00	.	
31/10/2014 14:15	0.03923396	31/10/2014 14:15	.	
31/10/2014 14:30	0.0353074	31/10/2014 14:30	.	
31/10/2014 14:45	0.04016678	31/10/2014 14:45	.	
31/10/2014 15:00	0.03732971	31/10/2014 15:00	.	
31/10/2014 15:15	0.04446743	31/10/2014 15:15	.	
31/10/2014 15:30	0.03518827	31/10/2014 15:30	.	
31/10/2014 15:45	0.03451	31/10/2014 15:45	.	
31/10/2014 16:00	0.04251281	31/10/2014 16:00	.	
31/10/2014 16:15	0.04093933	31/10/2014 16:15	.	
31/10/2014 16:30	0.04727525	31/10/2014 16:30	.	
31/10/2014 16:45	0.0511472	31/10/2014 16:45	.	
31/10/2014 17:00	0.04051554	31/10/2014 17:00	.	
31/10/2014 17:15	0.03419752	31/10/2014 17:15	.	
31/10/2014 17:30	0.03925786	31/10/2014 17:30	.	
31/10/2014 17:45	0.039597	31/10/2014 17:45	.	
31/10/2014 18:00	0.03933247	31/10/2014 18:00	.	
31/10/2014 18:15	0.03864781	31/10/2014 18:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
31/10/2014 18:30	0.04700483	31/10/2014 18:30	.	
31/10/2014 18:45	0.04330563	31/10/2014 18:45	.	
31/10/2014 19:00	0.04251281	31/10/2014 19:00	.	
31/10/2014 19:15	0.04225935	31/10/2014 19:15	.	
31/10/2014 19:30	0.05167592	31/10/2014 19:30	.	
31/10/2014 19:45	0.04516328	31/10/2014 19:45	.	
31/10/2014 20:00	0.03981801	31/10/2014 20:00	.	
31/10/2014 20:15	0.03812337	31/10/2014 20:15	.	
31/10/2014 20:30	0.0437553	31/10/2014 20:30	.	
31/10/2014 20:45	0.0438521	31/10/2014 20:45	.	
31/10/2014 21:00	0.04207589	31/10/2014 21:00	.	
31/10/2014 21:15	0.04035978	31/10/2014 21:15	.	
31/10/2014 21:30	0.04367151	31/10/2014 21:30	.	
31/10/2014 21:45	0.05032345	31/10/2014 21:45	.	
31/10/2014 22:00	0.04667294	31/10/2014 22:00	.	
31/10/2014 22:15	0.04005382	31/10/2014 22:15	.	
31/10/2014 22:30	0.0425862	31/10/2014 22:30	.	
31/10/2014 22:45	0.04041559	31/10/2014 22:45	.	
31/10/2014 23:00	0.03698417	31/10/2014 23:00	.	
31/10/2014 23:15	0.04623405	31/10/2014 23:15	.	
31/10/2014 23:30	0.0395151	31/10/2014 23:30	.	
31/10/2014 23:45	0.04489026	31/10/2014 23:45	.	
01/11/2014 00:00	0.04242412	01/11/2014 00:00	.	
01/11/2014 00:15	0.03377198	01/11/2014 00:15	.	
01/11/2014 00:30	0.04375521	01/11/2014 00:30	.	
01/11/2014 00:45	0.03703188	01/11/2014 00:45	.	
01/11/2014 01:00	0.03688402	01/11/2014 01:00	.	
01/11/2014 01:15	0.03552325	01/11/2014 01:15	.	
01/11/2014 01:30	0.03735435	01/11/2014 01:30	.	
01/11/2014 01:45	0.0435402	01/11/2014 01:45	.	
01/11/2014 02:00	0.03121188	01/11/2014 02:00	.	
01/11/2014 02:15	0.03939335	01/11/2014 02:15	.	
01/11/2014 02:30	0.03583686	01/11/2014 02:30	.	
01/11/2014 02:45	0.03474001	01/11/2014 02:45	.	
01/11/2014 03:00	0.02971001	01/11/2014 03:00	.	
01/11/2014 03:15	0.02703531	01/11/2014 03:15	.	
01/11/2014 03:30	0.02643405	01/11/2014 03:30	.	
01/11/2014 03:45	0.02611849	01/11/2014 03:45	.	
01/11/2014 04:00	0.02772887	01/11/2014 04:00	.	
01/11/2014 04:15	0.0287565	01/11/2014 04:15	.	
01/11/2014 04:30	0.02008619	01/11/2014 04:30	.	
01/11/2014 04:45	0.02325463	01/11/2014 04:45	.	
01/11/2014 05:00	0.02817276	01/11/2014 05:00	.	
01/11/2014 05:15	0.02448076	01/11/2014 05:15	.	
01/11/2014 05:30	0.02185767	01/11/2014 05:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
01/11/2014 05:45	0.01959118	01/11/2014 05:45	.	
01/11/2014 06:00	0.02236133	01/11/2014 06:00	.	
01/11/2014 06:15	0.0283024	01/11/2014 06:15	.	
01/11/2014 06:30	0.02780438	01/11/2014 06:30	.	
01/11/2014 06:45	0.02357114	01/11/2014 06:45	.	
01/11/2014 07:00	0.02481621	01/11/2014 07:00	.	
01/11/2014 07:15	0.01809283	01/11/2014 07:15	.	
01/11/2014 07:30	0.02563515	01/11/2014 07:30	.	
01/11/2014 07:45	0.02412416	01/11/2014 07:45	.	
01/11/2014 08:00	0.02499578	01/11/2014 08:00	.	
01/11/2014 08:15	0.03338006	01/11/2014 08:15	.	
01/11/2014 08:30	0.03206155	01/11/2014 08:30	.	
01/11/2014 08:45	0.03267612	01/11/2014 08:45	.	
01/11/2014 09:00	0.03015591	01/11/2014 09:00	.	0
01/11/2014 09:15	0.03532531	01/11/2014 09:15	.	
01/11/2014 09:30	0.0326218	01/11/2014 09:30	.	
01/11/2014 09:45	0.04259822	01/11/2014 09:45	.	
01/11/2014 10:00	0.03914732	01/11/2014 10:00	.	
01/11/2014 10:15	0.04705792	01/11/2014 10:15	.	
01/11/2014 10:30	0.05024645	01/11/2014 10:30	.	
01/11/2014 10:45	0.0644566	01/11/2014 10:45	.	
01/11/2014 11:00	0.04932994	01/11/2014 11:00	.	
01/11/2014 11:15	0.04915311	01/11/2014 11:15	.	
01/11/2014 11:30	0.04992309	01/11/2014 11:30	.	
01/11/2014 11:45	0.04752796	01/11/2014 11:45	.	
01/11/2014 12:00	0.04645817	01/11/2014 12:00	.	
01/11/2014 12:15	0.05685291	01/11/2014 12:15	.	
01/11/2014 12:30	0.0538695	01/11/2014 12:30	.	
01/11/2014 12:45	0.04959448	01/11/2014 12:45	.	
01/11/2014 13:00	0.04241519	01/11/2014 13:00	.	
01/11/2014 13:15	0.0405142	01/11/2014 13:15	.	
01/11/2014 13:30	0.05009116	01/11/2014 13:30	.	
01/11/2014 13:45	0.04959334	01/11/2014 13:45	.	
01/11/2014 14:00	0.04156223	01/11/2014 14:00	.	
01/11/2014 14:15	0.04776809	01/11/2014 14:15	.	
01/11/2014 14:30	0.04229233	01/11/2014 14:30	.	
01/11/2014 14:45	0.04656566	01/11/2014 14:45	.	
01/11/2014 15:00	0.03856728	01/11/2014 15:00	.	
01/11/2014 15:15	0.04071828	01/11/2014 15:15	.	
01/11/2014 15:30	0.03749179	01/11/2014 15:30	.	
01/11/2014 15:45	0.04511859	01/11/2014 15:45	.	
01/11/2014 16:00	0.04349686	01/11/2014 16:00	.	
01/11/2014 16:15	0.03737668	01/11/2014 16:15	.	
01/11/2014 16:30	0.04942361	01/11/2014 16:30	.	
01/11/2014 16:45	0.04366659	01/11/2014 16:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
01/11/2014 17:00	0.03281434	01/11/2014 17:00	.	
01/11/2014 17:15	0.0396748	01/11/2014 17:15	.	
01/11/2014 17:30	0.03421985	01/11/2014 17:30	.	
01/11/2014 17:45	0.04285835	01/11/2014 17:45	.	
01/11/2014 18:00	0.04138646	01/11/2014 18:00	.	
01/11/2014 18:15	0.04446743	01/11/2014 18:15	.	
01/11/2014 18:30	0.04138646	01/11/2014 18:30	.	
01/11/2014 18:45	0.04035947	01/11/2014 18:45	.	
01/11/2014 19:00	0.04129266	01/11/2014 19:00	.	
01/11/2014 19:15	0.04400316	01/11/2014 19:15	.	
01/11/2014 19:30	0.03994444	01/11/2014 19:30	.	
01/11/2014 19:45	0.04982158	01/11/2014 19:45	.	
01/11/2014 20:00	0.04594284	01/11/2014 20:00	.	
01/11/2014 20:15	0.03973697	01/11/2014 20:15	.	
01/11/2014 20:30	0.03754667	01/11/2014 20:30	.	
01/11/2014 20:45	0.04265738	01/11/2014 20:45	.	
01/11/2014 21:00	0.04584212	01/11/2014 21:00	.	
01/11/2014 21:15	0.04143528	01/11/2014 21:15	.	
01/11/2014 21:30	0.04752977	01/11/2014 21:30	.	
01/11/2014 21:45	0.05131217	01/11/2014 21:45	.	
01/11/2014 22:00	0.03812337	01/11/2014 22:00	.	
01/11/2014 22:15	0.04260811	01/11/2014 22:15	.	
01/11/2014 22:30	0.03877173	01/11/2014 22:30	.	
01/11/2014 22:45	0.04216727	01/11/2014 22:45	.	
01/11/2014 23:00	0.04458605	01/11/2014 23:00	.	
01/11/2014 23:15	0.04241345	01/11/2014 23:15	.	
01/11/2014 23:30	0.04241345	01/11/2014 23:30	.	
01/11/2014 23:45	0.04061439	01/11/2014 23:45	.	
02/11/2014 00:00	0.03688393	02/11/2014 00:00	.	
02/11/2014 00:15	0.04522621	02/11/2014 00:15	.	
02/11/2014 00:30	0.03850725	02/11/2014 00:30	.	
02/11/2014 00:45	0.04175857	02/11/2014 00:45	.	
02/11/2014 01:00	0.03548372	02/11/2014 01:00	.	
02/11/2014 01:15	0.04186673	02/11/2014 01:15	.	
02/11/2014 01:30	0.03703188	02/11/2014 01:30	.	
02/11/2014 01:45	0.03101249	02/11/2014 01:45	.	
02/11/2014 02:00	0.03151971	02/11/2014 02:00	.	
02/11/2014 02:15	0.03177407	02/11/2014 02:15	.	
02/11/2014 02:30	0.03464212	02/11/2014 02:30	.	
02/11/2014 02:45	0.03289616	02/11/2014 02:45	.	
02/11/2014 03:00	0.0250304	02/11/2014 03:00	.	
02/11/2014 03:15	0.0287565	02/11/2014 03:15	.	
02/11/2014 03:30	0.017425	02/11/2014 03:30	.	
02/11/2014 03:45	0.02061843	02/11/2014 03:45	.	
02/11/2014 04:00	0.0243441	02/11/2014 04:00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
02/11/2014 04:15	0.02299139	02/11/2014 04:15	.	
02/11/2014 04:30	0.03220464	02/11/2014 04:30	.	
02/11/2014 04:45	0.02878258	02/11/2014 04:45	.	
02/11/2014 05:00	0.02687093	02/11/2014 05:00	.	
02/11/2014 05:15	0.02757086	02/11/2014 05:15	.	
02/11/2014 05:30	0.02087565	02/11/2014 05:30	.	
02/11/2014 05:45	0.02697683	02/11/2014 05:45	.	
02/11/2014 06:00	0.0244302	02/11/2014 06:00	.	
02/11/2014 06:15	0.0236205	02/11/2014 06:15	.	
02/11/2014 06:30	0.02357114	02/11/2014 06:30	.	
02/11/2014 06:45	0.02412416	02/11/2014 06:45	.	
02/11/2014 07:00	0.02270509	02/11/2014 07:00	.	
02/11/2014 07:15	0.02851934	02/11/2014 07:15	.	
02/11/2014 07:30	0.03615318	02/11/2014 07:30	.	
02/11/2014 07:45	0.03155751	02/11/2014 07:45	.	
02/11/2014 08:00	0.02341154	02/11/2014 08:00	.	
02/11/2014 08:15	0.02672217	02/11/2014 08:15	.	
02/11/2014 08:30	0.02705584	02/11/2014 08:30	.	
02/11/2014 08:45	0.03378406	02/11/2014 08:45	.	
02/11/2014 09:00	0.03083319	02/11/2014 09:00	.	0
02/11/2014 09:15	0.03011613	02/11/2014 09:15	.	
02/11/2014 09:30	0.03056301	02/11/2014 09:30	.	
02/11/2014 09:45	0.03853778	02/11/2014 09:45	.	
02/11/2014 10:00	0.03255132	02/11/2014 10:00	.	
02/11/2014 10:15	0.02938975	02/11/2014 10:15	.	
02/11/2014 10:30	0.03753068	02/11/2014 10:30	.	
02/11/2014 10:45	0.04657	02/11/2014 10:45	.	
02/11/2014 11:00	0.04234731	02/11/2014 11:00	.	
02/11/2014 11:15	0.04557779	02/11/2014 11:15	.	
02/11/2014 11:30	0.0699173	02/11/2014 11:30	.	
02/11/2014 11:45	0.03835934	02/11/2014 11:45	.	
02/11/2014 12:00	0.05592399	02/11/2014 12:00	.	
02/11/2014 12:15	0.06332692	02/11/2014 12:15	.	
02/11/2014 12:30	0.04327719	02/11/2014 12:30	.	
02/11/2014 12:45	0.04776809	02/11/2014 12:45	.	
02/11/2014 13:00	0.04656566	02/11/2014 13:00	.	
02/11/2014 13:15	0.04656566	02/11/2014 13:15	.	
02/11/2014 13:30	0.04557779	02/11/2014 13:30	.	
02/11/2014 13:45	0.05183176	02/11/2014 13:45	0.4	
02/11/2014 14:00	0.04873628	02/11/2014 14:00	1.8	
02/11/2014 14:15	0.05690955	02/11/2014 14:15	1.4	
02/11/2014 14:30	0.10926725	02/11/2014 14:30	.	
02/11/2014 14:45	0.11289985	02/11/2014 14:45	0.2	
02/11/2014 15:00	0.1236964	02/11/2014 15:00	.	
02/11/2014 15:15	0.11525358	02/11/2014 15:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
02/11/2014 15:30	0.10875159	02/11/2014 15:30	.	
02/11/2014 15:45	0.11067115	02/11/2014 15:45	.	
02/11/2014 16:00	0.09141596	02/11/2014 16:00	0.2	
02/11/2014 16:15	0.08168718	02/11/2014 16:15	.	
02/11/2014 16:30	0.0849206	02/11/2014 16:30	.	
02/11/2014 16:45	0.07519652	02/11/2014 16:45	.	
02/11/2014 17:00	0.07228889	02/11/2014 17:00	.	
02/11/2014 17:15	0.06557545	02/11/2014 17:15	.	
02/11/2014 17:30	0.0738207	02/11/2014 17:30	.	
02/11/2014 17:45	0.07097591	02/11/2014 17:45	.	
02/11/2014 18:00	0.06137927	02/11/2014 18:00	.	
02/11/2014 18:15	0.07276142	02/11/2014 18:15	.	
02/11/2014 18:30	0.06290216	02/11/2014 18:30	0.2	
02/11/2014 18:45	0.05377289	02/11/2014 18:45	.	
02/11/2014 19:00	0.06033555	02/11/2014 19:00	.	
02/11/2014 19:15	0.05981994	02/11/2014 19:15	.	
02/11/2014 19:30	0.07128079	02/11/2014 19:30	.	
02/11/2014 19:45	0.05930665	02/11/2014 19:45	.	
02/11/2014 20:00	0.06679611	02/11/2014 20:00	.	
02/11/2014 20:15	0.06530122	02/11/2014 20:15	.	
02/11/2014 20:30	0.06334767	02/11/2014 20:30	.	
02/11/2014 20:45	0.05581736	02/11/2014 20:45	.	
02/11/2014 21:00	0.06585777	02/11/2014 21:00	.	
02/11/2014 21:15	0.07028419	02/11/2014 21:15	.	
02/11/2014 21:30	0.06474708	02/11/2014 21:30	.	
02/11/2014 21:45	0.05831748	02/11/2014 21:45	.	
02/11/2014 22:00	0.06223184	02/11/2014 22:00	.	
02/11/2014 22:15	0.05974855	02/11/2014 22:15	.	
02/11/2014 22:30	0.06745084	02/11/2014 22:30	.	
02/11/2014 22:45	0.05775635	02/11/2014 22:45	.	
02/11/2014 23:00	0.05679667	02/11/2014 23:00	.	
02/11/2014 23:15	0.05201288	02/11/2014 23:15	.	
02/11/2014 23:30	0.05010814	02/11/2014 23:30	.	
02/11/2014 23:45	0.05629855	02/11/2014 23:45	.	
03/11/2014 00:00	0.05485764	03/11/2014 00:00	.	
03/11/2014 00:15	0.05580272	03/11/2014 00:15	.	
03/11/2014 00:30	0.04968236	03/11/2014 00:30	.	
03/11/2014 00:45	0.05863794	03/11/2014 00:45	.	
03/11/2014 01:00	0.0610604	03/11/2014 01:00	.	
03/11/2014 01:15	0.05863794	03/11/2014 01:15	.	
03/11/2014 01:30	0.06619854	03/11/2014 01:30	.	
03/11/2014 01:45	0.05765368	03/11/2014 01:45	.	
03/11/2014 02:00	0.05621375	03/11/2014 02:00	.	
03/11/2014 02:15	0.04925068	03/11/2014 02:15	.	
03/11/2014 02:30	0.05377753	03/11/2014 02:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
03/11/2014 02:45	0.04484001	03/11/2014 02:45	.	
03/11/2014 03:00	0.04658194	03/11/2014 03:00	.	
03/11/2014 03:15	0.04235681	03/11/2014 03:15	.	
03/11/2014 03:30	0.03487827	03/11/2014 03:30	.	
03/11/2014 03:45	0.03535384	03/11/2014 03:45	.	
03/11/2014 04:00	0.0313973	03/11/2014 04:00	.	
03/11/2014 04:15	0.02935516	03/11/2014 04:15	.	
03/11/2014 04:30	0.02942301	03/11/2014 04:30	.	
03/11/2014 04:45	0.02780269	03/11/2014 04:45	.	
03/11/2014 05:00	0.02911916	03/11/2014 05:00	.	
03/11/2014 05:15	0.0278405	03/11/2014 05:15	.	
03/11/2014 05:30	0.03398237	03/11/2014 05:30	.	
03/11/2014 05:45	0.03390747	03/11/2014 05:45	.	
03/11/2014 06:00	0.02538288	03/11/2014 06:00	.	
03/11/2014 06:15	0.02745075	03/11/2014 06:15	0.2	
03/11/2014 06:30	0.02768246	03/11/2014 06:30	0.8	
03/11/2014 06:45	0.02888702	03/11/2014 06:45	0.8	
03/11/2014 07:00	0.02956447	03/11/2014 07:00	0.4	
03/11/2014 07:15	0.0342902	03/11/2014 07:15	.	
03/11/2014 07:30	0.04640772	03/11/2014 07:30	0.2	
03/11/2014 07:45	0.06609266	03/11/2014 07:45	0.2	
03/11/2014 08:00	0.07215165	03/11/2014 08:00	.	
03/11/2014 08:15	0.07288606	03/11/2014 08:15	.	
03/11/2014 08:30	0.07017632	03/11/2014 08:30	.	
03/11/2014 08:45	0.06823642	03/11/2014 08:45	.	
03/11/2014 09:00	0.06241469	03/11/2014 09:00	.	6.8
03/11/2014 09:15	0.06819886	03/11/2014 09:15	.	
03/11/2014 09:30	0.0629227	03/11/2014 09:30	.	
03/11/2014 09:45	0.0543113	03/11/2014 09:45	.	
03/11/2014 10:00	0.0563382	03/11/2014 10:00	.	
03/11/2014 10:15	0.04729704	03/11/2014 10:15	.	
03/11/2014 10:30	0.06079221	03/11/2014 10:30	.	
03/11/2014 10:45	0.04654089	03/11/2014 10:45	0.2	
03/11/2014 11:00	0.04926473	03/11/2014 11:00	.	
03/11/2014 11:15	0.04968229	03/11/2014 11:15	0.2	
03/11/2014 11:30	0.05053346	03/11/2014 11:30	0.2	
03/11/2014 11:45	0.05432731	03/11/2014 11:45	0.2	
03/11/2014 12:00	0.04994624	03/11/2014 12:00	0.2	
03/11/2014 12:15	0.05121415	03/11/2014 12:15	0.2	
03/11/2014 12:30	0.06894655	03/11/2014 12:30	.	
03/11/2014 12:45	0.05919588	03/11/2014 12:45	0.2	
03/11/2014 13:00	0.07309214	03/11/2014 13:00	.	
03/11/2014 13:15	0.07412285	03/11/2014 13:15	.	
03/11/2014 13:30	0.06400781	03/11/2014 13:30	.	
03/11/2014 13:45	0.07092971	03/11/2014 13:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
03/11/2014 14:00	0.06714969	03/11/2014 14:00	.	
03/11/2014 14:15	0.07596807	03/11/2014 14:15	.	
03/11/2014 14:30	0.06240944	03/11/2014 14:30	.	
03/11/2014 14:45	0.05363168	03/11/2014 14:45	.	
03/11/2014 15:00	0.061904	03/11/2014 15:00	0.2	
03/11/2014 15:15	0.06552314	03/11/2014 15:15	0.4	
03/11/2014 15:30	0.06872344	03/11/2014 15:30	2.4	
03/11/2014 15:45	0.09823641	03/11/2014 15:45	0.6	
03/11/2014 16:00	0.15026842	03/11/2014 16:00	1.2	
03/11/2014 16:15	0.17431543	03/11/2014 16:15	0.6	
03/11/2014 16:30	0.22933296	03/11/2014 16:30	0.2	
03/11/2014 16:45	0.20441246	03/11/2014 16:45	.	
03/11/2014 17:00	0.19910431	03/11/2014 17:00	.	
03/11/2014 17:15	0.15753877	03/11/2014 17:15	.	
03/11/2014 17:30	0.14456408	03/11/2014 17:30	.	
03/11/2014 17:45	0.12380665	03/11/2014 17:45	.	
03/11/2014 18:00	0.11567526	03/11/2014 18:00	.	
03/11/2014 18:15	0.1068835	03/11/2014 18:15	.	
03/11/2014 18:30	0.10366767	03/11/2014 18:30	.	
03/11/2014 18:45	0.09892064	03/11/2014 18:45	.	
03/11/2014 19:00	0.09053127	03/11/2014 19:00	.	
03/11/2014 19:15	0.09246978	03/11/2014 19:15	.	
03/11/2014 19:30	0.08495359	03/11/2014 19:30	.	
03/11/2014 19:45	0.08801918	03/11/2014 19:45	.	
03/11/2014 20:00	0.09076805	03/11/2014 20:00	.	
03/11/2014 20:15	0.0764345	03/11/2014 20:15	.	
03/11/2014 20:30	0.08175627	03/11/2014 20:30	.	
03/11/2014 20:45	0.07675639	03/11/2014 20:45	.	
03/11/2014 21:00	0.07935353	03/11/2014 21:00	.	
03/11/2014 21:15	0.08364803	03/11/2014 21:15	.	
03/11/2014 21:30	0.07331148	03/11/2014 21:30	.	
03/11/2014 21:45	0.06739351	03/11/2014 21:45	.	
03/11/2014 22:00	0.07460407	03/11/2014 22:00	.	
03/11/2014 22:15	0.06587073	03/11/2014 22:15	.	
03/11/2014 22:30	0.0687839	03/11/2014 22:30	.	
03/11/2014 22:45	0.07229531	03/11/2014 22:45	.	
03/11/2014 23:00	0.06829896	03/11/2014 23:00	.	
03/11/2014 23:15	0.06552117	03/11/2014 23:15	.	
03/11/2014 23:30	0.06834674	03/11/2014 23:30	.	
03/11/2014 23:45	0.0661307	03/11/2014 23:45	.	
04/11/2014 00:00	0.06338881	04/11/2014 00:00	.	
04/11/2014 00:15	0.06068009	04/11/2014 00:15	.	
04/11/2014 00:30	0.0715963	04/11/2014 00:30	.	
04/11/2014 00:45	0.06725039	04/11/2014 00:45	.	
04/11/2014 01:00	0.06506029	04/11/2014 01:00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
04/11/2014 01:15	0.06998802	04/11/2014 01:15	.	
04/11/2014 01:30	0.07105262	04/11/2014 01:30	.	
04/11/2014 01:45	0.07365595	04/11/2014 01:45	.	
04/11/2014 02:00	0.06720439	04/11/2014 02:00	.	
04/11/2014 02:15	0.06452678	04/11/2014 02:15	.	
04/11/2014 02:30	0.06397208	04/11/2014 02:30	.	
04/11/2014 02:45	0.06133959	04/11/2014 02:45	.	
04/11/2014 03:00	0.05534997	04/11/2014 03:00	.	
04/11/2014 03:15	0.05781389	04/11/2014 03:15	.	
04/11/2014 03:30	0.05732301	04/11/2014 03:30	.	
04/11/2014 03:45	0.06125008	04/11/2014 03:45	.	
04/11/2014 04:00	0.05877417	04/11/2014 04:00	.	
04/11/2014 04:15	0.0563382	04/11/2014 04:15	.	
04/11/2014 04:30	0.06462048	04/11/2014 04:30	0.2	
04/11/2014 04:45	0.05438943	04/11/2014 04:45	.	
04/11/2014 05:00	0.05633005	04/11/2014 05:00	.	
04/11/2014 05:15	0.0582641	04/11/2014 05:15	.	
04/11/2014 05:30	0.05391249	04/11/2014 05:30	.	
04/11/2014 05:45	0.05967573	04/11/2014 05:45	.	
04/11/2014 06:00	0.0548773	04/11/2014 06:00	.	
04/11/2014 06:15	0.05629855	04/11/2014 06:15	.	
04/11/2014 06:30	0.05679667	04/11/2014 06:30	.	
04/11/2014 06:45	0.0568254	04/11/2014 06:45	.	
04/11/2014 07:00	0.06125008	04/11/2014 07:00	.	
04/11/2014 07:15	0.05881207	04/11/2014 07:15	.	
04/11/2014 07:30	0.05828697	04/11/2014 07:30	.	
04/11/2014 07:45	0.0543851	04/11/2014 07:45	.	
04/11/2014 08:00	0.05063044	04/11/2014 08:00	.	
04/11/2014 08:15	0.05154988	04/11/2014 08:15	.	
04/11/2014 08:30	0.05725092	04/11/2014 08:30	.	
04/11/2014 08:45	0.05631682	04/11/2014 08:45	.	
04/11/2014 09:00	0.05877417	04/11/2014 09:00	.	7.2
04/11/2014 09:15	0.05926136	04/11/2014 09:15	.	
04/11/2014 09:30	0.05290506	04/11/2014 09:30	.	
04/11/2014 09:45	0.04990954	04/11/2014 09:45	.	
04/11/2014 10:00	0.05534997	04/11/2014 10:00	.	
04/11/2014 10:15	0.05584456	04/11/2014 10:15	.	
04/11/2014 10:30	0.05483697	04/11/2014 10:30	.	
04/11/2014 10:45	0.07010826	04/11/2014 10:45	.	
04/11/2014 11:00	0.07258393	04/11/2014 11:00	.	
04/11/2014 11:15	0.08344343	04/11/2014 11:15	.	
04/11/2014 11:30	0.07452961	04/11/2014 11:30	.	
04/11/2014 11:45	0.06670287	04/11/2014 11:45	.	
04/11/2014 12:00	0.0559677	04/11/2014 12:00	.	
04/11/2014 12:15	0.05868936	04/11/2014 12:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
04/11/2014 12:30	0.06136747	04/11/2014 12:30	.	
04/11/2014 12:45	0.06085345	04/11/2014 12:45	.	
04/11/2014 13:00	0.05292786	04/11/2014 13:00	.	
04/11/2014 13:15	0.04827566	04/11/2014 13:15	.	
04/11/2014 13:30	0.04832736	04/11/2014 13:30	.	
04/11/2014 13:45	0.04340719	04/11/2014 13:45	.	
04/11/2014 14:00	0.04792279	04/11/2014 14:00	.	
04/11/2014 14:15	0.05284324	04/11/2014 14:15	.	
04/11/2014 14:30	0.0488178	04/11/2014 14:30	.	
04/11/2014 14:45	0.04597768	04/11/2014 14:45	.	
04/11/2014 15:00	0.05106051	04/11/2014 15:00	.	
04/11/2014 15:15	0.05629855	04/11/2014 15:15	.	
04/11/2014 15:30	0.05296467	04/11/2014 15:30	.	
04/11/2014 15:45	0.05340563	04/11/2014 15:45	.	
04/11/2014 16:00	0.04747548	04/11/2014 16:00	.	
04/11/2014 16:15	0.0409267	04/11/2014 16:15	.	
04/11/2014 16:30	0.04107085	04/11/2014 16:30	.	
04/11/2014 16:45	0.04033005	04/11/2014 16:45	.	
04/11/2014 17:00	0.03490846	04/11/2014 17:00	.	
04/11/2014 17:15	0.03241062	04/11/2014 17:15	.	
04/11/2014 17:30	0.03141865	04/11/2014 17:30	.	
04/11/2014 17:45	0.02972783	04/11/2014 17:45	.	
04/11/2014 18:00	0.03451	04/11/2014 18:00	.	
04/11/2014 18:15	0.03078046	04/11/2014 18:15	.	
04/11/2014 18:30	0.02977261	04/11/2014 18:30	.	
04/11/2014 18:45	0.03722306	04/11/2014 18:45	.	
04/11/2014 19:00	0.03351286	04/11/2014 19:00	.	
04/11/2014 19:15	0.03008955	04/11/2014 19:15	.	
04/11/2014 19:30	0.03940295	04/11/2014 19:30	.	
04/11/2014 19:45	0.04029969	04/11/2014 19:45	.	
04/11/2014 20:00	0.04592527	04/11/2014 20:00	.	
04/11/2014 20:15	0.04267793	04/11/2014 20:15	.	
04/11/2014 20:30	0.03876182	04/11/2014 20:30	.	
04/11/2014 20:45	0.03607883	04/11/2014 20:45	.	
04/11/2014 21:00	0.03197101	04/11/2014 21:00	.	
04/11/2014 21:15	0.03798104	04/11/2014 21:15	.	
04/11/2014 21:30	0.03836865	04/11/2014 21:30	.	
04/11/2014 21:45	0.0398952	04/11/2014 21:45	.	
04/11/2014 22:00	0.03760538	04/11/2014 22:00	.	
04/11/2014 22:15	0.03875029	04/11/2014 22:15	.	
04/11/2014 22:30	0.04062912	04/11/2014 22:30	.	
04/11/2014 22:45	0.04264537	04/11/2014 22:45	.	
04/11/2014 23:00	0.04676737	04/11/2014 23:00	.	
04/11/2014 23:15	0.04937191	04/11/2014 23:15	.	
04/11/2014 23:30	0.04780105	04/11/2014 23:30	.	

G5 flow			Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}		Date & Time	Rainfall (mm)	Daily Rainfall (mm)
04/11/2014 23:45	0.04825569		04/11/2014 23:45	.	
05/11/2014 00:00	0.04696273		05/11/2014 00:00	.	
05/11/2014 00:15	0.04318034		05/11/2014 00:15	.	
05/11/2014 00:30	0.03953853		05/11/2014 00:30	.	
05/11/2014 00:45	0.03904083		05/11/2014 00:45	0.2	
05/11/2014 01:00	0.02865764		05/11/2014 01:00	.	
05/11/2014 01:15	0.02813231		05/11/2014 01:15	0.2	
05/11/2014 01:30	0.03003846		05/11/2014 01:30	0.2	
05/11/2014 01:45	0.02809598		05/11/2014 01:45	0.6	
05/11/2014 02:00	0.02742378		05/11/2014 02:00	0.4	
05/11/2014 02:15	0.02535122		05/11/2014 02:15	0.2	
05/11/2014 02:30	0.03231686		05/11/2014 02:30	0.4	
05/11/2014 02:45	0.0485754		05/11/2014 02:45	1.6	
05/11/2014 03:00	0.06721625		05/11/2014 03:00	1.6	
05/11/2014 03:15	0.10232886		05/11/2014 03:15	0.8	
05/11/2014 03:30	0.17030427		05/11/2014 03:30	0.4	
05/11/2014 03:45	0.1703796		05/11/2014 03:45	0.6	
05/11/2014 04:00	0.20729095		05/11/2014 04:00	1.8	
05/11/2014 04:15	0.23826593		05/11/2014 04:15	1.2	
05/11/2014 04:30	0.23473358		05/11/2014 04:30	0.6	
05/11/2014 04:45	0.19868001		05/11/2014 04:45	0.6	
05/11/2014 05:00	0.20060357		05/11/2014 05:00	1	
05/11/2014 05:15	0.21282078		05/11/2014 05:15	1.2	
05/11/2014 05:30	0.28824128		05/11/2014 05:30	0.6	
05/11/2014 05:45	0.34468291		05/11/2014 05:45	0.4	
05/11/2014 06:00	0.3469048		05/11/2014 06:00	0.6	
05/11/2014 06:15	0.34131633		05/11/2014 06:15	0.2	
05/11/2014 06:30	0.28692267		05/11/2014 06:30	0.2	
05/11/2014 06:45	0.28931097		05/11/2014 06:45	1.8	
05/11/2014 07:00	0.58779402		05/11/2014 07:00	1	
05/11/2014 07:15	0.76141826		05/11/2014 07:15	1	
05/11/2014 07:30	0.82030859		05/11/2014 07:30	1.2	
05/11/2014 07:45	0.82630812		05/11/2014 07:45	1.6	
05/11/2014 08:00	0.86841871		05/11/2014 08:00	0.4	
05/11/2014 08:15	0.85620954		05/11/2014 08:15	0.6	
05/11/2014 08:30	0.74765635		05/11/2014 08:30	0.2	
05/11/2014 08:45	0.9074587		05/11/2014 08:45	0.4	
05/11/2014 09:00	1.11074904	E, Int	05/11/2014 09:00	2.6	26.4
05/11/2014 09:15	1.31403938	E, Int	05/11/2014 09:15	1.4	
05/11/2014 09:30	1.51732973		05/11/2014 09:30	0.4	
05/11/2014 09:45	1.62501657		05/11/2014 09:45	0.4	
05/11/2014 10:00	1.42665165		05/11/2014 10:00	.	
05/11/2014 10:15	1.2680139		05/11/2014 10:15	0.2	
05/11/2014 10:30	1.16139022		05/11/2014 10:30	.	
05/11/2014 10:45	1.13854728		05/11/2014 10:45	.	

G5 flow			Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}		Date & Time	Rainfall (mm)	Daily Rainfall (mm)
05/11/2014 11:00	1.0561266		05/11/2014 11:00	.	
05/11/2014 11:15	1.00404664		05/11/2014 11:15	.	
05/11/2014 11:30	0.9837099		05/11/2014 11:30	.	
05/11/2014 11:45	0.99017907		05/11/2014 11:45	.	
05/11/2014 12:00	0.84799978		05/11/2014 12:00	.	
05/11/2014 12:15	0.8525882		05/11/2014 12:15	.	
05/11/2014 12:30	0.8793864		05/11/2014 12:30	.	
05/11/2014 12:45	0.83608153		05/11/2014 12:45	.	
05/11/2014 13:00	0.82791642		05/11/2014 13:00	.	
05/11/2014 13:15	0.73283779		05/11/2014 13:15	.	
05/11/2014 13:30	0.72142051		05/11/2014 13:30	.	
05/11/2014 13:45	0.75940494		05/11/2014 13:45	0.2	
05/11/2014 14:00	0.74108067		05/11/2014 14:00	.	
05/11/2014 14:15	0.80201787		05/11/2014 14:15	0.2	
05/11/2014 14:30	0.71179418		05/11/2014 14:30	.	
05/11/2014 14:45	0.59804892		05/11/2014 14:45	.	
05/11/2014 15:00	0.72944363		05/11/2014 15:00	.	
05/11/2014 15:15	0.70424137		05/11/2014 15:15	.	
05/11/2014 15:30	0.8006692		05/11/2014 15:30	.	
05/11/2014 15:45	0.70088531		05/11/2014 15:45	.	
05/11/2014 16:00	0.75220324		05/11/2014 16:00	.	
05/11/2014 16:15	0.78287308		05/11/2014 16:15	.	
05/11/2014 16:30	0.66133546	E, Int	05/11/2014 16:30	.	
05/11/2014 16:45	0.53979784		05/11/2014 16:45	.	
05/11/2014 17:00	0.69352846		05/11/2014 17:00	.	
05/11/2014 17:15	0.70114278		05/11/2014 17:15	.	
05/11/2014 17:30	0.23912129		05/11/2014 17:30	.	
05/11/2014 17:45	0.60206807		05/11/2014 17:45	.	
05/11/2014 18:00	0.62014385		05/11/2014 18:00	.	
05/11/2014 18:15	0.62028882		05/11/2014 18:15	0.6	
05/11/2014 18:30	0.60688921		05/11/2014 18:30	1	
05/11/2014 18:45	0.68811545		05/11/2014 18:45	0.4	
05/11/2014 19:00	0.74835288	E, Int	05/11/2014 19:00	0.4	
05/11/2014 19:15	0.80859031		05/11/2014 19:15	0.4	
05/11/2014 19:30	0.78353071		05/11/2014 19:30	1.4	
05/11/2014 19:45	0.85007441		05/11/2014 19:45	2.2	
05/11/2014 20:00	1.2795636		05/11/2014 20:00	1.6	
05/11/2014 20:15	1.4363514		05/11/2014 20:15	0.6	
05/11/2014 20:30	1.47945776		05/11/2014 20:30	0.4	
05/11/2014 20:45	1.24128567		05/11/2014 20:45	0.8	
05/11/2014 21:00	1.15319497		05/11/2014 21:00	.	
05/11/2014 21:15	1.16774343		05/11/2014 21:15	0.4	
05/11/2014 21:30	1.14527845		05/11/2014 21:30	0.2	
05/11/2014 21:45	1.04775064		05/11/2014 21:45	.	
05/11/2014 22:00	1.07123269		05/11/2014 22:00	.	

G5 flow			Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}		Date & Time	Rainfall (mm)	Daily Rainfall (mm)
05/11/2014 22:15	1.01188275		05/11/2014 22:15	.	
05/11/2014 22:30	0.99247277		05/11/2014 22:30	.	
05/11/2014 22:45	0.91541595		05/11/2014 22:45	.	
05/11/2014 23:00	0.91422567		05/11/2014 23:00	.	
05/11/2014 23:15	0.91716814		05/11/2014 23:15	.	
05/11/2014 23:30	0.911837		05/11/2014 23:30	.	
05/11/2014 23:45	0.91087296		05/11/2014 23:45	.	
06/11/2014 00:00	0.8635651		06/11/2014 00:00	.	
06/11/2014 00:15	0.94163576		06/11/2014 00:15	.	
06/11/2014 00:30	0.84632452		06/11/2014 00:30	.	
06/11/2014 00:45	0.89357257		06/11/2014 00:45	.	
06/11/2014 01:00	0.80193229		06/11/2014 01:00	.	
06/11/2014 01:15	0.77612219		06/11/2014 01:15	.	
06/11/2014 01:30	0.82304339		06/11/2014 01:30	.	
06/11/2014 01:45	0.77723371		06/11/2014 01:45	.	
06/11/2014 02:00	0.67288111		06/11/2014 02:00	0.2	
06/11/2014 02:15	0.70631328		06/11/2014 02:15	.	
06/11/2014 02:30	0.76477028		06/11/2014 02:30	.	
06/11/2014 02:45	0.75087401		06/11/2014 02:45	.	
06/11/2014 03:00	0.66468065		06/11/2014 03:00	.	
06/11/2014 03:15	0.66224145	E, Int	06/11/2014 03:15	.	
06/11/2014 03:30	0.65980225	E, Int	06/11/2014 03:30	.	
06/11/2014 03:45	0.65736304	E, Int	06/11/2014 03:45	.	
06/11/2014 04:00	0.65492384		06/11/2014 04:00	.	
06/11/2014 04:15	0.43376615		06/11/2014 04:15	.	
06/11/2014 04:30	0.49516724	E, Int	06/11/2014 04:30	.	
06/11/2014 04:45	0.55656833		06/11/2014 04:45	.	
06/11/2014 05:00	0.53977053		06/11/2014 05:00	.	
06/11/2014 05:15	0.60340187		06/11/2014 05:15	.	
06/11/2014 05:30	0.55398519		06/11/2014 05:30	.	
06/11/2014 05:45	0.56679138		06/11/2014 05:45	.	
06/11/2014 06:00	0.50141386		06/11/2014 06:00	.	
06/11/2014 06:15	0.48795364		06/11/2014 06:15	.	
06/11/2014 06:30	0.48636796		06/11/2014 06:30	.	
06/11/2014 06:45	0.46085391		06/11/2014 06:45	.	
06/11/2014 07:00	0.4757737		06/11/2014 07:00	.	
06/11/2014 07:15	0.47585786		06/11/2014 07:15	.	
06/11/2014 07:30	0.44746355		06/11/2014 07:30	.	
06/11/2014 07:45	0.41559893		06/11/2014 07:45	.	
06/11/2014 08:00	0.41177826		06/11/2014 08:00	.	
06/11/2014 08:15	0.39493094		06/11/2014 08:15	.	
06/11/2014 08:30	0.40664957		06/11/2014 08:30	.	
06/11/2014 08:45	0.36297225		06/11/2014 08:45	.	
06/11/2014 09:00	0.34528324		06/11/2014 09:00	.	
06/11/2014 09:15	0.34896872		06/11/2014 09:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
06/11/2014 09:30	0.33303582	06/11/2014 09:30	.	
06/11/2014 09:45	0.31621333	06/11/2014 09:45	.	
06/11/2014 10:00	0.3040295	06/11/2014 10:00	.	
06/11/2014 10:15	0.31325219	06/11/2014 10:15	.	
06/11/2014 10:30	0.31397948	06/11/2014 10:30	.	
06/11/2014 10:45	0.30772215	06/11/2014 10:45	.	
06/11/2014 11:00	0.30152486	06/11/2014 11:00	.	
06/11/2014 11:15	0.26129942	06/11/2014 11:15	.	
06/11/2014 11:30	0.26386742	06/11/2014 11:30	.	
06/11/2014 11:45	0.24767023	06/11/2014 11:45	.	
06/11/2014 12:00	0.26253216	06/11/2014 12:00	.	
06/11/2014 12:15	0.26641371	06/11/2014 12:15	.	
06/11/2014 12:30	0.24828598	06/11/2014 12:30	.	
06/11/2014 12:45	0.23691275	06/11/2014 12:45	.	
06/11/2014 13:00	0.23160168	06/11/2014 13:00	.	
06/11/2014 13:15	0.22066965	06/11/2014 13:15	.	
06/11/2014 13:30	0.22079258	06/11/2014 13:30	.	
06/11/2014 13:45	0.22116362	06/11/2014 13:45	.	
06/11/2014 14:00	0.20253991	06/11/2014 14:00	.	
06/11/2014 14:15	0.19071151	06/11/2014 14:15	.	
06/11/2014 14:30	0.18217594	06/11/2014 14:30	.	
06/11/2014 14:45	0.17729062	06/11/2014 14:45	.	
06/11/2014 15:00	0.17661651	06/11/2014 15:00	.	
06/11/2014 15:15	0.15457208	06/11/2014 15:15	.	
06/11/2014 15:30	0.15054965	06/11/2014 15:30	.	
06/11/2014 15:45	0.15248825	06/11/2014 15:45	.	
06/11/2014 16:00	0.14809282	06/11/2014 16:00	.	
06/11/2014 16:15	0.16202892	06/11/2014 16:15	.	
06/11/2014 16:30	0.14961923	06/11/2014 16:30	.	
06/11/2014 16:45	0.12765271	06/11/2014 16:45	.	
06/11/2014 17:00	0.14100222	06/11/2014 17:00	.	
06/11/2014 17:15	0.12193969	06/11/2014 17:15	.	
06/11/2014 17:30	0.12330536	06/11/2014 17:30	.	
06/11/2014 17:45	0.10741765	06/11/2014 17:45	.	
06/11/2014 18:00	0.12630678	06/11/2014 18:00	.	
06/11/2014 18:15	0.12918348	06/11/2014 18:15	.	
06/11/2014 18:30	0.13693235	06/11/2014 18:30	.	
06/11/2014 18:45	0.12104151	06/11/2014 18:45	.	
06/11/2014 19:00	0.12371838	06/11/2014 19:00	.	
06/11/2014 19:15	0.12033449	06/11/2014 19:15	.	
06/11/2014 19:30	0.12100034	06/11/2014 19:30	.	
06/11/2014 19:45	0.11860985	06/11/2014 19:45	.	
06/11/2014 20:00	0.11094084	06/11/2014 20:00	.	
06/11/2014 20:15	0.11391228	06/11/2014 20:15	.	
06/11/2014 20:30	0.11631464	06/11/2014 20:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
06/11/2014 20:45	0.10864135	06/11/2014 20:45	.	
06/11/2014 21:00	0.11801001	06/11/2014 21:00	.	
06/11/2014 21:15	0.10872868	06/11/2014 21:15	.	
06/11/2014 21:30	0.11692566	06/11/2014 21:30	.	
06/11/2014 21:45	0.11291877	06/11/2014 21:45	.	
06/11/2014 22:00	0.11399515	06/11/2014 22:00	.	
06/11/2014 22:15	0.10757851	06/11/2014 22:15	.	
06/11/2014 22:30	0.11355875	06/11/2014 22:30	.	
06/11/2014 22:45	0.10412675	06/11/2014 22:45	.	
06/11/2014 23:00	0.09559452	06/11/2014 23:00	.	
06/11/2014 23:15	0.09812364	06/11/2014 23:15	.	
06/11/2014 23:30	0.06579456	06/11/2014 23:30	.	
06/11/2014 23:45	0.09939218	06/11/2014 23:45	.	
07/11/2014 00:00	0.10112308	07/11/2014 00:00	.	
07/11/2014 00:15	0.10355057	07/11/2014 00:15	.	
07/11/2014 00:30	0.09392829	07/11/2014 00:30	.	
07/11/2014 00:45	0.10151746	07/11/2014 00:45	.	
07/11/2014 01:00	0.10379215	07/11/2014 01:00	.	
07/11/2014 01:15	0.08937391	07/11/2014 01:15	.	
07/11/2014 01:30	0.0909794	07/11/2014 01:30	.	
07/11/2014 01:45	0.10099159	07/11/2014 01:45	.	
07/11/2014 02:00	0.09748495	07/11/2014 02:00	.	
07/11/2014 02:15	0.10028757	07/11/2014 02:15	.	
07/11/2014 02:30	0.08850201	07/11/2014 02:30		0.2
07/11/2014 02:45	0.09200226	07/11/2014 02:45	.	
07/11/2014 03:00	0.09750767	07/11/2014 03:00	.	
07/11/2014 03:15	0.0961389	07/11/2014 03:15	.	
07/11/2014 03:30	0.09273713	07/11/2014 03:30	.	
07/11/2014 03:45	0.09545545	07/11/2014 03:45	.	
07/11/2014 04:00	0.08396303	07/11/2014 04:00	.	
07/11/2014 04:15	0.09139931	07/11/2014 04:15	.	
07/11/2014 04:30	0.09477525	07/11/2014 04:30	.	
07/11/2014 04:45	0.0860411	07/11/2014 04:45	.	
07/11/2014 05:00	0.08875592	07/11/2014 05:00	.	
07/11/2014 05:15	0.09011182	07/11/2014 05:15		0.4
07/11/2014 05:30	0.08545963	07/11/2014 05:30		0.8
07/11/2014 05:45	0.08681475	07/11/2014 05:45		0.8
07/11/2014 06:00	0.09746268	07/11/2014 06:00		0.6
07/11/2014 06:15	0.12236296	07/11/2014 06:15		0.6
07/11/2014 06:30	0.14594456	07/11/2014 06:30		0.6
07/11/2014 06:45	0.15503398	07/11/2014 06:45		0.4
07/11/2014 07:00	0.1623538	07/11/2014 07:00		0.8
07/11/2014 07:15	0.17884789	07/11/2014 07:15		0.8
07/11/2014 07:30	0.2079934	07/11/2014 07:30		0.4
07/11/2014 07:45	0.19470397	07/11/2014 07:45		0.4

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
07/11/2014 08:00	0.19861679	07/11/2014 08:00	.	
07/11/2014 08:15	0.21968341	07/11/2014 08:15	.	
07/11/2014 08:30	0.1910404	07/11/2014 08:30	.	
07/11/2014 08:45	0.175846	07/11/2014 08:45	.	
07/11/2014 09:00	0.17048961	07/11/2014 09:00	.	
07/11/2014 09:15	0.1535571	07/11/2014 09:15	.	
07/11/2014 09:30	0.17206282	07/11/2014 09:30	.	
07/11/2014 09:45	0.16030359	07/11/2014 09:45	.	
07/11/2014 10:00	0.16219757	07/11/2014 10:00	.	
07/11/2014 10:15	0.17204028	07/11/2014 10:15	.	
07/11/2014 10:30	0.18941216	07/11/2014 10:30	.	
07/11/2014 10:45	0.20549439	07/11/2014 10:45	0.2	
07/11/2014 11:00	0.21863268	07/11/2014 11:00	.	
07/11/2014 11:15	0.24337115	07/11/2014 11:15	.	
07/11/2014 11:30	0.26130508	07/11/2014 11:30	.	
07/11/2014 11:45	0.25732919	07/11/2014 11:45	.	
07/11/2014 12:00	0.28210416	07/11/2014 12:00	.	
07/11/2014 12:15	0.28896552	07/11/2014 12:15	.	
07/11/2014 12:30	0.27971393	07/11/2014 12:30	.	
07/11/2014 12:45	0.29333786	07/11/2014 12:45	.	
07/11/2014 13:00	0.30932835	07/11/2014 13:00	.	
07/11/2014 13:15	0.33269734	07/11/2014 13:15	.	
07/11/2014 13:30	0.33538873	07/11/2014 13:30	.	
07/11/2014 13:45	0.33977257	07/11/2014 13:45	.	
07/11/2014 14:00	0.32047842	07/11/2014 14:00	.	
07/11/2014 14:15	0.31539762	07/11/2014 14:15	.	
07/11/2014 14:30	0.29628267	07/11/2014 14:30	.	
07/11/2014 14:45	0.317951	07/11/2014 14:45	.	
07/11/2014 15:00	0.29798187	07/11/2014 15:00	.	
07/11/2014 15:15	0.34216112	07/11/2014 15:15	.	
07/11/2014 15:30	0.31412458	07/11/2014 15:30	.	
07/11/2014 15:45	0.32725282	07/11/2014 15:45	.	
07/11/2014 16:00	0.29266503	07/11/2014 16:00	.	
07/11/2014 16:15	0.28692267	07/11/2014 16:15	.	
07/11/2014 16:30	0.29164677	07/11/2014 16:30	.	
07/11/2014 16:45	0.28102031	07/11/2014 16:45	.	
07/11/2014 17:00	0.29540179	07/11/2014 17:00	.	
07/11/2014 17:15	0.29172769	07/11/2014 17:15	.	
07/11/2014 17:30	0.27054569	07/11/2014 17:30	.	
07/11/2014 17:45	0.26078855	07/11/2014 17:45	.	
07/11/2014 18:00	0.23869925	07/11/2014 18:00	.	
07/11/2014 18:15	0.22528023	07/11/2014 18:15	.	
07/11/2014 18:30	0.23946564	07/11/2014 18:30	.	
07/11/2014 18:45	0.2441949	07/11/2014 18:45	.	
07/11/2014 19:00	0.24906062	07/11/2014 19:00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
07/11/2014 19:15	0.23738895	07/11/2014 19:15	.	
07/11/2014 19:30	0.2235098	07/11/2014 19:30	.	
07/11/2014 19:45	0.25617152	07/11/2014 19:45	.	
07/11/2014 20:00	0.22708474	07/11/2014 20:00	.	
07/11/2014 20:15	0.19513924	07/11/2014 20:15	.	
07/11/2014 20:30	0.19635424	07/11/2014 20:30	.	
07/11/2014 20:45	0.21191169	07/11/2014 20:45	.	
07/11/2014 21:00	0.19291455	07/11/2014 21:00	.	
07/11/2014 21:15	0.17841308	07/11/2014 21:15	.	
07/11/2014 21:30	0.17517603	07/11/2014 21:30	.	
07/11/2014 21:45	0.1533686	07/11/2014 21:45	.	
07/11/2014 22:00	0.16841381	07/11/2014 22:00	.	
07/11/2014 22:15	0.1535571	07/11/2014 22:15	.	
07/11/2014 22:30	0.15746505	07/11/2014 22:30	.	
07/11/2014 22:45	0.16442975	07/11/2014 22:45	.	
07/11/2014 23:00	0.15518394	07/11/2014 23:00	.	
07/11/2014 23:15	0.16420573	07/11/2014 23:15	.	
07/11/2014 23:30	0.18036752	07/11/2014 23:30	.	
07/11/2014 23:45	0.15722562	07/11/2014 23:45	.	
08/11/2014 00:00	0.13947346	08/11/2014 00:00	.	
08/11/2014 00:15	0.14150139	08/11/2014 00:15	.	
08/11/2014 00:30	0.1375124	08/11/2014 00:30	.	
08/11/2014 00:45	0.12248778	08/11/2014 00:45	.	
08/11/2014 01:00	0.11792307	08/11/2014 01:00	.	
08/11/2014 01:15	0.11675663	08/11/2014 01:15	.	
08/11/2014 01:30	0.11464452	08/11/2014 01:30	.	
08/11/2014 01:45	0.12196868	08/11/2014 01:45	.	
08/11/2014 02:00	0.11613038	08/11/2014 02:00	.	
08/11/2014 02:15	0.12022734	08/11/2014 02:15	.	
08/11/2014 02:30	0.1004608	08/11/2014 02:30	.	
08/11/2014 02:45	0.10458495	08/11/2014 02:45	.	
08/11/2014 03:00	0.11265227	08/11/2014 03:00	.	
08/11/2014 03:15	0.09958426	08/11/2014 03:15	.	
08/11/2014 03:30	0.10328324	08/11/2014 03:30	.	
08/11/2014 03:45	0.11601473	08/11/2014 03:45	.	
08/11/2014 04:00	0.10332145	08/11/2014 04:00	.	
08/11/2014 04:15	0.10355879	08/11/2014 04:15	.	
08/11/2014 04:30	0.1014073	08/11/2014 04:30	.	
08/11/2014 04:45	0.13043458	08/11/2014 04:45	.	
08/11/2014 05:00	0.10411536	08/11/2014 05:00	.	
08/11/2014 05:15	0.09054628	08/11/2014 05:15	.	
08/11/2014 05:30	0.10661684	08/11/2014 05:30	.	
08/11/2014 05:45	0.09774761	08/11/2014 05:45	.	
08/11/2014 06:00	0.09200194	08/11/2014 06:00	.	
08/11/2014 06:15	0.10082599	08/11/2014 06:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
08/11/2014 06:30	0.09732114	08/11/2014 06:30	.	
08/11/2014 06:45	0.09312124	08/11/2014 06:45	.	
08/11/2014 07:00	0.09105039	08/11/2014 07:00	.	
08/11/2014 07:15	0.09678373	08/11/2014 07:15	.	
08/11/2014 07:30	0.09331758	08/11/2014 07:30	.	
08/11/2014 07:45	0.09542986	08/11/2014 07:45	.	
08/11/2014 08:00	0.08724187	08/11/2014 08:00	.	
08/11/2014 08:15	0.08933612	08/11/2014 08:15	.	
08/11/2014 08:30	0.09275136	08/11/2014 08:30	.	
08/11/2014 08:45	0.09004726	08/11/2014 08:45	.	
08/11/2014 09:00	0.0907441	08/11/2014 09:00	.	
08/11/2014 09:15	0.09544711	08/11/2014 09:15	.	
08/11/2014 09:30	0.10283755	08/11/2014 09:30	.	
08/11/2014 09:45	0.1057203	08/11/2014 09:45	.	
08/11/2014 10:00	0.09675887	08/11/2014 10:00	.	
08/11/2014 10:15	0.10597228	08/11/2014 10:15	.	
08/11/2014 10:30	0.10310796	08/11/2014 10:30	.	
08/11/2014 10:45	0.08774159	08/11/2014 10:45	.	
08/11/2014 11:00	0.09200226	08/11/2014 11:00	.	
08/11/2014 11:15	0.09273713	08/11/2014 11:15	.	
08/11/2014 11:30	0.09813454	08/11/2014 11:30	.	
08/11/2014 11:45	0.0907686	08/11/2014 11:45	.	
08/11/2014 12:00	0.08239514	08/11/2014 12:00	.	
08/11/2014 12:15	0.0768441	08/11/2014 12:15	.	
08/11/2014 12:30	0.07695046	08/11/2014 12:30	.	
08/11/2014 12:45	0.07158303	08/11/2014 12:45	.	
08/11/2014 13:00	0.07578311	08/11/2014 13:00	.	
08/11/2014 13:15	0.07981329	08/11/2014 13:15	.	
08/11/2014 13:30	0.07971576	08/11/2014 13:30	.	
08/11/2014 13:45	0.07058842	08/11/2014 13:45	.	
08/11/2014 14:00	0.07729293	08/11/2014 14:00	.	
08/11/2014 14:15	0.071724	08/11/2014 14:15	.	
08/11/2014 14:30	0.0768934	08/11/2014 14:30	.	
08/11/2014 14:45	0.07058842	08/11/2014 14:45	.	
08/11/2014 15:00	0.07386514	08/11/2014 15:00	.	
08/11/2014 15:15	0.07472796	08/11/2014 15:15	.	
08/11/2014 15:30	0.06347761	08/11/2014 15:30	.	
08/11/2014 15:45	0.06346896	08/11/2014 15:45	.	
08/11/2014 16:00	0.06544966	08/11/2014 16:00	.	
08/11/2014 16:15	0.0568214	08/11/2014 16:15	.	
08/11/2014 16:30	0.06276874	08/11/2014 16:30	.	
08/11/2014 16:45	0.06656925	08/11/2014 16:45	.	
08/11/2014 17:00	0.06551679	08/11/2014 17:00	.	
08/11/2014 17:15	0.06687337	08/11/2014 17:15	.	
08/11/2014 17:30	0.07008598	08/11/2014 17:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
08/11/2014 17:45	0.08345287	08/11/2014 17:45	.	
08/11/2014 18:00	0.06494016	08/11/2014 18:00	.	
08/11/2014 18:15	0.07349731	08/11/2014 18:15	.	
08/11/2014 18:30	0.05932165	08/11/2014 18:30	.	
08/11/2014 18:45	0.06623084	08/11/2014 18:45	.	
08/11/2014 19:00	0.06468626	08/11/2014 19:00	.	
08/11/2014 19:15	0.06121013	08/11/2014 19:15	.	
08/11/2014 19:30	0.06696733	08/11/2014 19:30	.	
08/11/2014 19:45	0.06358274	08/11/2014 19:45	.	
08/11/2014 20:00	0.06068167	08/11/2014 20:00	.	
08/11/2014 20:15	0.06351447	08/11/2014 20:15	.	
08/11/2014 20:30	0.06296513	08/11/2014 20:30	.	
08/11/2014 20:45	0.05812258	08/11/2014 20:45	.	
08/11/2014 21:00	0.05621375	08/11/2014 21:00	.	
08/11/2014 21:15	0.05432895	08/11/2014 21:15	.	
08/11/2014 21:30	0.05796479	08/11/2014 21:30	.	
08/11/2014 21:45	0.06017485	08/11/2014 21:45	.	
08/11/2014 22:00	0.07031401	08/11/2014 22:00	.	
08/11/2014 22:15	0.07485152	08/11/2014 22:15	0.2	
08/11/2014 22:30	0.06370449	08/11/2014 22:30	.	
08/11/2014 22:45	0.06303463	08/11/2014 22:45	.	
08/11/2014 23:00	0.06856123	08/11/2014 23:00	.	
08/11/2014 23:15	0.07234153	08/11/2014 23:15	0.2	
08/11/2014 23:30	0.0683129	08/11/2014 23:30	0.8	
08/11/2014 23:45	0.06793435	08/11/2014 23:45	0.8	
09/11/2014 00:00	0.0891757	09/11/2014 00:00	1	
09/11/2014 00:15	0.08838864	09/11/2014 00:15	1.2	
09/11/2014 00:30	0.14049705	09/11/2014 00:30	0.2	
09/11/2014 00:45	0.15069388	09/11/2014 00:45	0.2	
09/11/2014 01:00	0.1466226	09/11/2014 01:00	1.4	
09/11/2014 01:15	0.13236809	09/11/2014 01:15	.	
09/11/2014 01:30	0.15323833	09/11/2014 01:30	0.4	
09/11/2014 01:45	0.16199582	09/11/2014 01:45	0.6	
09/11/2014 02:00	0.14343051	09/11/2014 02:00	0.2	
09/11/2014 02:15	0.14665644	09/11/2014 02:15	.	
09/11/2014 02:30	0.14392659	09/11/2014 02:30	.	
09/11/2014 02:45	0.14608545	09/11/2014 02:45	.	
09/11/2014 03:00	0.12542793	09/11/2014 03:00	0.6	
09/11/2014 03:15	0.11770836	09/11/2014 03:15	.	
09/11/2014 03:30	0.10860617	09/11/2014 03:30	.	
09/11/2014 03:45	0.12564463	09/11/2014 03:45	.	
09/11/2014 04:00	0.12305569	09/11/2014 04:00	.	
09/11/2014 04:15	0.12065574	09/11/2014 04:15	0.2	
09/11/2014 04:30	0.06363768	09/11/2014 04:30	.	
09/11/2014 04:45	0.12214577	09/11/2014 04:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
09/11/2014 05:00	0.12379226	09/11/2014 05:00	.	
09/11/2014 05:15	0.12139737	09/11/2014 05:15	.	
09/11/2014 05:30	0.16623255	09/11/2014 05:30	.	
09/11/2014 05:45	0.17988615	09/11/2014 05:45	.	
09/11/2014 06:00	0.17126155	09/11/2014 06:00	.	
09/11/2014 06:15	0.17750677	09/11/2014 06:15	.	
09/11/2014 06:30	0.20880862	09/11/2014 06:30	.	
09/11/2014 06:45	0.20668057	09/11/2014 06:45	.	
09/11/2014 07:00	0.20426873	09/11/2014 07:00	0.2	
09/11/2014 07:15	0.22907454	09/11/2014 07:15	.	
09/11/2014 07:30	0.23978656	09/11/2014 07:30	0.4	
09/11/2014 07:45	0.21934592	09/11/2014 07:45	0.4	
09/11/2014 08:00	0.23131204	09/11/2014 08:00	0.8	
09/11/2014 08:15	0.25802089	09/11/2014 08:15	0.2	
09/11/2014 08:30	0.29586086	09/11/2014 08:30	0.8	
09/11/2014 08:45	0.28188357	09/11/2014 08:45	1.6	
09/11/2014 09:00	0.29989598	09/11/2014 09:00	0.6	
09/11/2014 09:15	0.41282328	09/11/2014 09:15	0.4	
09/11/2014 09:30	0.39757961	09/11/2014 09:30	.	
09/11/2014 09:45	0.4560799	09/11/2014 09:45	.	
09/11/2014 10:00	0.43540821	09/11/2014 10:00	0.2	
09/11/2014 10:15	0.39396541	09/11/2014 10:15	0.2	
09/11/2014 10:30	0.37359661	09/11/2014 10:30	.	
09/11/2014 10:45	0.41181537	09/11/2014 10:45	.	
09/11/2014 11:00	0.41876548	09/11/2014 11:00	.	
09/11/2014 11:15	0.39004349	09/11/2014 11:15	.	
09/11/2014 11:30	0.40786403	09/11/2014 11:30	.	
09/11/2014 11:45	0.37069982	09/11/2014 11:45	.	
09/11/2014 12:00	0.37769164	09/11/2014 12:00	.	
09/11/2014 12:15	0.37461184	09/11/2014 12:15	.	
09/11/2014 12:30	0.38918054	09/11/2014 12:30	.	
09/11/2014 12:45	0.36764135	09/11/2014 12:45	.	
09/11/2014 13:00	0.4057462	09/11/2014 13:00	.	
09/11/2014 13:15	0.41820667	09/11/2014 13:15	.	
09/11/2014 13:30	0.43540821	09/11/2014 13:30	.	
09/11/2014 13:45	0.45231409	09/11/2014 13:45	.	
09/11/2014 14:00	0.44671615	09/11/2014 14:00	.	
09/11/2014 14:15	0.46709208	09/11/2014 14:15	.	
09/11/2014 14:30	0.44230726	09/11/2014 14:30	.	
09/11/2014 14:45	0.42391677	09/11/2014 14:45	.	
09/11/2014 15:00	0.43831499	09/11/2014 15:00	.	
09/11/2014 15:15	0.397858	09/11/2014 15:15	.	
09/11/2014 15:30	0.40456424	09/11/2014 15:30	.	
09/11/2014 15:45	0.37581218	09/11/2014 15:45	.	
09/11/2014 16:00	0.41618657	09/11/2014 16:00	.	

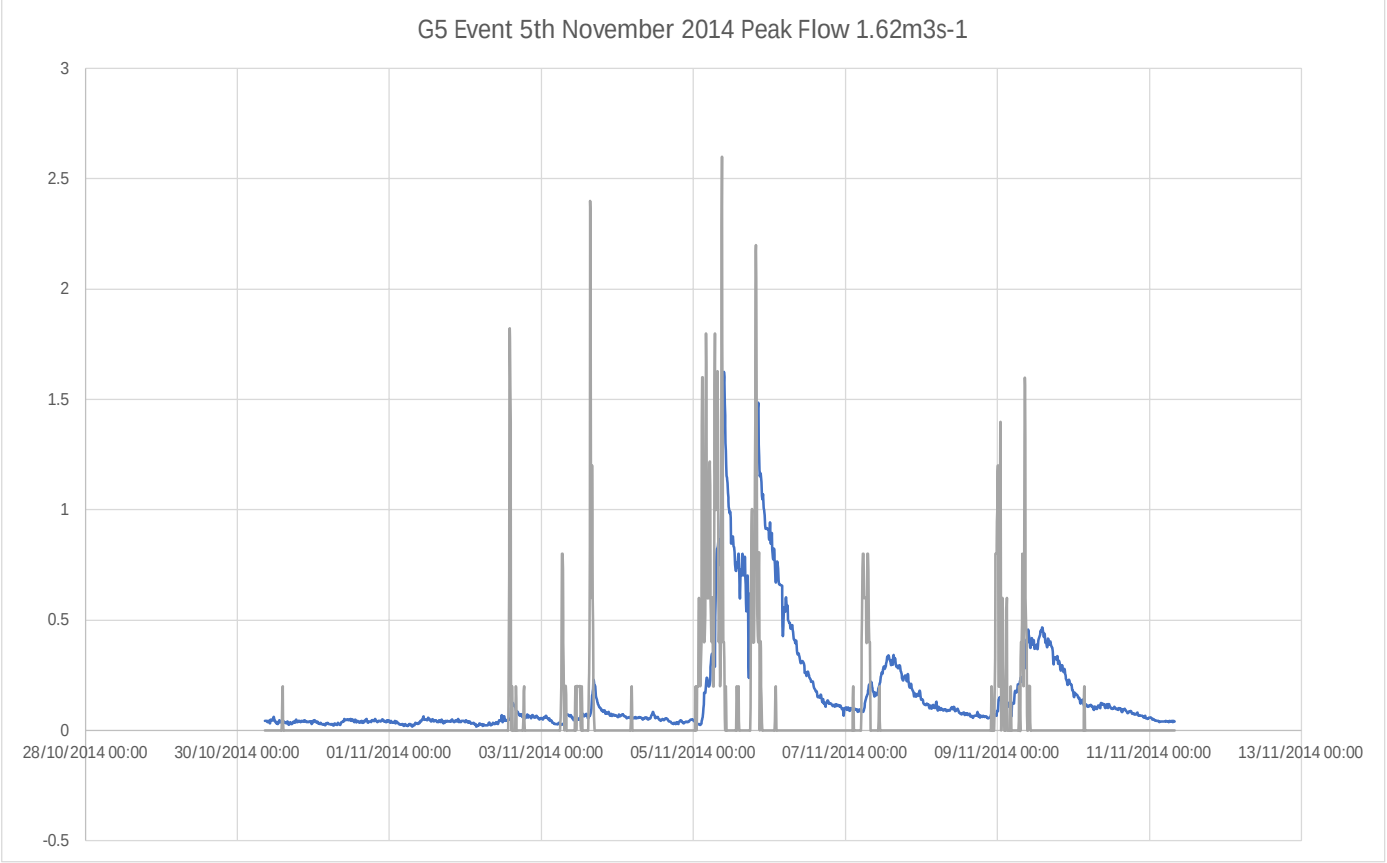
G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
09/11/2014 16:15	0.40774878	09/11/2014 16:15	.	
09/11/2014 16:30	0.38862701	09/11/2014 16:30	.	
09/11/2014 16:45	0.40443728	09/11/2014 16:45	.	
09/11/2014 17:00	0.38701649	09/11/2014 17:00	.	
09/11/2014 17:15	0.37802337	09/11/2014 17:15	.	
09/11/2014 17:30	0.37241413	09/11/2014 17:30	.	
09/11/2014 17:45	0.30083028	09/11/2014 17:45	.	
09/11/2014 18:00	0.3203849	09/11/2014 18:00	.	
09/11/2014 18:15	0.33204213	09/11/2014 18:15	.	
09/11/2014 18:30	0.32993017	09/11/2014 18:30	.	
09/11/2014 18:45	0.32333413	09/11/2014 18:45	.	
09/11/2014 19:00	0.33526094	09/11/2014 19:00	.	
09/11/2014 19:15	0.30286107	09/11/2014 19:15	.	
09/11/2014 19:30	0.3162188	09/11/2014 19:30	.	
09/11/2014 19:45	0.31022844	09/11/2014 19:45	.	
09/11/2014 20:00	0.27147746	09/11/2014 20:00	.	
09/11/2014 20:15	0.27733431	09/11/2014 20:15	.	
09/11/2014 20:30	0.29488297	09/11/2014 20:30	.	
09/11/2014 20:45	0.27521453	09/11/2014 20:45	.	
09/11/2014 21:00	0.26479398	09/11/2014 21:00	.	
09/11/2014 21:15	0.27965013	09/11/2014 21:15	.	
09/11/2014 21:30	0.25619758	09/11/2014 21:30	.	
09/11/2014 21:45	0.2348704	09/11/2014 21:45	.	
09/11/2014 22:00	0.22115767	09/11/2014 22:00	.	
09/11/2014 22:15	0.2060683	09/11/2014 22:15	.	
09/11/2014 22:30	0.22286006	09/11/2014 22:30	.	
09/11/2014 22:45	0.22890987	09/11/2014 22:45	.	
09/11/2014 23:00	0.21095185	09/11/2014 23:00	.	
09/11/2014 23:15	0.2075617	09/11/2014 23:15	.	
09/11/2014 23:30	0.20541139	09/11/2014 23:30	.	
09/11/2014 23:45	0.18320551	09/11/2014 23:45	.	
10/11/2014 00:00	0.18013432	10/11/2014 00:00	.	
10/11/2014 00:15	0.14974394	10/11/2014 00:15	.	
10/11/2014 00:30	0.16988135	10/11/2014 00:30	.	
10/11/2014 00:45	0.16659279	10/11/2014 00:45	.	
10/11/2014 01:00	0.16219757	10/11/2014 01:00	.	
10/11/2014 01:15	0.16091679	10/11/2014 01:15	.	
10/11/2014 01:30	0.15205882	10/11/2014 01:30	.	
10/11/2014 01:45	0.14554883	10/11/2014 01:45	.	
10/11/2014 02:00	0.14645692	10/11/2014 02:00	.	
10/11/2014 02:15	0.12250463	10/11/2014 02:15	.	
10/11/2014 02:30	0.13270576	10/11/2014 02:30	.	
10/11/2014 02:45	0.13139442	10/11/2014 02:45	.	
10/11/2014 03:00	0.13885356	10/11/2014 03:00	.	
10/11/2014 03:15	0.11502541	10/11/2014 03:15	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
10/11/2014 03:30	0.11104623	10/11/2014 03:30	0.2	
10/11/2014 03:45	0.11301201	10/11/2014 03:45	.	
10/11/2014 04:00	0.11994176	10/11/2014 04:00	.	
10/11/2014 04:15	0.11230035	10/11/2014 04:15	.	
10/11/2014 04:30	0.1082106	10/11/2014 04:30	.	
10/11/2014 04:45	0.10685889	10/11/2014 04:45	.	
10/11/2014 05:00	0.11274525	10/11/2014 05:00	.	
10/11/2014 05:15	0.11046533	10/11/2014 05:15	.	
10/11/2014 05:30	0.1159458	10/11/2014 05:30	.	
10/11/2014 05:45	0.10938829	10/11/2014 05:45	.	
10/11/2014 06:00	0.11135977	10/11/2014 06:00	.	
10/11/2014 06:15	0.10479254	10/11/2014 06:15	.	
10/11/2014 06:30	0.09371338	10/11/2014 06:30	.	
10/11/2014 06:45	0.10794305	10/11/2014 06:45	.	
10/11/2014 07:00	0.10573734	10/11/2014 07:00	.	
10/11/2014 07:15	0.09878023	10/11/2014 07:15	.	
10/11/2014 07:30	0.09733163	10/11/2014 07:30	.	
10/11/2014 07:45	0.11085842	10/11/2014 07:45	.	
10/11/2014 08:00	0.1131159	10/11/2014 08:00	.	
10/11/2014 08:15	0.10957144	10/11/2014 08:15	.	
10/11/2014 08:30	0.10112157	10/11/2014 08:30	.	
10/11/2014 08:45	0.12413079	10/11/2014 08:45	.	
10/11/2014 09:00	0.11502704	10/11/2014 09:00	.	
10/11/2014 09:15	0.12152456	10/11/2014 09:15	.	
10/11/2014 09:30	0.11948969	10/11/2014 09:30	.	
10/11/2014 09:45	0.11778033	10/11/2014 09:45	.	
10/11/2014 10:00	0.10311934	10/11/2014 10:00	.	
10/11/2014 10:15	0.10224368	10/11/2014 10:15	.	
10/11/2014 10:30	0.11633976	10/11/2014 10:30	.	
10/11/2014 10:45	0.11797801	10/11/2014 10:45	.	
10/11/2014 11:00	0.10044325	10/11/2014 11:00	.	
10/11/2014 11:15	0.11941127	10/11/2014 11:15	.	
10/11/2014 11:30	0.1118828	10/11/2014 11:30	.	
10/11/2014 11:45	0.10523802	10/11/2014 11:45	.	
10/11/2014 12:00	0.09872355	10/11/2014 12:00	.	
10/11/2014 12:15	0.09736609	10/11/2014 12:15	.	
10/11/2014 12:30	0.09743765	10/11/2014 12:30	.	
10/11/2014 12:45	0.10028614	10/11/2014 12:45	.	
10/11/2014 13:00	0.1079	10/11/2014 13:00	.	
10/11/2014 13:15	0.10026523	10/11/2014 13:15	.	
10/11/2014 13:30	0.09817873	10/11/2014 13:30	.	
10/11/2014 13:45	0.09613148	10/11/2014 13:45	.	
10/11/2014 14:00	0.09746268	10/11/2014 14:00	.	
10/11/2014 14:15	0.09208782	10/11/2014 14:15	.	
10/11/2014 14:30	0.10077453	10/11/2014 14:30	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
10/11/2014 14:45	0.09868421	10/11/2014 14:45	.	
10/11/2014 15:00	0.09792301	10/11/2014 15:00	.	
10/11/2014 15:15	0.08686831	10/11/2014 15:15	.	
10/11/2014 15:30	0.08367287	10/11/2014 15:30	.	
10/11/2014 15:45	0.09708909	10/11/2014 15:45	.	
10/11/2014 16:00	0.09133928	10/11/2014 16:00	.	
10/11/2014 16:15	0.09715563	10/11/2014 16:15	.	
10/11/2014 16:30	0.09265492	10/11/2014 16:30	.	
10/11/2014 16:45	0.08876474	10/11/2014 16:45	.	
10/11/2014 17:00	0.0811714	10/11/2014 17:00	.	
10/11/2014 17:15	0.07871192	10/11/2014 17:15	.	
10/11/2014 17:30	0.08120233	10/11/2014 17:30	.	
10/11/2014 17:45	0.08551215	10/11/2014 17:45	.	
10/11/2014 18:00	0.08735574	10/11/2014 18:00	.	
10/11/2014 18:15	0.08797027	10/11/2014 18:15	.	
10/11/2014 18:30	0.07876396	10/11/2014 18:30	.	
10/11/2014 18:45	0.07517405	10/11/2014 18:45	.	
10/11/2014 19:00	0.07807721	10/11/2014 19:00	.	
10/11/2014 19:15	0.07342275	10/11/2014 19:15	.	
10/11/2014 19:30	0.07673379	10/11/2014 19:30	.	
10/11/2014 19:45	0.07168326	10/11/2014 19:45	.	
10/11/2014 20:00	0.07276237	10/11/2014 20:00	.	
10/11/2014 20:15	0.08029511	10/11/2014 20:15	.	
10/11/2014 20:30	0.0694216	10/11/2014 20:30	.	
10/11/2014 20:45	0.06615836	10/11/2014 20:45	.	
10/11/2014 21:00	0.0699039	10/11/2014 21:00	.	
10/11/2014 21:15	0.06614001	10/11/2014 21:15	.	
10/11/2014 21:30	0.06557594	10/11/2014 21:30	.	
10/11/2014 21:45	0.06607294	10/11/2014 21:45	.	
10/11/2014 22:00	0.06497571	10/11/2014 22:00	.	
10/11/2014 22:15	0.05781892	10/11/2014 22:15	.	
10/11/2014 22:30	0.06330803	10/11/2014 22:30	.	
10/11/2014 22:45	0.06524167	10/11/2014 22:45	.	
10/11/2014 23:00	0.05634124	10/11/2014 23:00	.	
10/11/2014 23:15	0.05487952	10/11/2014 23:15	.	
10/11/2014 23:30	0.05343777	10/11/2014 23:30	.	
10/11/2014 23:45	0.05627525	10/11/2014 23:45	.	
11/11/2014 00:00	0.05671588	11/11/2014 00:00	.	
11/11/2014 00:15	0.05807485	11/11/2014 00:15	.	
11/11/2014 00:30	0.05933896	11/11/2014 00:30	.	
11/11/2014 00:45	0.05603195	11/11/2014 00:45	.	
11/11/2014 01:00	0.05012249	11/11/2014 01:00	.	
11/11/2014 01:15	0.05228014	11/11/2014 01:15	.	
11/11/2014 01:30	0.04917173	11/11/2014 01:30	.	
11/11/2014 01:45	0.04529723	11/11/2014 01:45	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
11/11/2014 02:00	0.0456859	11/11/2014 02:00	.	
11/11/2014 02:15	0.04236277	11/11/2014 02:15	.	
11/11/2014 02:30	0.04395387	11/11/2014 02:30	.	
11/11/2014 02:45	0.0442864	11/11/2014 02:45	.	
11/11/2014 03:00	0.04150274	11/11/2014 03:00	.	
11/11/2014 03:15	0.03837337	11/11/2014 03:15	.	
11/11/2014 03:30	0.04062912	11/11/2014 03:30	.	
11/11/2014 03:45	0.03984532	11/11/2014 03:45	.	
11/11/2014 04:00	0.03977751	11/11/2014 04:00	.	
11/11/2014 04:15	0.04156223	11/11/2014 04:15	.	
11/11/2014 04:30	0.03969205	11/11/2014 04:30	.	
11/11/2014 04:45	0.04143528	11/11/2014 04:45	.	
11/11/2014 05:00	0.04101017	11/11/2014 05:00	.	
11/11/2014 05:15	0.04410729	11/11/2014 05:15	.	
11/11/2014 05:30	0.0408643	11/11/2014 05:30	.	
11/11/2014 05:45	0.04156182	11/11/2014 05:45	.	
11/11/2014 06:00	0.03940295	11/11/2014 06:00	.	
11/11/2014 06:15	0.03802079	11/11/2014 06:15	.	
11/11/2014 06:30	0.04207112	11/11/2014 06:30	.	
11/11/2014 06:45	0.04035947	11/11/2014 06:45	.	
11/11/2014 07:00	0.04035947	11/11/2014 07:00	.	
11/11/2014 07:15	0.04480976	11/11/2014 07:15	.	
11/11/2014 07:30	0.03830548	11/11/2014 07:30	.	
11/11/2014 07:45	0.04251281	11/11/2014 07:45	.	
11/11/2014 08:00	0.04023534	11/11/2014 08:00	.	

G5 flow		Thorpeness TBR RG		
Date & Time	Flow m^3s^{-1}	Date & Time	Rainfall (mm)	Daily Rainfall (mm)



SAAR	592	mm
AREA	5.04	Km2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capacity in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
04-Nov-14	56.2	mm
11-Nov-14	44.0	mm

Source of Rainfall event data.

Gauge	**Easting**	**Northing**	**Distance from Catchment Centroid (m)**	**Reciprocal**	**Weighting**
Benhall	38166	60602	20912.0		0.00000
Soham	23243	62717	6550.0		0.00000
Thorpeness	60012	78834	3636.0	0.00028	1.00000
			Total	0.00028	1.00000

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**30/10/2014**	**31/10/2014**	**01/11/2014**	**02/11/2014**	**03/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0.2	0	0	6.8	7.2
Average Daily rainfall totals			0.2	0	0	6.8	7.2

Gauge	**SAAR**	**Weight**	**30/10/2014**	**31/10/2014**	**01/11/2014**	**02/11/2014**	**03/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0.000337838	0	0	0.011486486	0.012162162

Gauge	**SAAR**	**Weight**	**30/10/2014**	**31/10/2014**	**01/11/2014**	**02/11/2014**	**03/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.0000	0.000337838	0	0	0.011486486	0.012162162

Gauge	**SAAR**	**Weight**	**30/10/2014**	**31/10/2014**	**01/11/2014**	**02/11/2014**	**03/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0.2	0	0	6.8	7.2
Catchment Average Antecedent RF mm			0.2	0	0	6.8	7.2

Date	**Catchment Average Antecedent Rainfall (mm)**	
30/10/2014	0.20	d-5
31/10/2014	0.00	d-4
01/11/2014	0.00	d-3
02/11/2014	6.80	d-2
03/11/2014	7.20	d-1

API5

7.50	mm	7.504170715	mm / day

CWI Prior to Event November 2014 Event at G5
CWI 125 + API15 - SMD

SMD	56.2	mm
CWI	76.30417072	mm

TBR RG

Daily RF totals 9am 9am	**Benhall**	**Soham**	**Thorpeness**
Date	**Total RF (mm)**	**Total RF (mm)**	**Total RF (mm)**
03/11/2014		0	7.2
02/11/2014		0	6.8
01/11/2014		0	0
31/10/2014		0	0
30/10/2014		0	0.2
Total API5 RF			14.2

Rainall Event Depth P (mm)	28.8
Event duration (hours)	9.5

FEH Parameter							URBEXT2000		
SPR	52.09816633	%					PR	40	taken from PR calculations sheet using Thorpeness TBR RG record
PRrural	39.92	%		P=Storm Depth	28.8	mm	DPRrain	0	DPRrain is 0, as P<40mm
DPRrain	0	%		SPR	52.09816633		DPRcwi	-12.17395732	
DPRcwi	-12.17395732	CWI	76.3042				SPR	52.09816633	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural							DPRrain	0.45(P-40)^0.7	#NUM!
PR	40.07958054	%					P	28.8	
PRrural	39.92420901	%					CWI	76.30417072	
CWI	76.30417072	mm					SPR	52.09816633	
BF	0.00001		Baseflow equation taken from FEH				PR	40.07958054	
	-1254								
	1778.5		524.5	0.00525			SPRHOST	24.27	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
AREA	5.04		**0.02643**	m3s-1			Duration (hours)	9.5	
SPR	52.09816633								
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}								
SPR =	52.09816633								
PRrural	39.92420901								

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
05-Nov-14	05-Nov-14	9.50	7.50	56.20	76.30	39.92	-12.17	0.00	52.10	40.00	24.27

Site **Sub-catchment** **SPRg.cds** **SPRg.obs** **SPRs.cds** **SPRs.adj**

Site	Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Sizewell	Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	Leis Abbey	24.3	44.8	27.8	51.4
Leiston	Leiston	24.3	44.8	20.7	38.2
Leis Upper	Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	Mins Potters	24.3	44.8	25.3	46.8
				Mean	37.3

G5 Flow		Middleton Flow			Thorpeness TBR RG		
					Date & Time	Rainfall (mm)	Daily Rainfall (mm)
15/11/2014 09:00	0.031944497	15/11/2014	09 00:00	0.283	15/11/2014 09:00	.	
15/11/2014 09:15	0.032231161	15/11/2014	09:15:00	0.283	15/11/2014 09:15	.	
15/11/2014 09:30	0.032316863	15/11/2014	09 30:00	0.283	15/11/2014 09:30	.	
15/11/2014 09:45	0.034821784	15/11/2014	09:45:00	0.283	15/11/2014 09:45	.	
15/11/2014 10:00	0.039685917	15/11/2014	10 00:00	0.283	15/11/2014 10:00	.	
15/11/2014 10:15	0.044753539	15/11/2014	10:15:00	0.283	15/11/2014 10:15	.	
15/11/2014 10:30	0.046659291	15/11/2014	10 30:00	0.283	15/11/2014 10:30	.	
15/11/2014 10:45	0.043755296	15/11/2014	10:45:00	0.283	15/11/2014 10:45	.	
15/11/2014 11:00	0.052353968	15/11/2014	11 00:00	0.283	15/11/2014 11:00	.	
15/11/2014 11:15	0.045671027	15/11/2014	11:15:00	0.283	15/11/2014 11:15	.	
15/11/2014 11:30	0.052449745	15/11/2014	11 30:00	0.283	15/11/2014 11:30	.	
15/11/2014 11:45	0.04921951	15/11/2014	11:45:00	0.283	15/11/2014 11:45	.	
15/11/2014 12:00	0.047344673	15/11/2014	12 00:00	0.283	15/11/2014 12:00	.	
15/11/2014 12:15	0.051094347	15/11/2014	12:15:00	0.283	15/11/2014 12:15	.	
15/11/2014 12:30	0.042043544	15/11/2014	12 30:00	0.283	15/11/2014 12:30	.	
15/11/2014 12:45	0.045302682	15/11/2014	12:45:00	0.283	15/11/2014 12:45	.	
15/11/2014 13:00	0.048617783	15/11/2014	13 00:00	0.283	15/11/2014 13:00	.	
15/11/2014 13:15	0.037567448	15/11/2014	13:15:00	0.283	15/11/2014 13:15	.	
15/11/2014 13:30	0.036816566	15/11/2014	13 30:00	0.283	15/11/2014 13:30	.	
15/11/2014 13:45	0.042224433	15/11/2014	13:45:00	0.283	15/11/2014 13:45	.	
15/11/2014 14:00	0.041076779	15/11/2014	14 00:00	0.283	15/11/2014 14:00	.	
15/11/2014 14:15	0.041862664	15/11/2014	14:15:00	0.283	15/11/2014 14:15	.	
15/11/2014 14:30	0.041793778	15/11/2014	14 30:00	0.283	15/11/2014 14:30	.	
15/11/2014 14:45	0.049680762	15/11/2014	14:45:00	0.283	15/11/2014 14:45	.	
15/11/2014 15:00	0.042786376	15/11/2014	15 00:00	0.283	15/11/2014 15:00	.	
15/11/2014 15:15	0.043852101	15/11/2014	15:15:00	0.283	15/11/2014 15:15	.	
15/11/2014 15:30	0.050795208	15/11/2014	15 30:00	0.283	15/11/2014 15:30	.	
15/11/2014 15:45	0.049583345	15/11/2014	15:45:00	0.283	15/11/2014 15:45	.	
15/11/2014 16:00	0.04458605	15/11/2014	16 00:00	0.283	15/11/2014 16:00	.	
15/11/2014 16:15	0.04354943	15/11/2014	16:15:00	0.283	15/11/2014 16:15	.	
15/11/2014 16:30	0.045277131	15/11/2014	16 30:00	0.283	15/11/2014 16:30	.	
15/11/2014 16:45	0.039332474	15/11/2014	16:45:00	0.283	15/11/2014 16:45		0.2
15/11/2014 17:00	0.042649193	15/11/2014	17 00:00	0.283	15/11/2014 17:00	.	
15/11/2014 17:15	0.038305483	15/11/2014	17:15:00	0.283	15/11/2014 17:15	.	
15/11/2014 17:30	0.04344044	15/11/2014	17 30:00	0.283	15/11/2014 17:30	.	
15/11/2014 17:45	0.051151312	15/11/2014	17:45:00	0.283	15/11/2014 17:45	.	
15/11/2014 18:00	0.043654394	15/11/2014	18 00:00	0.283	15/11/2014 18:00	.	
15/11/2014 18:15	0.0434033	15/11/2014	18:15:00	0.283	15/11/2014 18:15	.	
15/11/2014 18:30	0.041365411	15/11/2014	18 30:00	0.283	15/11/2014 18:30	.	
15/11/2014 18:45	0.044917825	15/11/2014	18:45:00	0.283	15/11/2014 18:45	.	
15/11/2014 19:00	0.044562584	15/11/2014	19 00:00	0.283	15/11/2014 19:00	.	
15/11/2014 19:15	0.039284283	15/11/2014	19:15:00	0.283	15/11/2014 19:15	.	
15/11/2014 19:30	0.040777357	15/11/2014	19 30:00	0.278	15/11/2014 19:30	.	
15/11/2014 19:45	0.048133141	15/11/2014	19:45:00	0.278	15/11/2014 19:45	.	
15/11/2014 20:00	0.046407716	15/11/2014	20 00:00	0.278	15/11/2014 20:00		0.2
15/11/2014 20:15	0.044934338	15/11/2014	20:15:00	0.278	15/11/2014 20:15		0.6
15/11/2014 20:30	0.049848195	15/11/2014	20 30:00	0.278	15/11/2014 20:30		0.4
15/11/2014 20:45	0.046672938	15/11/2014	20:45:00	0.278	15/11/2014 20:45	.	
15/11/2014 21:00	0.043387481	15/11/2014	21 00:00	0.278	15/11/2014 21:00	.	
15/11/2014 21:15	0.050693068	15/11/2014	21:15:00	0.278	15/11/2014 21:15	.	
15/11/2014 21:30	0.06896448	15/11/2014	21 30:00	0.278	15/11/2014 21:30	.	
15/11/2014 21:45	0.064638461	15/11/2014	21:45:00	0.278	15/11/2014 21:45	.	

	DATE TIME
start of event	23/11/2014 05 00
end of event	23/11/2014 20:45
duration hours	15.75
total RF mm	21
SMD W/E AVERAGE	**mm**

		Thorpeness TBR RG
DATE	**API5**	**Daily Totals**
21/11/2014	d-1	1.4
20/11/2014	d-2	0
19/11/2014	d-3	0.2
18/11/2014	d-4	0
17/11/2014	d-5	6
		7.6

	G5 Flow			Middleton Flow		Thorpeness TBR RG		
					Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
15/11/2014 22:00	0.056809029	15/11/2014	22 00:00	0.278	15/11/2014 22:00	.		
15/11/2014 22:15	0.058699142	15/11/2014	22:15:00	0.278	15/11/2014 22:15	.		
15/11/2014 22:30	0.050538487	15/11/2014	22 30:00	0.278	15/11/2014 22:30	.		
15/11/2014 22:45	0.042330804	15/11/2014	22:45:00	0.278	15/11/2014 22:45	.		
15/11/2014 23:00	0.044587144	15/11/2014	23 00:00	0.278	15/11/2014 23:00	.		
15/11/2014 23:15	0.042948305	15/11/2014	23:15:00	0.273	15/11/2014 23:15	.		
15/11/2014 23:30	0.048733245	15/11/2014	23 30:00	0.273	15/11/2014 23:30	.		
15/11/2014 23:45	0.04677606	15/11/2014	23:45:00	0.273	15/11/2014 23:45	.		
16/11/2014 00:00	0.041562226	16/11/2014	00 00:00	0.273	16/11/2014 00:00	.		
16/11/2014 00:15	0.04071828	16/11/2014	00:15:00	0.273	16/11/2014 00:15	.		
16/11/2014 00:30	0.041365411	16/11/2014	00 30:00	0.273	16/11/2014 00:30	.		
16/11/2014 00:45	0.040864299	16/11/2014	00:45:00	0.273	16/11/2014 00:45	.		
16/11/2014 01:00	0.039402949	16/11/2014	01 00:00	0.273	16/11/2014 01:00	.		
16/11/2014 01:15	0.040094029	16/11/2014	01:15:00	0.273	16/11/2014 01:15	.		
16/11/2014 01:30	0.046040523	16/11/2014	01 30:00	0.273	16/11/2014 01:30	.		
16/11/2014 01:45	0.042755779	16/11/2014	01:45:00	0.273	16/11/2014 01:45	.		
16/11/2014 02:00	0.039596996	16/11/2014	02 00:00	0.268	16/11/2014 02:00	.		
16/11/2014 02:15	0.040858888	16/11/2014	02:15:00	0.268	16/11/2014 02:15	.		
16/11/2014 02:30	0.038430821	16/11/2014	02 30:00	0.268	16/11/2014 02:30	.		
16/11/2014 02:45	0.039998402	16/11/2014	02:45:00	0.268	16/11/2014 02:45	.		
16/11/2014 03:00	0.034297387	16/11/2014	03 00:00	0.268	16/11/2014 03:00	.		
16/11/2014 03:15	0.037124278	16/11/2014	03:15:00	0.268	16/11/2014 03:15	.		
16/11/2014 03:30	0.03631834	16/11/2014	03 30:00	0.268	16/11/2014 03:30	.		
16/11/2014 03:45	0.035296983	16/11/2014	03:45:00	0.268	16/11/2014 03:45	.		
16/11/2014 04:00	0.033982371	16/11/2014	04 00:00	0.268	16/11/2014 04:00	.		
16/11/2014 04:15	0.034821784	16/11/2014	04:15:00	0.268	16/11/2014 04:15	.		
16/11/2014 04:30	0.038957958	16/11/2014	04 30:00	0.268	16/11/2014 04:30	.		
16/11/2014 04:45	0.03075921	16/11/2014	04:45:00	0.268	16/11/2014 04:45	.		
16/11/2014 05:00	0.033363962	16/11/2014	05 00:00	0.268	16/11/2014 05:00	.		
16/11/2014 05:15	0.035032659	16/11/2014	05:15:00	0.264	16/11/2014 05:15	.		
16/11/2014 05:30	0.034054766	16/11/2014	05 30:00	0.264	16/11/2014 05:30	.		
16/11/2014 05:45	0.032316863	16/11/2014	05:45:00	0.264	16/11/2014 05:45	.		
16/11/2014 06:00	0.031084504	16/11/2014	06 00:00	0.264	16/11/2014 06:00	0.2		
16/11/2014 06:15	0.030511175	16/11/2014	06:15:00	0.264	16/11/2014 06:15	.		
16/11/2014 06:30	0.030155909	16/11/2014	06 30:00	0.264	16/11/2014 06:30	.		
16/11/2014 06:45	0.0304396	16/11/2014	06:45:00	0.264	16/11/2014 06:45	.		
16/11/2014 07:00	0.026995508	16/11/2014	07 00:00	0.259	16/11/2014 07:00	.		
16/11/2014 07:15	0.035136682	16/11/2014	07:15:00	0.259	16/11/2014 07:15	.		
16/11/2014 07:30	0.037382523	16/11/2014	07 30:00	0.259	16/11/2014 07:30	.		
16/11/2014 07:45	0.035698142	16/11/2014	07:45:00	0.259	16/11/2014 07:45	.		
16/11/2014 08:00	0.032992817	16/11/2014	08 00:00	0.259	16/11/2014 08:00	.		
16/11/2014 08:15	0.034524475	16/11/2014	08:15:00	0.259	16/11/2014 08:15	.		
16/11/2014 08:30	0.035213368	16/11/2014	08 30:00	0.259	16/11/2014 08:30	.		
16/11/2014 08:45	0.037959152	16/11/2014	08:45:00	0.259	16/11/2014 08:45	.		
16/11/2014 09:00	0.030111693	16/11/2014	09 00:00	0.259	16/11/2014 09:00	.		1.6
16/11/2014 09:15	0.039122391	16/11/2014	09:15:00	0.254	16/11/2014 09:15	.		
16/11/2014 09:30	0.029863155	16/11/2014	09 30:00	0.254	16/11/2014 09:30	.		
16/11/2014 09:45	0.036732911	16/11/2014	09:45:00	0.254	16/11/2014 09:45	.		
16/11/2014 10:00	0.035940741	16/11/2014	10 00:00	0.254	16/11/2014 10:00	.		
16/11/2014 10:15	0.03945828	16/11/2014	10:15:00	0.254	16/11/2014 10:15	0.2		
16/11/2014 10:30	0.047249904	16/11/2014	10 30:00	0.254	16/11/2014 10:30	.		
16/11/2014 10:45	0.046179084	16/11/2014	10:45:00	0.254	16/11/2014 10:45	.		

G5 Flow		Middleton Flow			Thorpeness TBR RG		
					Date & Time	Rainfall (mm)	Daily Rainfall (mm)
16/11/2014 11:00	0.048114998	16/11/2014	11 00:00	0.254	16/11/2014 11:00	0.2	
16/11/2014 11:15	0.049958396	16/11/2014	11:15:00	0.254	16/11/2014 11:15	0.4	
16/11/2014 11:30	0.050219845	16/11/2014	11 30:00	0.254	16/11/2014 11:30	0.4	
16/11/2014 11:45	0.05653509	16/11/2014	11:45:00	0.254	16/11/2014 11:45	0.2	
16/11/2014 12:00	0.061886897	16/11/2014	12 00:00	0.254	16/11/2014 12:00	0.4	
16/11/2014 12:15	0.073894216	16/11/2014	12:15:00	0.254	16/11/2014 12:15	0.4	
16/11/2014 12:30	0.083620979	16/11/2014	12 30:00	0.254	16/11/2014 12:30	0.2	
16/11/2014 12:45	0.06919835	16/11/2014	12:45:00	0.259	16/11/2014 12:45	0.2	
16/11/2014 13:00	0.070284191	16/11/2014	13 00:00	0.264	16/11/2014 13:00	.	
16/11/2014 13:15	0.073890101	16/11/2014	13:15:00	0.273	16/11/2014 13:15	0.2	
16/11/2014 13:30	0.07288606	16/11/2014	13 30:00	0.288	16/11/2014 13:30	0.4	
16/11/2014 13:45	0.070877978	16/11/2014	13:45:00	0.304	16/11/2014 13:45	0.2	
16/11/2014 14:00	0.08849195	16/11/2014	14 00:00	0.325	16/11/2014 14:00	0.4	
16/11/2014 14:15	0.094806333	16/11/2014	14:15:00	0.346	16/11/2014 14:15	0.2	
16/11/2014 14:30	0.112076486	16/11/2014	14 30:00	0.368	16/11/2014 14:30	0.4	
16/11/2014 14:45	0.112393041	16/11/2014	14:45:00	0.391	16/11/2014 14:45	0.2	
16/11/2014 15:00	0.107540551	16/11/2014	15 00:00	0.414	16/11/2014 15:00	0.2	
16/11/2014 15:15	0.107089077	16/11/2014	15:15:00	0.437	16/11/2014 15:15	0.2	
16/11/2014 15:30	0.106462464	16/11/2014	15 30:00	0.455	16/11/2014 15:30	0.2	
16/11/2014 15:45	0.096133744	16/11/2014	15:45:00	0.48	16/11/2014 15:45	0.2	
16/11/2014 16:00	0.101613986	16/11/2014	16 00:00	0.499	16/11/2014 16:00	0.2	
16/11/2014 16:15	0.104436075	16/11/2014	16:15:00	0.524	16/11/2014 16:15	0.4	
16/11/2014 16:30	0.105899622	16/11/2014	16 30:00	0.537	16/11/2014 16:30	0.4	
16/11/2014 16:45	0.113166635	16/11/2014	16:45:00	0.557	16/11/2014 16:45	0.6	
16/11/2014 17:00	0.103032006	16/11/2014	17 00:00	0 57	16/11/2014 17:00	0.2	
16/11/2014 17:15	0.115628435	16/11/2014	17:15:00	0.583	16/11/2014 17:15	0.2	
16/11/2014 17:30	0.111101528	16/11/2014	17 30:00	0.597	16/11/2014 17:30	0.2	
16/11/2014 17:45	0.112624138	16/11/2014	17:45:00	0.604	16/11/2014 17:45	0.2	
16/11/2014 18:00	0.105064479	16/11/2014	18 00:00	0.617	16/11/2014 18:00	.	
16/11/2014 18:15	0.108893906	16/11/2014	18:15:00	0.631	16/11/2014 18:15	0.2	
16/11/2014 18:30	0.098558891	16/11/2014	18 30:00	0.638	16/11/2014 18:30	.	
16/11/2014 18:45	0.107447354	16/11/2014	18:45:00	0.652	16/11/2014 18:45	0.2	
16/11/2014 19:00	0.095929677	16/11/2014	19 00:00	0.666	16/11/2014 19:00	0.2	
16/11/2014 19:15	0.083460509	16/11/2014	19:15:00	0.695	16/11/2014 19:15	.	
16/11/2014 19:30	0.091965933	16/11/2014	19 30:00	0.709	16/11/2014 19:30	.	
16/11/2014 19:45	0.092620582	16/11/2014	19:45:00	0.739	16/11/2014 19:45	.	
16/11/2014 20:00	0.088438586	16/11/2014	20 00:00	0.776	16/11/2014 20:00	0.2	
16/11/2014 20:15	0.093351505	16/11/2014	20:15:00	0.822	16/11/2014 20:15	.	
16/11/2014 20:30	0.085315084	16/11/2014	20 30:00	0.877	16/11/2014 20:30	0.2	
16/11/2014 20:45	0.100821971	16/11/2014	20:45:00	0.933	16/11/2014 20:45	.	
16/11/2014 21:00	0.092090068	16/11/2014	21 00:00	0.999	16/11/2014 21:00	0.2	
16/11/2014 21:15	0.093408897	16/11/2014	21:15:00	1 08	16/11/2014 21:15	0.2	
16/11/2014 21:30	0.10344533	16/11/2014	21 30:00	1.14	16/11/2014 21:30	0.2	
16/11/2014 21:45	0.094737076	16/11/2014	21:45:00	1 23	16/11/2014 21:45	0.2	
16/11/2014 22:00	0.108178395				16/11/2014 22:00	0.2	
16/11/2014 22:15	0.119521945				16/11/2014 22:15	0.2	
16/11/2014 22:30	0.13406215				16/11/2014 22:30	0.2	
16/11/2014 22:45	0.124451568				16/11/2014 22:45	0.2	
16/11/2014 23:00	0.164938931				16/11/2014 23:00	0.4	
16/11/2014 23:15	0.171925211				16/11/2014 23:15	0.2	
16/11/2014 23:30	0.166082371				16/11/2014 23:30	.	
16/11/2014 23:45	0.177756623				16/11/2014 23:45	0.2	

			Thorpeness TBR RG		
	G5 Flow	Middleton Flow	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
17/11/2014 00:00	0.174296846		17/11/2014 00:00	0.2	
17/11/2014 00:15	0.179086312		17/11/2014 00:15	0.2	
17/11/2014 00:30	0.18613206		17/11/2014 00:30	0.2	
17/11/2014 00:45	0.192219236		17/11/2014 00:45	0.2	
17/11/2014 01:00	0.206142524		17/11/2014 01:00	0.2	
17/11/2014 01:15	0.223126854		17/11/2014 01:15	.	
17/11/2014 01:30	0.222594545		17/11/2014 01:30	.	
17/11/2014 01:45	0.250636167		17/11/2014 01:45	.	
17/11/2014 02:00	0.229219002		17/11/2014 02:00	.	
17/11/2014 02:15	0.213769572		17/11/2014 02:15	.	
17/11/2014 02:30	0.248770298		17/11/2014 02:30	.	
17/11/2014 02:45	0.234134029		17/11/2014 02:45	.	
17/11/2014 03:00	0.257206677		17/11/2014 03:00	0.2	
17/11/2014 03:15	0.248846573		17/11/2014 03:15	.	
17/11/2014 03:30	0.252514178		17/11/2014 03:30	.	
17/11/2014 03:45	0.275130204		17/11/2014 03:45	.	
17/11/2014 04:00	0.255858072		17/11/2014 04:00	.	
17/11/2014 04:15	0.217391963		17/11/2014 04:15	.	
17/11/2014 04:30	0.27592952		17/11/2014 04:30	.	
17/11/2014 04:45	0.234309077		17/11/2014 04:45	.	
17/11/2014 05:00	0.24260634		17/11/2014 05:00	.	
17/11/2014 05:15	0.209417289		17/11/2014 05:15	.	
17/11/2014 05:30	0.27592952		17/11/2014 05:30	.	
17/11/2014 05:45	0.237357094		17/11/2014 05:45	.	
17/11/2014 06:00	0.241748156		17/11/2014 06:00	.	
17/11/2014 06:15	0.251772819		17/11/2014 06:15	.	
17/11/2014 06:30	0.223783709		17/11/2014 06:30	.	
17/11/2014 06:45	0.224359049		17/11/2014 06:45	.	
17/11/2014 07:00	0.239324906		17/11/2014 07:00	.	
17/11/2014 07:15	0.216174883		17/11/2014 07:15	.	
17/11/2014 07:30	0.229820775		17/11/2014 07:30	.	
17/11/2014 07:45	0.225258526		17/11/2014 07:45	.	
17/11/2014 08:00	0.229519428		17/11/2014 08:00	.	
17/11/2014 08:15	0.200868914		17/11/2014 08:15	.	
17/11/2014 08:30	0.232976323		17/11/2014 08:30	.	
17/11/2014 08:45	0.199917062		17/11/2014 08:45	.	
17/11/2014 09:00	0.210377338		17/11/2014 09:00	.	12.4
17/11/2014 09:15	0.216904352		17/11/2014 09:15	.	
17/11/2014 09:30	0.232740609		17/11/2014 09:30	.	
17/11/2014 09:45	0.188340071		17/11/2014 09:45	.	
17/11/2014 10:00	0.184286125		17/11/2014 10:00	.	
17/11/2014 10:15	0.198652388		17/11/2014 10:15	0.6	
17/11/2014 10:30	0.187735024		17/11/2014 10:30	0.2	
17/11/2014 10:45	0.173730383		17/11/2014 10:45	.	
17/11/2014 11:00	0.18368609		17/11/2014 11:00	.	
17/11/2014 11:15	0.193548623		17/11/2014 11:15	.	
17/11/2014 11:30	0.179712829		17/11/2014 11:30	.	
17/11/2014 11:45	0.183403304		17/11/2014 11:45	.	
17/11/2014 12:00	0.17736153		17/11/2014 12:00	.	
17/11/2014 12:15	0.157225617		17/11/2014 12:15	.	
17/11/2014 12:30	0.158413793		17/11/2014 12:30	.	
17/11/2014 12:45	0.142534227		17/11/2014 12:45	.	

			Thorpeness TBR RG		
	G5 Flow	Middleton Flow	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
17/11/2014 13:00	0.152643763		17/11/2014 13:00	.	
17/11/2014 13:15	0.147228455		17/11/2014 13:15	.	
17/11/2014 13:30	0.168135144		17/11/2014 13:30	1	
17/11/2014 13:45	0.186891212		17/11/2014 13:45	.	
17/11/2014 14:00	0.369350095		17/11/2014 14:00	0.6	
17/11/2014 14:15	0.314530066		17/11/2014 14:15	0.4	
17/11/2014 14:30	0.253303945		17/11/2014 14:30	.	
17/11/2014 14:45	0.239769495		17/11/2014 14:45	.	
17/11/2014 15:00	0.241489854		17/11/2014 15:00	.	
17/11/2014 15:15	0.217655447		17/11/2014 15:15	.	
17/11/2014 15:30	0.211774795		17/11/2014 15:30	.	
17/11/2014 15:45	0.202665295		17/11/2014 15:45	.	
17/11/2014 16:00	0.186887424		17/11/2014 16:00	.	
17/11/2014 16:15	0.186515514		17/11/2014 16:15	.	
17/11/2014 16:30	0.179877178		17/11/2014 16:30	.	
17/11/2014 16:45	0.161950809		17/11/2014 16:45	.	
17/11/2014 17:00	0.170411814		17/11/2014 17:00	0.8	
17/11/2014 17:15	0.167494683		17/11/2014 17:15	0.4	
17/11/2014 17:30	0.173358481		17/11/2014 17:30	.	
17/11/2014 17:45	0.225037987		17/11/2014 17:45	.	
17/11/2014 18:00	0.232566095		17/11/2014 18:00	.	
17/11/2014 18:15	0.23080282		17/11/2014 18:15	0.6	
17/11/2014 18:30	0.235432981		17/11/2014 18:30	0.2	
17/11/2014 18:45	0.265671639		17/11/2014 18:45	.	
17/11/2014 19:00	0.383507353		17/11/2014 19:00	.	
17/11/2014 19:15	0.344035774		17/11/2014 19:15	.	
17/11/2014 19:30	0.33661187		17/11/2014 19:30	.	
17/11/2014 19:45	0.31166945		17/11/2014 19:45	.	
17/11/2014 20:00	0.254609499		17/11/2014 20:00	.	
17/11/2014 20:15	0.228233221		17/11/2014 20:15	0.2	
17/11/2014 20:30	0.214321466		17/11/2014 20:30	0.4	
17/11/2014 20:45	0.269145493		17/11/2014 20:45	.	
17/11/2014 21:00	0.283427815		17/11/2014 21:00	.	
17/11/2014 21:15	0.303503058		17/11/2014 21:15	.	
17/11/2014 21:30	0.296443628		17/11/2014 21:30	.	
17/11/2014 21:45	0.306814461		17/11/2014 21:45	.	
17/11/2014 22:00	0.296132595		17/11/2014 22:00	.	
17/11/2014 22:15	0.308928899		17/11/2014 22:15	.	
17/11/2014 22:30	0.276894062		17/11/2014 22:30	0.2	
17/11/2014 22:45	0.280339316		17/11/2014 22:45	0.2	
17/11/2014 23:00	0.274872249		17/11/2014 23:00	.	
17/11/2014 23:15	0.281326083		17/11/2014 23:15	.	
17/11/2014 23:30	0.269805784		17/11/2014 23:30	.	
17/11/2014 23:45	0.262220747		17/11/2014 23:45	.	
18/11/2014 00:00	0.253907279		18/11/2014 00:00	.	
18/11/2014 00:15	0.268119875		18/11/2014 00:15	.	
18/11/2014 00:30	0.265774702		18/11/2014 00:30	.	
18/11/2014 00:45	0.260807141		18/11/2014 00:45	.	
18/11/2014 01:00	0.242824432		18/11/2014 01:00	.	
18/11/2014 01:15	0.256779825		18/11/2014 01:15	.	
18/11/2014 01:30	0.227770026		18/11/2014 01:30	.	
18/11/2014 01:45	0.233056129		18/11/2014 01:45	.	

			Thorpeness TBR RG		
G5 Flow		Middleton Flow	Date & Time	Rainfall (mm)	Daily Rainfall (mm)
18/11/2014 02:00	0.221514533		18/11/2014 02:00	.	
18/11/2014 02:15	0.237897315		18/11/2014 02:15	.	
18/11/2014 02:30	0.221081262		18/11/2014 02:30	.	
18/11/2014 02:45	0.228641082		18/11/2014 02:45	.	
18/11/2014 03:00	0.226733179		18/11/2014 03:00	.	
18/11/2014 03:15	0.219845556		18/11/2014 03:15	.	
18/11/2014 03:30	0.212835341		18/11/2014 03:30	.	
18/11/2014 03:45	0.204672576		18/11/2014 03:45	.	
18/11/2014 04:00	0.196655552		18/11/2014 04:00	.	
18/11/2014 04:15	0.197442959		18/11/2014 04:15	.	
18/11/2014 04:30	0.19693841		18/11/2014 04:30	.	
18/11/2014 04:45	0.193981819		18/11/2014 04:45	.	
18/11/2014 05:00	0.16722257		18/11/2014 05:00	.	
18/11/2014 05:15	0.151676266		18/11/2014 05:15	.	
18/11/2014 05:30	0.144609836		18/11/2014 05:30	.	
18/11/2014 05:45	0.152581425		18/11/2014 05:45	.	
18/11/2014 06:00	0.18502064		18/11/2014 06:00	.	
18/11/2014 06:15	0.153268835		18/11/2014 06:15	.	
18/11/2014 06:30	0.150500399		18/11/2014 06:30	.	
18/11/2014 06:45	0.170958426		18/11/2014 06:45	.	
18/11/2014 07:00	0.152899379		18/11/2014 07:00	.	
18/11/2014 07:15	0.149317904		18/11/2014 07:15	.	
18/11/2014 07:30	0.155257072		18/11/2014 07:30	.	
18/11/2014 07:45	0.150411032		18/11/2014 07:45	.	
18/11/2014 08:00	0.154581135		18/11/2014 08:00	.	
18/11/2014 08:15	0.147427316		18/11/2014 08:15	.	
18/11/2014 08:30	0.139716097		18/11/2014 08:30	0.2	
18/11/2014 08:45	0.144241362		18/11/2014 08:45	.	
18/11/2014 09:00	0.161053445		18/11/2014 09:00	.	6
18/11/2014 09:15	0.159109145		18/11/2014 09:15	.	
18/11/2014 09:30	0.133160021		18/11/2014 09:30	.	
18/11/2014 09:45	0.14769843		18/11/2014 09:45	.	
18/11/2014 10:00	0.146229555		18/11/2014 10:00	.	
18/11/2014 10:15	0.13069783		18/11/2014 10:15	.	
18/11/2014 10:30	0.139491059		18/11/2014 10:30	.	
18/11/2014 10:45	0.146656435		18/11/2014 10:45	.	
18/11/2014 11:00	0.135476818		18/11/2014 11:00	.	
18/11/2014 11:15	0.13230839		18/11/2014 11:15	.	
18/11/2014 11:30	0.111391076		18/11/2014 11:30	.	
18/11/2014 11:45	0.136770795		18/11/2014 11:45	.	
18/11/2014 12:00	0.122617793		18/11/2014 12:00	.	
18/11/2014 12:15	0.133595785		18/11/2014 12:15	.	
18/11/2014 12:30	0.126784623		18/11/2014 12:30	.	
18/11/2014 12:45	0.115675262		18/11/2014 12:45	.	
18/11/2014 13:00	0.119382675		18/11/2014 13:00	.	
18/11/2014 13:15	0.107687996		18/11/2014 13:15	.	
18/11/2014 13:30	0.112073148		18/11/2014 13:30	.	
18/11/2014 13:45	0.109812145		18/11/2014 13:45	.	
18/11/2014 14:00	0.10426806		18/11/2014 14:00	.	
18/11/2014 14:15	0.110284113		18/11/2014 14:15	.	
18/11/2014 14:30	0.100100278		18/11/2014 14:30	.	
18/11/2014 14:45	0.105845956		18/11/2014 14:45	.	

						Thorpeness TBR RG	
G5 Flow			Middleton Flow		Date & Time	Rainfall (mm)	Daily Rainfall (mm)
18/11/2014 15:00	0.102083663				18/11/2014 15:00	.	
18/11/2014 15:15	0.116371571				18/11/2014 15:15	.	
18/11/2014 15:30	0.104734328				18/11/2014 15:30	.	
18/11/2014 15:45	0.101035233				18/11/2014 15:45	.	
18/11/2014 16:00	0.103488475				18/11/2014 16:00	.	
18/11/2014 16:15	0.09900884				18/11/2014 16:15	.	
18/11/2014 16:30	0.096173128				18/11/2014 16:30	.	
18/11/2014 16:45	0.095515733				18/11/2014 16:45	.	
18/11/2014 17:00	0.100038177				18/11/2014 17:00	.	
18/11/2014 17:15	0.09282653				18/11/2014 17:15	.	
18/11/2014 17:30	0.09218277				18/11/2014 17:30	.	
18/11/2014 17:45	0.090096386				18/11/2014 17:45	.	
18/11/2014 18:00	0.096598667				18/11/2014 18:00	.	
18/11/2014 18:15	0.090902231				18/11/2014 18:15	.	
18/11/2014 18:30	0.098832811				18/11/2014 18:30	.	
18/11/2014 18:45	0.091760084				18/11/2014 18:45	.	
18/11/2014 19:00	0.096053413				18/11/2014 19:00	.	
18/11/2014 19:15	0.090472732				18/11/2014 19:15	.	
18/11/2014 19:30	0.088438586				18/11/2014 19:30	.	
18/11/2014 19:45	0.096815433				18/11/2014 19:45	.	
18/11/2014 20:00	0.092002255				18/11/2014 20:00	.	
18/11/2014 20:15	0.091348191				18/11/2014 20:15	.	
18/11/2014 20:30	0.08729552				18/11/2014 20:30	.	
18/11/2014 20:45	0.083963035				18/11/2014 20:45	.	
18/11/2014 21:00	0.086712955				18/11/2014 21:00	.	
18/11/2014 21:15	0.084749711				18/11/2014 21:15	.	
18/11/2014 21:30	0.084082011				18/11/2014 21:30	.	
18/11/2014 21:45	0.081478312				18/11/2014 21:45	.	
18/11/2014 22:00	0.076923531				18/11/2014 22:00	.	
18/11/2014 22:15	0.084215743				18/11/2014 22:15	.	
18/11/2014 22:30	0.083597338				18/11/2014 22:30	.	
18/11/2014 22:45	0.077804832				18/11/2014 22:45	.	
18/11/2014 23:00	0.078509857				18/11/2014 23:00	.	
18/11/2014 23:15	0.072895069				18/11/2014 23:15	.	
18/11/2014 23:30	0.076756386				18/11/2014 23:30	.	
18/11/2014 23:45	0.083696353				18/11/2014 23:45	.	
19/11/2014 00:00	0.075598897	19/11/2014	00:00:00	1 23	19/11/2014 00:00	.	
19/11/2014 00:15	0.075679657	19/11/2014	00:15:00	1 22	19/11/2014 00:15	.	
19/11/2014 00:30	0.078153452	19/11/2014	00:30:00	1.2	19/11/2014 00:30	.	
19/11/2014 00:45	0.070278992	19/11/2014	00:45:00	1.18	19/11/2014 00:45	.	
19/11/2014 01:00	0.072142866	19/11/2014	01:00:00	1.16	19/11/2014 01:00	.	
19/11/2014 01:15	0.070386029	19/11/2014	01:15:00	1.14	19/11/2014 01:15	.	
19/11/2014 01:30	0.064485755	19/11/2014	01:30:00	1.13	19/11/2014 01:30	.	
19/11/2014 01:45	0.071060772	19/11/2014	01:45:00	1.12	19/11/2014 01:45	.	
19/11/2014 02:00	0.07402335	19/11/2014	02:00:00	1.1	19/11/2014 02:00	.	
19/11/2014 02:15	0.072279715	19/11/2014	02:15:00	1 09	19/11/2014 02:15	.	
19/11/2014 02:30	0.065924651	19/11/2014	02:30:00	1 08	19/11/2014 02:30	.	
19/11/2014 02:45	0.069996262	19/11/2014	02:45:00	1 07	19/11/2014 02:45	.	
19/11/2014 03:00	0.064958144	19/11/2014	03:00:00	1 05	19/11/2014 03:00	.	
19/11/2014 03:15	0.059140491	19/11/2014	03:15:00	1 04	19/11/2014 03:15	.	
19/11/2014 03:30	0.056733797	19/11/2014	03:30:00	1 02	19/11/2014 03:30	.	
19/11/2014 03:45	0.05831748	19/11/2014	03:45:00	1 01	19/11/2014 03:45	.	

	G5 Flow			Middleton Flow		Thorpeness TBR RG		
						Date & Time	Rainfall (mm)	Daily Rainfall (mm)
19/11/2014 04:00	0.05103855	19/11/2014	04:00:00	0.999		19/11/2014 04:00	.	
19/11/2014 04:15	0.049682361	19/11/2014	04:15:00	0 99		19/11/2014 04:15	.	
19/11/2014 04:30	0.046540893	19/11/2014	04:30:00	0.974		19/11/2014 04:30	.	
19/11/2014 04:45	0.049699607	19/11/2014	04:45:00	0.966		19/11/2014 04:45	.	
19/11/2014 05:00	0.045293411	19/11/2014	05:00:00	0.949		19/11/2014 05:00	.	
19/11/2014 05:15	0.044451296	19/11/2014	05:15:00	0.941		19/11/2014 05:15	.	
19/11/2014 05:30	0.040256215	19/11/2014	05:30:00	0.933		19/11/2014 05:30	.	
19/11/2014 05:45	0.039478346	19/11/2014	05:45:00	0.925		19/11/2014 05:45	.	
19/11/2014 06:00	0.041140759	19/11/2014	06:00:00	0.909		19/11/2014 06:00	.	
19/11/2014 06:15	0.039532644	19/11/2014	06:15:00	0.901		19/11/2014 06:15	.	
19/11/2014 06:30	0.041125454	19/11/2014	06:30:00	0.893		19/11/2014 06:30	.	
19/11/2014 06:45	0.039935816	19/11/2014	06:45:00	0.885		19/11/2014 06:45	.	
19/11/2014 07:00	0.04109195	19/11/2014	07:00:00	0.877		19/11/2014 07:00	.	
19/11/2014 07:15	0.040703595	19/11/2014	07:15:00	0.869		19/11/2014 07:15	.	
19/11/2014 07:30	0.040703595	19/11/2014	07:30:00	0.861		19/11/2014 07:30	.	
19/11/2014 07:45	0.040703595	19/11/2014	07:45:00	0.853		19/11/2014 07:45	.	
19/11/2014 08:00	0.041894472	19/11/2014	08:00:00	0.845		19/11/2014 08:00	.	
19/11/2014 08:15	0.038754741	19/11/2014	08:15:00	0.837		19/11/2014 08:15	.	
19/11/2014 08:30	0.05339999	19/11/2014	08:30:00	0.822		19/11/2014 08:30	.	
19/11/2014 08:45	0.049427103	19/11/2014	08:45:00	0.814		19/11/2014 08:45	.	
19/11/2014 09:00	0.052059427	19/11/2014	09:00:00	0.814		19/11/2014 09:00	.	0
19/11/2014 09:15	0.050066277	19/11/2014	09:15:00	0.799		19/11/2014 09:15	.	
19/11/2014 09:30	0.05232353	19/11/2014	09:30:00	0.799		19/11/2014 09:30	.	
19/11/2014 09:45	0.054580912	19/11/2014	09:45:00	0.791		19/11/2014 09:45	.	
19/11/2014 10:00	0.055974442	19/11/2014	10:00:00	0.784		19/11/2014 10:00	.	
19/11/2014 10:15	0.059552953	19/11/2014	10:15:00	0.776		19/11/2014 10:15	.	
19/11/2014 10:30	0.056421756	19/11/2014	10:30:00	0.769		19/11/2014 10:30	.	
19/11/2014 10:45	0.051918382	19/11/2014	10:45:00	0.761		19/11/2014 10:45	.	
19/11/2014 11:00	0.050587117	19/11/2014	11:00:00	0.754		19/11/2014 11:00	.	
19/11/2014 11:15	0.0556745	19/11/2014	11:15:00	0.746		19/11/2014 11:15	.	
19/11/2014 11:30	0.059110478	19/11/2014	11:30:00	0.739		19/11/2014 11:30	.	
19/11/2014 11:45	0.062012765	19/11/2014	11:45:00	0.731		19/11/2014 11:45	.	
19/11/2014 12:00	0.05390247	19/11/2014	12:00:00	0.731		19/11/2014 12:00	.	
19/11/2014 12:15	0.054266803	19/11/2014	12:15:00	0.724		19/11/2014 12:15	.	
19/11/2014 12:30	0.047924587	19/11/2014	12:30:00	0.717		19/11/2014 12:30	.	
19/11/2014 12:45	0.047453205	19/11/2014	12:45:00	0.709		19/11/2014 12:45	.	
19/11/2014 13:00	0.045719866	19/11/2014	13:00:00	0.702		19/11/2014 13:00	.	
19/11/2014 13:15	0.041529014	19/11/2014	13:15:00	0.695		19/11/2014 13:15	.	
19/11/2014 13:30	0.042771551	19/11/2014	13:30:00	0.695		19/11/2014 13:30	.	
19/11/2014 13:45	0.042762166	19/11/2014	13:45:00	0.688		19/11/2014 13:45	.	
19/11/2014 14:00	0.043150008	19/11/2014	14:00:00	0.681		19/11/2014 14:00	.	
19/11/2014 14:15	0.045120432	19/11/2014	14:15:00	0.673		19/11/2014 14:15	.	
19/11/2014 14:30	0.041520573	19/11/2014	14:30:00	0.666		19/11/2014 14:30	.	
19/11/2014 14:45	0.040335216	19/11/2014	14:45:00	0.659		19/11/2014 14:45	.	
19/11/2014 15:00	0.041894472	19/11/2014	15:00:00	0.652		19/11/2014 15:00	.	
19/11/2014 15:15	0.041502741	19/11/2014	15:15:00	0.652		19/11/2014 15:15	.	
19/11/2014 15:30	0.043422079	19/11/2014	15:30:00	0.645		19/11/2014 15:30	.	
19/11/2014 15:45	0.039528346	19/11/2014	15:45:00	0.638		19/11/2014 15:45	.	
19/11/2014 16:00	0.040683317	19/11/2014	16:00:00	0.638		19/11/2014 16:00	.	
19/11/2014 16:15	0.041421755	19/11/2014	16:15:00	0.631		19/11/2014 16:15	.	
19/11/2014 16:30	0.046303565	19/11/2014	16:30:00	0.624		19/11/2014 16:30	.	
19/11/2014 16:45	0.037595519	19/11/2014	16:45:00	0.617		19/11/2014 16:45	.	

	G5 Flow		Middleton Flow		Thorpeness TBR RG		
				Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
19/11/2014 17:00	0.039470356	19/11/2014 17:00:00	0.617	19/11/2014 17:00	.		
19/11/2014 17:15	0.039813643	19/11/2014 17:15:00	0.611	19/11/2014 17:15	0.2		
19/11/2014 17:30	0.036840443	19/11/2014 17:30:00	0.604	19/11/2014 17:30	.		
19/11/2014 17:45	0.040970226	19/11/2014 17:45:00	0.597	19/11/2014 17:45	.		
19/11/2014 18:00	0.039494225	19/11/2014 18:00:00	0.597	19/11/2014 18:00	.		
19/11/2014 18:15	0.039513567	19/11/2014 18:15:00	0 59	19/11/2014 18:15	.		
19/11/2014 18:30	0.039143356	19/11/2014 18:30:00	0 59	19/11/2014 18:30	.		
19/11/2014 18:45	0.038760623	19/11/2014 18:45:00	0.583	19/11/2014 18:45	.		
19/11/2014 19:00	0.038326856	19/11/2014 19:00:00	0.577	19/11/2014 19:00	.		
19/11/2014 19:15	0.044383574	19/11/2014 19:15:00	0.577	19/11/2014 19:15	.		
19/11/2014 19:30	0.044425127	19/11/2014 19:30:00	0 57	19/11/2014 19:30	.		
19/11/2014 19:45	0.043607459	19/11/2014 19:45:00	0 57	19/11/2014 19:45	.		
19/11/2014 20:00	0.045270214	19/11/2014 20:00:00	0.563	19/11/2014 20:00	.		
19/11/2014 20:15	0.043607459	19/11/2014 20:15:00	0.563	19/11/2014 20:15	.		
19/11/2014 20:30	0.044028632	19/11/2014 20:30:00	0.557	19/11/2014 20:30	.		
19/11/2014 20:45	0.041113325	19/11/2014 20:45:00	0.557	19/11/2014 20:45	.		
19/11/2014 21:00	0.03945057	19/11/2014 21:00:00	0 55	19/11/2014 21:00	.		
19/11/2014 21:15	0.044438836	19/11/2014 21:15:00	0.544	19/11/2014 21:15	.		
19/11/2014 21:30	0.044406696	19/11/2014 21:30:00	0.544	19/11/2014 21:30	.		
19/11/2014 21:45	0.037866118	19/11/2014 21:45:00	0.544	19/11/2014 21:45	.		
19/11/2014 22:00	0.038303295	19/11/2014 22:00:00	0.537	19/11/2014 22:00	.		
19/11/2014 22:15	0.041140362	19/11/2014 22:15:00	0.537	19/11/2014 22:15	.		
19/11/2014 22:30	0.033563401	19/11/2014 22:30:00	0.531	19/11/2014 22:30	.		
19/11/2014 22:45	0.037569384	19/11/2014 22:45:00	0.531	19/11/2014 22:45	.		
19/11/2014 23:00	0.039544085	19/11/2014 23:00:00	0.524	19/11/2014 23:00	.		
19/11/2014 23:15	0.036820046	19/11/2014 23:15:00	0.524	19/11/2014 23:15	.		
19/11/2014 23:30	0.036448423	19/11/2014 23:30:00	0.524	19/11/2014 23:30	.		
19/11/2014 23:45	0.036078828	19/11/2014 23:45:00	0.518	19/11/2014 23:45	.		
20/11/2014 00:00	0.037602742	20/11/2014 00:00:00	0.518	20/11/2014 00:00	.		
20/11/2014 00:15	0.03459578	20/11/2014 00:15:00	0.511	20/11/2014 00:15	.		
20/11/2014 00:30	0.032008992	20/11/2014 00:30:00	0.511	20/11/2014 00:30	.		
20/11/2014 00:45	0.033896159	20/11/2014 00:45:00	0.505	20/11/2014 00:45	.		
20/11/2014 01:00	0.033548295	20/11/2014 01:00:00	0.505	20/11/2014 01:00	.		
20/11/2014 01:15	0.030027467	20/11/2014 01:15:00	0.499	20/11/2014 01:15	.		
20/11/2014 01:30	0.034910928	20/11/2014 01:30:00	0.499	20/11/2014 01:30	.		
20/11/2014 01:45	0.029436666	20/11/2014 01:45:00	0.493	20/11/2014 01:45	.		
20/11/2014 02:00	0.02678371	20/11/2014 02:00:00	0.493	20/11/2014 02:00	.		
20/11/2014 02:15	0.029777732	20/11/2014 02:15:00	0.486	20/11/2014 02:15	.		
20/11/2014 02:30	0.028158543	20/11/2014 02:30:00	0.486	20/11/2014 02:30	.		
20/11/2014 02:45	0.028475743	20/11/2014 02:45:00	0.48	20/11/2014 02:45	.		
20/11/2014 03:00	0.025938997	20/11/2014 03:00:00	0.48	20/11/2014 03:00	.		
20/11/2014 03:15	0.025658859	20/11/2014 03:15:00	0.48	20/11/2014 03:15	.		
20/11/2014 03:30	0.028133546	20/11/2014 03:30:00	0.48	20/11/2014 03:30	.		
20/11/2014 03:45	0.02506911	20/11/2014 03:45:00	0.474	20/11/2014 03:45	.		
20/11/2014 04:00	0.023292085	20/11/2014 04:00:00	0.474	20/11/2014 04:00	.		
20/11/2014 04:15	0.027450745	20/11/2014 04:15:00	0.468	20/11/2014 04:15	.		
20/11/2014 04:30	0.025381119	20/11/2014 04:30:00	0.468	20/11/2014 04:30	.		
20/11/2014 04:45	0.027131127	20/11/2014 04:45:00	0.468	20/11/2014 04:45	.		
20/11/2014 05:00	0.024206651	20/11/2014 05:00:00	0.462	20/11/2014 05:00	.		
20/11/2014 05:15	0.023917	20/11/2014 05:15:00	0.462	20/11/2014 05:15	.		
20/11/2014 05:30	0.025064554	20/11/2014 05:30:00	0.455	20/11/2014 05:30	.		
20/11/2014 05:45	0.025333165	20/11/2014 05:45:00	0.455	20/11/2014 05:45	.		

	G5 Flow		Middleton Flow	Thorpeness TBR RG Date & Time	Rainfall (mm)	Daily Rainfall (mm)
20/11/2014 06:00	0.023907477	20/11/2014 06:00:00	0.455	20/11/2014 06:00	.	
20/11/2014 06:15	0.021951756	20/11/2014 06:15:00	0.449	20/11/2014 06:15	.	
20/11/2014 06:30	0.023896232	20/11/2014 06:30:00	0.449	20/11/2014 06:30	.	
20/11/2014 06:45	0.021396192	20/11/2014 06:45:00	0.449	20/11/2014 06:45	.	
20/11/2014 07:00	0.023340667	20/11/2014 07:00:00	0.443	20/11/2014 07:00	.	
20/11/2014 07:15	0.021100175	20/11/2014 07:15:00	0.443	20/11/2014 07:15	.	
20/11/2014 07:30	0.024765783	20/11/2014 07:30:00	0.443	20/11/2014 07:30	.	
20/11/2014 07:45	0.028009075	20/11/2014 07:45:00	0.443	20/11/2014 07:45	.	
20/11/2014 08:00	0.027473675	20/11/2014 08:00:00	0.437	20/11/2014 08:00	.	
20/11/2014 08:15	0.028457024	20/11/2014 08:15:00	0.437	20/11/2014 08:15	.	
20/11/2014 08:30	0.03328182	20/11/2014 08:30:00	0.431	20/11/2014 08:30	.	
20/11/2014 08:45	0.033771977	20/11/2014 08:45:00	0.431	20/11/2014 08:45	.	
20/11/2014 09:00	0.035566839	20/11/2014 09:00:00	0.431	20/11/2014 09:00	.	0.2
20/11/2014 09:15	0.037027919	20/11/2014 09:15:00	0.431	20/11/2014 09:15	.	
20/11/2014 09:30	0.039642782	20/11/2014 09:30:00	0.425	20/11/2014 09:30	.	
20/11/2014 09:45	0.039736972	20/11/2014 09:45:00	0.425	20/11/2014 09:45	.	
20/11/2014 10:00	0.035725725	20/11/2014 10:00:00	0.42	20/11/2014 10:00	.	
20/11/2014 10:15	0.038672481	20/11/2014 10:15:00	0.42	20/11/2014 10:15	.	
20/11/2014 10:30	0.031265692	20/11/2014 10:30:00	0.42	20/11/2014 10:30	.	
20/11/2014 10:45	0.037583743	20/11/2014 10:45:00	0.42	20/11/2014 10:45	.	
20/11/2014 11:00	0.043092615	20/11/2014 11:00:00	0.414	20/11/2014 11:00	.	
20/11/2014 11:15	0.04346096	20/11/2014 11:15:00	0.414	20/11/2014 11:15	.	
20/11/2014 11:30	0.038672481	20/11/2014 11:30:00	0.414	20/11/2014 11:30	.	
20/11/2014 11:45	0.038720422	20/11/2014 11:45:00	0.414	20/11/2014 11:45	.	
20/11/2014 12:00	0.040629115	20/11/2014 12:00:00	0.408	20/11/2014 12:00	.	
20/11/2014 12:15	0.040276842	20/11/2014 12:15:00	0.408	20/11/2014 12:15	.	
20/11/2014 12:30	0.036846149	20/11/2014 12:30:00	0.408	20/11/2014 12:30	.	
20/11/2014 12:45	0.037583743	20/11/2014 12:45:00	0.408	20/11/2014 12:45	.	
20/11/2014 13:00	0.036036789	20/11/2014 13:00:00	0.402	20/11/2014 13:00	.	
20/11/2014 13:15	0.029323476	20/11/2014 13:15:00	0.402	20/11/2014 13:15	.	
20/11/2014 13:30	0.037725443	20/11/2014 13:30:00	0.402	20/11/2014 13:30	.	
20/11/2014 13:45	0.03528411	20/11/2014 13:45:00	0.396	20/11/2014 13:45	.	
20/11/2014 14:00	0.031801067	20/11/2014 14:00:00	0.396	20/11/2014 14:00	.	
20/11/2014 14:15	0.030431881	20/11/2014 14:15:00	0.396	20/11/2014 14:15	.	
20/11/2014 14:30	0.033492601	20/11/2014 14:30:00	0.396	20/11/2014 14:30	.	
20/11/2014 14:45	0.03111867	20/11/2014 14:45:00	0.391	20/11/2014 14:45	.	
20/11/2014 15:00	0.032475202	20/11/2014 15:00:00	0.391	20/11/2014 15:00	.	
20/11/2014 15:15	0.030440404	20/11/2014 15:15:00	0.391	20/11/2014 15:15	.	
20/11/2014 15:30	0.030779537	20/11/2014 15:30:00	0.391	20/11/2014 15:30	.	
20/11/2014 15:45	0.035527399	20/11/2014 15:45:00	0.391	20/11/2014 15:45	.	
20/11/2014 16:00	0.032796143	20/11/2014 16:00:00	0.385	20/11/2014 16:00	.	
20/11/2014 16:15	0.031452352	20/11/2014 16:15:00	0.385	20/11/2014 16:15	.	
20/11/2014 16:30	0.033803986	20/11/2014 16:30:00	0.385	20/11/2014 16:30	.	
20/11/2014 16:45	0.033803986	20/11/2014 16:45:00	0.385	20/11/2014 16:45	.	
20/11/2014 17:00	0.032796143	20/11/2014 17:00:00	0.379	20/11/2014 17:00	.	
20/11/2014 17:15	0.034475882	20/11/2014 17:15:00	0.379	20/11/2014 17:15	.	
20/11/2014 17:30	0.031116405	20/11/2014 17:30:00	0.379	20/11/2014 17:30	.	
20/11/2014 17:45	0.038507254	20/11/2014 17:45:00	0.379	20/11/2014 17:45	.	
20/11/2014 18:00	0.033831734	20/11/2014 18:00:00	0.374	20/11/2014 18:00	.	
20/11/2014 18:15	0.037278491	20/11/2014 18:15:00	0.374	20/11/2014 18:15	.	
20/11/2014 18:30	0.03659383	20/11/2014 18:30:00	0.374	20/11/2014 18:30	.	
20/11/2014 18:45	0.035602008	20/11/2014 18:45:00	0.374	20/11/2014 18:45	.	

	G5 Flow		Middleton Flow		Thorpeness TBR RG Date & Time	Rainfall (mm)	Daily Rainfall (mm)
20/11/2014 19:00	0.035659397	20/11/2014 19:00:00	0.368		20/11/2014 19:00	.	
20/11/2014 19:15	0.034615823	20/11/2014 19:15:00	0.368		20/11/2014 19:15	.	
20/11/2014 19:30	0.034627283	20/11/2014 19:30:00	0.368		20/11/2014 19:30	.	
20/11/2014 19:45	0.041562226	20/11/2014 19:45:00	0.362		20/11/2014 19:45	.	
20/11/2014 20:00	0.038327043	20/11/2014 20:00:00	0.362		20/11/2014 20:00	.	
20/11/2014 20:15	0.039845324	20/11/2014 20:15:00	0.362		20/11/2014 20:15	.	
20/11/2014 20:30	0.037595519	20/11/2014 20:30:00	0.362		20/11/2014 20:30	.	
20/11/2014 20:45	0.035720682	20/11/2014 20:45:00	0.362		20/11/2014 20:45	.	
20/11/2014 21:00	0.036845584	20/11/2014 21:00:00	0.362		20/11/2014 21:00	.	
20/11/2014 21:15	0.037970487	20/11/2014 21:15:00	0.357		20/11/2014 21:15	.	
20/11/2014 21:30	0.037970487	20/11/2014 21:30:00	0.357		20/11/2014 21:30	.	
20/11/2014 21:45	0.042095129	20/11/2014 21:45:00	0.357		20/11/2014 21:45	.	
20/11/2014 22:00	0.035725493	20/11/2014 22:00:00	0.357		20/11/2014 22:00	.	
20/11/2014 22:15	0.033884003	20/11/2014 22:15:00	0.357		20/11/2014 22:15	.	
20/11/2014 22:30	0.037181616	20/11/2014 22:30:00	0.351		20/11/2014 22:30	.	
20/11/2014 22:45	0.034627283	20/11/2014 22:45:00	0.351		20/11/2014 22:45	.	
20/11/2014 23:00	0.033550099	20/11/2014 23:00:00	0.351		20/11/2014 23:00	.	
20/11/2014 23:15	0.031787445	20/11/2014 23:15:00	0.351		20/11/2014 23:15	.	
20/11/2014 23:30	0.030401445	20/11/2014 23:30:00	0.351		20/11/2014 23:30	.	
20/11/2014 23:45	0.033889063	20/11/2014 23:45:00	0.351		20/11/2014 23:45	.	
21/11/2014 00:00	0.032842778	21/11/2014 00:00:00	0.346		21/11/2014 00:00	.	
21/11/2014 00:15	0.033874307	21/11/2014 00:15:00	0.346		21/11/2014 00:15	.	
21/11/2014 00:30	0.033855186	21/11/2014 00:30:00	0.346		21/11/2014 00:30	.	
21/11/2014 00:45	0.036491568	21/11/2014 00:45:00	0.346		21/11/2014 00:45	.	
21/11/2014 01:00	0.030439604	21/11/2014 01:00:00	0.346		21/11/2014 01:00	.	
21/11/2014 01:15	0.028800798	21/11/2014 01:15:00	0.341		21/11/2014 01:15	.	
21/11/2014 01:30	0.029119157	21/11/2014 01:30:00	0.341		21/11/2014 01:30	.	
21/11/2014 01:45	0.030695396	21/11/2014 01:45:00	0.341		21/11/2014 01:45	.	
21/11/2014 02:00	0.03003846	21/11/2014 02:00:00	0.341		21/11/2014 02:00	.	
21/11/2014 02:15	0.029364878	21/11/2014 02:15:00	0.335		21/11/2014 02:15	.	
21/11/2014 02:30	0.031469302	21/11/2014 02:30:00	0.335		21/11/2014 02:30	.	
21/11/2014 02:45	0.03195395	21/11/2014 02:45:00	0.335		21/11/2014 02:45	.	
21/11/2014 03:00	0.02567678	21/11/2014 03:00:00	0.335		21/11/2014 03:00	.	
21/11/2014 03:15	0.025654903	21/11/2014 03:15:00	0.335		21/11/2014 03:15	.	
21/11/2014 03:30	0.026211211	21/11/2014 03:30:00	0 33		21/11/2014 03:30	.	
21/11/2014 03:45	0.027886382	21/11/2014 03:45:00	0 33		21/11/2014 03:45	.	
21/11/2014 04:00	0.025311127	21/11/2014 04:00:00	0 33		21/11/2014 04:00	.	
21/11/2014 04:15	0.025872588	21/11/2014 04:15:00	0 33		21/11/2014 04:15	.	
21/11/2014 04:30	0.026396272	21/11/2014 04:30:00	0 33		21/11/2014 04:30	.	
21/11/2014 04:45	0.024705553	21/11/2014 04:45:00	0.325		21/11/2014 04:45	.	
21/11/2014 05:00	0.022781623	21/11/2014 05:00:00	0.325		21/11/2014 05:00	.	
21/11/2014 05:15	0.023318002	21/11/2014 05:15:00	0.325		21/11/2014 05:15	.	
21/11/2014 05:30	0.023861851	21/11/2014 05:30:00	0.325		21/11/2014 05:30	.	
21/11/2014 05:45	0.027066976	21/11/2014 05:45:00	0.325		21/11/2014 05:45	.	
21/11/2014 06:00	0.025183867	21/11/2014 06:00:00	0.319		21/11/2014 06:00	.	
21/11/2014 06:15	0.023013502	21/11/2014 06:15:00	0.319		21/11/2014 06:15	.	
21/11/2014 06:30	0.024344098	21/11/2014 06:30:00	0.319		21/11/2014 06:30	.	
21/11/2014 06:45	0.027605007	21/11/2014 06:45:00	0.319		21/11/2014 06:45	.	
21/11/2014 07:00	0.022215144	21/11/2014 07:00:00	0.319		21/11/2014 07:00	.	
21/11/2014 07:15	0.026259929	21/11/2014 07:15:00	0.314		21/11/2014 07:15	.	
21/11/2014 07:30	0.024677626	21/11/2014 07:30:00	0.314		21/11/2014 07:30	.	
21/11/2014 07:45	0.028062965	21/11/2014 07:45:00	0.314		21/11/2014 07:45	.	

	G5 Flow			Middleton Flow		Thorpeness TBR RG		
					Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
21/11/2014 08:00	0.028217861	21/11/2014	08:00:00	0.314	21/11/2014 08:00	.		
21/11/2014 08:15	0.027450745	21/11/2014	08:15:00	0.314	21/11/2014 08:15	.		
21/11/2014 08:30	0.033907471	21/11/2014	08:30:00	0.309	21/11/2014 08:30	.		
21/11/2014 08:45	0.035451794	21/11/2014	08:45:00	0.309	21/11/2014 08:45	.		
21/11/2014 09:00	0.037765272	21/11/2014	09:00:00	0.309	21/11/2014 09:00	.		0
21/11/2014 09:15	0.041010169	21/11/2014	09:15:00	0.309	21/11/2014 09:15	.		
21/11/2014 09:30	0.042586202	21/11/2014	09:30:00	0.309	21/11/2014 09:30	.		
21/11/2014 09:45	0.041927277	21/11/2014	09:45:00	0.304	21/11/2014 09:45	.		
21/11/2014 10:00	0.039040826	21/11/2014	10:00:00	0.304	21/11/2014 10:00	.		
21/11/2014 10:15	0.04346096	21/11/2014	10:15:00	0.304	21/11/2014 10:15	.		
21/11/2014 10:30	0.044197649	21/11/2014	10:30:00	0.304	21/11/2014 10:30	.		
21/11/2014 10:45	0.03864182	21/11/2014	10:45:00	0.304	21/11/2014 10:45	.		
21/11/2014 11:00	0.036816566	21/11/2014	11:00:00	0.298	21/11/2014 11:00	.		
21/11/2014 11:15	0.036074359	21/11/2014	11:15:00	0.304	21/11/2014 11:15	.		
21/11/2014 11:30	0.034265293	21/11/2014	11:30:00	0.298	21/11/2014 11:30	.		
21/11/2014 11:45	0.033889063	21/11/2014	11:45:00	0.298	21/11/2014 11:45	.		
21/11/2014 12:00	0.034565388	21/11/2014	12:00:00	0.298	21/11/2014 12:00	.		
21/11/2014 12:15	0.033170525	21/11/2014	12:15:00	0.298	21/11/2014 12:15	.		
21/11/2014 12:30	0.034811829	21/11/2014	12:30:00	0.298	21/11/2014 12:30	.		
21/11/2014 12:45	0.034811829	21/11/2014	12:45:00	0.298	21/11/2014 12:45	.		
21/11/2014 13:00	0.033468039	21/11/2014	13:00:00	0.298	21/11/2014 13:00	.		
21/11/2014 13:15	0.034475882	21/11/2014	13:15:00	0.298	21/11/2014 13:15	.		
21/11/2014 13:30	0.037963152	21/11/2014	13:30:00	0.298	21/11/2014 13:30	.		
21/11/2014 13:45	0.034910928	21/11/2014	13:45:00	0.298	21/11/2014 13:45	.		
21/11/2014 14:00	0.035602008	21/11/2014	14:00:00	0.298	21/11/2014 14:00	.		
21/11/2014 14:15	0.033170525	21/11/2014	14:15:00	0.293	21/11/2014 14:15	.		
21/11/2014 14:30	0.034170867	21/11/2014	14:30:00	0.293	21/11/2014 14:30	.		
21/11/2014 14:45	0.035527399	21/11/2014	14:45:00	0.293	21/11/2014 14:45	.		
21/11/2014 15:00	0.036544798	21/11/2014	15:00:00	0.293	21/11/2014 15:00	.		
21/11/2014 15:15	0.035566839	21/11/2014	15:15:00	0.293	21/11/2014 15:15	.		
21/11/2014 15:30	0.03659383	21/11/2014	15:30:00	0.293	21/11/2014 15:30	.		
21/11/2014 15:45	0.034539847	21/11/2014	15:45:00	0.293	21/11/2014 15:45	.		
21/11/2014 16:00	0.035224508	21/11/2014	16:00:00	0.288	21/11/2014 16:00	.		
21/11/2014 16:15	0.03615562	21/11/2014	16:15:00	0.288	21/11/2014 16:15	.		
21/11/2014 16:30	0.034104751	21/11/2014	16:30:00	0.288	21/11/2014 16:30	.		
21/11/2014 16:45	0.033076513	21/11/2014	16:45:00	0.288	21/11/2014 16:45	.		
21/11/2014 17:00	0.036372651	21/11/2014	17:00:00	0.288	21/11/2014 17:00	0.2		
21/11/2014 17:15	0.038098047	21/11/2014	17:15:00	0.288	21/11/2014 17:15	0.6		
21/11/2014 17:30	0.038843202	21/11/2014	17:30:00	0.288	21/11/2014 17:30	.		
21/11/2014 17:45	0.036544798	21/11/2014	17:45:00	0.288	21/11/2014 17:45	0.2		
21/11/2014 18:00	0.04147619	21/11/2014	18:00:00	0.288	21/11/2014 18:00	.		
21/11/2014 18:15	0.040053819	21/11/2014	18:15:00	0.283	21/11/2014 18:15	.		
21/11/2014 18:30	0.04867287	21/11/2014	18:30:00	0.283	21/11/2014 18:30	.		
21/11/2014 18:45	0.049247798	21/11/2014	18:45:00	0.283	21/11/2014 18:45	.		
21/11/2014 19:00	0.051020836	21/11/2014	19:00:00	0.283	21/11/2014 19:00	.		
21/11/2014 19:15	0.048085771	21/11/2014	19:15:00	0.283	21/11/2014 19:15	.		
21/11/2014 19:30	0.045194278	21/11/2014	19:30:00	0.283	21/11/2014 19:30	.		
21/11/2014 19:45	0.046714505	21/11/2014	19:45:00	0.283	21/11/2014 19:45	.		
21/11/2014 20:00	0.043526359	21/11/2014	20:00:00	0.283	21/11/2014 20:00	0.2		
21/11/2014 20:15	0.049580878	21/11/2014	20:15:00	0.283	21/11/2014 20:15	.		
21/11/2014 20:30	0.040738432	21/11/2014	20:30:00	0.283	21/11/2014 20:30	.		
21/11/2014 20:45	0.036353029	21/11/2014	20:45:00	0.283	21/11/2014 20:45	.		

G5 Flow		Middleton Flow		Thorpeness TBR RG		
				Date & Time	Rainfall (mm)	Daily Rainfall (mm)
21/11/2014 21:00	0.041915691	21/11/2014 21:00:00	0.278	21/11/2014 21:00	.	
21/11/2014 21:15	0.040719278	21/11/2014 21:15:00	0.283	21/11/2014 21:15	.	
21/11/2014 21:30	0.039926885	21/11/2014 21:30:00	0.278	21/11/2014 21:30	.	
21/11/2014 21:45	0.04031524	21/11/2014 21:45:00	0.278	21/11/2014 21:45	.	
21/11/2014 22:00	0.038758365	21/11/2014 22:00:00	0.278	21/11/2014 22:00	.	
21/11/2014 22:15	0.038359335	21/11/2014 22:15:00	0.278	21/11/2014 22:15	.	
21/11/2014 22:30	0.034220812	21/11/2014 22:30:00	0.278	21/11/2014 22:30	.	
21/11/2014 22:45	0.041300244	21/11/2014 22:45:00	0.278	21/11/2014 22:45	.	
21/11/2014 23:00	0.036830759	21/11/2014 23:00:00	0.278	21/11/2014 23:00	.	
21/11/2014 23:15	0.040832125	21/11/2014 23:15:00	0.278	21/11/2014 23:15	.	
21/11/2014 23:30	0.038208785	21/11/2014 23:30:00	0.278	21/11/2014 23:30	.	
21/11/2014 23:45	0.031418651	21/11/2014 23:45:00	0.278	21/11/2014 23:45	.	
22/11/2014 00:00	0.033547423	22/11/2014 00:00:00	0.278	22/11/2014 00:00	.	
22/11/2014 00:15	0.03144773	22/11/2014 00:15:00	0.278	22/11/2014 00:15	.	
22/11/2014 00:30	0.033170525	22/11/2014 00:30:00	0.278	22/11/2014 00:30	.	
22/11/2014 00:45	0.031457803	22/11/2014 00:45:00	0.278	22/11/2014 00:45	.	
22/11/2014 01:00	0.0317883	22/11/2014 01:00:00	0.278	22/11/2014 01:00	.	
22/11/2014 01:15	0.032124248	22/11/2014 01:15:00	0.278	22/11/2014 01:15	.	
22/11/2014 01:30	0.029780376	22/11/2014 01:30:00	0.278	22/11/2014 01:30	.	
22/11/2014 01:45	0.028798337	22/11/2014 01:45:00	0.278	22/11/2014 01:45	.	
22/11/2014 02:00	0.029119157	22/11/2014 02:00:00	0.273	22/11/2014 02:00	.	
22/11/2014 02:15	0.02815865	22/11/2014 02:15:00	0.273	22/11/2014 02:15	.	
22/11/2014 02:30	0.030666448	22/11/2014 02:30:00	0.273	22/11/2014 02:30	.	
22/11/2014 02:45	0.028749212	22/11/2014 02:45:00	0.273	22/11/2014 02:45	.	
22/11/2014 03:00	0.026592965	22/11/2014 03:00:00	0.273	22/11/2014 03:00	.	
22/11/2014 03:15	0.025682201	22/11/2014 03:15:00	0.273	22/11/2014 03:15	.	
22/11/2014 03:30	0.028633388	22/11/2014 03:30:00	0.273	22/11/2014 03:30	.	
22/11/2014 03:45	0.02596053	22/11/2014 03:45:00	0.273	22/11/2014 03:45	.	
22/11/2014 04:00	0.022468748	22/11/2014 04:00:00	0.273	22/11/2014 04:00	.	
22/11/2014 04:15	0.022212565	22/11/2014 04:15:00	0.268	22/11/2014 04:15	.	
22/11/2014 04:30	0.024188207	22/11/2014 04:30:00	0.273	22/11/2014 04:30	.	
22/11/2014 04:45	0.021951756	22/11/2014 04:45:00	0.268	22/11/2014 04:45	.	
22/11/2014 05:00	0.025255247	22/11/2014 05:00:00	0.268	22/11/2014 05:00	.	
22/11/2014 05:15	0.023589926	22/11/2014 05:15:00	0.268	22/11/2014 05:15	.	
22/11/2014 05:30	0.023589926	22/11/2014 05:30:00	0.268	22/11/2014 05:30	.	
22/11/2014 05:45	0.024645836	22/11/2014 05:45:00	0.268	22/11/2014 05:45	.	
22/11/2014 06:00	0.021955679	22/11/2014 06:00:00	0.268	22/11/2014 06:00	.	
22/11/2014 06:15	0.022481263	22/11/2014 06:15:00	0.268	22/11/2014 06:15	.	
22/11/2014 06:30	0.020884548	22/11/2014 06:30:00	0.268	22/11/2014 06:30	.	
22/11/2014 06:45	0.025674694	22/11/2014 06:45:00	0.268	22/11/2014 06:45	.	
22/11/2014 07:00	0.022728157	22/11/2014 07:00:00	0.268	22/11/2014 07:00	.	
22/11/2014 07:15	0.025886986	22/11/2014 07:15:00	0.268	22/11/2014 07:15	.	
22/11/2014 07:30	0.020884548	22/11/2014 07:30:00	0.268	22/11/2014 07:30	0.2	
22/11/2014 07:45	0.022762726	22/11/2014 07:45:00	0.268	22/11/2014 07:45	.	
22/11/2014 08:00	0.024949551	22/11/2014 08:00:00	0.268	22/11/2014 08:00	.	
22/11/2014 08:15	0.027728871	22/11/2014 08:15:00	0.268	22/11/2014 08:15	.	
22/11/2014 08:30	0.030285223	22/11/2014 08:30:00	0.268	22/11/2014 08:30	.	
22/11/2014 08:45	0.029710009	22/11/2014 08:45:00	0.268	22/11/2014 08:45	.	
22/11/2014 09:00	0.03016184	22/11/2014 09:00:00	0.268	22/11/2014 09:00	.	1.4
22/11/2014 09:15	0.032864406	22/11/2014 09:15:00	0.268	22/11/2014 09:15	.	
22/11/2014 09:30	0.034674709	22/11/2014 09:30:00	0.268	22/11/2014 09:30	.	
22/11/2014 09:45	0.039936129	22/11/2014 09:45:00	0.268	22/11/2014 09:45	.	

	G5 Flow		Middleton Flow		Thorpeness TBR RG		
					Date & Time	Rainfall (mm)	Daily Rainfall (mm)
22/11/2014 10:00	0.040939331	22/11/2014 10:00:00	0.268		22/11/2014 10:00	.	
22/11/2014 10:15	0.038244974	22/11/2014 10:15:00	0.264		22/11/2014 10:15	.	
22/11/2014 10:30	0.037567448	22/11/2014 10:30:00	0.264		22/11/2014 10:30	.	
22/11/2014 10:45	0.040185294	22/11/2014 10:45:00	0.264		22/11/2014 10:45	.	
22/11/2014 11:00	0.040629115	22/11/2014 11:00:00	0.264		22/11/2014 11:00	.	
22/11/2014 11:15	0.044412082	22/11/2014 11:15:00	0.264		22/11/2014 11:15	.	
22/11/2014 11:30	0.045925269	22/11/2014 11:30:00	0.264		22/11/2014 11:30	.	
22/11/2014 11:45	0.037595519	22/11/2014 11:45:00	0.264		22/11/2014 11:45	.	
22/11/2014 12:00	0.043220031	22/11/2014 12:00:00	0.264		22/11/2014 12:00	0.2	
22/11/2014 12:15	0.041720161	22/11/2014 12:15:00	0.264		22/11/2014 12:15	0.4	
22/11/2014 12:30	0.045388394	22/11/2014 12:30:00	0.264		22/11/2014 12:30	0.4	
22/11/2014 12:45	0.037212093	22/11/2014 12:45:00	0.264		22/11/2014 12:45	0.2	
22/11/2014 13:00	0.044412082	22/11/2014 13:00:00	0.268		22/11/2014 13:00	0.2	
22/11/2014 13:15	0.054730921	22/11/2014 13:15:00	0.268		22/11/2014 13:15	.	
22/11/2014 13:30	0.067446297	22/11/2014 13:30:00	0.268		22/11/2014 13:30	.	
22/11/2014 13:45	0.080505672	22/11/2014 13:45:00	0.268		22/11/2014 13:45	.	
22/11/2014 14:00	0.073772272	22/11/2014 14:00:00	0.268		22/11/2014 14:00	.	
22/11/2014 14:15	0.073890101	22/11/2014 14:15:00	0.268		22/11/2014 14:15	.	
22/11/2014 14:30	0.07227738	22/11/2014 14:30:00	0.268		22/11/2014 14:30	.	
22/11/2014 14:45	0.066796109	22/11/2014 14:45:00	0.268		22/11/2014 14:45	.	
22/11/2014 15:00	0.070187519	22/11/2014 15:00:00	0.268		22/11/2014 15:00	.	
22/11/2014 15:15	0.061250077	22/11/2014 15:15:00	0.268		22/11/2014 15:15	.	
22/11/2014 15:30	0.0698684	22/11/2014 15:30:00	0.268		22/11/2014 15:30	.	
22/11/2014 15:45	0.059110478	22/11/2014 15:45:00	0.268		22/11/2014 15:45	.	
22/11/2014 16:00	0.052926154	22/11/2014 16:00:00	0.268		22/11/2014 16:00	.	
22/11/2014 16:15	0.050533459	22/11/2014 16:15:00	0.268		22/11/2014 16:15	.	
22/11/2014 16:30	0.043606679	22/11/2014 16:30:00	0.268		22/11/2014 16:30	.	
22/11/2014 16:45	0.041545193	22/11/2014 16:45:00	0.268		22/11/2014 16:45	.	
22/11/2014 17:00	0.043526359	22/11/2014 17:00:00	0.268		22/11/2014 17:00	.	
22/11/2014 17:15	0.044244858	22/11/2014 17:15:00	0.268		22/11/2014 17:15	.	
22/11/2014 17:30	0.04299326	22/11/2014 17:30:00	0.268		22/11/2014 17:30	.	
22/11/2014 17:45	0.041421755	22/11/2014 17:45:00	0.268		22/11/2014 17:45	0.4	
22/11/2014 18:00	0.043329943	22/11/2014 18:00:00	0.268		22/11/2014 18:00	.	
22/11/2014 18:15	0.039895204	22/11/2014 18:15:00	0.268		22/11/2014 18:15	.	
22/11/2014 18:30	0.044474856	22/11/2014 18:30:00	0.268		22/11/2014 18:30	.	
22/11/2014 18:45	0.047527957	22/11/2014 18:45:00	0.268		22/11/2014 18:45	.	
22/11/2014 19:00	0.04299326	22/11/2014 19:00:00	0.268		22/11/2014 19:00	.	
22/11/2014 19:15	0.045420051	22/11/2014 19:15:00	0.268		22/11/2014 19:15	.	
22/11/2014 19:30	0.046315987	22/11/2014 19:30:00	0.268		22/11/2014 19:30	.	
22/11/2014 19:45	0.047511542	22/11/2014 19:45:00	0.268		22/11/2014 19:45	.	
22/11/2014 20:00	0.046365443	22/11/2014 20:00:00	0.268		22/11/2014 20:00	.	
22/11/2014 20:15	0.048707097	22/11/2014 20:15:00	0.268		22/11/2014 20:15	.	
22/11/2014 20:30	0.049337361	22/11/2014 20:30:00	0.268		22/11/2014 20:30	.	
22/11/2014 20:45	0.047998135	22/11/2014 20:45:00	0.268		22/11/2014 20:45	.	
22/11/2014 21:00	0.040629115	22/11/2014 21:00:00	0.268		22/11/2014 21:00	.	
22/11/2014 21:15	0.043158494	22/11/2014 21:15:00	0.268		22/11/2014 21:15	.	
22/11/2014 21:30	0.042724271	22/11/2014 21:30:00	0.268		22/11/2014 21:30	.	
22/11/2014 21:45	0.039371921	22/11/2014 21:45:00	0.268		22/11/2014 21:45	.	
22/11/2014 22:00	0.041500895	22/11/2014 22:00:00	0.268		22/11/2014 22:00	.	
22/11/2014 22:15	0.040415588	22/11/2014 22:15:00	0.268		22/11/2014 22:15	.	
22/11/2014 22:30	0.036774788	22/11/2014 22:30:00	0.268		22/11/2014 22:30	.	
22/11/2014 22:45	0.032484375	22/11/2014 22:45:00	0.268		22/11/2014 22:45	.	

	G5 Flow			Middleton Flow		Thorpeness TBR RG		
					Date & Time	Rainfall (mm)	Daily Rainfall (mm)	
22/11/2014 23:00	0.038475362	22/11/2014	23:00:00	0.268	22/11/2014 23:00	.		
22/11/2014 23:15	0.036984168	22/11/2014	23:15:00	0.268	22/11/2014 23:15	.		
22/11/2014 23:30	0.036638628	22/11/2014	23:30:00	0.268	22/11/2014 23:30	.		
22/11/2014 23:45	0.038366329	22/11/2014	23:45:00	0.268	22/11/2014 23:45	.		
23/11/2014 00:00	0.03659383	23/11/2014	00:00:00	0.268	23/11/2014 00:00	.		
23/11/2014 00:15	0.035147777	23/11/2014	00:15:00	0.268	23/11/2014 00:15	.		
23/11/2014 00:30	0.036827516	23/11/2014	00:30:00	0.268	23/11/2014 00:30	.		
23/11/2014 00:45	0.037835359	23/11/2014	00:45:00	0.268	23/11/2014 00:45	.		
23/11/2014 01:00	0.038430821	23/11/2014	01:00:00	0.268	23/11/2014 01:00	.		
23/11/2014 01:15	0.035713423	23/11/2014	01:15:00	0.268	23/11/2014 01:15	.		
23/11/2014 01:30	0.029450762	23/11/2014	01:30:00	0.268	23/11/2014 01:30	.		
23/11/2014 01:45	0.033406127	23/11/2014	01:45:00	0.273	23/11/2014 01:45	.		
23/11/2014 02:00	0.036043037	23/11/2014	02:00:00	0.273	23/11/2014 02:00	.		
23/11/2014 02:15	0.035327639	23/11/2014	02:15:00	0.273	23/11/2014 02:15	.		
23/11/2014 02:30	0.033004072	23/11/2014	02:30:00	0.273	23/11/2014 02:30	.		
23/11/2014 02:45	0.03328182	23/11/2014	02:45:00	0.273	23/11/2014 02:45	.		
23/11/2014 03:00	0.032915048	23/11/2014	03:00:00	0.273	23/11/2014 03:00	.		
23/11/2014 03:15	0.030352454	23/11/2014	03:15:00	0.273	23/11/2014 03:15	.		
23/11/2014 03:30	0.03218791	23/11/2014	03:30:00	0.273	23/11/2014 03:30	.		
23/11/2014 03:45	0.036445034	23/11/2014	03:45:00	0.273	23/11/2014 03:45	.		
23/11/2014 04:00	0.028726363	23/11/2014	04:00:00	0.278	23/11/2014 04:00	.		
23/11/2014 04:15	0.0289671	23/11/2014	04:15:00	0.278	23/11/2014 04:15	.		
23/11/2014 04:30	0.02567678	23/11/2014	04:30:00	0.278	23/11/2014 04:30	.		
23/11/2014 04:45	0.025375231	23/11/2014	04:45:00	0.278	23/11/2014 04:45	.		
23/11/2014 05:00	0.024204561	23/11/2014	05:00:00	0.278	23/11/2014 05:00	0.2		
23/11/2014 05:15	0.024198401	23/11/2014	05:15:00	0.278	23/11/2014 05:15	.		
23/11/2014 05:30	0.021118409	23/11/2014	05:30:00	0.278	23/11/2014 05:30	.		
23/11/2014 05:45	0.025804941	23/11/2014	05:45:00	0.278	23/11/2014 05:45	.		
23/11/2014 06:00	0.022230302	23/11/2014	06:00:00	0.278	23/11/2014 06:00	.		
23/11/2014 06:15	0.020870677	23/11/2014	06:15:00	0.278	23/11/2014 06:15	.		
23/11/2014 06:30	0.02437682	23/11/2014	06:30:00	0.278	23/11/2014 06:30	.		
23/11/2014 06:45	0.023569773	23/11/2014	06:45:00	0.283	23/11/2014 06:45	.		
23/11/2014 07:00	0.024645836	23/11/2014	07:00:00	0.283	23/11/2014 07:00	0.2		
23/11/2014 07:15	0.025183867	23/11/2014	07:15:00	0.283	23/11/2014 07:15	.		
23/11/2014 07:30	0.029028425	23/11/2014	07:30:00	0.283	23/11/2014 07:30	.		
23/11/2014 07:45	0.027454024	23/11/2014	07:45:00	0.288	23/11/2014 07:45	0.2		
23/11/2014 08:00	0.028399159	23/11/2014	08:00:00	0.288	23/11/2014 08:00	0.2		
23/11/2014 08:15	0.029179672	23/11/2014	08:15:00	0.288	23/11/2014 08:15	.		
23/11/2014 08:30	0.040646531	23/11/2014	08:30:00	0.288	23/11/2014 08:30	0.2		
23/11/2014 08:45	0.047171267	23/11/2014	08:45:00	0.293	23/11/2014 08:45	0.2		
23/11/2014 09:00	0.065256123	23/11/2014	09:00:00	0.293	23/11/2014 09:00	.		3
23/11/2014 09:15	0.073013271	23/11/2014	09:15:00	0.293	23/11/2014 09:15	0.2		
23/11/2014 09:30	0.065516789	23/11/2014	09:30:00	0.298	23/11/2014 09:30	0.4		
23/11/2014 09:45	0.076267307	23/11/2014	09:45:00	0.304	23/11/2014 09:45	.		
23/11/2014 10:00	0.085592476	23/11/2014	10:00:00	0.304	23/11/2014 10:00	.		
23/11/2014 10:15	0.080436608	23/11/2014	10:15:00	0.304	23/11/2014 10:15	.		
23/11/2014 10:30	0.101346066	23/11/2014	10:30:00	0.309	23/11/2014 10:30	0.2		
23/11/2014 10:45	0.081690656	23/11/2014	10:45:00	0.309	23/11/2014 10:45	.		
23/11/2014 11:00	0.08742823	23/11/2014	11:00:00	0.314	23/11/2014 11:00	.		
23/11/2014 11:15	0.082641019	23/11/2014	11:15:00	0.319	23/11/2014 11:15	.		
23/11/2014 11:30	0.081285943	23/11/2014	11:30:00	0.325	23/11/2014 11:30	.		
23/11/2014 11:45	0.085679979	23/11/2014	11:45:00	0 33	23/11/2014 11:45	0.8		

	G5 Flow			Middleton Flow		Thorpeness TBR RG		
						Date & Time	Rainfall (mm)	Daily Rainfall (mm)
23/11/2014	12:00	0.08064775	23/11/2014	12:00:00	0.335	23/11/2014 12:00	0.2	
23/11/2014	12:15	0.083898891	23/11/2014	12:15:00	0.346	23/11/2014 12:15	0.2	
23/11/2014	12:30	0.097635483	23/11/2014	12:30:00	0.351	23/11/2014 12:30	0.4	
23/11/2014	12:45	0.109510644	23/11/2014	12:45:00	0.362	23/11/2014 12:45	0.8	
23/11/2014	13:00	0.133444925	23/11/2014	13:00:00	0.379	23/11/2014 13:00	0.8	
23/11/2014	13:15	0.193552739	23/11/2014	13:15:00	0.396	23/11/2014 13:15	0.8	
23/11/2014	13:30	0.227078354	23/11/2014	13:30:00	0.425	23/11/2014 13:30	0.4	
23/11/2014	13:45	0.218741341	23/11/2014	13:45:00	0.455	23/11/2014 13:45	0.8	
23/11/2014	14:00	0.193118729	23/11/2014	14:00:00	0.505	23/11/2014 14:00	1	
23/11/2014	14:15	0.215761345	23/11/2014	14:15:00	0 57	23/11/2014 14:15	1.2	
23/11/2014	14:30	0.26530888	23/11/2014	14:30:00	0.645	23/11/2014 14:30	1	
23/11/2014	14:45	0.359327479	23/11/2014	14:45:00	0.739	23/11/2014 14:45	1	
23/11/2014	15:00	0.527947895	23/11/2014	15:00:00	0.853	23/11/2014 15:00	0.4	
23/11/2014	15:15	0.530437705	23/11/2014	15:15:00	0.982	23/11/2014 15:15	0.6	
23/11/2014	15:30	0.510112555	23/11/2014	15:30:00	1.13	23/11/2014 15:30	0.6	
23/11/2014	15:45	0.512984312	23/11/2014	15:45:00	---	23/11/2014 15:45	0.2	
23/11/2014	16:00	0.509358951	23/11/2014	16:00:00	---	23/11/2014 16:00	0.4	
23/11/2014	16:15	0.527149374	23/11/2014	16:15:00	---	23/11/2014 16:15	0.6	
23/11/2014	16:30	0.518544056	23/11/2014	16:30:00	---	23/11/2014 16:30	0.2	
23/11/2014	16:45	0.623937737	23/11/2014	16:45:00	---	23/11/2014 16:45	0.4	
23/11/2014	17:00	0.625898957	23/11/2014	17:00:00	---	23/11/2014 17:00	0.6	
23/11/2014	17:15	0.606698514	23/11/2014	17:15:00	---	23/11/2014 17:15	0.6	
23/11/2014	17:30	0.706827804	23/11/2014	17:30:00	---	23/11/2014 17:30	0.2	
23/11/2014	17:45	0.735243088	23/11/2014	17:45:00	---	23/11/2014 17:45	0.6	
23/11/2014	18:00	0.704255409	23/11/2014	18:00:00	---	23/11/2014 18:00	0.4	
23/11/2014	18:15	0.795293038	23/11/2014	18:15:00	---	23/11/2014 18:15	0.6	
23/11/2014	18:30	0.841643428	23/11/2014	18:30:00	---	23/11/2014 18:30	0.6	
23/11/2014	18:45	0.818550432	23/11/2014	18:45:00	---	23/11/2014 18:45	0.2	
23/11/2014	19:00	0.848632832	23/11/2014	19:00:00	---	23/11/2014 19:00	0.4	
23/11/2014	19:15	0.971054863	23/11/2014	19:15:00	---	23/11/2014 19:15	0.6	
23/11/2014	19:30	0.913067633	23/11/2014	19:30:00	---	23/11/2014 19:30	0.4	
23/11/2014	19:45	0.959455141	23/11/2014	19:45:00	---	23/11/2014 19:45	0.4	
23/11/2014	20:00	0.979133819	23/11/2014	20:00:00	---	23/11/2014 20:00	0.2	
23/11/2014	20:15	1.063237066	23/11/2014	20:15:00	---	23/11/2014 20:15	0.2	
23/11/2014	20:30	1.125416748	23/11/2014	20:30:00	---	23/11/2014 20:30	.	
23/11/2014	20:45	1.060657971	23/11/2014	20:45:00	---	23/11/2014 20:45	0.2	
23/11/2014	21:00	1.022114632	23/11/2014	21:00:00	---	23/11/2014 21:00	.	
23/11/2014	21:15	0.952227965	23/11/2014	21:15:00	---	23/11/2014 21:15	.	
23/11/2014	21:30	0.918809253	23/11/2014	21:30:00	---	23/11/2014 21:30	.	
23/11/2014	21:45	0.954354994	23/11/2014	21:45:00	---	23/11/2014 21:45	.	
23/11/2014	22:00	0.935805431	23/11/2014	22:00:00	---	23/11/2014 22:00	.	
23/11/2014	22:15	0.997195371	23/11/2014	22:15:00	---	23/11/2014 22:15	.	
23/11/2014	22:30	0.888627561	23/11/2014	22:30:00	---	23/11/2014 22:30	.	
23/11/2014	22:45	0.851738853	23/11/2014	22:45:00	---	23/11/2014 22:45	.	
23/11/2014	23:00	0.853207211	23/11/2014	23:00:00	---	23/11/2014 23:00	.	
23/11/2014	23:15	0.829241239	23/11/2014	23:15:00	---	23/11/2014 23:15	.	
23/11/2014	23:30	0.800448105	23/11/2014	23:30:00	---	23/11/2014 23:30	.	
23/11/2014	23:45	0.825830846	23/11/2014	23:45:00	---	23/11/2014 23:45	.	
24/11/2014	00:00	0.824712738	24/11/2014	00:00:00	---	24/11/2014 00:00	.	
24/11/2014	00:15	0.758492643	24/11/2014	00:15:00	---	24/11/2014 00:15	.	
24/11/2014	00:30	0.777968042	24/11/2014	00:30:00	---	24/11/2014 00:30	.	
24/11/2014	00:45	0.732200041	24/11/2014	00:45:00	---	24/11/2014 00:45	.	

					Thorpeness TBR RG		
G5 Flow			Middleton Flow		Date & Time	Rainfall (mm)	Daily Rainfall (mm)
24/11/2014 01:00	0.748165692	24/11/2014	01:00:00	---	24/11/2014 01:00	.	
24/11/2014 01:15	0.727597646	24/11/2014	01:15:00	---	24/11/2014 01:15	.	
24/11/2014 01:30	0.659187405	24/11/2014	01:30:00	---	24/11/2014 01:30	.	
24/11/2014 01:45	0.656763475	24/11/2014	01:45:00	---	24/11/2014 01:45	.	
24/11/2014 02:00	0.656006987	24/11/2014	02:00:00	---	24/11/2014 02:00	.	
24/11/2014 02:15	0.697188068	24/11/2014	02:15:00	---	24/11/2014 02:15	.	
24/11/2014 02:30	0.606698514	24/11/2014	02:30:00	---	24/11/2014 02:30	.	
24/11/2014 02:45	0.634165182	24/11/2014	02:45:00	---	24/11/2014 02:45	.	
24/11/2014 03:00	0.603733616	24/11/2014	03:00:00	---	24/11/2014 03:00	.	
24/11/2014 03:15	0.607334643	24/11/2014	03:15:00	---	24/11/2014 03:15	.	
24/11/2014 03:30	0.581907899	24/11/2014	03:30:00	---	24/11/2014 03:30	.	
24/11/2014 03:45	0.564642792	24/11/2014	03:45:00	---	24/11/2014 03:45	.	
24/11/2014 04:00	0.535546398	24/11/2014	04:00:00	---	24/11/2014 04:00	.	
24/11/2014 04:15	0.554387871	24/11/2014	04:15:00	---	24/11/2014 04:15	.	
24/11/2014 04:30	0.498896506	24/11/2014	04:30:00	---	24/11/2014 04:30	.	
24/11/2014 04:45	0.500159171	24/11/2014	04:45:00	---	24/11/2014 04:45	.	
24/11/2014 05:00	0.505000122	24/11/2014	05:00:00	---	24/11/2014 05:00	.	
24/11/2014 05:15	0.499271579	24/11/2014	05:15:00	---	24/11/2014 05:15	0.2	
24/11/2014 05:30	0.502332095	24/11/2014	05:30:00	---	24/11/2014 05:30	.	
24/11/2014 05:45	0.463252317	24/11/2014	05:45:00	---	24/11/2014 05:45	.	
24/11/2014 06:00	0.456162106	24/11/2014	06:00:00	---	24/11/2014 06:00	.	
24/11/2014 06:15	0.425208805	24/11/2014	06:15:00	---	24/11/2014 06:15	.	
24/11/2014 06:30	0.375184147	24/11/2014	06:30:00	---	24/11/2014 06:30	.	
24/11/2014 06:45	0.399939622	24/11/2014	06:45:00	---	24/11/2014 06:45	.	
24/11/2014 07:00	0.378495552	24/11/2014	07:00:00	---	24/11/2014 07:00	.	
24/11/2014 07:15	0.38104199	24/11/2014	07:15:00	---	24/11/2014 07:15	.	
24/11/2014 07:30	0.351293244	24/11/2014	07:30:00	---	24/11/2014 07:30	.	
24/11/2014 07:45	0.318535583	24/11/2014	07:45:00	---	24/11/2014 07:45	.	
24/11/2014 08:00	0.343814278	24/11/2014	08:00:00	---	24/11/2014 08:00	.	
24/11/2014 08:15	0.337414428	24/11/2014	08:15:00	---	24/11/2014 08:15	.	
24/11/2014 08:30	0.315719449	24/11/2014	08:30:00	---	24/11/2014 08:30	.	
24/11/2014 08:45	0.322748287	24/11/2014	08:45:00	---	24/11/2014 08:45	.	
24/11/2014 09:00	0.335437992	24/11/2014	09:00:00	---	24/11/2014 09:00	.	20
24/11/2014 09:15	0.324102334	24/11/2014	09:15:00	---	24/11/2014 09:15	.	
24/11/2014 09:30	0.297603372	24/11/2014	09:30:00	---	24/11/2014 09:30	.	
24/11/2014 09:45	0.264098248	24/11/2014	09:45:00	---	24/11/2014 09:45	.	
24/11/2014 10:00	0.293980123	24/11/2014	10:00:00	---	24/11/2014 10:00	.	
24/11/2014 10:15	0.294936299	24/11/2014	10:15:00	---	24/11/2014 10:15	.	
24/11/2014 10:30	0.237028042	24/11/2014	10:30:00	---	24/11/2014 10:30	.	
24/11/2014 10:45	0.238672521	24/11/2014	10:45:00	---	24/11/2014 10:45	.	
24/11/2014 11:00	0.264732374	24/11/2014	11:00:00	---	24/11/2014 11:00	.	
24/11/2014 11:15	0.245187677	24/11/2014	11:15:00	---	24/11/2014 11:15	.	
24/11/2014 11:30	0.225970127	24/11/2014	11:30:00	---	24/11/2014 11:30	.	
24/11/2014 11:45	0.216727203	24/11/2014	11:45:00	---	24/11/2014 11:45	.	
24/11/2014 12:00	0.217736384	24/11/2014	12:00:00	---	24/11/2014 12:00	.	
24/11/2014 12:15	0.21250684	24/11/2014	12:15:00	---	24/11/2014 12:15	.	
24/11/2014 12:30	0.202391165	24/11/2014	12:30:00	---	24/11/2014 12:30	.	
24/11/2014 12:45	0.217849652	24/11/2014	12:45:00	---	24/11/2014 12:45	.	
24/11/2014 13:00	0.194621022	24/11/2014	13:00:00	---	24/11/2014 13:00	.	
24/11/2014 13:15	0.193024263	24/11/2014	13:15:00	---	24/11/2014 13:15	.	
24/11/2014 13:30	0.149143532	24/11/2014	13:30:00	---	24/11/2014 13:30	.	
24/11/2014 13:45	0.168452617	24/11/2014	13:45:00	---	24/11/2014 13:45	.	

	G5 Flow		Middleton Flow	Thorpeness TBR RG		
				Date & Time	Rainfall (mm)	Daily Rainfall (mm)
24/11/2014 14:00	0.14607564	24/11/2014 14:00:00	---	24/11/2014 14:00	.	
24/11/2014 14:15	0.170958426	24/11/2014 14:15:00	---	24/11/2014 14:15	.	
24/11/2014 14:30	0.151220616	24/11/2014 14:30:00	---	24/11/2014 14:30	.	
24/11/2014 14:45	0.167883958	24/11/2014 14:45:00	---	24/11/2014 14:45	.	
24/11/2014 15:00	0.154758354	24/11/2014 15:00:00	---	24/11/2014 15:00	.	
24/11/2014 15:15	0.158449978	24/11/2014 15:15:00	---	24/11/2014 15:15	.	
24/11/2014 15:30	0.136721613	24/11/2014 15:30:00	---	24/11/2014 15:30	.	
24/11/2014 15:45	0.138321811	24/11/2014 15:45:00	---	24/11/2014 15:45	.	
24/11/2014 16:00	0.147631794	24/11/2014 16:00:00	---	24/11/2014 16:00	.	
24/11/2014 16:15	0.155661185	24/11/2014 16:15:00	---	24/11/2014 16:15	.	
24/11/2014 16:30	0.11131519	24/11/2014 16:30:00	---	24/11/2014 16:30	.	
24/11/2014 16:45	0.114644523	24/11/2014 16:45:00	---	24/11/2014 16:45	.	
24/11/2014 17:00	0.143032784	24/11/2014 17:00:00	---	24/11/2014 17:00	.	
24/11/2014 17:15	0.117940522	24/11/2014 17:15:00	---	24/11/2014 17:15	.	
24/11/2014 17:30	0.136200369	24/11/2014 17:30:00	---	24/11/2014 17:30	.	
24/11/2014 17:45	0.123156977	24/11/2014 17:45:00	---	24/11/2014 17:45	.	
24/11/2014 18:00	0.117275621	24/11/2014 18:00:00	---	24/11/2014 18:00	.	
24/11/2014 18:15	0.114086375	24/11/2014 18:15:00	---	24/11/2014 18:15	.	
24/11/2014 18:30	0.129745821	24/11/2014 18:30:00	---	24/11/2014 18:30	.	
24/11/2014 18:45	0.101080053	24/11/2014 18:45:00	---	24/11/2014 18:45	.	
24/11/2014 19:00	0.119925308	24/11/2014 19:00:00	---	24/11/2014 19:00	.	
24/11/2014 19:15	0.10770663	24/11/2014 19:15:00	---	24/11/2014 19:15	.	
24/11/2014 19:30	0.113558753	24/11/2014 19:30:00	---	24/11/2014 19:30	.	
24/11/2014 19:45	0.104812438	24/11/2014 19:45:00	---	24/11/2014 19:45	.	
24/11/2014 20:00	0.118659648	24/11/2014 20:00:00	---	24/11/2014 20:00	.	
24/11/2014 20:15	0.113963745	24/11/2014 20:15:00	---	24/11/2014 20:15	.	
24/11/2014 20:30	0.108495637	24/11/2014 20:30:00	---	24/11/2014 20:30	.	
24/11/2014 20:45	0.107070715	24/11/2014 20:45:00	---	24/11/2014 20:45	.	
24/11/2014 21:00	0.095645004	24/11/2014 21:00:00	---	24/11/2014 21:00	.	
24/11/2014 21:15	0.097294754	24/11/2014 21:15:00	---	24/11/2014 21:15	.	
24/11/2014 21:30	0.112634029	24/11/2014 21:30:00	---	24/11/2014 21:30	.	
24/11/2014 21:45	0.105864222	24/11/2014 21:45:00	---	24/11/2014 21:45	.	
24/11/2014 22:00	0.10440422	24/11/2014 22:00:00	---	24/11/2014 22:00	.	
24/11/2014 22:15	0.097079605	24/11/2014 22:15:00	---	24/11/2014 22:15	.	
24/11/2014 22:30	0.11110256	24/11/2014 22:30:00	---	24/11/2014 22:30	.	
24/11/2014 22:45	0.110351617	24/11/2014 22:45:00	---	24/11/2014 22:45	.	
24/11/2014 23:00	0.098802503	24/11/2014 23:00:00	---	24/11/2014 23:00	.	
24/11/2014 23:15	0.096727956	24/11/2014 23:15:00	---	24/11/2014 23:15	.	
24/11/2014 23:30	0.090409777	24/11/2014 23:30:00	---	24/11/2014 23:30	.	
24/11/2014 23:45	0.098893576	24/11/2014 23:45:00	---	24/11/2014 23:45	.	
25/11/2014 00:00	0.093379418	25/11/2014 00:00:00	---	25/11/2014 00:00	.	
25/11/2014 00:15	0.102298373	25/11/2014 00:15:00	---	25/11/2014 00:15	.	
25/11/2014 00:30	0.097483528	25/11/2014 00:30:00	---	25/11/2014 00:30	.	
25/11/2014 00:45	0.092087819	25/11/2014 00:45:00	---	25/11/2014 00:45	.	
25/11/2014 01:00	0.088777394	25/11/2014 01:00:00	---	25/11/2014 01:00	.	
25/11/2014 01:15	0.089458031	25/11/2014 01:15:00	---	25/11/2014 01:15	.	
25/11/2014 01:30	0.097923009	25/11/2014 01:30:00	---	25/11/2014 01:30	.	
25/11/2014 01:45	0.076580984	25/11/2014 01:45:00	---	25/11/2014 01:45	.	
25/11/2014 02:00	0.07983967	25/11/2014 02:00:00	---	25/11/2014 02:00	.	
25/11/2014 02:15	0.090034314	25/11/2014 02:15:00	---	25/11/2014 02:15	.	
25/11/2014 02:30	0.078017818	25/11/2014 02:30:00	---	25/11/2014 02:30	.	
25/11/2014 02:45	0.076176492	25/11/2014 02:45:00	---	25/11/2014 02:45	.	

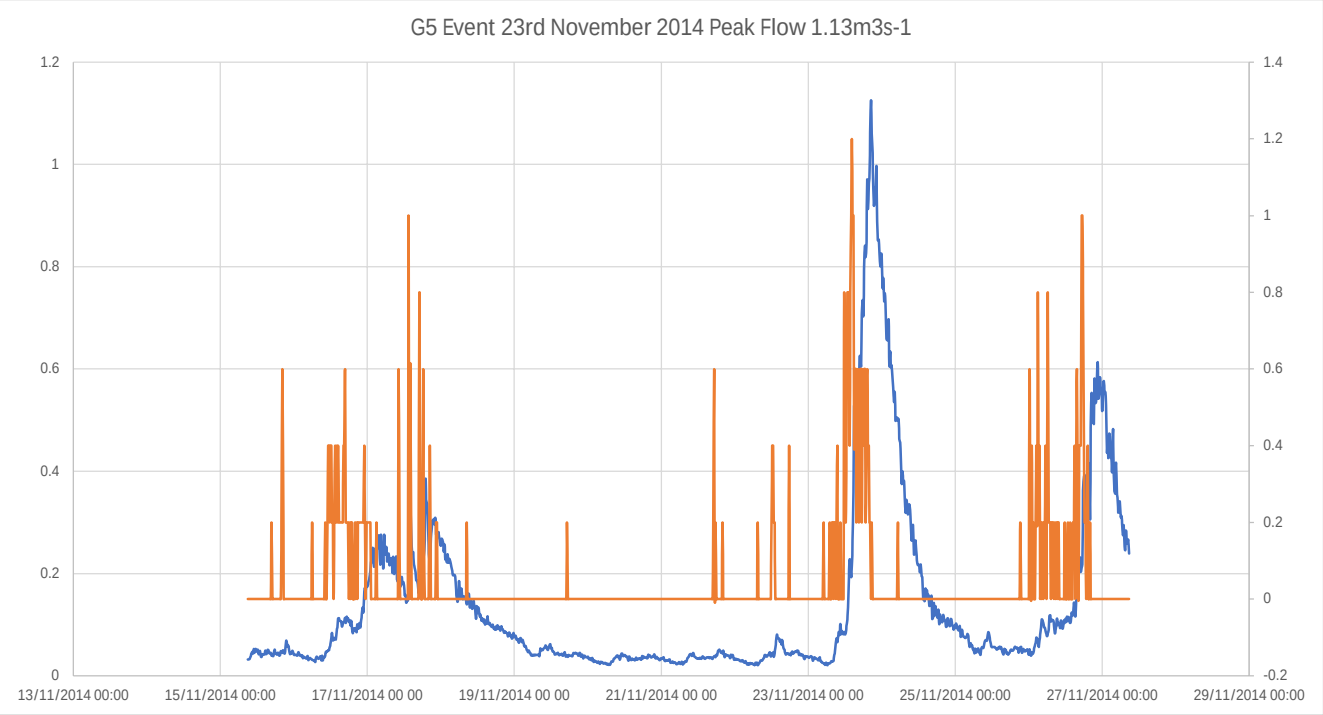
					Thorpeness TBR RG		
G5 Flow			Middleton Flow		Date & Time	Rainfall (mm)	Daily Rainfall (mm)
25/11/2014 03:00	0.076176492	25/11/2014	03:00:00	---	25/11/2014 03:00	.	
25/11/2014 03:15	0.073731085	25/11/2014	03:15:00	---	25/11/2014 03:15	.	
25/11/2014 03:30	0.075679657	25/11/2014	03:30:00	---	25/11/2014 03:30	.	
25/11/2014 03:45	0.076321925	25/11/2014	03:45:00	---	25/11/2014 03:45	.	
25/11/2014 04:00	0.081816506	25/11/2014	04:00:00	---	25/11/2014 04:00	.	
25/11/2014 04:15	0.077556957	25/11/2014	04:15:00	---	25/11/2014 04:15	.	
25/11/2014 04:30	0.063203991	25/11/2014	04:30:00	---	25/11/2014 04:30	.	
25/11/2014 04:45	0.056086863	25/11/2014	04:45:00	---	25/11/2014 04:45	.	
25/11/2014 05:00	0.063909678	25/11/2014	05:00:00	---	25/11/2014 05:00	.	
25/11/2014 05:15	0.059183747	25/11/2014	05:15:00	1 27	25/11/2014 05:15	.	
25/11/2014 05:30	0.059302583	25/11/2014	05:30:00	1 25	25/11/2014 05:30	.	
25/11/2014 05:45	0.051749871	25/11/2014	05:45:00	1 23	25/11/2014 05:45	.	
25/11/2014 06:00	0.052382461	25/11/2014	06:00:00	1 21	25/11/2014 06:00	.	
25/11/2014 06:15	0.043671202	25/11/2014	06:15:00	1.18	25/11/2014 06:15	.	
25/11/2014 06:30	0.052957922	25/11/2014	06:30:00	1.16	25/11/2014 06:30	.	
25/11/2014 06:45	0.045406892	25/11/2014	06:45:00	1.14	25/11/2014 06:45	.	
25/11/2014 07:00	0.047337856	25/11/2014	07:00:00	1.14	25/11/2014 07:00	.	
25/11/2014 07:15	0.051095714	25/11/2014	07:15:00	1.12	25/11/2014 07:15	.	
25/11/2014 07:30	0.053384211	25/11/2014	07:30:00	1.1	25/11/2014 07:30	.	
25/11/2014 07:45	0.046086427	25/11/2014	07:45:00	1 08	25/11/2014 07:45	.	
25/11/2014 08:00	0.044723031	25/11/2014	08:00:00	1 08	25/11/2014 08:00	.	
25/11/2014 08:15	0.041016654	25/11/2014	08:15:00	1 07	25/11/2014 08:15	.	
25/11/2014 08:30	0.052482307	25/11/2014	08:30:00	1 05	25/11/2014 08:30	.	
25/11/2014 08:45	0.056246975	25/11/2014	08:45:00	1 04	25/11/2014 08:45	.	
25/11/2014 09:00	0.054385103	25/11/2014	09:00:00	1 02	25/11/2014 09:00	.	
25/11/2014 09:15	0.054389435	25/11/2014	09:15:00	1 02	25/11/2014 09:15	.	
25/11/2014 09:30	0.063921161	25/11/2014	09:30:00	0.999	25/11/2014 09:30	.	
25/11/2014 09:45	0.068236419	25/11/2014	09:45:00	0 99	25/11/2014 09:45	.	
25/11/2014 10:00	0.070017493	25/11/2014	10:00:00	0.982	25/11/2014 10:00	.	
25/11/2014 10:15	0.068298956	25/11/2014	10:15:00	0.974	25/11/2014 10:15	.	
25/11/2014 10:30	0.07402762	25/11/2014	10:30:00	0.957	25/11/2014 10:30	.	
25/11/2014 10:45	0.085233951	25/11/2014	10:45:00	0.949	25/11/2014 10:45	.	
25/11/2014 11:00	0.083349784	25/11/2014	11:00:00	0.941	25/11/2014 11:00	.	
25/11/2014 11:15	0.073989677	25/11/2014	11:15:00	0.933	25/11/2014 11:15	.	
25/11/2014 11:30	0.065607817	25/11/2014	11:30:00	0.925	25/11/2014 11:30	.	
25/11/2014 11:45	0.058197179	25/11/2014	11:45:00	0.909	25/11/2014 11:45	.	
25/11/2014 12:00	0.055737136	25/11/2014	12:00:00	0.901	25/11/2014 12:00	.	
25/11/2014 12:15	0.056301661	25/11/2014	12:15:00	0.893	25/11/2014 12:15	.	
25/11/2014 12:30	0.056331863	25/11/2014	12:30:00	0.885	25/11/2014 12:30	.	
25/11/2014 12:45	0.056301661	25/11/2014	12:45:00	0.877	25/11/2014 12:45	.	
25/11/2014 13:00	0.055795907	25/11/2014	13:00:00	0.869	25/11/2014 13:00	.	
25/11/2014 13:15	0.053840376	25/11/2014	13:15:00	0.861	25/11/2014 13:15	.	
25/11/2014 13:30	0.051432411	25/11/2014	13:30:00	0.853	25/11/2014 13:30	.	
25/11/2014 13:45	0.051978443	25/11/2014	13:45:00	0.845	25/11/2014 13:45	.	
25/11/2014 14:00	0.055357138	25/11/2014	14:00:00	0.837	25/11/2014 14:00	.	
25/11/2014 14:15	0.053912566	25/11/2014	14:15:00	0 83	25/11/2014 14:15	.	
25/11/2014 14:30	0.057184777	25/11/2014	14:30:00	0.822	25/11/2014 14:30	.	
25/11/2014 14:45	0.052943968	25/11/2014	14:45:00	0.814	25/11/2014 14:45	.	
25/11/2014 15:00	0.05653913	25/11/2014	15:00:00	0.807	25/11/2014 15:00	.	
25/11/2014 15:15	0.049268687	25/11/2014	15:15:00	0.799	25/11/2014 15:15	.	
25/11/2014 15:30	0.044818302	25/11/2014	15:30:00	0.791	25/11/2014 15:30	.	
25/11/2014 15:45	0.042198764	25/11/2014	15:45:00	0.784	25/11/2014 15:45	.	

	G5 Flow			Middleton Flow	Thorpeness TBR RG Date & Time	Rainfall (mm)	Daily Rainfall (mm)
25/11/2014 16:00	0.052280142	25/11/2014	16:00:00	0.784	25/11/2014 16:00	.	
25/11/2014 16:15	0.050932568	25/11/2014	16:15:00	0.776	25/11/2014 16:15	.	
25/11/2014 16:30	0.050890256	25/11/2014	16:30:00	0.769	25/11/2014 16:30	.	
25/11/2014 16:45	0.043586522	25/11/2014	16:45:00	0.761	25/11/2014 16:45	.	
25/11/2014 17:00	0.045305048	25/11/2014	17:00:00	0.761	25/11/2014 17:00	.	
25/11/2014 17:15	0.041468395	25/11/2014	17:15:00	0.754	25/11/2014 17:15	.	
25/11/2014 17:30	0.044028632	25/11/2014	17:30:00	0.746	25/11/2014 17:30	.	
25/11/2014 17:45	0.045297228	25/11/2014	17:45:00	0.739	25/11/2014 17:45	.	
25/11/2014 18:00	0.049564841	25/11/2014	18:00:00	0.739	25/11/2014 18:00	.	
25/11/2014 18:15	0.051319887	25/11/2014	18:15:00	0.731	25/11/2014 18:15	.	
25/11/2014 18:30	0.049199986	25/11/2014	18:30:00	0.724	25/11/2014 18:30	.	
25/11/2014 18:45	0.049199986	25/11/2014	18:45:00	0.724	25/11/2014 18:45	.	
25/11/2014 19:00	0.05097013	25/11/2014	19:00:00	0.717	25/11/2014 19:00	.	
25/11/2014 19:15	0.054084359	25/11/2014	19:15:00	0.717	25/11/2014 19:15	.	
25/11/2014 19:30	0.056799688	25/11/2014	19:30:00	0.709	25/11/2014 19:30	.	
25/11/2014 19:45	0.054228412	25/11/2014	19:45:00	0.709	25/11/2014 19:45	.	
25/11/2014 20:00	0.053842269	25/11/2014	20:00:00	0.702	25/11/2014 20:00	.	
25/11/2014 20:15	0.055283194	25/11/2014	20:15:00	0.695	25/11/2014 20:15	.	
25/11/2014 20:30	0.051089064	25/11/2014	20:30:00	0.688	25/11/2014 20:30	.	
25/11/2014 20:45	0.045047132	25/11/2014	20:45:00	0.688	25/11/2014 20:45	.	
25/11/2014 21:00	0.053842269	25/11/2014	21:00:00	0.681	25/11/2014 21:00	.	
25/11/2014 21:15	0.055175734	25/11/2014	21:15:00	0.681	25/11/2014 21:15		0.2
25/11/2014 21:30	0.056482832	25/11/2014	21:30:00	0.673	25/11/2014 21:30	.	
25/11/2014 21:45	0.045262057	25/11/2014	21:45:00	0.666	25/11/2014 21:45	.	
25/11/2014 22:00	0.047041044	25/11/2014	22:00:00	0.666	25/11/2014 22:00	.	
25/11/2014 22:15	0.052280142	25/11/2014	22:15:00	0.659	25/11/2014 22:15	.	
25/11/2014 22:30	0.04917173	25/11/2014	22:30:00	0.659	25/11/2014 22:30	.	
25/11/2014 22:45	0.047860326	25/11/2014	22:45:00	0.652	25/11/2014 22:45	.	
25/11/2014 23:00	0.04994624	25/11/2014	23:00:00	0.652	25/11/2014 23:00	.	
25/11/2014 23:15	0.048595725	25/11/2014	23:15:00	0.645	25/11/2014 23:15	.	
25/11/2014 23:30	0.051921236	25/11/2014	23:30:00	0.645	25/11/2014 23:30	.	
25/11/2014 23:45	0.04731075	25/11/2014	23:45:00	0.638	25/11/2014 23:45	.	
26/11/2014 00:00	0.041136407	26/11/2014	00:00:00	0.631	26/11/2014 00:00	.	
26/11/2014 00:15	0.051992454	26/11/2014	00:15:00	0.631	26/11/2014 00:15		0.6
26/11/2014 00:30	0.042330804	26/11/2014	00:30:00	0.631	26/11/2014 00:30		0.2
26/11/2014 00:45	0.039149859	26/11/2014	00:45:00	0.624	26/11/2014 00:45	.	
26/11/2014 01:00	0.045811782	26/11/2014	01:00:00	0.624	26/11/2014 01:00		0.4
26/11/2014 01:15	0.042677934	26/11/2014	01:15:00	0.617	26/11/2014 01:15	.	
26/11/2014 01:30	0.04502832	26/11/2014	01:30:00	0.611	26/11/2014 01:30		0.2
26/11/2014 01:45	0.052895966	26/11/2014	01:45:00	0.611	26/11/2014 01:45	.	
26/11/2014 02:00	0.059595476	26/11/2014	02:00:00	0.611	26/11/2014 02:00	.	
26/11/2014 02:15	0.063749391	26/11/2014	02:15:00	0.604	26/11/2014 02:15		0.2
26/11/2014 02:30	0.074503925	26/11/2014	02:30:00	0.604	26/11/2014 02:30		0.4
26/11/2014 02:45	0.07288606	26/11/2014	02:45:00	0.604	26/11/2014 02:45		0.2
26/11/2014 03:00	0.06820918	26/11/2014	03:00:00	0.597	26/11/2014 03:00		0.8
26/11/2014 03:15	0.056338205	26/11/2014	03:15:00	0.597	26/11/2014 03:15		0.2
26/11/2014 03:30	0.068568493	26/11/2014	03:30:00	0.597	26/11/2014 03:30		0.4
26/11/2014 03:45	0.080088613	26/11/2014	03:45:00	0.597	26/11/2014 03:45	.	
26/11/2014 04:00	0.094637194	26/11/2014	04:00:00	0.597	26/11/2014 04:00		0.2
26/11/2014 04:15	0.110157702	26/11/2014	04:15:00	0.597	26/11/2014 04:15	.	
26/11/2014 04:30	0.108575435	26/11/2014	04:30:00	0 59	26/11/2014 04:30		0.2
26/11/2014 04:45	0.103219037	26/11/2014	04:45:00	0 59	26/11/2014 04:45	.	

G5 Flow		Middleton Flow		Thorpeness TBR RG		
				Date & Time	Rainfall (mm)	Daily Rainfall (mm)
26/11/2014 05:00	0.095275382	26/11/2014 05:00:00	0 59	26/11/2014 05:00	0.2	
26/11/2014 05:15	0.093894752	26/11/2014 05:15:00	0 59	26/11/2014 05:15	0.2	
26/11/2014 05:30	0.087478559	26/11/2014 05:30:00	0 59	26/11/2014 05:30	0.4	
26/11/2014 05:45	0.081189733	26/11/2014 05:45:00	0 59	26/11/2014 05:45	.	
26/11/2014 06:00	0.077497847	26/11/2014 06:00:00	0 59	26/11/2014 06:00	0.4	
26/11/2014 06:15	0.083069698	26/11/2014 06:15:00	0.597	26/11/2014 06:15	0.8	
26/11/2014 06:30	0.090113317	26/11/2014 06:30:00	0.597	26/11/2014 06:30	0.2	
26/11/2014 06:45	0.116318559	26/11/2014 06:45:00	0.597	26/11/2014 06:45	0.2	
26/11/2014 07:00	0.118578417	26/11/2014 07:00:00	0.604	26/11/2014 07:00	0.2	
26/11/2014 07:15	0.106291919	26/11/2014 07:15:00	0.604	26/11/2014 07:15	.	
26/11/2014 07:30	0.110003718	26/11/2014 07:30:00	0.611	26/11/2014 07:30	0.2	
26/11/2014 07:45	0.108419707	26/11/2014 07:45:00	0.624	26/11/2014 07:45	0.2	
26/11/2014 08:00	0.108419707	26/11/2014 08:00:00	0.631	26/11/2014 08:00	0.2	
26/11/2014 08:15	0.100619704	26/11/2014 08:15:00	0.645	26/11/2014 08:15	.	
26/11/2014 08:30	0.08329265	26/11/2014 08:30:00	0.666	26/11/2014 08:30	0.2	
26/11/2014 08:45	0.088426688	26/11/2014 08:45:00	0.681	26/11/2014 08:45	.	
26/11/2014 09:00	0.100239966	26/11/2014 09:00:00	0.709	26/11/2014 09:00	0.2	
26/11/2014 09:15	0.112179687	26/11/2014 09:15:00	0.731	26/11/2014 09:15	.	
26/11/2014 09:30	0.099294984	26/11/2014 09:30:00	0.761	26/11/2014 09:30	0.2	
26/11/2014 09:45	0.103443389	26/11/2014 09:45:00	0.791	26/11/2014 09:45	0.2	
26/11/2014 10:00	0.101169508	26/11/2014 10:00:00	0 83	26/11/2014 10:00	.	
26/11/2014 10:15	0.093205246			26/11/2014 10:15	.	
26/11/2014 10:30	0.108419707			26/11/2014 10:30	.	
26/11/2014 10:45	0.098915642			26/11/2014 10:45	.	
26/11/2014 11:00	0.091956177			26/11/2014 11:00	.	
26/11/2014 11:15	0.09574762			26/11/2014 11:15	.	
26/11/2014 11:30	0.109133771			26/11/2014 11:30	.	
26/11/2014 11:45	0.103443389			26/11/2014 11:45	0.2	
26/11/2014 12:00	0.111290363			26/11/2014 12:00	.	
26/11/2014 12:15	0.105372153			26/11/2014 12:15	.	
26/11/2014 12:30	0.115764792			26/11/2014 12:30	.	
26/11/2014 12:45	0.107845034			26/11/2014 12:45	0.2	
26/11/2014 13:00	0.115086586			26/11/2014 13:00	.	
26/11/2014 13:15	0.107480483			26/11/2014 13:15	.	
26/11/2014 13:30	0.103054449			26/11/2014 13:30	0.2	
26/11/2014 13:45	0.106597561			26/11/2014 13:45	.	
26/11/2014 14:00	0.124207689			26/11/2014 14:00	.	
26/11/2014 14:15	0.117465158			26/11/2014 14:15	.	
26/11/2014 14:30	0.119604225			26/11/2014 14:30	0.2	
26/11/2014 14:45	0.143430513			26/11/2014 14:45	0.2	
26/11/2014 15:00	0.128938929			26/11/2014 15:00	0.4	
26/11/2014 15:15	0.116007209			26/11/2014 15:15	.	
26/11/2014 15:30	0.148943629			26/11/2014 15:30	0.4	
26/11/2014 15:45	0.196796402			26/11/2014 15:45	0.6	
26/11/2014 16:00	0.186405624			26/11/2014 16:00	0.2	
26/11/2014 16:15	0.210363576			26/11/2014 16:15	.	
26/11/2014 16:30	0.201768445			26/11/2014 16:30	0.4	
26/11/2014 16:45	0.231381741			26/11/2014 16:45	0.4	
26/11/2014 17:00	0.204268734			26/11/2014 17:00	0.4	
26/11/2014 17:15	0.212279899			26/11/2014 17:15	1	
26/11/2014 17:30	0.218036561			26/11/2014 17:30	1	
26/11/2014 17:45	0.362350629			26/11/2014 17:45	0.8	

	G5 Flow	Middleton Flow	Thorpeness TBR RG Date & Time	Rainfall (mm)	Daily Rainfall (mm)
26/11/2014 18:00	0.387848132		26/11/2014 18:00	0.4	
26/11/2014 18:15	0.392503157		26/11/2014 18:15	0.2	
26/11/2014 18:30	0.366086167		26/11/2014 18:30	0.2	
26/11/2014 18:45	0.319028483		26/11/2014 18:45	.	
26/11/2014 19:00	0.159279884		26/11/2014 19:00	0.2	
26/11/2014 19:15	0.331316837		26/11/2014 19:15	0.4	
26/11/2014 19:30	0.362203532		26/11/2014 19:30	.	
26/11/2014 19:45	0.415435332		26/11/2014 19:45	.	
26/11/2014 20:00	0.305636504		26/11/2014 20:00	0.2	
26/11/2014 20:15	0.486456466		26/11/2014 20:15	.	
26/11/2014 20:30	0.553253239		26/11/2014 20:30	.	
26/11/2014 20:45	0.531463998		26/11/2014 20:45	.	
26/11/2014 21:00	0.501419386		26/11/2014 21:00	.	
26/11/2014 21:15	0.493489775		26/11/2014 21:15	.	
26/11/2014 21:30	0.581427611		26/11/2014 21:30	.	
26/11/2014 21:45	0.533572024		26/11/2014 21:45	.	
26/11/2014 22:00	0.536727856		26/11/2014 22:00	.	
26/11/2014 22:15	0.570702068		26/11/2014 22:15	.	
26/11/2014 22:30	0.613761035		26/11/2014 22:30	.	
26/11/2014 22:45	0.54300057		26/11/2014 22:45	.	
26/11/2014 23:00	0.551385058		26/11/2014 23:00	.	
26/11/2014 23:15	0.584109158		26/11/2014 23:15	.	
26/11/2014 23:30	0.561623425		26/11/2014 23:30	.	
26/11/2014 23:45	0.561623425		26/11/2014 23:45	.	
27/11/2014 00:00	0.517832853		27/11/2014 00:00	.	
27/11/2014 00:15	0.558381539		27/11/2014 00:15	.	
27/11/2014 00:30	0.576609805		27/11/2014 00:30	.	
27/11/2014 00:45	0.555487806		27/11/2014 00:45	.	
27/11/2014 01:00	0.554359575		27/11/2014 01:00	.	
27/11/2014 01:15	0.529284469		27/11/2014 01:15	.	
27/11/2014 01:30	0.437473682		27/11/2014 01:30	.	
27/11/2014 01:45	0.451875255		27/11/2014 01:45	.	
27/11/2014 02:00	0.425468783		27/11/2014 02:00	.	
27/11/2014 02:15	0.472808077		27/11/2014 02:15	.	
27/11/2014 02:30	0.464265931		27/11/2014 02:30	.	
27/11/2014 02:45	0.430248641		27/11/2014 02:45	.	
27/11/2014 03:00	0.423075745		27/11/2014 03:00	.	
27/11/2014 03:15	0.4000397		27/11/2014 03:15	.	
27/11/2014 03:30	0.482422959		27/11/2014 03:30	.	
27/11/2014 03:45	0.39571554		27/11/2014 03:45	.	
27/11/2014 04:00	0.361312328		27/11/2014 04:00	.	
27/11/2014 04:15	0.356678698		27/11/2014 04:15	.	
27/11/2014 04:30	0.417159015		27/11/2014 04:30	.	
27/11/2014 04:45	0.359359809		27/11/2014 04:45	.	
27/11/2014 05:00	0.34588243		27/11/2014 05:00	.	
27/11/2014 05:15	0.319416588		27/11/2014 05:15	.	
27/11/2014 05:30	0.330909827		27/11/2014 05:30	.	
27/11/2014 05:45	0.340462653		27/11/2014 05:45	.	
27/11/2014 06:00	0.30995771		27/11/2014 06:00	.	
27/11/2014 06:15	0.312768555		27/11/2014 06:15	.	
27/11/2014 06:30	0.298864475		27/11/2014 06:30	.	
27/11/2014 06:45	0.274681677		27/11/2014 06:45	.	

	G5 Flow	Middleton Flow	Thorpeness TBR RG Date & Time	Rainfall (mm)	Daily Rainfall (mm)
27/11/2014 07:00	0.294761416		27/11/2014 07:00	.	
27/11/2014 07:15	0.252766345		27/11/2014 07:15	.	
27/11/2014 07:30	0.24569301		27/11/2014 07:30	.	
27/11/2014 07:45	0.284092653		27/11/2014 07:45	.	
27/11/2014 08:00	0.260109003		27/11/2014 08:00	.	
27/11/2014 08:15	0.259357074		27/11/2014 08:15	.	
27/11/2014 08:30	0.26640866		27/11/2014 08:30	.	
27/11/2014 08:45	0.239329838		27/11/2014 08:45	.	



SAAR	592	mm
AREA	5.04	Km2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capacity in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
18-Nov-14	24.8	mm
25-Nov-14	0.0	mm

Source of Rainfall event data.

Gauge	**Easting**	**Northing**	**Distance from Catchment Centroid (m)**	**Reciprocal**	**Weighting**
Benhall	38166	60602	20912.0		0.00000
Soham	23243	62717	6550.0		0.00000
Thorpeness	60012	78834	3636.0	0.00028	1.00000
			Total	0.00028	1.00000

TBR RG

Daily RF totals 9am 9am	Benhall	Soham	Thorpeness
Date	Total RF (mm)	Total RF (mm)	Total RF (mm)
21/11/2014		0	1.4
20/11/2014		0	0
19/11/2014		0	0.2
18/11/2014		0	0
17/11/2014		0	6
Total API5 RF			7.6

Rainall Event Depth P (mm)	17
Event duration (hours)	3.75

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**17/11/2014**	**18/11/2014**	**19/11/2014**	**20/11/2014**	**21/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	6	0	0.2	0	1.4
Average Daily rainfall totals			6	0	0.2	0	1.4

Gauge	**SAAR**	**Weight**	**17/11/2014**	**18/11/2014**	**19/11/2014**	**20/11/2014**	**21/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0.010135135	0	0.000337838	0	0.002364865

Gauge	**SAAR**	**Weight**	**17/11/2014**	**18/11/2014**	**19/11/2014**	**20/11/2014**	**21/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.0000	0.010135135	0	0.000337838	0	0.002364865

Gauge	**SAAR**	**Weight**	**17/11/2014**	**18/11/2014**	**19/11/2014**	**20/11/2014**	**21/11/2014**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	6	0	0.2	0	1.4
Catchment Average Antecedent RF mm			6	0	0.2	0	1.4

Date	**Catchment Average Antecedent Rainfall (mm)**	
17/11/2014	6.00	d-5
18/11/2014	0.00	d-4
19/11/2014	0.20	d-3
20/11/2014	0.00	d-2
21/11/2014	1.40	d-1

API5
1.29 mm 1.290469876 mm / day

CWI Prior to Event November 2014 Event at G5
CWI 125 + API15 - SMD
SMD 24.8 mm
CWI 101.4904699 mm

FEH Parameter								**URBEXT2000**		As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
SPR	45.80159154	%						**PR**	40	taken from PR calculations sheet using Benhall TBR RG record
PRrural	39.92	%		P=Storm Depth	17	mm		**DPRrain**	0	DPRrain is 0, as P<40mm
DPRrain	0	%		SPR	45.80159154			**DPRcwi**	-5.877382531	
DPRcwi	-5.877382531	CWI	101.49					**SPR**	45.80159154	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural								**DPRrain**	0.45(P-40)^0.7	#NUM!
PR	40.07958054	%						**P**	17	
PRrural	39.92420901	%						**CWI**	101.4904699	
CWI	101.4904699	mm						**SPR**	45.80159154	
BF	0.00001		Baseflow equation taken from FEH					**PR**	40.07958054	
	-1254									
	1778.5	524.5	0.00525					**SPRHOST**	24.27	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
AREA	50.52		**0.26498** m3s-1					**Duration (hours)**	3.75	
SPR	45.80159154									
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	45 80159154									
PRrural	39 92420901									

Calculation of SPR

Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
23-Nov-14	23-Nov-14	3.75	1.29	24.80	101.49	39.92	-5.88	0.00	45.80	40.00	24.27

Site **Sub-catchment** **SPRg.cds** **SPRg.obs** **SPRs.cds** **SPRs.adj**

Site	Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Sizewell	Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	Leis Abbey	24.3	44.8	27.8	51.4
Leiston	Leiston	24.3	44.8	20.7	38.2
Leis Upper	Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	Mins Potters	24.3	44.8	25.3	46.8
				Mean	37.3

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
16/07/2015 09:00	0 019991997		16/07/2015 09:00	.	
16/07/2015 09:15	0 017124398		16/07/2015 09:15	.	
16/07/2015 09:30	0 022642558	Ed,Int	16/07/2015 09:30	.	
16/07/2015 09:45	0 028160719		16/07/2015 09:45	.	
16/07/2015 10:00	0 016492046		16/07/2015 10:00	.	
16/07/2015 10:15	0 028091716		16/07/2015 10:15	.	
16/07/2015 10:30	0.02914805	Ed,Int	16/07/2015 10:30	.	
16/07/2015 10:45	0 030204383		16/07/2015 10:45	.	
16/07/2015 11:00	0 029282587	Ed,Int	16/07/2015 11:00	.	
16/07/2015 11:15	0 028360791		16/07/2015 11:15	.	
16/07/2015 11:30	0 025039171		16/07/2015 11:30	.	
16/07/2015 11:45	0 020155099		16/07/2015 11:45	.	
16/07/2015 12:00	0.02550589	Ed,Int	16/07/2015 12:00	.	
16/07/2015 12:15	0.03085668		16/07/2015 12:15	.	
16/07/2015 12:30	0 026955728		16/07/2015 12:30	.	
16/07/2015 12:45	0 025750738		16/07/2015 12:45	.	
16/07/2015 13:00	0 023104279		16/07/2015 13:00	.	
16/07/2015 13:15	0 018707627		16/07/2015 13:15	.	
16/07/2015 13:30	0 025588489		16/07/2015 13:30	.	
16/07/2015 13:45	0 020273547		16/07/2015 13:45	.	
16/07/2015 14:00	0 019672963	Ed,Int	16/07/2015 14:00	.	
16/07/2015 14:15	0 019072378	Ed,Int	16/07/2015 14:15	.	
16/07/2015 14:30	0 018471793		16/07/2015 14:30	.	
16/07/2015 14:45	0 013669618		16/07/2015 14:45	.	
16/07/2015 15:00	0 030903094		16/07/2015 15:00	.	
16/07/2015 15:15	0 038153368		16/07/2015 15:15	.	
16/07/2015 15:30	0 022586283		16/07/2015 15:30	.	
16/07/2015 15:45	0 027637394	Ed,Int	16/07/2015 15:45	.	
16/07/2015 16:00	0 032688506		16/07/2015 16:00	.	
16/07/2015 16:15	0 019192595		16/07/2015 16:15	.	
16/07/2015 16:30	0 017856819	Ed,Int	16/07/2015 16:30	.	
16/07/2015 16:45	0 016521042		16/07/2015 16:45	.	
16/07/2015 17:00	0 021710228		16/07/2015 17:00	.	
16/07/2015 17:15	0 021561921	Ed,Int	16/07/2015 17:15	.	
16/07/2015 17:30	0 021413613	Ed,Int	16/07/2015 17:30	.	
16/07/2015 17:45	0 021265306		16/07/2015 17:45	.	
16/07/2015 18:00	0 028309581		16/07/2015 18:00	.	
16/07/2015 18:15	0 016329542		16/07/2015 18:15	.	
16/07/2015 18:30	0 021986626		16/07/2015 18:30	.	
16/07/2015 18:45	0 039146982		16/07/2015 18:45	.	
16/07/2015 19:00	0 028110561	Ed,Int	16/07/2015 19:00	.	
16/07/2015 19:15	0.01707414		16/07/2015 19:15	.	
16/07/2015 19:30	0 022910814		16/07/2015 19:30	.	
16/07/2015 19:45	0 017897573		16/07/2015 19:45	.	
16/07/2015 20:00	0 019777538	Ed,Int	16/07/2015 20:00	.	
16/07/2015 20:15	0 021657503		16/07/2015 20:15	.	
16/07/2015 20:30	0 019150883		16/07/2015 20:30	.	
16/07/2015 20:45	0 022677574		16/07/2015 20:45	.	
16/07/2015 21:00	0.02189932	Ed,Int	16/07/2015 21:00	.	
16/07/2015 21:15	0 021121065	Ed,Int	16/07/2015 21:15	.	
16/07/2015 21:30	0.02034281	Ed,Int	16/07/2015 21:30	.	
16/07/2015 21:45	0 019564555		16/07/2015 21:45	.	
16/07/2015 22:00	0 021208674		16/07/2015 22:00	.	

	DATE TIME
start of event	24/07/2015 13 00
end of event	25/07/2015 08:15
duration hours	19 25
total RF mm	42.6
SMD W/E AVERAGE	**mm**

		Thorpeness TBR RG
DATE	**API5**	**Daily Totals**
23/07/2015	d-1	0
22/07/2015	d-2	0.4
21/07/2015	d-3	0
20/07/2015	d-4	0
19/07/2015	d-5	0
		0.4

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
16/07/2015 22:15	0 022445799	Ed,Int	16/07/2015 22:15	.	
16/07/2015 22:30	0 023682923		16/07/2015 22:30	.	
16/07/2015 22:45	0 021208674		16/07/2015 22:45	.	
16/07/2015 23:00	0 020133317	Ed,Int	16/07/2015 23:00	.	
16/07/2015 23:15	0.01905796	Ed,Int	16/07/2015 23:15	.	
16/07/2015 23:30	0 017982603	Ed,Int	16/07/2015 23:30	.	
16/07/2015 23:45	0 016907247		16/07/2015 23:45	.	
17/07/2015 00:00	0 024791709		17/07/2015 00:00	.	
17/07/2015 00:15	0 024066233	Ed,Int	17/07/2015 00:15	.	
17/07/2015 00:30	0 023340757		17/07/2015 00:30	.	
17/07/2015 00:45	0 021085712		17/07/2015 00:45	.	
17/07/2015 01:00	0 020273547		17/07/2015 01:00	.	
17/07/2015 01:15	0.01925991		17/07/2015 01:15	.	
17/07/2015 01:30	0 019050487		17/07/2015 01:30	.	
17/07/2015 01:45	0 016189395	Ed,Int	17/07/2015 01:45	.	
17/07/2015 02:00	0 013328304		17/07/2015 02:00	.	
17/07/2015 02:15	0.01970186		17/07/2015 02:15	.	
17/07/2015 02:30	0 015969656		17/07/2015 02:30	.	
17/07/2015 02:45	0 018316074		17/07/2015 02:45	.	
17/07/2015 03:00	0 019192595		17/07/2015 03:00	.	
17/07/2015 03:15	0 020903943		17/07/2015 03:15	.	
17/07/2015 03:30	0 017838843		17/07/2015 03:30	.	
17/07/2015 03:45	0 016960142	Ed,Int	17/07/2015 03:45	.	
17/07/2015 04:00	0 016081441	Ed,Int	17/07/2015 04:00	.	
17/07/2015 04:15	0.01520274	Ed,Int	17/07/2015 04:15	.	
17/07/2015 04:30	0 014324039		17/07/2015 04:30	.	
17/07/2015 04:45	0 011639547		17/07/2015 04:45	.	
17/07/2015 05:00	0 014651671		17/07/2015 05:00	.	
17/07/2015 05:15	0 017464665		17/07/2015 05:15	.	
17/07/2015 05:30	0 011826493		17/07/2015 05:30	.	
17/07/2015 05:45	0 011179981		17/07/2015 05:45	.	
17/07/2015 06:00	0 011516503		17/07/2015 06:00	.	
17/07/2015 06:15	0 012045977	Ed,Int	17/07/2015 06:15	.	
17/07/2015 06:30	0.01257545	Ed,Int	17/07/2015 06:30	.	
17/07/2015 06:45	0 013104924	Ed,Int	17/07/2015 06:45	.	
17/07/2015 07:00	0 013634398		17/07/2015 07:00	.	
17/07/2015 07:15	0.01380549	Ed,Int	17/07/2015 07:15	.	
17/07/2015 07:30	0 013976583		17/07/2015 07:30	.	
17/07/2015 07:45	0.01786432		17/07/2015 07:45	.	
17/07/2015 08:00	0.01775632		17/07/2015 08:00	.	
17/07/2015 08:15	0 023055455	Ed,Int	17/07/2015 08:15	.	
17/07/2015 08:30	0.02835459		17/07/2015 08:30	.	
17/07/2015 08:45	0 012661343		17/07/2015 08:45	.	
17/07/2015 09:00	0 013328304		17/07/2015 09:00	.	
17/07/2015 09:15	0 016505651	Ed,Int	17/07/2015 09:15	.	
17/07/2015 09:30	0 019682998		17/07/2015 09:30	.	
17/07/2015 09:45	0 018993199	Ed,Int	17/07/2015 09:45	.	
17/07/2015 10:00	0 0183034		17/07/2015 10:00	.	
17/07/2015 10:15	0.02548623	Ed,Int	17/07/2015 10:15	.	
17/07/2015 10:30	0 032669059		17/07/2015 10:30	.	
17/07/2015 10:45	0 029057633		17/07/2015 10:45	.	
17/07/2015 11:00	0 024170356		17/07/2015 11:00	.	
17/07/2015 11:15	0 024992317		17/07/2015 11:15	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
17/07/2015 11:30	0 021929593		17/07/2015 11:30	.	
17/07/2015 11:45	0 020842547		17/07/2015 11:45	.	
17/07/2015 12:00	0 017270918		17/07/2015 12:00	.	
17/07/2015 12:15	0.02801286		17/07/2015 12:15	.	
17/07/2015 12:30	0 016492046		17/07/2015 12:30	.	
17/07/2015 12:45	0 016805646	Ed,Int	17/07/2015 12:45	.	
17/07/2015 13:00	0 017119247		17/07/2015 13:00	.	
17/07/2015 13:15	0 023463796		17/07/2015 13:15	.	
17/07/2015 13:30	0 021173978	Ed,Int	17/07/2015 13:30	.	
17/07/2015 13:45	0 018884159		17/07/2015 13:45	.	
17/07/2015 14:00	0.02186079	Ed,Int	17/07/2015 14:00	.	
17/07/2015 14:15	0 024837421		17/07/2015 14:15	.	
17/07/2015 14:30	0 018842473		17/07/2015 14:30	.	
17/07/2015 14:45	0 014069145		17/07/2015 14:45	.	
17/07/2015 15:00	0 017863733		17/07/2015 15:00	.	
17/07/2015 15:15	0 019341933	Ed,Int	17/07/2015 15:15	.	
17/07/2015 15:30	0 020820134		17/07/2015 15:30	.	
17/07/2015 15:45	0 015787904		17/07/2015 15:45	.	
17/07/2015 16:00	0 019489204		17/07/2015 16:00	.	
17/07/2015 16:15	0 019786383	Ed,Int	17/07/2015 16:15	.	
17/07/2015 16:30	0 020083562	Ed,Int	17/07/2015 16:30	.	
17/07/2015 16:45	0 020380741		17/07/2015 16:45	.	
17/07/2015 17:00	0 017425576		17/07/2015 17:00	.	
17/07/2015 17:15	0 019250661	Ed,Int	17/07/2015 17:15	.	
17/07/2015 17:30	0 021075746	Ed,Int	17/07/2015 17:30	.	
17/07/2015 17:45	0 022900831		17/07/2015 17:45	.	
17/07/2015 18:00	0 012497847		17/07/2015 18:00	.	
17/07/2015 18:15	0 012661343		17/07/2015 18:15	.	
17/07/2015 18:30	0 022460717	Ed,Int	17/07/2015 18:30	.	
17/07/2015 18:45	0 032260091		17/07/2015 18:45	.	
17/07/2015 19:00	0 023272878	Ed,Int	17/07/2015 19:00	.	
17/07/2015 19:15	0 014285665		17/07/2015 19:15	.	
17/07/2015 19:30	0 019564519		17/07/2015 19:30	.	
17/07/2015 19:45	0 022631747		17/07/2015 19:45	.	
17/07/2015 20:00	0 019394383	Ed,Int	17/07/2015 20:00	.	
17/07/2015 20:15	0.01615702		17/07/2015 20:15	.	
17/07/2015 20:30	0.01615702		17/07/2015 20:30	.	
17/07/2015 20:45	0.03149525		17/07/2015 20:45	.	
17/07/2015 21:00	0 040147676	Ed,Int	17/07/2015 21:00	.	
17/07/2015 21:15	0 048800103		17/07/2015 21:15	.	
17/07/2015 21:30	0 020057333		17/07/2015 21:30	.	
17/07/2015 21:45	0 023576856		17/07/2015 21:45	.	
17/07/2015 22:00	0 021230508		17/07/2015 22:00	.	
17/07/2015 22:15	0.02337314	Ed,Int	17/07/2015 22:15	.	
17/07/2015 22:30	0 025515772	Ed,Int	17/07/2015 22:30	.	
17/07/2015 22:45	0 027658405		17/07/2015 22:45	.	
17/07/2015 23:00	0 023933082	Ed,Int	17/07/2015 23:00	.	
17/07/2015 23:15	0.02020776		17/07/2015 23:15	.	
17/07/2015 23:30	0 021366148	Ed,Int	17/07/2015 23:30	.	
17/07/2015 23:45	0 022524536	Ed,Int	17/07/2015 23:45	.	
18/07/2015 00:00	0 023682923		18/07/2015 00:00	.	
18/07/2015 00:15	0 021986626		18/07/2015 00:15	.	
18/07/2015 00:30	0 015087755		18/07/2015 00:30	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
18/07/2015 00:45	0 015922241		18/07/2015 00:45	.	
18/07/2015 01:00	0 018663965	Ed,Int	18/07/2015 01:00	.	
18/07/2015 01:15	0 021405689	Ed,Int	18/07/2015 01:15	.	
18/07/2015 01:30	0 024147413	Ed,Int	18/07/2015 01:30	.	
18/07/2015 01:45	0 026889137		18/07/2015 01:45	.	
18/07/2015 02:00	0 028635379		18/07/2015 02:00	.	
18/07/2015 02:15	0 020820134		18/07/2015 02:15	.	
18/07/2015 02:30	0 020383618	Ed,Int	18/07/2015 02:30	.	
18/07/2015 02:45	0 019947102		18/07/2015 02:45	.	
18/07/2015 03:00	0 018370043	Ed,Int	18/07/2015 03:00	.	
18/07/2015 03:15	0 016792984	Ed,Int	18/07/2015 03:15	.	
18/07/2015 03:30	0 015215926		18/07/2015 03:30	.	
18/07/2015 03:45	0 012787088		18/07/2015 03:45	.	
18/07/2015 04:00	0 018428821	Ed,Int	18/07/2015 04:00	.	
18/07/2015 04:15	0 024070555	Ed,Int	18/07/2015 04:15	.	
18/07/2015 04:30	0 029712289		18/07/2015 04:30	.	
18/07/2015 04:45	0 036399966		18/07/2015 04:45	.	
18/07/2015 05:00	0.01854323		18/07/2015 05:00	.	
18/07/2015 05:15	0 016978636	Ed,Int	18/07/2015 05:15	.	
18/07/2015 05:30	0 015414042		18/07/2015 05:30	.	
18/07/2015 05:45	0 013072884	Ed,Int	18/07/2015 05:45	.	
18/07/2015 06:00	0 010731725		18/07/2015 06:00	.	
18/07/2015 06:15	0.01157145	Ed,Int	18/07/2015 06:15	.	
18/07/2015 06:30	0 012411176	Ed,Int	18/07/2015 06:30	.	
18/07/2015 06:45	0 013250901	Ed,Int	18/07/2015 06:45	.	
18/07/2015 07:00	0 014090627		18/07/2015 07:00	.	
18/07/2015 07:15	0.01381249	Ed,Int	18/07/2015 07:15	.	
18/07/2015 07:30	0 013534354	Ed,Int	18/07/2015 07:30	.	
18/07/2015 07:45	0 013256217	Ed,Int	18/07/2015 07:45	.	
18/07/2015 08:00	0.01297808		18/07/2015 08:00	.	
18/07/2015 08:15	0 019337102	Ed,Int	18/07/2015 08:15	.	
18/07/2015 08:30	0 025696124		18/07/2015 08:30	.	
18/07/2015 08:45	0 013480754		18/07/2015 08:45	.	
18/07/2015 09:00	0 012270068		18/07/2015 09:00	.	
18/07/2015 09:15	0 016924098	Ed,Int	18/07/2015 09:15	.	
18/07/2015 09:30	0 021578129		18/07/2015 09:30	.	
18/07/2015 09:45	0 021266726	Ed,Int	18/07/2015 09:45	.	
18/07/2015 10:00	0 020955323	Ed,Int	18/07/2015 10:00	.	
18/07/2015 10:15	0.02064392		18/07/2015 10:15	.	
18/07/2015 10:30	0 018377368	Ed,Int	18/07/2015 10:30	.	
18/07/2015 10:45	0 016110816		18/07/2015 10:45	.	
18/07/2015 11:00	0.03085668		18/07/2015 11:00	.	
18/07/2015 11:15	0 033586297		18/07/2015 11:15	.	
18/07/2015 11:30	0 064111745		18/07/2015 11:30	.	
18/07/2015 11:45	0 024428662		18/07/2015 11:45	.	
18/07/2015 12:00	0 041773628		18/07/2015 12:00	.	
18/07/2015 12:15	0 025398206		18/07/2015 12:15	.	
18/07/2015 12:30	0 045030583		18/07/2015 12:30	.	
18/07/2015 12:45	0 033877336		18/07/2015 12:45	.	
18/07/2015 13:00	0 039005632		18/07/2015 13:00	.	
18/07/2015 13:15	0 057396147		18/07/2015 13:15	.	
18/07/2015 13:30	0 080579727		18/07/2015 13:30	.	
18/07/2015 13:45	0 041790513		18/07/2015 13:45	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
18/07/2015 14:00	0.05258189		18/07/2015 14:00	.	
18/07/2015 14:15	0 028821964		18/07/2015 14:15	.	
18/07/2015 14:30	0 030817081	Ed,Int	18/07/2015 14:30	.	
18/07/2015 14:45	0 032812198	Ed,Int	18/07/2015 14:45	.	
18/07/2015 15:00	0 034807315		18/07/2015 15:00	.	
18/07/2015 15:15	0 042422118	Ed,Int	18/07/2015 15:15	.	
18/07/2015 15:30	0 050036921		18/07/2015 15:30	.	
18/07/2015 15:45	0 026769588		18/07/2015 15:45	.	
18/07/2015 16:00	0 025923205		18/07/2015 16:00	.	
18/07/2015 16:15	0 036738967		18/07/2015 16:15	.	
18/07/2015 16:30	0 022291043		18/07/2015 16:30	.	
18/07/2015 16:45	0 030453157	Ed,Int	18/07/2015 16:45	.	
18/07/2015 17:00	0.03861527		18/07/2015 17:00	.	
18/07/2015 17:15	0 062084174		18/07/2015 17:15	.	
18/07/2015 17:30	0 020478968		18/07/2015 17:30	.	
18/07/2015 17:45	0 022168051		18/07/2015 17:45	.	
18/07/2015 18:00	0 020820134		18/07/2015 18:00	.	
18/07/2015 18:15	0 021938407		18/07/2015 18:15	.	
18/07/2015 18:30	0 020820134		18/07/2015 18:30	.	
18/07/2015 18:45	0 029487409		18/07/2015 18:45	.	
18/07/2015 19:00	0 015974748		18/07/2015 19:00	.	
18/07/2015 19:15	0 026672271		18/07/2015 19:15	.	
18/07/2015 19:30	0 027290406	Ed,Int	18/07/2015 19:30	.	
18/07/2015 19:45	0 027908541	Ed,Int	18/07/2015 19:45	.	
18/07/2015 20:00	0 028526675	Ed,Int	18/07/2015 20:00	.	
18/07/2015 20:15	0.02914481	Ed,Int	18/07/2015 20:15	.	
18/07/2015 20:30	0 029762945		18/07/2015 20:30	.	
18/07/2015 20:45	0.04183294		18/07/2015 20:45	.	
18/07/2015 21:00	0 020207874		18/07/2015 21:00	.	
18/07/2015 21:15	0.01615702		18/07/2015 21:15	.	
18/07/2015 21:30	0 017626933	Ed,Int	18/07/2015 21:30	.	
18/07/2015 21:45	0 019096845	Ed,Int	18/07/2015 21:45	.	
18/07/2015 22:00	0 020566758		18/07/2015 22:00	.	
18/07/2015 22:15	0 018267712		18/07/2015 22:15	.	
18/07/2015 22:30	0 055052459		18/07/2015 22:30	.	
18/07/2015 22:45	0 014819142		18/07/2015 22:45	.	
18/07/2015 23:00	0 023202587		18/07/2015 23:00	.	
18/07/2015 23:15	0 018635866		18/07/2015 23:15	.	
18/07/2015 23:30	0 030052668		18/07/2015 23:30	.	
18/07/2015 23:45	0.03747359		18/07/2015 23:45	.	
19/07/2015 00:00	0 034043527	Ed,Int	19/07/2015 00:00	.	
19/07/2015 00:15	0 030613464		19/07/2015 00:15	.	
19/07/2015 00:30	0.01315961		19/07/2015 00:30	.	
19/07/2015 00:45	0 033121139		19/07/2015 00:45	.	
19/07/2015 01:00	0 018933949		19/07/2015 01:00	.	
19/07/2015 01:15	0 019173448	Ed,Int	19/07/2015 01:15	.	
19/07/2015 01:30	0 019412948	Ed,Int	19/07/2015 01:30	.	
19/07/2015 01:45	0 019652448	Ed,Int	19/07/2015 01:45	.	
19/07/2015 02:00	0 019891948	Ed,Int	19/07/2015 02:00	.	
19/07/2015 02:15	0 020131448		19/07/2015 02:15	.	
19/07/2015 02:30	0 015974748		19/07/2015 02:30	.	
19/07/2015 02:45	0 025852363		19/07/2015 02:45	.	
19/07/2015 03:00	0 018175199		19/07/2015 03:00	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
19/07/2015 03:15	0 024543407		19/07/2015 03:15	.	
19/07/2015 03:30	0 031608833		19/07/2015 03:30	.	
19/07/2015 03:45	0 019307376		19/07/2015 03:45	.	
19/07/2015 04:00	0 025965937		19/07/2015 04:00	.	
19/07/2015 04:15	0 028330514		19/07/2015 04:15	.	
19/07/2015 04:30	0.02209345		19/07/2015 04:30	.	
19/07/2015 04:45	0 021695249	Ed,Int	19/07/2015 04:45	.	
19/07/2015 05:00	0 021297048	Ed,Int	19/07/2015 05:00	.	
19/07/2015 05:15	0 020898847		19/07/2015 05:15	.	
19/07/2015 05:30	0 011137526		19/07/2015 05:30	.	
19/07/2015 05:45	0 016675152	Ed,Int	19/07/2015 05:45	.	
19/07/2015 06:00	0 022212777		19/07/2015 06:00	.	
19/07/2015 06:15	0.02737913		19/07/2015 06:15	.	
19/07/2015 06:30	0 014439658		19/07/2015 06:30	.	
19/07/2015 06:45	0 057312589		19/07/2015 06:45	0.2	
19/07/2015 07:00	0.01297808		19/07/2015 07:00	0.4	
19/07/2015 07:15	0.01492685	Ed,Int	19/07/2015 07:15	.	
19/07/2015 07:30	0.01687562		19/07/2015 07:30	.	
19/07/2015 07:45	0 020285966		19/07/2015 07:45	.	
19/07/2015 08:00	0 019524997		19/07/2015 08:00	.	
19/07/2015 08:15	0 018343385	Ed,Int	19/07/2015 08:15	.	
19/07/2015 08:30	0 017161774		19/07/2015 08:30	.	
19/07/2015 08:45	0 058316671		19/07/2015 08:45	.	
19/07/2015 09:00	0 041223194		19/07/2015 09:00	.	
19/07/2015 09:15	0.03305123	Ed,Int	19/07/2015 09:15	.	
19/07/2015 09:30	0 024879266		19/07/2015 09:30	.	
19/07/2015 09:45	0 017425576		19/07/2015 09:45	.	
19/07/2015 10:00	0 031662956	Ed,Int	19/07/2015 10:00	.	
19/07/2015 10:15	0 045900337	Ed,Int	19/07/2015 10:15	.	
19/07/2015 10:30	0 060137717		19/07/2015 10:30	.	
19/07/2015 10:45	0 040587883		19/07/2015 10:45	.	
19/07/2015 11:00	0 063296713		19/07/2015 11:00	.	
19/07/2015 11:15	0 060695458		19/07/2015 11:15	.	
19/07/2015 11:30	0 015271028		19/07/2015 11:30	.	
19/07/2015 11:45	0 015881537		19/07/2015 11:45	.	
19/07/2015 12:00	0 032975788		19/07/2015 12:00	.	
19/07/2015 12:15	0 028975322		19/07/2015 12:15	.	
19/07/2015 12:30	0 034807315		19/07/2015 12:30	.	
19/07/2015 12:45	0 053122584		19/07/2015 12:45	.	
19/07/2015 13:00	0 028430692		19/07/2015 13:00	.	
19/07/2015 13:15	0 039954137		19/07/2015 13:15	.	
19/07/2015 13:30	0 020930777		19/07/2015 13:30	.	
19/07/2015 13:45	0 019123291		19/07/2015 13:45	.	
19/07/2015 14:00	0 036595651		19/07/2015 14:00	.	
19/07/2015 14:15	0 026353233		19/07/2015 14:15	.	
19/07/2015 14:30	0 047044405		19/07/2015 14:30	.	
19/07/2015 14:45	0 028763214		19/07/2015 14:45	.	
19/07/2015 15:00	0 040912404		19/07/2015 15:00	.	
19/07/2015 15:15	0 031724234		19/07/2015 15:15	.	
19/07/2015 15:30	0 029526216		19/07/2015 15:30	.	
19/07/2015 15:45	0 040733084		19/07/2015 15:45	.	
19/07/2015 16:00	0 042239794		19/07/2015 16:00	.	
19/07/2015 16:15	0 042743931		19/07/2015 16:15	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
19/07/2015 16:30	0 019725787		19/07/2015 16:30	.	
19/07/2015 16:45	0 041059374		19/07/2015 16:45	.	
19/07/2015 17:00	0 020273547		19/07/2015 17:00	.	
19/07/2015 17:15	0.02885614		19/07/2015 17:15	.	
19/07/2015 17:30	0 025994807		19/07/2015 17:30	.	
19/07/2015 17:45	0 013669618		19/07/2015 17:45	.	
19/07/2015 18:00	0 021861143	Ed,Int	19/07/2015 18:00	.	
19/07/2015 18:15	0 030052668		19/07/2015 18:15	.	
19/07/2015 18:30	0 040540882		19/07/2015 18:30	.	
19/07/2015 18:45	0 024666878		19/07/2015 18:45	.	
19/07/2015 19:00	0 026934593		19/07/2015 19:00	.	
19/07/2015 19:15	0 029769236		19/07/2015 19:15	.	
19/07/2015 19:30	0 022490031	Ed,Int	19/07/2015 19:30	.	
19/07/2015 19:45	0 015210825		19/07/2015 19:45	.	
19/07/2015 20:00	0 016451888	Ed,Int	19/07/2015 20:00	.	
19/07/2015 20:15	0.01769295		19/07/2015 20:15	.	
19/07/2015 20:30	0 018471793		19/07/2015 20:30	.	
19/07/2015 20:45	0 018471793		19/07/2015 20:45	.	
19/07/2015 21:00	0 019842545		19/07/2015 21:00	.	
19/07/2015 21:15	0 061118433		19/07/2015 21:15	.	
19/07/2015 21:30	0 044693993		19/07/2015 21:30	.	
19/07/2015 21:45	0 074604067		19/07/2015 21:45	.	
19/07/2015 22:00	0.02499794		19/07/2015 22:00	.	
19/07/2015 22:15	0 050811769		19/07/2015 22:15	.	
19/07/2015 22:30	0 076376178		19/07/2015 22:30	.	
19/07/2015 22:45	0 052000811		19/07/2015 22:45	.	
19/07/2015 23:00	0 041533316		19/07/2015 23:00	.	
19/07/2015 23:15	0 033265628	Ed,Int	19/07/2015 23:15	.	
19/07/2015 23:30	0.02499794		19/07/2015 23:30	.	
19/07/2015 23:45	0 023876831	Ed,Int	19/07/2015 23:45	.	
20/07/2015 00:00	0 022755721		20/07/2015 00:00	.	
20/07/2015 00:15	0 024503627		20/07/2015 00:15	.	
20/07/2015 00:30	0 020786567		20/07/2015 00:30	.	
20/07/2015 00:45	0 025164852		20/07/2015 00:45	.	
20/07/2015 01:00	0.04183294		20/07/2015 01:00	.	
20/07/2015 01:15	0 025416114		20/07/2015 01:15	.	
20/07/2015 01:30	0 043147954		20/07/2015 01:30	.	
20/07/2015 01:45	0 018677275		20/07/2015 01:45	.	
20/07/2015 02:00	0 023101341		20/07/2015 02:00	.	
20/07/2015 02:15	0 022291043		20/07/2015 02:15	.	
20/07/2015 02:30	0 024496711	Ed,Int	20/07/2015 02:30	.	
20/07/2015 02:45	0 026702378	Ed,Int	20/07/2015 02:45	.	
20/07/2015 03:00	0 028908045	Ed,Int	20/07/2015 03:00	.	
20/07/2015 03:15	0 031113713		20/07/2015 03:15	.	
20/07/2015 03:30	0 020272268		20/07/2015 03:30	.	
20/07/2015 03:45	0.01717862		20/07/2015 03:45	.	
20/07/2015 04:00	0 032527182		20/07/2015 04:00	.	
20/07/2015 04:15	0 014338148		20/07/2015 04:15	.	
20/07/2015 04:30	0 018124252	Ed,Int	20/07/2015 04:30	.	
20/07/2015 04:45	0 021910356		20/07/2015 04:45	.	
20/07/2015 05:00	0 012141568		20/07/2015 05:00	.	
20/07/2015 05:15	0 019245268		20/07/2015 05:15	.	
20/07/2015 05:30	0 011179981		20/07/2015 05:30	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
20/07/2015 05:45	0 020997647		20/07/2015 05:45	.	
20/07/2015 06:00	0 011516503		20/07/2015 06:00	.	
20/07/2015 06:15	0 010542118		20/07/2015 06:15	.	
20/07/2015 06:30	0 013780967		20/07/2015 06:30	.	
20/07/2015 06:45	0 011846918		20/07/2015 06:45	.	
20/07/2015 07:00	0 011516503		20/07/2015 07:00	.	
20/07/2015 07:15	0 012907961	Ed,Int	20/07/2015 07:15	.	
20/07/2015 07:30	0 014299418		20/07/2015 07:30	.	
20/07/2015 07:45	0 019169856		20/07/2015 07:45	.	
20/07/2015 08:00	0 020114633	Ed,Int	20/07/2015 08:00	.	
20/07/2015 08:15	0.02105941		20/07/2015 08:15	.	
20/07/2015 08:30	0 028607842		20/07/2015 08:30	.	
20/07/2015 08:45	0 027827368	Ed,Int	20/07/2015 08:45	.	
20/07/2015 09:00	0 027046895	Ed,Int	20/07/2015 09:00	.	0
20/07/2015 09:15	0 026266421	Ed,Int	20/07/2015 09:15	.	
20/07/2015 09:30	0 025485947		20/07/2015 09:30	.	
20/07/2015 09:45	0 017512004		20/07/2015 09:45	.	
20/07/2015 10:00	0 023576856		20/07/2015 10:00	.	
20/07/2015 10:15	0 035354219		20/07/2015 10:15	.	
20/07/2015 10:30	0 027625444	Ed,Int	20/07/2015 10:30	.	
20/07/2015 10:45	0 019896669		20/07/2015 10:45	.	
20/07/2015 11:00	0 027625444		20/07/2015 11:00	.	
20/07/2015 11:15	0 044051889		20/07/2015 11:15	.	
20/07/2015 11:30	0 056162459		20/07/2015 11:30	.	
20/07/2015 11:45	0 024058317		20/07/2015 11:45	.	
20/07/2015 12:00	0 037732304		20/07/2015 12:00	.	
20/07/2015 12:15	0 034165177		20/07/2015 12:15	.	
20/07/2015 12:30	0 030312882		20/07/2015 12:30	.	
20/07/2015 12:45	0 040587883		20/07/2015 12:45	.	
20/07/2015 13:00	0 057012323		20/07/2015 13:00	.	
20/07/2015 13:15	0 022173086		20/07/2015 13:15	.	
20/07/2015 13:30	0 026251533		20/07/2015 13:30	.	
20/07/2015 13:45	0 057012323		20/07/2015 13:45	.	
20/07/2015 14:00	0.03059805		20/07/2015 14:00	.	
20/07/2015 14:15	0 038807772	Ed,Int	20/07/2015 14:15	.	
20/07/2015 14:30	0 047017494		20/07/2015 14:30	.	
20/07/2015 14:45	0 045796476		20/07/2015 14:45	.	
20/07/2015 15:00	0 026260189		20/07/2015 15:00	.	
20/07/2015 15:15	0.07695046		20/07/2015 15:15	.	
20/07/2015 15:30	0 037198146		20/07/2015 15:30	.	
20/07/2015 15:45	0 036271348		20/07/2015 15:45	.	
20/07/2015 16:00	0 039761668		20/07/2015 16:00	.	
20/07/2015 16:15	0 017710985		20/07/2015 16:15	.	
20/07/2015 16:30	0 021689941	Ed,Int	20/07/2015 16:30	.	
20/07/2015 16:45	0 025668897		20/07/2015 16:45	.	
20/07/2015 17:00	0 054218023		20/07/2015 17:00	.	
20/07/2015 17:15	0 030624355		20/07/2015 17:15	.	
20/07/2015 17:30	0 029466968	Ed,Int	20/07/2015 17:30	.	
20/07/2015 17:45	0 028309581		20/07/2015 17:45	.	
20/07/2015 18:00	0 051029127		20/07/2015 18:00	.	
20/07/2015 18:15	0 022865805		20/07/2015 18:15	.	
20/07/2015 18:30	0 013669618		20/07/2015 18:30	.	
20/07/2015 18:45	0 019417235	Ed,Int	20/07/2015 18:45	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
20/07/2015 19:00	0 025164852		20/07/2015 19:00	.	
20/07/2015 19:15	0 036085323		20/07/2015 19:15	.	
20/07/2015 19:30	0 029188183		20/07/2015 19:30	.	
20/07/2015 19:45	0 024837421		20/07/2015 19:45	.	
20/07/2015 20:00	0 022631301	Ed,Int	20/07/2015 20:00	.	
20/07/2015 20:15	0.02042518		20/07/2015 20:15	.	
20/07/2015 20:30	0 014778049		20/07/2015 20:30	.	
20/07/2015 20:45	0 040001296		20/07/2015 20:45	.	
20/07/2015 21:00	0 020864096		20/07/2015 21:00	.	
20/07/2015 21:15	0 024407391		20/07/2015 21:15	.	
20/07/2015 21:30	0 016329542		20/07/2015 21:30	.	
20/07/2015 21:45	0 046650121		20/07/2015 21:45	.	
20/07/2015 22:00	0 026436402		20/07/2015 22:00	.	
20/07/2015 22:15	0 021308769		20/07/2015 22:15	.	
20/07/2015 22:30	0 043453386		20/07/2015 22:30	.	
20/07/2015 22:45	0 024899788		20/07/2015 22:45	.	
20/07/2015 23:00	0 032378185		20/07/2015 23:00	.	
20/07/2015 23:15	0 021152726		20/07/2015 23:15	.	
20/07/2015 23:30	0 018528299		20/07/2015 23:30	.	
20/07/2015 23:45	0 015828933		20/07/2015 23:45	.	
21/07/2015 00:00	0 054870221		21/07/2015 00:00	.	
21/07/2015 00:15	0 047977015		21/07/2015 00:15	.	
21/07/2015 00:30	0 040457155		21/07/2015 00:30	.	
21/07/2015 00:45	0 045091311		21/07/2015 00:45	.	
21/07/2015 01:00	0 024920048		21/07/2015 01:00	.	
21/07/2015 01:15	0.02713173		21/07/2015 01:15	.	
21/07/2015 01:30	0.02236572		21/07/2015 01:30	.	
21/07/2015 01:45	0.04046087		21/07/2015 01:45	.	
21/07/2015 02:00	0 043304963		21/07/2015 02:00	.	
21/07/2015 02:15	0.05946174		21/07/2015 02:15	.	
21/07/2015 02:30	0 032636753		21/07/2015 02:30	.	
21/07/2015 02:45	0 013895232		21/07/2015 02:45	.	
21/07/2015 03:00	0 021168054	Ed,Int	21/07/2015 03:00	.	
21/07/2015 03:15	0 028440876	Ed,Int	21/07/2015 03:15	.	
21/07/2015 03:30	0 035713699		21/07/2015 03:30	.	
21/07/2015 03:45	0 028990484	Ed,Int	21/07/2015 03:45	.	
21/07/2015 04:00	0.02226727		21/07/2015 04:00	.	
21/07/2015 04:15	0 027013198		21/07/2015 04:15	.	
21/07/2015 04:30	0 034767699	Ed,Int	21/07/2015 04:30	.	
21/07/2015 04:45	0 042522201		21/07/2015 04:45	.	
21/07/2015 05:00	0 021404602		21/07/2015 05:00	.	
21/07/2015 05:15	0 023186021		21/07/2015 05:15	.	
21/07/2015 05:30	0 014973177		21/07/2015 05:30	.	
21/07/2015 05:45	0 015625468	Ed,Int	21/07/2015 05:45	.	
21/07/2015 06:00	0 016277758		21/07/2015 06:00	.	
21/07/2015 06:15	0.02296118		21/07/2015 06:15	.	
21/07/2015 06:30	0 019034114		21/07/2015 06:30	.	
21/07/2015 06:45	0 020506764		21/07/2015 06:45	.	
21/07/2015 07:00	0 036215029		21/07/2015 07:00	.	
21/07/2015 07:15	0 014794003		21/07/2015 07:15	.	
21/07/2015 07:30	0 026198144		21/07/2015 07:30	.	
21/07/2015 07:45	0 022142238		21/07/2015 07:45	.	
21/07/2015 08:00	0 030137977		21/07/2015 08:00	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
21/07/2015 08:15	0 051770907		21/07/2015 08:15	.	
21/07/2015 08:30	0 052122617		21/07/2015 08:30	.	
21/07/2015 08:45	0 037684018		21/07/2015 08:45	.	
21/07/2015 09:00	0 058282286		21/07/2015 09:00	.	0
21/07/2015 09:15	0 051173752		21/07/2015 09:15	.	
21/07/2015 09:30	0 030912614		21/07/2015 09:30	.	
21/07/2015 09:45	0 072832419		21/07/2015 09:45	.	
21/07/2015 10:00	0 074592614		21/07/2015 10:00	.	
21/07/2015 10:15	0 036672733		21/07/2015 10:15	.	
21/07/2015 10:30	0 059395914		21/07/2015 10:30	.	
21/07/2015 10:45	0 046209155		21/07/2015 10:45	.	
21/07/2015 11:00	0 050696977		21/07/2015 11:00	.	
21/07/2015 11:15	0.117224356		21/07/2015 11:15	.	
21/07/2015 11:30	0 052753119		21/07/2015 11:30	.	
21/07/2015 11:45	0.07326072		21/07/2015 11:45	.	
21/07/2015 12:00	0 087809219		21/07/2015 12:00	.	
21/07/2015 12:15	0 060097793		21/07/2015 12:15	.	
21/07/2015 12:30	0 025647098		21/07/2015 12:30	.	
21/07/2015 12:45	0 035339862		21/07/2015 12:45	.	
21/07/2015 13:00	0 048434325		21/07/2015 13:00	.	
21/07/2015 13:15	0 051652273	Ed,Int	21/07/2015 13:15	.	
21/07/2015 13:30	0 054870221		21/07/2015 13:30	.	
21/07/2015 13:45	0 022215484		21/07/2015 13:45	.	
21/07/2015 14:00	0 039005632		21/07/2015 14:00	.	
21/07/2015 14:15	0 050982102		21/07/2015 14:15	.	
21/07/2015 14:30	0 016735713		21/07/2015 14:30	.	
21/07/2015 14:45	0 036085323		21/07/2015 14:45	.	
21/07/2015 15:00	0 058594674		21/07/2015 15:00	.	
21/07/2015 15:15	0 025546216		21/07/2015 15:15	.	
21/07/2015 15:30	0.01766383		21/07/2015 15:30	.	
21/07/2015 15:45	0 024486508		21/07/2015 15:45	.	
21/07/2015 16:00	0 046847246		21/07/2015 16:00	.	
21/07/2015 16:15	0 015235474		21/07/2015 16:15	.	
21/07/2015 16:30	0 034626347		21/07/2015 16:30	.	
21/07/2015 16:45	0 037007198		21/07/2015 16:45	.	
21/07/2015 17:00	0 056981145		21/07/2015 17:00	.	
21/07/2015 17:15	0 018112923		21/07/2015 17:15	.	
21/07/2015 17:30	0 047803926		21/07/2015 17:30	.	
21/07/2015 17:45	0.03680105		21/07/2015 17:45	.	
21/07/2015 18:00	0 026185984		21/07/2015 18:00	.	
21/07/2015 18:15	0 013764114		21/07/2015 18:15	.	
21/07/2015 18:30	0 027818043		21/07/2015 18:30	.	
21/07/2015 18:45	0 031739519		21/07/2015 18:45	.	
21/07/2015 19:00	0 019417235		21/07/2015 19:00	.	
21/07/2015 19:15	0 030903431		21/07/2015 19:15	.	
21/07/2015 19:30	0.02713173		21/07/2015 19:30	.	
21/07/2015 19:45	0 017033826		21/07/2015 19:45	.	
21/07/2015 20:00	0 028248151		21/07/2015 20:00	.	
21/07/2015 20:15	0 019131815		21/07/2015 20:15	.	
21/07/2015 20:30	0.04092256		21/07/2015 20:30	.	
21/07/2015 20:45	0 026430296		21/07/2015 20:45	.	
21/07/2015 21:00	0 058929759		21/07/2015 21:00	.	
21/07/2015 21:15	0 024406951		21/07/2015 21:15	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
21/07/2015 21:30	0 023300178		21/07/2015 21:30	.	
21/07/2015 21:45	0 024301486		21/07/2015 21:45	.	
21/07/2015 22:00	0 061415226		21/07/2015 22:00	.	
21/07/2015 22:15	0 038807813		21/07/2015 22:15	.	
21/07/2015 22:30	0.03785986		21/07/2015 22:30	.	
21/07/2015 22:45	0 028091716		21/07/2015 22:45	.	
21/07/2015 23:00	0 040560634		21/07/2015 23:00	.	
21/07/2015 23:15	0 046235574		21/07/2015 23:15	.	
21/07/2015 23:30	0.03088482		21/07/2015 23:30	.	
21/07/2015 23:45	0 022869275		21/07/2015 23:45	.	
22/07/2015 00:00	0.03706836		22/07/2015 00:00	.	
22/07/2015 00:15	0 014598828		22/07/2015 00:15	.	
22/07/2015 00:30	0 053902935		22/07/2015 00:30	.	
22/07/2015 00:45	0 044954194	Ed,Int	22/07/2015 00:45	.	
22/07/2015 01:00	0 036005452		22/07/2015 01:00	.	
22/07/2015 01:15	0 034171196	Ed,Int	22/07/2015 01:15	.	
22/07/2015 01:30	0 032336939	Ed,Int	22/07/2015 01:30	.	
22/07/2015 01:45	0 030502682	Ed,Int	22/07/2015 01:45	.	
22/07/2015 02:00	0 028668425	Ed,Int	22/07/2015 02:00	.	
22/07/2015 02:15	0 026834168		22/07/2015 02:15	.	
22/07/2015 02:30	0 028051835	Ed,Int	22/07/2015 02:30	.	
22/07/2015 02:45	0 029269501	Ed,Int	22/07/2015 02:45	.	
22/07/2015 03:00	0 030487168	Ed,Int	22/07/2015 03:00	.	
22/07/2015 03:15	0 031704835		22/07/2015 03:15	.	
22/07/2015 03:30	0 027927943	Ed,Int	22/07/2015 03:30	.	
22/07/2015 03:45	0 024151051	Ed,Int	22/07/2015 03:45	.	
22/07/2015 04:00	0 020374159	Ed,Int	22/07/2015 04:00	.	
22/07/2015 04:15	0 016597267		22/07/2015 04:15	.	
22/07/2015 04:30	0 018474309		22/07/2015 04:30	.	
22/07/2015 04:45	0 011442758		22/07/2015 04:45	.	
22/07/2015 05:00	0 013549235	Ed,Int	22/07/2015 05:00	.	
22/07/2015 05:15	0 015655712		22/07/2015 05:15	.	
22/07/2015 05:30	0 016214027	Ed,Int	22/07/2015 05:30	.	
22/07/2015 05:45	0 016772343		22/07/2015 05:45	.	
22/07/2015 06:00	0 015597931		22/07/2015 06:00	.	
22/07/2015 06:15	0.02001588		22/07/2015 06:15	.	
22/07/2015 06:30	0 021856206	Ed,Int	22/07/2015 06:30	.	
22/07/2015 06:45	0 023696532		22/07/2015 06:45	.	
22/07/2015 07:00	0 022989832	Ed,Int	22/07/2015 07:00	.	
22/07/2015 07:15	0 022283131	Ed,Int	22/07/2015 07:15	.	
22/07/2015 07:30	0.02157643		22/07/2015 07:30	.	
22/07/2015 07:45	0 023898031	Ed,Int	22/07/2015 07:45	.	
22/07/2015 08:00	0 026219633	Ed,Int	22/07/2015 08:00	.	
22/07/2015 08:15	0 028541235		22/07/2015 08:15	.	
22/07/2015 08:30	0 027548432	Ed,Int	22/07/2015 08:30	.	
22/07/2015 08:45	0 026555629		22/07/2015 08:45	.	
22/07/2015 09:00	0 022192112		22/07/2015 09:00	.	0
22/07/2015 09:15	0 038621437		22/07/2015 09:15	.	
22/07/2015 09:30	0 037676231		22/07/2015 09:30	.	
22/07/2015 09:45	0 027553159		22/07/2015 09:45	.	
22/07/2015 10:00	0 050134324		22/07/2015 10:00	.	
22/07/2015 10:15	0 038974961	Ed,Int	22/07/2015 10:15	.	
22/07/2015 10:30	0 027815598		22/07/2015 10:30	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
22/07/2015 10:45	0 030791428		22/07/2015 10:45	.	
22/07/2015 11:00	0 028762911		22/07/2015 11:00	.	
22/07/2015 11:15	0 034504238	Ed,Int	22/07/2015 11:15	.	
22/07/2015 11:30	0 040245566		22/07/2015 11:30	.	
22/07/2015 11:45	0 022440515		22/07/2015 11:45	.	
22/07/2015 12:00	0 031981642		22/07/2015 12:00	.	
22/07/2015 12:15	0 030557088		22/07/2015 12:15	.	
22/07/2015 12:30	0 019554454		22/07/2015 12:30	.	
22/07/2015 12:45	0 021286635		22/07/2015 12:45	.	
22/07/2015 13:00	0 017897573		22/07/2015 13:00	.	
22/07/2015 13:15	0 023682923		22/07/2015 13:15	.	
22/07/2015 13:30	0.30984535		22/07/2015 13:30	.	
22/07/2015 13:45	0 016300749		22/07/2015 13:45	.	
22/07/2015 14:00	0 016410747	Ed,Int	22/07/2015 14:00	.	
22/07/2015 14:15	0 016520744		22/07/2015 14:15	.	
22/07/2015 14:30	0 017963319	Ed,Int	22/07/2015 14:30	.	
22/07/2015 14:45	0 019405894	Ed,Int	22/07/2015 14:45	.	
22/07/2015 15:00	0 020848468	Ed,Int	22/07/2015 15:00	.	
22/07/2015 15:15	0 022291043		22/07/2015 15:15	.	
22/07/2015 15:30	0 018569868	Ed,Int	22/07/2015 15:30	.	
22/07/2015 15:45	0 014848693		22/07/2015 15:45	.	
22/07/2015 16:00	0 014220795	Ed,Int	22/07/2015 16:00	.	
22/07/2015 16:15	0 013592898		22/07/2015 16:15	.	
22/07/2015 16:30	0 013422993		22/07/2015 16:30	.	
22/07/2015 16:45	0 025112021	Ed,Int	22/07/2015 16:45	.	
22/07/2015 17:00	0.03680105		22/07/2015 17:00	.	
22/07/2015 17:15	0.015783		22/07/2015 17:15	0.2	
22/07/2015 17:30	0 015745603	Ed,Int	22/07/2015 17:30	.	
22/07/2015 17:45	0 015708207	Ed,Int	22/07/2015 17:45	.	
22/07/2015 18:00	0 015670811	Ed,Int	22/07/2015 18:00	.	
22/07/2015 18:15	0 015633415	Ed,Int	22/07/2015 18:15	.	
22/07/2015 18:30	0 015596018		22/07/2015 18:30	.	
22/07/2015 18:45	0 016618868	Ed,Int	22/07/2015 18:45	.	
22/07/2015 19:00	0 017641717	Ed,Int	22/07/2015 19:00	.	
22/07/2015 19:15	0 018664567	Ed,Int	22/07/2015 19:15	.	
22/07/2015 19:30	0 019687416	Ed,Int	22/07/2015 19:30	.	
22/07/2015 19:45	0 020710266		22/07/2015 19:45	.	
22/07/2015 20:00	0 019812511	Ed,Int	22/07/2015 20:00	.	
22/07/2015 20:15	0 018914756		22/07/2015 20:15	.	
22/07/2015 20:30	0 087144117		22/07/2015 20:30	.	
22/07/2015 20:45	0.02524736		22/07/2015 20:45	.	
22/07/2015 21:00	0 024652838		22/07/2015 21:00	.	
22/07/2015 21:15	0 019302148		22/07/2015 21:15	.	
22/07/2015 21:30	0 018707627	Ed,Int	22/07/2015 21:30	.	
22/07/2015 21:45	0 018113106	Ed,Int	22/07/2015 21:45	.	
22/07/2015 22:00	0 017518585		22/07/2015 22:00	.	
22/07/2015 22:15	0 018622186		22/07/2015 22:15	.	
22/07/2015 22:30	0 019725787		22/07/2015 22:30	.	
22/07/2015 22:45	0 021156018	Ed,Int	22/07/2015 22:45	.	
22/07/2015 23:00	0.02258625	Ed,Int	22/07/2015 23:00	.	
22/07/2015 23:15	0 024016481		22/07/2015 23:15	.	
22/07/2015 23:30	0 040229894		22/07/2015 23:30	.	
22/07/2015 23:45	0 028949253	Ed,Int	22/07/2015 23:45	.	

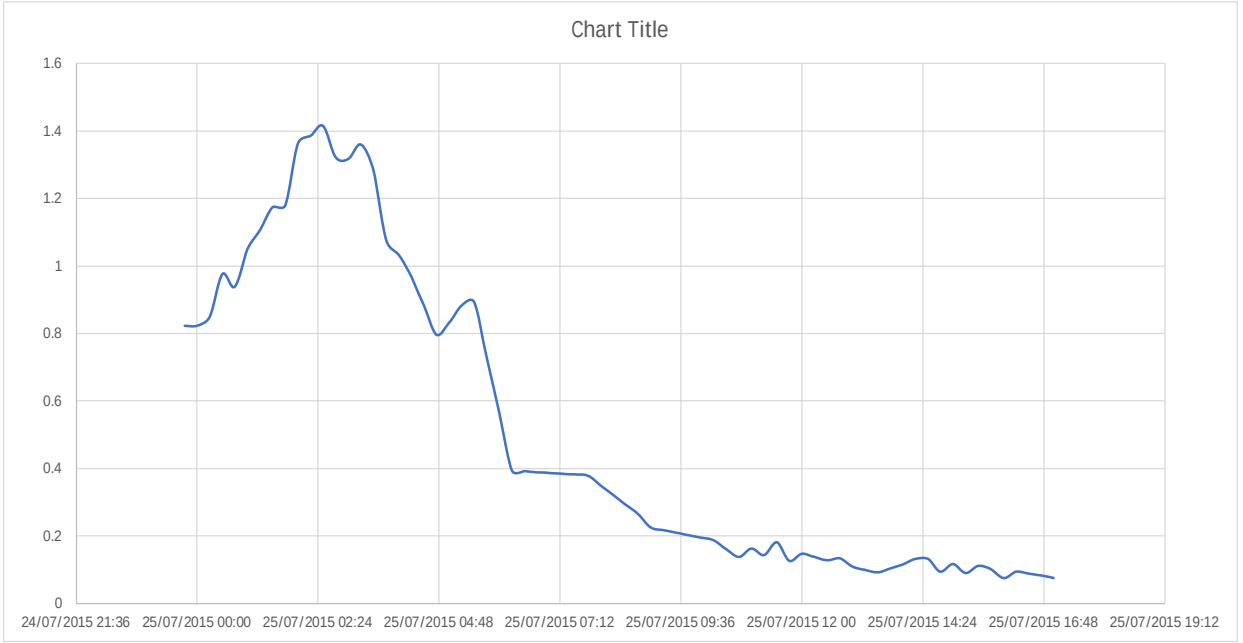
Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
23/07/2015 00:00	0 017668613		23/07/2015 00:00	.	
23/07/2015 00:15	0 021353892	Ed,Int	23/07/2015 00:15	.	
23/07/2015 00:30	0 025039171		23/07/2015 00:30	.	
23/07/2015 00:45	0 021475261	Ed,Int	23/07/2015 00:45	.	
23/07/2015 01:00	0 017911351		23/07/2015 01:00	.	
23/07/2015 01:15	0.01809464		23/07/2015 01:15	.	
23/07/2015 01:30	0 026889137		23/07/2015 01:30	.	
23/07/2015 01:45	0 015974748		23/07/2015 01:45	.	
23/07/2015 02:00	0 098335545		23/07/2015 02:00	.	
23/07/2015 02:15	0 014687949		23/07/2015 02:15	.	
23/07/2015 02:30	0 014336717	Ed,Int	23/07/2015 02:30	.	
23/07/2015 02:45	0 013985486		23/07/2015 02:45	.	
23/07/2015 03:00	0 020461761		23/07/2015 03:00	.	
23/07/2015 03:15	0 024621161	Ed,Int	23/07/2015 03:15	.	
23/07/2015 03:30	0 028780562	Ed,Int	23/07/2015 03:30	.	
23/07/2015 03:45	0 032939962	Ed,Int	23/07/2015 03:45	.	
23/07/2015 04:00	0 037099362	Ed,Int	23/07/2015 04:00	.	
23/07/2015 04:15	0 041258762		23/07/2015 04:15	.	
23/07/2015 04:30	0 037383026	Ed,Int	23/07/2015 04:30	.	
23/07/2015 04:45	0 033507289	Ed,Int	23/07/2015 04:45	.	
23/07/2015 05:00	0 029631552		23/07/2015 05:00	.	
23/07/2015 05:15	0.02148853		23/07/2015 05:15	.	
23/07/2015 05:30	0.02443383	Ed,Int	23/07/2015 05:30	.	
23/07/2015 05:45	0.02737913		23/07/2015 05:45	.	
23/07/2015 06:00	0 036705912		23/07/2015 06:00	0.2	
23/07/2015 06:15	0 029833546	Ed,Int	23/07/2015 06:15	.	
23/07/2015 06:30	0.02296118		23/07/2015 06:30	.	
23/07/2015 06:45	0 019245268		23/07/2015 06:45	.	
23/07/2015 07:00	0 010635506		23/07/2015 07:00	.	
23/07/2015 07:15	0.02342762		23/07/2015 07:15	.	
23/07/2015 07:30	0 022964065	Ed,Int	23/07/2015 07:30	.	
23/07/2015 07:45	0.02250051		23/07/2015 07:45	.	
23/07/2015 08:00	0 014687949		23/07/2015 08:00	.	
23/07/2015 08:15	0 025852363		23/07/2015 08:15	.	
23/07/2015 08:30	0 025177995	Ed,Int	23/07/2015 08:30	.	
23/07/2015 08:45	0 024503627		23/07/2015 08:45	.	
23/07/2015 09:00	0 023931591	Ed,Int	23/07/2015 09:00	.	0.4
23/07/2015 09:15	0 023359555	Ed,Int	23/07/2015 09:15	.	
23/07/2015 09:30	0.02278752	Ed,Int	23/07/2015 09:30	.	
23/07/2015 09:45	0 022215484		23/07/2015 09:45	.	
23/07/2015 10:00	0 021467506	Ed,Int	23/07/2015 10:00	.	
23/07/2015 10:15	0 020719527	Ed,Int	23/07/2015 10:15	.	
23/07/2015 10:30	0 019971549		23/07/2015 10:30	.	
23/07/2015 10:45	0 022015313	Ed,Int	23/07/2015 10:45	.	
23/07/2015 11:00	0 024059076		23/07/2015 11:00	.	
23/07/2015 11:15	0 017299238		23/07/2015 11:15	.	
23/07/2015 11:30	0 016501434	Ed,Int	23/07/2015 11:30	.	
23/07/2015 11:45	0 015703629	Ed,Int	23/07/2015 11:45	.	
23/07/2015 12:00	0 014905825		23/07/2015 12:00	.	
23/07/2015 12:15	0 026260189		23/07/2015 12:15	.	
23/07/2015 12:30	0 025578633	Ed,Int	23/07/2015 12:30	.	
23/07/2015 12:45	0 024897077		23/07/2015 12:45	.	
23/07/2015 13:00	0.01742889		23/07/2015 13:00	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
23/07/2015 13:15	0 017329779	Ed,Int	23/07/2015 13:15	.	
23/07/2015 13:30	0 017230669		23/07/2015 13:30	.	
23/07/2015 13:45	0.02138464	Ed,Int	23/07/2015 13:45	.	
23/07/2015 14:00	0.02553861		23/07/2015 14:00	.	
23/07/2015 14:15	0 018934081		23/07/2015 14:15	.	
23/07/2015 14:30	0 018523594	Ed,Int	23/07/2015 14:30	.	
23/07/2015 14:45	0 018113106		23/07/2015 14:45	.	
23/07/2015 15:00	0 015549154		23/07/2015 15:00	.	
23/07/2015 15:15	0 019416834	Ed,Int	23/07/2015 15:15	.	
23/07/2015 15:30	0 023284514	Ed,Int	23/07/2015 15:30	.	
23/07/2015 15:45	0 027152194		23/07/2015 15:45	.	
23/07/2015 16:00	0 024313418	Ed,Int	23/07/2015 16:00	.	
23/07/2015 16:15	0 021474642	Ed,Int	23/07/2015 16:15	.	
23/07/2015 16:30	0 018635866		23/07/2015 16:30	.	
23/07/2015 16:45	0.02085228	Ed,Int	23/07/2015 16:45	.	
23/07/2015 17:00	0 023068694	Ed,Int	23/07/2015 17:00	.	
23/07/2015 17:15	0 025285108	Ed,Int	23/07/2015 17:15	.	
23/07/2015 17:30	0 027501522		23/07/2015 17:30	.	
23/07/2015 17:45	0 023773427		23/07/2015 17:45	.	
23/07/2015 18:00	0 020463033	Ed,Int	23/07/2015 18:00	.	
23/07/2015 18:15	0.01715264	Ed,Int	23/07/2015 18:15	.	
23/07/2015 18:30	0 013842246		23/07/2015 18:30	.	
23/07/2015 18:45	0 015286249	Ed,Int	23/07/2015 18:45	.	
23/07/2015 19:00	0 016730252		23/07/2015 19:00	.	
23/07/2015 19:15	0 031192571		23/07/2015 19:15	.	
23/07/2015 19:30	0 027037293	Ed,Int	23/07/2015 19:30	.	
23/07/2015 19:45	0 022882016	Ed,Int	23/07/2015 19:45	.	
23/07/2015 20:00	0 018726738		23/07/2015 20:00	.	
23/07/2015 20:15	0 019939732		23/07/2015 20:15	.	
23/07/2015 20:30	0 021152726		23/07/2015 20:30	.	
23/07/2015 20:45	0 015694252		23/07/2015 20:45	.	
23/07/2015 21:00	0 042986622		23/07/2015 21:00	.	
23/07/2015 21:15	0 016300749		23/07/2015 21:15	.	
23/07/2015 21:30	0 022972218		23/07/2015 21:30	.	
23/07/2015 21:45	0 020344063	Ed,Int	23/07/2015 21:45	.	
23/07/2015 22:00	0 017715909	Ed,Int	23/07/2015 22:00	.	
23/07/2015 22:15	0 015087755		23/07/2015 22:15	.	
23/07/2015 22:30	0 023818153		23/07/2015 22:30	.	
23/07/2015 22:45	0 023599924	Ed,Int	23/07/2015 22:45	.	
23/07/2015 23:00	0 023381695		23/07/2015 23:00	.	
23/07/2015 23:15	0 031216699		23/07/2015 23:15	.	
23/07/2015 23:30	0 018480648		23/07/2015 23:30	.	
23/07/2015 23:45	0 037040215		23/07/2015 23:45	.	
24/07/2015 00:00	0 021063873		24/07/2015 00:00	.	
24/07/2015 00:15	0 019589868	Ed,Int	24/07/2015 00:15	.	
24/07/2015 00:30	0 018115862		24/07/2015 00:30	.	
24/07/2015 00:45	0 018515309	Ed,Int	24/07/2015 00:45	.	
24/07/2015 01:00	0 018914756		24/07/2015 01:00	.	
24/07/2015 01:15	0 019669968	Ed,Int	24/07/2015 01:15	.	
24/07/2015 01:30	0.02042518		24/07/2015 01:30	.	
24/07/2015 01:45	0.02803866		24/07/2015 01:45	.	
24/07/2015 02:00	0 026423527	Ed,Int	24/07/2015 02:00	.	
24/07/2015 02:15	0 024808394	Ed,Int	24/07/2015 02:15	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
24/07/2015 02:30	0.023193262	Ed,Int	24/07/2015 02:30	.	
24/07/2015 02:45	0.021578129		24/07/2015 02:45	.	
24/07/2015 03:00	0.014695124		24/07/2015 03:00	.	
24/07/2015 03:15	0.014518339	Ed,Int	24/07/2015 03:15	.	
24/07/2015 03:30	0.014341554		24/07/2015 03:30	.	
24/07/2015 03:45	0.019412594		24/07/2015 03:45	.	
24/07/2015 04:00	0.027585825	Ed,Int	24/07/2015 04:00	.	
24/07/2015 04:15	0.035759057	Ed,Int	24/07/2015 04:15	.	
24/07/2015 04:30	0.043932288		24/07/2015 04:30	.	
24/07/2015 04:45	0.017556747		24/07/2015 04:45	.	
24/07/2015 05:00	0.028256227		24/07/2015 05:00	.	
24/07/2015 05:15	0.028117819	Ed,Int	24/07/2015 05:15	.	
24/07/2015 05:30	0.02797941		24/07/2015 05:30	.	
24/07/2015 05:45	0.011795266		24/07/2015 05:45	.	
24/07/2015 06:00	0.018370075	Ed,Int	24/07/2015 06:00	.	
24/07/2015 06:15	0.024944883	Ed,Int	24/07/2015 06:15	.	
24/07/2015 06:30	0.031519691		24/07/2015 06:30	.	
24/07/2015 06:45	0.023161236		24/07/2015 06:45	.	
24/07/2015 07:00	0.019098057	Ed,Int	24/07/2015 07:00	.	
24/07/2015 07:15	0.015034878		24/07/2015 07:15	.	
24/07/2015 07:30	0.017662712	Ed,Int	24/07/2015 07:30	.	
24/07/2015 07:45	0.020290547	Ed,Int	24/07/2015 07:45	.	
24/07/2015 08:00	0.022918381	Ed,Int	24/07/2015 08:00	.	
24/07/2015 08:15	0.025546216		24/07/2015 08:15	.	
24/07/2015 08:30	0.019991997		24/07/2015 08:30	.	
24/07/2015 08:45	0.014778049		24/07/2015 08:45	.	
24/07/2015 09:00	0.015663374	Ed,Int	24/07/2015 09:00	.	0
24/07/2015 09:15	0.016548698	Ed,Int	24/07/2015 09:15	.	
24/07/2015 09:30	0.017434023	Ed,Int	24/07/2015 09:30	.	
24/07/2015 09:45	0.018319348		24/07/2015 09:45	.	
24/07/2015 10:00	0.028281008		24/07/2015 10:00	.	
24/07/2015 10:15	0.019564555		24/07/2015 10:15	.	
24/07/2015 10:30	0.033563949		24/07/2015 10:30	.	
24/07/2015 10:45	0.016017608		24/07/2015 10:45	.	
24/07/2015 11:00	0.01960365	Ed,Int	24/07/2015 11:00	.	
24/07/2015 11:15	0.023189693	Ed,Int	24/07/2015 11:15	.	
24/07/2015 11:30	0.026775735		24/07/2015 11:30	.	
24/07/2015 11:45	0.015828933		24/07/2015 11:45	.	
24/07/2015 12:00	0.025535944		24/07/2015 12:00	.	
24/07/2015 12:15	0.022618859		24/07/2015 12:15	.	
24/07/2015 12:30	0.026403421		24/07/2015 12:30	.	
24/07/2015 12:45	0.018895039		24/07/2015 12:45	.	
24/07/2015 13:00	0.023689983		24/07/2015 13:00	0.2	
24/07/2015 13:15	0.017230669		24/07/2015 13:15	.	
24/07/2015 13:30	0.025668384		24/07/2015 13:30	0.2	
24/07/2015 13:45	0.020404193		24/07/2015 13:45	0.2	
24/07/2015 14:00	0.027035801		24/07/2015 14:00	.	
24/07/2015 14:15	0.030487109		24/07/2015 14:15	0.2	
24/07/2015 14:30	0.030487109		24/07/2015 14:30	.	
24/07/2015 14:45	0.022677574		24/07/2015 14:45	0.2	
24/07/2015 15:00	0.030771424		24/07/2015 15:00	.	
24/07/2015 15:15	0.024406951		24/07/2015 15:15	0.6	
24/07/2015 15:30	0.034173071		24/07/2015 15:30	0.4	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
24/07/2015 15:45	0 025787338		24/07/2015 15:45	.	
24/07/2015 16:00	0 036039821		24/07/2015 16:00	0.2	
24/07/2015 16:15	0 032386366		24/07/2015 16:15	0.4	
24/07/2015 16:30	0 046783878		24/07/2015 16:30	0.2	
24/07/2015 16:45	0 058785397		24/07/2015 16:45	0.4	
24/07/2015 17:00	0 042578352		24/07/2015 17:00	.	
24/07/2015 17:15	0 037013153	Ed,Int	24/07/2015 17:15	.	
24/07/2015 17:30	0 031447953		24/07/2015 17:30	.	
24/07/2015 17:45	0 043162989		24/07/2015 17:45	.	
24/07/2015 18:00	0 049008909		24/07/2015 18:00	0.2	
24/07/2015 18:15	0 042109988	Ed,Int	24/07/2015 18:15	0.8	
24/07/2015 18:30	0 035211066		24/07/2015 18:30	0.6	
24/07/2015 18:45	0 040901637		24/07/2015 18:45	1.2	
24/07/2015 19:00	0 044424896		24/07/2015 19:00	1	
24/07/2015 19:15	0 059247881		24/07/2015 19:15	1.8	
24/07/2015 19:30	0.1147646		24/07/2015 19:30	1.6	
24/07/2015 19:45	0 269334212		24/07/2015 19:45	0.8	
24/07/2015 20:00	0 289290462		24/07/2015 20:00	0.4	
24/07/2015 20:15	0 326313276		24/07/2015 20:15	0.4	
24/07/2015 20:30	0.701473898		24/07/2015 20:30	0.6	
24/07/2015 20:45	0 505155704	Ed,Int	24/07/2015 20:45	.	
24/07/2015 21:00	0 308837509	Ed,Int	24/07/2015 21:00	.	
24/07/2015 21:15	0.112519315		24/07/2015 21:15	.	
24/07/2015 21:30	0.126533385	Ed,Int	24/07/2015 21:30	.	
24/07/2015 21:45	0.140547454	Ed,Int	24/07/2015 21:45	.	
24/07/2015 22:00	0.154561524	Ed,Int	24/07/2015 22:00	0.4	
24/07/2015 22:15	0.168575594	Ed,Int	24/07/2015 22:15	2.4	
24/07/2015 22:30	0.182589664	Ed,Int	24/07/2015 22:30	1.6	
24/07/2015 22:45	0.196603734	Ed,Int	24/07/2015 22:45	1	
24/07/2015 23:00	0 210617804	Ed,Int	24/07/2015 23:00	1	
24/07/2015 23:15	0 224631873		24/07/2015 23:15	1	
24/07/2015 23:30	0 523319462	Ed,Int	24/07/2015 23:30	1.4	
24/07/2015 23:45	0 822007051		24/07/2015 23:45	1	
25/07/2015 00:00	0 822826796		25/07/2015 00:00	1	
25/07/2015 00:15	0 850147187		25/07/2015 00:15	1.2	
25/07/2015 00:30	0 975771721		25/07/2015 00:30	1.8	
25/07/2015 00:45	0 938009579		25/07/2015 00:45	1	
25/07/2015 01:00	1 049524149		25/07/2015 01:00	1.4	
25/07/2015 01:15	1.106997531		25/07/2015 01:15	1.8	
25/07/2015 01:30	1.173940384		25/07/2015 01:30	1	
25/07/2015 01:45	1.180049452		25/07/2015 01:45	1.4	
25/07/2015 02:00	1 362648845		25/07/2015 02:00	0.8	
25/07/2015 02:15	1 385932958		25/07/2015 02:15	0.6	
25/07/2015 02:30	1.415109937		25/07/2015 02:30	0.6	
25/07/2015 02:45	1 321359652		25/07/2015 02:45	0.8	
25/07/2015 03:00	1 317158071		25/07/2015 03:00	0.8	
25/07/2015 03:15	1 360460081		25/07/2015 03:15	0.4	
25/07/2015 03:30	1 282118336		25/07/2015 03:30	0.2	
25/07/2015 03:45	1 074514596		25/07/2015 03:45	0.4	
25/07/2015 04:00	1 033953793		25/07/2015 04:00	0.6	
25/07/2015 04:15	0 967840992		25/07/2015 04:15	0.6	
25/07/2015 04:30	0 881171865		25/07/2015 04:30	0.6	
25/07/2015 04:45	0.796662751		25/07/2015 04:45	0.8	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
25/07/2015 05:00	0 831531646		25/07/2015 05:00	0.8	
25/07/2015 05:15	0 884075889		25/07/2015 05:15	0.4	
25/07/2015 05:30	0 892324147		25/07/2015 05:30	0.2	
25/07/2015 05:45	0.725989154	Ed,Int	25/07/2015 05:45	0.2	
25/07/2015 06:00	0 559654161	Ed,Int	25/07/2015 06:00	.	
25/07/2015 06:15	0 393319169		25/07/2015 06:15	.	
25/07/2015 06:30	0 391018769	Ed,Int	25/07/2015 06:30	0.2	
25/07/2015 06:45	0 388718369	Ed,Int	25/07/2015 06:45	.	
25/07/2015 07:00	0 386417969	Ed,Int	25/07/2015 07:00	.	
25/07/2015 07:15	0 384117569	Ed,Int	25/07/2015 07:15	.	
25/07/2015 07:30	0 381817169	Ed,Int	25/07/2015 07:30	.	
25/07/2015 07:45	0.37951677		25/07/2015 07:45	0.2	
25/07/2015 08:00	0.35080724	Ed,Int	25/07/2015 08:00	0.2	
25/07/2015 08:15	0 322097711	Ed,Int	25/07/2015 08:15	0.2	
25/07/2015 08:30	0 293388181	Ed,Int	25/07/2015 08:30	.	
25/07/2015 08:45	0 264678651		25/07/2015 08:45	.	
25/07/2015 09:00	0 225018073		25/07/2015 09:00	.	
25/07/2015 09:15	0 217351256	Ed,Int	25/07/2015 09:15	.	
25/07/2015 09:30	0 209684439	Ed,Int	25/07/2015 09:30	.	
25/07/2015 09:45	0 202017622	Ed,Int	25/07/2015 09:45	.	
25/07/2015 10:00	0.194350805	Ed,Int	25/07/2015 10:00	.	
25/07/2015 10:15	0.186683988		25/07/2015 10:15	.	
25/07/2015 10:30	0.160283528		25/07/2015 10:30	.	
25/07/2015 10:45	0.137773526		25/07/2015 10:45	.	
25/07/2015 11:00	0.162887449		25/07/2015 11:00	.	
25/07/2015 11:15	0.142595775		25/07/2015 11:15	.	
25/07/2015 11:30	0.181228604		25/07/2015 11:30	.	
25/07/2015 11:45	0.125730561		25/07/2015 11:45	.	
25/07/2015 12:00	0.146763965		25/07/2015 12:00	.	
25/07/2015 12:15	0.137150155	Ed,Int	25/07/2015 12:15	.	
25/07/2015 12:30	0.127536344		25/07/2015 12:30	.	
25/07/2015 12:45	0.133498234		25/07/2015 12:45	.	
25/07/2015 13:00	0.108375262		25/07/2015 13:00	.	
25/07/2015 13:15	0 099253784		25/07/2015 13:15	.	
25/07/2015 13:30	0 092174634		25/07/2015 13:30	.	
25/07/2015 13:45	0.103482932		25/07/2015 13:45	.	
25/07/2015 14:00	0.115344729		25/07/2015 14:00	.	
25/07/2015 14:15	0.131485457		25/07/2015 14:15	.	
25/07/2015 14:30	0.13220797		25/07/2015 14:30	.	
25/07/2015 14:45	0 093993494		25/07/2015 14:45	.	
25/07/2015 15:00	0.116244535		25/07/2015 15:00	.	
25/07/2015 15:15	0 090101718		25/07/2015 15:15	.	
25/07/2015 15:30	0.11053974		25/07/2015 15:30	.	
25/07/2015 15:45	0.100812537		25/07/2015 15:45	.	
25/07/2015 16:00	0 074792733		25/07/2015 16:00	.	
25/07/2015 16:15	0.09346972		25/07/2015 16:15	.	
25/07/2015 16:30	0 088536178		25/07/2015 16:30	.	
25/07/2015 16:45	0 083172126		25/07/2015 16:45	.	
25/07/2015 17:00	0 075779646		25/07/2015 17:00	.	
25/07/2015 17:15	0 075286792		25/07/2015 17:15	.	
25/07/2015 17:30	0 053456128		25/07/2015 17:30	.	
25/07/2015 17:45	0 060753809		25/07/2015 17:45	.	
25/07/2015 18:00	0 088346863		25/07/2015 18:00	.	



Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
25/07/2015 18:15	0 078498107		25/07/2015 18:15	.	
25/07/2015 18:30	0 086816955		25/07/2015 18:30	.	
25/07/2015 18:45	0 067322775		25/07/2015 18:45	.	
25/07/2015 19:00	0 085306213		25/07/2015 19:00	.	
25/07/2015 19:15	0 081464428		25/07/2015 19:15	.	
25/07/2015 19:30	0 073211483		25/07/2015 19:30	.	
25/07/2015 19:45	0.104383623		25/07/2015 19:45	.	
25/07/2015 20:00	0 092332047		25/07/2015 20:00	.	
25/07/2015 20:15	0 070369717		25/07/2015 20:15	.	
25/07/2015 20:30	0 076836755		25/07/2015 20:30	.	
25/07/2015 20:45	0 080547995		25/07/2015 20:45	.	
25/07/2015 21:00	0 064923913		25/07/2015 21:00	.	
25/07/2015 21:15	0 059291836		25/07/2015 21:15	.	
25/07/2015 21:30	0 075399585		25/07/2015 21:30	.	
25/07/2015 21:45	0 066682252		25/07/2015 21:45	.	
25/07/2015 22:00	0.05497441		25/07/2015 22:00	.	
25/07/2015 22:15	0 069851916		25/07/2015 22:15	.	
25/07/2015 22:30	0 062288559		25/07/2015 22:30	.	
25/07/2015 22:45	0 061856444	Ed,Int	25/07/2015 22:45	.	
25/07/2015 23:00	0.06142433		25/07/2015 23:00	.	
25/07/2015 23:15	0 068988292		25/07/2015 23:15	.	
25/07/2015 23:30	0 062555986		25/07/2015 23:30	.	
25/07/2015 23:45	0 058996519		25/07/2015 23:45	.	
26/07/2015 00:00	0 062288559		26/07/2015 00:00	.	
26/07/2015 00:15	0 075438112		26/07/2015 00:15	.	
26/07/2015 00:30	0 080563788		26/07/2015 00:30	.	
26/07/2015 00:45	0 070136542		26/07/2015 00:45	.	
26/07/2015 01:00	0 064321997		26/07/2015 01:00	.	
26/07/2015 01:15	0 065369377		26/07/2015 01:15	.	
26/07/2015 01:30	0 063442554		26/07/2015 01:30	.	
26/07/2015 01:45	0 064038338		26/07/2015 01:45	.	
26/07/2015 02:00	0 067815179		26/07/2015 02:00	.	
26/07/2015 02:15	0 065890589		26/07/2015 02:15	.	
26/07/2015 02:30	0 053001456		26/07/2015 02:30	.	
26/07/2015 02:45	0 062268471	Ed,Int	26/07/2015 02:45	.	
26/07/2015 03:00	0 071535485		26/07/2015 03:00	.	
26/07/2015 03:15	0.03773238		26/07/2015 03:15	.	
26/07/2015 03:30	0 0618002		26/07/2015 03:30	.	
26/07/2015 03:45	0 048379316		26/07/2015 03:45	.	
26/07/2015 04:00	0 063389795		26/07/2015 04:00	.	
26/07/2015 04:15	0 052955612	Ed,Int	26/07/2015 04:15	.	
26/07/2015 04:30	0 042521429		26/07/2015 04:30	.	
26/07/2015 04:45	0 046917042		26/07/2015 04:45	.	
26/07/2015 05:00	0 062069548		26/07/2015 05:00	.	
26/07/2015 05:15	0 046555663		26/07/2015 05:15	.	
26/07/2015 05:30	0 048251112	Ed,Int	26/07/2015 05:30	.	
26/07/2015 05:45	0 049946561		26/07/2015 05:45	.	
26/07/2015 06:00	0 060260729		26/07/2015 06:00	.	
26/07/2015 06:15	0 035881787		26/07/2015 06:15	.	
26/07/2015 06:30	0 068229429		26/07/2015 06:30	.	
26/07/2015 06:45	0 041569696		26/07/2015 06:45	.	
26/07/2015 07:00	0 060935827		26/07/2015 07:00	.	
26/07/2015 07:15	0 064726277		26/07/2015 07:15	.	

Date Time	G5 Flow	Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
26/07/2015 07:30	0 054203511	26/07/2015 07:30	.	
26/07/2015 07:45	0 041011328	26/07/2015 07:45	.	
26/07/2015 08:00	0 045360909	26/07/2015 08:00	.	
26/07/2015 08:15	0 046364873	26/07/2015 08:15	.	
26/07/2015 08:30	0 043009683	26/07/2015 08:30	.	
26/07/2015 08:45	0 057583994	26/07/2015 08:45	.	
26/07/2015 09:00	0.107643372	26/07/2015 09:00	.	
26/07/2015 09:15	0 055193138	26/07/2015 09:15	.	
26/07/2015 09:30	0 053807944	26/07/2015 09:30	.	
26/07/2015 09:45	0 041989584	26/07/2015 09:45	.	
26/07/2015 10:00	0 069095815	26/07/2015 10:00	.	
26/07/2015 10:15	0.05243399	26/07/2015 10:15	.	
26/07/2015 10:30	0 043268379	26/07/2015 10:30	.	
26/07/2015 10:45	0 044866609	26/07/2015 10:45	0.4	
26/07/2015 11:00	0 052631556	26/07/2015 11:00	0.4	
26/07/2015 11:15	0 046807846	26/07/2015 11:15	.	
26/07/2015 11:30	0 065249595	26/07/2015 11:30	0.2	
26/07/2015 11:45	0 041954754	26/07/2015 11:45	0.4	
26/07/2015 12:00	0 058455266	26/07/2015 12:00	0.4	
26/07/2015 12:15	0 063750918	26/07/2015 12:15	0.4	
26/07/2015 12:30	0 064641442	26/07/2015 12:30	0.6	
26/07/2015 12:45	0 072907022	26/07/2015 12:45	0.2	
26/07/2015 13:00	0 087986921	26/07/2015 13:00	0.2	
26/07/2015 13:15	0.09642917	26/07/2015 13:15	1.4	
26/07/2015 13:30	0.112003398	26/07/2015 13:30	0.8	
26/07/2015 13:45	0.114013752	26/07/2015 13:45	1.2	
26/07/2015 14:00	0.120385594	26/07/2015 14:00	0.4	
26/07/2015 14:15	0.119112545	26/07/2015 14:15	0.4	
26/07/2015 14:30	0.128718371	26/07/2015 14:30	.	
26/07/2015 14:45	0.131981687	26/07/2015 14:45	.	
26/07/2015 15:00	0.129414904	26/07/2015 15:00	0.2	
26/07/2015 15:15	0.143751713	26/07/2015 15:15	.	
26/07/2015 15:30	0.134695401	26/07/2015 15:30	0.4	
26/07/2015 15:45	0.139682035	26/07/2015 15:45	0.2	
26/07/2015 16:00	0.123527793	26/07/2015 16:00	0.4	
26/07/2015 16:15	0.138576677	26/07/2015 16:15	0.4	
26/07/2015 16:30	0.16000447	26/07/2015 16:30	0.2	
26/07/2015 16:45	0.170131746	26/07/2015 16:45	.	
26/07/2015 17:00	0.166175019	26/07/2015 17:00	0.2	
26/07/2015 17:15	0.171748908	26/07/2015 17:15	0.2	
26/07/2015 17:30	0.162653005	26/07/2015 17:30	0.8	
26/07/2015 17:45	0.181518154	26/07/2015 17:45	0.4	
26/07/2015 18:00	0.162298797	26/07/2015 18:00	0.8	
26/07/2015 18:15	0.189438526	26/07/2015 18:15	0.4	
26/07/2015 18:30	0.19656963	26/07/2015 18:30	0.2	
26/07/2015 18:45	0 234788404	26/07/2015 18:45	.	
26/07/2015 19:00	0 205785483	26/07/2015 19:00	.	
26/07/2015 19:15	0 227077632	26/07/2015 19:15	.	
26/07/2015 19:30	0 204939718	26/07/2015 19:30	0.2	
26/07/2015 19:45	0.189888049	26/07/2015 19:45	.	
26/07/2015 20:00	0.16353838	26/07/2015 20:00	.	
26/07/2015 20:15	0.163344488	26/07/2015 20:15	0.2	
26/07/2015 20:30	0.162430065	26/07/2015 20:30	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
26/07/2015 20:45	0.167310885		26/07/2015 20:45	.	
26/07/2015 21:00	0.158186364		26/07/2015 21:00	.	
26/07/2015 21:15	0.126444661		26/07/2015 21:15	.	
26/07/2015 21:30	0.130549282		26/07/2015 21:30	.	
26/07/2015 21:45	0.130388725		26/07/2015 21:45	.	
26/07/2015 22:00	0.121093484		26/07/2015 22:00	.	
26/07/2015 22:15	0.106437361		26/07/2015 22:15	.	
26/07/2015 22:30	0.130642186		26/07/2015 22:30	.	
26/07/2015 22:45	0.104087634		26/07/2015 22:45	.	
26/07/2015 23:00	0 098711539		26/07/2015 23:00	.	
26/07/2015 23:15	0.104881219	Ed,Int	26/07/2015 23:15	0.2	
26/07/2015 23:30	0.111050898		26/07/2015 23:30	0.2	
26/07/2015 23:45	0 097587823		26/07/2015 23:45	.	
27/07/2015 00:00	0 091845313		27/07/2015 00:00	.	
27/07/2015 00:15	0.11857657		27/07/2015 00:15	.	
27/07/2015 00:30	0.120089448		27/07/2015 00:30	.	
27/07/2015 00:45	0.129102983		27/07/2015 00:45	.	
27/07/2015 01:00	0 093993494		27/07/2015 01:00	.	
27/07/2015 01:15	0 099924393		27/07/2015 01:15	.	
27/07/2015 01:30	0.105889346		27/07/2015 01:30	.	
27/07/2015 01:45	0.108323931		27/07/2015 01:45	.	
27/07/2015 02:00	0.11073683		27/07/2015 02:00	.	
27/07/2015 02:15	0.107684844	Ed,Int	27/07/2015 02:15	0.4	
27/07/2015 02:30	0.104632858		27/07/2015 02:30	0.2	
27/07/2015 02:45	0.101653054		27/07/2015 02:45	0.8	
27/07/2015 03:00	0 088950751		27/07/2015 03:00	0.6	
27/07/2015 03:15	0.132568783		27/07/2015 03:15	0.8	
27/07/2015 03:30	0.111489606		27/07/2015 03:30	.	
27/07/2015 03:45	0.147303457		27/07/2015 03:45	.	
27/07/2015 04:00	0.162430065		27/07/2015 04:00	.	
27/07/2015 04:15	0.174572211		27/07/2015 04:15	.	
27/07/2015 04:30	0.148499529		27/07/2015 04:30	.	
27/07/2015 04:45	0.164406518		27/07/2015 04:45	.	
27/07/2015 05:00	0.15032534		27/07/2015 05:00	.	
27/07/2015 05:15	0.157457069		27/07/2015 05:15	0.2	
27/07/2015 05:30	0.147937987		27/07/2015 05:30	.	
27/07/2015 05:45	0.12378979		27/07/2015 05:45	.	
27/07/2015 06:00	0.125749773		27/07/2015 06:00	.	
27/07/2015 06:15	0.125749773		27/07/2015 06:15	.	
27/07/2015 06:30	0.128918907		27/07/2015 06:30	.	
27/07/2015 06:45	0.124281339		27/07/2015 06:45	.	
27/07/2015 07:00	0.130983068		27/07/2015 07:00	.	
27/07/2015 07:15	0.128168084		27/07/2015 07:15	.	
27/07/2015 07:30	0 084021054		27/07/2015 07:30	.	
27/07/2015 07:45	0.105889346		27/07/2015 07:45	.	
27/07/2015 08:00	0 096975181		27/07/2015 08:00	.	
27/07/2015 08:15	0.119248235		27/07/2015 08:15	.	
27/07/2015 08:30	0.105679665		27/07/2015 08:30	.	
27/07/2015 08:45	0 087415226	Ed,Int	27/07/2015 08:45	.	
27/07/2015 09:00	0 069150787		27/07/2015 09:00	.	
27/07/2015 09:15	0 070148158	Ed,Int	27/07/2015 09:15	.	
27/07/2015 09:30	0 071145528		27/07/2015 09:30	.	
27/07/2015 09:45	0 090212876		27/07/2015 09:45	.	

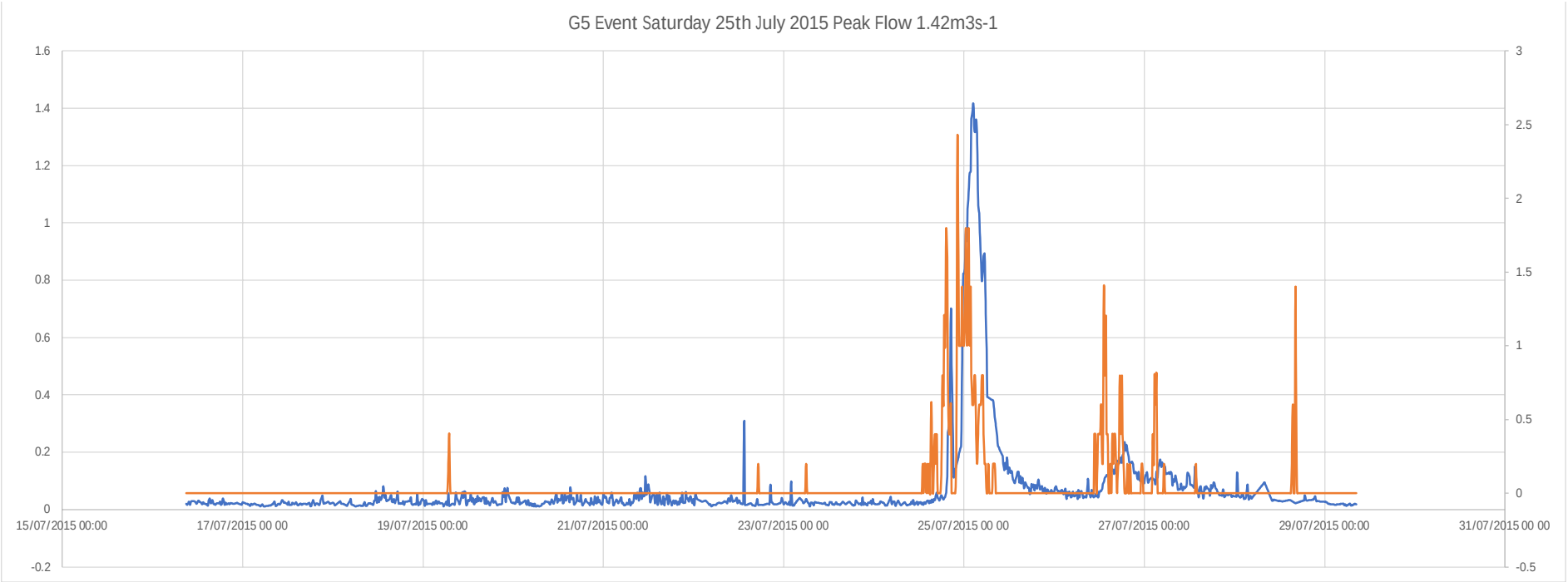
Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
27/07/2015 10:00	0 076995231		27/07/2015 10:00	.	
27/07/2015 10:15	0 066633586		27/07/2015 10:15	.	
27/07/2015 10:30	0 080373038		27/07/2015 10:30	.	
27/07/2015 10:45	0 074429894		27/07/2015 10:45	.	
27/07/2015 11:00	0 077947161	Ed,Int	27/07/2015 11:00	.	
27/07/2015 11:15	0 081464428		27/07/2015 11:15	.	
27/07/2015 11:30	0.128376604		27/07/2015 11:30	.	
27/07/2015 11:45	0.123411767		27/07/2015 11:45	.	
27/07/2015 12:00	0.115063726		27/07/2015 12:00	.	
27/07/2015 12:15	0 086253066		27/07/2015 12:15	.	
27/07/2015 12:30	0.08741944		27/07/2015 12:30	.	
27/07/2015 12:45	0 083843951	Ed,Int	27/07/2015 12:45	.	
27/07/2015 13:00	0 080268463	Ed,Int	27/07/2015 13:00	.	
27/07/2015 13:15	0 076692974		27/07/2015 13:15	.	
27/07/2015 13:30	0.150384771		27/07/2015 13:30	.	
27/07/2015 13:45	0.106854008		27/07/2015 13:45	0.2	
27/07/2015 14:00	0 069558895		27/07/2015 14:00	.	
27/07/2015 14:15	0 063442554		27/07/2015 14:15	.	
27/07/2015 14:30	0 042348684		27/07/2015 14:30	.	
27/07/2015 14:45	0 077990353		27/07/2015 14:45	.	
27/07/2015 15:00	0 080554038		27/07/2015 15:00	.	
27/07/2015 15:15	0 064760074		27/07/2015 15:15	.	
27/07/2015 15:30	0 058234322		27/07/2015 15:30	.	
27/07/2015 15:45	0 038976692		27/07/2015 15:45	.	
27/07/2015 16:00	0 077995683		27/07/2015 16:00	.	
27/07/2015 16:15	0 070460004		27/07/2015 16:15	.	
27/07/2015 16:30	0.08097842		27/07/2015 16:30	.	
27/07/2015 16:45	0 074983356		27/07/2015 16:45	.	
27/07/2015 17:00	0.07249997		27/07/2015 17:00	.	
27/07/2015 17:15	0 066533579		27/07/2015 17:15	.	
27/07/2015 17:30	0 048741706		27/07/2015 17:30	.	
27/07/2015 17:45	0 085186417		27/07/2015 17:45	.	
27/07/2015 18:00	0 074234552		27/07/2015 18:00	.	
27/07/2015 18:15	0 080522293		27/07/2015 18:15	.	
27/07/2015 18:30	0 094807606		27/07/2015 18:30	.	
27/07/2015 18:45	0 086316967		27/07/2015 18:45	.	
27/07/2015 19:00	0 073264119		27/07/2015 19:00	.	
27/07/2015 19:15	0 070235382		27/07/2015 19:15	.	
27/07/2015 19:30	0 063159891		27/07/2015 19:30	.	
27/07/2015 19:45	0 057631494		27/07/2015 19:45	.	
27/07/2015 20:00	0 050125846		27/07/2015 20:00	.	
27/07/2015 20:15	0 050064885	Ed,Int	27/07/2015 20:15	.	
27/07/2015 20:30	0 050003924		27/07/2015 20:30	.	
27/07/2015 20:45	0 048005569		27/07/2015 20:45	.	
27/07/2015 21:00	0 070511173		27/07/2015 21:00	.	
27/07/2015 21:15	0 043662417		27/07/2015 21:15	.	
27/07/2015 21:30	0.04695371	Ed,Int	27/07/2015 21:30	.	
27/07/2015 21:45	0 050245003		27/07/2015 21:45	.	
27/07/2015 22:00	0 054792808		27/07/2015 22:00	.	
27/07/2015 22:15	0 049493668		27/07/2015 22:15	.	
27/07/2015 22:30	0.05243399		27/07/2015 22:30	.	
27/07/2015 22:45	0 053703339	Ed,Int	27/07/2015 22:45	.	
27/07/2015 23:00	0 054972687		27/07/2015 23:00	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
27/07/2015 23:15	0 043895991		27/07/2015 23:15	.	
27/07/2015 23:30	0 048379316		27/07/2015 23:30	.	
27/07/2015 23:45	0 047286886	Ed,Int	27/07/2015 23:45	.	
28/07/2015 00:00	0 046194456		28/07/2015 00:00	.	
28/07/2015 00:15	0 045626252	Ed,Int	28/07/2015 00:15	.	
28/07/2015 00:30	0 045058049		28/07/2015 00:30	.	
28/07/2015 00:45	0.129666923		28/07/2015 00:45	.	
28/07/2015 01:00	0 050502914		28/07/2015 01:00	.	
28/07/2015 01:15	0 046088267	Ed,Int	28/07/2015 01:15	.	
28/07/2015 01:30	0.04167362		28/07/2015 01:30	.	
28/07/2015 01:45	0.04395931		28/07/2015 01:45	.	
28/07/2015 02:00	0 053021969		28/07/2015 02:00	.	
28/07/2015 02:15	0 054572793		28/07/2015 02:15	.	
28/07/2015 02:30	0 037438467		28/07/2015 02:30	.	
28/07/2015 02:45	0 038389628	Ed,Int	28/07/2015 02:45	.	
28/07/2015 03:00	0.03934079		28/07/2015 03:00	.	
28/07/2015 03:15	0 062927882	Ed,Int	28/07/2015 03:15	.	
28/07/2015 03:30	0 086514974		28/07/2015 03:30	.	
28/07/2015 03:45	0 035575207		28/07/2015 03:45	.	
28/07/2015 04:00	0 038055118		28/07/2015 04:00	.	
28/07/2015 04:15	0 048266454		28/07/2015 04:15	.	
28/07/2015 04:30	0.03773771		28/07/2015 04:30	.	
28/07/2015 04:45	0 041824703	Ed,Int	28/07/2015 04:45	.	
28/07/2015 05:00	0 045911696	Ed,Int	28/07/2015 05:00	.	
28/07/2015 05:15	0.04999869	Ed,Int	28/07/2015 05:15	.	
28/07/2015 05:30	0 054085683	Ed,Int	28/07/2015 05:30	.	
28/07/2015 05:45	0 058172676	Ed,Int	28/07/2015 05:45	.	
28/07/2015 06:00	0 062259669	Ed,Int	28/07/2015 06:00	.	
28/07/2015 06:15	0 066346662	Ed,Int	28/07/2015 06:15	.	
28/07/2015 06:30	0 070433655	Ed,Int	28/07/2015 06:30	.	
28/07/2015 06:45	0 074520649	Ed,Int	28/07/2015 06:45	.	
28/07/2015 07:00	0 078607642	Ed,Int	28/07/2015 07:00	.	
28/07/2015 07:15	0 082694635	Ed,Int	28/07/2015 07:15	.	
28/07/2015 07:30	0 086781628	Ed,Int	28/07/2015 07:30	.	
28/07/2015 07:45	0 090868621	Ed,Int	28/07/2015 07:45	.	
28/07/2015 08:00	0 094955614		28/07/2015 08:00	.	
28/07/2015 08:15	0 086947834	Ed,Int	28/07/2015 08:15	.	
28/07/2015 08:30	0 078940054	Ed,Int	28/07/2015 08:30	.	
28/07/2015 08:45	0 070932274	Ed,Int	28/07/2015 08:45	.	
28/07/2015 09:00	0 062924494	Ed,Int	28/07/2015 09:00	.	
28/07/2015 09:15	0 054916714	Ed,Int	28/07/2015 09:15	.	
28/07/2015 09:30	0 046908934	Ed,Int	28/07/2015 09:30	.	
28/07/2015 09:45	0 038901154	Ed,Int	28/07/2015 09:45	.	
28/07/2015 10:00	0 030893374		28/07/2015 10:00	.	
28/07/2015 10:15	0 031732624		28/07/2015 10:15	.	
28/07/2015 10:30	0 034669284		28/07/2015 10:30	.	
28/07/2015 10:45	0.03363034	Ed,Int	28/07/2015 10:45	.	
28/07/2015 11:00	0 032591397	Ed,Int	28/07/2015 11:00	.	
28/07/2015 11:15	0 031552454	Ed,Int	28/07/2015 11:15	.	
28/07/2015 11:30	0.03051351	Ed,Int	28/07/2015 11:30	.	
28/07/2015 11:45	0 029474567		28/07/2015 11:45	.	
28/07/2015 12:00	0 030335029		28/07/2015 12:00	.	
28/07/2015 12:15	0 029611002	Ed,Int	28/07/2015 12:15	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
28/07/2015 12:30	0 028886976	Ed,Int	28/07/2015 12:30	.	
28/07/2015 12:45	0 028162949		28/07/2015 12:45	.	
28/07/2015 13:00	0 028863488	Ed,Int	28/07/2015 13:00	.	
28/07/2015 13:15	0 029564026	Ed,Int	28/07/2015 13:15	.	
28/07/2015 13:30	0 030264565	Ed,Int	28/07/2015 13:30	.	
28/07/2015 13:45	0 030965104	Ed,Int	28/07/2015 13:45	.	
28/07/2015 14:00	0 031665642	Ed,Int	28/07/2015 14:00	.	
28/07/2015 14:15	0 032366181	Ed,Int	28/07/2015 14:15	.	
28/07/2015 14:30	0 033066719	Ed,Int	28/07/2015 14:30	.	
28/07/2015 14:45	0 033767258		28/07/2015 14:45	.	
28/07/2015 15:00	0 031729838	Ed,Int	28/07/2015 15:00	.	
28/07/2015 15:15	0 029692418	Ed,Int	28/07/2015 15:15	0.2	
28/07/2015 15:30	0 027654998	Ed,Int	28/07/2015 15:30	0.6	
28/07/2015 15:45	0 025617577	Ed,Int	28/07/2015 15:45	.	
28/07/2015 16:00	0 023580157	Ed,Int	28/07/2015 16:00	.	
28/07/2015 16:15	0 021542737		28/07/2015 16:15	1.4	
28/07/2015 16:30	0 022886453		28/07/2015 16:30	0.2	
28/07/2015 16:45	0 024072757	Ed,Int	28/07/2015 16:45	.	
28/07/2015 17:00	0.02525906		28/07/2015 17:00	.	
28/07/2015 17:15	0 026381816	Ed,Int	28/07/2015 17:15	.	
28/07/2015 17:30	0 027504572	Ed,Int	28/07/2015 17:30	.	
28/07/2015 17:45	0 028627327	Ed,Int	28/07/2015 17:45	.	
28/07/2015 18:00	0 029750083	Ed,Int	28/07/2015 18:00	.	
28/07/2015 18:15	0 030872839	Ed,Int	28/07/2015 18:15	.	
28/07/2015 18:30	0 031995594		28/07/2015 18:30	.	
28/07/2015 18:45	0.04892896		28/07/2015 18:45	.	
28/07/2015 19:00	0 035560513		28/07/2015 19:00	.	
28/07/2015 19:15	0 031424573		28/07/2015 19:15	.	
28/07/2015 19:30	0 031887549	Ed,Int	28/07/2015 19:30	.	
28/07/2015 19:45	0 032350525	Ed,Int	28/07/2015 19:45	.	
28/07/2015 20:00	0 0328135	Ed,Int	28/07/2015 20:00	.	
28/07/2015 20:15	0 033276476	Ed,Int	28/07/2015 20:15	.	
28/07/2015 20:30	0 033739451	Ed,Int	28/07/2015 20:30	.	
28/07/2015 20:45	0 034202427	Ed,Int	28/07/2015 20:45	.	
28/07/2015 21:00	0 034665403		28/07/2015 21:00	.	
28/07/2015 21:15	0 040209386	Ed,Int	28/07/2015 21:15	.	
28/07/2015 21:30	0.04575337		28/07/2015 21:30	.	
28/07/2015 21:45	0 029498428		28/07/2015 21:45	.	
28/07/2015 22:00	0 029204356	Ed,Int	28/07/2015 22:00	.	
28/07/2015 22:15	0 028910284	Ed,Int	28/07/2015 22:15	.	
28/07/2015 22:30	0 028616212	Ed,Int	28/07/2015 22:30	.	
28/07/2015 22:45	0.02832214	Ed,Int	28/07/2015 22:45	.	
28/07/2015 23:00	0 028028068	Ed,Int	28/07/2015 23:00	.	
28/07/2015 23:15	0 027733997	Ed,Int	28/07/2015 23:15	.	
28/07/2015 23:30	0 027439925	Ed,Int	28/07/2015 23:30	.	
28/07/2015 23:45	0 027145853	Ed,Int	28/07/2015 23:45	.	
29/07/2015 00:00	0 026851781	Ed,Int	29/07/2015 00:00	.	
29/07/2015 00:15	0 026557709	Ed,Int	29/07/2015 00:15	.	
29/07/2015 00:30	0 026263638		29/07/2015 00:30	.	
29/07/2015 00:45	0 022849646	Ed,Int	29/07/2015 00:45	.	
29/07/2015 01:00	0 019435654		29/07/2015 01:00	.	
29/07/2015 01:15	0 019291484	Ed,Int	29/07/2015 01:15	.	
29/07/2015 01:30	0 019147314	Ed,Int	29/07/2015 01:30	.	

Date Time	G5 Flow		Date Time	Thorpeness RF mm	Daily Rainfall Totals mm
29/07/2015 01:45	0.019003145	Ed,Int	29/07/2015 01:45	.	
29/07/2015 02:00	0.018858975	Ed,Int	29/07/2015 02:00	.	
29/07/2015 02:15	0.018714805		29/07/2015 02:15	.	
29/07/2015 02:30	0.017469075		29/07/2015 02:30	.	
29/07/2015 02:45	0.017173906	Ed,Int	29/07/2015 02:45	.	
29/07/2015 03:00	0.016878738		29/07/2015 03:00	.	
29/07/2015 03:15	0.017367216	Ed,Int	29/07/2015 03:15	.	
29/07/2015 03:30	0.017855695	Ed,Int	29/07/2015 03:30	.	
29/07/2015 03:45	0.018344174	Ed,Int	29/07/2015 03:45	.	
29/07/2015 04:00	0.018832652	Ed,Int	29/07/2015 04:00	.	
29/07/2015 04:15	0.019321131	Ed,Int	29/07/2015 04:15	.	
29/07/2015 04:30	0.01980961	Ed,Int	29/07/2015 04:30	.	
29/07/2015 04:45	0.020298088	Ed,Int	29/07/2015 04:45	.	
29/07/2015 05:00	0.020786567		29/07/2015 05:00	.	
29/07/2015 05:15	0.014819142		29/07/2015 05:15	.	
29/07/2015 05:30	0.018065026		29/07/2015 05:30	.	
29/07/2015 05:45	0.013328304		29/07/2015 05:45	.	
29/07/2015 06:00	0.015083324	Ed,Int	29/07/2015 06:00	.	
29/07/2015 06:15	0.016838345	Ed,Int	29/07/2015 06:15	.	
29/07/2015 06:30	0.018593366	Ed,Int	29/07/2015 06:30	.	
29/07/2015 06:45	0.020348386		29/07/2015 06:45	.	
29/07/2015 07:00	0.013669618		29/07/2015 07:00	.	
29/07/2015 07:15	0.014016193		29/07/2015 07:15	.	
29/07/2015 07:30	0.015764968	Ed,Int	29/07/2015 07:30	.	
29/07/2015 07:45	0.017513744		29/07/2015 07:45	.	
29/07/2015 08:00	0.020187159		29/07/2015 08:00	.	
29/07/2015 08:15	0.018881684	Ed,Int	29/07/2015 08:15	.	
29/07/2015 08:30	0.01757621		29/07/2015 08:30	.	

Date Time	G5 Flow	Date Time	Thorpeness RF mm	Daily Rainfall Totals mm



SAAR	592	mm
AREA	5.04	Km2

Catchment Area = Combined areas of LEIS_ABBEY and LEIS_LEISTON

SMD on the first day of the event 0mm
Soil conditions were saturated prior to the event
approx. 0 mm of free capac ty in the so l column
Weekly Soil Moisture Deficit data sourcedfrom the Met Office

Weekly average ending	**SMD mm**	
21-Jul-15	116.4	mm
28-Jul-15	78.8	mm

Source of Rainfall event data.

Gauge	**Easting**	**Northing**	**Distance from Catchment Centroid (m)**	**Reciprocal**	**Weighting**
Benhall	38166	60602	20912.0		0.00000
Soham	23243	62717	6550.0		0.00000
Thorpeness	60012	78834	3636.0	0.00028	1.00000
			Total	0.00028	1.00000

TBR RG

Daily RF totals 9am 9am	Benhall	Soham	Thorpeness
Date	Total RF (mm)	Total RF (mm)	Total RF (mm)
23/07/2015		0	0
22/07/2015		0	0.4
21/07/2015		0	0
20/07/2015		0	0
19/07/2015		0	0
Total API5 RF			0.4

Rainall Event Depth P (mm)	42.6
Event duration (hours)	19.25

			Daily Rainfall totals mm				
RF Gauge	**SAAR**	**Weight**	**19/07/2015**	**20/07/2015**	**21/07/2015**	**22/07/2015**	**23/07/2015**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0	0	0	0.4	0
Average Daily rainfa l totals			0	0	0	0.4	0

Gauge	**SAAR**	**Weight**	**19/07/2015**	**20/07/2015**	**21/07/2015**	**22/07/2015**	**23/07/2015**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0	0	0	0.000675676	0

Gauge	**SAAR**	**Weight**	**19/07/2015**	**20/07/2015**	**21/07/2015**	**22/07/2015**	**23/07/2015**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.0000	0	0	0	0.00675676	0

Gauge	**SAAR**	**Weight**	**19/07/2015**	**20/07/2015**	**21/07/2015**	**22/07/2015**	**23/07/2015**
Benhall	592	0.0000	0	0	0	0	0
Soham	592	0.0000	0	0	0	0	0
Thorpeness	592	1.00000	0	0	0	0.4	0
Catchment Average Antecedent RF mm			0	0	0	0.4	0

Date	**Catchment Average Antecedent Rainfall (mm)**	
19/07/2015	0.00	d-5
20/07/2015	0.00	d-4
21/07/2015	0.00	d-3
22/07/2015	0.40	d-2
23/07/2015	0.00	d-1

API5
0.14 mm 0.141421356 mm / day

CWI Prior to Event February 2014 Event at G5
CWI 125 + API15 - SMD
SMD 116.4 mm
CWI 8.741421356 mm

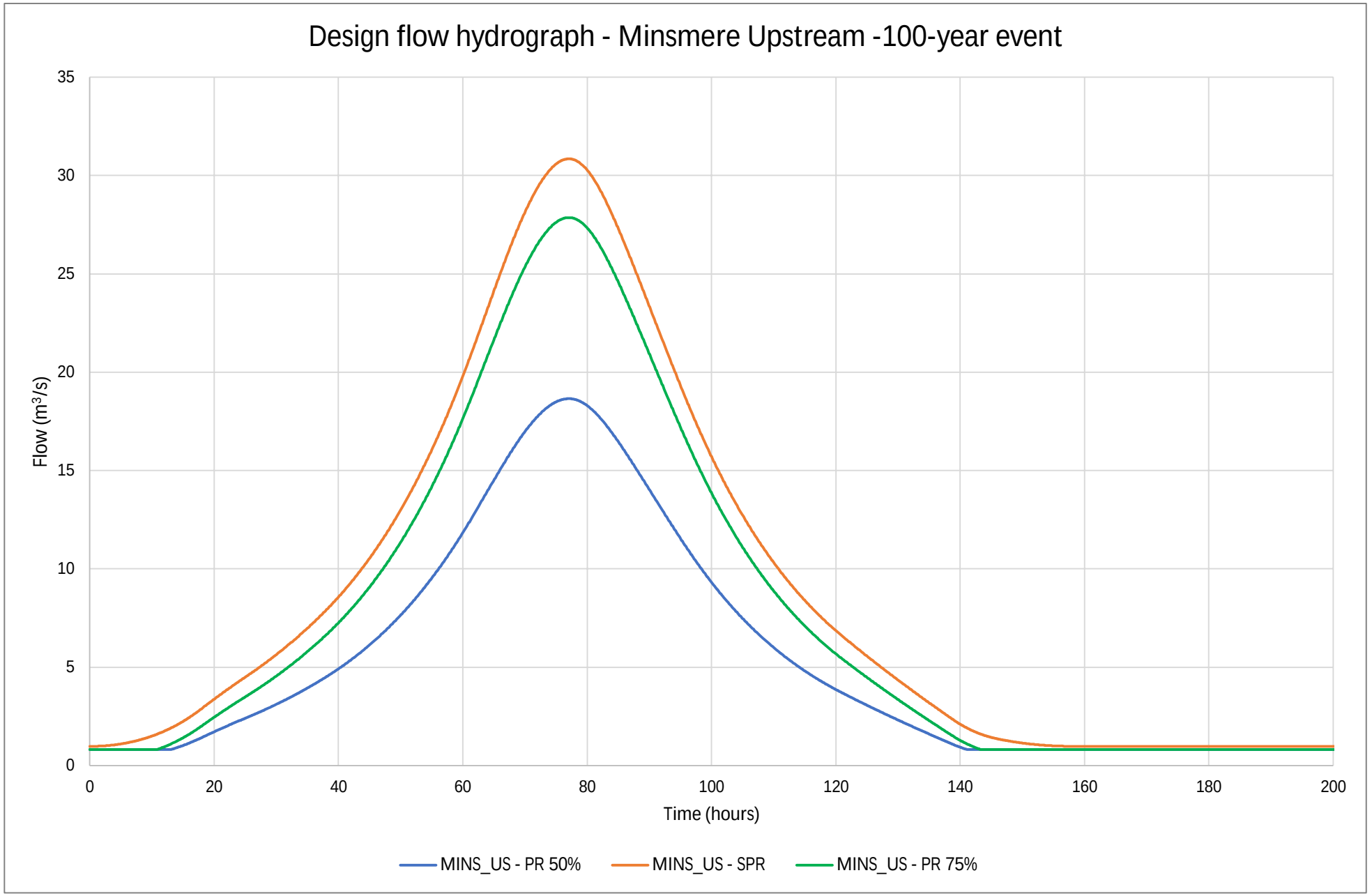
FEH Parameter										
SPR	52.1	%						**URBEXT2000**		As URBEXT2000 value is essentially rural the PR is the same as the PRrural value
PRrural	23.88	%			P=Storm Depth	42.6	mm	**PR**	24	taken from PR calculations sheet using Thorpeness TBR RG record
DPRrain	0.88	%			SPR	52.1		**DPRrain**	0	DPRrain is 0, as P<40mm
DPRcwi	-29.1	CWI	8.741421					**DPRcwi**	-29.1	
As there is no urban area in the catchment i.e. URBEXT2000 is essentially rural PR = PRrural								**SPR**	52.1	
PR	24.1	%						**DPRrain**	0.88	
PRrural	23.9	%						**P**	42.6	
CWI	8.7	mm						**CWI**	8.7	
BF	0.00001		Baseflow equation taken from FEH					**SPR**	52.1	
	-1254							**PR**	24.1	
	1778.5		524.5	0.005245						
AREA	5.04		**0.026435**	m3s-1				**SPRHOST**	24.27	from FEH Catchment descriptors & SPRHOST is the same as SPRcds
SPR	52.1							**Duration (hours)**	19.25	
SPR =	PR_{RURAL} - DPR_{CWI} - DPR_{RAIN}									
SPR =	52.1									
PRrural	23.9									

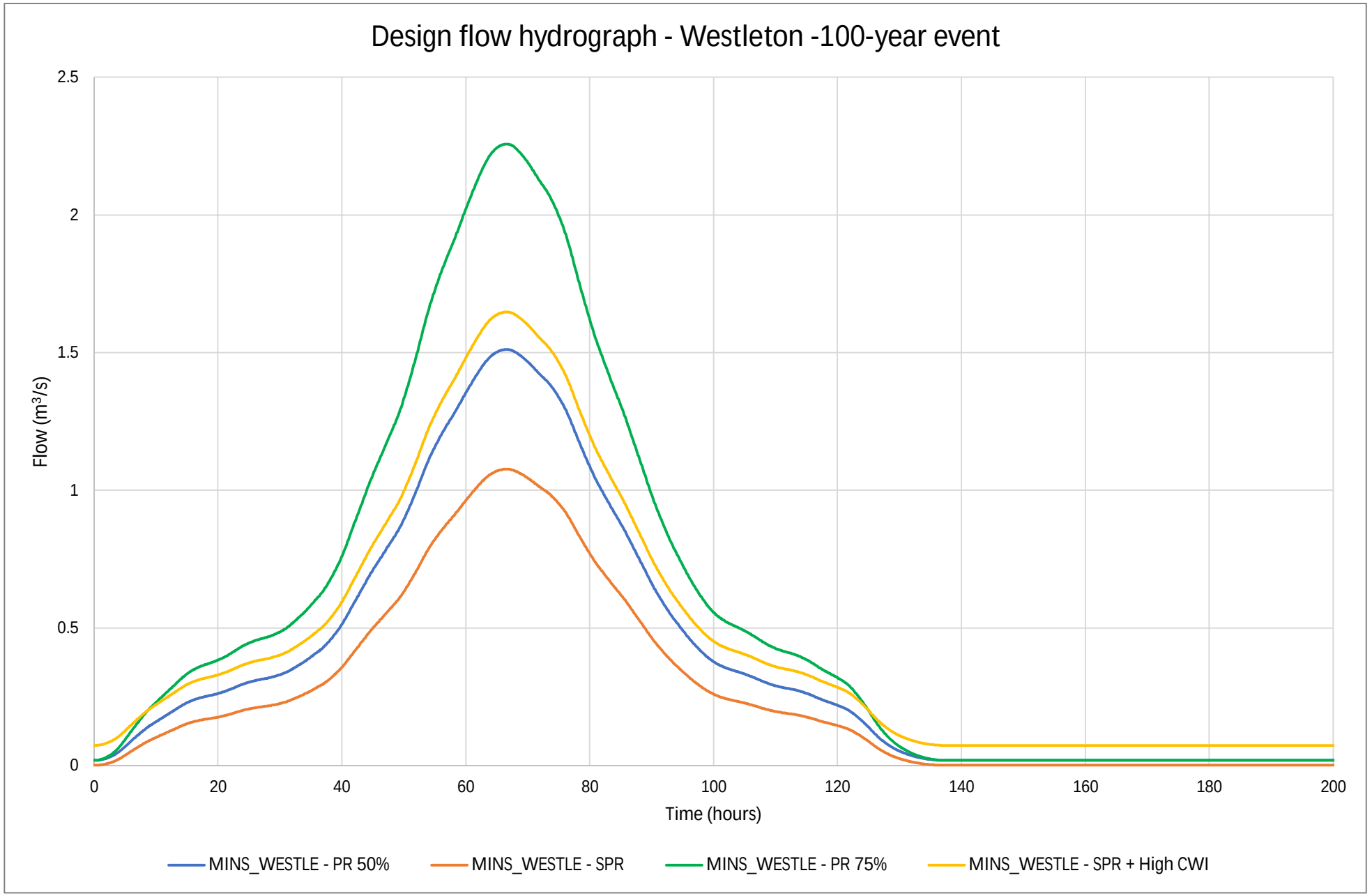
Calculation of SPR

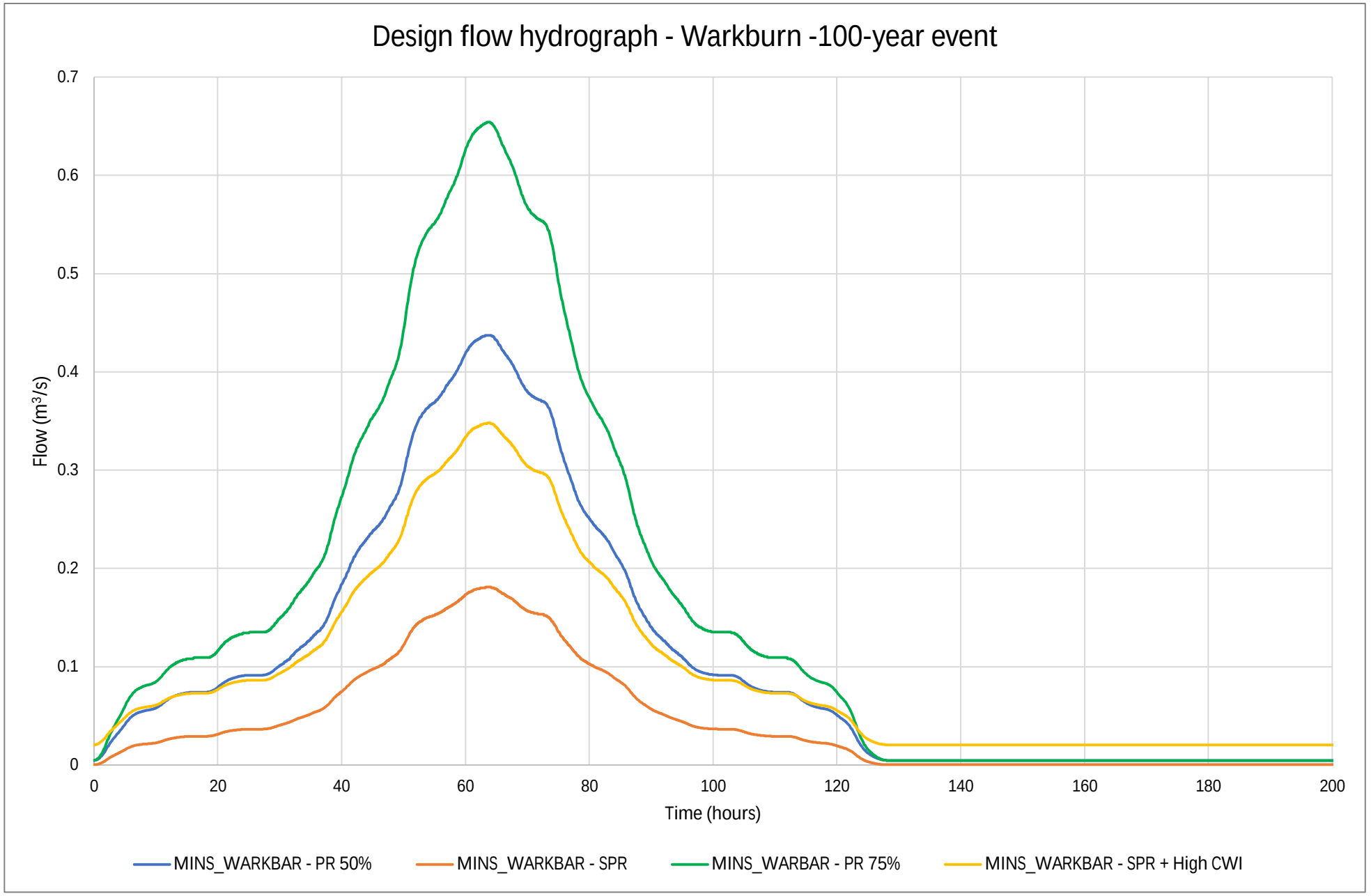
Event start	Event end	Storm Duration	API5	SMD	CWI	PRRURAL	DPRCWI	DPRRAIN	SPR	$PR_{observed}$	FEH SPRHOST
24-Jul-15	25-Jul-15	19.25	0.14	116.40	8.74	23.88	-29.06	0.88	52.07	24.00	24.27

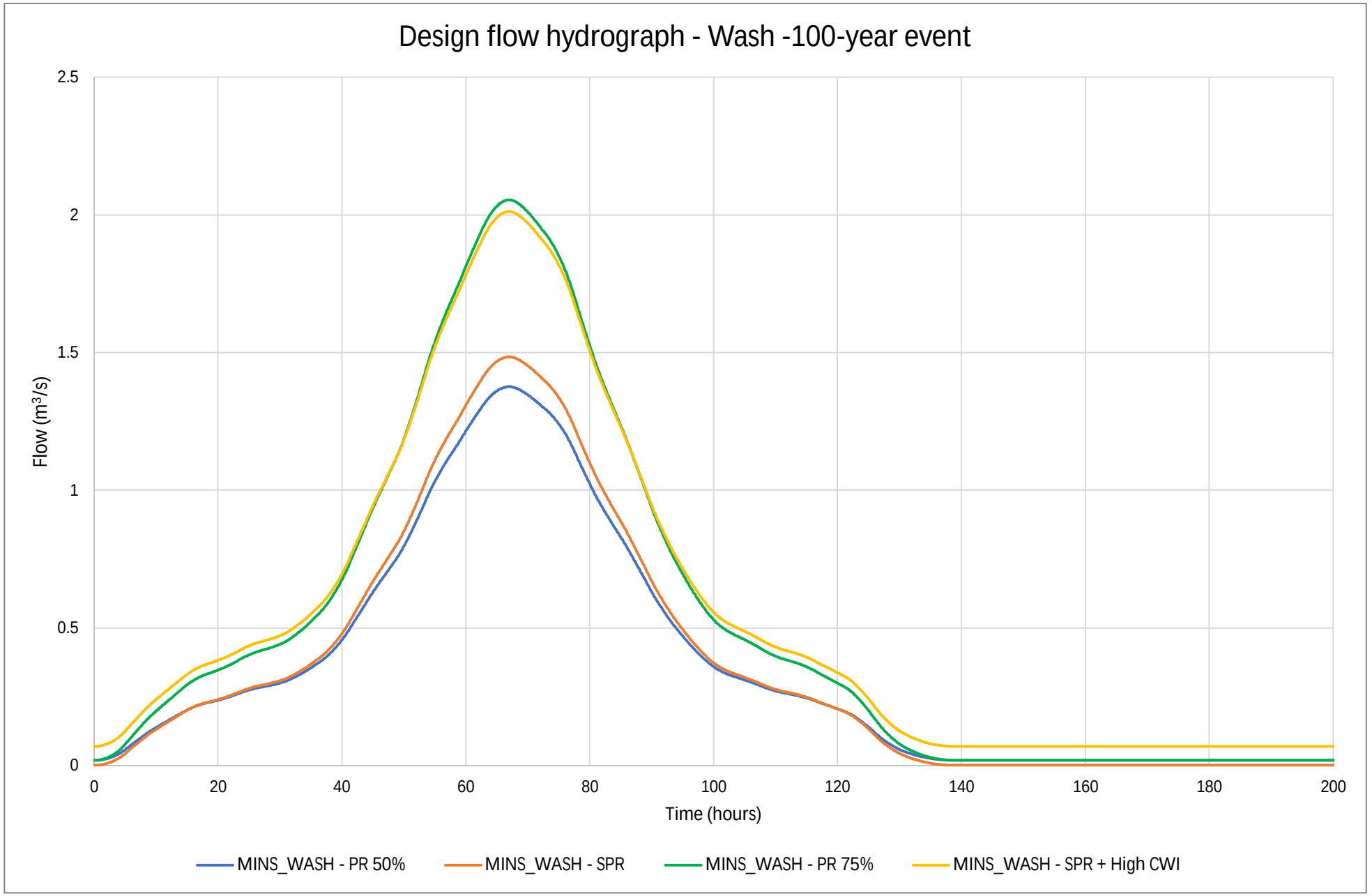
Site	Sub-catchment	SPRg.cds	SPRg.obs	SPRs.cds	SPRs.adj
Sizewell	Sizewell	24.3	44.8	14.5	26.8
Leis Lovers	Leis Lovers	24.3	44.8	18.2	33.6
Leis Abbey	Leis Abbey	24.3	44.8	27.8	51.4
Leiston	Leiston	24.3	44.8	20.7	38.2
Leis Upper	Leis Upper	24.3	44.8	17.1	31.5
Mins_Eastbridge	Mins_Eastbridge	24.3	44.8	13.3	24.5
Mins Westleton	Mins Westleton	24.3	44.8	21.9	40.5
Mins Docwra	Mins Docwra	24.3	44.8	14.4	26.6
Mins Warkburn	Mins Warkburn	24.3	44.8	14.0	25.9
Mins Scott	Mins Scott	24.3	44.8	13.5	25.0
Mins Theberton	Mins Theberton	24.3	44.8	29.5	54.5
Mins Wash	Mins Wash	24.3	44.8	32.4	59.9
Mins Potters	Mins Potters	24.3	44.8	25.3	46.8
				Mean	37.3

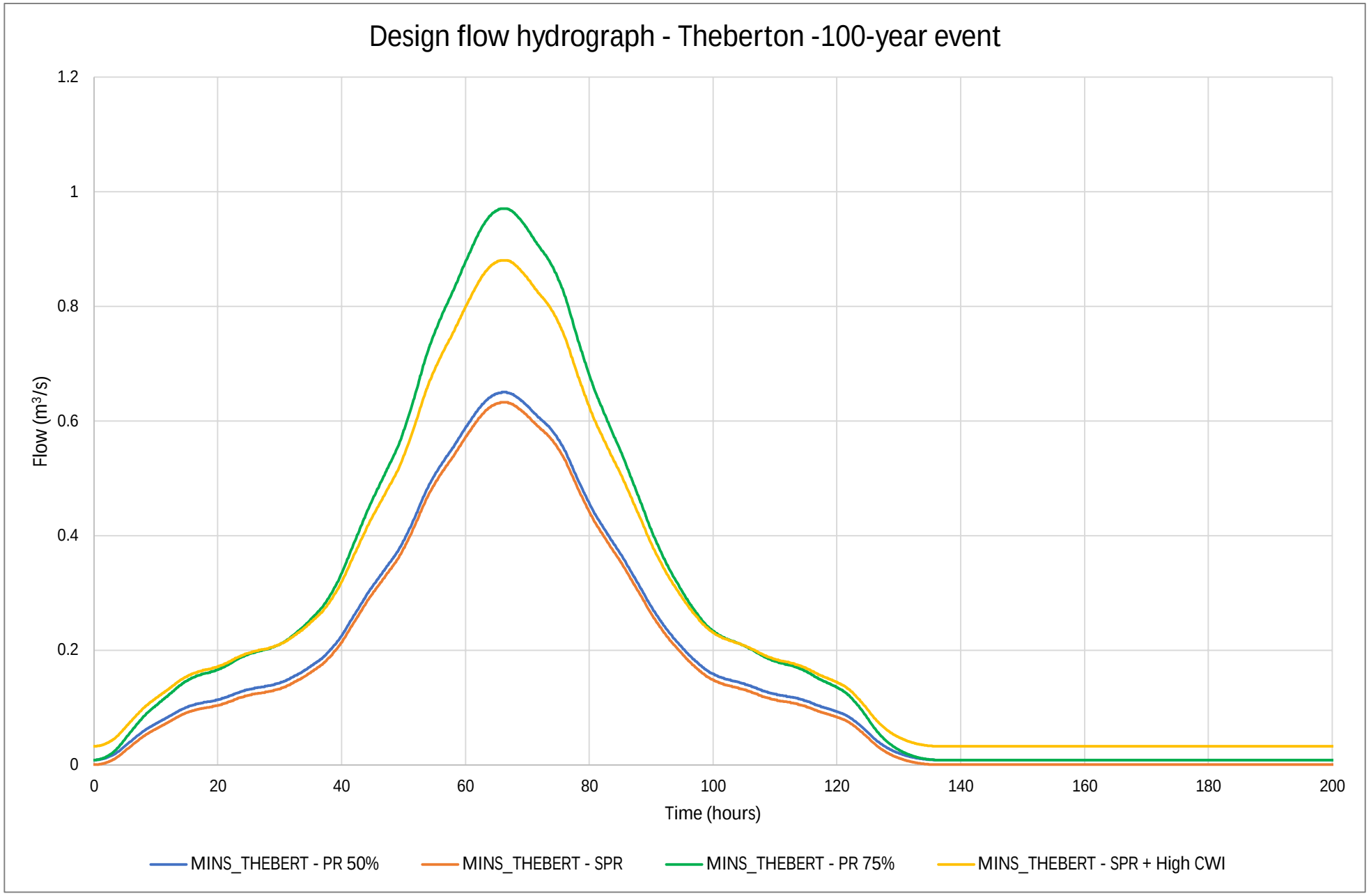
APPENDIX D: COMPARISON OF FLOW HYDROGRAPHS DERIVED WITH PR AND SPR

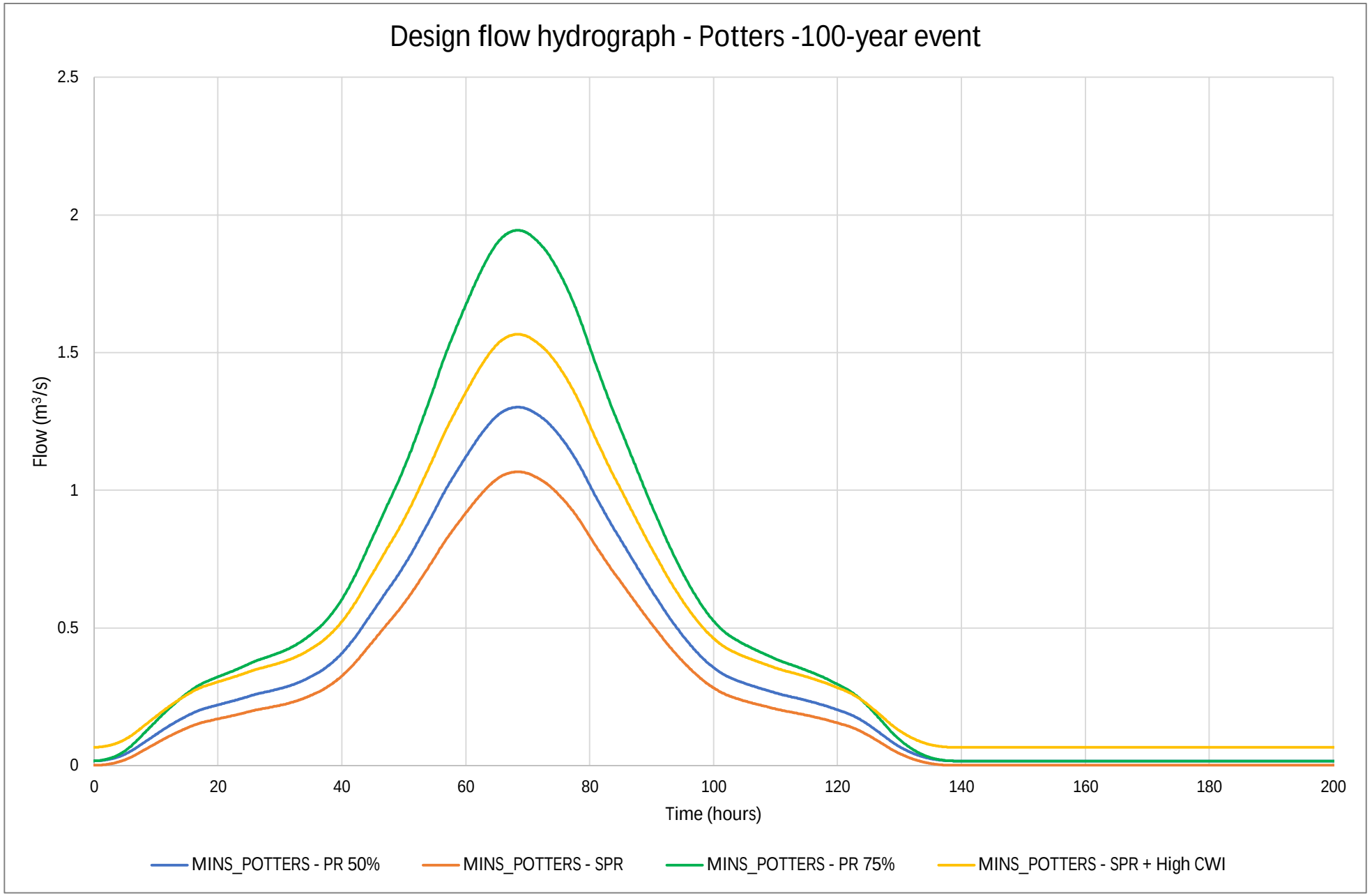

Design flow hydrograph - Minsmere Upstream -100-year event
Flow (m3/s)
0
5
10
15
20
25
30
35
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_US - PR 50%
MINS_US - SPR
MINS_US - PR 75%

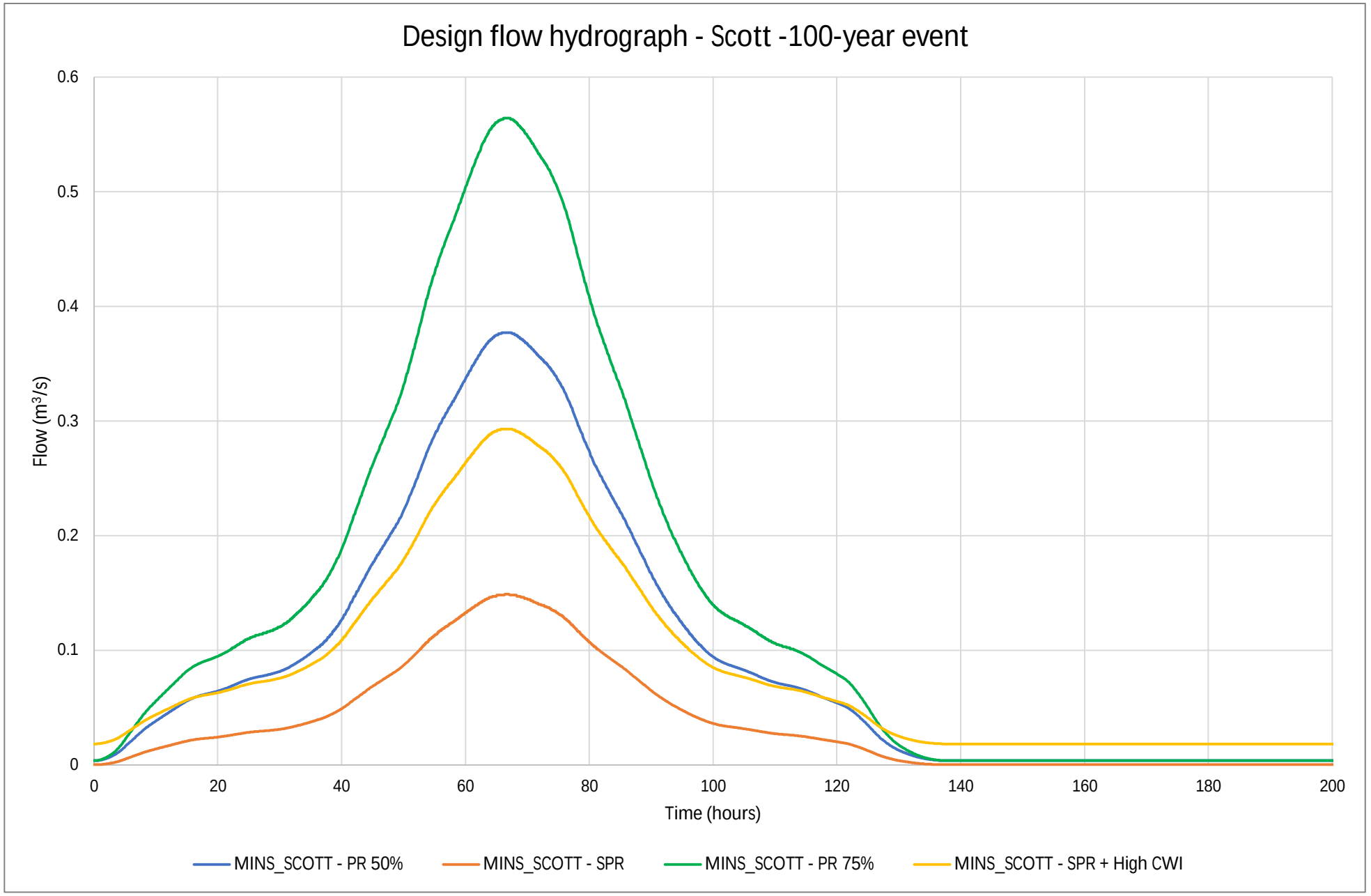

Design flow hydrograph - Westleton -100-year event
Flow (m3/s)
2.5
2
1.5
1
0.5
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_WESTLE - PR 50%
MINS_WESTLE - SPR
MINS_WESTLE - PR 75%
MINS_WESTLE - SPR + High CWI

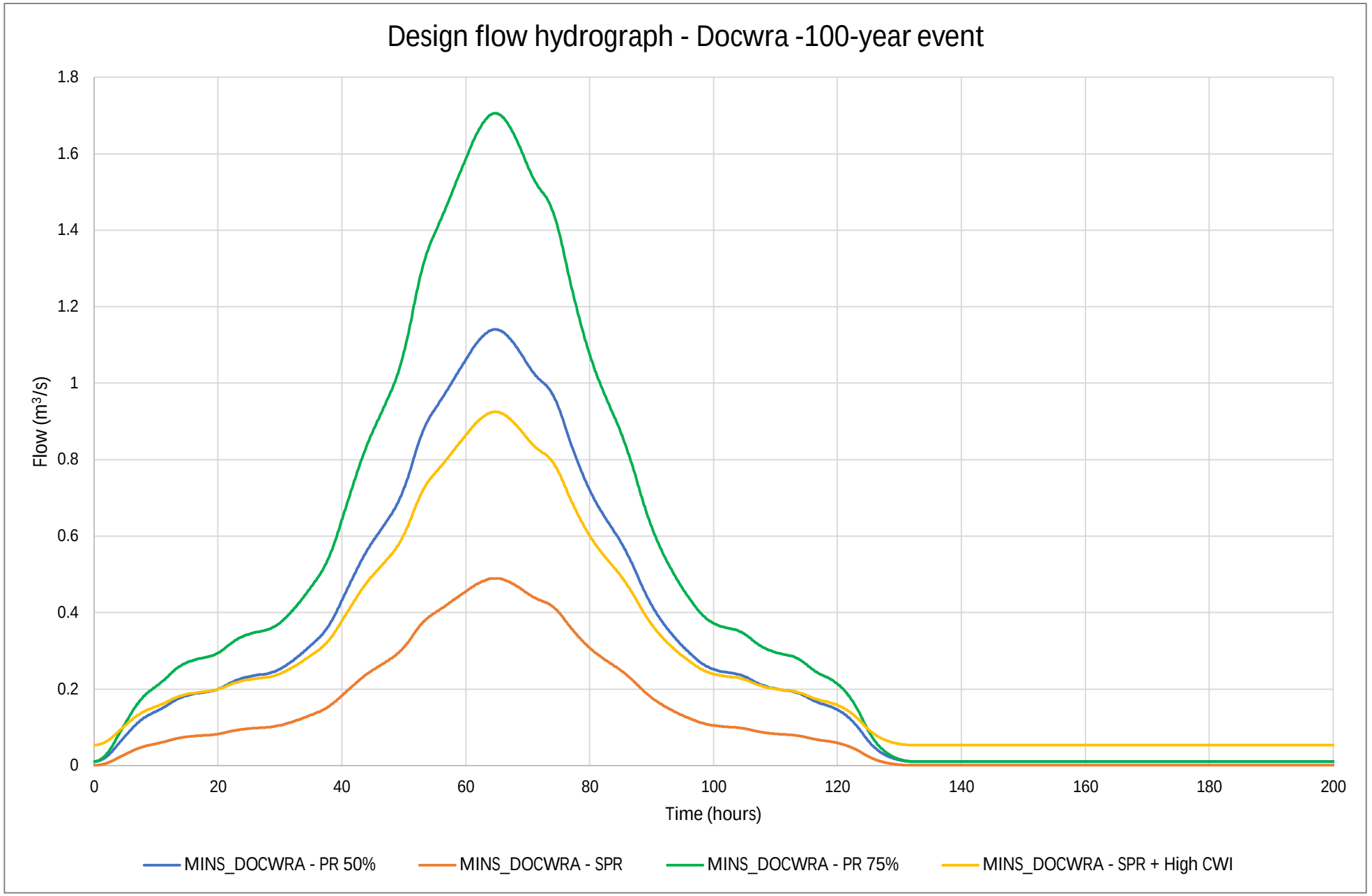

Design flow hydrograph - Warkburn -100-year event
Flow (m3/s)
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_WARKBAR - PR 50%
MINS_WARKBAR - SPR
MINS_WARBAR - PR 75%
MINS_WARKBAR - SPR + High CWI

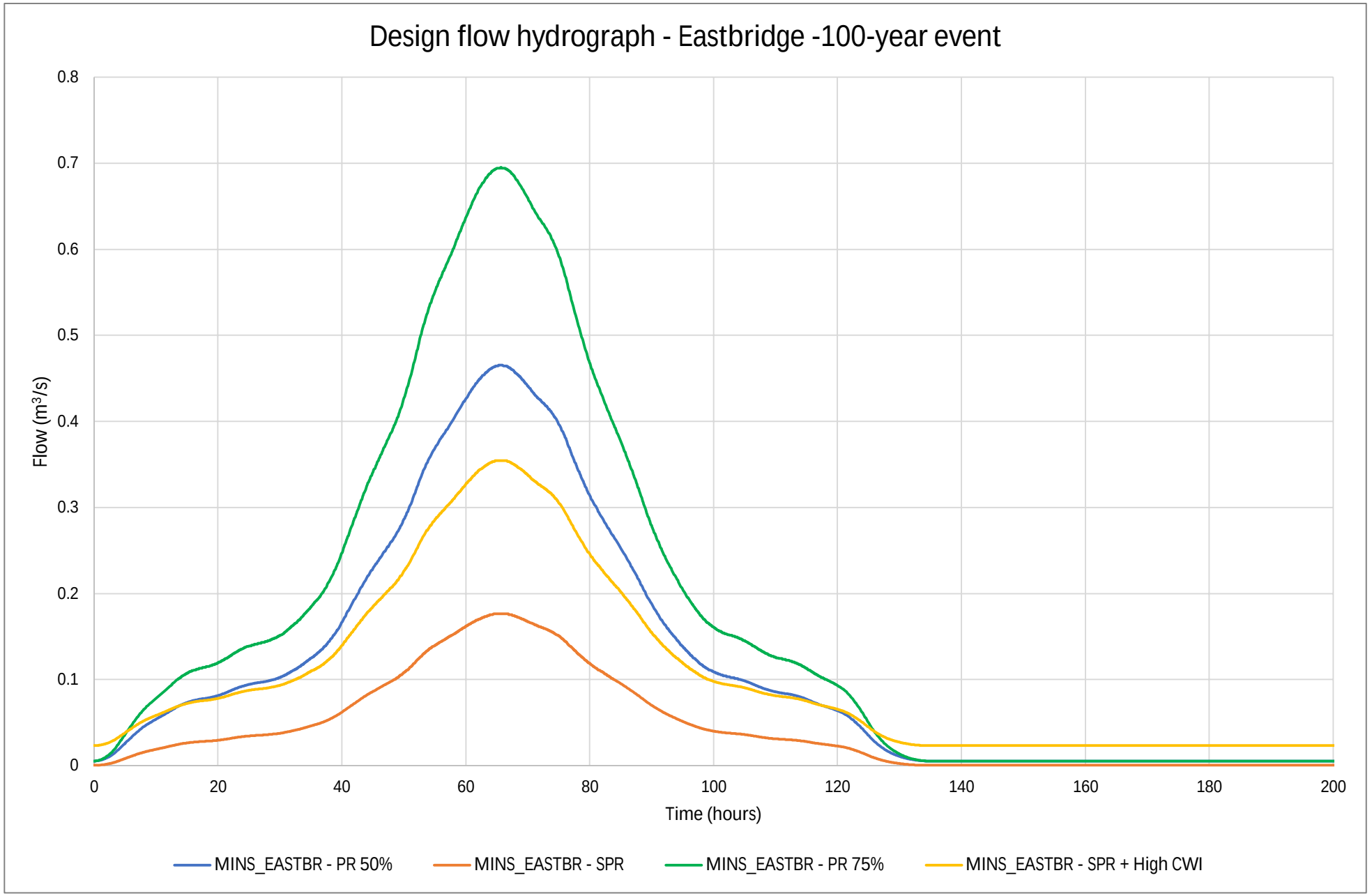

Design flow hydrograph - Wash -100-year event
Flow (m3/s)
2.5
2
1.5
1
0.5
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_WASH - PR 50%
MINS_WASH - SPR
MINS_WASH - PR 75%
MINS_WASH - SPR + High CWI

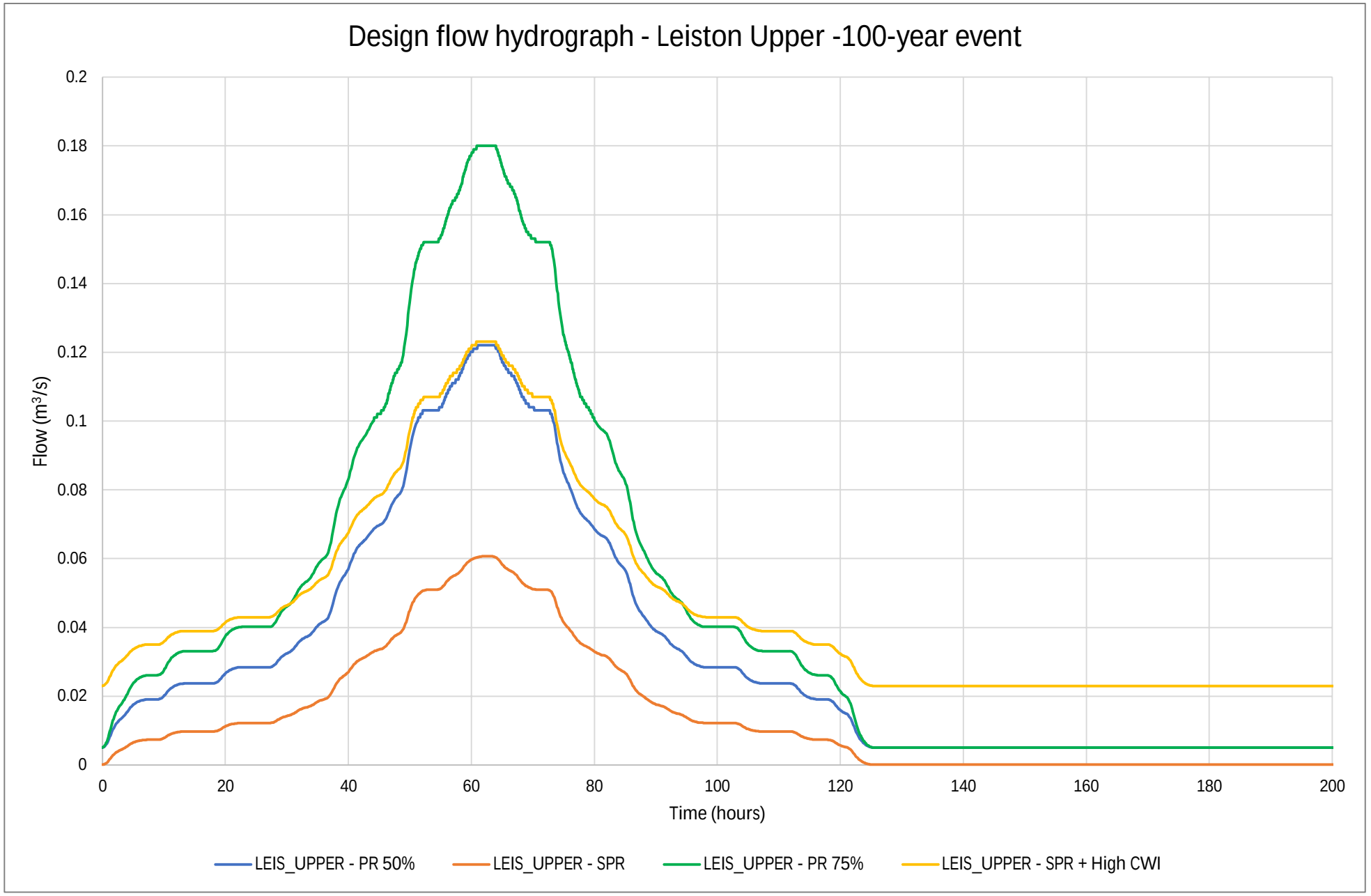

Design flow hydrograph - Theberton -100-year event
Flow (m3/s)
1.2
1
0.8
0.6
0.4
0.2
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_THEBERT - PR 50%
MINS_THEBERT - SPR
MINS_THEBERT - PR 75%
MINS_THEBERT - SPR + High CWI

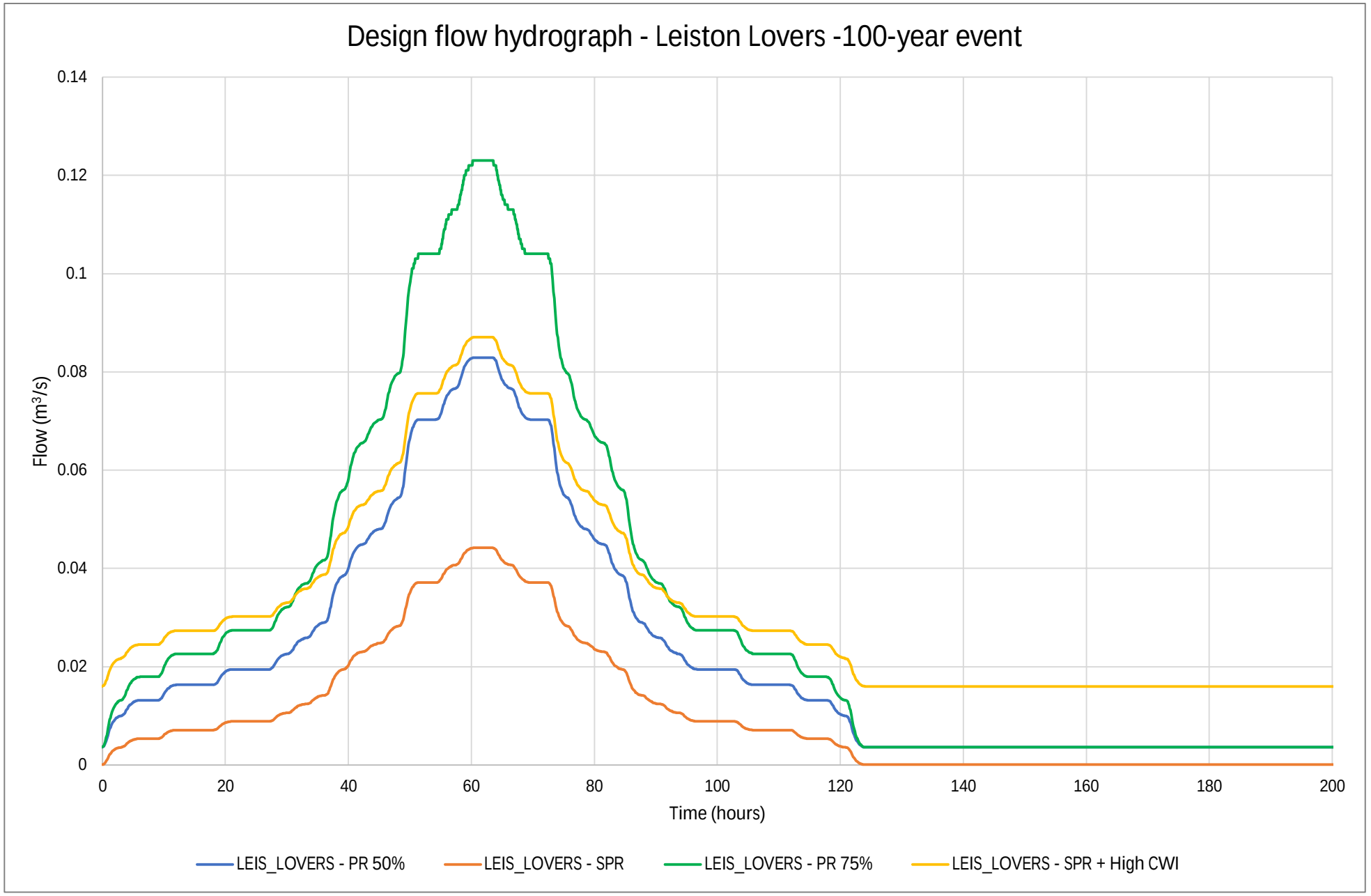

Design flow hydrograph - Potters -100-year event
Flow (m3/s)
2.5
2
1.5
1
0.5
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_POTTERS - PR 50%
MINS_POTTERS - SPR
MINS_POTTERS - PR 75%
MINS_POTTERS - SPR + High CWI

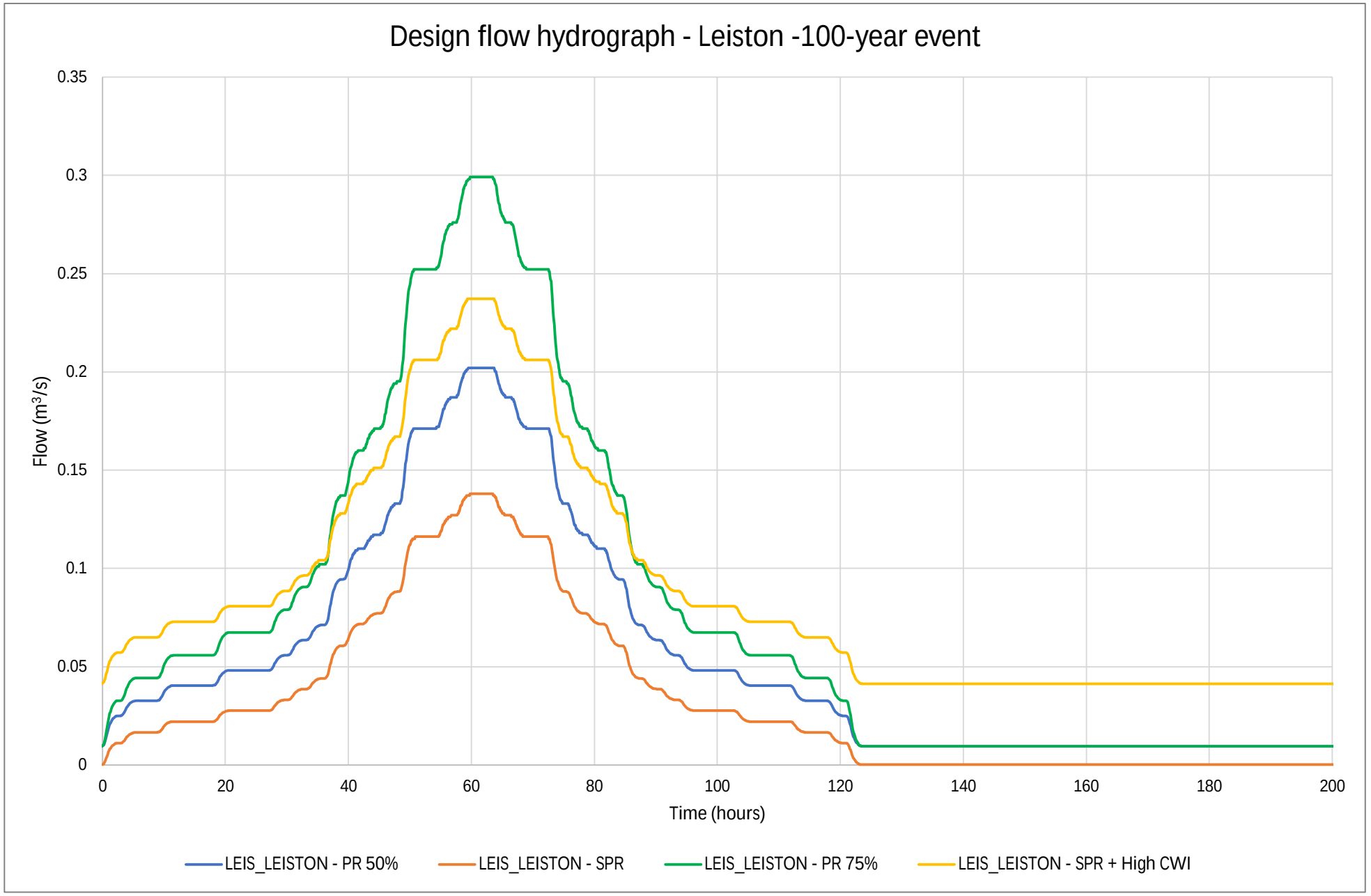

Design flow hydrograph - Scott -100-year event
Flow (m3/s)
0.6
0.5
0.4
0.3
0.2
0.1
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_SCOTT - PR 50%
MINS_SCOTT - SPR
MINS_SCOTT - PR 75%
MINS_SCOTT - SPR + High CWI

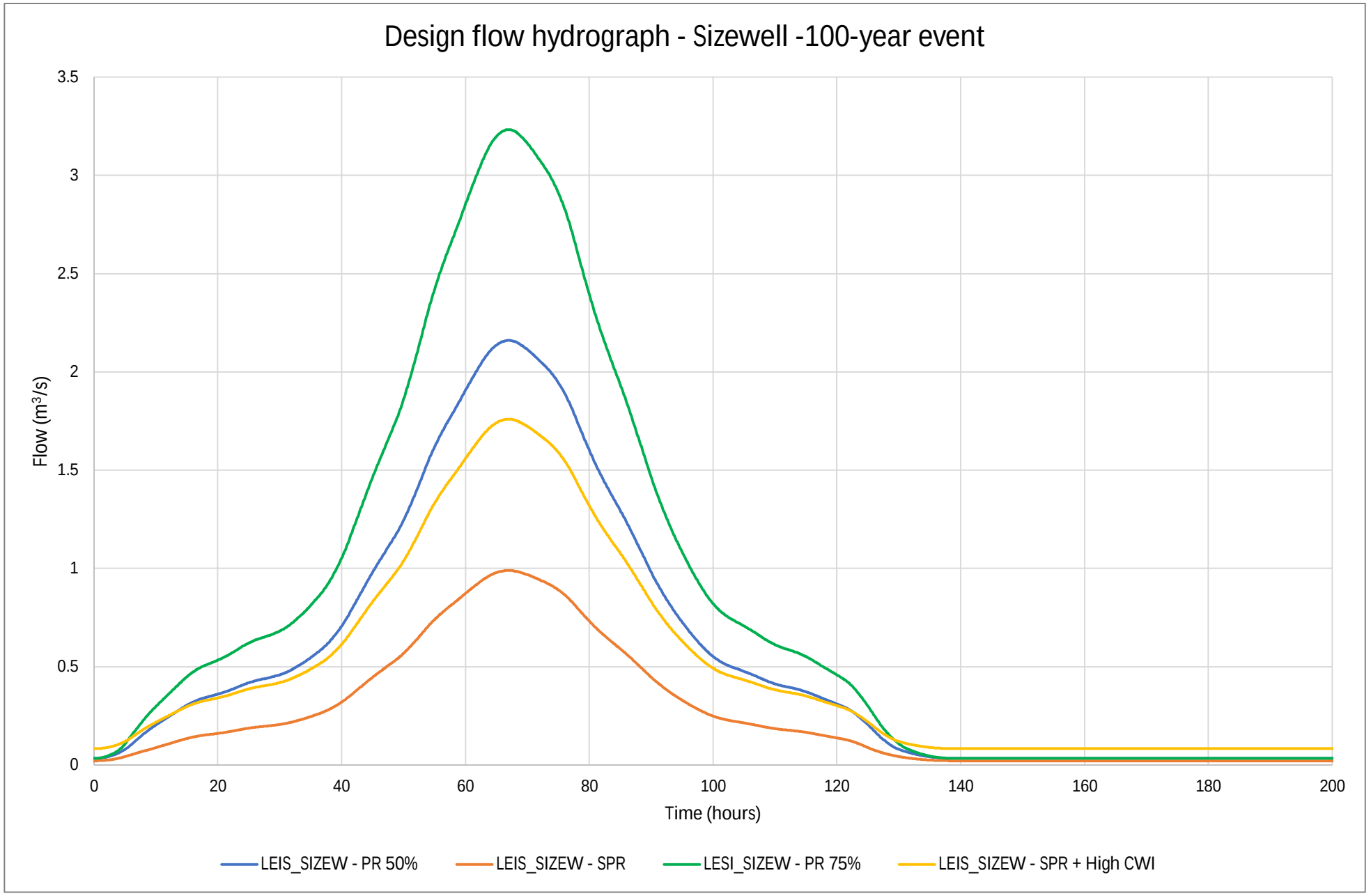

Design flow hydrograph - Docwra -100-year event
Flow (m3/s)
1.8
1.6
1.4
1.2
1
0.8
0.6
0.4
0.2
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_DOCWRA - PR 50%
MINS_DOCWRA - SPR
MINS_DOCWRA - PR 75%
MINS_DOCWRA - SPR + High CWI


Design flow hydrograph - Eastbridge -100-year event
Flow (m3/s)
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
MINS_EASTBR - PR 50%
MINS_EASTBR - SPR
MINS_EASTBR - PR 75%
MINS_EASTBR - SPR + High CWI

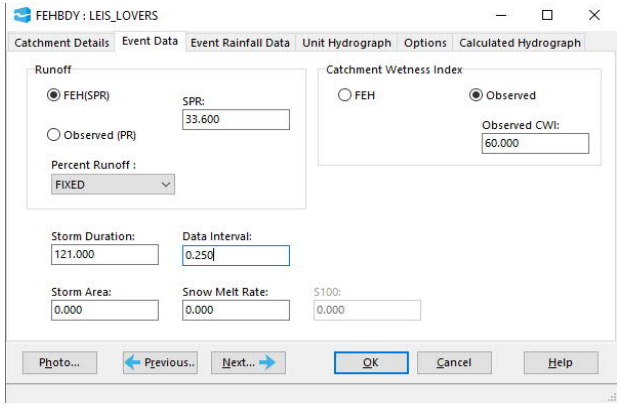

Design flow hydrograph - Leiston Upper -100-year event
Flow (m3/s)
0.2
0.18
0.16
0.14
0.12
0.1
0.08
0.06
0.04
0.02
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
LEIS_UPPER - PR 50%
LEIS_UPPER - SPR
LEIS_UPPER - PR 75%
LEIS_UPPER - SPR + High CWI


Design flow hydrograph - Leiston Lovers -100-year event
0.14
0.12
0.1
0.08
0.06
0.04
0.02
0
Flow (m3/s)
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
LEIS_LOVERS - PR 50%
LEIS_LOVERS - SPR
LEIS_LOVERS - PR 75%
LEIS_LOVERS - SPR + High CWI


Design flow hydrograph - Leiston -100-year event
0.35
0.3
0.25
0.2
0.15
0.1
0.05
0
Flow (m3/s)
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
LEIS_LEISTON - PR 50%
LEIS_LEISTON - SPR
LEIS_LEISTON - PR 75%
LEIS_LEISTON - SPR + High CWI


Design flow hydrograph - Sizewell -100-year event
Flow (m3/s)
3.5
3
2.5
2
1.5
1
0.5
0
0
20
40
60
80
100
120
140
160
180
200
Time (hours)
LEIS_SIZEW - PR 50%
LEIS_SIZEW - SPR
LESI_SIZEW - PR 75%
LEIS_SIZEW - SPR + High CWI

Output data from file C:\USERS\304490\BOX\PB6582 EDF SZC NNB\EDF SZC NNB TEAM\TECH DATA\E01 CALCULATIONS\EXAMINATION HYDROLOGY\HYDROLOGY CALCS MAY 2021\MDS EA ACTIONS MAY 2021\DESIGN FLOWS\SIZE_T100_121SD_SPR.ZZN
Selected output data from time (hr): 0
to time (hr): 300



Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
0	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
0.083	0.965	0.0000279	0.000024	0.0000308	0.0000184	0.0000291	0.00000377	0.0000292	0.00000707	0.0000235	0.0000348	0.1	0.000155	0.00000426	0.00000427	0.00000427	0.02	0.02001
0.167	0.965	0.0000558	0.000048	0.0000616	0.0000367	0.0000583	0.00000755	0.0000584	0.0000141	0.0000471	0.0000696	0.1	0.000311	0.00000852	0.00000853	0.00000854	0.02	0.02003
0.25	0.965	0.0000837	0.000072	0.0000924	0.0000551	0.0000874	0.0000113	0.0000875	0.0000212	0.0000706	0.000104	0.1	0.000466	0.0000128	0.0000128	0.0000128	0.02	0.02004
0.333	0.965	0.000167	0.000144	0.000185	0.00011	0.000146	0.0000226	0.000171	0.0000424	0.000137	0.000204	0.1	0.000932	0.0000298	0.0000299	0.0000299	0.02	0.02009
0.417	0.966	0.000251	0.000216	0.000277	0.000165	0.000204	0.000034	0.000254	0.0000636	0.000202	0.000303	0.1	0.0014	0.0000469	0.0000469	0.000047	0.02	0.02014
0.5	0.966	0.000335	0.000288	0.000369	0.00022	0.000262	0.0000453	0.000338	0.0000848	0.000268	0.000403	0.1	0.00186	0.0000639	0.000064	0.000064	0.02	0.02019
0.583	0.967	0.000474	0.000408	0.000534	0.000312	0.00035	0.0000641	0.000475	0.000117	0.000377	0.000572	0.1	0.00263	0.0000895	0.0000896	0.0000897	0.02	0.02027
0.667	0.967	0.000614	0.000528	0.000698	0.000404	0.000437	0.000083	0.000613	0.000148	0.000485	0.000741	0.1	0.00339	0.000115	0.000115	0.000115	0.02	0.02035
0.75	0.968	0.000753	0.000648	0.000862	0.000496	0.000524	0.000102	0.00075	0.00018	0.000593	0.00091	0.1	0.00416	0.000141	0.000141	0.000141	0.02	0.02042
0.833	0.969	0.000948	0.000816	0.00109	0.000624	0.000641	0.000128	0.000942	0.000226	0.000744	0.00112	0.1	0.00489	0.000179	0.000179	0.000179	0.02	0.02054
0.917	0.969	0.00114	0.000984	0.00131	0.000753	0.000757	0.000155	0.00113	0.000272	0.000895	0.00134	0.1	0.00562	0.000217	0.000218	0.000218	0.02	0.02065
1	0.97	0.00134	0.00115	0.00154	0.000881	0.000874	0.000181	0.00133	0.000318	0.00105	0.00155	0.1	0.00635	0.000256	0.000256	0.000256	0.02	0.02077
1.083	0.971	0.00159	0.00137	0.00183	0.00105	0.00102	0.000215	0.00157	0.000378	0.00124	0.00173	0.1	0.00689	0.000303	0.000303	0.000303	0.02	0.02091
1.167	0.972	0.00184	0.00158	0.00211	0.00121	0.00117	0.000249	0.00182	0.000438	0.00143	0.00192	0.1	0.00743	0.00035	0.00035	0.00035	0.02	0.02105
1.25	0.973	0.00209	0.0018	0.0024	0.00138	0.00131	0.000283	0.00206	0.000498	0.00162	0.0021	0.1	0.00798	0.000396	0.000397	0.000397	0.02	0.02119
1.333	0.974	0.0024	0.00206	0.00276	0.00158	0.00149	0.000324	0.00236	0.000569	0.00182	0.00225	0.1	0.00835	0.000456	0.000457	0.000457	0.02	0.02137
1.417	0.975	0.00271	0.00233	0.00312	0.00178	0.00166	0.000366	0.00266	0.00064	0.00202	0.00239	0.1	0.00873	0.000516	0.000516	0.000517	0.02	0.02155
1.5	0.976	0.00301	0.00259	0.00348	0.00198	0.00184	0.000407	0.00296	0.00071	0.00222	0.00253	0.1	0.00911	0.000575	0.000576	0.000576	0.02	0.02173
1.583	0.977	0.00337	0.0029	0.0039	0.00222	0.00204	0.000457	0.00332	0.000795	0.00239	0.00264	0.1	0.00939	0.000644	0.000644	0.000645	0.02	0.02193
1.667	0.979	0.00374	0.00322	0.00432	0.00246	0.00224	0.000506	0.00367	0.00088	0.00257	0.00274	0.1	0.00967	0.000712	0.000713	0.000713	0.02	0.02214
1.75	0.98	0.0041	0.00353	0.00474	0.0027	0.00245	0.000555	0.00403	0.000965	0.00274	0.00285	0.1	0.00995	0.00078	0.000781	0.000781	0.02	0.02234
1.833	0.982	0.00452	0.00389	0.00522	0.00298	0.00268	0.000611	0.00444	0.00106	0.00289	0.00293	0.1	0.0101	0.000861	0.000862	0.000862	0.02	0.02259
1.917	0.983	0.00494	0.00426	0.00571	0.00327	0.00291	0.000668	0.00485	0.00116	0.00303	0.00301	0.1	0.0103	0.000942	0.000943	0.000944	0.02	0.02283
2	0.985	0.00535	0.00462	0.00619	0.00355	0.00315	0.000724	0.00526	0.00126	0.00318	0.00309	0.1	0.0105	0.00102	0.00102	0.00102	0.02	0.02306
2.083	0.986	0.00583	0.00499	0.00673	0.00387	0.00341	0.000789	0.00573	0.00137	0.0033	0.00315	0.1	0.0107	0.00112	0.00112	0.00112	0.02	0.02336
2.167	0.988	0.0063	0.00537	0.00728	0.0042	0.00367	0.000853	0.0062	0.00148	0.00342	0.00322	0.1	0.0108	0.00121	0.00121	0.00121	0.02	0.02363
2.25	0.99	0.00678	0.00575	0.00782	0.00452	0.00393	0.000917	0.00667	0.00159	0.00355	0.00328	0.1	0.0109	0.0013	0.00131	0.00131	0.02	0.02392
2.333	0.992	0.00731	0.00609	0.00844	0.00487	0.00422	0.000989	0.00719	0.00171	0.00364	0.00333	0.1	0.0109	0.00141	0.00141	0.00141	0.02	0.02423
2.417	0.993	0.00784	0.00644	0.00905	0.00523	0.00452	0.00106	0.00771	0.00184	0.00374	0.00337	0.1	0.011	0.00151	0.00151	0.00151	0.02	0.02453
2.5	0.995	0.00837	0.00679	0.00967	0.00559	0.00481	0.00113	0.00823	0.00196	0.00384	0.00341	0.1	0.011	0.00161	0.00161	0.00161	0.02	0.02483
2.583	0.997	0.00895	0.00711	0.0103	0.00599	0.00513	0.00121	0.0088	0.0021	0.00392	0.00344	0.1	0.011	0.00173	0.00173	0.00173	0.02	0.02519
2.667	1	0.00954	0.00743	0.011	0.00638	0.00545	0.00129	0.00938	0.00224	0.004	0.00347	0.1	0.011	0.00184	0.00184	0.00184	0.02	0.02552
2.75	1.002	0.0101	0.00775	0.0117	0.00677	0.00577	0.00137	0.00995	0.00238	0.00408	0.0035	0.1	0.011	0.00196	0.00196	0.00196	0.02	0.02588
2.833	1.004	0.0108	0.00804	0.0124	0.00721	0.00612	0.00145	0.0106	0.00252	0.00415	0.00351	0.1	0.011	0.00208	0.00208	0.00208	0.02	0.02624
2.917	1.006	0.0114	0.00833	0.0132	0.00764	0.00647	0.00154	0.0112	0.00267	0.00422	0.00352	0.1	0.011	0.0022	0.00221	0.00221	0.02	0.02662
3	1.009	0.012	0.00863	0.0139	0.00807	0.00682	0.00162	0.0118	0.00282	0.00429	0.00353	0.1	0.011	0.00233	0.00233	0.00233	0.02	0.02699
3.083	1.011	0.0128	0.0089	0.0147	0.00855	0.00721	0.00171	0.0125	0.00299	0.00436	0.00355	0.1	0.0111	0.00247	0.00247	0.00247	0.02	0.02741

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
3.167	1.014	0.0135	0.00918	0.0155	0.00902	0.0076	0.0018	0.0132	0.00315	0.00443	0.00357	0.1	0.0111	0.0026	0.00261	0.00261	0.02	0.02782
3.25	1.016	0.0142	0.00945	0.0164	0.0095	0.00799	0.0019	0.0139	0.00332	0.0045	0.00358	0.1	0.0112	0.00274	0.00275	0.00275	0.02	0.02824
3.333	1.019	0.015	0.00972	0.0173	0.01	0.00843	0.002	0.0146	0.0035	0.00457	0.00363	0.1	0.0114	0.00289	0.0029	0.0029	0.02	0.02869
3.417	1.022	0.0158	0.00999	0.0182	0.0106	0.00886	0.0021	0.0153	0.00369	0.00465	0.00367	0.1	0.0117	0.00305	0.00305	0.00305	0.02	0.02915
3.5	1.024	0.0166	0.0103	0.0191	0.0111	0.0093	0.00221	0.016	0.00388	0.00473	0.00372	0.1	0.0119	0.0032	0.0032	0.00321	0.02	0.02961
3.583	1.027	0.0174	0.0105	0.0201	0.0117	0.00978	0.00232	0.0167	0.00408	0.00482	0.0038	0.1	0.0122	0.00337	0.00337	0.00338	0.02	0.03012
3.667	1.03	0.0183	0.0108	0.0211	0.0123	0.0103	0.00244	0.0174	0.00428	0.00491	0.00388	0.1	0.0126	0.00354	0.00354	0.00355	0.02	0.03063
3.75	1.033	0.0192	0.0111	0.0221	0.0128	0.0107	0.00255	0.0181	0.00449	0.005	0.00396	0.1	0.013	0.00371	0.00372	0.00372	0.02	0.03115
3.833	1.036	0.0201	0.0113	0.0233	0.0135	0.0113	0.00268	0.0187	0.00471	0.0051	0.00407	0.1	0.0133	0.0039	0.0039	0.0039	0.02	0.0317
3.917	1.039	0.0211	0.0116	0.0244	0.0141	0.0118	0.0028	0.0194	0.00493	0.00519	0.00417	0.1	0.0137	0.00408	0.00409	0.00409	0.02	0.03226
4	1.043	0.0221	0.0118	0.0255	0.0148	0.0123	0.00293	0.0201	0.00515	0.00529	0.00428	0.1	0.0141	0.00427	0.00427	0.00427	0.02	0.03281
4.083	1.046	0.0231	0.0121	0.0267	0.0155	0.0129	0.00307	0.0208	0.00537	0.0054	0.00437	0.1	0.0144	0.00447	0.00447	0.00447	0.02	0.03341
4.167	1.049	0.0241	0.0124	0.0279	0.0162	0.0134	0.0032	0.0215	0.00559	0.00551	0.00446	0.1	0.0146	0.00467	0.00467	0.00468	0.02	0.03402
4.25	1.053	0.0252	0.0126	0.0291	0.0169	0.014	0.00334	0.0222	0.00582	0.00561	0.00456	0.1	0.0149	0.00487	0.00488	0.00488	0.02	0.03463
4.333	1.056	0.0263	0.0129	0.0304	0.0176	0.0146	0.00349	0.0228	0.00604	0.00572	0.00463	0.1	0.0151	0.00509	0.00509	0.0051	0.02	0.03528
4.417	1.06	0.0274	0.0132	0.0317	0.0183	0.0152	0.00364	0.0235	0.00626	0.00582	0.00471	0.1	0.0153	0.0053	0.00531	0.00531	0.02	0.03592
4.5	1.063	0.0286	0.0134	0.033	0.0191	0.0158	0.00379	0.0242	0.00648	0.00592	0.00478	0.1	0.0155	0.00552	0.00553	0.00553	0.02	0.03658
4.583	1.067	0.0298	0.0137	0.0344	0.0198	0.0165	0.00395	0.0249	0.00671	0.00601	0.00483	0.1	0.0156	0.00576	0.00576	0.00577	0.02	0.03729
4.667	1.071	0.031	0.014	0.0358	0.0206	0.0171	0.00411	0.0255	0.00693	0.0061	0.00489	0.1	0.0158	0.00599	0.006	0.006	0.02	0.03799
4.75	1.075	0.0322	0.0143	0.0372	0.0213	0.0178	0.00427	0.0262	0.00715	0.00619	0.00494	0.1	0.0159	0.00622	0.00623	0.00623	0.02	0.03868
4.833	1.079	0.0334	0.0146	0.0387	0.0221	0.0185	0.00443	0.0269	0.00737	0.00626	0.00498	0.1	0.016	0.00647	0.00648	0.00648	0.02	0.03943
4.917	1.083	0.0346	0.0149	0.0402	0.0228	0.0192	0.0046	0.0275	0.00759	0.00634	0.00502	0.1	0.0161	0.00672	0.00673	0.00673	0.02	0.04018
5	1.087	0.0358	0.0152	0.0417	0.0235	0.0199	0.00477	0.0282	0.00782	0.00641	0.00507	0.1	0.0162	0.00697	0.00698	0.00698	0.02	0.04093
5.083	1.091	0.037	0.0155	0.0432	0.0243	0.0206	0.00494	0.0289	0.00803	0.00648	0.0051	0.1	0.0163	0.00723	0.00724	0.00725	0.02	0.04172
5.167	1.096	0.0382	0.0158	0.0448	0.025	0.0214	0.0051	0.0295	0.00825	0.00654	0.00513	0.1	0.0164	0.0075	0.00751	0.00751	0.02	0.04252
5.25	1.1	0.0395	0.0161	0.0464	0.0258	0.0221	0.00527	0.0302	0.00847	0.0066	0.00516	0.1	0.0164	0.00776	0.00777	0.00777	0.02	0.0433
5.333	1.104	0.0407	0.0164	0.048	0.0265	0.0229	0.00543	0.0308	0.00868	0.00665	0.00519	0.1	0.0165	0.00802	0.00803	0.00804	0.02	0.04409
5.417	1.109	0.0419	0.0166	0.0495	0.0273	0.0237	0.0056	0.0315	0.0089	0.0067	0.00521	0.1	0.0165	0.00829	0.0083	0.0083	0.02	0.04489
5.5	1.113	0.0431	0.0169	0.0511	0.028	0.0245	0.00576	0.0322	0.00912	0.00675	0.00523	0.1	0.0165	0.00855	0.00856	0.00857	0.02	0.04568
5.583	1.118	0.0443	0.0171	0.0527	0.0287	0.0253	0.00593	0.0328	0.00933	0.00679	0.00525	0.1	0.0165	0.00881	0.00882	0.00883	0.02	0.04646
5.667	1.123	0.0455	0.0174	0.0542	0.0295	0.0261	0.00609	0.0335	0.00955	0.00683	0.00527	0.1	0.0165	0.00907	0.00909	0.00909	0.02	0.04725
5.75	1.127	0.0467	0.0176	0.0558	0.0302	0.027	0.00625	0.0341	0.00977	0.00687	0.00528	0.1	0.0165	0.00934	0.00935	0.00935	0.02	0.04804
5.833	1.132	0.0479	0.0179	0.0574	0.0309	0.0278	0.00642	0.0348	0.00998	0.00691	0.00529	0.1	0.0165	0.0096	0.00961	0.00961	0.02	0.04882
5.917	1.137	0.0491	0.0181	0.0589	0.0317	0.0287	0.00658	0.0354	0.0102	0.00695	0.00529	0.1	0.0165	0.00986	0.00987	0.00988	0.02	0.04961
6	1.142	0.0503	0.0183	0.0605	0.0324	0.0296	0.00674	0.0361	0.0104	0.00698	0.0053	0.1	0.0165	0.0101	0.0101	0.0101	0.02	0.0503
6.083	1.148	0.0515	0.0185	0.0621	0.0331	0.0305	0.0069	0.0367	0.0106	0.00701	0.0053	0.1	0.0165	0.0104	0.0104	0.0104	0.02	0.0512
6.167	1.153	0.0526	0.0187	0.0636	0.0338	0.0314	0.00706	0.0373	0.0108	0.00704	0.0053	0.1	0.0165	0.0106	0.0107	0.0107	0.02	0.052
6.25	1.158	0.0538	0.0189	0.0652	0.0346	0.0323	0.00723	0.038	0.0111	0.00707	0.0053	0.1	0.0165	0.0109	0.0109	0.0109	0.02	0.0527
6.333	1.163	0.055	0.019	0.0667	0.0353	0.0333	0.00739	0.0386	0.0113	0.00709	0.0053	0.1	0.0165	0.0112	0.0112	0.0112	0.02	0.0536
6.417	1.169	0.0562	0.0192	0.0683	0.036	0.0342	0.00755	0.0392	0.0115	0.00712	0.0053	0.1	0.0165	0.0114	0.0114	0.0114	0.02	0.0542
6.5	1.174	0.0574	0.0193	0.0698	0.0368	0.0352	0.00771	0.0398	0.0117	0.00714	0.0053	0.1	0.0165	0.0117	0.0117	0.0117	0.02	0.0551
6.583	1.18	0.0586	0.0195	0.0714	0.0375	0.0362	0.00787	0.0404	0.0119	0.00716	0.0053	0.1	0.0165	0.0119	0.0119	0.012	0.02	0.0558
6.667	1.186	0.0598	0.0196	0.0729	0.0382	0.0372	0.00803	0.0409	0.0121	0.00718	0.0053	0.1	0.0165	0.0122	0.0122	0.0122	0.02	0.0566
6.75	1.191	0.061	0.0198	0.0745	0.0389	0.0382	0.0082	0.0415	0.0123	0.0072	0.0053	0.1	0.0165	0.0124	0.0125	0.0125	0.02	0.0574
6.833	1.197	0.0621	0.0199	0.076	0.0396	0.0393	0.00836	0.0421	0.0125	0.00721	0.0053	0.1	0.0165	0.0127	0.0127	0.0127	0.02	0.0581
6.917	1.203	0.0633	0.02	0.0776	0.0404	0.0403	0.00852	0.0426	0.0128	0.00722	0.0053	0.1	0.0165	0.013	0.013	0.013	0.02	0.059
7	1.209	0.0645	0.0201	0.0791	0.0411	0.0414	0.00868	0.0432	0.013	0.00724	0.0053	0.1	0.0165	0.0132	0.0132	0.0132	0.02	0.0596
7.083	1.215	0.0657	0.0202	0.0807	0.0418	0.0424	0.00884	0.0437	0.0132	0.00724	0.0053	0.1	0.0165	0.0135	0.0135	0.0135	0.02	0.0605
7.167	1.221	0.0668	0.0203	0.0822	0.0425	0.0435	0.009	0.0442	0.0134	0.00725	0.0053	0.1	0.0165	0.0137	0.0137	0.0138	0.02	0.0612
7.25	1.228	0.068	0.0203	0.0837	0.0432	0.0446	0.00916	0.0447	0.0136	0.00726	0.0053	0.1	0.0165	0.014	0.014	0.014	0.02	0.062
7.333	1.234	0.0692	0.0204	0.0853	0.0439	0.0456	0.00931	0.0452	0.0138	0.00726	0.0053	0.1	0.0165	0.0142	0.0143	0.0143	0.02	0.0628
7.417	1.241	0.0703	0.0205	0.0868	0.0446	0.0467	0.00947	0.0457	0.0139	0.00726	0.0053	0.1	0.0165	0.0145	0.0145	0.0145	0.02	0.0635
7.5	1.247	0.0715	0.0206	0.0883	0.0453	0.0477	0.00963	0.0462	0.0141	0.00727	0.0053	0.1	0.0165	0.0148	0.0148	0.0148	0.02	0.0644
7.583	1.254	0.0727	0.0206	0.0899	0.046	0.0488	0.00979	0.0466	0.0143	0.00727	0.0053	0.1	0.0165	0.015	0.015	0.015	0.02	0.065
7.667	1.26	0.0738	0.0207	0.0914	0.0467	0.0498	0.00995	0.0471	0.0145	0.00727	0.0053	0.1	0.0165	0.0153	0.0153	0.0153	0.02	0.0659
7.75	1.267	0.075	0.0208	0.0929	0.0474	0.0509	0.0101	0.0476	0.0147	0.00727	0.0053	0.1	0.0165	0.0155	0.0155	0.0155	0.02	0.0665
7.833	1.274	0.0761	0.0208	0.0944	0.048	0.052	0.0103	0.048	0.0148	0.00727	0.0053	0.1	0.0165	0.0158	0.0158	0.0158	0.02	0.0674
7.917	1.281	0.0772	0.0209	0.0959	0.0486	0.053	0.0104	0.0484	0.015	0.00727	0.0053	0.1	0.0165	0.016	0.016	0.016	0.02	0.068
8	1.288	0.0784	0.0209	0.0975	0.0493	0.0541	0.0106	0.0488	0.0152	0.00727	0.0053	0.1	0.0165	0.0163	0.0163	0.0163	0.02	0.0689
8.083	1.295	0.0794	0.021	0.099	0.0499	0.0551	0.0107	0.0492	0.0153	0.00727	0.0053	0.1	0.0165	0.0165	0.0165	0.0165	0.02	0.0695
8.167	1.302	0.0805	0.0211	0.1	0.0505	0.0562	0.0109	0.0496	0.0155	0.00727	0.0053	0.1	0.0165	0.0168	0.0168	0.0168	0.02	0.0704
8.25	1.31	0.0816	0.0211	0.102	0.0511	0.0572	0.011	0.05	0.0157	0.00727	0.0053	0.1	0.0165	0.017	0.017	0.017	0.02	0.071
8.333	1.317	0.0826	0.0212	0.103	0.0517	0.0582	0.0112	0.0504	0.0158	0.00727	0.0053	0.1	0.0165	0.0173	0.0173	0.0173	0.02	0.0719

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
8.417	1.325	0.0836	0.0212	0.105	0.0523	0.0593	0.0113	0.0508	0.016	0.00727	0.0053	0.1	0.0165	0.0175	0.0175	0.0175	0.02	0.0725
8.5	1.332	0.0847	0.0213	0.106	0.0529	0.0603	0.0115	0.0511	0.0161	0.00727	0.0053	0.1	0.0165	0.0177	0.0178	0.0178	0.02	0.0733
8.583	1.34	0.0856	0.0213	0.108	0.0534	0.0614	0.0116	0.0515	0.0163	0.00727	0.0053	0.1	0.0165	0.018	0.018	0.018	0.02	0.074
8.667	1.347	0.0866	0.0213	0.109	0.054	0.0624	0.0117	0.0518	0.0164	0.00727	0.0053	0.1	0.0165	0.0182	0.0182	0.0182	0.02	0.0746
8.75	1.355	0.0876	0.0214	0.111	0.0545	0.0634	0.0119	0.0521	0.0165	0.00727	0.0053	0.1	0.0165	0.0184	0.0185	0.0185	0.02	0.0754
8.833	1.363	0.0885	0.0214	0.112	0.0551	0.0645	0.012	0.0524	0.0167	0.00727	0.0053	0.1	0.0165	0.0187	0.0187	0.0187	0.02	0.0761
8.917	1.371	0.0895	0.0215	0.113	0.0556	0.0655	0.0121	0.0527	0.0168	0.00727	0.0053	0.1	0.0165	0.0189	0.0189	0.0189	0.02	0.0767
9	1.379	0.0904	0.0215	0.115	0.0561	0.0665	0.0122	0.0531	0.017	0.00727	0.0053	0.1	0.0165	0.0191	0.0191	0.0191	0.02	0.0773
9.083	1.388	0.0913	0.0215	0.116	0.0566	0.0676	0.0124	0.0533	0.0171	0.00728	0.00531	0.1	0.0166	0.0193	0.0194	0.0194	0.02	0.0781
9.167	1.396	0.0922	0.0216	0.117	0.0571	0.0686	0.0125	0.0536	0.0172	0.00728	0.00533	0.1	0.0166	0.0195	0.0196	0.0196	0.02	0.0787
9.25	1.404	0.0931	0.0216	0.119	0.0576	0.0697	0.0126	0.0539	0.0174	0.00729	0.00534	0.1	0.0167	0.0198	0.0198	0.0198	0.02	0.0794
9.333	1.413	0.0939	0.0217	0.12	0.0581	0.0707	0.0127	0.0542	0.0175	0.00732	0.00538	0.1	0.0169	0.02	0.02	0.02	0.0202	0.0802
9.417	1.421	0.0948	0.0217	0.121	0.0587	0.0718	0.0129	0.0545	0.0176	0.00735	0.00542	0.1	0.017	0.0202	0.0202	0.0202	0.0203	0.0809
9.5	1.43	0.0957	0.0218	0.122	0.0592	0.0728	0.013	0.0548	0.0178	0.00737	0.00546	0.1	0.0172	0.0204	0.0204	0.0204	0.0205	0.0817
9.583	1.439	0.0965	0.0218	0.124	0.0597	0.0739	0.0131	0.055	0.0179	0.00742	0.00553	0.1	0.0176	0.0206	0.0206	0.0206	0.0207	0.0825
9.667	1.448	0.0974	0.0219	0.125	0.0602	0.0749	0.0132	0.0553	0.018	0.00747	0.00561	0.1	0.0179	0.0208	0.0208	0.0209	0.0209	0.0834
9.75	1.456	0.0983	0.022	0.126	0.0607	0.076	0.0133	0.0556	0.0182	0.00752	0.00568	0.1	0.0182	0.021	0.021	0.0211	0.0211	0.0842
9.833	1.466	0.0991	0.022	0.127	0.0612	0.077	0.0135	0.0559	0.0183	0.00759	0.00578	0.1	0.0186	0.0212	0.0213	0.0213	0.0213	0.0851
9.917	1.475	0.1	0.0221	0.129	0.0617	0.0781	0.0136	0.0562	0.0184	0.00765	0.00588	0.1	0.019	0.0214	0.0215	0.0215	0.0215	0.0859
10	1.484	0.101	0.0222	0.13	0.0622	0.0792	0.0137	0.0565	0.0186	0.00772	0.00598	0.1	0.0194	0.0216	0.0217	0.0217	0.0217	0.0867
10.083	1.493	0.102	0.0223	0.131	0.0627	0.0802	0.0138	0.0568	0.0187	0.00781	0.00608	0.1	0.0197	0.0218	0.0219	0.0219	0.0219	0.0875
10.167	1.503	0.103	0.0224	0.132	0.0632	0.0813	0.0139	0.0571	0.0188	0.0079	0.00617	0.1	0.02	0.022	0.0221	0.0221	0.0221	0.0883
10.25	1.512	0.103	0.0225	0.133	0.0636	0.0824	0.0141	0.0574	0.019	0.00799	0.00627	0.1	0.0203	0.0222	0.0223	0.0223	0.0223	0.0891
10.333	1.522	0.104	0.0227	0.135	0.0641	0.0834	0.0142	0.0577	0.0191	0.00809	0.00635	0.1	0.0205	0.0224	0.0225	0.0225	0.0225	0.0899
10.417	1.532	0.105	0.0228	0.136	0.0646	0.0845	0.0143	0.058	0.0192	0.00819	0.00643	0.1	0.0207	0.0226	0.0227	0.0227	0.0227	0.0907
10.5	1.541	0.106	0.0229	0.137	0.0651	0.0855	0.0144	0.0583	0.0194	0.00829	0.0065	0.1	0.0209	0.0228	0.0229	0.0229	0.0229	0.0915
10.583	1.551	0.107	0.0231	0.138	0.0656	0.0866	0.0145	0.0586	0.0195	0.00838	0.00656	0.1	0.0211	0.023	0.023	0.0231	0.0231	0.0922
10.667	1.561	0.108	0.0232	0.139	0.0661	0.0876	0.0147	0.0589	0.0196	0.00847	0.00662	0.1	0.0212	0.0232	0.0232	0.0233	0.0233	0.093
10.75	1.571	0.109	0.0234	0.14	0.0666	0.0887	0.0148	0.0592	0.0198	0.00856	0.00668	0.1	0.0214	0.0234	0.0234	0.0235	0.0235	0.0938
10.833	1.582	0.109	0.0235	0.142	0.0671	0.0897	0.0149	0.0596	0.0199	0.00864	0.00672	0.1	0.0215	0.0236	0.0236	0.0236	0.0237	0.0945
10.917	1.592	0.11	0.0237	0.143	0.0676	0.0907	0.015	0.0599	0.02	0.00871	0.00676	0.1	0.0216	0.0238	0.0238	0.0238	0.0239	0.0953
11	1.602	0.111	0.0239	0.144	0.0681	0.0917	0.0151	0.0602	0.0202	0.00879	0.00681	0.1	0.0217	0.024	0.024	0.024	0.0241	0.0961
11.083	1.613	0.112	0.0241	0.145	0.0686	0.0927	0.0153	0.0605	0.0203	0.00886	0.00684	0.1	0.0218	0.0242	0.0242	0.0242	0.0243	0.0969
11.167	1.624	0.113	0.0243	0.146	0.069	0.0938	0.0154	0.0608	0.0204	0.00892	0.00688	0.1	0.0218	0.0244	0.0244	0.0244	0.0245	0.0977
11.25	1.634	0.114	0.0244	0.148	0.0695	0.0948	0.0155	0.0612	0.0206	0.00899	0.00691	0.1	0.0219	0.0246	0.0246	0.0246	0.0247	0.0985
11.333	1.645	0.115	0.0246	0.149	0.07	0.0958	0.0156	0.0615	0.0207	0.00904	0.00694	0.1	0.0219	0.0248	0.0248	0.0248	0.0249	0.0993
11.417	1.656	0.115	0.0248	0.15	0.0705	0.0968	0.0157	0.0618	0.0208	0.00909	0.00696	0.1	0.022	0.025	0.025	0.025	0.0251	0.1001
11.5	1.667	0.116	0.025	0.151	0.071	0.0978	0.0158	0.0622	0.0209	0.00915	0.00699	0.1	0.022	0.0252	0.0252	0.0252	0.0253	0.1009
11.583	1.678	0.117	0.0251	0.152	0.0715	0.0987	0.016	0.0625	0.0211	0.00919	0.00701	0.1	0.022	0.0254	0.0254	0.0254	0.0255	0.1017
11.667	1.689	0.118	0.0253	0.153	0.072	0.0997	0.0161	0.0629	0.0212	0.00923	0.00702	0.1	0.022	0.0256	0.0256	0.0256	0.0257	0.1025
11.75	1.701	0.119	0.0255	0.155	0.0725	0.101	0.0162	0.0632	0.0214	0.00927	0.00704	0.1	0.022	0.0258	0.0258	0.0258	0.0259	0.1033
11.833	1.712	0.12	0.0256	0.156	0.073	0.102	0.0163	0.0636	0.0215	0.00931	0.00705	0.1	0.022	0.026	0.026	0.026	0.0261	0.1041
11.917	1.724	0.12	0.0258	0.157	0.0735	0.103	0.0164	0.064	0.0216	0.00935	0.00706	0.1	0.022	0.0261	0.0262	0.0262	0.0263	0.1048
12	1.735	0.121	0.0259	0.158	0.0739	0.104	0.0165	0.0644	0.0218	0.00938	0.00706	0.1	0.022	0.0263	0.0264	0.0264	0.0265	0.1056
12.083	1.747	0.122	0.0261	0.159	0.0744	0.105	0.0167	0.0648	0.0219	0.00941	0.00706	0.1	0.022	0.0265	0.0266	0.0266	0.0267	0.1064
12.167	1.759	0.123	0.0262	0.16	0.0749	0.106	0.0168	0.0651	0.022	0.00944	0.00707	0.1	0.022	0.0267	0.0268	0.0268	0.0269	0.1072
12.25	1.771	0.124	0.0263	0.162	0.0754	0.106	0.0169	0.0655	0.0222	0.00947	0.00707	0.1	0.022	0.0269	0.027	0.027	0.027	0.1079
12.333	1.783	0.125	0.0265	0.163	0.0759	0.107	0.017	0.0659	0.0223	0.0095	0.00707	0.1	0.022	0.0271	0.0272	0.0272	0.0272	0.1087
12.417	1.795	0.125	0.0266	0.164	0.0764	0.108	0.0171	0.0663	0.0224	0.00952	0.00707	0.1	0.022	0.0273	0.0274	0.0274	0.0274	0.1095
12.5	1.807	0.126	0.0267	0.165	0.0769	0.109	0.0172	0.0667	0.0226	0.00955	0.00707	0.1	0.022	0.0275	0.0275	0.0276	0.0276	0.1102
12.583	1.82	0.127	0.0268	0.166	0.0774	0.11	0.0174	0.0671	0.0227	0.00957	0.00707	0.1	0.022	0.0277	0.0277	0.0278	0.0278	0.111
12.667	1.832	0.128	0.0269	0.167	0.0779	0.111	0.0175	0.0674	0.0229	0.00959	0.00707	0.1	0.022	0.0279	0.0279	0.028	0.028	0.1118
12.75	1.845	0.129	0.027	0.169	0.0784	0.112	0.0176	0.0678	0.023	0.00961	0.00707	0.1	0.022	0.0281	0.0281	0.0281	0.0282	0.1125
12.833	1.858	0.13	0.0271	0.17	0.0789	0.113	0.0177	0.0681	0.0231	0.00962	0.00707	0.1	0.022	0.0283	0.0283	0.0283	0.0284	0.1133
12.917	1.871	0.13	0.0272	0.171	0.0795	0.114	0.0178	0.0685	0.0233	0.00964	0.00707	0.1	0.022	0.0285	0.0285	0.0285	0.0286	0.1141
13	1.883	0.131	0.0273	0.172	0.08	0.115	0.0179	0.0688	0.0234	0.00965	0.00707	0.1	0.022	0.0287	0.0287	0.0287	0.0288	0.1149
13.083	1.897	0.132	0.0274	0.173	0.0805	0.116	0.018	0.0691	0.0236	0.00966	0.00707	0.1	0.022	0.0289	0.0289	0.0289	0.029	0.1157
13.167	1.91	0.133	0.0275	0.174	0.081	0.117	0.0182	0.0695	0.0237	0.00967	0.00707	0.1	0.022	0.0291	0.0291	0.0291	0.0292	0.1165
13.25	1.923	0.134	0.0275	0.175	0.0815	0.118	0.0183	0.0698	0.0238	0.00968	0.00707	0.1	0.022	0.0293	0.0293	0.0293	0.0294	0.1173
13.333	1.936	0.135	0.0276	0.177	0.082	0.118	0.0184	0.0701	0.024	0.00968	0.00707	0.1	0.022	0.0294	0.0295	0.0295	0.0296	0.118
13.417	1.95	0.136	0.0277	0.178	0.0825	0.119	0.0185	0.0704	0.0241	0.00969	0.00707	0.1	0.022	0.0296	0.0297	0.0297	0.0298	0.1188
13.5	1.963	0.136	0.0278	0.179	0.083	0.12	0.0186	0.0707	0.0242	0.00969	0.00707	0.1	0.022	0.0298	0.0299	0.0299	0.03	0.1196
13.583	1.977	0.137	0.0278	0.18	0.0835	0.121	0.0188	0.0709	0.0243	0.00969	0.00707	0.1	0.022	0.03	0.0301	0.0301	0.0302	0.1204

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
13.667	1.991	0.138	0.0279	0.181	0.084	0.122	0.0189	0.0712	0.0244	0.00969	0.00707	0.1	0.022	0.0302	0.0303	0.0303	0.0303	0.1211
13.75	2.005	0.139	0.028	0.182	0.0845	0.123	0.019	0.0715	0.0246	0.00969	0.00707	0.1	0.022	0.0304	0.0304	0.0305	0.0305	0.1218
13.833	2.019	0.14	0.028	0.184	0.085	0.124	0.0191	0.0717	0.0247	0.00969	0.00707	0.1	0.022	0.0306	0.0306	0.0307	0.0307	0.1226
13.917	2.033	0.141	0.0281	0.185	0.0854	0.124	0.0192	0.072	0.0248	0.00969	0.00707	0.1	0.022	0.0308	0.0308	0.0309	0.0309	0.1234
14	2.047	0.142	0.0282	0.186	0.0859	0.125	0.0194	0.0722	0.0249	0.00969	0.00707	0.1	0.022	0.031	0.031	0.031	0.0311	0.1241
14.083	2.062	0.142	0.0282	0.187	0.0864	0.126	0.0195	0.0724	0.025	0.00969	0.00707	0.1	0.022	0.0312	0.0312	0.0312	0.0313	0.1249
14.167	2.076	0.143	0.0283	0.188	0.0868	0.127	0.0196	0.0727	0.0251	0.00969	0.00707	0.1	0.022	0.0314	0.0314	0.0314	0.0315	0.1257
14.25	2.091	0.144	0.0283	0.189	0.0872	0.128	0.0197	0.0729	0.0252	0.00969	0.00707	0.1	0.022	0.0316	0.0316	0.0316	0.0317	0.1265
14.333	2.106	0.145	0.0284	0.191	0.0876	0.129	0.0198	0.0731	0.0253	0.00969	0.00707	0.1	0.022	0.0318	0.0318	0.0318	0.0319	0.1273
14.417	2.121	0.146	0.0284	0.192	0.0881	0.13	0.0199	0.0733	0.0254	0.00969	0.00707	0.1	0.022	0.032	0.032	0.032	0.0321	0.1281
14.5	2.136	0.146	0.0285	0.193	0.0885	0.13	0.02	0.0735	0.0255	0.00969	0.00707	0.1	0.022	0.0321	0.0322	0.0322	0.0323	0.1288
14.583	2.151	0.147	0.0285	0.194	0.0889	0.131	0.0201	0.0737	0.0256	0.00969	0.00707	0.1	0.022	0.0323	0.0324	0.0324	0.0325	0.1296
14.667	2.166	0.148	0.0286	0.195	0.0892	0.132	0.0202	0.0739	0.0257	0.00969	0.00707	0.1	0.022	0.0325	0.0325	0.0326	0.0327	0.1303
14.75	2.181	0.149	0.0286	0.196	0.0896	0.133	0.0203	0.0741	0.0258	0.00969	0.00707	0.1	0.022	0.0327	0.0327	0.0328	0.0328	0.131
14.833	2.197	0.149	0.0286	0.197	0.09	0.134	0.0204	0.0742	0.0258	0.00969	0.00707	0.1	0.022	0.0329	0.0329	0.0329	0.033	0.1317
14.917	2.212	0.15	0.0287	0.198	0.0904	0.134	0.0205	0.0744	0.0259	0.00969	0.00707	0.1	0.022	0.033	0.0331	0.0331	0.0332	0.1324
15	2.228	0.151	0.0287	0.199	0.0907	0.135	0.0206	0.0746	0.026	0.00969	0.00707	0.1	0.022	0.0332	0.0333	0.0333	0.0334	0.1332
15.083	2.244	0.151	0.0287	0.2	0.0911	0.136	0.0207	0.0747	0.0261	0.00969	0.00707	0.1	0.022	0.0334	0.0334	0.0334	0.0335	0.1337
15.167	2.26	0.152	0.0288	0.201	0.0914	0.137	0.0208	0.0749	0.0262	0.00969	0.00707	0.1	0.022	0.0336	0.0336	0.0336	0.0337	0.1345
15.25	2.276	0.153	0.0288	0.202	0.0917	0.138	0.0209	0.0751	0.0263	0.00969	0.00707	0.1	0.022	0.0337	0.0338	0.0338	0.0339	0.1352
15.333	2.292	0.153	0.0288	0.203	0.0921	0.138	0.021	0.0752	0.0263	0.00969	0.00707	0.1	0.022	0.0339	0.0339	0.0339	0.034	0.1357
15.417	2.309	0.154	0.0289	0.204	0.0924	0.139	0.0211	0.0753	0.0264	0.00969	0.00707	0.1	0.022	0.034	0.0341	0.0341	0.0342	0.1364
15.5	2.325	0.154	0.0289	0.205	0.0927	0.14	0.0212	0.0755	0.0265	0.00969	0.00707	0.1	0.022	0.0342	0.0342	0.0343	0.0344	0.1371
15.583	2.342	0.155	0.0289	0.206	0.093	0.141	0.0213	0.0756	0.0266	0.00969	0.00707	0.1	0.022	0.0344	0.0344	0.0344	0.0345	0.1377
15.667	2.358	0.156	0.0289	0.207	0.0933	0.141	0.0214	0.0758	0.0266	0.00969	0.00707	0.1	0.022	0.0345	0.0346	0.0346	0.0347	0.1384
15.75	2.375	0.156	0.0289	0.208	0.0936	0.142	0.0214	0.0759	0.0267	0.00969	0.00707	0.1	0.022	0.0347	0.0347	0.0347	0.0348	0.1389
15.833	2.392	0.157	0.0289	0.209	0.0938	0.143	0.0215	0.076	0.0268	0.00969	0.00707	0.1	0.022	0.0348	0.0349	0.0349	0.035	0.1396
15.917	2.409	0.157	0.029	0.21	0.0941	0.144	0.0216	0.0761	0.0268	0.00969	0.00707	0.1	0.022	0.035	0.035	0.035	0.0351	0.1401
16	2.426	0.158	0.029	0.211	0.0944	0.144	0.0217	0.0763	0.0269	0.00969	0.00707	0.1	0.022	0.0351	0.0351	0.0352	0.0353	0.1407
16.083	2.444	0.158	0.029	0.212	0.0946	0.145	0.0217	0.0764	0.0269	0.00969	0.00707	0.1	0.022	0.0352	0.0353	0.0353	0.0354	0.1412
16.167	2.461	0.159	0.029	0.212	0.0949	0.146	0.0218	0.0765	0.027	0.00969	0.00707	0.1	0.022	0.0354	0.0354	0.0354	0.0355	0.1417
16.25	2.479	0.159	0.029	0.213	0.0951	0.146	0.0219	0.0766	0.0271	0.00969	0.00707	0.1	0.022	0.0355	0.0356	0.0356	0.0357	0.1424
16.333	2.496	0.16	0.029	0.214	0.0954	0.147	0.022	0.0767	0.0271	0.00969	0.00707	0.1	0.022	0.0356	0.0357	0.0357	0.0358	0.1428
16.417	2.514	0.16	0.029	0.215	0.0956	0.148	0.022	0.0769	0.0272	0.00969	0.00707	0.1	0.022	0.0358	0.0358	0.0358	0.0359	0.1433
16.5	2.532	0.161	0.029	0.216	0.0959	0.149	0.0221	0.077	0.0272	0.00969	0.00707	0.1	0.022	0.0359	0.036	0.036	0.0361	0.144
16.583	2.55	0.161	0.029	0.216	0.0961	0.149	0.0222	0.0771	0.0273	0.00969	0.00707	0.1	0.022	0.036	0.0361	0.0361	0.0362	0.1444
16.667	2.569	0.162	0.029	0.217	0.0963	0.15	0.0222	0.0772	0.0273	0.00969	0.00707	0.1	0.022	0.0361	0.0362	0.0362	0.0363	0.1448
16.75	2.587	0.162	0.029	0.218	0.0966	0.15	0.0223	0.0773	0.0274	0.00969	0.00707	0.1	0.022	0.0363	0.0363	0.0363	0.0364	0.1453
16.833	2.605	0.162	0.029	0.219	0.0968	0.151	0.0223	0.0774	0.0274	0.00969	0.00707	0.1	0.022	0.0364	0.0364	0.0365	0.0365	0.1458
16.917	2.624	0.163	0.029	0.219	0.097	0.152	0.0224	0.0775	0.0274	0.00969	0.00707	0.1	0.022	0.0365	0.0366	0.0366	0.0367	0.1464
17	2.643	0.163	0.029	0.22	0.0972	0.152	0.0225	0.0776	0.0275	0.00969	0.00707	0.1	0.022	0.0366	0.0367	0.0367	0.0368	0.1468
17.083	2.662	0.164	0.029	0.221	0.0974	0.153	0.0225	0.0777	0.0275	0.00969	0.00707	0.1	0.022	0.0367	0.0368	0.0368	0.0369	0.1472
17.167	2.681	0.164	0.029	0.221	0.0976	0.153	0.0226	0.0778	0.0276	0.00969	0.00707	0.1	0.022	0.0368	0.0369	0.0369	0.037	0.1476
17.25	2.7	0.164	0.029	0.222	0.0978	0.154	0.0226	0.0779	0.0276	0.00969	0.00707	0.1	0.022	0.0369	0.037	0.037	0.0371	0.148
17.333	2.719	0.165	0.029	0.223	0.0979	0.155	0.0227	0.0779	0.0276	0.00969	0.00707	0.1	0.022	0.037	0.0371	0.0371	0.0372	0.1484
17.417	2.739	0.165	0.029	0.223	0.0981	0.155	0.0227	0.078	0.0277	0.00969	0.00707	0.1	0.022	0.0371	0.0372	0.0372	0.0373	0.1488
17.5	2.758	0.165	0.029	0.224	0.0983	0.156	0.0228	0.0781	0.0277	0.00969	0.00707	0.1	0.022	0.0372	0.0373	0.0373	0.0374	0.1492
17.583	2.778	0.166	0.029	0.224	0.0985	0.156	0.0228	0.0782	0.0278	0.00969	0.00707	0.1	0.022	0.0373	0.0374	0.0374	0.0375	0.1496
17.667	2.798	0.166	0.029	0.225	0.0986	0.157	0.0229	0.0783	0.0278	0.00969	0.00707	0.1	0.022	0.0374	0.0375	0.0375	0.0376	0.15
17.75	2.818	0.166	0.029	0.225	0.0988	0.157	0.0229	0.0784	0.0278	0.00969	0.00707	0.1	0.022	0.0375	0.0376	0.0376	0.0377	0.1504
17.833	2.838	0.167	0.029	0.226	0.0989	0.158	0.023	0.0784	0.0279	0.00969	0.00707	0.1	0.022	0.0376	0.0377	0.0377	0.0378	0.1508
17.917	2.858	0.167	0.029	0.227	0.0991	0.158	0.023	0.0785	0.0279	0.00969	0.00707	0.1	0.022	0.0377	0.0377	0.0378	0.0379	0.1511
18	2.878	0.167	0.029	0.227	0.0992	0.158	0.023	0.0786	0.0279	0.00969	0.00707	0.1	0.022	0.0378	0.0378	0.0379	0.038	0.1515
18.083	2.899	0.168	0.029	0.228	0.0994	0.159	0.0231	0.0786	0.028	0.0097	0.00707	0.1	0.022	0.0379	0.0379	0.0379	0.038	0.1517
18.167	2.919	0.168	0.029	0.228	0.0995	0.159	0.0231	0.0787	0.028	0.0097	0.00708	0.1	0.0221	0.0379	0.038	0.038	0.0381	0.152
18.25	2.939	0.168	0.029	0.229	0.0997	0.16	0.0232	0.0788	0.028	0.00971	0.00709	0.1	0.0221	0.038	0.0381	0.0381	0.0382	0.1524
18.333	2.959	0.168	0.029	0.229	0.0998	0.16	0.0232	0.0789	0.0281	0.00973	0.00712	0.1	0.0222	0.0381	0.0381	0.0382	0.0383	0.1527
18.417	2.979	0.169	0.029	0.229	0.0999	0.161	0.0232	0.0789	0.0281	0.00975	0.00715	0.1	0.0224	0.0382	0.0382	0.0382	0.0384	0.153
18.5	2.999	0.169	0.0291	0.23	0.1	0.161	0.0233	0.079	0.0282	0.00977	0.00718	0.1	0.0225	0.0383	0.0383	0.0383	0.0384	0.1533
18.583	3.019	0.169	0.0291	0.23	0.1	0.162	0.0233	0.0791	0.0282	0.00981	0.00724	0.1	0.0228	0.0383	0.0384	0.0384	0.0385	0.1536
18.667	3.039	0.17	0.0292	0.231	0.1	0.162	0.0234	0.0792	0.0282	0.00985	0.00731	0.1	0.0231	0.0384	0.0385	0.0385	0.0386	0.154
18.75	3.059	0.17	0.0292	0.231	0.101	0.162	0.0234	0.0793	0.0283	0.00989	0.00737	0.1	0.0234	0.0385	0.0385	0.0386	0.0387	0.1543
18.833	3.079	0.17	0.0293	0.232	0.101	0.163	0.0235	0.0794	0.0283	0.00995	0.00746	0.1	0.0238	0.0386	0.0386	0.0386	0.0387	0.1545

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
18.917	3.099	0.171	0.0293	0.232	0.101	0.163	0.0235	0.0796	0.0284	0.01	0.00756	0.1	0.0242	0.0387	0.0387	0.0387	0.0388	0.1549
19	3.119	0.171	0.0294	0.233	0.101	0.164	0.0235	0.0797	0.0284	0.0101	0.00765	0.1	0.0245	0.0387	0.0388	0.0388	0.0389	0.1552
19.083	3.139	0.171	0.0295	0.233	0.101	0.164	0.0236	0.0798	0.0285	0.0102	0.00775	0.1	0.0249	0.0388	0.0389	0.0389	0.039	0.1556
19.167	3.159	0.171	0.0296	0.234	0.101	0.165	0.0236	0.08	0.0285	0.0102	0.00785	0.1	0.0252	0.0389	0.0389	0.039	0.0391	0.1559
19.25	3.179	0.172	0.0297	0.234	0.102	0.165	0.0237	0.0801	0.0286	0.0103	0.00795	0.1	0.0255	0.039	0.039	0.039	0.0391	0.1561
19.333	3.198	0.172	0.0298	0.235	0.102	0.165	0.0237	0.0803	0.0286	0.0104	0.00804	0.1	0.0258	0.0391	0.0391	0.0391	0.0392	0.1565
19.417	3.218	0.172	0.0299	0.235	0.102	0.166	0.0238	0.0804	0.0287	0.0105	0.00812	0.1	0.026	0.0391	0.0392	0.0392	0.0393	0.1568
19.5	3.238	0.173	0.03	0.236	0.102	0.166	0.0238	0.0806	0.0288	0.0106	0.00821	0.1	0.0262	0.0392	0.0393	0.0393	0.0394	0.1572
19.583	3.258	0.173	0.0302	0.236	0.102	0.167	0.0239	0.0808	0.0288	0.0107	0.00827	0.1	0.0264	0.0393	0.0394	0.0394	0.0395	0.1576
19.667	3.277	0.173	0.0303	0.237	0.103	0.167	0.0239	0.081	0.0289	0.0108	0.00833	0.1	0.0266	0.0394	0.0394	0.0395	0.0396	0.1579
19.75	3.297	0.174	0.0305	0.237	0.103	0.167	0.024	0.0811	0.0289	0.0109	0.0084	0.1	0.0267	0.0395	0.0395	0.0395	0.0396	0.1581
19.833	3.317	0.174	0.0306	0.238	0.103	0.168	0.024	0.0813	0.029	0.011	0.00844	0.1	0.0269	0.0396	0.0396	0.0396	0.0397	0.1585
19.917	3.336	0.175	0.0308	0.238	0.103	0.168	0.0241	0.0815	0.0291	0.0111	0.00849	0.1	0.027	0.0396	0.0397	0.0397	0.0398	0.1588
20	3.356	0.175	0.031	0.239	0.103	0.169	0.0241	0.0817	0.0291	0.0111	0.00854	0.1	0.0271	0.0397	0.0398	0.0398	0.0399	0.1592
20.083	3.375	0.175	0.0312	0.239	0.104	0.169	0.0242	0.082	0.0292	0.0112	0.00858	0.1	0.0272	0.0398	0.0399	0.0399	0.04	0.1596
20.167	3.395	0.176	0.0313	0.24	0.104	0.17	0.0242	0.0822	0.0293	0.0113	0.00861	0.1	0.0273	0.0399	0.04	0.04	0.0401	0.16
20.25	3.414	0.176	0.0315	0.24	0.104	0.17	0.0243	0.0824	0.0294	0.0114	0.00865	0.1	0.0274	0.04	0.0401	0.0401	0.0402	0.1604
20.333	3.434	0.176	0.0317	0.241	0.104	0.17	0.0243	0.0827	0.0294	0.0114	0.00868	0.1	0.0274	0.0401	0.0401	0.0402	0.0403	0.1607
20.417	3.453	0.177	0.0319	0.242	0.105	0.171	0.0244	0.0829	0.0295	0.0115	0.00871	0.1	0.0274	0.0402	0.0402	0.0403	0.0404	0.1611
20.5	3.473	0.177	0.0321	0.242	0.105	0.171	0.0244	0.0832	0.0296	0.0115	0.00873	0.1	0.0275	0.0403	0.0403	0.0403	0.0405	0.1614
20.583	3.492	0.178	0.0322	0.243	0.105	0.172	0.0245	0.0834	0.0297	0.0116	0.00875	0.1	0.0275	0.0404	0.0404	0.0404	0.0406	0.1618
20.667	3.511	0.178	0.0324	0.243	0.105	0.172	0.0246	0.0837	0.0297	0.0116	0.00877	0.1	0.0275	0.0405	0.0405	0.0405	0.0407	0.1622
20.75	3.531	0.179	0.0326	0.244	0.106	0.172	0.0246	0.084	0.0298	0.0117	0.00879	0.1	0.0275	0.0406	0.0406	0.0406	0.0407	0.1625
20.833	3.55	0.179	0.0327	0.244	0.106	0.173	0.0247	0.0843	0.0299	0.0117	0.0088	0.1	0.0275	0.0407	0.0407	0.0407	0.0408	0.1629
20.917	3.569	0.179	0.0329	0.245	0.106	0.173	0.0247	0.0846	0.03	0.0117	0.00881	0.1	0.0275	0.0408	0.0408	0.0408	0.0409	0.1633
21	3.589	0.18	0.033	0.246	0.107	0.174	0.0248	0.0849	0.0301	0.0118	0.00883	0.1	0.0275	0.0409	0.0409	0.0409	0.041	0.1637
21.083	3.608	0.18	0.0332	0.246	0.107	0.174	0.0249	0.0852	0.0302	0.0118	0.00883	0.1	0.0275	0.041	0.041	0.041	0.0411	0.1641
21.167	3.627	0.181	0.0333	0.247	0.107	0.174	0.0249	0.0855	0.0303	0.0118	0.00883	0.1	0.0275	0.0411	0.0411	0.0411	0.0412	0.1645
21.25	3.646	0.181	0.0335	0.247	0.107	0.175	0.025	0.0858	0.0304	0.0119	0.00883	0.1	0.0275	0.0412	0.0412	0.0412	0.0413	0.1649
21.333	3.665	0.182	0.0336	0.248	0.108	0.175	0.0251	0.0862	0.0304	0.0119	0.00883	0.1	0.0275	0.0413	0.0413	0.0413	0.0414	0.1653
21.417	3.684	0.182	0.0337	0.249	0.108	0.176	0.0251	0.0865	0.0305	0.0119	0.00883	0.1	0.0275	0.0414	0.0414	0.0414	0.0416	0.1658
21.5	3.703	0.183	0.0338	0.249	0.108	0.176	0.0252	0.0868	0.0306	0.012	0.00883	0.1	0.0275	0.0415	0.0415	0.0415	0.0417	0.1662
21.583	3.722	0.183	0.0339	0.25	0.109	0.176	0.0253	0.0872	0.0307	0.012	0.00883	0.1	0.0275	0.0416	0.0416	0.0417	0.0418	0.1667
21.667	3.741	0.184	0.0341	0.251	0.109	0.177	0.0253	0.0875	0.0308	0.012	0.00883	0.1	0.0275	0.0417	0.0417	0.0418	0.0419	0.1671
21.75	3.76	0.184	0.0342	0.251	0.109	0.177	0.0254	0.0878	0.0309	0.012	0.00883	0.1	0.0275	0.0418	0.0418	0.0419	0.042	0.1675
21.833	3.779	0.185	0.0343	0.252	0.11	0.178	0.0255	0.0881	0.031	0.012	0.00883	0.1	0.0275	0.0419	0.042	0.042	0.0421	0.168
21.917	3.798	0.185	0.0344	0.253	0.11	0.178	0.0255	0.0884	0.0311	0.012	0.00883	0.1	0.0275	0.042	0.0421	0.0421	0.0422	0.1684
22	3.817	0.186	0.0345	0.253	0.11	0.178	0.0256	0.0887	0.0312	0.0121	0.00883	0.1	0.0275	0.0421	0.0422	0.0422	0.0423	0.1688
22.083	3.836	0.186	0.0346	0.254	0.111	0.179	0.0257	0.089	0.0314	0.0121	0.00883	0.1	0.0275	0.0422	0.0423	0.0423	0.0424	0.1692
22.167	3.854	0.187	0.0346	0.255	0.111	0.179	0.0258	0.0893	0.0315	0.0121	0.00883	0.1	0.0275	0.0424	0.0424	0.0424	0.0425	0.1697
22.25	3.873	0.188	0.0347	0.255	0.111	0.18	0.0258	0.0896	0.0316	0.0121	0.00883	0.1	0.0275	0.0425	0.0425	0.0426	0.0427	0.1703
22.333	3.892	0.188	0.0348	0.256	0.112	0.18	0.0259	0.0899	0.0317	0.0121	0.00883	0.1	0.0275	0.0426	0.0426	0.0427	0.0428	0.1707
22.417	3.911	0.189	0.0349	0.257	0.112	0.181	0.026	0.0901	0.0318	0.0121	0.00883	0.1	0.0275	0.0427	0.0428	0.0428	0.0429	0.1712
22.5	3.929	0.189	0.035	0.257	0.112	0.181	0.0261	0.0904	0.0319	0.0121	0.00883	0.1	0.0275	0.0428	0.0429	0.0429	0.043	0.1716
22.583	3.948	0.19	0.035	0.258	0.113	0.181	0.0261	0.0907	0.032	0.0121	0.00883	0.1	0.0275	0.043	0.043	0.043	0.0431	0.1721
22.667	3.967	0.19	0.0351	0.259	0.113	0.182	0.0262	0.0909	0.032	0.0121	0.00883	0.1	0.0275	0.0431	0.0431	0.0432	0.0433	0.1727
22.75	3.985	0.191	0.0352	0.26	0.114	0.182	0.0263	0.0912	0.0321	0.0121	0.00883	0.1	0.0275	0.0432	0.0433	0.0433	0.0434	0.1732
22.833	4.004	0.192	0.0352	0.26	0.114	0.183	0.0264	0.0914	0.0322	0.0121	0.00883	0.1	0.0275	0.0433	0.0434	0.0434	0.0435	0.1736
22.917	4.022	0.192	0.0353	0.261	0.114	0.183	0.0265	0.0917	0.0323	0.0121	0.00883	0.1	0.0275	0.0435	0.0435	0.0435	0.0437	0.1742
23	4.041	0.193	0.0353	0.262	0.115	0.184	0.0265	0.0919	0.0324	0.0121	0.00883	0.1	0.0275	0.0436	0.0436	0.0437	0.0438	0.1747
23.083	4.059	0.193	0.0354	0.263	0.115	0.184	0.0266	0.0921	0.0325	0.0121	0.00883	0.1	0.0275	0.0437	0.0438	0.0438	0.0439	0.1752
23.167	4.078	0.194	0.0355	0.263	0.115	0.184	0.0267	0.0924	0.0326	0.0121	0.00883	0.1	0.0275	0.0438	0.0439	0.0439	0.044	0.1756
23.25	4.096	0.195	0.0355	0.264	0.116	0.185	0.0268	0.0926	0.0327	0.0121	0.00883	0.1	0.0275	0.044	0.044	0.0441	0.0442	0.1763
23.333	4.114	0.195	0.0356	0.265	0.116	0.185	0.0269	0.0928	0.0327	0.0121	0.00883	0.1	0.0275	0.0441	0.0442	0.0442	0.0443	0.1768
23.417	4.133	0.196	0.0356	0.266	0.116	0.186	0.0269	0.093	0.0328	0.0121	0.00883	0.1	0.0275	0.0442	0.0443	0.0443	0.0444	0.1772
23.5	4.151	0.196	0.0357	0.267	0.117	0.186	0.027	0.0932	0.0329	0.0121	0.00883	0.1	0.0275	0.0444	0.0444	0.0444	0.0446	0.1778
23.583	4.169	0.197	0.0357	0.267	0.117	0.187	0.0271	0.0934	0.033	0.0121	0.00883	0.1	0.0275	0.0445	0.0445	0.0446	0.0447	0.1783
23.667	4.187	0.197	0.0358	0.268	0.117	0.187	0.0272	0.0936	0.0331	0.0121	0.00883	0.1	0.0275	0.0446	0.0447	0.0447	0.0448	0.1788
23.75	4.205	0.198	0.0358	0.269	0.117	0.188	0.0272	0.0938	0.0331	0.0121	0.00883	0.1	0.0275	0.0447	0.0448	0.0448	0.0449	0.1792
23.833	4.224	0.198	0.0359	0.27	0.118	0.188	0.0273	0.094	0.0332	0.0121	0.00883	0.1	0.0275	0.0449	0.0449	0.0449	0.0451	0.1798
23.917	4.242	0.199	0.0359	0.27	0.118	0.189	0.0274	0.0941	0.0333	0.0121	0.00883	0.1	0.0275	0.045	0.045	0.0451	0.0452	0.1803
24	4.26	0.199	0.0359	0.271	0.118	0.189	0.0275	0.0943	0.0334	0.0121	0.00883	0.1	0.0275	0.0451	0.0452	0.0452	0.0453	0.1808
24.083	4.278	0.2	0.036	0.272	0.118	0.189	0.0275	0.0945	0.0334	0.0121	0.00883	0.1	0.0275	0.0452	0.0453	0.0453	0.0454	0.1812

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
24.167	4.296	0.2	0.036	0.272	0.119	0.19	0.0276	0.0946	0.0335	0.0121	0.00883	0.1	0.0275	0.0453	0.0454	0.0454	0.0455	0.1816
24.25	4.314	0.201	0.036	0.273	0.119	0.19	0.0277	0.0948	0.0336	0.0121	0.00883	0.1	0.0275	0.0455	0.0455	0.0455	0.0457	0.1822
24.333	4.332	0.201	0.0361	0.274	0.119	0.191	0.0277	0.0949	0.0336	0.0121	0.00883	0.1	0.0275	0.0456	0.0456	0.0456	0.0458	0.1826
24.417	4.35	0.202	0.0361	0.274	0.12	0.191	0.0278	0.0951	0.0337	0.0121	0.00883	0.1	0.0275	0.0457	0.0457	0.0458	0.0459	0.1831
24.5	4.367	0.202	0.0361	0.275	0.12	0.192	0.0279	0.0952	0.0338	0.0121	0.00883	0.1	0.0275	0.0458	0.0458	0.0459	0.046	0.1835
24.583	4.385	0.203	0.0361	0.276	0.12	0.192	0.0279	0.0954	0.0338	0.0121	0.00883	0.1	0.0275	0.0459	0.046	0.046	0.0461	0.184
24.667	4.403	0.203	0.0361	0.276	0.12	0.193	0.028	0.0955	0.0339	0.0121	0.00883	0.1	0.0275	0.046	0.0461	0.0461	0.0462	0.1844
24.75	4.421	0.203	0.0362	0.277	0.12	0.193	0.028	0.0957	0.0339	0.0121	0.00883	0.1	0.0275	0.0461	0.0462	0.0462	0.0463	0.1848
24.833	4.438	0.204	0.0362	0.278	0.121	0.194	0.0281	0.0958	0.034	0.0121	0.00883	0.1	0.0275	0.0462	0.0463	0.0463	0.0464	0.1852
24.917	4.456	0.204	0.0362	0.278	0.121	0.194	0.0282	0.0959	0.0341	0.0121	0.00883	0.1	0.0275	0.0463	0.0464	0.0464	0.0465	0.1856
25	4.474	0.205	0.0362	0.279	0.121	0.195	0.0282	0.096	0.0341	0.0121	0.00883	0.1	0.0275	0.0464	0.0465	0.0465	0.0466	0.186
25.083	4.492	0.205	0.0362	0.28	0.121	0.195	0.0283	0.0962	0.0342	0.0121	0.00883	0.1	0.0275	0.0465	0.0466	0.0466	0.0467	0.1864
25.167	4.509	0.205	0.0362	0.28	0.122	0.196	0.0283	0.0963	0.0342	0.0121	0.00883	0.1	0.0275	0.0466	0.0467	0.0467	0.0468	0.1868
25.25	4.527	0.206	0.0362	0.281	0.122	0.196	0.0284	0.0964	0.0343	0.0121	0.00883	0.1	0.0275	0.0467	0.0468	0.0468	0.0469	0.1872
25.333	4.545	0.206	0.0362	0.281	0.122	0.197	0.0284	0.0965	0.0343	0.0121	0.00883	0.1	0.0275	0.0468	0.0469	0.0469	0.047	0.1876
25.417	4.563	0.207	0.0362	0.282	0.122	0.197	0.0285	0.0966	0.0344	0.0121	0.00883	0.1	0.0275	0.0469	0.047	0.047	0.0471	0.188
25.5	4.581	0.207	0.0362	0.282	0.122	0.197	0.0285	0.0968	0.0344	0.0121	0.00883	0.1	0.0275	0.047	0.0471	0.0471	0.0472	0.1884
25.583	4.599	0.207	0.0362	0.283	0.123	0.198	0.0286	0.0969	0.0345	0.0121	0.00883	0.1	0.0275	0.0471	0.0471	0.0472	0.0473	0.1887
25.667	4.617	0.208	0.0362	0.284	0.123	0.198	0.0286	0.097	0.0345	0.0121	0.00883	0.1	0.0275	0.0472	0.0472	0.0473	0.0474	0.1891
25.75	4.635	0.208	0.0362	0.284	0.123	0.199	0.0287	0.0971	0.0346	0.0121	0.00883	0.1	0.0275	0.0473	0.0473	0.0473	0.0475	0.1894
25.833	4.653	0.208	0.0362	0.285	0.123	0.199	0.0287	0.0972	0.0346	0.0121	0.00883	0.1	0.0275	0.0473	0.0474	0.0474	0.0476	0.1897
25.917	4.672	0.209	0.0362	0.285	0.123	0.2	0.0288	0.0973	0.0347	0.0121	0.00883	0.1	0.0275	0.0474	0.0475	0.0475	0.0476	0.19
26	4.69	0.209	0.0362	0.286	0.123	0.2	0.0288	0.0974	0.0347	0.0121	0.00883	0.1	0.0275	0.0475	0.0476	0.0476	0.0477	0.1904
26.083	4.708	0.209	0.0362	0.286	0.124	0.2	0.0289	0.0975	0.0347	0.0121	0.00883	0.1	0.0275	0.0476	0.0477	0.0477	0.0478	0.1908
26.167	4.726	0.21	0.0362	0.287	0.124	0.201	0.0289	0.0976	0.0348	0.0121	0.00883	0.1	0.0275	0.0477	0.0477	0.0478	0.0479	0.1911
26.25	4.745	0.21	0.0362	0.287	0.124	0.201	0.0289	0.0977	0.0348	0.0121	0.00883	0.1	0.0275	0.0478	0.0478	0.0478	0.048	0.1914
26.333	4.763	0.21	0.0362	0.287	0.124	0.202	0.029	0.0977	0.0349	0.0121	0.00883	0.1	0.0275	0.0478	0.0479	0.0479	0.048	0.1916
26.417	4.782	0.21	0.0362	0.288	0.124	0.202	0.029	0.0978	0.0349	0.0121	0.00883	0.1	0.0275	0.0479	0.048	0.048	0.0481	0.192
26.5	4.8	0.211	0.0362	0.288	0.124	0.202	0.0291	0.0979	0.0349	0.0121	0.00883	0.1	0.0275	0.048	0.048	0.0481	0.0482	0.1923
26.583	4.819	0.211	0.0362	0.289	0.125	0.203	0.0291	0.098	0.035	0.0121	0.00883	0.1	0.0275	0.048	0.0481	0.0481	0.0483	0.1925
26.667	4.837	0.211	0.0362	0.289	0.125	0.203	0.0291	0.0981	0.035	0.0121	0.00883	0.1	0.0275	0.0481	0.0482	0.0482	0.0483	0.1928
26.75	4.856	0.212	0.0362	0.29	0.125	0.204	0.0292	0.0982	0.035	0.0121	0.00883	0.1	0.0275	0.0482	0.0482	0.0483	0.0484	0.1931
26.833	4.875	0.212	0.0362	0.29	0.125	0.204	0.0292	0.0982	0.0351	0.0121	0.00883	0.1	0.0275	0.0483	0.0483	0.0483	0.0485	0.1934
26.917	4.894	0.212	0.0362	0.29	0.125	0.204	0.0292	0.0983	0.0351	0.0121	0.00883	0.1	0.0275	0.0483	0.0484	0.0484	0.0485	0.1936
27	4.912	0.212	0.0362	0.291	0.125	0.205	0.0293	0.0984	0.0351	0.0121	0.00883	0.1	0.0275	0.0484	0.0484	0.0485	0.0486	0.1939
27.083	4.931	0.213	0.0362	0.291	0.125	0.205	0.0293	0.0984	0.0352	0.0121	0.00884	0.1	0.0275	0.0484	0.0485	0.0485	0.0487	0.1941
27.167	4.95	0.213	0.0362	0.292	0.126	0.205	0.0294	0.0985	0.0352	0.0121	0.00884	0.1	0.0275	0.0485	0.0486	0.0486	0.0487	0.1944
27.25	4.969	0.213	0.0362	0.292	0.126	0.206	0.0294	0.0986	0.0352	0.0121	0.00884	0.1	0.0275	0.0486	0.0486	0.0487	0.0488	0.1947
27.333	4.988	0.213	0.0362	0.292	0.126	0.206	0.0294	0.0987	0.0353	0.0121	0.00886	0.1	0.0276	0.0486	0.0487	0.0487	0.0489	0.1949
27.417	5.007	0.213	0.0363	0.293	0.126	0.206	0.0295	0.0987	0.0353	0.0121	0.00888	0.1	0.0277	0.0487	0.0488	0.0488	0.0489	0.1952
27.5	5.026	0.214	0.0363	0.293	0.126	0.207	0.0295	0.0988	0.0354	0.0122	0.0089	0.1	0.0278	0.0488	0.0488	0.0488	0.049	0.1954
27.583	5.045	0.214	0.0363	0.294	0.126	0.207	0.0295	0.0989	0.0354	0.0122	0.00895	0.1	0.0281	0.0488	0.0489	0.0489	0.049	0.1956
27.667	5.064	0.214	0.0364	0.294	0.126	0.207	0.0296	0.099	0.0354	0.0122	0.00901	0.1	0.0283	0.0489	0.0489	0.049	0.0491	0.1959
27.75	5.084	0.214	0.0364	0.294	0.127	0.208	0.0296	0.0991	0.0355	0.0123	0.00906	0.1	0.0286	0.0489	0.049	0.049	0.0492	0.1961
27.833	5.103	0.215	0.0365	0.295	0.127	0.208	0.0296	0.0992	0.0355	0.0123	0.00915	0.1	0.0289	0.049	0.0491	0.0491	0.0492	0.1964
27.917	5.122	0.215	0.0365	0.295	0.127	0.208	0.0297	0.0993	0.0356	0.0124	0.00923	0.1	0.0293	0.0491	0.0491	0.0492	0.0493	0.1967
28	5.141	0.215	0.0366	0.295	0.127	0.209	0.0297	0.0994	0.0356	0.0124	0.00932	0.1	0.0297	0.0491	0.0492	0.0492	0.0494	0.1969
28.083	5.161	0.216	0.0367	0.296	0.127	0.209	0.0297	0.0996	0.0357	0.0125	0.00943	0.1	0.0301	0.0492	0.0493	0.0493	0.0494	0.1972
28.167	5.18	0.216	0.0368	0.296	0.127	0.209	0.0298	0.0997	0.0357	0.0126	0.00953	0.1	0.0304	0.0493	0.0493	0.0494	0.0495	0.1975
28.25	5.2	0.216	0.0368	0.297	0.128	0.21	0.0298	0.0998	0.0358	0.0127	0.00964	0.1	0.0308	0.0493	0.0494	0.0494	0.0496	0.1977
28.333	5.219	0.216	0.037	0.297	0.128	0.21	0.0299	0.1	0.0358	0.0128	0.00973	0.1	0.031	0.0494	0.0495	0.0495	0.0496	0.198
28.417	5.239	0.217	0.0371	0.298	0.128	0.211	0.0299	0.1	0.0359	0.0129	0.00982	0.1	0.0313	0.0495	0.0495	0.0496	0.0497	0.1983
28.5	5.259	0.217	0.0372	0.298	0.128	0.211	0.03	0.1	0.0359	0.013	0.00991	0.1	0.0316	0.0496	0.0496	0.0496	0.0498	0.1986
28.583	5.278	0.217	0.0373	0.298	0.128	0.211	0.03	0.1	0.036	0.0131	0.00998	0.1	0.0317	0.0496	0.0497	0.0497	0.0498	0.1988
28.667	5.298	0.218	0.0374	0.299	0.129	0.212	0.0301	0.101	0.0361	0.0132	0.01	0.1	0.0319	0.0497	0.0498	0.0498	0.0499	0.1992
28.75	5.318	0.218	0.0376	0.299	0.129	0.212	0.0301	0.101	0.0361	0.0132	0.0101	0.1	0.0321	0.0498	0.0498	0.0499	0.05	0.1995
28.833	5.338	0.219	0.0377	0.3	0.129	0.212	0.0302	0.101	0.0362	0.0133	0.0102	0.1	0.0323	0.0499	0.0499	0.0499	0.0501	0.1998
28.917	5.358	0.219	0.0379	0.3	0.129	0.213	0.0302	0.101	0.0363	0.0134	0.0102	0.1	0.0324	0.0499	0.05	0.05	0.0502	0.2001
29	5.378	0.219	0.038	0.301	0.129	0.213	0.0302	0.101	0.0363	0.0135	0.0103	0.1	0.0325	0.05	0.0501	0.0501	0.0502	0.2004
29.083	5.398	0.22	0.0382	0.301	0.13	0.214	0.0303	0.102	0.0364	0.0136	0.0103	0.1	0.0326	0.0501	0.0501	0.0502	0.0503	0.2007
29.167	5.418	0.22	0.0384	0.302	0.13	0.214	0.0304	0.102	0.0365	0.0136	0.0103	0.1	0.0327	0.0502	0.0502	0.0503	0.0504	0.2011
29.25	5.438	0.22	0.0386	0.302	0.13	0.214	0.0304	0.102	0.0365	0.0137	0.0104	0.1	0.0328	0.0503	0.0503	0.0503	0.0505	0.2014
29.333	5.458	0.221	0.0388	0.303	0.13	0.215	0.0305	0.102	0.0366	0.0138	0.0104	0.1	0.0329	0.0503	0.0504	0.0504	0.0506	0.2017

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
29.417	5.478	0.221	0.039	0.303	0.131	0.215	0.0305	0.103	0.0367	0.0138	0.0105	0.1	0.0329	0.0504	0.0505	0.0505	0.0506	0.202
29.5	5.498	0.222	0.0392	0.304	0.131	0.215	0.0306	0.103	0.0368	0.0139	0.0105	0.1	0.033	0.0505	0.0506	0.0506	0.0507	0.2024
29.583	5.519	0.222	0.0393	0.304	0.131	0.216	0.0306	0.103	0.0368	0.014	0.0105	0.1	0.033	0.0506	0.0507	0.0507	0.0508	0.2028
29.667	5.539	0.222	0.0395	0.305	0.131	0.216	0.0307	0.103	0.0369	0.014	0.0105	0.1	0.033	0.0507	0.0508	0.0508	0.0509	0.2032
29.75	5.559	0.223	0.0397	0.305	0.132	0.217	0.0307	0.104	0.037	0.014	0.0105	0.1	0.033	0.0508	0.0508	0.0509	0.051	0.2035
29.833	5.58	0.223	0.0398	0.306	0.132	0.217	0.0308	0.104	0.0371	0.0141	0.0106	0.1	0.033	0.0509	0.0509	0.051	0.0511	0.2039
29.917	5.6	0.224	0.04	0.306	0.132	0.217	0.0309	0.104	0.0372	0.0141	0.0106	0.1	0.033	0.051	0.051	0.0511	0.0512	0.2043
30	5.621	0.224	0.0402	0.307	0.132	0.218	0.0309	0.104	0.0372	0.0142	0.0106	0.1	0.033	0.0511	0.0511	0.0512	0.0513	0.2047
30.083	5.642	0.225	0.0403	0.308	0.133	0.218	0.031	0.105	0.0373	0.0142	0.0106	0.1	0.033	0.0512	0.0512	0.0513	0.0514	0.2051
30.167	5.662	0.225	0.0404	0.308	0.133	0.219	0.0311	0.105	0.0374	0.0142	0.0106	0.1	0.033	0.0513	0.0513	0.0514	0.0515	0.2055
30.25	5.683	0.226	0.0406	0.309	0.133	0.219	0.0311	0.105	0.0375	0.0143	0.0106	0.1	0.033	0.0514	0.0514	0.0515	0.0516	0.2059
30.333	5.704	0.226	0.0407	0.309	0.134	0.219	0.0312	0.106	0.0376	0.0143	0.0106	0.1	0.0331	0.0515	0.0515	0.0516	0.0517	0.2063
30.417	5.725	0.227	0.0409	0.31	0.134	0.22	0.0312	0.106	0.0377	0.0143	0.0106	0.1	0.0332	0.0516	0.0516	0.0517	0.0518	0.2067
30.5	5.746	0.227	0.041	0.311	0.134	0.22	0.0313	0.106	0.0378	0.0144	0.0107	0.1	0.0333	0.0517	0.0517	0.0518	0.0519	0.2071
30.583	5.767	0.228	0.0412	0.311	0.135	0.221	0.0314	0.107	0.0379	0.0144	0.0107	0.1	0.0335	0.0518	0.0519	0.0519	0.052	0.2076
30.667	5.788	0.228	0.0413	0.312	0.135	0.221	0.0315	0.107	0.038	0.0145	0.0108	0.1	0.0337	0.0519	0.052	0.052	0.0521	0.208
30.75	5.809	0.229	0.0415	0.313	0.135	0.222	0.0315	0.108	0.0381	0.0146	0.0108	0.1	0.034	0.052	0.0521	0.0521	0.0523	0.2085
30.833	5.83	0.229	0.0416	0.313	0.136	0.222	0.0316	0.108	0.0382	0.0146	0.0109	0.1	0.0343	0.0521	0.0522	0.0522	0.0524	0.2089
30.917	5.851	0.23	0.0418	0.314	0.136	0.222	0.0317	0.108	0.0384	0.0147	0.011	0.1	0.0347	0.0523	0.0523	0.0524	0.0525	0.2095
31	5.872	0.23	0.042	0.315	0.136	0.223	0.0318	0.109	0.0385	0.0148	0.0111	0.1	0.0351	0.0524	0.0525	0.0525	0.0526	0.21
31.083	5.893	0.231	0.0421	0.316	0.137	0.223	0.0319	0.109	0.0386	0.0149	0.0112	0.1	0.0355	0.0525	0.0526	0.0526	0.0528	0.2105
31.167	5.915	0.232	0.0423	0.316	0.137	0.224	0.0319	0.109	0.0387	0.0149	0.0113	0.1	0.0358	0.0527	0.0527	0.0527	0.0529	0.211
31.25	5.936	0.232	0.0425	0.317	0.138	0.224	0.032	0.11	0.0389	0.015	0.0114	0.1	0.0362	0.0528	0.0529	0.0529	0.053	0.2116
31.333	5.958	0.233	0.0427	0.318	0.138	0.225	0.0321	0.11	0.039	0.0151	0.0115	0.1	0.0365	0.0529	0.053	0.053	0.0532	0.2121
31.417	5.979	0.234	0.0428	0.319	0.139	0.225	0.0322	0.111	0.0391	0.0152	0.0116	0.1	0.0367	0.0531	0.0531	0.0532	0.0533	0.2127
31.5	6.001	0.234	0.043	0.32	0.139	0.226	0.0323	0.111	0.0393	0.0153	0.0117	0.1	0.037	0.0532	0.0533	0.0533	0.0535	0.2133
31.583	6.022	0.235	0.0432	0.321	0.139	0.226	0.0324	0.111	0.0394	0.0154	0.0117	0.1	0.0372	0.0534	0.0534	0.0535	0.0536	0.2139
31.667	6.044	0.236	0.0434	0.322	0.14	0.227	0.0325	0.112	0.0395	0.0155	0.0118	0.1	0.0374	0.0535	0.0536	0.0536	0.0538	0.2145
31.75	6.066	0.237	0.0436	0.323	0.14	0.227	0.0326	0.112	0.0397	0.0156	0.0119	0.1	0.0376	0.0537	0.0537	0.0538	0.0539	0.2151
31.833	6.087	0.237	0.0439	0.324	0.141	0.228	0.0327	0.113	0.0398	0.0157	0.0119	0.1	0.0377	0.0538	0.0539	0.0539	0.0541	0.2157
31.917	6.109	0.238	0.0441	0.324	0.141	0.229	0.0328	0.113	0.0399	0.0158	0.012	0.1	0.0379	0.054	0.0541	0.0541	0.0542	0.2164
32	6.131	0.239	0.0443	0.325	0.142	0.229	0.0329	0.114	0.0401	0.0159	0.012	0.1	0.038	0.0541	0.0542	0.0542	0.0544	0.2169
32.083	6.153	0.24	0.0445	0.326	0.142	0.23	0.033	0.114	0.0402	0.016	0.0121	0.1	0.0381	0.0543	0.0544	0.0544	0.0546	0.2177
32.167	6.175	0.241	0.0448	0.327	0.143	0.23	0.0331	0.114	0.0403	0.0161	0.0121	0.1	0.0382	0.0545	0.0546	0.0546	0.0547	0.2184
32.25	6.197	0.241	0.045	0.329	0.143	0.231	0.0333	0.115	0.0405	0.0161	0.0121	0.1	0.0383	0.0547	0.0547	0.0548	0.0549	0.2191
32.333	6.219	0.242	0.0453	0.33	0.144	0.231	0.0334	0.115	0.0406	0.0162	0.0122	0.1	0.0384	0.0548	0.0549	0.0549	0.0551	0.2197
32.417	6.242	0.243	0.0455	0.331	0.144	0.232	0.0335	0.116	0.0407	0.0162	0.0122	0.1	0.0384	0.055	0.0551	0.0551	0.0553	0.2205
32.5	6.264	0.244	0.0458	0.332	0.145	0.232	0.0336	0.116	0.0409	0.0163	0.0122	0.1	0.0385	0.0552	0.0553	0.0553	0.0554	0.2212
32.583	6.286	0.245	0.046	0.333	0.145	0.233	0.0337	0.117	0.041	0.0164	0.0123	0.1	0.0385	0.0554	0.0554	0.0555	0.0556	0.2219
32.667	6.309	0.245	0.0462	0.334	0.146	0.234	0.0338	0.117	0.0411	0.0164	0.0123	0.1	0.0385	0.0556	0.0556	0.0556	0.0558	0.2226
32.75	6.331	0.246	0.0464	0.335	0.146	0.234	0.0339	0.118	0.0413	0.0165	0.0123	0.1	0.0385	0.0557	0.0558	0.0558	0.056	0.2233
32.833	6.353	0.247	0.0466	0.336	0.147	0.235	0.034	0.118	0.0414	0.0165	0.0123	0.1	0.0385	0.0559	0.056	0.056	0.0562	0.2241
32.917	6.376	0.248	0.0468	0.337	0.147	0.235	0.0341	0.119	0.0416	0.0165	0.0123	0.1	0.0385	0.0561	0.0562	0.0562	0.0563	0.2248
33	6.398	0.249	0.047	0.338	0.148	0.236	0.0343	0.119	0.0417	0.0166	0.0124	0.1	0.0385	0.0563	0.0563	0.0564	0.0565	0.2255
33.083	6.421	0.249	0.0472	0.339	0.148	0.237	0.0344	0.12	0.0419	0.0166	0.0124	0.1	0.0385	0.0564	0.0565	0.0565	0.0567	0.2261
33.167	6.444	0.25	0.0474	0.34	0.148	0.237	0.0345	0.12	0.042	0.0166	0.0124	0.1	0.0385	0.0566	0.0567	0.0567	0.0569	0.2269
33.25	6.467	0.251	0.0476	0.341	0.149	0.238	0.0346	0.12	0.0422	0.0167	0.0124	0.1	0.0385	0.0568	0.0569	0.0569	0.0571	0.2277
33.333	6.49	0.252	0.0477	0.342	0.149	0.239	0.0347	0.121	0.0423	0.0167	0.0124	0.1	0.0386	0.057	0.0571	0.0571	0.0572	0.2284
33.417	6.513	0.253	0.0479	0.344	0.15	0.239	0.0348	0.121	0.0425	0.0168	0.0124	0.1	0.0387	0.0572	0.0572	0.0573	0.0574	0.2291
33.5	6.535	0.254	0.0481	0.345	0.15	0.24	0.0349	0.122	0.0426	0.0168	0.0124	0.1	0.0387	0.0574	0.0574	0.0575	0.0576	0.2299
33.583	6.559	0.254	0.0482	0.346	0.151	0.241	0.035	0.122	0.0428	0.0169	0.0125	0.1	0.039	0.0575	0.0576	0.0577	0.0578	0.2306
33.667	6.582	0.255	0.0484	0.347	0.151	0.241	0.0352	0.123	0.0429	0.0169	0.0125	0.1	0.0392	0.0577	0.0578	0.0578	0.058	0.2313
33.75	6.605	0.256	0.0486	0.348	0.152	0.242	0.0353	0.123	0.0431	0.017	0.0126	0.1	0.0394	0.0579	0.058	0.058	0.0582	0.2321
33.833	6.628	0.257	0.0488	0.349	0.153	0.243	0.0354	0.124	0.0433	0.017	0.0126	0.1	0.0398	0.0581	0.0582	0.0582	0.0584	0.2329
33.917	6.651	0.258	0.0489	0.35	0.153	0.244	0.0355	0.125	0.0434	0.0171	0.0127	0.1	0.0401	0.0583	0.0584	0.0584	0.0586	0.2337
34	6.675	0.259	0.0491	0.352	0.154	0.244	0.0356	0.125	0.0436	0.0172	0.0128	0.1	0.0405	0.0585	0.0586	0.0586	0.0588	0.2345
34.083	6.698	0.26	0.0493	0.353	0.154	0.245	0.0358	0.126	0.0438	0.0173	0.0129	0.1	0.0409	0.0587	0.0588	0.0588	0.059	0.2353
34.167	6.722	0.261	0.0495	0.354	0.155	0.246	0.0359	0.126	0.0439	0.0173	0.013	0.1	0.0412	0.0589	0.059	0.059	0.0592	0.2361
34.25	6.745	0.262	0.0497	0.355	0.155	0.247	0.036	0.127	0.0441	0.0174	0.0131	0.1	0.0416	0.0591	0.0592	0.0592	0.0594	0.2369
34.333	6.769	0.262	0.0498	0.356	0.156	0.247	0.0361	0.127	0.0443	0.0175	0.0132	0.1	0.0419	0.0593	0.0594	0.0594	0.0596	0.2377
34.417	6.792	0.263	0.05	0.358	0.156	0.248	0.0363	0.128	0.0445	0.0176	0.0133	0.1	0.0422	0.0595	0.0596	0.0596	0.0598	0.2385
34.5	6.816	0.264	0.0502	0.359	0.157	0.249	0.0364	0.128	0.0447	0.0177	0.0134	0.1	0.0424	0.0597	0.0598	0.0598	0.06	0.2393
34.583	6.84	0.265	0.0504	0.36	0.158	0.25	0.0365	0.129	0.0448	0.0178	0.0135	0.1	0.0426	0.06	0.06	0.0601	0.0602	0.2403

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
34.667	6.864	0.266	0.0506	0.362	0.158	0.251	0.0367	0.129	0.045	0.0179	0.0135	0.1	0.0428	0.0602	0.0602	0.0603	0.0604	0.2411
34.75	6.888	0.267	0.0508	0.363	0.159	0.251	0.0368	0.13	0.0452	0.018	0.0136	0.1	0.043	0.0604	0.0605	0.0605	0.0606	0.242
34.833	6.912	0.268	0.051	0.364	0.16	0.252	0.0369	0.13	0.0454	0.0181	0.0137	0.1	0.0432	0.0606	0.0607	0.0607	0.0609	0.2429
34.917	6.936	0.269	0.0513	0.365	0.16	0.253	0.0371	0.131	0.0455	0.0182	0.0137	0.1	0.0433	0.0608	0.0609	0.0609	0.0611	0.2437
35	6.96	0.27	0.0515	0.367	0.161	0.254	0.0372	0.131	0.0457	0.0183	0.0138	0.1	0.0435	0.061	0.0611	0.0611	0.0613	0.2445
35.083	6.984	0.271	0.0517	0.368	0.161	0.255	0.0374	0.132	0.0459	0.0184	0.0138	0.1	0.0436	0.0613	0.0613	0.0614	0.0615	0.2455
35.167	7.008	0.272	0.052	0.37	0.162	0.255	0.0375	0.132	0.0461	0.0185	0.0139	0.1	0.0437	0.0615	0.0616	0.0616	0.0618	0.2465
35.25	7.033	0.273	0.0522	0.371	0.163	0.256	0.0376	0.133	0.0462	0.0185	0.0139	0.1	0.0438	0.0617	0.0618	0.0618	0.062	0.2473
35.333	7.057	0.274	0.0524	0.372	0.163	0.257	0.0378	0.133	0.0464	0.0186	0.0139	0.1	0.0438	0.0619	0.062	0.0621	0.0622	0.2482
35.417	7.081	0.275	0.0527	0.374	0.164	0.258	0.0379	0.134	0.0466	0.0187	0.014	0.1	0.0439	0.0622	0.0622	0.0623	0.0625	0.2492
35.5	7.106	0.276	0.0529	0.375	0.164	0.259	0.0381	0.134	0.0468	0.0187	0.014	0.1	0.044	0.0624	0.0625	0.0625	0.0627	0.2501
35.583	7.131	0.277	0.0532	0.376	0.165	0.26	0.0382	0.135	0.0469	0.0188	0.014	0.1	0.044	0.0626	0.0627	0.0627	0.0629	0.2509
35.667	7.155	0.278	0.0534	0.378	0.166	0.26	0.0383	0.136	0.0471	0.0188	0.014	0.1	0.044	0.0629	0.0629	0.063	0.0631	0.2519
35.75	7.18	0.279	0.0536	0.379	0.166	0.261	0.0385	0.136	0.0473	0.0189	0.0141	0.1	0.044	0.0631	0.0632	0.0632	0.0634	0.2529
35.833	7.205	0.281	0.0538	0.381	0.167	0.262	0.0386	0.137	0.0475	0.0189	0.0141	0.1	0.044	0.0633	0.0634	0.0634	0.0636	0.2537
35.917	7.23	0.282	0.054	0.382	0.167	0.263	0.0388	0.137	0.0476	0.0189	0.0141	0.1	0.044	0.0635	0.0636	0.0637	0.0638	0.2546
36	7.254	0.283	0.0542	0.383	0.168	0.264	0.0389	0.138	0.0478	0.019	0.0141	0.1	0.044	0.0638	0.0638	0.0639	0.0641	0.2556
36.083	7.279	0.284	0.0544	0.385	0.169	0.265	0.039	0.138	0.048	0.019	0.0141	0.1	0.044	0.064	0.0641	0.0641	0.0643	0.2565
36.167	7.305	0.285	0.0546	0.386	0.169	0.265	0.0392	0.139	0.0482	0.0191	0.0141	0.1	0.044	0.0642	0.0643	0.0643	0.0645	0.2573
36.25	7.33	0.286	0.0548	0.387	0.17	0.266	0.0393	0.139	0.0484	0.0191	0.0141	0.1	0.044	0.0644	0.0645	0.0646	0.0647	0.2582
36.333	7.355	0.287	0.0549	0.389	0.171	0.267	0.0394	0.14	0.0485	0.0192	0.0142	0.1	0.0442	0.0647	0.0648	0.0648	0.065	0.2593
36.417	7.38	0.288	0.0551	0.39	0.171	0.268	0.0396	0.14	0.0487	0.0192	0.0142	0.1	0.0444	0.0649	0.065	0.065	0.0652	0.2601
36.5	7.405	0.289	0.0553	0.391	0.172	0.269	0.0397	0.141	0.0489	0.0193	0.0143	0.1	0.0446	0.0651	0.0652	0.0652	0.0654	0.2609
36.583	7.431	0.29	0.0556	0.393	0.172	0.27	0.0399	0.142	0.0491	0.0194	0.0144	0.1	0.0452	0.0654	0.0655	0.0655	0.0657	0.2621
36.667	7.456	0.291	0.0558	0.394	0.173	0.271	0.04	0.142	0.0493	0.0195	0.0145	0.1	0.0458	0.0656	0.0657	0.0657	0.0659	0.2629
36.75	7.482	0.292	0.056	0.396	0.174	0.272	0.0402	0.143	0.0496	0.0196	0.0146	0.1	0.0464	0.0659	0.0659	0.066	0.0662	0.264
36.833	7.508	0.293	0.0563	0.397	0.175	0.273	0.0403	0.144	0.0498	0.0198	0.0149	0.1	0.0475	0.0661	0.0662	0.0662	0.0664	0.2649
36.917	7.533	0.294	0.0566	0.399	0.175	0.274	0.0405	0.144	0.05	0.0199	0.0151	0.1	0.0485	0.0664	0.0665	0.0665	0.0667	0.2661
37	7.559	0.295	0.0569	0.4	0.176	0.275	0.0407	0.145	0.0502	0.0201	0.0153	0.1	0.0496	0.0666	0.0667	0.0667	0.0669	0.2669
37.083	7.585	0.297	0.0572	0.402	0.177	0.276	0.0408	0.146	0.0505	0.0203	0.0157	0.1	0.0507	0.0669	0.067	0.067	0.0672	0.2681
37.167	7.611	0.298	0.0576	0.404	0.178	0.277	0.041	0.146	0.0507	0.0206	0.016	0.1	0.0518	0.0672	0.0673	0.0673	0.0675	0.2693
37.25	7.637	0.299	0.0579	0.405	0.178	0.279	0.0412	0.147	0.051	0.0208	0.0163	0.1	0.0529	0.0674	0.0675	0.0676	0.0677	0.2702
37.333	7.663	0.301	0.0583	0.407	0.179	0.28	0.0414	0.148	0.0512	0.0211	0.0166	0.1	0.0538	0.0677	0.0678	0.0678	0.068	0.2713
37.417	7.689	0.302	0.0587	0.409	0.18	0.281	0.0415	0.149	0.0515	0.0214	0.0168	0.1	0.0546	0.068	0.0681	0.0681	0.0683	0.2725
37.5	7.715	0.303	0.0591	0.41	0.181	0.282	0.0417	0.15	0.0518	0.0216	0.0171	0.1	0.0555	0.0683	0.0684	0.0684	0.0686	0.2737
37.583	7.741	0.305	0.0595	0.412	0.182	0.283	0.0419	0.15	0.052	0.0219	0.0174	0.1	0.0561	0.0686	0.0687	0.0687	0.0689	0.2749
37.667	7.768	0.306	0.06	0.414	0.183	0.284	0.0421	0.151	0.0523	0.0222	0.0176	0.1	0.0567	0.0689	0.069	0.069	0.0692	0.2761
37.75	7.794	0.308	0.0604	0.416	0.184	0.286	0.0423	0.152	0.0526	0.0225	0.0178	0.1	0.0574	0.0692	0.0693	0.0693	0.0695	0.2773
37.833	7.821	0.309	0.061	0.418	0.185	0.287	0.0425	0.153	0.0528	0.0228	0.018	0.1	0.0578	0.0695	0.0696	0.0697	0.0698	0.2786
37.917	7.847	0.311	0.0615	0.42	0.186	0.288	0.0427	0.154	0.0531	0.0231	0.0181	0.1	0.0583	0.0699	0.0699	0.07	0.0702	0.28
38	7.874	0.312	0.062	0.422	0.187	0.289	0.0429	0.155	0.0534	0.0233	0.0183	0.1	0.0587	0.0702	0.0703	0.0703	0.0705	0.2813
38.083	7.9	0.314	0.0626	0.424	0.187	0.291	0.0432	0.156	0.0537	0.0236	0.0184	0.1	0.059	0.0705	0.0706	0.0706	0.0708	0.2825
38.167	7.927	0.316	0.0632	0.426	0.188	0.292	0.0434	0.157	0.054	0.0238	0.0186	0.1	0.0593	0.0708	0.0709	0.071	0.0712	0.2839
38.25	7.954	0.317	0.0638	0.428	0.189	0.293	0.0436	0.158	0.0543	0.024	0.0187	0.1	0.0597	0.0712	0.0713	0.0713	0.0715	0.2853
38.333	7.981	0.319	0.0644	0.43	0.19	0.294	0.0438	0.159	0.0546	0.0242	0.0188	0.101	0.0599	0.0715	0.0716	0.0717	0.0719	0.2867
38.417	8.009	0.32	0.065	0.432	0.191	0.296	0.0441	0.16	0.0549	0.0244	0.0189	0.101	0.0601	0.0719	0.072	0.072	0.0722	0.2881
38.5	8.036	0.322	0.0656	0.434	0.192	0.297	0.0443	0.161	0.0552	0.0246	0.019	0.102	0.0603	0.0722	0.0723	0.0724	0.0726	0.2895
38.583	8.063	0.324	0.0662	0.436	0.194	0.298	0.0445	0.162	0.0555	0.0247	0.0191	0.102	0.0604	0.0726	0.0727	0.0727	0.0729	0.2909
38.667	8.091	0.325	0.0668	0.439	0.195	0.3	0.0447	0.163	0.0558	0.0249	0.0191	0.103	0.0604	0.073	0.0731	0.0731	0.0733	0.2925
38.75	8.118	0.327	0.0674	0.441	0.196	0.301	0.045	0.164	0.0561	0.0251	0.0192	0.103	0.0605	0.0733	0.0734	0.0735	0.0737	0.2939
38.833	8.146	0.329	0.0679	0.443	0.197	0.303	0.0452	0.165	0.0565	0.0252	0.0193	0.104	0.0605	0.0737	0.0738	0.0738	0.074	0.2953
38.917	8.174	0.331	0.0684	0.445	0.198	0.304	0.0455	0.166	0.0568	0.0253	0.0193	0.104	0.0605	0.0741	0.0742	0.0742	0.0744	0.2969
39	8.202	0.332	0.069	0.447	0.199	0.305	0.0457	0.167	0.0571	0.0254	0.0194	0.105	0.0605	0.0745	0.0746	0.0746	0.0748	0.2985
39.083	8.23	0.334	0.0694	0.45	0.2	0.307	0.0459	0.168	0.0575	0.0255	0.0194	0.105	0.0605	0.0748	0.0749	0.075	0.0752	0.2999
39.167	8.258	0.336	0.0699	0.452	0.201	0.308	0.0462	0.169	0.0578	0.0257	0.0194	0.105	0.0605	0.0752	0.0753	0.0754	0.0756	0.3015
39.25	8.286	0.338	0.0704	0.454	0.202	0.31	0.0464	0.171	0.0581	0.0258	0.0194	0.106	0.0605	0.0756	0.0757	0.0757	0.0759	0.3029
39.333	8.314	0.339	0.0708	0.457	0.203	0.311	0.0466	0.172	0.0585	0.0259	0.0195	0.106	0.0607	0.076	0.0761	0.0761	0.0763	0.3045
39.417	8.343	0.341	0.0713	0.459	0.204	0.313	0.0469	0.173	0.0588	0.026	0.0195	0.107	0.0608	0.0764	0.0765	0.0765	0.0767	0.3061
39.5	8.371	0.343	0.0717	0.461	0.206	0.314	0.0471	0.174	0.0592	0.0261	0.0195	0.107	0.0609	0.0768	0.0769	0.0769	0.0771	0.3077
39.583	8.4	0.345	0.0722	0.464	0.207	0.316	0.0474	0.175	0.0596	0.0262	0.0196	0.107	0.0612	0.0772	0.0773	0.0773	0.0775	0.3093
39.667	8.429	0.347	0.0726	0.466	0.208	0.317	0.0477	0.177	0.06	0.0263	0.0197	0.108	0.0616	0.0776	0.0777	0.0777	0.078	0.311
39.75	8.457	0.349	0.0731	0.469	0.209	0.319	0.0479	0.178	0.0604	0.0265	0.0197	0.108	0.062	0.078	0.0781	0.0782	0.0784	0.3127
39.833	8.486	0.351	0.0735	0.471	0.21	0.32	0.0482	0.179	0.0608	0.0266	0.0199	0.109	0.0627	0.0785	0.0785	0.0786	0.0788	0.3144

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
39.917	8.516	0.353	0.074	0.474	0.212	0.322	0.0485	0.18	0.0612	0.0268	0.02	0.11	0.0633	0.0789	0.079	0.079	0.0792	0.3161
40	8.545	0.355	0.0744	0.476	0.213	0.324	0.0487	0.182	0.0616	0.0269	0.0202	0.11	0.064	0.0793	0.0794	0.0795	0.0797	0.3179
40.083	8.574	0.357	0.0748	0.479	0.214	0.325	0.049	0.183	0.062	0.0271	0.0204	0.111	0.0648	0.0798	0.0799	0.0799	0.0801	0.3197
40.167	8.603	0.359	0.0753	0.482	0.216	0.327	0.0493	0.184	0.0624	0.0273	0.0206	0.112	0.0655	0.0802	0.0803	0.0804	0.0806	0.3215
40.25	8.633	0.361	0.0757	0.484	0.217	0.329	0.0496	0.185	0.0628	0.0275	0.0208	0.112	0.0662	0.0807	0.0808	0.0808	0.081	0.3233
40.333	8.663	0.364	0.0762	0.487	0.219	0.331	0.0499	0.187	0.0633	0.0277	0.021	0.113	0.0668	0.0811	0.0812	0.0813	0.0815	0.3251
40.417	8.692	0.366	0.0766	0.49	0.22	0.332	0.0502	0.188	0.0637	0.0279	0.0212	0.114	0.0674	0.0816	0.0817	0.0817	0.082	0.327
40.5	8.722	0.368	0.0771	0.493	0.221	0.334	0.0505	0.189	0.0641	0.0281	0.0214	0.115	0.068	0.0821	0.0822	0.0822	0.0824	0.3289
40.583	8.752	0.371	0.0775	0.496	0.223	0.336	0.0508	0.19	0.0646	0.0283	0.0215	0.116	0.0685	0.0826	0.0827	0.0827	0.0829	0.3309
40.667	8.782	0.373	0.078	0.499	0.224	0.338	0.0511	0.192	0.065	0.0285	0.0217	0.117	0.0689	0.083	0.0831	0.0832	0.0834	0.3327
40.75	8.812	0.375	0.0785	0.502	0.226	0.339	0.0515	0.193	0.0654	0.0287	0.0218	0.118	0.0693	0.0835	0.0836	0.0837	0.0839	0.3347
40.833	8.843	0.378	0.079	0.505	0.227	0.341	0.0518	0.194	0.0658	0.0289	0.022	0.118	0.0696	0.084	0.0841	0.0842	0.0844	0.3367
40.917	8.873	0.38	0.0795	0.508	0.229	0.343	0.0521	0.195	0.0663	0.0291	0.0221	0.119	0.0699	0.0845	0.0846	0.0847	0.0849	0.3387
41	8.904	0.383	0.08	0.511	0.23	0.345	0.0525	0.196	0.0667	0.0292	0.0222	0.12	0.0702	0.085	0.0852	0.0852	0.0854	0.3408
41.083	8.934	0.385	0.0805	0.514	0.232	0.347	0.0528	0.198	0.0671	0.0294	0.0223	0.12	0.0705	0.0856	0.0857	0.0857	0.086	0.343
41.167	8.965	0.388	0.081	0.517	0.233	0.349	0.0531	0.199	0.0675	0.0295	0.0224	0.121	0.0707	0.0861	0.0862	0.0863	0.0865	0.3451
41.25	8.996	0.39	0.0816	0.52	0.235	0.351	0.0535	0.2	0.0679	0.0297	0.0225	0.122	0.0709	0.0866	0.0867	0.0868	0.087	0.3471
41.333	9.027	0.393	0.0821	0.524	0.236	0.353	0.0538	0.201	0.0684	0.0298	0.0225	0.122	0.071	0.0872	0.0873	0.0873	0.0876	0.3494
41.417	9.058	0.395	0.0826	0.527	0.238	0.354	0.0542	0.202	0.0688	0.03	0.0226	0.123	0.0712	0.0877	0.0878	0.0879	0.0881	0.3515
41.5	9.089	0.398	0.0832	0.53	0.239	0.356	0.0545	0.204	0.0692	0.0301	0.0227	0.123	0.0713	0.0883	0.0884	0.0884	0.0887	0.3538
41.583	9.12	0.4	0.0837	0.533	0.241	0.358	0.0549	0.205	0.0696	0.0302	0.0227	0.123	0.0714	0.0888	0.0889	0.089	0.0892	0.3559
41.667	9.152	0.402	0.0842	0.537	0.242	0.36	0.0552	0.206	0.07	0.0303	0.0228	0.124	0.0715	0.0894	0.0895	0.0895	0.0898	0.3582
41.75	9.183	0.405	0.0847	0.54	0.244	0.362	0.0555	0.207	0.0704	0.0304	0.0228	0.124	0.0715	0.0899	0.09	0.0901	0.0903	0.3603
41.833	9.215	0.407	0.0852	0.543	0.245	0.364	0.0559	0.208	0.0708	0.0305	0.0228	0.125	0.0715	0.0905	0.0906	0.0906	0.0909	0.3626
41.917	9.247	0.41	0.0856	0.547	0.246	0.366	0.0562	0.21	0.0712	0.0306	0.0229	0.125	0.0715	0.091	0.0911	0.0912	0.0914	0.3647
42	9.279	0.412	0.0861	0.55	0.248	0.368	0.0565	0.211	0.0716	0.0307	0.0229	0.125	0.0715	0.0916	0.0917	0.0917	0.092	0.367
42.083	9.311	0.415	0.0865	0.553	0.249	0.37	0.0569	0.212	0.072	0.0307	0.0229	0.125	0.0715	0.0921	0.0922	0.0923	0.0925	0.3691
42.167	9.343	0.417	0.0869	0.556	0.251	0.373	0.0572	0.213	0.0725	0.0308	0.0229	0.126	0.0715	0.0926	0.0928	0.0928	0.0931	0.3713
42.25	9.375	0.419	0.0873	0.56	0.252	0.375	0.0575	0.214	0.0729	0.0309	0.023	0.126	0.0715	0.0932	0.0933	0.0933	0.0936	0.3734
42.333	9.408	0.422	0.0877	0.563	0.254	0.377	0.0578	0.216	0.0733	0.0309	0.023	0.126	0.0716	0.0937	0.0938	0.0939	0.0941	0.3755
42.417	9.44	0.424	0.088	0.566	0.255	0.379	0.0582	0.217	0.0737	0.031	0.023	0.126	0.0716	0.0942	0.0944	0.0944	0.0947	0.3777
42.5	9.473	0.426	0.0884	0.569	0.256	0.381	0.0585	0.218	0.0741	0.0311	0.023	0.127	0.0717	0.0948	0.0949	0.095	0.0952	0.3799
42.583	9.506	0.429	0.0887	0.572	0.258	0.383	0.0588	0.219	0.0745	0.0312	0.023	0.127	0.0719	0.0953	0.0954	0.0955	0.0957	0.3819
42.667	9.539	0.431	0.0891	0.576	0.259	0.385	0.0591	0.22	0.0749	0.0312	0.0231	0.127	0.072	0.0959	0.096	0.096	0.0963	0.3842
42.75	9.572	0.434	0.0894	0.579	0.261	0.387	0.0595	0.222	0.0753	0.0313	0.0231	0.127	0.0722	0.0964	0.0965	0.0966	0.0968	0.3863
42.833	9.605	0.436	0.0897	0.582	0.262	0.39	0.0598	0.223	0.0758	0.0314	0.0232	0.128	0.0725	0.0969	0.0971	0.0971	0.0974	0.3885
42.917	9.638	0.438	0.0901	0.585	0.264	0.392	0.0601	0.224	0.0762	0.0315	0.0233	0.128	0.0728	0.0975	0.0976	0.0976	0.0979	0.3906
43	9.671	0.441	0.0904	0.589	0.265	0.394	0.0604	0.225	0.0766	0.0316	0.0233	0.128	0.0732	0.098	0.0981	0.0982	0.0984	0.3927
43.083	9.705	0.443	0.0907	0.592	0.266	0.396	0.0608	0.226	0.077	0.0317	0.0234	0.129	0.0735	0.0985	0.0987	0.0987	0.099	0.3949
43.167	9.739	0.446	0.091	0.595	0.268	0.399	0.0611	0.227	0.0774	0.0318	0.0235	0.129	0.0739	0.0991	0.0992	0.0993	0.0995	0.3971
43.25	9.772	0.448	0.0913	0.598	0.269	0.401	0.0614	0.228	0.0779	0.0319	0.0236	0.13	0.0743	0.0996	0.0997	0.0998	0.1	0.3991
43.333	9.806	0.45	0.0915	0.601	0.271	0.403	0.0618	0.229	0.0783	0.032	0.0237	0.13	0.0746	0.1	0.1	0.1	0.101	0.401
43.417	9.84	0.453	0.0918	0.605	0.272	0.406	0.0621	0.23	0.0787	0.0321	0.0238	0.13	0.0749	0.101	0.101	0.101	0.101	0.404
43.5	9.874	0.455	0.0921	0.608	0.274	0.408	0.0624	0.231	0.0791	0.0322	0.0239	0.131	0.0752	0.101	0.101	0.101	0.102	0.405
43.583	9.909	0.458	0.0924	0.611	0.275	0.41	0.0628	0.233	0.0795	0.0323	0.024	0.131	0.0754	0.102	0.102	0.102	0.102	0.408
43.667	9.943	0.46	0.0926	0.614	0.277	0.413	0.0631	0.234	0.0799	0.0324	0.0241	0.132	0.0757	0.102	0.102	0.102	0.103	0.409
43.75	9.977	0.462	0.0929	0.618	0.278	0.415	0.0634	0.235	0.0803	0.0325	0.0242	0.132	0.0759	0.103	0.103	0.103	0.103	0.412
43.833	10.012	0.465	0.0932	0.621	0.279	0.417	0.0638	0.236	0.0807	0.0326	0.0242	0.133	0.076	0.103	0.104	0.104	0.104	0.415
43.917	10.047	0.467	0.0935	0.624	0.281	0.42	0.0641	0.237	0.081	0.0327	0.0243	0.133	0.0762	0.104	0.104	0.104	0.104	0.416
44	10.082	0.47	0.0938	0.627	0.282	0.422	0.0644	0.238	0.0814	0.0328	0.0243	0.133	0.0764	0.104	0.105	0.105	0.105	0.419
44.083	10.117	0.472	0.094	0.631	0.284	0.424	0.0648	0.239	0.0818	0.0328	0.0244	0.134	0.0765	0.105	0.105	0.105	0.105	0.42
44.167	10.152	0.475	0.0943	0.634	0.285	0.426	0.0651	0.24	0.0822	0.0329	0.0244	0.134	0.0766	0.106	0.106	0.106	0.106	0.424
44.25	10.187	0.477	0.0946	0.637	0.287	0.429	0.0654	0.241	0.0825	0.033	0.0245	0.134	0.0767	0.106	0.106	0.106	0.107	0.425
44.333	10.223	0.479	0.0949	0.64	0.288	0.431	0.0658	0.241	0.0829	0.0331	0.0245	0.134	0.0768	0.107	0.107	0.107	0.107	0.428
44.417	10.258	0.482	0.0952	0.644	0.289	0.433	0.0661	0.242	0.0832	0.0331	0.0245	0.135	0.0769	0.107	0.107	0.107	0.108	0.429
44.5	10.294	0.484	0.0955	0.647	0.291	0.435	0.0664	0.243	0.0836	0.0332	0.0246	0.135	0.0769	0.108	0.108	0.108	0.108	0.432
44.583	10.33	0.486	0.0958	0.65	0.292	0.438	0.0667	0.244	0.0839	0.0332	0.0246	0.135	0.077	0.108	0.108	0.108	0.109	0.433
44.667	10.366	0.489	0.0961	0.653	0.293	0.44	0.067	0.245	0.0843	0.0333	0.0246	0.135	0.077	0.109	0.109	0.109	0.109	0.436
44.75	10.402	0.491	0.0964	0.657	0.294	0.442	0.0674	0.246	0.0846	0.0334	0.0247	0.136	0.077	0.109	0.109	0.11	0.11	0.438
44.833	10.438	0.493	0.0966	0.66	0.296	0.444	0.0677	0.247	0.085	0.0334	0.0247	0.136	0.077	0.11	0.11	0.11	0.11	0.44
44.917	10.475	0.495	0.0969	0.663	0.297	0.447	0.068	0.248	0.0853	0.0334	0.0247	0.136	0.077	0.11	0.11	0.111	0.111	0.442
45	10.511	0.497	0.0971	0.666	0.298	0.449	0.0683	0.249	0.0856	0.0335	0.0247	0.136	0.0771	0.111	0.111	0.111	0.111	0.444
45.083	10.548	0.5	0.0974	0.669	0.299	0.451	0.0686	0.25	0.086	0.0335	0.0247	0.136	0.0771	0.111	0.112	0.112	0.112	0.447

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
45.167	10.584	0.502	0.0976	0.672	0.301	0.453	0.0689	0.25	0.0863	0.0336	0.0247	0.136	0.0771	0.112	0.112	0.112	0.112	0.448
45.25	10.621	0.504	0.0978	0.675	0.302	0.456	0.0692	0.251	0.0866	0.0336	0.0247	0.136	0.0771	0.112	0.113	0.113	0.113	0.451
45.333	10.658	0.506	0.098	0.678	0.303	0.458	0.0695	0.252	0.087	0.0336	0.0248	0.137	0.0771	0.113	0.113	0.113	0.113	0.452
45.417	10.695	0.508	0.0982	0.681	0.304	0.46	0.0697	0.253	0.0873	0.0337	0.0248	0.137	0.0772	0.113	0.114	0.114	0.114	0.455
45.5	10.733	0.51	0.0984	0.684	0.306	0.462	0.07	0.254	0.0876	0.0337	0.0248	0.137	0.0773	0.114	0.114	0.114	0.114	0.456
45.583	10.77	0.512	0.0986	0.687	0.307	0.465	0.0703	0.255	0.088	0.0338	0.0249	0.137	0.0776	0.114	0.115	0.115	0.115	0.459
45.667	10.808	0.514	0.0989	0.69	0.308	0.467	0.0706	0.256	0.0883	0.0339	0.0249	0.137	0.0779	0.115	0.115	0.115	0.115	0.46
45.75	10.845	0.516	0.0991	0.693	0.309	0.469	0.0709	0.256	0.0886	0.0339	0.025	0.138	0.0782	0.115	0.115	0.116	0.116	0.462
45.833	10.883	0.518	0.0993	0.696	0.31	0.472	0.0712	0.257	0.089	0.034	0.0251	0.138	0.0788	0.116	0.116	0.116	0.116	0.464
45.917	10.921	0.52	0.0996	0.699	0.312	0.474	0.0715	0.258	0.0893	0.0342	0.0253	0.139	0.0794	0.116	0.116	0.117	0.117	0.466
46	10.959	0.522	0.0998	0.702	0.313	0.476	0.0717	0.259	0.0897	0.0343	0.0254	0.139	0.0801	0.117	0.117	0.117	0.117	0.468
46.083	10.998	0.525	0.1	0.705	0.314	0.478	0.072	0.26	0.09	0.0344	0.0256	0.14	0.0808	0.117	0.117	0.118	0.118	0.47
46.167	11.036	0.527	0.1	0.708	0.315	0.481	0.0723	0.261	0.0904	0.0346	0.0258	0.141	0.0816	0.118	0.118	0.118	0.118	0.472
46.25	11.075	0.529	0.101	0.71	0.316	0.483	0.0726	0.261	0.0907	0.0347	0.026	0.141	0.0823	0.118	0.118	0.118	0.119	0.473
46.333	11.114	0.531	0.101	0.713	0.318	0.485	0.0729	0.262	0.091	0.0349	0.0262	0.142	0.0829	0.119	0.119	0.119	0.119	0.476
46.417	11.152	0.533	0.101	0.716	0.319	0.488	0.0732	0.263	0.0914	0.0351	0.0264	0.143	0.0836	0.119	0.119	0.119	0.12	0.477
46.5	11.191	0.535	0.101	0.719	0.32	0.49	0.0735	0.264	0.0917	0.0352	0.0266	0.144	0.0842	0.12	0.12	0.12	0.12	0.48
46.583	11.23	0.537	0.102	0.722	0.321	0.492	0.0738	0.265	0.0921	0.0354	0.0267	0.145	0.0847	0.12	0.12	0.12	0.121	0.481
46.667	11.27	0.539	0.102	0.725	0.323	0.495	0.0741	0.266	0.0924	0.0356	0.0269	0.146	0.0851	0.121	0.121	0.121	0.121	0.484
46.75	11.309	0.541	0.102	0.728	0.324	0.497	0.0744	0.267	0.0927	0.0358	0.0271	0.147	0.0856	0.121	0.121	0.121	0.122	0.485
46.833	11.349	0.544	0.103	0.731	0.325	0.499	0.0747	0.267	0.0931	0.036	0.0272	0.147	0.0859	0.122	0.122	0.122	0.122	0.488
46.917	11.389	0.546	0.103	0.734	0.326	0.502	0.0749	0.268	0.0934	0.0362	0.0273	0.148	0.0863	0.122	0.122	0.122	0.123	0.489
47	11.428	0.548	0.103	0.737	0.328	0.504	0.0752	0.269	0.0937	0.0364	0.0274	0.149	0.0866	0.123	0.123	0.123	0.123	0.492
47.083	11.468	0.55	0.104	0.739	0.329	0.506	0.0755	0.27	0.0941	0.0366	0.0275	0.149	0.0868	0.123	0.123	0.123	0.124	0.493
47.167	11.509	0.552	0.104	0.742	0.33	0.508	0.0758	0.271	0.0944	0.0367	0.0276	0.15	0.0871	0.124	0.124	0.124	0.124	0.496
47.25	11.549	0.554	0.105	0.745	0.331	0.511	0.0761	0.272	0.0947	0.0369	0.0277	0.151	0.0873	0.124	0.124	0.124	0.125	0.497
47.333	11.589	0.556	0.105	0.748	0.333	0.513	0.0764	0.273	0.095	0.037	0.0278	0.151	0.0875	0.125	0.125	0.125	0.125	0.5
47.417	11.63	0.558	0.106	0.751	0.334	0.515	0.0767	0.273	0.0954	0.0371	0.0278	0.152	0.0876	0.125	0.125	0.125	0.126	0.501
47.5	11.671	0.56	0.106	0.754	0.335	0.517	0.077	0.274	0.0957	0.0373	0.0279	0.152	0.0878	0.126	0.126	0.126	0.126	0.504
47.583	11.712	0.563	0.106	0.757	0.336	0.52	0.0773	0.275	0.096	0.0374	0.028	0.153	0.0879	0.126	0.126	0.126	0.127	0.505
47.667	11.753	0.565	0.107	0.76	0.337	0.522	0.0776	0.276	0.0963	0.0375	0.028	0.153	0.0879	0.126	0.127	0.127	0.127	0.507
47.75	11.794	0.567	0.107	0.763	0.339	0.524	0.0779	0.277	0.0967	0.0376	0.0281	0.153	0.088	0.127	0.127	0.127	0.128	0.509
47.833	11.835	0.569	0.108	0.766	0.34	0.526	0.0782	0.278	0.097	0.0377	0.0281	0.154	0.088	0.127	0.128	0.128	0.128	0.511
47.917	11.877	0.571	0.108	0.769	0.341	0.528	0.0785	0.279	0.0973	0.0378	0.0282	0.154	0.088	0.128	0.128	0.128	0.129	0.513
48	11.918	0.573	0.108	0.772	0.342	0.531	0.0787	0.28	0.0976	0.0379	0.0282	0.154	0.0881	0.128	0.129	0.129	0.129	0.515
48.083	11.96	0.575	0.109	0.774	0.343	0.533	0.079	0.28	0.098	0.038	0.0282	0.155	0.0881	0.129	0.129	0.129	0.129	0.516
48.167	12.002	0.577	0.109	0.777	0.345	0.535	0.0793	0.281	0.0983	0.038	0.0282	0.155	0.0881	0.129	0.13	0.13	0.13	0.519
48.25	12.044	0.579	0.109	0.78	0.346	0.537	0.0796	0.282	0.0986	0.0381	0.0283	0.155	0.0881	0.13	0.13	0.13	0.13	0.52
48.333	12.087	0.581	0.11	0.783	0.347	0.539	0.0799	0.283	0.099	0.0382	0.0283	0.156	0.0882	0.13	0.13	0.131	0.131	0.522
48.417	12.129	0.583	0.11	0.786	0.348	0.541	0.0802	0.284	0.0993	0.0383	0.0283	0.156	0.0884	0.131	0.131	0.131	0.131	0.524
48.5	12.171	0.585	0.11	0.789	0.349	0.544	0.0804	0.285	0.0996	0.0384	0.0284	0.156	0.0885	0.131	0.131	0.132	0.132	0.526
48.583	12.214	0.587	0.111	0.792	0.351	0.546	0.0807	0.286	0.1	0.0385	0.0285	0.157	0.0892	0.132	0.132	0.132	0.132	0.528
48.667	12.257	0.589	0.111	0.795	0.352	0.548	0.081	0.287	0.1	0.0387	0.0287	0.157	0.0899	0.132	0.132	0.132	0.133	0.529
48.75	12.3	0.592	0.112	0.798	0.353	0.55	0.0813	0.288	0.101	0.0388	0.0288	0.158	0.0906	0.133	0.133	0.133	0.133	0.532
48.833	12.343	0.594	0.112	0.801	0.354	0.553	0.0816	0.289	0.101	0.0391	0.0291	0.159	0.0921	0.133	0.133	0.134	0.134	0.534
48.917	12.387	0.596	0.112	0.804	0.356	0.555	0.0819	0.291	0.102	0.0393	0.0295	0.16	0.0936	0.134	0.134	0.134	0.134	0.536
49	12.43	0.598	0.113	0.807	0.357	0.557	0.0822	0.292	0.102	0.0396	0.0298	0.162	0.095	0.134	0.134	0.135	0.135	0.538
49.083	12.474	0.601	0.113	0.81	0.359	0.56	0.0826	0.293	0.102	0.0399	0.0303	0.163	0.0969	0.135	0.135	0.135	0.135	0.54
49.167	12.518	0.603	0.114	0.813	0.36	0.562	0.0829	0.294	0.103	0.0403	0.0307	0.165	0.0988	0.135	0.136	0.136	0.136	0.543
49.25	12.562	0.605	0.115	0.816	0.361	0.564	0.0832	0.295	0.103	0.0406	0.0312	0.167	0.101	0.136	0.136	0.136	0.136	0.544
49.333	12.606	0.608	0.115	0.82	0.363	0.567	0.0836	0.297	0.104	0.041	0.0317	0.169	0.102	0.136	0.137	0.137	0.137	0.547
49.417	12.65	0.611	0.116	0.823	0.365	0.569	0.0839	0.298	0.104	0.0415	0.0322	0.171	0.104	0.137	0.137	0.137	0.138	0.549
49.5	12.695	0.613	0.116	0.826	0.366	0.572	0.0843	0.299	0.105	0.0419	0.0327	0.173	0.106	0.138	0.138	0.138	0.138	0.552
49.583	12.739	0.616	0.117	0.83	0.368	0.574	0.0846	0.301	0.105	0.0424	0.0331	0.175	0.107	0.138	0.138	0.138	0.139	0.553
49.667	12.784	0.618	0.118	0.833	0.369	0.576	0.085	0.302	0.105	0.0429	0.0335	0.177	0.108	0.139	0.139	0.139	0.139	0.556
49.75	12.829	0.621	0.119	0.837	0.371	0.579	0.0854	0.303	0.106	0.0434	0.034	0.18	0.109	0.139	0.139	0.14	0.14	0.558
49.833	12.874	0.624	0.12	0.841	0.373	0.581	0.0857	0.305	0.106	0.0439	0.0343	0.182	0.11	0.14	0.14	0.14	0.141	0.561
49.917	12.919	0.627	0.12	0.844	0.374	0.584	0.0861	0.306	0.107	0.0444	0.0346	0.183	0.111	0.141	0.141	0.141	0.141	0.564
50	12.965	0.629	0.121	0.848	0.376	0.586	0.0865	0.308	0.107	0.0448	0.0349	0.185	0.112	0.141	0.141	0.141	0.142	0.565
50.083	13.01	0.632	0.122	0.852	0.378	0.589	0.0869	0.309	0.108	0.0452	0.0352	0.187	0.112	0.142	0.142	0.142	0.142	0.568
50.167	13.056	0.635	0.123	0.855	0.379	0.591	0.0873	0.311	0.108	0.0456	0.0354	0.189	0.113	0.142	0.143	0.143	0.143	0.571
50.25	13.102	0.638	0.124	0.859	0.381	0.594	0.0877	0.313	0.109	0.0461	0.0356	0.19	0.114	0.143	0.143	0.143	0.144	0.573
50.333	13.148	0.641	0.125	0.863	0.383	0.597	0.0881	0.314	0.109	0.0464	0.0358	0.192	0.114	0.144	0.144	0.144	0.144	0.576

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
50.417	13.195	0.644	0.126	0.867	0.385	0.599	0.0885	0.316	0.11	0.0467	0.036	0.193	0.114	0.144	0.145	0.145	0.145	0.579
50.5	13.241	0.647	0.127	0.871	0.386	0.602	0.0889	0.317	0.11	0.0471	0.0362	0.194	0.115	0.145	0.145	0.145	0.146	0.581
50.583	13.288	0.65	0.128	0.875	0.388	0.604	0.0894	0.319	0.111	0.0474	0.0363	0.195	0.115	0.146	0.146	0.146	0.146	0.584
50.667	13.334	0.653	0.129	0.879	0.39	0.607	0.0898	0.321	0.111	0.0476	0.0365	0.196	0.115	0.146	0.147	0.147	0.147	0.587
50.75	13.381	0.656	0.13	0.883	0.392	0.609	0.0902	0.323	0.112	0.0479	0.0366	0.197	0.115	0.147	0.147	0.147	0.148	0.589
50.833	13.428	0.659	0.131	0.887	0.394	0.612	0.0906	0.324	0.112	0.0482	0.0367	0.198	0.115	0.148	0.148	0.148	0.148	0.592
50.917	13.476	0.662	0.132	0.891	0.396	0.615	0.091	0.326	0.113	0.0484	0.0368	0.199	0.116	0.148	0.149	0.149	0.149	0.595
51	13.523	0.665	0.133	0.896	0.397	0.617	0.0915	0.328	0.114	0.0486	0.0369	0.2	0.116	0.149	0.149	0.149	0.15	0.597
51.083	13.571	0.668	0.134	0.9	0.399	0.62	0.0919	0.33	0.114	0.0488	0.037	0.2	0.116	0.15	0.15	0.15	0.15	0.6
51.167	13.619	0.672	0.135	0.904	0.401	0.623	0.0923	0.332	0.115	0.049	0.037	0.201	0.116	0.15	0.151	0.151	0.151	0.603
51.25	13.666	0.675	0.136	0.908	0.403	0.625	0.0928	0.334	0.115	0.0492	0.0371	0.202	0.116	0.151	0.151	0.151	0.152	0.605
51.333	13.715	0.678	0.136	0.912	0.405	0.628	0.0932	0.336	0.116	0.0493	0.0371	0.202	0.116	0.152	0.152	0.152	0.153	0.609
51.417	13.763	0.681	0.137	0.916	0.407	0.631	0.0936	0.338	0.116	0.0495	0.0371	0.203	0.116	0.153	0.153	0.153	0.153	0.612
51.5	13.811	0.684	0.138	0.921	0.409	0.633	0.094	0.34	0.117	0.0497	0.0371	0.203	0.116	0.153	0.153	0.154	0.154	0.614
51.583	13.86	0.687	0.139	0.925	0.411	0.636	0.0945	0.342	0.118	0.0498	0.0371	0.204	0.116	0.154	0.154	0.154	0.155	0.617
51.667	13.909	0.691	0.139	0.929	0.413	0.639	0.0949	0.344	0.118	0.0499	0.0371	0.204	0.116	0.155	0.155	0.155	0.155	0.62
51.75	13.958	0.694	0.14	0.933	0.415	0.642	0.0954	0.346	0.119	0.0501	0.0371	0.205	0.116	0.155	0.156	0.156	0.156	0.623
51.833	14.007	0.697	0.141	0.938	0.417	0.644	0.0958	0.348	0.119	0.0502	0.0371	0.205	0.116	0.156	0.156	0.156	0.157	0.625
51.917	14.056	0.7	0.141	0.942	0.419	0.647	0.0963	0.35	0.12	0.0503	0.0371	0.205	0.116	0.157	0.157	0.157	0.158	0.629
52	14.106	0.704	0.142	0.946	0.421	0.65	0.0967	0.352	0.121	0.0504	0.0371	0.205	0.116	0.158	0.158	0.158	0.158	0.632
52.083	14.156	0.707	0.142	0.951	0.423	0.653	0.0972	0.353	0.121	0.0505	0.0371	0.205	0.116	0.158	0.159	0.159	0.159	0.635
52.167	14.206	0.71	0.143	0.955	0.425	0.656	0.0976	0.355	0.122	0.0506	0.0371	0.206	0.116	0.159	0.159	0.159	0.16	0.637
52.25	14.255	0.714	0.143	0.96	0.427	0.659	0.0981	0.357	0.123	0.0506	0.0371	0.206	0.116	0.16	0.16	0.16	0.16	0.64
52.333	14.306	0.717	0.144	0.964	0.429	0.661	0.0985	0.359	0.123	0.0507	0.0371	0.206	0.116	0.161	0.161	0.161	0.161	0.644
52.417	14.356	0.721	0.144	0.969	0.431	0.664	0.099	0.361	0.124	0.0507	0.0371	0.206	0.116	0.161	0.161	0.162	0.162	0.646
52.5	14.407	0.724	0.145	0.973	0.433	0.667	0.0995	0.362	0.124	0.0508	0.0371	0.206	0.116	0.162	0.162	0.162	0.163	0.649
52.583	14.458	0.727	0.145	0.978	0.435	0.67	0.0999	0.364	0.125	0.0508	0.0371	0.206	0.116	0.163	0.163	0.163	0.163	0.652
52.667	14.509	0.731	0.145	0.982	0.438	0.673	0.1	0.366	0.126	0.0508	0.0371	0.206	0.116	0.164	0.164	0.164	0.164	0.656
52.75	14.559	0.734	0.146	0.987	0.44	0.676	0.101	0.367	0.126	0.0509	0.0371	0.206	0.116	0.164	0.164	0.165	0.165	0.658
52.833	14.611	0.738	0.146	0.991	0.442	0.679	0.101	0.369	0.127	0.0509	0.0371	0.206	0.116	0.165	0.165	0.165	0.166	0.661
52.917	14.663	0.741	0.146	0.996	0.444	0.682	0.102	0.37	0.127	0.0509	0.0371	0.206	0.116	0.166	0.166	0.166	0.167	0.665
53	14.714	0.745	0.147	1	0.446	0.685	0.102	0.372	0.128	0.0509	0.0371	0.206	0.116	0.167	0.167	0.167	0.167	0.668
53.083	14.766	0.749	0.147	1.005	0.448	0.687	0.103	0.373	0.129	0.0509	0.0371	0.206	0.116	0.167	0.168	0.168	0.168	0.671
53.167	14.818	0.752	0.147	1.01	0.45	0.69	0.103	0.375	0.129	0.0509	0.0371	0.206	0.116	0.168	0.168	0.168	0.169	0.673
53.25	14.87	0.756	0.148	1.014	0.452	0.693	0.104	0.376	0.13	0.0509	0.0371	0.206	0.116	0.169	0.169	0.169	0.17	0.677
53.333	14.923	0.759	0.148	1.019	0.454	0.696	0.104	0.377	0.13	0.0509	0.0371	0.206	0.116	0.17	0.17	0.17	0.17	0.68
53.417	14.975	0.762	0.148	1.024	0.456	0.699	0.105	0.379	0.131	0.0509	0.0371	0.206	0.116	0.17	0.171	0.171	0.171	0.683
53.5	15.028	0.766	0.149	1.029	0.458	0.702	0.105	0.38	0.131	0.0509	0.0371	0.206	0.116	0.171	0.171	0.172	0.172	0.686
53.583	15.081	0.769	0.149	1.033	0.46	0.705	0.106	0.381	0.132	0.0509	0.0371	0.206	0.116	0.172	0.172	0.172	0.173	0.689
53.667	15.134	0.772	0.149	1.038	0.462	0.707	0.106	0.382	0.132	0.0509	0.0371	0.206	0.116	0.173	0.173	0.173	0.174	0.693
53.75	15.187	0.776	0.149	1.043	0.464	0.71	0.107	0.384	0.133	0.0509	0.0371	0.206	0.116	0.174	0.174	0.174	0.174	0.696
53.833	15.241	0.779	0.15	1.047	0.466	0.713	0.107	0.385	0.133	0.0509	0.0371	0.206	0.116	0.174	0.175	0.175	0.175	0.699
53.917	15.295	0.782	0.15	1.052	0.468	0.716	0.107	0.386	0.134	0.0509	0.0371	0.206	0.116	0.175	0.175	0.175	0.176	0.701
54	15.349	0.785	0.15	1.056	0.469	0.719	0.108	0.387	0.134	0.0509	0.0371	0.206	0.116	0.176	0.176	0.176	0.177	0.705
54.083	15.403	0.788	0.15	1.06	0.471	0.722	0.108	0.388	0.135	0.0509	0.0371	0.206	0.116	0.177	0.177	0.177	0.177	0.708
54.167	15.457	0.791	0.15	1.065	0.473	0.725	0.109	0.389	0.135	0.0509	0.0371	0.206	0.116	0.177	0.177	0.178	0.178	0.71
54.25	15.512	0.794	0.151	1.069	0.474	0.728	0.109	0.39	0.136	0.0509	0.0371	0.206	0.116	0.178	0.178	0.178	0.179	0.713
54.333	15.566	0.797	0.151	1.073	0.476	0.73	0.11	0.391	0.136	0.0509	0.0371	0.206	0.116	0.179	0.179	0.179	0.179	0.716
54.417	15.621	0.8	0.151	1.077	0.478	0.733	0.11	0.392	0.136	0.0509	0.0371	0.206	0.116	0.179	0.18	0.18	0.18	0.719
54.5	15.676	0.803	0.151	1.082	0.479	0.736	0.11	0.393	0.137	0.0509	0.0371	0.206	0.116	0.18	0.18	0.18	0.181	0.721
54.583	15.732	0.806	0.151	1.086	0.481	0.739	0.111	0.394	0.137	0.0509	0.0372	0.206	0.116	0.181	0.181	0.181	0.182	0.725
54.667	15.787	0.808	0.151	1.09	0.482	0.742	0.111	0.395	0.138	0.051	0.0372	0.206	0.116	0.181	0.182	0.182	0.182	0.727
54.75	15.842	0.811	0.152	1.094	0.484	0.745	0.111	0.396	0.138	0.051	0.0373	0.206	0.116	0.182	0.182	0.182	0.183	0.729
54.833	15.898	0.814	0.152	1.097	0.486	0.748	0.112	0.396	0.138	0.0511	0.0374	0.207	0.117	0.183	0.183	0.183	0.184	0.733
54.917	15.954	0.817	0.152	1.101	0.487	0.751	0.112	0.397	0.139	0.0511	0.0375	0.207	0.117	0.183	0.184	0.184	0.184	0.735
55	16.01	0.819	0.152	1.105	0.489	0.754	0.113	0.398	0.139	0.0512	0.0376	0.207	0.118	0.184	0.184	0.184	0.185	0.737
55.083	16.067	0.822	0.152	1.109	0.49	0.757	0.113	0.399	0.14	0.0513	0.0378	0.208	0.119	0.185	0.185	0.185	0.185	0.74
55.167	16.124	0.825	0.153	1.113	0.492	0.76	0.113	0.4	0.14	0.0514	0.038	0.209	0.119	0.185	0.185	0.186	0.186	0.742
55.25	16.18	0.827	0.153	1.117	0.493	0.763	0.114	0.401	0.14	0.0516	0.0381	0.209	0.12	0.186	0.186	0.186	0.187	0.745
55.333	16.237	0.83	0.153	1.121	0.495	0.766	0.114	0.402	0.141	0.0517	0.0384	0.21	0.121	0.187	0.187	0.187	0.187	0.748
55.417	16.295	0.832	0.153	1.124	0.496	0.769	0.114	0.403	0.141	0.0519	0.0386	0.211	0.122	0.187	0.187	0.187	0.188	0.749
55.5	16.352	0.835	0.153	1.128	0.497	0.772	0.115	0.404	0.142	0.052	0.0388	0.212	0.122	0.188	0.188	0.188	0.189	0.753
55.583	16.41	0.837	0.154	1.132	0.499	0.775	0.115	0.404	0.142	0.0522	0.0389	0.213	0.123	0.188	0.189	0.189	0.189	0.755

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
55.667	16.467	0.84	0.154	1.135	0.5	0.779	0.116	0.405	0.142	0.0524	0.0391	0.213	0.123	0.189	0.189	0.189	0.19	0.757
55.75	16.525	0.842	0.154	1.139	0.502	0.782	0.116	0.406	0.143	0.0526	0.0393	0.214	0.124	0.19	0.19	0.19	0.19	0.76
55.833	16.584	0.845	0.154	1.142	0.503	0.785	0.116	0.407	0.143	0.0528	0.0394	0.215	0.124	0.19	0.19	0.19	0.191	0.761
55.917	16.642	0.847	0.155	1.146	0.505	0.788	0.117	0.408	0.143	0.053	0.0396	0.216	0.124	0.191	0.191	0.191	0.192	0.765
56	16.7	0.85	0.155	1.15	0.506	0.791	0.117	0.409	0.144	0.0532	0.0397	0.217	0.125	0.191	0.192	0.192	0.192	0.767
56.083	16.759	0.852	0.155	1.153	0.507	0.793	0.117	0.41	0.144	0.0534	0.0398	0.217	0.125	0.192	0.192	0.192	0.193	0.769
56.167	16.818	0.855	0.156	1.157	0.509	0.796	0.118	0.411	0.144	0.0535	0.0399	0.218	0.125	0.192	0.193	0.193	0.193	0.771
56.25	16.877	0.857	0.156	1.16	0.51	0.799	0.118	0.412	0.145	0.0537	0.04	0.219	0.126	0.193	0.193	0.193	0.194	0.773
56.333	16.937	0.859	0.156	1.163	0.511	0.802	0.118	0.413	0.145	0.0538	0.0401	0.219	0.126	0.194	0.194	0.194	0.194	0.776
56.417	16.996	0.862	0.157	1.167	0.513	0.805	0.119	0.413	0.145	0.054	0.0402	0.22	0.126	0.194	0.194	0.195	0.195	0.778
56.5	17.056	0.864	0.157	1.17	0.514	0.808	0.119	0.414	0.146	0.0541	0.0402	0.22	0.126	0.195	0.195	0.195	0.196	0.781
56.583	17.116	0.866	0.157	1.174	0.515	0.811	0.119	0.415	0.146	0.0542	0.0403	0.221	0.126	0.195	0.196	0.196	0.196	0.783
56.667	17.176	0.869	0.158	1.177	0.517	0.813	0.12	0.416	0.146	0.0544	0.0404	0.221	0.126	0.196	0.196	0.196	0.197	0.785
56.75	17.237	0.871	0.158	1.18	0.518	0.816	0.12	0.417	0.147	0.0545	0.0404	0.222	0.127	0.196	0.197	0.197	0.197	0.787
56.833	17.297	0.873	0.158	1.184	0.519	0.819	0.12	0.418	0.147	0.0546	0.0405	0.222	0.127	0.197	0.197	0.197	0.198	0.789
56.917	17.358	0.876	0.159	1.187	0.521	0.822	0.121	0.419	0.147	0.0547	0.0405	0.222	0.127	0.198	0.198	0.198	0.198	0.792
57	17.419	0.878	0.159	1.19	0.522	0.824	0.121	0.42	0.148	0.0548	0.0405	0.223	0.127	0.198	0.198	0.198	0.199	0.793
57.083	17.48	0.88	0.159	1.193	0.523	0.827	0.121	0.421	0.148	0.0548	0.0406	0.223	0.127	0.199	0.199	0.199	0.199	0.796
57.167	17.542	0.882	0.16	1.197	0.524	0.83	0.121	0.422	0.149	0.0549	0.0406	0.223	0.127	0.199	0.199	0.199	0.2	0.797
57.25	17.603	0.885	0.16	1.2	0.526	0.832	0.122	0.423	0.149	0.055	0.0406	0.224	0.127	0.2	0.2	0.2	0.201	0.801
57.333	17.665	0.887	0.16	1.203	0.527	0.835	0.122	0.424	0.149	0.0551	0.0406	0.224	0.127	0.2	0.2	0.201	0.201	0.802
57.417	17.727	0.889	0.161	1.206	0.528	0.837	0.122	0.425	0.15	0.0551	0.0406	0.224	0.127	0.201	0.201	0.201	0.202	0.805
57.5	17.789	0.891	0.161	1.209	0.529	0.84	0.123	0.426	0.15	0.0552	0.0406	0.224	0.127	0.201	0.201	0.202	0.202	0.806
57.583	17.852	0.893	0.161	1.212	0.531	0.843	0.123	0.427	0.15	0.0553	0.0407	0.225	0.127	0.202	0.202	0.202	0.203	0.809
57.667	17.915	0.895	0.162	1.215	0.532	0.845	0.123	0.428	0.151	0.0554	0.0407	0.225	0.127	0.202	0.202	0.203	0.203	0.81
57.75	17.977	0.897	0.162	1.219	0.533	0.848	0.124	0.429	0.151	0.0555	0.0408	0.225	0.127	0.203	0.203	0.203	0.204	0.813
57.833	18.041	0.9	0.162	1.222	0.534	0.85	0.124	0.43	0.151	0.0556	0.0409	0.226	0.128	0.203	0.204	0.204	0.204	0.815
57.917	18.104	0.902	0.162	1.225	0.536	0.853	0.124	0.431	0.152	0.0557	0.041	0.226	0.128	0.204	0.204	0.204	0.205	0.817
58	18.167	0.904	0.163	1.228	0.537	0.856	0.124	0.432	0.152	0.0558	0.0411	0.227	0.129	0.204	0.205	0.205	0.205	0.819
58.083	18.231	0.906	0.163	1.231	0.538	0.858	0.125	0.433	0.153	0.056	0.0413	0.227	0.129	0.205	0.205	0.205	0.206	0.821
58.167	18.295	0.908	0.163	1.234	0.54	0.861	0.125	0.434	0.153	0.0561	0.0414	0.228	0.13	0.205	0.206	0.206	0.206	0.823
58.25	18.359	0.911	0.164	1.237	0.541	0.863	0.125	0.435	0.153	0.0562	0.0416	0.228	0.131	0.206	0.206	0.206	0.207	0.825
58.333	18.423	0.913	0.164	1.24	0.542	0.866	0.126	0.436	0.154	0.0564	0.0418	0.229	0.132	0.206	0.207	0.207	0.207	0.827
58.417	18.488	0.915	0.164	1.244	0.544	0.868	0.126	0.436	0.154	0.0566	0.042	0.23	0.132	0.207	0.207	0.207	0.208	0.829
58.5	18.553	0.918	0.165	1.247	0.545	0.871	0.126	0.437	0.154	0.0568	0.0422	0.231	0.133	0.207	0.208	0.208	0.208	0.831
58.583	18.618	0.92	0.165	1.25	0.547	0.873	0.127	0.438	0.155	0.057	0.0424	0.232	0.134	0.208	0.208	0.208	0.209	0.833
58.667	18.683	0.922	0.166	1.253	0.548	0.876	0.127	0.439	0.155	0.0572	0.0426	0.233	0.134	0.209	0.209	0.209	0.209	0.836
58.75	18.748	0.925	0.166	1.256	0.549	0.878	0.127	0.44	0.156	0.0574	0.0428	0.234	0.135	0.209	0.209	0.209	0.21	0.837
58.833	18.814	0.927	0.166	1.259	0.551	0.881	0.128	0.441	0.156	0.0576	0.0429	0.235	0.135	0.21	0.21	0.21	0.211	0.841
58.917	18.88	0.929	0.167	1.263	0.552	0.883	0.128	0.442	0.156	0.0578	0.0431	0.235	0.135	0.21	0.21	0.21	0.211	0.841
59	18.946	0.932	0.167	1.266	0.554	0.886	0.128	0.443	0.157	0.058	0.0432	0.236	0.136	0.211	0.211	0.211	0.212	0.845
59.083	19.012	0.934	0.168	1.269	0.555	0.888	0.129	0.444	0.157	0.0582	0.0433	0.237	0.136	0.211	0.211	0.212	0.212	0.846
59.167	19.079	0.937	0.168	1.272	0.556	0.891	0.129	0.445	0.158	0.0583	0.0434	0.238	0.136	0.212	0.212	0.212	0.213	0.849
59.25	19.145	0.939	0.168	1.276	0.558	0.893	0.129	0.446	0.158	0.0585	0.0435	0.238	0.137	0.212	0.213	0.213	0.213	0.851
59.333	19.212	0.942	0.169	1.279	0.559	0.896	0.13	0.447	0.158	0.0587	0.0436	0.239	0.137	0.213	0.213	0.213	0.214	0.853
59.417	19.279	0.944	0.169	1.282	0.561	0.898	0.13	0.448	0.159	0.0588	0.0437	0.239	0.137	0.213	0.214	0.214	0.214	0.855
59.5	19.346	0.946	0.17	1.286	0.562	0.901	0.13	0.449	0.159	0.0589	0.0437	0.24	0.137	0.214	0.214	0.214	0.215	0.857
59.583	19.414	0.949	0.17	1.289	0.563	0.903	0.131	0.45	0.159	0.0591	0.0438	0.24	0.137	0.214	0.215	0.215	0.215	0.859
59.667	19.482	0.951	0.171	1.292	0.565	0.905	0.131	0.45	0.16	0.0592	0.0439	0.241	0.137	0.215	0.215	0.215	0.216	0.861
59.75	19.549	0.954	0.171	1.296	0.566	0.908	0.131	0.451	0.16	0.0593	0.0439	0.241	0.137	0.216	0.216	0.216	0.217	0.865
59.833	19.618	0.956	0.172	1.299	0.568	0.91	0.132	0.452	0.16	0.0594	0.044	0.241	0.138	0.216	0.216	0.217	0.217	0.866
59.917	19.686	0.958	0.172	1.302	0.569	0.913	0.132	0.453	0.161	0.0595	0.044	0.242	0.138	0.217	0.217	0.217	0.218	0.869
60	19.754	0.961	0.173	1.306	0.57	0.915	0.132	0.454	0.161	0.0596	0.0441	0.242	0.138	0.217	0.218	0.218	0.218	0.871
60.083	19.823	0.963	0.173	1.309	0.572	0.918	0.133	0.455	0.162	0.0597	0.0441	0.242	0.138	0.218	0.218	0.218	0.219	0.873
60.167	19.892	0.965	0.173	1.312	0.573	0.92	0.133	0.456	0.162	0.0597	0.0441	0.243	0.138	0.218	0.219	0.219	0.219	0.875
60.25	19.961	0.968	0.174	1.315	0.574	0.922	0.133	0.457	0.162	0.0598	0.0441	0.243	0.138	0.219	0.219	0.219	0.22	0.877
60.333	20.031	0.97	0.174	1.319	0.576	0.925	0.134	0.458	0.163	0.0599	0.0442	0.243	0.138	0.219	0.22	0.22	0.22	0.879
60.417	20.1	0.972	0.175	1.322	0.577	0.927	0.134	0.459	0.163	0.06	0.0442	0.244	0.138	0.22	0.22	0.22	0.221	0.881
60.5	20.17	0.975	0.175	1.325	0.578	0.93	0.134	0.46	0.163	0.06	0.0442	0.244	0.138	0.221	0.221	0.221	0.221	0.884
60.583	20.24	0.977	0.175	1.328	0.58	0.932	0.135	0.461	0.164	0.0601	0.0442	0.244	0.138	0.221	0.221	0.221	0.222	0.885
60.667	20.31	0.979	0.176	1.332	0.581	0.934	0.135	0.462	0.164	0.0601	0.0442	0.244	0.138	0.222	0.222	0.222	0.223	0.889
60.75	20.38	0.982	0.176	1.335	0.582	0.937	0.135	0.463	0.164	0.0602	0.0442	0.244	0.138	0.222	0.222	0.223	0.223	0.89
60.833	20.45	0.984	0.176	1.338	0.584	0.939	0.136	0.464	0.165	0.0602	0.0442	0.244	0.138	0.223	0.223	0.223	0.224	0.893

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
60.917	20.52	0.986	0.176	1.341	0.585	0.941	0.136	0.465	0.165	0.0603	0.0442	0.245	0.138	0.223	0.223	0.224	0.224	0.894
61	20.591	0.988	0.177	1.344	0.586	0.944	0.136	0.466	0.166	0.0603	0.0442	0.245	0.138	0.224	0.224	0.224	0.225	0.897
61.083	20.662	0.991	0.177	1.347	0.587	0.946	0.136	0.466	0.166	0.0604	0.0442	0.245	0.138	0.224	0.224	0.225	0.225	0.898
61.167	20.733	0.993	0.177	1.35	0.589	0.949	0.137	0.467	0.166	0.0604	0.0442	0.245	0.138	0.225	0.225	0.225	0.226	0.901
61.25	20.804	0.995	0.177	1.354	0.59	0.951	0.137	0.468	0.167	0.0604	0.0442	0.245	0.138	0.225	0.226	0.226	0.226	0.903
61.333	20.875	0.997	0.178	1.357	0.591	0.953	0.137	0.469	0.167	0.0605	0.0442	0.245	0.138	0.226	0.226	0.226	0.227	0.905
61.417	20.947	0.999	0.178	1.36	0.593	0.956	0.138	0.47	0.167	0.0605	0.0442	0.245	0.138	0.226	0.227	0.227	0.227	0.907
61.5	21.018	1.002	0.178	1.363	0.594	0.958	0.138	0.471	0.168	0.0605	0.0442	0.245	0.138	0.227	0.227	0.227	0.228	0.909
61.583	21.09	1.004	0.178	1.366	0.595	0.96	0.138	0.472	0.168	0.0605	0.0442	0.245	0.138	0.227	0.228	0.228	0.228	0.911
61.667	21.162	1.006	0.178	1.369	0.596	0.963	0.139	0.472	0.168	0.0605	0.0442	0.245	0.138	0.228	0.228	0.228	0.229	0.913
61.75	21.234	1.008	0.178	1.372	0.598	0.965	0.139	0.473	0.169	0.0606	0.0442	0.245	0.138	0.228	0.229	0.229	0.229	0.915
61.833	21.306	1.01	0.179	1.375	0.599	0.967	0.139	0.474	0.169	0.0606	0.0442	0.245	0.138	0.229	0.229	0.229	0.23	0.917
61.917	21.378	1.012	0.179	1.378	0.6	0.969	0.139	0.475	0.169	0.0606	0.0442	0.245	0.138	0.229	0.23	0.23	0.23	0.919
62	21.451	1.015	0.179	1.381	0.601	0.972	0.14	0.475	0.169	0.0606	0.0442	0.245	0.138	0.23	0.23	0.23	0.231	0.921
62.083	21.523	1.017	0.179	1.384	0.603	0.974	0.14	0.476	0.17	0.0606	0.0442	0.245	0.138	0.23	0.231	0.231	0.231	0.923
62.167	21.596	1.019	0.179	1.387	0.604	0.976	0.14	0.477	0.17	0.0606	0.0442	0.245	0.138	0.231	0.231	0.231	0.232	0.925
62.25	21.668	1.021	0.179	1.39	0.605	0.978	0.141	0.477	0.17	0.0606	0.0442	0.245	0.138	0.231	0.232	0.232	0.232	0.927
62.333	21.741	1.023	0.179	1.393	0.606	0.98	0.141	0.478	0.17	0.0606	0.0442	0.245	0.138	0.232	0.232	0.232	0.233	0.929
62.417	21.814	1.025	0.18	1.396	0.607	0.982	0.141	0.479	0.171	0.0606	0.0442	0.245	0.138	0.232	0.233	0.233	0.233	0.931
62.5	21.886	1.027	0.18	1.399	0.608	0.985	0.142	0.479	0.171	0.0606	0.0442	0.245	0.138	0.233	0.233	0.233	0.234	0.933
62.583	21.96	1.029	0.18	1.402	0.609	0.987	0.142	0.48	0.171	0.0606	0.0442	0.245	0.138	0.233	0.234	0.234	0.234	0.935
62.667	22.033	1.031	0.18	1.405	0.61	0.989	0.142	0.481	0.171	0.0606	0.0442	0.245	0.138	0.234	0.234	0.234	0.235	0.937
62.75	22.106	1.033	0.18	1.408	0.611	0.991	0.142	0.481	0.172	0.0606	0.0442	0.245	0.138	0.234	0.235	0.235	0.235	0.939
62.833	22.179	1.035	0.18	1.411	0.612	0.993	0.143	0.482	0.172	0.0606	0.0442	0.245	0.138	0.235	0.235	0.235	0.236	0.941
62.917	22.253	1.036	0.18	1.413	0.613	0.995	0.143	0.482	0.172	0.0606	0.0442	0.245	0.138	0.235	0.235	0.236	0.236	0.942
63	22.326	1.038	0.18	1.416	0.614	0.997	0.143	0.483	0.172	0.0606	0.0442	0.245	0.138	0.236	0.236	0.236	0.237	0.945
63.083	22.4	1.04	0.18	1.419	0.615	0.999	0.143	0.483	0.173	0.0606	0.0442	0.245	0.138	0.236	0.236	0.237	0.237	0.946
63.167	22.473	1.042	0.18	1.422	0.616	1.001	0.144	0.484	0.173	0.0606	0.0442	0.245	0.138	0.237	0.237	0.237	0.238	0.949
63.25	22.546	1.043	0.18	1.424	0.617	1.003	0.144	0.484	0.173	0.0606	0.0442	0.245	0.138	0.237	0.237	0.237	0.238	0.949
63.333	22.62	1.045	0.181	1.427	0.618	1.005	0.144	0.485	0.173	0.0606	0.0442	0.245	0.138	0.237	0.238	0.238	0.238	0.951
63.417	22.693	1.047	0.181	1.429	0.619	1.007	0.144	0.485	0.173	0.0606	0.0442	0.245	0.138	0.238	0.238	0.238	0.239	0.953
63.5	22.767	1.048	0.181	1.432	0.619	1.009	0.145	0.486	0.174	0.0606	0.0442	0.245	0.138	0.238	0.239	0.239	0.239	0.955
63.583	22.84	1.05	0.181	1.434	0.62	1.011	0.145	0.486	0.174	0.0605	0.0441	0.245	0.137	0.239	0.239	0.239	0.24	0.957
63.667	22.914	1.051	0.181	1.437	0.621	1.012	0.145	0.487	0.174	0.0605	0.0441	0.245	0.137	0.239	0.239	0.239	0.24	0.957
63.75	22.987	1.053	0.181	1.439	0.622	1.014	0.145	0.487	0.174	0.0605	0.0441	0.245	0.137	0.239	0.24	0.24	0.24	0.959
63.833	23.061	1.054	0.181	1.441	0.622	1.016	0.145	0.487	0.174	0.0604	0.044	0.244	0.137	0.24	0.24	0.24	0.241	0.961
63.917	23.135	1.055	0.181	1.443	0.623	1.018	0.146	0.488	0.175	0.0604	0.0439	0.244	0.136	0.24	0.24	0.241	0.241	0.962
64	23.209	1.057	0.181	1.445	0.624	1.02	0.146	0.488	0.175	0.0603	0.0438	0.244	0.136	0.24	0.241	0.241	0.242	0.964
64.083	23.282	1.058	0.181	1.447	0.624	1.021	0.146	0.488	0.175	0.0602	0.0436	0.243	0.135	0.241	0.241	0.241	0.242	0.965
64.167	23.356	1.059	0.181	1.449	0.625	1.023	0.146	0.488	0.175	0.0601	0.0435	0.243	0.134	0.241	0.241	0.242	0.242	0.966
64.25	23.429	1.06	0.18	1.451	0.626	1.025	0.146	0.489	0.175	0.06	0.0433	0.242	0.134	0.241	0.242	0.242	0.243	0.968
64.333	23.503	1.061	0.18	1.453	0.626	1.026	0.146	0.489	0.175	0.0599	0.0431	0.241	0.133	0.242	0.242	0.242	0.243	0.969
64.417	23.576	1.062	0.18	1.455	0.627	1.028	0.147	0.489	0.175	0.0597	0.0429	0.241	0.132	0.242	0.242	0.243	0.243	0.97
64.5	23.649	1.063	0.18	1.457	0.627	1.03	0.147	0.489	0.176	0.0596	0.0427	0.24	0.131	0.242	0.243	0.243	0.243	0.971
64.583	23.723	1.064	0.18	1.458	0.628	1.031	0.147	0.489	0.176	0.0594	0.0425	0.239	0.131	0.243	0.243	0.243	0.244	0.973
64.667	23.796	1.065	0.18	1.46	0.628	1.033	0.147	0.489	0.176	0.0592	0.0423	0.238	0.13	0.243	0.243	0.243	0.244	0.973
64.75	23.869	1.066	0.179	1.462	0.628	1.034	0.147	0.489	0.176	0.059	0.0421	0.237	0.13	0.243	0.243	0.244	0.244	0.974
64.833	23.942	1.067	0.179	1.463	0.629	1.036	0.147	0.489	0.176	0.0588	0.042	0.236	0.129	0.243	0.244	0.244	0.245	0.976
64.917	24.015	1.068	0.179	1.465	0.629	1.037	0.147	0.489	0.176	0.0586	0.0418	0.235	0.129	0.244	0.244	0.244	0.245	0.977
65	24.088	1.069	0.179	1.466	0.63	1.039	0.147	0.489	0.176	0.0584	0.0417	0.235	0.129	0.244	0.244	0.244	0.245	0.977
65.083	24.161	1.069	0.178	1.467	0.63	1.04	0.148	0.489	0.176	0.0582	0.0416	0.234	0.128	0.244	0.244	0.245	0.245	0.978
65.167	24.234	1.07	0.178	1.469	0.63	1.041	0.148	0.489	0.176	0.0581	0.0415	0.233	0.128	0.244	0.245	0.245	0.245	0.979
65.25	24.307	1.071	0.178	1.47	0.631	1.043	0.148	0.489	0.176	0.0579	0.0414	0.232	0.128	0.245	0.245	0.245	0.246	0.981
65.333	24.379	1.071	0.177	1.471	0.631	1.044	0.148	0.489	0.176	0.0577	0.0413	0.232	0.128	0.245	0.245	0.245	0.246	0.981
65.417	24.452	1.072	0.177	1.472	0.631	1.045	0.148	0.488	0.176	0.0576	0.0412	0.231	0.127	0.245	0.245	0.245	0.246	0.981
65.5	24.524	1.072	0.177	1.473	0.631	1.046	0.148	0.488	0.176	0.0574	0.0411	0.231	0.127	0.245	0.245	0.246	0.246	0.982
65.583	24.596	1.073	0.176	1.474	0.631	1.048	0.148	0.488	0.176	0.0573	0.041	0.23	0.127	0.245	0.246	0.246	0.246	0.983
65.667	24.668	1.073	0.176	1.475	0.632	1.049	0.148	0.488	0.176	0.0572	0.041	0.23	0.127	0.245	0.246	0.246	0.247	0.984
65.75	24.74	1.073	0.176	1.476	0.632	1.05	0.148	0.487	0.176	0.0571	0.0409	0.229	0.127	0.246	0.246	0.246	0.247	0.985
65.833	24.812	1.074	0.175	1.477	0.632	1.051	0.148	0.487	0.176	0.057	0.0409	0.229	0.127	0.246	0.246	0.246	0.247	0.985
65.917	24.884	1.074	0.175	1.478	0.632	1.052	0.148	0.487	0.176	0.0569	0.0408	0.229	0.127	0.246	0.246	0.246	0.247	0.985
66	24.955	1.074	0.174	1.479	0.632	1.053	0.148	0.486	0.176	0.0568	0.0408	0.228	0.127	0.246	0.246	0.246	0.247	0.985
66.083	25.026	1.075	0.174	1.479	0.632	1.054	0.148	0.486	0.176	0.0567	0.0407	0.228	0.127	0.246	0.246	0.247	0.247	0.986

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
66.167	25.098	1.075	0.174	1.48	0.632	1.054	0.148	0.485	0.176	0.0566	0.0407	0.228	0.127	0.246	0.246	0.247	0.247	0.986
66.25	25.169	1.075	0.174	1.481	0.632	1.055	0.148	0.485	0.176	0.0565	0.0407	0.227	0.127	0.246	0.247	0.247	0.247	0.987
66.333	25.24	1.075	0.173	1.481	0.632	1.056	0.148	0.485	0.176	0.0564	0.0407	0.227	0.127	0.246	0.247	0.247	0.247	0.987
66.417	25.311	1.075	0.173	1.482	0.632	1.057	0.149	0.484	0.176	0.0564	0.0407	0.227	0.127	0.246	0.247	0.247	0.248	0.988
66.5	25.381	1.076	0.173	1.482	0.632	1.058	0.149	0.484	0.176	0.0563	0.0406	0.227	0.127	0.247	0.247	0.247	0.248	0.989
66.583	25.452	1.076	0.172	1.483	0.632	1.058	0.149	0.483	0.176	0.0562	0.0406	0.226	0.126	0.247	0.247	0.247	0.248	0.989
66.667	25.522	1.076	0.172	1.483	0.632	1.059	0.149	0.482	0.176	0.0561	0.0406	0.226	0.126	0.247	0.247	0.247	0.248	0.989
66.75	25.592	1.076	0.172	1.483	0.632	1.06	0.149	0.482	0.176	0.0561	0.0406	0.226	0.126	0.247	0.247	0.247	0.248	0.989
66.833	25.661	1.075	0.171	1.483	0.632	1.06	0.149	0.481	0.176	0.056	0.0405	0.225	0.126	0.247	0.247	0.247	0.248	0.989
66.917	25.731	1.075	0.171	1.483	0.632	1.061	0.149	0.481	0.176	0.0559	0.0404	0.225	0.125	0.247	0.247	0.247	0.248	0.989
67	25.8	1.075	0.171	1.484	0.631	1.062	0.149	0.48	0.175	0.0557	0.0403	0.224	0.125	0.247	0.247	0.247	0.248	0.989
67.083	25.869	1.075	0.171	1.484	0.631	1.062	0.149	0.479	0.175	0.0556	0.0401	0.224	0.124	0.247	0.247	0.247	0.248	0.989
67.167	25.938	1.075	0.17	1.483	0.631	1.063	0.148	0.479	0.175	0.0555	0.04	0.223	0.124	0.247	0.247	0.247	0.248	0.989
67.25	26.007	1.074	0.17	1.483	0.631	1.063	0.148	0.478	0.175	0.0553	0.0398	0.223	0.123	0.247	0.247	0.247	0.248	0.989
67.333	26.075	1.074	0.17	1.483	0.63	1.063	0.148	0.477	0.175	0.0552	0.0396	0.222	0.122	0.247	0.247	0.247	0.248	0.989
67.417	26.143	1.073	0.169	1.483	0.63	1.064	0.148	0.477	0.175	0.055	0.0394	0.221	0.121	0.247	0.247	0.247	0.248	0.989
67.5	26.211	1.073	0.169	1.483	0.629	1.064	0.148	0.476	0.175	0.0548	0.0392	0.22	0.121	0.247	0.247	0.247	0.248	0.989
67.583	26.279	1.072	0.169	1.482	0.629	1.065	0.148	0.475	0.174	0.0546	0.039	0.22	0.12	0.246	0.247	0.247	0.248	0.988
67.667	26.346	1.072	0.168	1.482	0.629	1.065	0.148	0.474	0.174	0.0544	0.0388	0.219	0.12	0.246	0.247	0.247	0.248	0.988
67.75	26.414	1.071	0.168	1.481	0.628	1.065	0.148	0.474	0.174	0.0542	0.0386	0.218	0.119	0.246	0.247	0.247	0.247	0.987
67.833	26.48	1.071	0.167	1.481	0.628	1.065	0.148	0.473	0.174	0.054	0.0385	0.217	0.119	0.246	0.247	0.247	0.247	0.987
67.917	26.547	1.07	0.167	1.48	0.627	1.066	0.148	0.472	0.174	0.0538	0.0383	0.216	0.118	0.246	0.246	0.247	0.247	0.986
68	26.613	1.069	0.167	1.48	0.626	1.066	0.148	0.471	0.173	0.0536	0.0382	0.215	0.118	0.246	0.246	0.246	0.247	0.985
68.083	26.679	1.068	0.166	1.479	0.626	1.066	0.148	0.471	0.173	0.0534	0.0381	0.214	0.117	0.246	0.246	0.246	0.247	0.985
68.167	26.745	1.067	0.166	1.478	0.625	1.066	0.148	0.47	0.173	0.0533	0.038	0.214	0.117	0.246	0.246	0.246	0.247	0.985
68.25	26.81	1.067	0.165	1.477	0.625	1.066	0.148	0.469	0.173	0.0531	0.0379	0.213	0.117	0.246	0.246	0.246	0.247	0.985
68.333	26.875	1.066	0.165	1.476	0.624	1.066	0.147	0.468	0.172	0.0529	0.0378	0.212	0.117	0.246	0.246	0.246	0.247	0.985
68.417	26.94	1.065	0.164	1.475	0.623	1.066	0.147	0.467	0.172	0.0528	0.0377	0.212	0.116	0.245	0.246	0.246	0.246	0.983
68.5	27.004	1.064	0.164	1.474	0.623	1.066	0.147	0.466	0.172	0.0526	0.0376	0.211	0.116	0.245	0.245	0.246	0.246	0.982
68.583	27.068	1.063	0.163	1.473	0.622	1.066	0.147	0.466	0.172	0.0525	0.0375	0.211	0.116	0.245	0.245	0.245	0.246	0.981
68.667	27.132	1.062	0.163	1.472	0.621	1.066	0.147	0.465	0.172	0.0524	0.0375	0.21	0.116	0.245	0.245	0.245	0.246	0.981
68.75	27.196	1.061	0.162	1.471	0.621	1.066	0.147	0.464	0.171	0.0523	0.0374	0.21	0.116	0.245	0.245	0.245	0.246	0.981
68.833	27.259	1.06	0.162	1.47	0.62	1.066	0.147	0.463	0.171	0.0521	0.0373	0.209	0.116	0.244	0.245	0.245	0.246	0.98
68.917	27.322	1.059	0.161	1.469	0.619	1.066	0.147	0.462	0.171	0.052	0.0373	0.209	0.116	0.244	0.245	0.245	0.245	0.979
69	27.384	1.058	0.161	1.468	0.619	1.066	0.146	0.461	0.171	0.0519	0.0373	0.209	0.116	0.244	0.244	0.245	0.245	0.978
69.083	27.446	1.057	0.161	1.467	0.618	1.065	0.146	0.46	0.17	0.0519	0.0372	0.208	0.116	0.244	0.244	0.244	0.245	0.977
69.167	27.508	1.056	0.16	1.465	0.617	1.065	0.146	0.459	0.17	0.0518	0.0372	0.208	0.116	0.244	0.244	0.244	0.245	0.977
69.25	27.569	1.055	0.16	1.464	0.616	1.065	0.146	0.458	0.17	0.0517	0.0372	0.208	0.116	0.243	0.244	0.244	0.245	0.976
69.333	27.63	1.054	0.159	1.463	0.616	1.064	0.146	0.457	0.17	0.0516	0.0371	0.208	0.116	0.243	0.244	0.244	0.244	0.975
69.417	27.69	1.053	0.159	1.462	0.615	1.064	0.146	0.456	0.169	0.0515	0.0371	0.207	0.116	0.243	0.243	0.243	0.244	0.973
69.5	27.751	1.051	0.159	1.46	0.614	1.064	0.146	0.455	0.169	0.0515	0.0371	0.207	0.116	0.243	0.243	0.243	0.244	0.973
69.583	27.81	1.05	0.158	1.459	0.613	1.063	0.145	0.454	0.169	0.0514	0.0371	0.207	0.116	0.243	0.243	0.243	0.244	0.973
69.667	27.869	1.049	0.158	1.458	0.613	1.063	0.145	0.453	0.169	0.0514	0.0371	0.207	0.116	0.242	0.243	0.243	0.243	0.971
69.75	27.929	1.048	0.158	1.456	0.612	1.062	0.145	0.452	0.168	0.0513	0.0371	0.206	0.116	0.242	0.242	0.243	0.243	0.97
69.833	27.987	1.047	0.157	1.455	0.611	1.062	0.145	0.451	0.168	0.0512	0.0371	0.206	0.116	0.242	0.242	0.242	0.243	0.969
69.917	28.045	1.045	0.157	1.454	0.61	1.061	0.145	0.451	0.168	0.0512	0.0371	0.206	0.116	0.242	0.242	0.242	0.243	0.969
70	28.103	1.044	0.157	1.452	0.609	1.061	0.145	0.45	0.167	0.0511	0.0371	0.206	0.116	0.241	0.242	0.242	0.243	0.968
70.083	28.16	1.043	0.157	1.451	0.608	1.06	0.144	0.449	0.167	0.0511	0.0371	0.206	0.116	0.241	0.242	0.242	0.242	0.967
70.167	28.217	1.042	0.156	1.449	0.607	1.059	0.144	0.448	0.167	0.0511	0.0371	0.206	0.116	0.241	0.241	0.241	0.242	0.965
70.25	28.274	1.04	0.156	1.448	0.607	1.059	0.144	0.447	0.167	0.051	0.0371	0.206	0.116	0.241	0.241	0.241	0.242	0.965
70.333	28.329	1.039	0.156	1.446	0.606	1.058	0.144	0.446	0.166	0.051	0.0371	0.206	0.116	0.24	0.241	0.241	0.242	0.964
70.417	28.385	1.038	0.156	1.445	0.605	1.057	0.144	0.445	0.166	0.051	0.0371	0.206	0.116	0.24	0.241	0.241	0.241	0.963
70.5	28.44	1.036	0.156	1.443	0.604	1.056	0.144	0.444	0.166	0.0509	0.0371	0.206	0.116	0.24	0.24	0.24	0.241	0.961
70.583	28.494	1.035	0.155	1.442	0.603	1.056	0.143	0.444	0.165	0.0509	0.0371	0.206	0.116	0.24	0.24	0.24	0.241	0.961
70.667	28.548	1.034	0.155	1.44	0.602	1.055	0.143	0.443	0.165	0.0509	0.0371	0.206	0.116	0.239	0.24	0.24	0.241	0.96
70.75	28.602	1.032	0.155	1.439	0.601	1.054	0.143	0.442	0.165	0.0509	0.0371	0.206	0.116	0.239	0.239	0.24	0.24	0.958
70.833	28.655	1.031	0.155	1.437	0.6	1.053	0.143	0.441	0.165	0.0509	0.0371	0.206	0.116	0.239	0.239	0.239	0.24	0.957
70.917	28.707	1.029	0.155	1.435	0.599	1.052	0.143	0.44	0.164	0.0509	0.0371	0.206	0.116	0.239	0.239	0.239	0.24	0.957
71	28.76	1.028	0.155	1.434	0.598	1.051	0.142	0.44	0.164	0.0509	0.0371	0.206	0.116	0.238	0.239	0.239	0.239	0.955
71.083	28.811	1.026	0.154	1.432	0.597	1.05	0.142	0.439	0.164	0.0509	0.0371	0.206	0.116	0.238	0.238	0.239	0.239	0.954
71.167	28.863	1.025	0.154	1.43	0.597	1.049	0.142	0.438	0.163	0.0509	0.0371	0.206	0.116	0.238	0.238	0.238	0.239	0.953
71.25	28.914	1.023	0.154	1.429	0.596	1.048	0.142	0.438	0.163	0.0509	0.0371	0.206	0.116	0.238	0.238	0.238	0.239	0.953
71.333	28.963	1.022	0.154	1.427	0.595	1.047	0.142	0.437	0.163	0.0509	0.0371	0.206	0.116	0.237	0.238	0.238	0.238	0.951

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
71.417	29.013	1.02	0.154	1.425	0.594	1.047	0.141	0.436	0.163	0.0509	0.0371	0.206	0.116	0.237	0.237	0.237	0.238	0.949
71.5	29.063	1.019	0.154	1.423	0.593	1.046	0.141	0.436	0.162	0.0509	0.0371	0.206	0.116	0.237	0.237	0.237	0.238	0.949
71.583	29.11	1.018	0.154	1.422	0.592	1.045	0.141	0.435	0.162	0.0509	0.0371	0.206	0.116	0.236	0.237	0.237	0.237	0.947
71.667	29.158	1.016	0.154	1.42	0.591	1.043	0.141	0.434	0.162	0.0509	0.0371	0.206	0.116	0.236	0.236	0.236	0.237	0.945
71.75	29.206	1.015	0.153	1.418	0.59	1.042	0.141	0.434	0.162	0.0509	0.0371	0.206	0.116	0.236	0.236	0.236	0.237	0.945
71.833	29.253	1.013	0.153	1.416	0.59	1.041	0.14	0.433	0.161	0.0509	0.0371	0.206	0.116	0.235	0.236	0.236	0.237	0.944
71.917	29.299	1.012	0.153	1.415	0.589	1.04	0.14	0.433	0.161	0.0509	0.0371	0.206	0.116	0.235	0.235	0.236	0.236	0.942
72	29.345	1.011	0.153	1.413	0.588	1.039	0.14	0.432	0.161	0.0509	0.0371	0.206	0.116	0.235	0.235	0.235	0.236	0.941
72.083	29.39	1.009	0.153	1.411	0.587	1.038	0.14	0.431	0.161	0.0509	0.0371	0.206	0.116	0.235	0.235	0.235	0.236	0.941
72.167	29.434	1.008	0.153	1.409	0.586	1.037	0.14	0.431	0.161	0.0509	0.0371	0.206	0.116	0.234	0.235	0.235	0.235	0.939
72.25	29.479	1.007	0.153	1.408	0.586	1.036	0.14	0.43	0.16	0.0509	0.0371	0.206	0.116	0.234	0.234	0.234	0.235	0.937
72.333	29.522	1.005	0.153	1.406	0.585	1.035	0.139	0.43	0.16	0.0509	0.0371	0.206	0.116	0.234	0.234	0.234	0.235	0.937
72.417	29.565	1.004	0.153	1.404	0.584	1.034	0.139	0.429	0.16	0.0509	0.0371	0.206	0.116	0.233	0.234	0.234	0.234	0.935
72.5	29.608	1.003	0.153	1.402	0.583	1.032	0.139	0.429	0.16	0.0509	0.0371	0.206	0.116	0.233	0.233	0.234	0.234	0.934
72.583	29.649	1.002	0.153	1.401	0.583	1.031	0.139	0.428	0.159	0.0508	0.0371	0.206	0.115	0.233	0.233	0.233	0.234	0.933
72.667	29.69	1	0.153	1.399	0.582	1.03	0.139	0.428	0.159	0.0508	0.037	0.205	0.115	0.233	0.233	0.233	0.234	0.933
72.75	29.731	0.999	0.152	1.397	0.581	1.029	0.139	0.428	0.159	0.0508	0.0369	0.205	0.115	0.232	0.233	0.233	0.233	0.931
72.833	29.77	0.998	0.152	1.396	0.58	1.027	0.138	0.427	0.159	0.0506	0.0368	0.205	0.114	0.232	0.232	0.232	0.233	0.929
72.917	29.809	0.996	0.152	1.394	0.579	1.026	0.138	0.426	0.159	0.0505	0.0366	0.204	0.113	0.232	0.232	0.232	0.233	0.929
73	29.848	0.995	0.152	1.392	0.579	1.025	0.138	0.426	0.158	0.0504	0.0364	0.203	0.112	0.231	0.232	0.232	0.232	0.927
73.083	29.885	0.994	0.152	1.39	0.578	1.023	0.138	0.425	0.158	0.0502	0.036	0.202	0.111	0.231	0.231	0.232	0.232	0.926
73.167	29.922	0.992	0.151	1.388	0.577	1.022	0.138	0.425	0.158	0.0499	0.0357	0.201	0.109	0.231	0.231	0.231	0.232	0.925
73.25	29.959	0.991	0.151	1.386	0.576	1.02	0.137	0.424	0.158	0.0497	0.0353	0.2	0.107	0.23	0.231	0.231	0.231	0.923
73.333	29.995	0.989	0.151	1.384	0.575	1.019	0.137	0.423	0.157	0.0494	0.0348	0.198	0.106	0.23	0.23	0.231	0.231	0.922
73.417	30.03	0.988	0.15	1.382	0.574	1.017	0.137	0.422	0.157	0.0491	0.0344	0.196	0.104	0.23	0.23	0.23	0.231	0.921
73.5	30.065	0.986	0.15	1.38	0.573	1.016	0.137	0.422	0.157	0.0487	0.0339	0.195	0.102	0.229	0.23	0.23	0.23	0.919
73.583	30.099	0.985	0.149	1.378	0.572	1.014	0.137	0.421	0.156	0.0483	0.0334	0.193	0.1	0.229	0.229	0.23	0.23	0.918
73.667	30.132	0.983	0.149	1.376	0.571	1.013	0.136	0.42	0.156	0.0478	0.0329	0.19	0.0988	0.229	0.229	0.229	0.23	0.917
73.75	30.165	0.981	0.148	1.374	0.57	1.011	0.136	0.419	0.156	0.0474	0.0324	0.188	0.0973	0.228	0.229	0.229	0.229	0.915
73.833	30.197	0.979	0.148	1.372	0.569	1.009	0.136	0.418	0.156	0.0469	0.032	0.186	0.0962	0.228	0.228	0.228	0.229	0.913
73.917	30.228	0.978	0.147	1.37	0.568	1.008	0.136	0.417	0.155	0.0464	0.0316	0.184	0.095	0.228	0.228	0.228	0.229	0.913
74	30.259	0.976	0.146	1.368	0.567	1.006	0.135	0.416	0.155	0.0459	0.0312	0.182	0.0939	0.227	0.228	0.228	0.228	0.911
74.083	30.288	0.974	0.146	1.365	0.566	1.004	0.135	0.415	0.155	0.0455	0.0309	0.18	0.0931	0.227	0.227	0.227	0.228	0.909
74.167	30.317	0.972	0.145	1.363	0.565	1.003	0.135	0.414	0.154	0.045	0.0306	0.178	0.0923	0.227	0.227	0.227	0.228	0.909
74.25	30.346	0.97	0.144	1.361	0.563	1.001	0.135	0.413	0.154	0.0445	0.0303	0.176	0.0915	0.226	0.226	0.227	0.227	0.906
74.333	30.373	0.968	0.143	1.358	0.562	0.999	0.134	0.412	0.154	0.0442	0.0301	0.174	0.091	0.226	0.226	0.226	0.227	0.905
74.417	30.399	0.966	0.143	1.356	0.561	0.997	0.134	0.41	0.153	0.0438	0.0299	0.173	0.0904	0.225	0.226	0.226	0.226	0.903
74.5	30.426	0.965	0.142	1.353	0.56	0.995	0.134	0.409	0.153	0.0434	0.0296	0.171	0.0898	0.225	0.225	0.225	0.226	0.901
74.583	30.451	0.962	0.141	1.351	0.559	0.994	0.134	0.408	0.152	0.043	0.0295	0.17	0.0894	0.225	0.225	0.225	0.226	0.901
74.667	30.475	0.96	0.14	1.348	0.557	0.992	0.133	0.407	0.152	0.0427	0.0293	0.169	0.0891	0.224	0.224	0.224	0.225	0.897
74.75	30.5	0.958	0.139	1.345	0.556	0.99	0.133	0.405	0.152	0.0424	0.0291	0.168	0.0887	0.224	0.224	0.224	0.225	0.897
74.833	30.523	0.956	0.138	1.343	0.555	0.988	0.133	0.404	0.151	0.0421	0.029	0.167	0.0885	0.223	0.223	0.224	0.224	0.894
74.917	30.545	0.954	0.137	1.34	0.553	0.986	0.132	0.403	0.151	0.0418	0.0288	0.166	0.0883	0.223	0.223	0.223	0.224	0.893
75	30.568	0.952	0.136	1.337	0.552	0.984	0.132	0.401	0.151	0.0416	0.0287	0.165	0.0882	0.222	0.223	0.223	0.223	0.891
75.083	30.588	0.95	0.135	1.334	0.551	0.982	0.132	0.4	0.15	0.0413	0.0286	0.164	0.0881	0.222	0.222	0.222	0.223	0.889
75.167	30.608	0.947	0.135	1.332	0.549	0.98	0.131	0.398	0.15	0.0411	0.0285	0.163	0.0881	0.221	0.222	0.222	0.222	0.887
75.25	30.628	0.945	0.134	1.329	0.548	0.978	0.131	0.397	0.149	0.0409	0.0284	0.162	0.0881	0.221	0.221	0.221	0.222	0.885
75.333	30.645	0.943	0.133	1.326	0.546	0.976	0.131	0.395	0.149	0.0407	0.0284	0.162	0.0881	0.22	0.221	0.221	0.221	0.883
75.417	30.663	0.941	0.132	1.323	0.545	0.974	0.131	0.393	0.148	0.0405	0.0283	0.161	0.0881	0.22	0.22	0.22	0.221	0.881
75.5	30.68	0.938	0.131	1.32	0.544	0.972	0.13	0.392	0.148	0.0404	0.0283	0.16	0.0881	0.219	0.22	0.22	0.22	0.879
75.583	30.695	0.936	0.131	1.317	0.542	0.97	0.13	0.39	0.147	0.0402	0.0283	0.16	0.088	0.219	0.219	0.219	0.22	0.877
75.667	30.711	0.933	0.13	1.314	0.54	0.968	0.13	0.388	0.147	0.04	0.0282	0.159	0.0879	0.218	0.219	0.219	0.219	0.875
75.75	30.726	0.931	0.129	1.311	0.539	0.966	0.129	0.386	0.146	0.0399	0.0282	0.159	0.0878	0.218	0.218	0.218	0.219	0.873
75.833	30.738	0.928	0.129	1.308	0.537	0.964	0.129	0.384	0.146	0.0397	0.0282	0.158	0.0875	0.217	0.218	0.218	0.218	0.871
75.917	30.751	0.926	0.128	1.304	0.536	0.962	0.129	0.383	0.145	0.0395	0.0281	0.157	0.0872	0.217	0.217	0.217	0.218	0.869
76	30.764	0.923	0.127	1.301	0.534	0.96	0.128	0.381	0.145	0.0393	0.028	0.157	0.0869	0.216	0.216	0.217	0.217	0.866
76.083	30.774	0.921	0.127	1.298	0.532	0.958	0.128	0.379	0.144	0.0391	0.0279	0.156	0.0863	0.216	0.216	0.216	0.217	0.865
76.167	30.785	0.918	0.126	1.294	0.531	0.956	0.127	0.377	0.144	0.039	0.0277	0.156	0.0857	0.215	0.215	0.215	0.216	0.861
76.25	30.795	0.915	0.125	1.291	0.529	0.954	0.127	0.375	0.143	0.0388	0.0276	0.155	0.085	0.214	0.215	0.215	0.215	0.859
76.333	30.802	0.912	0.125	1.287	0.527	0.951	0.127	0.374	0.143	0.0386	0.0274	0.154	0.0843	0.214	0.214	0.214	0.215	0.857
76.417	30.81	0.909	0.124	1.284	0.525	0.949	0.126	0.372	0.142	0.0384	0.0272	0.153	0.0836	0.213	0.214	0.214	0.214	0.855
76.5	30.818	0.906	0.124	1.28	0.523	0.947	0.126	0.37	0.141	0.0382	0.027	0.153	0.0828	0.213	0.213	0.213	0.214	0.853
76.583	30.822	0.903	0.123	1.276	0.521	0.945	0.126	0.368	0.141	0.0379	0.0268	0.152	0.0822	0.212	0.212	0.212	0.213	0.849

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
76.667	30.827	0.9	0.122	1.272	0.519	0.942	0.125	0.367	0.14	0.0377	0.0266	0.151	0.0815	0.211	0.212	0.212	0.212	0.847
76.75	30.832	0.897	0.122	1.269	0.517	0.94	0.125	0.365	0.139	0.0375	0.0264	0.15	0.0809	0.211	0.211	0.211	0.212	0.845
76.833	30.834	0.894	0.121	1.265	0.515	0.938	0.124	0.363	0.139	0.0373	0.0263	0.149	0.0804	0.21	0.21	0.211	0.211	0.842
76.917	30.836	0.891	0.121	1.261	0.513	0.935	0.124	0.362	0.138	0.0371	0.0261	0.148	0.08	0.209	0.21	0.21	0.21	0.839
77	30.838	0.887	0.12	1.257	0.511	0.933	0.123	0.36	0.138	0.0369	0.026	0.147	0.0795	0.209	0.209	0.209	0.21	0.837
77.083	30.838	0.884	0.119	1.253	0.509	0.93	0.123	0.358	0.137	0.0367	0.0258	0.147	0.0792	0.208	0.208	0.208	0.209	0.833
77.167	30.838	0.881	0.119	1.249	0.507	0.928	0.122	0.357	0.137	0.0365	0.0257	0.146	0.0789	0.207	0.208	0.208	0.208	0.831
77.25	30.837	0.877	0.118	1.244	0.505	0.926	0.122	0.355	0.136	0.0363	0.0256	0.145	0.0785	0.207	0.207	0.207	0.208	0.829
77.333	30.834	0.874	0.117	1.24	0.503	0.923	0.122	0.353	0.135	0.0361	0.0255	0.144	0.0783	0.206	0.206	0.206	0.207	0.825
77.417	30.831	0.87	0.117	1.236	0.501	0.921	0.121	0.352	0.135	0.036	0.0254	0.144	0.0781	0.205	0.206	0.206	0.206	0.823
77.5	30.828	0.867	0.116	1.231	0.499	0.918	0.121	0.35	0.134	0.0358	0.0253	0.143	0.0778	0.205	0.205	0.205	0.205	0.82
77.583	30.822	0.864	0.115	1.227	0.497	0.916	0.12	0.349	0.134	0.0357	0.0252	0.143	0.0777	0.204	0.204	0.204	0.205	0.817
77.667	30.816	0.86	0.115	1.222	0.495	0.913	0.12	0.347	0.133	0.0355	0.0252	0.142	0.0775	0.203	0.203	0.203	0.204	0.813
77.75	30.81	0.857	0.114	1.218	0.493	0.911	0.119	0.345	0.133	0.0354	0.0251	0.142	0.0773	0.202	0.203	0.203	0.203	0.811
77.833	30.801	0.853	0.114	1.213	0.491	0.908	0.119	0.344	0.132	0.0353	0.025	0.141	0.0773	0.202	0.202	0.202	0.202	0.808
77.917	30.792	0.85	0.113	1.209	0.489	0.905	0.118	0.342	0.131	0.0352	0.025	0.141	0.0772	0.201	0.201	0.201	0.202	0.805
78	30.783	0.847	0.112	1.204	0.487	0.903	0.118	0.341	0.131	0.0351	0.0249	0.14	0.0771	0.2	0.2	0.2	0.201	0.801
78.083	30.772	0.843	0.112	1.2	0.485	0.9	0.117	0.339	0.13	0.035	0.0249	0.14	0.0771	0.199	0.2	0.2	0.2	0.799
78.167	30.76	0.84	0.111	1.195	0.483	0.897	0.117	0.338	0.13	0.0349	0.0248	0.14	0.0771	0.199	0.199	0.199	0.199	0.796
78.25	30.749	0.837	0.111	1.191	0.481	0.895	0.116	0.336	0.129	0.0348	0.0248	0.139	0.0771	0.198	0.198	0.198	0.199	0.793
78.333	30.735	0.834	0.11	1.186	0.479	0.892	0.116	0.335	0.129	0.0347	0.0248	0.139	0.0771	0.197	0.197	0.197	0.198	0.789
78.417	30.72	0.83	0.11	1.182	0.477	0.889	0.116	0.333	0.128	0.0347	0.0248	0.139	0.0771	0.196	0.197	0.197	0.197	0.787
78.5	30.706	0.827	0.109	1.178	0.475	0.886	0.115	0.332	0.128	0.0346	0.0248	0.139	0.0771	0.196	0.196	0.196	0.196	0.784
78.583	30.689	0.824	0.109	1.173	0.473	0.884	0.115	0.331	0.127	0.0345	0.0247	0.138	0.077	0.195	0.195	0.195	0.196	0.781
78.667	30.673	0.821	0.108	1.169	0.471	0.881	0.114	0.329	0.127	0.0344	0.0247	0.138	0.077	0.194	0.194	0.195	0.195	0.778
78.75	30.656	0.818	0.108	1.165	0.47	0.878	0.114	0.328	0.126	0.0344	0.0247	0.138	0.077	0.193	0.194	0.194	0.194	0.775
78.833	30.636	0.814	0.107	1.16	0.468	0.875	0.113	0.326	0.126	0.0343	0.0247	0.138	0.0768	0.193	0.193	0.193	0.194	0.773
78.917	30.617	0.811	0.107	1.156	0.466	0.872	0.113	0.325	0.125	0.0342	0.0247	0.137	0.0767	0.192	0.192	0.192	0.193	0.769
79	30.597	0.808	0.107	1.152	0.464	0.869	0.112	0.323	0.125	0.0342	0.0246	0.137	0.0765	0.191	0.192	0.192	0.192	0.767
79.083	30.575	0.805	0.106	1.147	0.462	0.866	0.112	0.322	0.124	0.0341	0.0246	0.137	0.0762	0.191	0.191	0.191	0.191	0.764
79.167	30.553	0.802	0.106	1.143	0.46	0.863	0.112	0.321	0.123	0.034	0.0245	0.137	0.076	0.19	0.19	0.19	0.191	0.761
79.25	30.53	0.799	0.106	1.139	0.459	0.86	0.111	0.319	0.123	0.0339	0.0244	0.136	0.0757	0.189	0.189	0.189	0.19	0.757
79.333	30.506	0.796	0.105	1.135	0.457	0.857	0.111	0.318	0.122	0.0338	0.0243	0.136	0.0753	0.188	0.189	0.189	0.189	0.755
79.417	30.481	0.793	0.105	1.13	0.455	0.854	0.11	0.317	0.122	0.0337	0.0242	0.136	0.0749	0.188	0.188	0.188	0.189	0.753
79.5	30.456	0.789	0.105	1.126	0.453	0.851	0.11	0.315	0.121	0.0336	0.0242	0.135	0.0745	0.187	0.187	0.187	0.188	0.749
79.583	30.428	0.786	0.104	1.122	0.451	0.848	0.109	0.314	0.121	0.0335	0.0241	0.135	0.0742	0.186	0.187	0.187	0.187	0.747
79.667	30.401	0.783	0.104	1.118	0.449	0.845	0.109	0.313	0.12	0.0334	0.024	0.134	0.0739	0.186	0.186	0.186	0.186	0.744
79.75	30.374	0.78	0.104	1.113	0.448	0.842	0.109	0.311	0.12	0.0333	0.0239	0.134	0.0736	0.185	0.185	0.185	0.186	0.741
79.833	30.344	0.777	0.103	1.109	0.446	0.839	0.108	0.31	0.119	0.0332	0.0238	0.133	0.0733	0.184	0.184	0.185	0.185	0.738
79.917	30.314	0.774	0.103	1.105	0.444	0.836	0.108	0.309	0.119	0.0331	0.0237	0.133	0.0731	0.184	0.184	0.184	0.184	0.736
80	30.284	0.771	0.103	1.101	0.442	0.833	0.107	0.308	0.119	0.033	0.0236	0.133	0.0728	0.183	0.183	0.183	0.184	0.733
80.083	30.252	0.768	0.103	1.097	0.44	0.83	0.107	0.306	0.118	0.0329	0.0235	0.132	0.0727	0.182	0.182	0.182	0.183	0.729
80.167	30.22	0.765	0.102	1.092	0.439	0.827	0.107	0.305	0.118	0.0328	0.0235	0.132	0.0725	0.181	0.182	0.182	0.182	0.727
80.25	30.188	0.762	0.102	1.088	0.437	0.824	0.106	0.304	0.117	0.0327	0.0234	0.131	0.0723	0.181	0.181	0.181	0.182	0.725
80.333	30.153	0.759	0.102	1.084	0.435	0.821	0.106	0.303	0.117	0.0326	0.0234	0.131	0.0722	0.18	0.18	0.18	0.181	0.721
80.417	30.118	0.756	0.101	1.08	0.434	0.818	0.105	0.302	0.116	0.0325	0.0233	0.131	0.0721	0.179	0.18	0.18	0.18	0.719
80.5	30.084	0.753	0.101	1.076	0.432	0.815	0.105	0.301	0.116	0.0325	0.0233	0.13	0.072	0.179	0.179	0.179	0.18	0.717
80.583	30.047	0.75	0.101	1.072	0.43	0.812	0.104	0.299	0.115	0.0324	0.0232	0.13	0.0719	0.178	0.178	0.178	0.179	0.713
80.667	30.01	0.747	0.101	1.068	0.429	0.809	0.104	0.298	0.115	0.0323	0.0232	0.13	0.0718	0.177	0.178	0.178	0.178	0.711
80.75	29.973	0.745	0.1	1.064	0.427	0.806	0.104	0.297	0.115	0.0323	0.0232	0.13	0.0717	0.177	0.177	0.177	0.177	0.708
80.833	29.934	0.742	0.1	1.06	0.425	0.803	0.103	0.296	0.114	0.0322	0.0231	0.129	0.0717	0.176	0.176	0.176	0.177	0.705
80.917	29.895	0.739	0.0997	1.056	0.424	0.8	0.103	0.295	0.114	0.0321	0.0231	0.129	0.0716	0.175	0.176	0.176	0.176	0.703
81	29.855	0.736	0.0994	1.052	0.422	0.797	0.103	0.294	0.113	0.0321	0.0231	0.129	0.0716	0.175	0.175	0.175	0.175	0.7
81.083	29.814	0.734	0.0992	1.048	0.421	0.795	0.102	0.293	0.113	0.032	0.0231	0.129	0.0716	0.174	0.174	0.174	0.175	0.697
81.167	29.773	0.731	0.0989	1.044	0.419	0.792	0.102	0.292	0.113	0.032	0.023	0.129	0.0716	0.173	0.174	0.174	0.174	0.695
81.25	29.732	0.728	0.0987	1.04	0.418	0.789	0.101	0.291	0.112	0.0319	0.023	0.129	0.0715	0.173	0.173	0.173	0.174	0.693
81.333	29.689	0.726	0.0984	1.036	0.416	0.786	0.101	0.29	0.112	0.0319	0.023	0.128	0.0715	0.172	0.172	0.172	0.173	0.689
81.417	29.646	0.723	0.0982	1.033	0.415	0.783	0.101	0.289	0.111	0.0319	0.023	0.128	0.0715	0.172	0.172	0.172	0.172	0.688
81.5	29.603	0.721	0.098	1.029	0.414	0.78	0.1	0.288	0.111	0.0318	0.023	0.128	0.0715	0.171	0.171	0.171	0.172	0.685
81.583	29.558	0.718	0.0978	1.025	0.412	0.778	0.1	0.287	0.111	0.0318	0.023	0.128	0.0715	0.17	0.171	0.171	0.171	0.683
81.667	29.513	0.716	0.0976	1.022	0.411	0.775	0.0997	0.286	0.11	0.0318	0.023	0.128	0.0715	0.17	0.17	0.17	0.17	0.68
81.75	29.468	0.713	0.0974	1.018	0.409	0.772	0.0993	0.285	0.11	0.0317	0.0229	0.128	0.0714	0.169	0.169	0.169	0.17	0.677
81.833	29.421	0.711	0.0971	1.014	0.408	0.769	0.099	0.284	0.109	0.0317	0.0229	0.127	0.0712	0.169	0.169	0.169	0.169	0.676

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
81.917	29.374	0.708	0.0969	1.011	0.406	0.766	0.0986	0.283	0.109	0.0316	0.0228	0.127	0.0709	0.168	0.168	0.168	0.169	0.673
82	29.327	0.706	0.0967	1.007	0.405	0.764	0.0983	0.282	0.109	0.0315	0.0228	0.127	0.0707	0.167	0.168	0.168	0.168	0.671
82.083	29.279	0.704	0.0965	1.004	0.404	0.761	0.098	0.281	0.108	0.0314	0.0227	0.127	0.0701	0.167	0.167	0.167	0.168	0.669
82.167	29.23	0.701	0.0962	1.001	0.402	0.758	0.0976	0.28	0.108	0.0313	0.0225	0.126	0.0696	0.166	0.166	0.166	0.167	0.665
82.25	29.182	0.699	0.096	0.997	0.401	0.755	0.0973	0.279	0.108	0.0312	0.0224	0.126	0.069	0.166	0.166	0.166	0.166	0.664
82.333	29.132	0.696	0.0957	0.994	0.4	0.752	0.097	0.278	0.107	0.0311	0.0222	0.125	0.0682	0.165	0.165	0.165	0.166	0.661
82.417	29.082	0.694	0.0955	0.99	0.398	0.75	0.0966	0.277	0.107	0.031	0.0221	0.124	0.0675	0.164	0.165	0.165	0.165	0.659
82.5	29.032	0.692	0.0952	0.987	0.397	0.747	0.0963	0.276	0.106	0.0308	0.0219	0.124	0.0667	0.164	0.164	0.164	0.165	0.657
82.583	28.98	0.689	0.0949	0.983	0.395	0.744	0.096	0.275	0.106	0.0306	0.0217	0.123	0.0661	0.163	0.164	0.164	0.164	0.655
82.667	28.929	0.687	0.0947	0.98	0.394	0.741	0.0956	0.275	0.106	0.0305	0.0215	0.122	0.0654	0.163	0.163	0.163	0.164	0.653
82.75	28.877	0.684	0.0944	0.977	0.393	0.738	0.0953	0.274	0.105	0.0303	0.0213	0.121	0.0647	0.162	0.162	0.163	0.163	0.65
82.833	28.824	0.682	0.0941	0.973	0.391	0.736	0.095	0.273	0.105	0.0301	0.0211	0.12	0.0642	0.162	0.162	0.162	0.162	0.648
82.917	28.771	0.68	0.0938	0.97	0.39	0.733	0.0947	0.272	0.104	0.0299	0.0209	0.119	0.0637	0.161	0.161	0.161	0.162	0.645
83	28.718	0.677	0.0934	0.967	0.388	0.73	0.0943	0.271	0.104	0.0297	0.0207	0.118	0.0632	0.161	0.161	0.161	0.161	0.644
83.083	28.663	0.675	0.0931	0.963	0.387	0.727	0.094	0.27	0.104	0.0295	0.0206	0.118	0.0629	0.16	0.16	0.16	0.161	0.641
83.167	28.609	0.672	0.0928	0.96	0.386	0.725	0.0937	0.269	0.103	0.0293	0.0205	0.117	0.0625	0.159	0.16	0.16	0.16	0.639
83.25	28.554	0.67	0.0924	0.957	0.384	0.722	0.0933	0.268	0.103	0.0291	0.0203	0.116	0.0622	0.159	0.159	0.159	0.16	0.637
83.333	28.499	0.668	0.092	0.953	0.383	0.719	0.093	0.267	0.103	0.029	0.0202	0.115	0.0619	0.158	0.159	0.159	0.159	0.635
83.417	28.443	0.665	0.0916	0.95	0.381	0.716	0.0927	0.266	0.102	0.0288	0.0201	0.115	0.0617	0.158	0.158	0.158	0.159	0.633
83.5	28.388	0.663	0.0912	0.947	0.38	0.714	0.0923	0.266	0.102	0.0286	0.0201	0.114	0.0614	0.157	0.157	0.158	0.158	0.63
83.583	28.331	0.66	0.0908	0.943	0.379	0.711	0.092	0.265	0.101	0.0285	0.02	0.114	0.0612	0.157	0.157	0.157	0.157	0.628
83.667	28.274	0.658	0.0904	0.94	0.377	0.708	0.0917	0.264	0.101	0.0283	0.0199	0.113	0.0611	0.156	0.156	0.156	0.157	0.625
83.75	28.217	0.656	0.09	0.937	0.376	0.706	0.0913	0.263	0.101	0.0282	0.0198	0.113	0.0609	0.156	0.156	0.156	0.156	0.624
83.833	28.16	0.653	0.0895	0.933	0.375	0.703	0.091	0.262	0.1	0.0281	0.0198	0.112	0.0608	0.155	0.155	0.155	0.156	0.621
83.917	28.102	0.651	0.0891	0.93	0.373	0.701	0.0907	0.261	0.0999	0.028	0.0197	0.112	0.0607	0.155	0.155	0.155	0.155	0.62
84	28.044	0.649	0.0887	0.927	0.372	0.698	0.0904	0.26	0.0996	0.0279	0.0196	0.111	0.0606	0.154	0.154	0.154	0.155	0.617
84.083	27.985	0.646	0.0883	0.923	0.371	0.695	0.09	0.259	0.0992	0.0278	0.0196	0.111	0.0606	0.153	0.154	0.154	0.154	0.615
84.167	27.926	0.644	0.0879	0.92	0.369	0.693	0.0897	0.259	0.0989	0.0277	0.0196	0.111	0.0606	0.153	0.153	0.153	0.154	0.613
84.25	27.868	0.642	0.0875	0.917	0.368	0.69	0.0894	0.258	0.0985	0.0276	0.0195	0.11	0.0605	0.152	0.153	0.153	0.153	0.611
84.333	27.808	0.639	0.0872	0.914	0.367	0.688	0.0891	0.257	0.0981	0.0275	0.0195	0.11	0.0605	0.152	0.152	0.152	0.152	0.608
84.417	27.748	0.637	0.0868	0.911	0.365	0.685	0.0888	0.256	0.0978	0.0274	0.0195	0.11	0.0605	0.151	0.151	0.152	0.152	0.606
84.5	27.688	0.635	0.0865	0.907	0.364	0.683	0.0885	0.255	0.0974	0.0273	0.0195	0.109	0.0605	0.151	0.151	0.151	0.151	0.604
84.583	27.628	0.633	0.0862	0.904	0.363	0.68	0.0881	0.254	0.0971	0.0273	0.0194	0.109	0.0605	0.15	0.15	0.15	0.151	0.601
84.667	27.567	0.63	0.0858	0.901	0.361	0.678	0.0878	0.253	0.0967	0.0272	0.0194	0.109	0.0604	0.15	0.15	0.15	0.15	0.6
84.75	27.507	0.628	0.0855	0.898	0.36	0.675	0.0875	0.252	0.0964	0.0271	0.0194	0.109	0.0604	0.149	0.149	0.149	0.15	0.597
84.833	27.445	0.626	0.0852	0.895	0.359	0.673	0.0872	0.251	0.096	0.027	0.0193	0.108	0.0601	0.149	0.149	0.149	0.149	0.596
84.917	27.384	0.624	0.0849	0.892	0.357	0.67	0.0869	0.25	0.0956	0.0269	0.0193	0.108	0.0597	0.148	0.148	0.148	0.149	0.593
85	27.323	0.621	0.0845	0.888	0.356	0.668	0.0866	0.249	0.0953	0.0268	0.0192	0.107	0.0594	0.148	0.148	0.148	0.148	0.592
85.083	27.261	0.619	0.0842	0.885	0.355	0.665	0.0863	0.248	0.0949	0.0267	0.019	0.107	0.0586	0.147	0.147	0.147	0.148	0.589
85.167	27.199	0.617	0.0838	0.882	0.353	0.663	0.0859	0.247	0.0945	0.0265	0.0189	0.106	0.0578	0.146	0.147	0.147	0.147	0.587
85.25	27.137	0.614	0.0834	0.879	0.352	0.66	0.0856	0.246	0.0941	0.0264	0.0187	0.105	0.0571	0.146	0.146	0.146	0.147	0.585
85.333	27.074	0.612	0.083	0.875	0.35	0.657	0.0853	0.245	0.0937	0.0261	0.0184	0.104	0.0559	0.145	0.146	0.146	0.146	0.583
85.417	27.011	0.609	0.0826	0.872	0.349	0.655	0.0849	0.244	0.0933	0.0259	0.0181	0.104	0.0548	0.145	0.145	0.145	0.145	0.58
85.5	26.949	0.607	0.0822	0.869	0.347	0.652	0.0846	0.243	0.0929	0.0257	0.0179	0.103	0.0536	0.144	0.144	0.145	0.145	0.578
85.583	26.885	0.605	0.0818	0.865	0.346	0.65	0.0843	0.242	0.0925	0.0255	0.0176	0.102	0.0526	0.144	0.144	0.144	0.144	0.576
85.667	26.822	0.602	0.0813	0.862	0.344	0.647	0.0839	0.241	0.0921	0.0252	0.0173	0.101	0.0516	0.143	0.143	0.143	0.144	0.573
85.75	26.759	0.6	0.0809	0.859	0.343	0.645	0.0836	0.24	0.0917	0.025	0.0169	0.1	0.0505	0.143	0.143	0.143	0.143	0.572
85.833	26.695	0.597	0.0804	0.855	0.341	0.642	0.0832	0.239	0.0913	0.0247	0.0167	0.1	0.0498	0.142	0.142	0.142	0.143	0.569
85.917	26.631	0.594	0.0799	0.852	0.34	0.639	0.0829	0.237	0.0909	0.0243	0.0164	0.1	0.049	0.141	0.142	0.142	0.142	0.567
86	26.567	0.592	0.0794	0.848	0.338	0.637	0.0825	0.236	0.0905	0.024	0.0162	0.1	0.0482	0.141	0.141	0.141	0.142	0.565
86.083	26.503	0.589	0.0788	0.845	0.337	0.634	0.0822	0.235	0.0901	0.0238	0.0159	0.1	0.0477	0.14	0.14	0.141	0.141	0.562
86.167	26.439	0.587	0.0783	0.841	0.335	0.632	0.0818	0.234	0.0897	0.0235	0.0157	0.1	0.0472	0.14	0.14	0.14	0.14	0.56
86.25	26.374	0.584	0.0777	0.838	0.334	0.629	0.0814	0.233	0.0893	0.0232	0.0155	0.1	0.0466	0.139	0.139	0.139	0.14	0.557
86.333	26.31	0.581	0.0771	0.834	0.332	0.626	0.0811	0.232	0.0889	0.0229	0.0154	0.1	0.0462	0.139	0.139	0.139	0.139	0.556
86.417	26.245	0.579	0.0765	0.831	0.331	0.624	0.0807	0.231	0.0885	0.0227	0.0152	0.1	0.0458	0.138	0.138	0.138	0.139	0.553
86.5	26.18	0.576	0.0759	0.827	0.329	0.621	0.0803	0.229	0.0881	0.0224	0.0151	0.1	0.0454	0.137	0.138	0.138	0.138	0.551
86.583	26.115	0.573	0.0752	0.823	0.328	0.619	0.0799	0.228	0.0876	0.0222	0.015	0.1	0.0452	0.137	0.137	0.137	0.137	0.548
86.667	26.05	0.571	0.0746	0.82	0.326	0.616	0.0796	0.227	0.0872	0.022	0.0149	0.1	0.0449	0.136	0.136	0.136	0.137	0.545
86.75	25.985	0.568	0.0739	0.816	0.324	0.614	0.0792	0.226	0.0868	0.0218	0.0147	0.1	0.0446	0.136	0.136	0.136	0.136	0.544
86.833	25.919	0.565	0.0732	0.812	0.323	0.611	0.0788	0.225	0.0864	0.0216	0.0147	0.1	0.0445	0.135	0.135	0.135	0.136	0.541
86.917	25.854	0.563	0.0726	0.809	0.321	0.608	0.0784	0.223	0.086	0.0214	0.0146	0.1	0.0443	0.134	0.134	0.135	0.135	0.538
87	25.788	0.56	0.0719	0.805	0.32	0.606	0.0781	0.222	0.0856	0.0212	0.0145	0.1	0.0442	0.134	0.134	0.134	0.134	0.536
87.083	25.722	0.557	0.0713	0.801	0.318	0.603	0.0777	0.221	0.0852	0.0211	0.0144	0.1	0.0441	0.133	0.133	0.133	0.134	0.533

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
87.167	25.657	0.555	0.0707	0.798	0.317	0.601	0.0773	0.22	0.0848	0.021	0.0143	0.1	0.0441	0.132	0.133	0.133	0.133	0.531
87.25	25.591	0.552	0.0701	0.794	0.315	0.598	0.077	0.218	0.0844	0.0208	0.0143	0.1	0.044	0.132	0.132	0.132	0.132	0.528
87.333	25.525	0.549	0.0695	0.79	0.314	0.596	0.0766	0.217	0.084	0.0207	0.0142	0.1	0.044	0.131	0.131	0.131	0.132	0.525
87.417	25.459	0.547	0.069	0.786	0.312	0.593	0.0762	0.216	0.0835	0.0206	0.0142	0.1	0.044	0.131	0.131	0.131	0.131	0.524
87.5	25.393	0.544	0.0684	0.783	0.311	0.591	0.0759	0.214	0.0831	0.0205	0.0142	0.1	0.044	0.13	0.13	0.13	0.131	0.521
87.583	25.326	0.541	0.0679	0.779	0.309	0.588	0.0755	0.213	0.0827	0.0204	0.0142	0.1	0.044	0.129	0.13	0.13	0.13	0.519
87.667	25.26	0.539	0.0675	0.775	0.308	0.585	0.0751	0.212	0.0823	0.0203	0.0141	0.1	0.044	0.129	0.129	0.129	0.129	0.516
87.75	25.194	0.536	0.067	0.772	0.306	0.583	0.0748	0.21	0.0818	0.0202	0.0141	0.1	0.044	0.128	0.128	0.128	0.129	0.513
87.833	25.127	0.534	0.0665	0.768	0.305	0.58	0.0744	0.209	0.0814	0.0201	0.0141	0.1	0.0439	0.128	0.128	0.128	0.128	0.512
87.917	25.06	0.531	0.0661	0.764	0.303	0.578	0.074	0.208	0.081	0.02	0.0141	0.1	0.0438	0.127	0.127	0.127	0.127	0.508
88	24.994	0.528	0.0656	0.761	0.302	0.575	0.0737	0.206	0.0805	0.0199	0.0141	0.1	0.0437	0.126	0.126	0.127	0.127	0.506
88.083	24.927	0.526	0.0652	0.757	0.3	0.573	0.0733	0.205	0.0801	0.0198	0.014	0.1	0.0435	0.126	0.126	0.126	0.126	0.504
88.167	24.86	0.523	0.0647	0.753	0.299	0.57	0.073	0.204	0.0796	0.0197	0.014	0.1	0.0432	0.125	0.125	0.125	0.126	0.501
88.25	24.793	0.521	0.0643	0.75	0.297	0.567	0.0726	0.202	0.0792	0.0196	0.0139	0.1	0.043	0.124	0.125	0.125	0.125	0.499
88.333	24.726	0.518	0.0639	0.746	0.296	0.565	0.0722	0.201	0.0787	0.0194	0.0138	0.1	0.0426	0.124	0.124	0.124	0.124	0.496
88.417	24.659	0.515	0.0635	0.742	0.294	0.562	0.0719	0.2	0.0782	0.0193	0.0137	0.1	0.0422	0.123	0.123	0.123	0.124	0.493
88.5	24.592	0.513	0.0631	0.739	0.293	0.56	0.0715	0.198	0.0778	0.0192	0.0136	0.1	0.0418	0.123	0.123	0.123	0.123	0.492
88.583	24.525	0.51	0.0628	0.735	0.291	0.557	0.0711	0.197	0.0773	0.0191	0.0135	0.1	0.0415	0.122	0.122	0.122	0.123	0.489
88.667	24.457	0.507	0.0624	0.731	0.289	0.554	0.0708	0.196	0.0768	0.019	0.0134	0.1	0.0411	0.121	0.122	0.122	0.122	0.487
88.75	24.39	0.505	0.062	0.728	0.288	0.552	0.0704	0.194	0.0764	0.0189	0.0133	0.1	0.0408	0.121	0.121	0.121	0.121	0.484
88.833	24.323	0.502	0.0617	0.724	0.286	0.549	0.07	0.193	0.0759	0.0188	0.0132	0.1	0.0405	0.12	0.12	0.12	0.121	0.481
88.917	24.255	0.499	0.0614	0.72	0.285	0.547	0.0697	0.192	0.0755	0.0187	0.0132	0.1	0.0402	0.12	0.12	0.12	0.12	0.48
89	24.188	0.497	0.061	0.716	0.283	0.544	0.0693	0.191	0.075	0.0186	0.0131	0.1	0.04	0.119	0.119	0.119	0.119	0.476
89.083	24.12	0.494	0.0607	0.713	0.281	0.542	0.0689	0.19	0.0746	0.0185	0.013	0.1	0.0398	0.118	0.118	0.119	0.119	0.474
89.167	24.053	0.491	0.0603	0.709	0.28	0.539	0.0685	0.188	0.0741	0.0184	0.0129	0.1	0.0396	0.118	0.118	0.118	0.118	0.472
89.25	23.985	0.488	0.06	0.705	0.278	0.537	0.0682	0.187	0.0737	0.0182	0.0129	0.1	0.0394	0.117	0.117	0.117	0.118	0.469
89.333	23.918	0.486	0.0596	0.701	0.277	0.534	0.0678	0.186	0.0733	0.0182	0.0128	0.1	0.0393	0.116	0.117	0.117	0.117	0.467
89.417	23.85	0.483	0.0593	0.698	0.275	0.532	0.0674	0.185	0.0729	0.0181	0.0128	0.1	0.0392	0.116	0.116	0.116	0.116	0.464
89.5	23.782	0.48	0.0589	0.694	0.273	0.529	0.0671	0.184	0.0724	0.018	0.0127	0.1	0.039	0.115	0.115	0.115	0.116	0.461
89.583	23.714	0.478	0.0585	0.69	0.272	0.527	0.0667	0.183	0.072	0.0179	0.0127	0.1	0.0389	0.115	0.115	0.115	0.115	0.46
89.667	23.647	0.475	0.0582	0.686	0.27	0.524	0.0663	0.182	0.0716	0.0178	0.0126	0.1	0.0388	0.114	0.114	0.114	0.114	0.456
89.75	23.579	0.472	0.0578	0.682	0.269	0.522	0.0659	0.181	0.0712	0.0178	0.0126	0.1	0.0387	0.113	0.113	0.113	0.114	0.453
89.833	23.511	0.47	0.0575	0.679	0.267	0.519	0.0656	0.18	0.0708	0.0177	0.0126	0.1	0.0387	0.113	0.113	0.113	0.113	0.452
89.917	23.443	0.467	0.0571	0.675	0.266	0.517	0.0652	0.179	0.0704	0.0177	0.0125	0.1	0.0386	0.112	0.112	0.112	0.113	0.449
90	23.375	0.465	0.0568	0.671	0.264	0.514	0.0649	0.177	0.07	0.0176	0.0125	0.1	0.0386	0.111	0.112	0.112	0.112	0.447
90.083	23.307	0.462	0.0565	0.668	0.263	0.512	0.0645	0.176	0.0696	0.0175	0.0125	0.1	0.0386	0.111	0.111	0.111	0.111	0.444
90.167	23.239	0.46	0.0562	0.664	0.262	0.51	0.0642	0.175	0.0693	0.0175	0.0124	0.1	0.0385	0.11	0.11	0.11	0.111	0.441
90.25	23.172	0.457	0.0559	0.66	0.26	0.507	0.0638	0.174	0.0689	0.0174	0.0124	0.1	0.0385	0.11	0.11	0.11	0.11	0.44
90.333	23.104	0.455	0.0556	0.657	0.259	0.505	0.0635	0.173	0.0685	0.0174	0.0124	0.1	0.0385	0.109	0.109	0.109	0.11	0.437
90.417	23.036	0.452	0.0553	0.653	0.257	0.503	0.0631	0.172	0.0681	0.0174	0.0124	0.1	0.0385	0.108	0.109	0.109	0.109	0.435
90.5	22.968	0.45	0.055	0.65	0.256	0.5	0.0628	0.171	0.0678	0.0173	0.0124	0.1	0.0385	0.108	0.108	0.108	0.108	0.432
90.583	22.9	0.447	0.0548	0.646	0.255	0.498	0.0625	0.171	0.0674	0.0173	0.0124	0.1	0.0385	0.107	0.107	0.107	0.108	0.429
90.667	22.832	0.445	0.0545	0.643	0.253	0.495	0.0622	0.17	0.067	0.0173	0.0124	0.1	0.0385	0.107	0.107	0.107	0.107	0.428
90.75	22.763	0.443	0.0543	0.64	0.252	0.493	0.0618	0.169	0.0667	0.0172	0.0124	0.1	0.0385	0.106	0.106	0.106	0.107	0.425
90.833	22.695	0.44	0.0541	0.636	0.251	0.491	0.0615	0.168	0.0663	0.0172	0.0124	0.1	0.0384	0.106	0.106	0.106	0.106	0.424
90.917	22.628	0.438	0.0538	0.633	0.249	0.488	0.0612	0.167	0.0659	0.0171	0.0123	0.1	0.0384	0.105	0.105	0.105	0.106	0.421
91	22.56	0.436	0.0536	0.63	0.248	0.486	0.0609	0.166	0.0656	0.0171	0.0123	0.1	0.0383	0.105	0.105	0.105	0.105	0.42
91.083	22.492	0.434	0.0534	0.627	0.247	0.484	0.0606	0.165	0.0652	0.0171	0.0123	0.1	0.0381	0.104	0.104	0.104	0.104	0.416
91.167	22.424	0.431	0.0532	0.623	0.245	0.481	0.0602	0.164	0.0648	0.017	0.0122	0.1	0.0378	0.103	0.104	0.104	0.104	0.415
91.25	22.356	0.429	0.053	0.62	0.244	0.479	0.0599	0.163	0.0645	0.0169	0.0122	0.1	0.0376	0.103	0.103	0.103	0.103	0.412
91.333	22.288	0.427	0.0528	0.617	0.243	0.476	0.0596	0.162	0.0641	0.0169	0.0121	0.1	0.0372	0.102	0.103	0.103	0.103	0.411
91.417	22.22	0.425	0.0526	0.614	0.241	0.474	0.0593	0.162	0.0638	0.0168	0.012	0.1	0.0368	0.102	0.102	0.102	0.102	0.408
91.5	22.152	0.422	0.0524	0.611	0.24	0.471	0.059	0.161	0.0634	0.0167	0.0119	0.1	0.0364	0.101	0.102	0.102	0.102	0.407
91.583	22.084	0.42	0.0522	0.608	0.239	0.469	0.0587	0.16	0.0631	0.0166	0.0118	0.1	0.0361	0.101	0.101	0.101	0.101	0.404
91.667	22.016	0.418	0.052	0.605	0.238	0.467	0.0584	0.159	0.0627	0.0165	0.0117	0.1	0.0357	0.1	0.1	0.101	0.101	0.402
91.75	21.949	0.416	0.0518	0.601	0.236	0.464	0.0581	0.158	0.0624	0.0165	0.0116	0.1	0.0354	0.0998	0.1	0.1	0.1	0.3998
91.833	21.881	0.414	0.0516	0.598	0.235	0.462	0.0578	0.157	0.0621	0.0164	0.0115	0.1	0.0351	0.0993	0.0995	0.0995	0.0998	0.3981
91.917	21.813	0.412	0.0514	0.595	0.234	0.459	0.0575	0.157	0.0617	0.0163	0.0114	0.1	0.0348	0.0988	0.099	0.099	0.0993	0.3961
92	21.745	0.409	0.0512	0.592	0.233	0.457	0.0572	0.156	0.0614	0.0162	0.0113	0.1	0.0345	0.0983	0.0984	0.0985	0.0988	0.394
92.083	21.677	0.407	0.051	0.589	0.231	0.455	0.0569	0.155	0.0611	0.0161	0.0112	0.1	0.0343	0.0978	0.0979	0.098	0.0983	0.392
92.167	21.61	0.405	0.0508	0.586	0.23	0.452	0.0566	0.154	0.0607	0.016	0.0112	0.1	0.0342	0.0973	0.0974	0.0975	0.0978	0.39
92.25	21.542	0.403	0.0506	0.583	0.229	0.45	0.0563	0.153	0.0604	0.0159	0.0111	0.1	0.034	0.0968	0.0969	0.097	0.0973	0.388
92.333	21.475	0.401	0.0503	0.58	0.228	0.447	0.056	0.153	0.0601	0.0158	0.011	0.1	0.0338	0.0963	0.0965	0.0965	0.0968	0.3861

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
92.417	21.407	0.399	0.0501	0.577	0.227	0.445	0.0557	0.152	0.0598	0.0157	0.011	0.1	0.0337	0.0958	0.096	0.096	0.0963	0.3841
92.5	21.34	0.397	0.0499	0.574	0.225	0.443	0.0554	0.151	0.0595	0.0156	0.0109	0.1	0.0336	0.0954	0.0955	0.0955	0.0958	0.3822
92.583	21.272	0.395	0.0497	0.571	0.224	0.44	0.0551	0.15	0.0592	0.0155	0.0109	0.1	0.0335	0.0949	0.095	0.095	0.0953	0.3802
92.667	21.205	0.393	0.0494	0.568	0.223	0.438	0.0549	0.15	0.0589	0.0154	0.0109	0.1	0.0334	0.0944	0.0945	0.0945	0.0948	0.3782
92.75	21.138	0.391	0.0492	0.566	0.222	0.436	0.0546	0.149	0.0586	0.0154	0.0108	0.1	0.0333	0.0939	0.094	0.0941	0.0943	0.3763
92.833	21.07	0.389	0.0489	0.563	0.221	0.434	0.0543	0.148	0.0583	0.0153	0.0108	0.1	0.0332	0.0934	0.0935	0.0936	0.0938	0.3743
92.917	21.003	0.387	0.0487	0.56	0.22	0.431	0.054	0.147	0.058	0.0152	0.0108	0.1	0.0331	0.0929	0.0931	0.0931	0.0934	0.3725
93	20.936	0.385	0.0484	0.557	0.218	0.429	0.0537	0.147	0.0577	0.0152	0.0107	0.1	0.0331	0.0925	0.0926	0.0926	0.0929	0.3706
93.083	20.869	0.383	0.0482	0.554	0.217	0.427	0.0535	0.146	0.0574	0.0151	0.0107	0.1	0.0331	0.092	0.0921	0.0922	0.0924	0.3687
93.167	20.802	0.381	0.048	0.551	0.216	0.425	0.0532	0.145	0.0572	0.0151	0.0107	0.1	0.033	0.0915	0.0916	0.0917	0.0919	0.3667
93.25	20.735	0.379	0.0478	0.548	0.215	0.423	0.0529	0.145	0.0569	0.015	0.0107	0.1	0.033	0.0911	0.0912	0.0912	0.0915	0.365
93.333	20.668	0.377	0.0476	0.546	0.214	0.421	0.0527	0.144	0.0566	0.015	0.0106	0.1	0.033	0.0906	0.0907	0.0908	0.091	0.3631
93.417	20.601	0.375	0.0474	0.543	0.213	0.418	0.0524	0.143	0.0563	0.015	0.0106	0.1	0.033	0.0902	0.0903	0.0903	0.0906	0.3614
93.5	20.534	0.373	0.0472	0.54	0.212	0.416	0.0521	0.143	0.056	0.0149	0.0106	0.1	0.033	0.0897	0.0898	0.0899	0.0901	0.3595
93.583	20.468	0.371	0.047	0.538	0.211	0.414	0.0519	0.142	0.0558	0.0149	0.0106	0.1	0.033	0.0893	0.0894	0.0894	0.0897	0.3578
93.667	20.401	0.37	0.0468	0.535	0.21	0.412	0.0516	0.141	0.0555	0.0148	0.0106	0.1	0.033	0.0888	0.0889	0.089	0.0892	0.3559
93.75	20.335	0.368	0.0466	0.532	0.209	0.41	0.0514	0.14	0.0552	0.0148	0.0106	0.1	0.033	0.0884	0.0885	0.0886	0.0888	0.3543
93.833	20.268	0.366	0.0465	0.53	0.208	0.408	0.0511	0.14	0.055	0.0148	0.0106	0.1	0.033	0.088	0.0881	0.0881	0.0884	0.3526
93.917	20.202	0.364	0.0463	0.527	0.207	0.406	0.0509	0.139	0.0547	0.0147	0.0106	0.1	0.0329	0.0875	0.0876	0.0877	0.0879	0.3507
94	20.136	0.362	0.0461	0.525	0.206	0.404	0.0507	0.138	0.0544	0.0147	0.0106	0.1	0.0328	0.0871	0.0872	0.0873	0.0875	0.3491
94.083	20.07	0.361	0.046	0.522	0.205	0.402	0.0504	0.138	0.0541	0.0146	0.0105	0.1	0.0326	0.0867	0.0868	0.0868	0.0871	0.3474
94.167	20.003	0.359	0.0458	0.52	0.204	0.4	0.0502	0.137	0.0539	0.0146	0.0105	0.1	0.0324	0.0863	0.0864	0.0864	0.0867	0.3458
94.25	19.937	0.357	0.0456	0.517	0.203	0.397	0.0499	0.136	0.0536	0.0145	0.0104	0.1	0.0322	0.0858	0.086	0.086	0.0862	0.344
94.333	19.871	0.356	0.0454	0.515	0.202	0.395	0.0497	0.136	0.0533	0.0145	0.0103	0.1	0.0318	0.0854	0.0855	0.0856	0.0858	0.3423
94.417	19.806	0.354	0.0453	0.512	0.201	0.393	0.0494	0.135	0.053	0.0144	0.0103	0.1	0.0314	0.085	0.0851	0.0852	0.0854	0.3407
94.5	19.74	0.352	0.0451	0.51	0.2	0.391	0.0492	0.134	0.0528	0.0143	0.0102	0.1	0.0311	0.0846	0.0847	0.0848	0.085	0.3391
94.583	19.674	0.35	0.0449	0.507	0.199	0.389	0.049	0.134	0.0525	0.0142	0.0101	0.1	0.0307	0.0842	0.0843	0.0843	0.0846	0.3374
94.667	19.609	0.349	0.0447	0.505	0.198	0.387	0.0487	0.133	0.0522	0.0141	0.00996	0.1	0.0303	0.0838	0.0839	0.0839	0.0842	0.3358
94.75	19.543	0.347	0.0445	0.502	0.197	0.385	0.0485	0.133	0.0519	0.0141	0.00986	0.1	0.03	0.0834	0.0835	0.0835	0.0838	0.3342
94.833	19.478	0.345	0.0444	0.5	0.196	0.383	0.0482	0.132	0.0517	0.014	0.00976	0.1	0.0297	0.083	0.0831	0.0831	0.0833	0.3325
94.917	19.413	0.343	0.0442	0.497	0.195	0.381	0.048	0.131	0.0514	0.0139	0.00967	0.1	0.0294	0.0826	0.0827	0.0827	0.0829	0.3309
95	19.348	0.342	0.044	0.495	0.194	0.379	0.0478	0.131	0.0511	0.0138	0.00958	0.1	0.0291	0.0822	0.0823	0.0823	0.0825	0.3293
95.083	19.283	0.34	0.0438	0.493	0.193	0.377	0.0475	0.13	0.0509	0.0137	0.0095	0.1	0.0289	0.0818	0.0819	0.0819	0.0821	0.3277
95.167	19.218	0.338	0.0436	0.49	0.192	0.375	0.0473	0.13	0.0506	0.0136	0.00943	0.1	0.0287	0.0814	0.0815	0.0815	0.0817	0.3261
95.25	19.154	0.337	0.0434	0.488	0.191	0.373	0.047	0.129	0.0504	0.0135	0.00936	0.1	0.0285	0.081	0.0811	0.0811	0.0813	0.3245
95.333	19.089	0.335	0.0432	0.485	0.19	0.371	0.0468	0.128	0.0501	0.0134	0.0093	0.1	0.0284	0.0806	0.0807	0.0807	0.0809	0.3229
95.417	19.024	0.333	0.0429	0.483	0.189	0.369	0.0466	0.128	0.0499	0.0133	0.00925	0.1	0.0282	0.0802	0.0803	0.0803	0.0805	0.3213
95.5	18.96	0.331	0.0427	0.481	0.188	0.367	0.0463	0.127	0.0496	0.0132	0.00919	0.1	0.0281	0.0798	0.0799	0.0799	0.0801	0.3197
95.583	18.896	0.33	0.0425	0.478	0.187	0.365	0.0461	0.127	0.0494	0.0131	0.00915	0.1	0.028	0.0794	0.0795	0.0795	0.0797	0.3181
95.667	18.832	0.328	0.0422	0.476	0.186	0.363	0.0458	0.126	0.0492	0.013	0.00911	0.1	0.0279	0.079	0.0791	0.0791	0.0793	0.3165
95.75	18.768	0.326	0.042	0.473	0.185	0.362	0.0456	0.126	0.0489	0.013	0.00907	0.1	0.0278	0.0786	0.0787	0.0787	0.0789	0.3149
95.833	18.704	0.325	0.0418	0.471	0.184	0.36	0.0454	0.125	0.0487	0.0129	0.00904	0.1	0.0277	0.0782	0.0783	0.0783	0.0785	0.3133
95.917	18.64	0.323	0.0415	0.469	0.183	0.358	0.0451	0.124	0.0485	0.0128	0.009	0.1	0.0277	0.0778	0.0779	0.0779	0.0781	0.3117
96	18.577	0.321	0.0413	0.466	0.182	0.356	0.0449	0.124	0.0482	0.0128	0.00897	0.1	0.0276	0.0774	0.0775	0.0775	0.0777	0.3101
96.083	18.513	0.32	0.041	0.464	0.181	0.354	0.0447	0.123	0.048	0.0127	0.00895	0.1	0.0276	0.077	0.0771	0.0771	0.0774	0.3086
96.167	18.45	0.318	0.0408	0.462	0.181	0.352	0.0445	0.123	0.0478	0.0127	0.00892	0.1	0.0275	0.0766	0.0767	0.0768	0.077	0.3071
96.25	18.387	0.316	0.0406	0.459	0.18	0.35	0.0442	0.122	0.0475	0.0126	0.0089	0.1	0.0275	0.0762	0.0763	0.0764	0.0766	0.3055
96.333	18.324	0.315	0.0404	0.457	0.179	0.349	0.044	0.122	0.0473	0.0126	0.00889	0.1	0.0275	0.0759	0.0759	0.076	0.0762	0.304
96.417	18.261	0.313	0.0402	0.455	0.178	0.347	0.0438	0.121	0.0471	0.0125	0.00887	0.1	0.0275	0.0755	0.0756	0.0756	0.0758	0.3025
96.5	18.198	0.312	0.04	0.452	0.177	0.345	0.0436	0.121	0.0469	0.0125	0.00885	0.1	0.0275	0.0751	0.0752	0.0752	0.0754	0.3009
96.583	18.136	0.31	0.0398	0.45	0.176	0.343	0.0434	0.12	0.0467	0.0125	0.00885	0.1	0.0275	0.0747	0.0748	0.0749	0.0751	0.2995
96.667	18.073	0.309	0.0396	0.448	0.175	0.342	0.0431	0.12	0.0464	0.0124	0.00884	0.1	0.0275	0.0744	0.0744	0.0745	0.0747	0.298
96.75	18.011	0.307	0.0394	0.446	0.174	0.34	0.0429	0.119	0.0462	0.0124	0.00884	0.1	0.0275	0.074	0.0741	0.0741	0.0743	0.2965
96.833	17.949	0.306	0.0393	0.444	0.174	0.338	0.0427	0.119	0.046	0.0124	0.00884	0.1	0.0275	0.0736	0.0737	0.0738	0.074	0.2951
96.917	17.887	0.304	0.0391	0.441	0.173	0.336	0.0425	0.118	0.0458	0.0123	0.00884	0.1	0.0275	0.0733	0.0734	0.0734	0.0736	0.2937
97	17.825	0.303	0.039	0.439	0.172	0.335	0.0423	0.117	0.0456	0.0123	0.00883	0.1	0.0275	0.0729	0.073	0.073	0.0732	0.2921
97.083	17.764	0.301	0.0388	0.437	0.171	0.333	0.0421	0.117	0.0453	0.0123	0.00883	0.1	0.0275	0.0725	0.0726	0.0727	0.0729	0.2907
97.167	17.703	0.3	0.0387	0.435	0.17	0.331	0.0419	0.116	0.0451	0.0123	0.00883	0.1	0.0275	0.0722	0.0723	0.0723	0.0725	0.2893
97.25	17.641	0.298	0.0385	0.433	0.17	0.33	0.0417	0.116	0.0449	0.0122	0.00883	0.1	0.0275	0.0718	0.0719	0.072	0.0722	0.2879
97.333	17.58	0.297	0.0384	0.431	0.169	0.328	0.0415	0.115	0.0447	0.0122	0.00883	0.1	0.0275	0.0715	0.0716	0.0716	0.0718	0.2865
97.417	17.519	0.296	0.0383	0.429	0.168	0.326	0.0413	0.115	0.0445	0.0122	0.00883	0.1	0.0275	0.0712	0.0712	0.0713	0.0715	0.2852
97.5	17.458	0.294	0.0382	0.427	0.167	0.324	0.0411	0.114	0.0443	0.0122	0.00883	0.1	0.0275	0.0708	0.0709	0.0709	0.0711	0.2837
97.583	17.398	0.293	0.0381	0.425	0.166	0.323	0.0409	0.114	0.0441	0.0122	0.00883	0.1	0.0275	0.0705	0.0706	0.0706	0.0708	0.2825

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
97.667	17.338	0.291	0.038	0.423	0.166	0.321	0.0407	0.113	0.0439	0.0122	0.00883	0.1	0.0275	0.0701	0.0702	0.0703	0.0705	0.2811
97.75	17.277	0.29	0.0379	0.421	0.165	0.32	0.0405	0.113	0.0437	0.0121	0.00883	0.1	0.0275	0.0698	0.0699	0.0699	0.0701	0.2797
97.833	17.217	0.289	0.0378	0.419	0.164	0.318	0.0403	0.113	0.0435	0.0121	0.00883	0.1	0.0275	0.0695	0.0696	0.0696	0.0698	0.2785
97.917	17.157	0.287	0.0377	0.417	0.163	0.316	0.0402	0.112	0.0433	0.0121	0.00883	0.1	0.0275	0.0691	0.0692	0.0693	0.0695	0.2771
98	17.097	0.286	0.0376	0.415	0.163	0.315	0.04	0.112	0.0431	0.0121	0.00883	0.1	0.0275	0.0688	0.0689	0.0689	0.0691	0.2757
98.083	17.038	0.285	0.0376	0.413	0.162	0.313	0.0398	0.111	0.0429	0.0121	0.00883	0.1	0.0275	0.0685	0.0686	0.0686	0.0688	0.2745
98.167	16.979	0.283	0.0375	0.411	0.161	0.312	0.0396	0.111	0.0428	0.0121	0.00883	0.1	0.0275	0.0682	0.0683	0.0683	0.0685	0.2733
98.25	16.919	0.282	0.0374	0.409	0.16	0.31	0.0394	0.11	0.0426	0.0121	0.00883	0.1	0.0275	0.0679	0.0679	0.068	0.0682	0.272
98.333	16.861	0.281	0.0373	0.407	0.16	0.309	0.0392	0.11	0.0424	0.0121	0.00883	0.1	0.0275	0.0675	0.0676	0.0677	0.0678	0.2706
98.417	16.802	0.28	0.0373	0.405	0.159	0.307	0.0391	0.11	0.0423	0.0121	0.00883	0.1	0.0275	0.0672	0.0673	0.0673	0.0675	0.2693
98.5	16.743	0.278	0.0372	0.403	0.158	0.306	0.0389	0.109	0.0421	0.0121	0.00883	0.1	0.0275	0.0669	0.067	0.067	0.0672	0.2681
98.583	16.685	0.277	0.0371	0.401	0.158	0.304	0.0387	0.109	0.042	0.0121	0.00883	0.1	0.0275	0.0666	0.0667	0.0667	0.0669	0.2669
98.667	16.627	0.276	0.0371	0.399	0.157	0.303	0.0385	0.109	0.0418	0.0121	0.00883	0.1	0.0275	0.0663	0.0664	0.0664	0.0666	0.2657
98.75	16.568	0.275	0.037	0.398	0.156	0.301	0.0383	0.108	0.0417	0.0121	0.00883	0.1	0.0275	0.066	0.0661	0.0661	0.0663	0.2645
98.833	16.511	0.273	0.037	0.396	0.156	0.3	0.0382	0.108	0.0415	0.0121	0.00883	0.1	0.0275	0.0657	0.0658	0.0658	0.066	0.2633
98.917	16.453	0.272	0.0369	0.394	0.155	0.298	0.038	0.108	0.0414	0.0121	0.00883	0.1	0.0275	0.0654	0.0655	0.0655	0.0657	0.2621
99	16.395	0.271	0.0369	0.392	0.154	0.297	0.0378	0.107	0.0412	0.0121	0.00883	0.1	0.0275	0.0651	0.0652	0.0652	0.0654	0.2609
99.083	16.338	0.27	0.0368	0.39	0.154	0.296	0.0377	0.107	0.0411	0.0121	0.00883	0.1	0.0275	0.0648	0.0649	0.0649	0.0651	0.2597
99.167	16.281	0.269	0.0368	0.389	0.153	0.294	0.0375	0.107	0.041	0.0121	0.00883	0.1	0.0275	0.0645	0.0646	0.0646	0.0648	0.2585
99.25	16.224	0.268	0.0367	0.387	0.153	0.293	0.0374	0.107	0.0408	0.0121	0.00883	0.1	0.0275	0.0642	0.0643	0.0643	0.0645	0.2573
99.333	16.167	0.267	0.0367	0.385	0.152	0.292	0.0372	0.106	0.0407	0.0121	0.00883	0.1	0.0275	0.064	0.064	0.0641	0.0642	0.2563
99.417	16.111	0.266	0.0366	0.384	0.152	0.29	0.0371	0.106	0.0406	0.0121	0.00883	0.1	0.0275	0.0637	0.0638	0.0638	0.064	0.2553
99.5	16.054	0.265	0.0366	0.382	0.151	0.289	0.0369	0.106	0.0405	0.0121	0.00883	0.1	0.0275	0.0634	0.0635	0.0635	0.0637	0.2541
99.583	15.998	0.264	0.0366	0.38	0.15	0.288	0.0368	0.106	0.0404	0.0121	0.00883	0.1	0.0275	0.0631	0.0632	0.0633	0.0634	0.253
99.667	15.942	0.263	0.0365	0.379	0.15	0.287	0.0366	0.105	0.0402	0.0121	0.00883	0.1	0.0275	0.0629	0.063	0.063	0.0632	0.2521
99.75	15.886	0.262	0.0365	0.377	0.149	0.285	0.0365	0.105	0.0401	0.0121	0.00883	0.1	0.0275	0.0626	0.0627	0.0627	0.0629	0.2509
99.833	15.831	0.261	0.0365	0.376	0.149	0.284	0.0364	0.105	0.04	0.0121	0.00883	0.1	0.0275	0.0624	0.0625	0.0625	0.0627	0.2501
99.917	15.775	0.26	0.0364	0.374	0.149	0.283	0.0362	0.105	0.0399	0.0121	0.00883	0.1	0.0275	0.0621	0.0622	0.0623	0.0624	0.249
100	15.72	0.259	0.0364	0.373	0.148	0.282	0.0361	0.104	0.0398	0.0121	0.00883	0.1	0.0275	0.0619	0.062	0.062	0.0622	0.2481
100.083	15.665	0.258	0.0364	0.372	0.148	0.281	0.036	0.104	0.0397	0.0121	0.00883	0.1	0.0275	0.0617	0.0618	0.0618	0.0619	0.2472
100.167	15.61	0.257	0.0364	0.37	0.147	0.279	0.0358	0.104	0.0396	0.0121	0.00883	0.1	0.0275	0.0614	0.0615	0.0616	0.0617	0.2462
100.25	15.555	0.256	0.0363	0.369	0.147	0.278	0.0357	0.104	0.0395	0.0121	0.00883	0.1	0.0275	0.0612	0.0613	0.0613	0.0615	0.2453
100.333	15.501	0.255	0.0363	0.367	0.146	0.277	0.0356	0.104	0.0394	0.0121	0.00883	0.1	0.0275	0.061	0.0611	0.0611	0.0613	0.2445
100.417	15.446	0.255	0.0363	0.366	0.146	0.276	0.0355	0.103	0.0393	0.0121	0.00883	0.1	0.0275	0.0608	0.0608	0.0609	0.061	0.2435
100.5	15.392	0.254	0.0363	0.365	0.146	0.275	0.0354	0.103	0.0392	0.0121	0.00883	0.1	0.0275	0.0606	0.0606	0.0607	0.0608	0.2427
100.583	15.338	0.253	0.0363	0.364	0.145	0.274	0.0353	0.103	0.0391	0.0121	0.00883	0.1	0.0275	0.0603	0.0604	0.0605	0.0606	0.2418
100.667	15.285	0.252	0.0363	0.362	0.145	0.273	0.0352	0.103	0.039	0.0121	0.00883	0.1	0.0275	0.0601	0.0602	0.0602	0.0604	0.2409
100.75	15.231	0.252	0.0362	0.361	0.144	0.271	0.035	0.103	0.0389	0.0121	0.00883	0.1	0.0275	0.0599	0.06	0.06	0.0602	0.2401
100.833	15.178	0.251	0.0362	0.36	0.144	0.27	0.0349	0.103	0.0388	0.0121	0.00883	0.1	0.0275	0.0597	0.0598	0.0598	0.06	0.2393
100.917	15.125	0.25	0.0362	0.359	0.144	0.269	0.0348	0.103	0.0387	0.0121	0.00883	0.1	0.0275	0.0595	0.0596	0.0596	0.0598	0.2385
101	15.072	0.249	0.0362	0.357	0.143	0.268	0.0347	0.102	0.0386	0.0121	0.00883	0.1	0.0275	0.0593	0.0594	0.0595	0.0596	0.2378
101.083	15.019	0.249	0.0362	0.356	0.143	0.267	0.0346	0.102	0.0386	0.0121	0.00883	0.1	0.0275	0.0592	0.0592	0.0593	0.0594	0.2371
101.167	14.966	0.248	0.0362	0.355	0.143	0.266	0.0346	0.102	0.0385	0.0121	0.00883	0.1	0.0275	0.059	0.0591	0.0591	0.0592	0.2364
101.25	14.914	0.247	0.0362	0.354	0.142	0.265	0.0345	0.102	0.0384	0.0121	0.00883	0.1	0.0275	0.0588	0.0589	0.0589	0.0591	0.2357
101.333	14.862	0.247	0.0362	0.353	0.142	0.264	0.0344	0.102	0.0383	0.0121	0.00883	0.1	0.0275	0.0586	0.0587	0.0587	0.0589	0.2349
101.417	14.809	0.246	0.0362	0.352	0.142	0.263	0.0343	0.102	0.0383	0.0121	0.00883	0.1	0.0275	0.0585	0.0585	0.0586	0.0587	0.2343
101.5	14.757	0.246	0.0362	0.351	0.141	0.262	0.0342	0.102	0.0382	0.0121	0.00883	0.1	0.0275	0.0583	0.0584	0.0584	0.0585	0.2336
101.583	14.706	0.245	0.0362	0.35	0.141	0.261	0.0341	0.101	0.0381	0.0121	0.00883	0.1	0.0275	0.0581	0.0582	0.0582	0.0584	0.2329
101.667	14.654	0.245	0.0362	0.349	0.141	0.261	0.034	0.101	0.0381	0.0121	0.00883	0.1	0.0275	0.058	0.058	0.0581	0.0582	0.2323
101.75	14.603	0.244	0.0362	0.348	0.14	0.26	0.034	0.101	0.038	0.0121	0.00883	0.1	0.0275	0.0578	0.0579	0.0579	0.058	0.2316
101.833	14.552	0.243	0.0362	0.347	0.14	0.259	0.0339	0.101	0.038	0.0121	0.00883	0.1	0.0275	0.0576	0.0577	0.0577	0.0579	0.2309
101.917	14.501	0.243	0.0362	0.346	0.14	0.258	0.0338	0.101	0.0379	0.0121	0.00883	0.1	0.0275	0.0575	0.0576	0.0576	0.0577	0.2304
102	14.45	0.242	0.0362	0.345	0.14	0.257	0.0337	0.101	0.0378	0.0121	0.00883	0.1	0.0275	0.0573	0.0574	0.0574	0.0576	0.2297
102.083	14.399	0.242	0.0362	0.344	0.139	0.256	0.0337	0.101	0.0378	0.0121	0.00883	0.1	0.0275	0.0572	0.0573	0.0573	0.0574	0.2292
102.167	14.349	0.241	0.0362	0.343	0.139	0.256	0.0336	0.101	0.0377	0.0121	0.00883	0.1	0.0275	0.057	0.0571	0.0571	0.0573	0.2285
102.25	14.298	0.241	0.0362	0.343	0.139	0.255	0.0335	0.101	0.0377	0.0121	0.00883	0.1	0.0275	0.0569	0.057	0.057	0.0572	0.2281
102.333	14.248	0.24	0.0362	0.342	0.139	0.254	0.0334	0.101	0.0376	0.0121	0.00883	0.1	0.0275	0.0568	0.0568	0.0569	0.057	0.2275
102.417	14.198	0.24	0.0362	0.341	0.138	0.253	0.0334	0.101	0.0376	0.0121	0.00883	0.1	0.0275	0.0566	0.0567	0.0567	0.0569	0.2269
102.5	14.149	0.239	0.0362	0.34	0.138	0.253	0.0333	0.1	0.0375	0.0121	0.00883	0.1	0.0275	0.0565	0.0566	0.0566	0.0568	0.2265
102.583	14.099	0.239	0.0362	0.339	0.138	0.252	0.0332	0.1	0.0375	0.0121	0.00883	0.1	0.0275	0.0564	0.0564	0.0565	0.0566	0.2259
102.667	14.05	0.239	0.0362	0.339	0.138	0.251	0.0332	0.1	0.0374	0.0121	0.00883	0.1	0.0275	0.0563	0.0563	0.0564	0.0565	0.2255
102.75	14	0.238	0.0362	0.338	0.137	0.251	0.0331	0.1	0.0374	0.0121	0.00883	0.1	0.0275	0.0561	0.0562	0.0562	0.0564	0.2249
102.833	13.951	0.238	0.0362	0.337	0.137	0.25	0.0331	0.1	0.0373	0.0121	0.00882	0.1	0.0275	0.056	0.0561	0.0561	0.0563	0.2245

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
102.917	13.902	0.237	0.0362	0.337	0.137	0.249	0.033	0.1	0.0373	0.0121	0.00881	0.1	0.0274	0.0559	0.056	0.056	0.0562	0.2241
103	13.853	0.237	0.0362	0.336	0.137	0.249	0.0329	0.1	0.0372	0.0121	0.0088	0.1	0.0274	0.0558	0.0559	0.0559	0.056	0.2236
103.083	13.805	0.236	0.0362	0.335	0.137	0.248	0.0329	0.1	0.0372	0.0121	0.00877	0.1	0.0272	0.0557	0.0558	0.0558	0.0559	0.2232
103.167	13.757	0.236	0.0362	0.334	0.136	0.247	0.0328	0.0999	0.0371	0.012	0.00873	0.1	0.027	0.0556	0.0556	0.0557	0.0558	0.2227
103.25	13.708	0.236	0.0361	0.334	0.136	0.247	0.0327	0.0998	0.0371	0.012	0.00869	0.1	0.0269	0.0555	0.0555	0.0556	0.0557	0.2223
103.333	13.66	0.235	0.0361	0.333	0.136	0.246	0.0327	0.0997	0.037	0.012	0.00862	0.1	0.0265	0.0553	0.0554	0.0554	0.0556	0.2217
103.417	13.613	0.235	0.036	0.332	0.136	0.245	0.0326	0.0996	0.037	0.0119	0.00855	0.1	0.0262	0.0552	0.0553	0.0553	0.0555	0.2213
103.5	13.565	0.234	0.036	0.332	0.136	0.245	0.0326	0.0995	0.0369	0.0119	0.00848	0.1	0.0259	0.0551	0.0552	0.0552	0.0554	0.2209
103.583	13.518	0.234	0.0359	0.331	0.135	0.244	0.0325	0.0994	0.0369	0.0118	0.00838	0.1	0.0255	0.055	0.0551	0.0551	0.0553	0.2205
103.667	13.47	0.234	0.0358	0.33	0.135	0.243	0.0325	0.0992	0.0368	0.0117	0.00829	0.1	0.0252	0.0549	0.055	0.055	0.0552	0.2201
103.75	13.423	0.233	0.0358	0.33	0.135	0.243	0.0324	0.0991	0.0368	0.0117	0.00819	0.1	0.0248	0.0548	0.0549	0.0549	0.055	0.2196
103.833	13.376	0.233	0.0357	0.329	0.135	0.242	0.0323	0.099	0.0367	0.0116	0.00809	0.1	0.0245	0.0547	0.0548	0.0548	0.0549	0.2192
103.917	13.329	0.232	0.0356	0.328	0.134	0.242	0.0323	0.0988	0.0366	0.0115	0.00799	0.1	0.0242	0.0546	0.0546	0.0547	0.0548	0.2187
104	13.282	0.232	0.0355	0.328	0.134	0.241	0.0322	0.0987	0.0366	0.0114	0.00789	0.1	0.0239	0.0545	0.0545	0.0546	0.0547	0.2183
104.083	13.236	0.231	0.0353	0.327	0.134	0.24	0.0321	0.0985	0.0365	0.0113	0.00781	0.1	0.0236	0.0544	0.0544	0.0545	0.0546	0.2179
104.167	13.189	0.231	0.0352	0.327	0.134	0.24	0.0321	0.0984	0.0365	0.0112	0.00773	0.1	0.0234	0.0542	0.0543	0.0543	0.0545	0.2173
104.25	13.143	0.231	0.0351	0.326	0.133	0.239	0.032	0.0982	0.0364	0.0111	0.00765	0.1	0.0232	0.0541	0.0542	0.0542	0.0544	0.2169
104.333	13.097	0.23	0.0349	0.325	0.133	0.239	0.032	0.098	0.0363	0.011	0.00759	0.1	0.023	0.054	0.0541	0.0541	0.0543	0.2165
104.417	13.051	0.23	0.0348	0.325	0.133	0.238	0.0319	0.0978	0.0363	0.0109	0.00753	0.1	0.0229	0.0539	0.054	0.054	0.0542	0.2161
104.5	13.006	0.229	0.0347	0.324	0.133	0.237	0.0318	0.0976	0.0362	0.0108	0.00747	0.1	0.0227	0.0538	0.0539	0.0539	0.054	0.2156
104.583	12.96	0.229	0.0345	0.323	0.132	0.237	0.0318	0.0974	0.0361	0.0108	0.00743	0.1	0.0226	0.0537	0.0538	0.0538	0.0539	0.2152
104.667	12.915	0.228	0.0343	0.322	0.132	0.236	0.0317	0.0972	0.0361	0.0107	0.00738	0.1	0.0225	0.0536	0.0536	0.0537	0.0538	0.2147
104.75	12.87	0.228	0.0341	0.322	0.132	0.236	0.0316	0.097	0.036	0.0106	0.00734	0.1	0.0224	0.0535	0.0535	0.0536	0.0537	0.2143
104.833	12.825	0.227	0.034	0.321	0.132	0.235	0.0316	0.0968	0.0359	0.0105	0.0073	0.1	0.0223	0.0534	0.0534	0.0534	0.0536	0.2138
104.917	12.78	0.227	0.0338	0.32	0.131	0.235	0.0315	0.0966	0.0358	0.0105	0.00727	0.1	0.0222	0.0532	0.0533	0.0533	0.0535	0.2133
105	12.735	0.226	0.0336	0.32	0.131	0.234	0.0314	0.0963	0.0358	0.0104	0.00723	0.1	0.0221	0.0531	0.0532	0.0532	0.0534	0.2129
105.083	12.69	0.226	0.0334	0.319	0.131	0.234	0.0314	0.0961	0.0357	0.0104	0.00721	0.1	0.0221	0.053	0.0531	0.0531	0.0532	0.2124
105.167	12.646	0.226	0.0332	0.318	0.131	0.233	0.0313	0.0958	0.0356	0.0103	0.00718	0.1	0.0221	0.0529	0.053	0.053	0.0531	0.212
105.25	12.602	0.225	0.033	0.318	0.13	0.233	0.0312	0.0956	0.0355	0.0103	0.00715	0.1	0.022	0.0528	0.0528	0.0529	0.053	0.2115
105.333	12.558	0.225	0.0329	0.317	0.13	0.232	0.0312	0.0953	0.0355	0.0102	0.00714	0.1	0.022	0.0527	0.0527	0.0528	0.0529	0.2111
105.417	12.514	0.224	0.0327	0.316	0.13	0.232	0.0311	0.095	0.0354	0.0102	0.00712	0.1	0.022	0.0525	0.0526	0.0526	0.0528	0.2105
105.5	12.47	0.224	0.0325	0.316	0.129	0.231	0.031	0.0948	0.0353	0.0101	0.0071	0.1	0.022	0.0524	0.0525	0.0525	0.0527	0.2101
105.583	12.426	0.223	0.0324	0.315	0.129	0.23	0.031	0.0944	0.0352	0.0101	0.00709	0.1	0.022	0.0523	0.0524	0.0524	0.0525	0.2096
105.667	12.383	0.223	0.0322	0.314	0.129	0.23	0.0309	0.0941	0.0351	0.01	0.00708	0.1	0.022	0.0522	0.0523	0.0523	0.0524	0.2092
105.75	12.34	0.222	0.0321	0.313	0.129	0.229	0.0308	0.0938	0.035	0.01	0.00707	0.1	0.022	0.0521	0.0521	0.0522	0.0523	0.2087
105.833	12.297	0.221	0.032	0.313	0.128	0.229	0.0308	0.0935	0.0349	0.00998	0.00707	0.1	0.022	0.052	0.052	0.0521	0.0522	0.2083
105.917	12.254	0.221	0.0318	0.312	0.128	0.228	0.0307	0.0932	0.0349	0.00995	0.00707	0.1	0.022	0.0518	0.0519	0.0519	0.0521	0.2077
106	12.211	0.22	0.0317	0.311	0.128	0.228	0.0306	0.0929	0.0348	0.00992	0.00707	0.1	0.022	0.0517	0.0518	0.0518	0.052	0.2073
106.083	12.168	0.22	0.0316	0.311	0.127	0.227	0.0305	0.0925	0.0347	0.00989	0.00707	0.1	0.022	0.0516	0.0517	0.0517	0.0518	0.2068
106.167	12.126	0.219	0.0314	0.31	0.127	0.227	0.0305	0.0922	0.0346	0.00986	0.00707	0.1	0.022	0.0515	0.0515	0.0516	0.0517	0.2063
106.25	12.083	0.219	0.0313	0.309	0.127	0.226	0.0304	0.0919	0.0345	0.00984	0.00707	0.1	0.022	0.0514	0.0514	0.0515	0.0516	0.2059
106.333	12.041	0.218	0.0312	0.308	0.126	0.226	0.0303	0.0915	0.0344	0.00982	0.00707	0.1	0.022	0.0512	0.0513	0.0513	0.0515	0.2053
106.417	11.999	0.218	0.0311	0.308	0.126	0.225	0.0302	0.0912	0.0343	0.0098	0.00707	0.1	0.022	0.0511	0.0512	0.0512	0.0513	0.2048
106.5	11.957	0.217	0.031	0.307	0.126	0.225	0.0302	0.0909	0.0342	0.00978	0.00707	0.1	0.022	0.051	0.0511	0.0511	0.0512	0.2044
106.583	11.915	0.217	0.0309	0.306	0.125	0.224	0.0301	0.0906	0.0341	0.00976	0.00707	0.1	0.022	0.0509	0.0509	0.051	0.0511	0.2039
106.667	11.874	0.216	0.0308	0.305	0.125	0.224	0.03	0.0903	0.034	0.00975	0.00707	0.1	0.022	0.0507	0.0508	0.0508	0.051	0.2033
106.75	11.832	0.216	0.0307	0.305	0.125	0.223	0.0299	0.09	0.0339	0.00973	0.00707	0.1	0.022	0.0506	0.0507	0.0507	0.0508	0.2028
106.833	11.791	0.215	0.0306	0.304	0.124	0.223	0.0299	0.0897	0.0338	0.00972	0.00707	0.1	0.022	0.0505	0.0505	0.0506	0.0507	0.2023
106.917	11.75	0.214	0.0305	0.303	0.124	0.223	0.0298	0.0894	0.0337	0.00972	0.00707	0.1	0.022	0.0504	0.0504	0.0504	0.0506	0.2018
107	11.709	0.214	0.0304	0.302	0.124	0.222	0.0297	0.0891	0.0336	0.00971	0.00707	0.1	0.022	0.0502	0.0503	0.0503	0.0505	0.2013
107.083	11.668	0.213	0.0304	0.302	0.123	0.222	0.0296	0.0889	0.0335	0.0097	0.00707	0.1	0.022	0.0501	0.0502	0.0502	0.0503	0.2008
107.167	11.627	0.213	0.0303	0.301	0.123	0.221	0.0295	0.0886	0.0334	0.0097	0.00707	0.1	0.022	0.05	0.05	0.0501	0.0502	0.2003
107.25	11.587	0.212	0.0302	0.3	0.123	0.221	0.0295	0.0883	0.0333	0.00969	0.00707	0.1	0.022	0.0498	0.0499	0.0499	0.0501	0.1997
107.333	11.546	0.211	0.0302	0.299	0.122	0.22	0.0294	0.0881	0.0332	0.00969	0.00707	0.1	0.022	0.0497	0.0498	0.0498	0.0499	0.1992
107.417	11.506	0.211	0.0301	0.298	0.122	0.22	0.0293	0.0878	0.0331	0.00969	0.00707	0.1	0.022	0.0496	0.0496	0.0497	0.0498	0.1987
107.5	11.466	0.21	0.03	0.298	0.121	0.219	0.0292	0.0876	0.033	0.00969	0.00707	0.1	0.022	0.0494	0.0495	0.0495	0.0497	0.1981
107.583	11.426	0.21	0.03	0.297	0.121	0.219	0.0291	0.0873	0.0329	0.00969	0.00707	0.1	0.022	0.0493	0.0494	0.0494	0.0495	0.1976
107.667	11.386	0.209	0.0299	0.296	0.121	0.218	0.0291	0.0871	0.0328	0.00969	0.00707	0.1	0.022	0.0492	0.0492	0.0493	0.0494	0.1971
107.75	11.346	0.209	0.0298	0.295	0.12	0.218	0.029	0.0868	0.0327	0.00969	0.00707	0.1	0.022	0.049	0.0491	0.0491	0.0492	0.1964
107.833	11.307	0.208	0.0298	0.294	0.12	0.217	0.0289	0.0866	0.0326	0.00969	0.00707	0.1	0.022	0.0489	0.049	0.049	0.0491	0.196
107.917	11.267	0.207	0.0297	0.294	0.12	0.217	0.0288	0.0864	0.0325	0.00969	0.00707	0.1	0.022	0.0488	0.0488	0.0488	0.049	0.1954
108	11.228	0.207	0.0297	0.293	0.119	0.216	0.0287	0.0862	0.0325	0.00969	0.00707	0.1	0.022	0.0486	0.0487	0.0487	0.0488	0.1948
108.083	11.189	0.206	0.0296	0.292	0.119	0.216	0.0287	0.086	0.0324	0.00969	0.00707	0.1	0.022	0.0485	0.0485	0.0486	0.0487	0.1943

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
108.167	11.15	0.206	0.0296	0.291	0.119	0.215	0.0286	0.0858	0.0323	0.00969	0.00707	0.1	0.022	0.0484	0.0484	0.0484	0.0486	0.1938
108.25	11.111	0.205	0.0295	0.29	0.119	0.215	0.0285	0.0856	0.0322	0.00969	0.00707	0.1	0.022	0.0482	0.0483	0.0483	0.0484	0.1932
108.333	11.073	0.205	0.0295	0.289	0.118	0.214	0.0284	0.0854	0.0322	0.00969	0.00707	0.1	0.022	0.0481	0.0481	0.0482	0.0483	0.1927
108.417	11.034	0.204	0.0294	0.289	0.118	0.214	0.0284	0.0852	0.0321	0.00969	0.00707	0.1	0.022	0.048	0.048	0.048	0.0482	0.1922
108.5	10.996	0.204	0.0294	0.288	0.118	0.214	0.0283	0.085	0.032	0.00969	0.00707	0.1	0.022	0.0478	0.0479	0.0479	0.048	0.1916
108.583	10.958	0.203	0.0293	0.287	0.117	0.213	0.0282	0.0848	0.0319	0.00969	0.00707	0.1	0.022	0.0477	0.0478	0.0478	0.0479	0.1912
108.667	10.92	0.203	0.0293	0.286	0.117	0.213	0.0281	0.0846	0.0319	0.00969	0.00707	0.1	0.022	0.0476	0.0476	0.0477	0.0478	0.1907
108.75	10.881	0.202	0.0293	0.286	0.117	0.212	0.0281	0.0845	0.0318	0.00969	0.00707	0.1	0.022	0.0475	0.0475	0.0475	0.0477	0.1902
108.833	10.844	0.202	0.0292	0.285	0.117	0.212	0.028	0.0843	0.0317	0.00969	0.00707	0.1	0.022	0.0473	0.0474	0.0474	0.0476	0.1897
108.917	10.806	0.201	0.0292	0.284	0.116	0.211	0.0279	0.0842	0.0316	0.00969	0.00707	0.1	0.022	0.0472	0.0473	0.0473	0.0474	0.1892
109	10.768	0.201	0.0292	0.284	0.116	0.211	0.0279	0.084	0.0316	0.00969	0.00707	0.1	0.022	0.0471	0.0472	0.0472	0.0473	0.1888
109.083	10.731	0.2	0.0292	0.283	0.116	0.21	0.0278	0.0839	0.0315	0.00969	0.00707	0.1	0.022	0.047	0.0471	0.0471	0.0472	0.1884
109.167	10.694	0.2	0.0291	0.282	0.116	0.21	0.0277	0.0837	0.0314	0.00969	0.00707	0.1	0.022	0.0469	0.047	0.047	0.0471	0.188
109.25	10.656	0.199	0.0291	0.282	0.115	0.209	0.0277	0.0836	0.0314	0.00969	0.00707	0.1	0.022	0.0468	0.0468	0.0469	0.047	0.1875
109.333	10.62	0.199	0.0291	0.281	0.115	0.209	0.0276	0.0834	0.0313	0.00969	0.00707	0.1	0.022	0.0467	0.0467	0.0468	0.0469	0.1871
109.417	10.583	0.198	0.0291	0.28	0.115	0.208	0.0276	0.0833	0.0313	0.00969	0.00707	0.1	0.022	0.0466	0.0466	0.0467	0.0468	0.1867
109.5	10.546	0.198	0.029	0.28	0.115	0.208	0.0275	0.0832	0.0312	0.00969	0.00707	0.1	0.022	0.0465	0.0465	0.0465	0.0467	0.1862
109.583	10.51	0.198	0.029	0.279	0.114	0.207	0.0274	0.083	0.0311	0.00969	0.00707	0.1	0.022	0.0464	0.0464	0.0464	0.0466	0.1858
109.667	10.473	0.197	0.029	0.278	0.114	0.207	0.0274	0.0829	0.0311	0.00969	0.00707	0.1	0.022	0.0463	0.0463	0.0463	0.0465	0.1854
109.75	10.437	0.197	0.029	0.278	0.114	0.207	0.0273	0.0828	0.031	0.00969	0.00707	0.1	0.022	0.0462	0.0462	0.0462	0.0464	0.185
109.833	10.401	0.196	0.029	0.277	0.114	0.206	0.0273	0.0827	0.031	0.00969	0.00707	0.1	0.022	0.0461	0.0461	0.0461	0.0463	0.1846
109.917	10.364	0.196	0.029	0.277	0.114	0.206	0.0272	0.0825	0.0309	0.00969	0.00707	0.1	0.022	0.046	0.046	0.046	0.0462	0.1842
110	10.328	0.196	0.029	0.276	0.113	0.205	0.0272	0.0824	0.0309	0.00969	0.00707	0.1	0.022	0.0459	0.0459	0.0459	0.0461	0.1838
110.083	10.293	0.195	0.029	0.276	0.113	0.205	0.0271	0.0823	0.0308	0.00969	0.00707	0.1	0.022	0.0458	0.0458	0.0459	0.046	0.1835
110.167	10.257	0.195	0.029	0.275	0.113	0.204	0.0271	0.0822	0.0308	0.00969	0.00707	0.1	0.022	0.0457	0.0457	0.0458	0.0459	0.1831
110.25	10.221	0.195	0.029	0.274	0.113	0.204	0.027	0.0821	0.0307	0.00969	0.00707	0.1	0.022	0.0456	0.0456	0.0457	0.0458	0.1827
110.333	10.186	0.194	0.029	0.274	0.113	0.203	0.027	0.082	0.0307	0.00969	0.00707	0.1	0.022	0.0455	0.0456	0.0456	0.0457	0.1824
110.417	10.151	0.194	0.029	0.273	0.112	0.203	0.0269	0.0819	0.0306	0.00969	0.00707	0.1	0.022	0.0454	0.0455	0.0455	0.0456	0.182
110.5	10.116	0.194	0.029	0.273	0.112	0.202	0.0269	0.0818	0.0306	0.00969	0.00707	0.1	0.022	0.0453	0.0454	0.0454	0.0455	0.1816
110.583	10.081	0.193	0.029	0.272	0.112	0.202	0.0268	0.0817	0.0305	0.00969	0.00707	0.1	0.022	0.0452	0.0453	0.0453	0.0454	0.1812
110.667	10.046	0.193	0.029	0.272	0.112	0.202	0.0268	0.0816	0.0305	0.00969	0.00707	0.1	0.022	0.0452	0.0452	0.0452	0.0454	0.181
110.75	10.011	0.193	0.029	0.271	0.112	0.201	0.0267	0.0815	0.0305	0.00969	0.00707	0.1	0.022	0.0451	0.0451	0.0452	0.0453	0.1807
110.833	9.976	0.192	0.029	0.271	0.111	0.201	0.0267	0.0814	0.0304	0.00969	0.00707	0.1	0.022	0.045	0.0451	0.0451	0.0452	0.1804
110.917	9.942	0.192	0.029	0.27	0.111	0.2	0.0266	0.0813	0.0304	0.00969	0.00707	0.1	0.022	0.0449	0.045	0.045	0.0451	0.18
111	9.907	0.192	0.029	0.27	0.111	0.2	0.0266	0.0812	0.0303	0.00969	0.00707	0.1	0.022	0.0448	0.0449	0.0449	0.045	0.1796
111.083	9.873	0.191	0.029	0.269	0.111	0.2	0.0266	0.0811	0.0303	0.00969	0.00707	0.1	0.022	0.0448	0.0448	0.0448	0.045	0.1794
111.167	9.839	0.191	0.029	0.269	0.111	0.199	0.0265	0.081	0.0303	0.00969	0.00707	0.1	0.022	0.0447	0.0447	0.0448	0.0449	0.1791
111.25	9.805	0.191	0.029	0.268	0.111	0.199	0.0265	0.0809	0.0302	0.00969	0.00707	0.1	0.022	0.0446	0.0447	0.0447	0.0448	0.1788
111.333	9.771	0.191	0.029	0.268	0.111	0.198	0.0264	0.0808	0.0302	0.00969	0.00707	0.1	0.022	0.0445	0.0446	0.0446	0.0447	0.1784
111.417	9.738	0.19	0.029	0.268	0.11	0.198	0.0264	0.0808	0.0302	0.00969	0.00707	0.1	0.022	0.0445	0.0445	0.0446	0.0447	0.1783
111.5	9.704	0.19	0.029	0.267	0.11	0.198	0.0264	0.0807	0.0301	0.00969	0.00707	0.1	0.022	0.0444	0.0445	0.0445	0.0446	0.178
111.583	9.67	0.19	0.029	0.267	0.11	0.197	0.0263	0.0806	0.0301	0.00969	0.00707	0.1	0.022	0.0443	0.0444	0.0444	0.0445	0.1776
111.667	9.637	0.19	0.029	0.266	0.11	0.197	0.0263	0.0805	0.03	0.00969	0.00707	0.1	0.022	0.0443	0.0443	0.0444	0.0445	0.1775
111.75	9.604	0.189	0.029	0.266	0.11	0.197	0.0263	0.0805	0.03	0.00969	0.00707	0.1	0.022	0.0442	0.0443	0.0443	0.0444	0.1772
111.833	9.571	0.189	0.029	0.266	0.11	0.196	0.0262	0.0804	0.03	0.00969	0.00706	0.1	0.022	0.0442	0.0442	0.0442	0.0444	0.177
111.917	9.538	0.189	0.029	0.265	0.11	0.196	0.0262	0.0803	0.0299	0.00968	0.00706	0.1	0.022	0.0441	0.0441	0.0442	0.0443	0.1767
112	9.505	0.189	0.029	0.265	0.109	0.196	0.0262	0.0803	0.0299	0.00968	0.00705	0.1	0.0219	0.044	0.0441	0.0441	0.0442	0.1764
112.083	9.472	0.188	0.029	0.265	0.109	0.195	0.0261	0.0802	0.0299	0.00966	0.00702	0.1	0.0218	0.044	0.044	0.044	0.0442	0.1762
112.167	9.44	0.188	0.0289	0.264	0.109	0.195	0.0261	0.0801	0.0298	0.00964	0.007	0.1	0.0217	0.0439	0.044	0.044	0.0441	0.176
112.25	9.407	0.188	0.0289	0.264	0.109	0.195	0.0261	0.08	0.0298	0.00963	0.00697	0.1	0.0216	0.0438	0.0439	0.0439	0.044	0.1756
112.333	9.375	0.188	0.0289	0.263	0.109	0.194	0.026	0.0799	0.0298	0.00959	0.00691	0.1	0.0213	0.0438	0.0438	0.0439	0.044	0.1755
112.417	9.342	0.187	0.0288	0.263	0.109	0.194	0.026	0.0798	0.0297	0.00955	0.00685	0.1	0.021	0.0437	0.0438	0.0438	0.0439	0.1752
112.5	9.31	0.187	0.0288	0.263	0.109	0.194	0.026	0.0797	0.0297	0.00951	0.00679	0.1	0.0207	0.0437	0.0437	0.0437	0.0439	0.175
112.583	9.278	0.187	0.0287	0.262	0.108	0.193	0.0259	0.0796	0.0296	0.00945	0.0067	0.1	0.0204	0.0436	0.0436	0.0437	0.0438	0.1747
112.667	9.246	0.187	0.0287	0.262	0.108	0.193	0.0259	0.0795	0.0296	0.00939	0.00661	0.1	0.02	0.0435	0.0436	0.0436	0.0437	0.1744
112.75	9.214	0.186	0.0286	0.261	0.108	0.192	0.0258	0.0794	0.0295	0.00933	0.00652	0.1	0.0196	0.0435	0.0435	0.0435	0.0437	0.1742
112.833	9.183	0.186	0.0285	0.261	0.108	0.192	0.0258	0.0792	0.0295	0.00924	0.00641	0.1	0.0193	0.0434	0.0434	0.0435	0.0436	0.1739
112.917	9.151	0.186	0.0284	0.261	0.108	0.192	0.0258	0.0791	0.0294	0.00916	0.00631	0.1	0.0189	0.0433	0.0434	0.0434	0.0435	0.1736
113	9.12	0.185	0.0283	0.26	0.108	0.191	0.0257	0.0789	0.0294	0.00908	0.00621	0.1	0.0186	0.0433	0.0433	0.0433	0.0434	0.1733
113.083	9.089	0.185	0.0282	0.26	0.107	0.191	0.0257	0.0788	0.0293	0.00898	0.00612	0.1	0.0184	0.0432	0.0432	0.0433	0.0434	0.1731
113.167	9.057	0.185	0.0281	0.259	0.107	0.191	0.0256	0.0786	0.0293	0.00889	0.00604	0.1	0.0181	0.0431	0.0432	0.0432	0.0433	0.1728
113.25	9.026	0.184	0.028	0.259	0.107	0.19	0.0256	0.0785	0.0292	0.00879	0.00595	0.1	0.0179	0.043	0.0431	0.0431	0.0432	0.1724
113.333	8.995	0.184	0.0278	0.259	0.107	0.19	0.0255	0.0783	0.0291	0.00869	0.00589	0.1	0.0177	0.043	0.043	0.043	0.0432	0.1722

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
113.417	8.965	0.184	0.0277	0.258	0.107	0.19	0.0255	0.0781	0.0291	0.0086	0.00582	0.1	0.0175	0.0429	0.0429	0.043	0.0431	0.1719
113.5	8.934	0.183	0.0275	0.258	0.106	0.189	0.0254	0.0779	0.029	0.0085	0.00575	0.1	0.0173	0.0428	0.0429	0.0429	0.043	0.1716
113.583	8.903	0.183	0.0274	0.257	0.106	0.189	0.0254	0.0777	0.0289	0.00842	0.0057	0.1	0.0172	0.0427	0.0428	0.0428	0.0429	0.1712
113.667	8.873	0.183	0.0272	0.257	0.106	0.188	0.0253	0.0775	0.0289	0.00834	0.00566	0.1	0.0171	0.0427	0.0427	0.0427	0.0429	0.171
113.75	8.842	0.182	0.0271	0.256	0.106	0.188	0.0253	0.0773	0.0288	0.00826	0.00561	0.1	0.017	0.0426	0.0426	0.0427	0.0428	0.1707
113.833	8.812	0.182	0.0269	0.256	0.105	0.188	0.0252	0.0771	0.0287	0.00819	0.00557	0.1	0.0169	0.0425	0.0426	0.0426	0.0427	0.1704
113.917	8.782	0.181	0.0267	0.255	0.105	0.187	0.0252	0.0769	0.0287	0.00812	0.00553	0.1	0.0168	0.0424	0.0425	0.0425	0.0426	0.17
114	8.752	0.181	0.0265	0.255	0.105	0.187	0.0251	0.0767	0.0286	0.00805	0.0055	0.1	0.0167	0.0423	0.0424	0.0424	0.0425	0.1696
114.083	8.722	0.181	0.0263	0.254	0.105	0.187	0.0251	0.0764	0.0285	0.00799	0.00547	0.1	0.0166	0.0422	0.0423	0.0423	0.0424	0.1692
114.167	8.692	0.18	0.0261	0.254	0.104	0.186	0.025	0.0762	0.0285	0.00793	0.00544	0.1	0.0166	0.0422	0.0422	0.0422	0.0424	0.169
114.25	8.662	0.18	0.026	0.253	0.104	0.186	0.025	0.0759	0.0284	0.00787	0.00541	0.1	0.0165	0.0421	0.0421	0.0421	0.0423	0.1686
114.333	8.633	0.179	0.0258	0.253	0.104	0.185	0.0249	0.0757	0.0283	0.00783	0.00539	0.1	0.0165	0.042	0.042	0.0421	0.0422	0.1683
114.417	8.603	0.179	0.0256	0.252	0.104	0.185	0.0248	0.0754	0.0282	0.00778	0.00537	0.1	0.0165	0.0419	0.0419	0.042	0.0421	0.1679
114.5	8.574	0.179	0.0254	0.251	0.103	0.185	0.0248	0.0751	0.0281	0.00773	0.00535	0.1	0.0165	0.0418	0.0419	0.0419	0.042	0.1676
114.583	8.545	0.178	0.0253	0.251	0.103	0.184	0.0247	0.0748	0.028	0.0077	0.00534	0.1	0.0165	0.0417	0.0418	0.0418	0.0419	0.1672
114.667	8.515	0.178	0.0251	0.25	0.103	0.184	0.0247	0.0745	0.028	0.00766	0.00532	0.1	0.0165	0.0416	0.0417	0.0417	0.0418	0.1668
114.75	8.486	0.177	0.025	0.25	0.103	0.183	0.0246	0.0742	0.0279	0.00762	0.00531	0.1	0.0165	0.0415	0.0416	0.0416	0.0417	0.1664
114.833	8.457	0.177	0.0248	0.249	0.102	0.183	0.0245	0.0739	0.0278	0.00758	0.00531	0.1	0.0165	0.0414	0.0415	0.0415	0.0416	0.166
114.917	8.428	0.176	0.0247	0.249	0.102	0.183	0.0245	0.0736	0.0277	0.00755	0.0053	0.1	0.0165	0.0413	0.0414	0.0414	0.0415	0.1656
115	8.4	0.176	0.0246	0.248	0.102	0.182	0.0244	0.0733	0.0276	0.00752	0.0053	0.1	0.0165	0.0412	0.0413	0.0413	0.0414	0.1652
115.083	8.371	0.175	0.0244	0.247	0.101	0.182	0.0244	0.0729	0.0275	0.00749	0.0053	0.1	0.0165	0.0411	0.0412	0.0412	0.0413	0.1648
115.167	8.343	0.175	0.0243	0.247	0.101	0.181	0.0243	0.0726	0.0274	0.00746	0.0053	0.1	0.0165	0.041	0.0411	0.0411	0.0412	0.1644
115.25	8.314	0.174	0.0242	0.246	0.101	0.181	0.0242	0.0723	0.0273	0.00744	0.0053	0.1	0.0165	0.0409	0.041	0.041	0.0411	0.164
115.333	8.286	0.174	0.0241	0.246	0.1	0.181	0.0242	0.072	0.0272	0.00742	0.0053	0.1	0.0165	0.0408	0.0408	0.0409	0.041	0.1635
115.417	8.258	0.173	0.0239	0.245	0.1	0.18	0.0241	0.0716	0.0271	0.00739	0.0053	0.1	0.0165	0.0407	0.0407	0.0408	0.0409	0.1631
115.5	8.23	0.173	0.0238	0.244	0.0999	0.18	0.024	0.0713	0.027	0.00737	0.0053	0.1	0.0165	0.0406	0.0406	0.0407	0.0408	0.1627
115.583	8.202	0.172	0.0237	0.244	0.0995	0.179	0.024	0.071	0.0269	0.00735	0.0053	0.1	0.0165	0.0405	0.0405	0.0405	0.0407	0.1622
115.667	8.174	0.172	0.0236	0.243	0.0992	0.179	0.0239	0.0707	0.0268	0.00734	0.0053	0.1	0.0165	0.0404	0.0404	0.0404	0.0405	0.1617
115.75	8.146	0.171	0.0235	0.242	0.0989	0.179	0.0238	0.0704	0.0267	0.00732	0.0053	0.1	0.0165	0.0403	0.0403	0.0403	0.0404	0.1613
115.833	8.118	0.171	0.0234	0.242	0.0985	0.178	0.0237	0.0701	0.0266	0.00731	0.0053	0.1	0.0165	0.0401	0.0402	0.0402	0.0403	0.1608
115.917	8.091	0.17	0.0234	0.241	0.0982	0.178	0.0237	0.0698	0.0265	0.0073	0.0053	0.1	0.0165	0.04	0.0401	0.0401	0.0402	0.1604
116	8.063	0.17	0.0233	0.24	0.0978	0.177	0.0236	0.0695	0.0264	0.00729	0.0053	0.1	0.0165	0.0399	0.04	0.04	0.0401	0.16
116.083	8.036	0.169	0.0232	0.239	0.0975	0.177	0.0235	0.0692	0.0263	0.00728	0.0053	0.1	0.0165	0.0398	0.0398	0.0399	0.04	0.1595
116.167	8.009	0.169	0.0231	0.239	0.0971	0.176	0.0234	0.069	0.0262	0.00728	0.0053	0.1	0.0165	0.0397	0.0397	0.0397	0.0398	0.1589
116.25	7.981	0.168	0.023	0.238	0.0967	0.176	0.0234	0.0687	0.0261	0.00727	0.0053	0.1	0.0165	0.0395	0.0396	0.0396	0.0397	0.1584
116.333	7.954	0.167	0.023	0.237	0.0964	0.176	0.0233	0.0684	0.026	0.00727	0.0053	0.1	0.0165	0.0394	0.0395	0.0395	0.0396	0.158
116.417	7.927	0.167	0.0229	0.237	0.096	0.175	0.0232	0.0682	0.0259	0.00727	0.0053	0.1	0.0165	0.0393	0.0394	0.0394	0.0395	0.1576
116.5	7.9	0.166	0.0228	0.236	0.0956	0.175	0.0231	0.0679	0.0258	0.00727	0.0053	0.1	0.0165	0.0392	0.0392	0.0393	0.0394	0.1571
116.583	7.874	0.166	0.0228	0.235	0.0953	0.174	0.023	0.0677	0.0257	0.00727	0.0053	0.1	0.0165	0.0391	0.0391	0.0391	0.0392	0.1565
116.667	7.847	0.165	0.0227	0.234	0.095	0.174	0.023	0.0674	0.0256	0.00727	0.0053	0.1	0.0165	0.0389	0.039	0.039	0.0391	0.156
116.75	7.821	0.164	0.0226	0.234	0.0946	0.173	0.0229	0.0672	0.0255	0.00727	0.0053	0.1	0.0165	0.0388	0.0388	0.0389	0.039	0.1555
116.833	7.794	0.164	0.0226	0.233	0.0943	0.173	0.0228	0.067	0.0255	0.00727	0.0053	0.1	0.0165	0.0387	0.0387	0.0387	0.0388	0.1549
116.917	7.768	0.163	0.0225	0.232	0.0939	0.172	0.0227	0.0667	0.0254	0.00727	0.0053	0.1	0.0165	0.0385	0.0386	0.0386	0.0387	0.1544
117	7.742	0.163	0.0225	0.231	0.0936	0.172	0.0226	0.0665	0.0253	0.00727	0.0053	0.1	0.0165	0.0384	0.0385	0.0385	0.0386	0.154
117.083	7.715	0.162	0.0224	0.23	0.0933	0.172	0.0226	0.0663	0.0252	0.00727	0.0053	0.1	0.0165	0.0383	0.0383	0.0383	0.0385	0.1534
117.167	7.689	0.162	0.0224	0.23	0.093	0.171	0.0225	0.0661	0.0251	0.00727	0.0053	0.1	0.0165	0.0382	0.0382	0.0382	0.0383	0.1529
117.25	7.663	0.161	0.0223	0.229	0.0927	0.171	0.0224	0.0659	0.0251	0.00727	0.0053	0.1	0.0165	0.038	0.0381	0.0381	0.0382	0.1524
117.333	7.638	0.16	0.0223	0.228	0.0924	0.17	0.0223	0.0657	0.025	0.00727	0.0053	0.1	0.0165	0.0379	0.0379	0.038	0.0381	0.1519
117.417	7.612	0.16	0.0222	0.227	0.0921	0.17	0.0222	0.0655	0.0249	0.00727	0.0053	0.1	0.0165	0.0378	0.0378	0.0378	0.0379	0.1513
117.5	7.586	0.159	0.0222	0.227	0.0918	0.169	0.0222	0.0653	0.0248	0.00727	0.0053	0.1	0.0165	0.0376	0.0377	0.0377	0.0378	0.1508
117.583	7.561	0.159	0.0221	0.226	0.0915	0.169	0.0221	0.0651	0.0248	0.00727	0.0053	0.1	0.0165	0.0375	0.0376	0.0376	0.0377	0.1504
117.667	7.535	0.158	0.0221	0.225	0.0912	0.168	0.022	0.0649	0.0247	0.00727	0.0053	0.1	0.0165	0.0374	0.0374	0.0375	0.0376	0.1499
117.75	7.51	0.158	0.0221	0.224	0.0909	0.168	0.022	0.0647	0.0246	0.00727	0.0053	0.1	0.0165	0.0373	0.0373	0.0373	0.0374	0.1493
117.833	7.484	0.157	0.022	0.224	0.0907	0.168	0.0219	0.0646	0.0245	0.00727	0.0053	0.1	0.0165	0.0372	0.0372	0.0372	0.0373	0.1489
117.917	7.459	0.157	0.022	0.223	0.0904	0.167	0.0218	0.0644	0.0245	0.00727	0.0053	0.1	0.0165	0.037	0.0371	0.0371	0.0372	0.1484
118	7.434	0.156	0.022	0.222	0.0901	0.167	0.0218	0.0643	0.0244	0.00726	0.0053	0.1	0.0165	0.0369	0.037	0.037	0.0371	0.148
118.083	7.409	0.156	0.0219	0.222	0.0899	0.166	0.0217	0.0641	0.0243	0.00725	0.00527	0.1	0.0164	0.0368	0.0369	0.0369	0.037	0.1476
118.167	7.384	0.155	0.0219	0.221	0.0896	0.166	0.0216	0.0639	0.0243	0.00724	0.00525	0.1	0.0163	0.0367	0.0367	0.0368	0.0369	0.1471
118.25	7.359	0.155	0.0218	0.22	0.0893	0.165	0.0216	0.0638	0.0242	0.00722	0.00523	0.1	0.0162	0.0366	0.0366	0.0366	0.0367	0.1465
118.333	7.335	0.155	0.0218	0.22	0.0891	0.165	0.0215	0.0636	0.0241	0.00719	0.00518	0.1	0.016	0.0365	0.0365	0.0365	0.0366	0.1461
118.417	7.31	0.154	0.0217	0.219	0.0888	0.164	0.0214	0.0634	0.024	0.00715	0.00513	0.1	0.0157	0.0363	0.0364	0.0364	0.0365	0.1456
118.5	7.285	0.154	0.0217	0.218	0.0885	0.164	0.0213	0.0632	0.024	0.00712	0.00507	0.1	0.0155	0.0362	0.0363	0.0363	0.0364	0.1452
118.583	7.261	0.153	0.0216	0.217	0.0883	0.163	0.0213	0.063	0.0239	0.00706	0.00499	0.1	0.0151	0.0361	0.0362	0.0362	0.0363	0.1448

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
118.667	7.237	0.153	0.0215	0.217	0.088	0.163	0.0212	0.0628	0.0238	0.00701	0.0049	0.1	0.0147	0.036	0.036	0.0361	0.0362	0.1443
118.75	7.212	0.152	0.0214	0.216	0.0877	0.162	0.0211	0.0626	0.0237	0.00695	0.00481	0.1	0.0143	0.0359	0.0359	0.0359	0.036	0.1437
118.833	7.188	0.152	0.0213	0.215	0.0875	0.162	0.0211	0.0624	0.0237	0.00687	0.00471	0.1	0.014	0.0358	0.0358	0.0358	0.0359	0.1433
118.917	7.164	0.151	0.0212	0.215	0.0872	0.161	0.021	0.0622	0.0236	0.00679	0.0046	0.1	0.0136	0.0356	0.0357	0.0357	0.0358	0.1428
119	7.14	0.151	0.0211	0.214	0.0869	0.16	0.0209	0.0619	0.0235	0.00672	0.0045	0.1	0.0133	0.0355	0.0356	0.0356	0.0357	0.1424
119.083	7.116	0.15	0.021	0.213	0.0866	0.16	0.0209	0.0617	0.0234	0.00662	0.00441	0.1	0.013	0.0354	0.0355	0.0355	0.0356	0.142
119.167	7.093	0.15	0.0209	0.212	0.0863	0.159	0.0208	0.0615	0.0233	0.00652	0.00432	0.1	0.0127	0.0353	0.0353	0.0354	0.0354	0.1414
119.25	7.069	0.149	0.0208	0.212	0.086	0.159	0.0207	0.0612	0.0233	0.00643	0.00423	0.1	0.0125	0.0352	0.0352	0.0352	0.0353	0.1409
119.333	7.045	0.149	0.0207	0.211	0.0858	0.158	0.0207	0.061	0.0232	0.00633	0.00416	0.1	0.0123	0.0351	0.0351	0.0351	0.0352	0.1405
119.417	7.022	0.148	0.0205	0.21	0.0855	0.158	0.0206	0.0607	0.0231	0.00623	0.00409	0.1	0.0121	0.0349	0.035	0.035	0.0351	0.14
119.5	6.998	0.148	0.0204	0.21	0.0852	0.157	0.0205	0.0604	0.023	0.00613	0.00402	0.1	0.0119	0.0348	0.0349	0.0349	0.035	0.1396
119.583	6.975	0.147	0.0202	0.209	0.0849	0.157	0.0205	0.0602	0.0229	0.00605	0.00397	0.1	0.0118	0.0347	0.0347	0.0348	0.0348	0.139
119.667	6.952	0.147	0.0201	0.208	0.0846	0.156	0.0204	0.0599	0.0228	0.00596	0.00392	0.1	0.0116	0.0346	0.0346	0.0346	0.0347	0.1385
119.75	6.929	0.146	0.0199	0.207	0.0843	0.156	0.0203	0.0596	0.0228	0.00588	0.00386	0.1	0.0115	0.0345	0.0345	0.0345	0.0346	0.1381
119.833	6.905	0.146	0.0197	0.207	0.084	0.155	0.0202	0.0593	0.0227	0.0058	0.00383	0.1	0.0114	0.0343	0.0344	0.0344	0.0345	0.1376
119.917	6.882	0.145	0.0196	0.206	0.0836	0.155	0.0202	0.059	0.0226	0.00573	0.00379	0.1	0.0113	0.0342	0.0343	0.0343	0.0344	0.1372
120	6.859	0.145	0.0194	0.205	0.0833	0.154	0.0201	0.0587	0.0225	0.00566	0.00375	0.1	0.0112	0.0341	0.0341	0.0342	0.0342	0.1366
120.083	6.837	0.144	0.0192	0.204	0.083	0.154	0.02	0.0584	0.0224	0.0056	0.00372	0.1	0.0112	0.034	0.034	0.034	0.0341	0.1361
120.167	6.814	0.144	0.019	0.204	0.0827	0.153	0.0199	0.058	0.0223	0.00554	0.00369	0.1	0.0111	0.0338	0.0339	0.0339	0.034	0.1356
120.25	6.791	0.143	0.0188	0.203	0.0824	0.153	0.0199	0.0577	0.0222	0.00548	0.00365	0.1	0.0111	0.0337	0.0338	0.0338	0.0339	0.1352
120.333	6.769	0.142	0.0186	0.202	0.082	0.152	0.0198	0.0574	0.0221	0.00543	0.00363	0.1	0.011	0.0336	0.0336	0.0337	0.0338	0.1347
120.417	6.746	0.142	0.0185	0.201	0.0817	0.151	0.0197	0.057	0.022	0.00538	0.00361	0.1	0.011	0.0335	0.0335	0.0335	0.0336	0.1341
120.5	6.724	0.141	0.0183	0.201	0.0814	0.151	0.0197	0.0567	0.0219	0.00534	0.00359	0.1	0.011	0.0334	0.0334	0.0334	0.0335	0.1337
120.583	6.702	0.141	0.0181	0.2	0.0811	0.15	0.0196	0.0563	0.0218	0.0053	0.00358	0.1	0.011	0.0332	0.0333	0.0333	0.0334	0.1332
120.667	6.679	0.14	0.018	0.199	0.0807	0.15	0.0195	0.0559	0.0217	0.00526	0.00356	0.1	0.011	0.0331	0.0331	0.0332	0.0333	0.1327
120.75	6.657	0.14	0.0178	0.198	0.0804	0.149	0.0194	0.0556	0.0216	0.00522	0.00355	0.1	0.011	0.033	0.033	0.033	0.0331	0.1321
120.833	6.635	0.139	0.0177	0.198	0.08	0.149	0.0194	0.0552	0.0215	0.00518	0.00354	0.1	0.011	0.0329	0.0329	0.0329	0.033	0.1317
120.917	6.613	0.139	0.0175	0.197	0.0797	0.148	0.0193	0.0548	0.0214	0.00515	0.00354	0.1	0.011	0.0327	0.0328	0.0328	0.0329	0.1312
121	6.591	0.138	0.0174	0.196	0.0793	0.148	0.0192	0.0544	0.0213	0.00511	0.00353	0.1	0.011	0.0326	0.0326	0.0327	0.0328	0.1307
121.083	6.569	0.137	0.0172	0.195	0.079	0.147	0.0191	0.054	0.0211	0.00506	0.0035	0.1	0.0109	0.0325	0.0325	0.0325	0.0326	0.1301
121.167	6.547	0.137	0.0171	0.195	0.0786	0.147	0.019	0.0536	0.021	0.00501	0.00346	0.1	0.0107	0.0323	0.0324	0.0324	0.0325	0.1296
121.25	6.526	0.136	0.0169	0.194	0.0782	0.146	0.019	0.0532	0.0209	0.00496	0.00343	0.1	0.0105	0.0322	0.0323	0.0323	0.0324	0.1292
121.333	6.504	0.136	0.0167	0.193	0.0778	0.146	0.0189	0.0527	0.0208	0.00487	0.00333	0.1	0.0101	0.0321	0.0321	0.0321	0.0322	0.1285
121.417	6.482	0.135	0.0165	0.192	0.0773	0.145	0.0188	0.0522	0.0206	0.00478	0.00323	0.1	0.00961	0.0319	0.032	0.032	0.0321	0.128
121.5	6.46	0.134	0.0164	0.191	0.0769	0.144	0.0187	0.0518	0.0205	0.00469	0.00313	0.1	0.00914	0.0318	0.0318	0.0318	0.0319	0.1273
121.583	6.438	0.133	0.0161	0.19	0.0764	0.144	0.0186	0.0513	0.0203	0.00457	0.00296	0.1	0.00838	0.0316	0.0317	0.0317	0.0318	0.1268
121.667	6.417	0.133	0.0159	0.189	0.0759	0.143	0.0185	0.0508	0.0202	0.00444	0.00279	0.1	0.00761	0.0315	0.0315	0.0315	0.0316	0.1261
121.75	6.395	0.132	0.0157	0.188	0.0755	0.143	0.0184	0.0503	0.02	0.00431	0.00262	0.1	0.00685	0.0313	0.0313	0.0314	0.0314	0.1254
121.833	6.373	0.131	0.0154	0.187	0.0749	0.142	0.0183	0.0498	0.0198	0.00415	0.00241	0.1	0.00612	0.0311	0.0312	0.0312	0.0313	0.1248
121.917	6.351	0.13	0.0152	0.186	0.0744	0.141	0.0182	0.0492	0.0197	0.00399	0.0022	0.1	0.00539	0.031	0.031	0.031	0.0311	0.1241
122	6.33	0.129	0.0149	0.185	0.0739	0.141	0.0181	0.0487	0.0195	0.00383	0.00198	0.1	0.00466	0.0308	0.0308	0.0309	0.0309	0.1234
122.083	6.308	0.129	0.0146	0.184	0.0733	0.14	0.0179	0.0482	0.0193	0.00363	0.0018	0.1	0.00412	0.0306	0.0307	0.0307	0.0308	0.1228
122.167	6.286	0.128	0.0143	0.183	0.0727	0.139	0.0178	0.0476	0.0191	0.00343	0.00162	0.1	0.00357	0.0304	0.0305	0.0305	0.0306	0.122
122.25	6.265	0.127	0.014	0.182	0.0721	0.139	0.0177	0.0471	0.0189	0.00323	0.00143	0.1	0.00303	0.0302	0.0303	0.0303	0.0304	0.1212
122.333	6.243	0.126	0.0137	0.181	0.0715	0.138	0.0176	0.0465	0.0188	0.00303	0.00129	0.1	0.00265	0.0301	0.0301	0.0301	0.0302	0.1205
122.417	6.222	0.125	0.0134	0.18	0.0709	0.137	0.0174	0.0459	0.0186	0.00283	0.00114	0.1	0.00228	0.0299	0.0299	0.0299	0.03	0.1197
122.5	6.2	0.124	0.013	0.179	0.0703	0.136	0.0173	0.0453	0.0184	0.00263	0.000999	0.1	0.0019	0.0297	0.0297	0.0297	0.0298	0.1189
122.583	6.179	0.123	0.0127	0.177	0.0696	0.136	0.0172	0.0447	0.0182	0.00245	0.000895	0.1	0.00162	0.0294	0.0295	0.0295	0.0296	0.118
122.667	6.157	0.122	0.0123	0.176	0.069	0.135	0.017	0.0441	0.018	0.00228	0.00079	0.1	0.00134	0.0292	0.0293	0.0293	0.0294	0.1172
122.75	6.136	0.121	0.0119	0.175	0.0683	0.134	0.0169	0.0435	0.0178	0.0021	0.000686	0.1	0.00106	0.029	0.0291	0.0291	0.0292	0.1164
122.833	6.114	0.12	0.0115	0.173	0.0677	0.133	0.0167	0.0428	0.0176	0.00196	0.000606	0.1	0.000861	0.0288	0.0288	0.0288	0.0289	0.1153
122.917	6.093	0.118	0.0111	0.172	0.067	0.133	0.0166	0.0421	0.0174	0.00181	0.000527	0.1	0.000663	0.0286	0.0286	0.0286	0.0287	0.1145
123	6.072	0.117	0.0106	0.171	0.0663	0.132	0.0164	0.0415	0.0172	0.00167	0.000447	0.1	0.000466	0.0283	0.0284	0.0284	0.0285	0.1136
123.083	6.05	0.116	0.0102	0.169	0.0656	0.131	0.0163	0.0408	0.017	0.00154	0.000383	0.1	0.000347	0.0281	0.0281	0.0282	0.0282	0.1126
123.167	6.029	0.115	0.00977	0.168	0.0649	0.13	0.0161	0.0401	0.0168	0.00142	0.000318	0.1	0.000227	0.0279	0.0279	0.0279	0.028	0.1117
123.25	6.007	0.114	0.00934	0.166	0.0642	0.129	0.016	0.0394	0.0165	0.0013	0.000253	0.1	0.000108	0.0276	0.0277	0.0277	0.0277	0.1107
123.333	5.986	0.113	0.00895	0.165	0.0635	0.129	0.0158	0.0387	0.0163	0.0012	0.000209	0.1	0.0000717	0.0274	0.0274	0.0274	0.0275	0.1097
123.417	5.965	0.112	0.00855	0.163	0.0628	0.128	0.0156	0.038	0.0161	0.0011	0.000164	0.1	0.0000359	0.0271	0.0272	0.0272	0.0272	0.1087
123.5	5.944	0.111	0.00816	0.162	0.062	0.127	0.0155	0.0373	0.0159	0.001	0.000119	0.1	0	0.0269	0.0269	0.0269	0.027	0.1077
123.583	5.922	0.109	0.0078	0.16	0.0613	0.126	0.0153	0.0365	0.0157	0.000923	0.0000895	0.1	0	0.0266	0.0267	0.0267	0.0267	0.1067
123.667	5.901	0.108	0.00744	0.159	0.0606	0.125	0.0152	0.0358	0.0154	0.000843	0.0000596	0.1	0	0.0264	0.0264	0.0264	0.0265	0.1057
123.75	5.88	0.107	0.00707	0.157	0.0598	0.124	0.015	0.035	0.0152	0.000763	0.0000298	0.1	0	0.0261	0.0261	0.0262	0.0262	0.1046
123.833	5.859	0.106	0.00675	0.156	0.0591	0.123	0.0148	0.0342	0.015	0.000692	0.0000199	0.1	0	0.0259	0.0259	0.0259	0.026	0.1037

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
123.917	5.838	0.105	0.00642	0.154	0.0583	0.122	0.0147	0.0334	0.0147	0.000622	0.00000994	0.1	0	0.0256	0.0256	0.0256	0.0257	0.1025
124	5.817	0.103	0.0061	0.153	0.0575	0.121	0.0145	0.0326	0.0145	0.000551	0	0.1	0	0.0253	0.0254	0.0254	0.0254	0.1015
124.083	5.795	0.102	0.00581	0.151	0.0568	0.12	0.0143	0.0318	0.0143	0.000494	0	0.1	0	0.0251	0.0251	0.0251	0.0252	0.1005
124.167	5.774	0.101	0.00552	0.15	0.056	0.119	0.0142	0.031	0.014	0.000438	0	0.1	0	0.0248	0.0248	0.0248	0.0249	0.0993
124.25	5.753	0.0996	0.00522	0.148	0.0552	0.118	0.014	0.0302	0.0138	0.000381	0	0.1	0	0.0245	0.0246	0.0246	0.0246	0.0983
124.333	5.732	0.0983	0.00497	0.146	0.0544	0.117	0.0138	0.0294	0.0135	0.000334	0	0.1	0	0.0243	0.0243	0.0243	0.0244	0.0973
124.417	5.711	0.097	0.00471	0.145	0.0536	0.116	0.0137	0.0286	0.0133	0.000287	0	0.1	0	0.024	0.024	0.024	0.0241	0.0961
124.5	5.69	0.0958	0.00445	0.143	0.0528	0.115	0.0135	0.0278	0.013	0.00024	0	0.1	0	0.0237	0.0238	0.0238	0.0238	0.0951
124.583	5.669	0.0944	0.00423	0.141	0.052	0.114	0.0133	0.027	0.0128	0.000202	0	0.1	0	0.0234	0.0235	0.0235	0.0235	0.0939
124.667	5.648	0.0931	0.00401	0.14	0.0511	0.113	0.0131	0.0263	0.0125	0.000165	0	0.1	0	0.0232	0.0232	0.0232	0.0233	0.0929
124.75	5.627	0.0918	0.00378	0.138	0.0503	0.112	0.013	0.0255	0.0123	0.000127	0	0.1	0	0.0229	0.0229	0.0229	0.023	0.0917
124.833	5.606	0.0905	0.00359	0.136	0.0495	0.111	0.0128	0.0248	0.012	0.000104	0	0.1	0	0.0226	0.0226	0.0226	0.0227	0.0905
124.917	5.585	0.0891	0.0034	0.135	0.0486	0.11	0.0126	0.0241	0.0118	0.0000801	0	0.1	0	0.0223	0.0223	0.0224	0.0224	0.0894
125	5.565	0.0878	0.00321	0.133	0.0478	0.109	0.0124	0.0234	0.0115	0.0000565	0	0.1	0	0.022	0.0221	0.0221	0.0221	0.0883
125.083	5.544	0.0864	0.00305	0.131	0.0469	0.108	0.0122	0.0227	0.0112	0.0000424	0	0.1	0	0.0217	0.0218	0.0218	0.0218	0.0871
125.167	5.523	0.085	0.00289	0.129	0.046	0.107	0.012	0.022	0.011	0.0000283	0	0.1	0	0.0215	0.0215	0.0215	0.0216	0.0861
125.25	5.502	0.0836	0.00274	0.128	0.0452	0.106	0.0119	0.0213	0.0107	0.0000141	0	0.1	0	0.0212	0.0212	0.0212	0.0213	0.0849
125.333	5.481	0.0822	0.00259	0.126	0.0443	0.105	0.0117	0.0207	0.0105	0.00000942	0	0.1	0	0.0209	0.0209	0.0209	0.021	0.0837
125.417	5.46	0.0808	0.00245	0.124	0.0434	0.104	0.0115	0.02	0.0103	0.00000471	0	0.1	0	0.0206	0.0206	0.0206	0.0207	0.0825
125.5	5.44	0.0794	0.0023	0.122	0.0425	0.103	0.0113	0.0194	0.01	0	0	0.1	0	0.0203	0.0203	0.0203	0.0204	0.0813
125.583	5.419	0.078	0.00217	0.121	0.0417	0.102	0.0111	0.0188	0.00981	0	0	0.1	0	0.02	0.02	0.02	0.0202	0.0802
125.667	5.398	0.0765	0.00204	0.119	0.0408	0.101	0.0109	0.0182	0.00958	0	0	0.1	0	0.0197	0.0197	0.0197	0.0201	0.0792
125.75	5.377	0.0751	0.00191	0.117	0.04	0.0994	0.0107	0.0176	0.00936	0	0	0.1	0	0.0194	0.0194	0.0194	0.02	0.0782
125.833	5.357	0.0737	0.00179	0.115	0.0392	0.0983	0.0105	0.0171	0.00914	0	0	0.1	0	0.0191	0.0191	0.0191	0.02	0.0773
125.917	5.336	0.0723	0.00167	0.113	0.0384	0.0972	0.0103	0.0165	0.00893	0	0	0.1	0	0.0188	0.0188	0.0188	0.02	0.0764
126	5.315	0.0709	0.00155	0.111	0.0376	0.0961	0.0101	0.0159	0.00871	0	0	0.1	0	0.0184	0.0185	0.0185	0.02	0.0754
126.083	5.295	0.0696	0.00144	0.11	0.0368	0.095	0.00993	0.0154	0.00851	0	0	0.1	0	0.0181	0.0182	0.0182	0.02	0.0745
126.167	5.274	0.0682	0.00133	0.108	0.036	0.0938	0.00974	0.0149	0.00831	0	0	0.1	0	0.0178	0.0178	0.0179	0.02	0.0735
126.25	5.254	0.0669	0.00122	0.106	0.0353	0.0927	0.00955	0.0144	0.00811	0	0	0.1	0	0.0175	0.0175	0.0175	0.02	0.0725
126.333	5.233	0.0656	0.00113	0.104	0.0345	0.0916	0.00937	0.0139	0.00792	0	0	0.1	0	0.0172	0.0172	0.0172	0.02	0.0716
126.417	5.213	0.0643	0.00103	0.102	0.0338	0.0904	0.00919	0.0134	0.00773	0	0	0.1	0	0.0169	0.0169	0.0169	0.02	0.0707
126.5	5.192	0.063	0.000936	0.1	0.0331	0.0893	0.00901	0.0129	0.00753	0	0	0.1	0	0.0166	0.0166	0.0166	0.02	0.0698
126.583	5.172	0.0618	0.000852	0.0987	0.0324	0.0882	0.00884	0.0125	0.00735	0	0	0.1	0	0.0163	0.0163	0.0163	0.02	0.0689
126.667	5.151	0.0606	0.000768	0.0969	0.0317	0.087	0.00867	0.012	0.00717	0	0	0.1	0	0.016	0.0161	0.0161	0.02	0.0682
126.75	5.131	0.0593	0.000684	0.0952	0.031	0.0859	0.0085	0.0116	0.00698	0	0	0.1	0	0.0157	0.0158	0.0158	0.02	0.0673
126.833	5.11	0.0581	0.000616	0.0935	0.0303	0.0847	0.00834	0.0112	0.00681	0	0	0.1	0	0.0155	0.0155	0.0155	0.02	0.0665
126.917	5.09	0.057	0.000548	0.0918	0.0297	0.0836	0.00818	0.0108	0.00663	0	0	0.1	0	0.0152	0.0152	0.0152	0.02	0.0656
127	5.069	0.0558	0.00048	0.0901	0.029	0.0824	0.00801	0.0104	0.00646	0	0	0.1	0	0.0149	0.0149	0.0149	0.02	0.0647
127.083	5.049	0.0547	0.000424	0.0885	0.0284	0.0813	0.00786	0.01	0.00629	0	0	0.1	0	0.0146	0.0147	0.0147	0.02	0.064
127.167	5.029	0.0536	0.000368	0.0869	0.0277	0.0801	0.0077	0.00966	0.00612	0	0	0.1	0	0.0144	0.0144	0.0144	0.02	0.0632
127.25	5.008	0.0525	0.000312	0.0853	0.0271	0.079	0.00755	0.0093	0.00595	0	0	0.1	0	0.0141	0.0141	0.0141	0.02	0.0623
127.333	4.988	0.0514	0.000268	0.0837	0.0265	0.0778	0.0074	0.00897	0.0058	0	0	0.1	0	0.0138	0.0139	0.0139	0.02	0.0616
127.417	4.968	0.0503	0.000224	0.0822	0.0259	0.0766	0.00725	0.00863	0.00564	0	0	0.1	0	0.0136	0.0136	0.0136	0.02	0.0608
127.5	4.947	0.0493	0.00018	0.0806	0.0253	0.0755	0.0071	0.0083	0.00548	0	0	0.1	0	0.0133	0.0133	0.0133	0.02	0.0599
127.583	4.927	0.0482	0.000148	0.0791	0.0247	0.0743	0.00695	0.00799	0.00533	0	0	0.1	0	0.0131	0.0131	0.0131	0.02	0.0593
127.667	4.907	0.0472	0.000116	0.0776	0.0242	0.0731	0.00681	0.00768	0.00518	0	0	0.1	0	0.0128	0.0128	0.0129	0.02	0.0585
127.75	4.887	0.0462	0.000084	0.0761	0.0236	0.0719	0.00667	0.00737	0.00503	0	0	0.1	0	0.0126	0.0126	0.0126	0.02	0.0578
127.833	4.866	0.0452	0.000064	0.0747	0.023	0.0707	0.00653	0.00708	0.00489	0	0	0.1	0	0.0123	0.0124	0.0124	0.02	0.0571
127.917	4.846	0.0443	0.000044	0.0733	0.0225	0.0695	0.00639	0.00679	0.00475	0	0	0.1	0	0.0121	0.0121	0.0121	0.02	0.0563
128	4.826	0.0433	0.000024	0.0719	0.022	0.0683	0.00625	0.00651	0.00461	0	0	0.1	0	0.0119	0.0119	0.0119	0.02	0.0557
128.083	4.806	0.0424	0.000016	0.0705	0.0214	0.0672	0.00613	0.00623	0.00449	0	0	0.1	0	0.0116	0.0117	0.0117	0.02	0.055
128.167	4.786	0.0415	0.000008	0.0692	0.0209	0.066	0.006	0.00596	0.00436	0	0	0.1	0	0.0114	0.0114	0.0114	0.02	0.0542
128.25	4.766	0.0405	0	0.0678	0.0204	0.0648	0.00587	0.00569	0.00423	0	0	0.1	0	0.0112	0.0112	0.0112	0.02	0.0536
128.333	4.746	0.0397	0	0.0665	0.0199	0.0637	0.00575	0.00545	0.00411	0	0	0.1	0	0.011	0.011	0.011	0.02	0.053
128.417	4.725	0.0388	0	0.0652	0.0195	0.0626	0.00563	0.0052	0.00399	0	0	0.1	0	0.0108	0.0108	0.0108	0.02	0.0524
128.5	4.705	0.0379	0	0.0639	0.019	0.0614	0.0055	0.00496	0.00387	0	0	0.1	0	0.0105	0.0106	0.0106	0.02	0.0517
128.583	4.685	0.0371	0	0.0626	0.0185	0.0603	0.00539	0.00473	0.00376	0	0	0.1	0	0.0103	0.0104	0.0104	0.02	0.0511
128.667	4.665	0.0363	0	0.0614	0.018	0.0592	0.00527	0.00451	0.00365	0	0	0.1	0	0.0101	0.0102	0.0102	0.02	0.0505
128.75	4.645	0.0354	0	0.0602	0.0176	0.0581	0.00515	0.00428	0.00354	0	0	0.1	0	0.00993	0.00995	0.00995	0.02	0.04983
128.833	4.625	0.0346	0	0.059	0.0172	0.0571	0.00504	0.00408	0.00343	0	0	0.1	0	0.00974	0.00975	0.00975	0.02	0.04924
128.917	4.605	0.0339	0	0.0578	0.0167	0.056	0.00493	0.00388	0.00333	0	0	0.1	0	0.00954	0.00955	0.00956	0.02	0.04865
129	4.585	0.0331	0	0.0566	0.0163	0.0549	0.00482	0.00368	0.00323	0	0	0.1	0	0.00934	0.00935	0.00936	0.02	0.04805
129.083	4.565	0.0323	0	0.0554	0.0159	0.0539	0.00472	0.00349	0.00313	0	0	0.1	0	0.00916	0.00917	0.00917	0.02	0.0475

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
129.167	4.546	0.0316	0	0.0543	0.0155	0.0529	0.00461	0.00331	0.00303	0	0	0.1	0	0.00897	0.00898	0.00898	0.02	0.04693
129.25	4.526	0.0308	0	0.0532	0.0151	0.0519	0.0045	0.00313	0.00294	0	0	0.1	0	0.00878	0.00879	0.0088	0.02	0.04637
129.333	4.506	0.0301	0	0.0521	0.0147	0.0509	0.0044	0.00296	0.00285	0	0	0.1	0	0.0086	0.00861	0.00862	0.02	0.04583
129.417	4.486	0.0294	0	0.051	0.0143	0.0499	0.0043	0.00279	0.00275	0	0	0.1	0	0.00842	0.00843	0.00844	0.02	0.04529
129.5	4.466	0.0287	0	0.0499	0.0139	0.0489	0.0042	0.00263	0.00266	0	0	0.1	0	0.00824	0.00825	0.00826	0.02	0.04475
129.583	4.446	0.028	0	0.0489	0.0136	0.048	0.00411	0.00248	0.00258	0	0	0.1	0	0.00808	0.00809	0.00809	0.02	0.04426
129.667	4.426	0.0273	0	0.0478	0.0132	0.047	0.00401	0.00233	0.00249	0	0	0.1	0	0.00791	0.00792	0.00792	0.02	0.04375
129.75	4.406	0.0267	0	0.0468	0.0129	0.0461	0.00392	0.00218	0.0024	0	0	0.1	0	0.00774	0.00775	0.00775	0.02	0.04324
129.833	4.387	0.026	0	0.0458	0.0125	0.0452	0.00383	0.00204	0.00232	0	0	0.1	0	0.00757	0.00758	0.00759	0.02	0.04274
129.917	4.367	0.0254	0	0.0449	0.0122	0.0443	0.00374	0.0019	0.00224	0	0	0.1	0	0.00741	0.00742	0.00743	0.02	0.04226
130	4.347	0.0248	0	0.0439	0.0118	0.0434	0.00366	0.00176	0.00216	0	0	0.1	0	0.00725	0.00726	0.00727	0.02	0.04178
130.083	4.327	0.0242	0	0.043	0.0115	0.0425	0.00357	0.00164	0.00208	0	0	0.1	0	0.0071	0.00711	0.00711	0.02	0.04132
130.167	4.308	0.0236	0	0.042	0.0112	0.0416	0.00349	0.00152	0.002	0	0	0.1	0	0.00695	0.00695	0.00696	0.02	0.04086
130.25	4.288	0.023	0	0.0411	0.0109	0.0407	0.00341	0.0014	0.00192	0	0	0.1	0	0.00679	0.0068	0.0068	0.02	0.04039
130.333	4.268	0.0225	0	0.0403	0.0105	0.0399	0.00333	0.00129	0.00185	0	0	0.1	0	0.00665	0.00666	0.00666	0.02	0.03997
130.417	4.249	0.0219	0	0.0394	0.0102	0.039	0.00325	0.00118	0.00177	0	0	0.1	0	0.0065	0.00651	0.00651	0.02	0.03952
130.5	4.229	0.0214	0	0.0385	0.00992	0.0382	0.00317	0.00108	0.0017	0	0	0.1	0	0.00636	0.00637	0.00637	0.02	0.0391
130.583	4.209	0.0209	0	0.0377	0.00963	0.0373	0.0031	0.00098	0.00163	0	0	0.1	0	0.00622	0.00623	0.00623	0.02	0.03868
130.667	4.19	0.0203	0	0.0369	0.00933	0.0365	0.00302	0.000884	0.00156	0	0	0.1	0	0.00608	0.00609	0.00609	0.02	0.03826
130.75	4.17	0.0198	0	0.036	0.00903	0.0357	0.00295	0.000788	0.00149	0	0	0.1	0	0.00594	0.00595	0.00595	0.02	0.03784
130.833	4.151	0.0193	0	0.0353	0.00876	0.0349	0.00288	0.000709	0.00143	0	0	0.1	0	0.00582	0.00582	0.00583	0.02	0.03747
130.917	4.131	0.0188	0	0.0345	0.00848	0.0341	0.0028	0.000629	0.00137	0	0	0.1	0	0.00569	0.00569	0.0057	0.02	0.03708
131	4.111	0.0183	0	0.0337	0.00821	0.0333	0.00273	0.00055	0.0013	0	0	0.1	0	0.00556	0.00557	0.00557	0.02	0.0367
131.083	4.092	0.0178	0	0.033	0.00794	0.0325	0.00266	0.000484	0.00124	0	0	0.1	0	0.00544	0.00544	0.00545	0.02	0.03633
131.167	4.072	0.0173	0	0.0323	0.00768	0.0318	0.00259	0.000417	0.00119	0	0	0.1	0	0.00531	0.00532	0.00532	0.02	0.03595
131.25	4.053	0.0168	0	0.0315	0.00742	0.031	0.00253	0.00035	0.00113	0	0	0.1	0	0.00519	0.0052	0.0052	0.02	0.03559
131.333	4.033	0.0163	0	0.0308	0.00717	0.0303	0.00246	0.0003	0.00108	0	0	0.1	0	0.00507	0.00508	0.00508	0.02	0.03523
131.417	4.014	0.0159	0	0.0301	0.00693	0.0295	0.00239	0.00025	0.00102	0	0	0.1	0	0.00496	0.00496	0.00496	0.02	0.03488
131.5	3.995	0.0154	0	0.0294	0.00668	0.0288	0.00232	0.0002	0.00097	0	0	0.1	0	0.00484	0.00484	0.00485	0.02	0.03453
131.583	3.975	0.015	0	0.0288	0.00645	0.0281	0.00226	0.000163	0.000922	0	0	0.1	0	0.00473	0.00473	0.00474	0.02	0.0342
131.667	3.956	0.0145	0	0.0281	0.00621	0.0274	0.0022	0.000125	0.000875	0	0	0.1	0	0.00462	0.00462	0.00463	0.02	0.03387
131.75	3.936	0.0141	0	0.0274	0.00598	0.0266	0.00214	0.0000875	0.000827	0	0	0.1	0	0.00451	0.00451	0.00451	0.02	0.03353
131.833	3.917	0.0136	0	0.0268	0.00576	0.026	0.00207	0.0000667	0.000785	0	0	0.1	0	0.0044	0.00441	0.00441	0.02	0.03322
131.917	3.897	0.0132	0	0.0261	0.00554	0.0253	0.00201	0.0000459	0.000742	0	0	0.1	0	0.00429	0.0043	0.0043	0.02	0.03289
132	3.878	0.0128	0	0.0255	0.00532	0.0246	0.00195	0.000025	0.0007	0	0	0.1	0	0.00419	0.00419	0.00419	0.02	0.03257
132.083	3.859	0.0124	0	0.0248	0.00512	0.024	0.00189	0.0000167	0.000661	0	0	0.1	0	0.00408	0.00409	0.00409	0.02	0.03226
132.167	3.839	0.012	0	0.0242	0.00492	0.0233	0.00184	0.00000834	0.000622	0	0	0.1	0	0.00398	0.00398	0.00399	0.02	0.03195
132.25	3.82	0.0116	0	0.0236	0.00472	0.0226	0.00178	0	0.000583	0	0	0.1	0	0.00387	0.00388	0.00388	0.02	0.03163
132.333	3.801	0.0112	0	0.023	0.00453	0.022	0.00172	0	0.000548	0	0	0.1	0	0.00378	0.00378	0.00378	0.02	0.03134
132.417	3.782	0.0108	0	0.0224	0.00434	0.0214	0.00167	0	0.000512	0	0	0.1	0	0.00368	0.00368	0.00368	0.02	0.03104
132.5	3.762	0.0104	0	0.0218	0.00415	0.0208	0.00161	0	0.000477	0	0	0.1	0	0.00358	0.00358	0.00359	0.02	0.03075
132.583	3.743	0.0101	0	0.0212	0.00398	0.0202	0.00156	0	0.000445	0	0	0.1	0	0.00348	0.00349	0.00349	0.02	0.03046
132.667	3.724	0.00972	0	0.0206	0.00381	0.0196	0.00151	0	0.000414	0	0	0.1	0	0.00338	0.00339	0.00339	0.02	0.03016
132.75	3.705	0.00935	0	0.0201	0.00363	0.019	0.00146	0	0.000382	0	0	0.1	0	0.00329	0.00329	0.00329	0.02	0.02987
132.833	3.685	0.00901	0	0.0195	0.00347	0.0184	0.00141	0	0.000353	0	0	0.1	0	0.0032	0.0032	0.0032	0.02	0.0296
132.917	3.666	0.00867	0	0.019	0.00331	0.0179	0.00136	0	0.000325	0	0	0.1	0	0.0031	0.00311	0.00311	0.02	0.02932
133	3.647	0.00833	0	0.0184	0.00315	0.0173	0.00131	0	0.000297	0	0	0.1	0	0.00301	0.00302	0.00302	0.02	0.02905
133.083	3.628	0.00802	0	0.0179	0.003	0.0168	0.00126	0	0.000272	0	0	0.1	0	0.00293	0.00293	0.00293	0.02	0.02879
133.167	3.609	0.00771	0	0.0174	0.00286	0.0162	0.00121	0	0.000247	0	0	0.1	0	0.00284	0.00285	0.00285	0.02	0.02854
133.25	3.59	0.00739	0	0.0168	0.00271	0.0157	0.00117	0	0.000223	0	0	0.1	0	0.00276	0.00276	0.00276	0.02	0.02828
133.333	3.57	0.0071	0	0.0163	0.00258	0.0152	0.00112	0	0.000201	0	0	0.1	0	0.00267	0.00268	0.00268	0.02	0.02803
133.417	3.551	0.00682	0	0.0158	0.00245	0.0147	0.00108	0	0.00018	0	0	0.1	0	0.00259	0.00259	0.00259	0.02	0.02777
133.5	3.532	0.00653	0	0.0153	0.00231	0.0142	0.00103	0	0.000159	0	0	0.1	0	0.0025	0.0025	0.00251	0.02	0.02751
133.583	3.513	0.00626	0	0.0149	0.00219	0.0137	0.000995	0	0.000141	0	0	0.1	0	0.00242	0.00243	0.00243	0.02	0.02728
133.667	3.494	0.00599	0	0.0144	0.00207	0.0132	0.000955	0	0.000124	0	0	0.1	0	0.00234	0.00235	0.00235	0.02	0.02704
133.75	3.475	0.00572	0	0.0139	0.00196	0.0127	0.000916	0	0.000106	0	0	0.1	0	0.00227	0.00227	0.00227	0.02	0.02681
133.833	3.456	0.00548	0	0.0135	0.00185	0.0123	0.000878	0	0.0000919	0	0	0.1	0	0.00219	0.0022	0.0022	0.02	0.02659
133.917	3.437	0.00523	0	0.013	0.00173	0.0118	0.00084	0	0.0000778	0	0	0.1	0	0.00212	0.00212	0.00212	0.02	0.02636
134	3.418	0.00498	0	0.0126	0.00162	0.0114	0.000803	0	0.0000636	0	0	0.1	0	0.00205	0.00205	0.00205	0.02	0.02615
134.083	3.399	0.00476	0	0.0121	0.00152	0.0109	0.000769	0	0.000053	0	0	0.1	0	0.00198	0.00198	0.00198	0.02	0.02594
134.167	3.38	0.00453	0	0.0117	0.00142	0.0105	0.000735	0	0.0000424	0	0	0.1	0	0.0019	0.00191	0.00191	0.02	0.02572
134.25	3.361	0.00431	0	0.0113	0.00132	0.0101	0.000701	0	0.0000318	0	0	0.1	0	0.00183	0.00183	0.00183	0.02	0.02549
134.333	3.342	0.0041	0	0.0109	0.00123	0.0097	0.000669	0	0.0000247	0	0	0.1	0	0.00177	0.00177	0.00177	0.02	0.02531

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
134.417	3.323	0.0039	0	0.0105	0.00114	0.0093	0.000637	0	0.0000177	0	0	0.1	0	0.0017	0.0017	0.0017	0.02	0.0251
134.5	3.304	0.00369	0	0.0101	0.00105	0.00891	0.000605	0	0.0000106	0	0	0.1	0	0.00163	0.00164	0.00164	0.02	0.02491
134.583	3.285	0.00351	0	0.00974	0.000964	0.00855	0.000577	0	0.00000707	0	0	0.1	0	0.00157	0.00158	0.00158	0.02	0.02473
134.667	3.267	0.00332	0	0.00937	0.000881	0.00818	0.000549	0	0.00000353	0	0	0.1	0	0.00151	0.00152	0.00152	0.02	0.02455
134.75	3.248	0.00314	0	0.00899	0.000799	0.00782	0.000521	0	0	0	0	0.1	0	0.00146	0.00146	0.00146	0.02	0.02438
134.833	3.229	0.00297	0	0.00864	0.000725	0.00748	0.000494	0	0	0	0	0.1	0	0.0014	0.0014	0.0014	0.02	0.0242
134.917	3.21	0.0028	0	0.0083	0.000652	0.00714	0.000468	0	0	0	0	0.1	0	0.00134	0.00134	0.00134	0.02	0.02402
135	3.191	0.00264	0	0.00795	0.000578	0.00681	0.000441	0	0	0	0	0.1	0	0.00128	0.00128	0.00128	0.02	0.02384
135.083	3.172	0.00248	0	0.00762	0.000523	0.0065	0.000419	0	0	0	0	0.1	0	0.00122	0.00123	0.00123	0.02	0.02368
135.167	3.154	0.00233	0	0.00729	0.000468	0.00619	0.000396	0	0	0	0	0.1	0	0.00117	0.00117	0.00117	0.02	0.02351
135.25	3.135	0.00218	0	0.00696	0.000413	0.00588	0.000374	0	0	0	0	0.1	0	0.00112	0.00112	0.00112	0.02	0.02336
135.333	3.116	0.00204	0	0.00667	0.000367	0.00561	0.000351	0	0	0	0	0.1	0	0.00107	0.00107	0.00107	0.02	0.02321
135.417	3.097	0.0019	0	0.00637	0.000321	0.00533	0.000328	0	0	0	0	0.1	0	0.00102	0.00103	0.00103	0.02	0.02308
135.5	3.078	0.00176	0	0.00607	0.000275	0.00505	0.000306	0	0	0	0	0.1	0	0.000977	0.000978	0.000979	0.02	0.02293
135.583	3.06	0.00163	0	0.0058	0.000239	0.0048	0.000287	0	0	0	0	0.1	0	0.00093	0.000931	0.000932	0.02	0.02279
135.667	3.041	0.00151	0	0.00553	0.000202	0.00455	0.000268	0	0	0	0	0.1	0	0.000884	0.000885	0.000885	0.02	0.02265
135.75	3.022	0.00138	0	0.00526	0.000165	0.0043	0.000249	0	0	0	0	0.1	0	0.000837	0.000838	0.000838	0.02	0.02251
135.833	3.004	0.00127	0	0.00501	0.000138	0.00407	0.00023	0	0	0	0	0.1	0	0.000797	0.000798	0.000798	0.02	0.02239
135.917	2.985	0.00116	0	0.00476	0.00011	0.00385	0.000211	0	0	0	0	0.1	0	0.000756	0.000757	0.000758	0.02	0.02227
136	2.966	0.00105	0	0.00451	0.0000826	0.00362	0.000192	0	0	0	0	0.1	0	0.000716	0.000717	0.000717	0.02	0.02215
136.083	2.948	0.000948	0	0.00429	0.0000643	0.00342	0.000177	0	0	0	0	0.1	0	0.000682	0.000683	0.000683	0.02	0.02205
136.167	2.929	0.000851	0	0.00407	0.0000459	0.00321	0.000162	0	0	0	0	0.1	0	0.000648	0.000649	0.000649	0.02	0.02195
136.25	2.91	0.000753	0	0.00385	0.0000275	0.00301	0.000147	0	0	0	0	0.1	0	0.000614	0.000615	0.000615	0.02	0.02184
136.333	2.892	0.000676	0	0.00365	0.0000184	0.00282	0.000132	0	0	0	0	0.1	0	0.00058	0.00058	0.000581	0.02	0.02174
136.417	2.873	0.0006	0	0.00346	0.00000918	0.00263	0.000117	0	0	0	0	0.1	0	0.000546	0.000546	0.000547	0.02	0.02164
136.5	2.855	0.000523	0	0.00326	0	0.00245	0.000102	0	0	0	0	0.1	0	0.000511	0.000512	0.000512	0.02	0.02154
136.583	2.836	0.00046	0	0.00308	0	0.00228	0.0000906	0	0	0	0	0.1	0	0.000482	0.000482	0.000482	0.02	0.02145
136.667	2.818	0.000397	0	0.00289	0	0.00211	0.0000792	0	0	0	0	0.1	0	0.000452	0.000452	0.000453	0.02	0.02136
136.75	2.799	0.000335	0	0.00271	0	0.00194	0.0000679	0	0	0	0	0.1	0	0.000422	0.000422	0.000423	0.02	0.02127
136.833	2.78	0.000286	0	0.00255	0	0.0018	0.0000604	0	0	0	0	0.1	0	0.000396	0.000397	0.000397	0.02	0.02119
136.917	2.762	0.000237	0	0.00238	0	0.00165	0.0000528	0	0	0	0	0.1	0	0.000371	0.000371	0.000371	0.02	0.02111
137	2.743	0.000188	0	0.00222	0	0.0015	0.0000453	0	0	0	0	0.1	0	0.000345	0.000346	0.000346	0.02	0.02104
137.083	2.725	0.000153	0	0.00206	0	0.00137	0.0000377	0	0	0	0	0.1	0	0.00032	0.00032	0.00032	0.02	0.02096
137.167	2.706	0.000119	0	0.00191	0	0.00124	0.0000302	0	0	0	0	0.1	0	0.000294	0.000294	0.000295	0.02	0.02088
137.25	2.688	0.0000837	0	0.00176	0	0.00111	0.0000226	0	0	0	0	0.1	0	0.000269	0.000269	0.000269	0.02	0.02081
137.333	2.67	0.0000627	0	0.00162	0	0.001	0.0000189	0	0	0	0	0.1	0	0.000247	0.000248	0.000248	0.02	0.02074
137.417	2.651	0.0000418	0	0.00149	0	0.000894	0.0000151	0	0	0	0	0.1	0	0.000226	0.000226	0.000226	0.02	0.02068
137.5	2.633	0.0000209	0	0.00135	0	0.000784	0.0000113	0	0	0	0	0.1	0	0.000205	0.000205	0.000205	0.02	0.02062
137.583	2.614	0.0000139	0	0.00124	0	0.000694	0.00000755	0	0	0	0	0.1	0	0.000188	0.000188	0.000188	0.02	0.02056
137.667	2.596	0.00000697	0	0.00113	0	0.000603	0.00000377	0	0	0	0	0.1	0	0.00017	0.000171	0.000171	0.02	0.02051
137.75	2.577	0	0	0.00102	0	0.000512	0	0	0	0	0	0.1	0	0.000153	0.000154	0.000154	0.02	0.02046
137.833	2.559	0	0	0.000913	0	0.000441	0	0	0	0	0	0.1	0	0.000136	0.000137	0.000137	0.02	0.02041
137.917	2.541	0	0	0.000811	0	0.00037	0	0	0	0	0	0.1	0	0.000119	0.000119	0.00012	0.02	0.02036
138	2.522	0	0	0.000708	0	0.000298	0	0	0	0	0	0.1	0	0.000102	0.000102	0.000102	0.02	0.02031
138.083	2.504	0	0	0.000626	0	0.000246	0	0	0	0	0	0.1	0	0.0000895	0.0000896	0.0000897	0.02	0.02027
138.167	2.486	0	0	0.000544	0	0.000193	0	0	0	0	0	0.1	0	0.0000767	0.0000768	0.0000769	0.02	0.02023
138.25	2.467	0	0	0.000462	0	0.000141	0	0	0	0	0	0.1	0	0.0000639	0.000064	0.000064	0.02	0.02019
138.333	2.449	0	0	0.0004	0	0.000108	0	0	0	0	0	0.1	0	0.0000554	0.0000555	0.0000555	0.02	0.02017
138.417	2.431	0	0	0.000339	0	0.000075	0	0	0	0	0	0.1	0	0.0000469	0.0000469	0.000047	0.02	0.02014
138.5	2.412	0	0	0.000277	0	0.0000419	0	0	0	0	0	0.1	0	0.0000384	0.0000384	0.0000384	0.02	0.02012
138.583	2.394	0	0	0.000226	0	0.0000279	0	0	0	0	0	0.1	0	0.0000298	0.0000299	0.0000299	0.02	0.02009
138.667	2.376	0	0	0.000174	0	0.000014	0	0	0	0	0	0.1	0	0.0000213	0.0000213	0.0000213	0.02	0.02006
138.75	2.358	0	0	0.000123	0	0	0	0	0	0	0	0.1	0	0.0000128	0.0000128	0.0000128	0.02	0.02004
138.833	2.339	0	0	0.0000924	0	0	0	0	0	0	0	0.1	0	0.00000852	0.00000853	0.00000854	0.02	0.02003
138.917	2.321	0	0	0.0000616	0	0	0	0	0	0	0	0.1	0	0.00000426	0.00000427	0.00000427	0.02	0.02001
139	2.303	0	0	0.0000308	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.083	2.285	0	0	0.0000205	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.167	2.268	0	0	0.0000103	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.25	2.25	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.333	2.233	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.417	2.215	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.5	2.198	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.583	2.182	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
139.667	2.165	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.75	2.148	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.833	2.132	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
139.917	2.116	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140	2.1	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.083	2.084	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.167	2.068	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.25	2.053	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.333	2.038	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.417	2.022	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.5	2.007	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.583	1.993	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.667	1.978	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.75	1.963	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.833	1.949	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
140.917	1.935	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141	1.921	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.083	1.907	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.167	1.893	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.25	1.88	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.333	1.866	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.417	1.853	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.5	1.84	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.583	1.827	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.667	1.814	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.75	1.801	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.833	1.789	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
141.917	1.777	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142	1.765	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.083	1.753	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.167	1.741	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.25	1.729	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.333	1.718	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.417	1.706	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.5	1.695	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.583	1.684	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.667	1.673	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.75	1.662	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.833	1.651	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
142.917	1.641	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143	1.63	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.083	1.62	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.167	1.61	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.25	1.6	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.333	1.59	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.417	1.581	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.5	1.571	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.583	1.562	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.667	1.553	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.75	1.543	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.833	1.535	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
143.917	1.526	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144	1.517	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.083	1.509	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.167	1.5	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.25	1.492	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.333	1.484	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.417	1.476	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.5	1.468	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.583	1.46	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.667	1.453	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.75	1.445	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
144.833	1.438	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
144.917	1.431	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145	1.424	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.083	1.417	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.167	1.41	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.25	1.403	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.333	1.397	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.417	1.391	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.5	1.384	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.583	1.378	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.667	1.372	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.75	1.366	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.833	1.361	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
145.917	1.355	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146	1.349	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.083	1.344	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.167	1.338	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.25	1.333	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.333	1.328	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.417	1.322	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.5	1.317	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.583	1.312	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.667	1.307	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.75	1.302	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.833	1.296	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
146.917	1.291	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147	1.286	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.083	1.281	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.167	1.277	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.25	1.272	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.333	1.267	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.417	1.262	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.5	1.257	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.583	1.253	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.667	1.248	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.75	1.243	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.833	1.239	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
147.917	1.234	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148	1.23	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.083	1.225	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.167	1.221	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.25	1.217	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.333	1.212	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.417	1.208	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.5	1.204	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.583	1.2	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.667	1.196	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.75	1.192	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.833	1.188	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
148.917	1.184	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149	1.18	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.083	1.176	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.167	1.172	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.25	1.168	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.333	1.164	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.417	1.16	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.5	1.157	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.583	1.153	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.667	1.15	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.75	1.146	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.833	1.142	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
149.917	1.139	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150	1.135	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.083	1.132	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
150.167	1.129	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.25	1.125	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.333	1.122	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.417	1.119	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.5	1.115	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.583	1.112	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.667	1.109	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.75	1.106	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.833	1.103	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
150.917	1.1	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151	1.097	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.083	1.094	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.167	1.091	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.25	1.088	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.333	1.085	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.417	1.082	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.5	1.08	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.583	1.077	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.667	1.074	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.75	1.071	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.833	1.069	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
151.917	1.066	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152	1.064	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.083	1.061	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.167	1.059	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.25	1.056	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.333	1.054	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.417	1.051	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.5	1.049	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.583	1.047	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.667	1.045	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.75	1.042	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.833	1.04	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
152.917	1.038	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153	1.036	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.083	1.034	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.167	1.032	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.25	1.03	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.333	1.028	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.417	1.026	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.5	1.024	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.583	1.022	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.667	1.02	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.75	1.018	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.833	1.016	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
153.917	1.015	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154	1.013	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.083	1.011	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.167	1.009	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.25	1.008	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.333	1.006	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.417	1.005	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.5	1.003	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.583	1.002	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.667	1	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.75	0.999	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.833	0.997	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
154.917	0.996	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155	0.995	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.083	0.993	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.167	0.992	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.25	0.991	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.333	0.989	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
155.417	0.988	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.5	0.987	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.583	0.986	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.667	0.985	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.75	0.984	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.833	0.983	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
155.917	0.982	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156	0.981	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.083	0.98	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.167	0.979	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.25	0.978	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.333	0.977	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.417	0.976	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.5	0.975	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.583	0.975	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.667	0.974	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.75	0.973	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.833	0.973	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
156.917	0.972	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157	0.971	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.083	0.971	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.167	0.97	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.25	0.97	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.333	0.969	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.417	0.969	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.5	0.968	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.583	0.968	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.667	0.967	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.75	0.967	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.833	0.967	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
157.917	0.966	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158	0.966	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.083	0.966	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.167	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.25	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.333	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.417	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.5	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.583	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.667	0.965	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
158.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
159.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
160.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
160.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
161.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
162.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
163.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
164.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
165.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
165.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
166.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
167.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
168.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
169.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
170.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
171.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
171.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
172.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
173.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
174.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
175.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
176.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
176.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
177.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
178.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
179.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
180.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
181.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
181.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
182.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
183.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
184.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
185.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
186.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
186.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
187.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
188.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
189.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
190.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
191.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
192.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
192.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
193.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
194.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
195.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
196.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
197.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
197.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
198.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
199.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
200.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
201.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
202.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
202.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
203.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
204.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
205.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
206.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
207.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
207.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
208.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
209.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
210.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
211.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
212.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
213.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
213.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
214.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
215.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
216.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
217.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
218.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
218.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
219.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
220.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
221.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
222.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
223.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
223.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
224.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
225.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
226.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
227.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
228.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
228.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
229.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
230.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
231.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
232.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
233.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
234.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
234.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
235.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
236.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
237.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
238.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
239.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
239.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
240.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
241.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
242.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
243.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
244.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
244.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
245.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
246.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
247.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
248.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
249.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
249.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
250.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
251.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
252.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
253.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
254.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
255.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
255.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
256.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
257.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
258.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
259.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
260.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
260.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
261.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
262.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
263.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
264.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
265.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
265.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
266.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
267.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
268.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
269.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
270.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
270.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
271.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
272.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
273.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
274.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
275.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
276.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
276.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
277.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
278.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
279.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
280.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
281.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
281.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
282.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
283.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
284.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
285.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

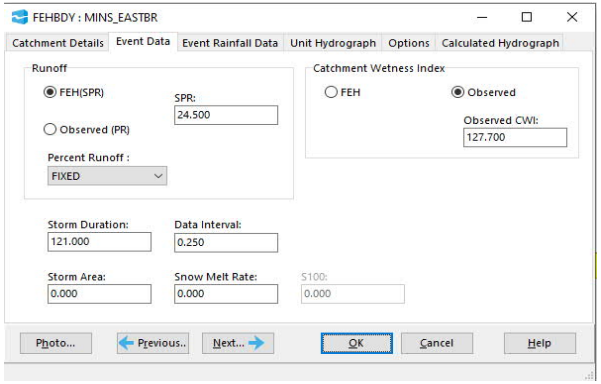
Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
286.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
286.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
287.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
288.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
289.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
290.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
291.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
291.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
292.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
293.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
294.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
295.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
296.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
297.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
297.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
298.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.083	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.167	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.25	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.333	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.417	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.5	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.583	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.667	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.75	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.833	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
299.917	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02
300	0.964	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0.02	0.02

Output data from file C:\USERS\304490\BOX\PB6582 EDF SZC NNB\EDF SZC NNB TEAM\TECH DATA\E01 CALCULATIONS\EXAMINATION HYDROLOGY\HYDROLOGY CALCS MAY 2021\MDS EA ACTIONS MAY 2021\DESIGN FLOWS\SIZE_T100_121SD_SPR_HIGHCWI.ZZN
Selected output data from time (hr): 0
to time (hr): 300



Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
0	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
0.083	0.965	0.0722	0.0204	0.0684	0.0323	0.0656	0.0182	0.053	0.0229	0.023	0.016	0.1	0.0416	0.0269	0.0189	0.0159	0.02	0.0817
0.167	0.965	0.0723	0.0204	0.0684	0.0323	0.0657	0.0182	0.053	0.023	0.023	0.0161	0.1	0.0418	0.0269	0.0189	0.0159	0.02	0.0817
0.25	0.965	0.0723	0.0205	0.0685	0.0323	0.0657	0.0182	0.0531	0.023	0.023	0.0161	0.1	0.042	0.0269	0.0189	0.016	0.02	0.0818
0.333	0.965	0.0724	0.0206	0.0686	0.0324	0.0658	0.0182	0.0532	0.023	0.0231	0.0163	0.1	0.0427	0.0269	0.0189	0.016	0.02	0.0818
0.417	0.966	0.0725	0.0207	0.0687	0.0325	0.0659	0.0182	0.0534	0.0231	0.0233	0.0164	0.1	0.0433	0.0269	0.019	0.016	0.02	0.0819
0.5	0.966	0.0727	0.0208	0.0689	0.0325	0.066	0.0182	0.0535	0.0231	0.0234	0.0166	0.1	0.044	0.027	0.019	0.016	0.02	0.082
0.583	0.967	0.0729	0.0211	0.0691	0.0327	0.0661	0.0183	0.0537	0.0232	0.0235	0.0169	0.1	0.0451	0.027	0.019	0.0161	0.02	0.0821
0.667	0.967	0.0731	0.0213	0.0693	0.0328	0.0662	0.0183	0.054	0.0232	0.0237	0.0171	0.1	0.0462	0.0271	0.0191	0.0161	0.02	0.0823
0.75	0.968	0.0733	0.0215	0.0695	0.0329	0.0663	0.0183	0.0542	0.0233	0.0239	0.0174	0.1	0.0473	0.0271	0.0191	0.0162	0.02	0.0824
0.833	0.969	0.0736	0.0218	0.0698	0.0331	0.0665	0.0184	0.0546	0.0234	0.0241	0.0178	0.1	0.0483	0.0272	0.0192	0.0162	0.02	0.0826
0.917	0.969	0.0739	0.0221	0.0701	0.0333	0.0667	0.0184	0.0549	0.0234	0.0244	0.0181	0.1	0.0493	0.0272	0.0193	0.0163	0.02	0.0828
1	0.97	0.0741	0.0224	0.0704	0.0334	0.0668	0.0185	0.0553	0.0235	0.0246	0.0184	0.1	0.0504	0.0273	0.0193	0.0164	0.02	0.083
1.083	0.971	0.0745	0.0228	0.0708	0.0336	0.067	0.0186	0.0557	0.0236	0.025	0.0187	0.1	0.0512	0.0274	0.0194	0.0165	0.02	0.0833
1.167	0.972	0.0749	0.0232	0.0711	0.0339	0.0672	0.0186	0.0561	0.0238	0.0253	0.019	0.1	0.0519	0.0275	0.0195	0.0165	0.02	0.0835
1.25	0.973	0.0752	0.0236	0.0715	0.0341	0.0674	0.0187	0.0566	0.0239	0.0256	0.0193	0.1	0.0527	0.0275	0.0196	0.0166	0.02	0.0837
1.333	0.974	0.0757	0.0241	0.072	0.0344	0.0677	0.0188	0.0571	0.024	0.0259	0.0196	0.1	0.0532	0.0276	0.0197	0.0167	0.02	0.084
1.417	0.975	0.0761	0.0245	0.0725	0.0346	0.0679	0.0188	0.0576	0.0241	0.0263	0.0198	0.1	0.0538	0.0277	0.0198	0.0168	0.02	0.0843
1.5	0.976	0.0766	0.025	0.0729	0.0349	0.0682	0.0189	0.0582	0.0243	0.0266	0.02	0.1	0.0543	0.0278	0.0199	0.0169	0.02	0.0846
1.583	0.977	0.0771	0.0256	0.0735	0.0352	0.0685	0.019	0.0588	0.0244	0.0269	0.0202	0.1	0.0547	0.028	0.02	0.017	0.02	0.085
1.667	0.979	0.0776	0.0261	0.074	0.0355	0.0688	0.0191	0.0594	0.0246	0.0272	0.0204	0.1	0.0551	0.0281	0.0201	0.0172	0.02	0.0854
1.75	0.98	0.0782	0.0267	0.0746	0.0359	0.069	0.0192	0.0601	0.0247	0.0274	0.0205	0.1	0.0555	0.0282	0.0202	0.0173	0.02	0.0857
1.833	0.982	0.0788	0.0274	0.0752	0.0362	0.0694	0.0193	0.0608	0.0249	0.0277	0.0207	0.1	0.0558	0.0283	0.0204	0.0174	0.02	0.0861
1.917	0.983	0.0794	0.028	0.0758	0.0366	0.0697	0.0194	0.0615	0.0251	0.0279	0.0208	0.1	0.0561	0.0285	0.0205	0.0175	0.02	0.0865
2	0.985	0.08	0.0287	0.0765	0.037	0.07	0.0195	0.0623	0.0253	0.0282	0.0209	0.1	0.0564	0.0286	0.0206	0.0177	0.02	0.0869
2.083	0.986	0.0807	0.0294	0.0772	0.0374	0.0704	0.0196	0.0631	0.0255	0.0284	0.021	0.1	0.0565	0.0288	0.0208	0.0178	0.02	0.0874
2.167	0.988	0.0814	0.03	0.0779	0.0379	0.0708	0.0197	0.0639	0.0257	0.0286	0.0211	0.1	0.0567	0.0289	0.021	0.018	0.02	0.0879
2.25	0.99	0.0821	0.0307	0.0786	0.0383	0.0711	0.0199	0.0648	0.0259	0.0288	0.0212	0.1	0.0569	0.0291	0.0211	0.0182	0.02	0.0884
2.333	0.992	0.0829	0.0314	0.0794	0.0388	0.0715	0.02	0.0657	0.0262	0.0289	0.0213	0.1	0.0569	0.0293	0.0213	0.0183	0.02	0.0889
2.417	0.993	0.0836	0.032	0.0802	0.0393	0.072	0.0201	0.0666	0.0264	0.0291	0.0214	0.1	0.057	0.0294	0.0215	0.0185	0.02	0.0894
2.5	0.995	0.0844	0.0326	0.081	0.0397	0.0724	0.0203	0.0676	0.0266	0.0293	0.0214	0.1	0.057	0.0296	0.0217	0.0187	0.02	0.09
2.583	0.997	0.0853	0.0332	0.0819	0.0403	0.0728	0.0204	0.0686	0.0269	0.0294	0.0215	0.1	0.057	0.0298	0.0219	0.0189	0.02	0.0906
2.667	1	0.0861	0.0338	0.0828	0.0408	0.0733	0.0205	0.0696	0.0271	0.0295	0.0215	0.1	0.057	0.03	0.022	0.0191	0.02	0.0911
2.75	1.002	0.087	0.0344	0.0837	0.0413	0.0737	0.0207	0.0706	0.0274	0.0297	0.0216	0.1	0.057	0.0302	0.0222	0.0193	0.02	0.0917
2.833	1.004	0.0879	0.0349	0.0847	0.0419	0.0742	0.0208	0.0718	0.0277	0.0298	0.0216	0.1	0.057	0.0304	0.0225	0.0195	0.02	0.0924
2.917	1.006	0.0889	0.0354	0.0856	0.0425	0.0747	0.021	0.0729	0.028	0.0299	0.0216	0.1	0.057	0.0306	0.0227	0.0197	0.02	0.093
3	1.009	0.0898	0.0359	0.0866	0.0431	0.0752	0.0212	0.074	0.0282	0.03	0.0216	0.1	0.057	0.0308	0.0229	0.0199	0.02	0.0936
3.083	1.011	0.0908	0.0364	0.0877	0.0437	0.0757	0.0213	0.0752	0.0286	0.0301	0.0217	0.1	0.0571	0.0311	0.0231	0.0202	0.02	0.0944
3.167	1.014	0.0919	0.0369	0.0887	0.0443	0.0763	0.0215	0.0765	0.0289	0.0302	0.0217	0.1	0.0572	0.0313	0.0234	0.0204	0.02	0.0951
3.25	1.016	0.0929	0.0374	0.0898	0.045	0.0768	0.0217	0.0777	0.0292	0.0303	0.0217	0.1	0.0573	0.0316	0.0236	0.0206	0.02	0.0958
3.333	1.019	0.0941	0.0379	0.091	0.0457	0.0775	0.0219	0.0789	0.0295	0.0305	0.0218	0.1	0.0576	0.0318	0.0239	0.0209	0.02	0.0966

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
3.417	1.022	0.0952	0.0384	0.0922	0.0464	0.0781	0.022	0.0802	0.0299	0.0306	0.0219	0.1	0.058	0.0321	0.0241	0.0212	0.02	0.0974
3.5	1.024	0.0964	0.0389	0.0934	0.0471	0.0787	0.0222	0.0814	0.0302	0.0307	0.0219	0.1	0.0583	0.0323	0.0244	0.0214	0.02	0.0981
3.583	1.027	0.0977	0.0394	0.0947	0.0479	0.0794	0.0225	0.0826	0.0306	0.0309	0.0221	0.1	0.0588	0.0326	0.0247	0.0217	0.02	0.099
3.667	1.03	0.099	0.0399	0.096	0.0487	0.08	0.0227	0.0839	0.031	0.031	0.0222	0.1	0.0593	0.0329	0.025	0.022	0.02	0.0999
3.75	1.033	0.1	0.0403	0.0974	0.0495	0.0807	0.0229	0.0851	0.0314	0.0312	0.0223	0.1	0.0598	0.0332	0.0253	0.0223	0.02	0.1008
3.833	1.036	0.102	0.0408	0.0988	0.0503	0.0814	0.0231	0.0863	0.0318	0.0313	0.0225	0.1	0.0604	0.0335	0.0256	0.0226	0.02	0.1017
3.917	1.039	0.103	0.0413	0.1	0.0512	0.0822	0.0233	0.0875	0.0322	0.0315	0.0227	0.1	0.0609	0.0338	0.0259	0.0229	0.02	0.1026
4	1.043	0.104	0.0418	0.102	0.0521	0.0829	0.0236	0.0887	0.0326	0.0317	0.0228	0.1	0.0614	0.0342	0.0262	0.0232	0.02	0.1036
4.083	1.046	0.106	0.0422	0.103	0.053	0.0837	0.0238	0.09	0.033	0.0318	0.023	0.1	0.0618	0.0345	0.0265	0.0236	0.02	0.1046
4.167	1.049	0.108	0.0427	0.105	0.0539	0.0845	0.0241	0.0912	0.0335	0.032	0.0231	0.1	0.0622	0.0349	0.0269	0.0239	0.02	0.1057
4.25	1.053	0.109	0.0432	0.106	0.0549	0.0853	0.0243	0.0924	0.0339	0.0322	0.0233	0.1	0.0626	0.0352	0.0272	0.0243	0.02	0.1067
4.333	1.056	0.111	0.0437	0.108	0.0559	0.0862	0.0246	0.0936	0.0343	0.0324	0.0234	0.1	0.0629	0.0356	0.0276	0.0246	0.02	0.1078
4.417	1.06	0.112	0.0442	0.11	0.0569	0.087	0.0249	0.0948	0.0347	0.0325	0.0235	0.1	0.0632	0.0359	0.028	0.025	0.02	0.1089
4.5	1.063	0.114	0.0447	0.112	0.0578	0.0879	0.0252	0.096	0.0351	0.0327	0.0236	0.1	0.0634	0.0363	0.0284	0.0254	0.02	0.1101
4.583	1.067	0.116	0.0452	0.113	0.0588	0.0888	0.0255	0.0972	0.0355	0.0329	0.0237	0.1	0.0637	0.0367	0.0288	0.0258	0.02	0.1113
4.667	1.071	0.118	0.0457	0.115	0.0598	0.0897	0.0258	0.0984	0.036	0.033	0.0238	0.1	0.0639	0.0371	0.0292	0.0262	0.02	0.1125
4.75	1.075	0.119	0.0462	0.117	0.0608	0.0906	0.0261	0.0996	0.0364	0.0331	0.0239	0.1	0.0641	0.0375	0.0296	0.0266	0.02	0.1137
4.833	1.079	0.121	0.0468	0.119	0.0618	0.0916	0.0264	0.101	0.0368	0.0333	0.024	0.1	0.0642	0.0379	0.03	0.027	0.02	0.1149
4.917	1.083	0.123	0.0473	0.121	0.0628	0.0926	0.0267	0.102	0.0372	0.0334	0.024	0.1	0.0644	0.0384	0.0304	0.0274	0.02	0.1162
5	1.087	0.125	0.0478	0.123	0.0638	0.0936	0.027	0.103	0.0376	0.0335	0.0241	0.1	0.0645	0.0388	0.0308	0.0279	0.02	0.1175
5.083	1.091	0.126	0.0484	0.125	0.0648	0.0946	0.0273	0.104	0.038	0.0336	0.0241	0.1	0.0646	0.0392	0.0313	0.0283	0.02	0.1188
5.167	1.096	0.128	0.0489	0.127	0.0658	0.0957	0.0276	0.106	0.0384	0.0337	0.0242	0.1	0.0647	0.0397	0.0317	0.0288	0.02	0.1202
5.25	1.1	0.13	0.0494	0.129	0.0668	0.0967	0.0279	0.107	0.0389	0.0338	0.0243	0.1	0.0648	0.0401	0.0322	0.0292	0.02	0.1215
5.333	1.104	0.132	0.0499	0.131	0.0678	0.0978	0.0282	0.108	0.0393	0.0339	0.0243	0.1	0.0648	0.0406	0.0326	0.0297	0.0202	0.1231
5.417	1.109	0.133	0.0504	0.133	0.0688	0.0989	0.0285	0.109	0.0397	0.034	0.0243	0.1	0.0648	0.041	0.0331	0.0301	0.0203	0.1245
5.5	1.113	0.135	0.0509	0.135	0.0698	0.1	0.0288	0.11	0.0401	0.0341	0.0244	0.1	0.0649	0.0415	0.0335	0.0306	0.0205	0.1261
5.583	1.118	0.137	0.0514	0.137	0.0708	0.101	0.0291	0.111	0.0405	0.0341	0.0244	0.1	0.0649	0.0419	0.034	0.031	0.021	0.1279
5.667	1.123	0.139	0.0518	0.139	0.0718	0.102	0.0294	0.113	0.0409	0.0342	0.0244	0.1	0.0649	0.0424	0.0344	0.0315	0.0214	0.1297
5.75	1.127	0.141	0.0523	0.141	0.0728	0.104	0.0297	0.114	0.0413	0.0343	0.0244	0.1	0.0649	0.0428	0.0349	0.0319	0.0219	0.1315
5.833	1.132	0.142	0.0526	0.144	0.0737	0.105	0.03	0.115	0.0417	0.0343	0.0245	0.1	0.0649	0.0433	0.0353	0.0324	0.0223	0.1333
5.917	1.137	0.144	0.053	0.146	0.0747	0.106	0.0303	0.116	0.0421	0.0344	0.0245	0.1	0.0649	0.0437	0.0358	0.0328	0.0228	0.1351
6	1.142	0.146	0.0534	0.148	0.0757	0.107	0.0306	0.117	0.0425	0.0345	0.0245	0.1	0.0649	0.0442	0.0362	0.0333	0.0232	0.1369
6.083	1.148	0.147	0.0538	0.15	0.0767	0.108	0.0309	0.118	0.0429	0.0345	0.0245	0.1	0.0649	0.0446	0.0367	0.0337	0.0236	0.1386
6.167	1.153	0.149	0.0541	0.152	0.0777	0.11	0.0312	0.119	0.0433	0.0346	0.0245	0.1	0.0649	0.0451	0.0371	0.0342	0.0241	0.1405
6.25	1.158	0.151	0.0545	0.154	0.0786	0.111	0.0315	0.121	0.0437	0.0346	0.0245	0.1	0.0649	0.0455	0.0376	0.0346	0.0245	0.1422
6.333	1.163	0.153	0.0548	0.156	0.0796	0.112	0.0318	0.122	0.0441	0.0346	0.0245	0.1	0.0649	0.046	0.038	0.0351	0.025	0.1441
6.417	1.169	0.154	0.055	0.158	0.0806	0.114	0.0321	0.123	0.0445	0.0347	0.0245	0.1	0.0649	0.0464	0.0385	0.0355	0.0254	0.1458
6.5	1.174	0.156	0.0553	0.16	0.0816	0.115	0.0324	0.124	0.0449	0.0347	0.0245	0.1	0.0649	0.0468	0.0389	0.0359	0.0259	0.1475
6.583	1.18	0.158	0.0556	0.162	0.0825	0.117	0.0327	0.125	0.0453	0.0348	0.0245	0.1	0.0649	0.0473	0.0393	0.0364	0.0263	0.1493
6.667	1.186	0.16	0.0558	0.164	0.0835	0.118	0.033	0.126	0.0457	0.0348	0.0245	0.1	0.0649	0.0477	0.0398	0.0368	0.0268	0.1511
6.75	1.191	0.161	0.0561	0.166	0.0845	0.119	0.0333	0.127	0.0461	0.0348	0.0245	0.1	0.0649	0.0482	0.0402	0.0373	0.0272	0.1529
6.833	1.197	0.163	0.0563	0.168	0.0854	0.121	0.0336	0.128	0.0465	0.0348	0.0245	0.1	0.0649	0.0486	0.0407	0.0377	0.0276	0.1546
6.917	1.203	0.165	0.0565	0.17	0.0864	0.122	0.0339	0.129	0.0469	0.0349	0.0245	0.1	0.0649	0.049	0.0411	0.0381	0.0281	0.1563
7	1.209	0.167	0.0567	0.172	0.0873	0.124	0.0342	0.13	0.0473	0.0349	0.0245	0.1	0.0649	0.0495	0.0415	0.0386	0.0285	0.1581
7.083	1.215	0.168	0.0569	0.174	0.0883	0.125	0.0345	0.131	0.0477	0.0349	0.0245	0.1	0.0649	0.0499	0.042	0.039	0.029	0.1599
7.167	1.221	0.17	0.057	0.176	0.0893	0.127	0.0348	0.132	0.0481	0.0349	0.0245	0.1	0.0649	0.0504	0.0424	0.0395	0.0294	0.1617
7.25	1.228	0.172	0.0572	0.178	0.0902	0.128	0.0351	0.133	0.0484	0.0349	0.0245	0.1	0.0649	0.0508	0.0429	0.0399	0.0298	0.1634
7.333	1.234	0.173	0.0573	0.18	0.0912	0.13	0.0354	0.133	0.0488	0.0349	0.0245	0.1	0.0649	0.0512	0.0433	0.0403	0.0303	0.1651
7.417	1.241	0.175	0.0574	0.182	0.0921	0.131	0.0357	0.134	0.0492	0.0349	0.0245	0.1	0.0649	0.0517	0.0437	0.0408	0.0307	0.1669
7.5	1.247	0.177	0.0576	0.184	0.093	0.133	0.036	0.135	0.0495	0.0349	0.0245	0.1	0.0649	0.0521	0.0442	0.0412	0.0312	0.1687
7.583	1.254	0.179	0.0577	0.186	0.094	0.134	0.0363	0.136	0.0498	0.0349	0.0245	0.1	0.0649	0.0525	0.0446	0.0416	0.0316	0.1703
7.667	1.26	0.18	0.0578	0.188	0.0949	0.136	0.0366	0.137	0.0502	0.0349	0.0245	0.1	0.0649	0.053	0.045	0.0421	0.032	0.1721
7.75	1.267	0.182	0.0579	0.19	0.0958	0.137	0.0369	0.138	0.0505	0.0349	0.0245	0.1	0.0649	0.0534	0.0455	0.0425	0.0325	0.1739
7.833	1.274	0.184	0.058	0.192	0.0966	0.139	0.0372	0.138	0.0508	0.0349	0.0245	0.1	0.0649	0.0538	0.0459	0.0429	0.0329	0.1755
7.917	1.281	0.185	0.0581	0.194	0.0975	0.14	0.0374	0.139	0.0512	0.0349	0.0245	0.1	0.0649	0.0543	0.0463	0.0434	0.0333	0.1773
8	1.288	0.187	0.0583	0.196	0.0984	0.142	0.0377	0.14	0.0515	0.0349	0.0245	0.1	0.0649	0.0547	0.0468	0.0438	0.0338	0.1791
8.083	1.295	0.188	0.0584	0.198	0.0992	0.143	0.038	0.141	0.0518	0.0349	0.0245	0.1	0.0649	0.0551	0.0472	0.0442	0.0342	0.1807
8.167	1.302	0.19	0.0584	0.2	0.1	0.145	0.0383	0.141	0.0521	0.0349	0.0245	0.1	0.0649	0.0556	0.0476	0.0447	0.0346	0.1825
8.25	1.31	0.192	0.0585	0.202	0.101	0.146	0.0386	0.142	0.0524	0.0349	0.0245	0.1	0.0649	0.056	0.048	0.0451	0.035	0.1841
8.333	1.317	0.193	0.0586	0.204	0.102	0.148	0.0388	0.143	0.0527	0.0349	0.0245	0.1	0.0649	0.0564	0.0485	0.0455	0.0355	0.1859
8.417	1.325	0.195	0.0587	0.206	0.102	0.149	0.0391	0.143	0.0529	0.0349	0.0245	0.1	0.0649	0.0568	0.0489	0.0459	0.0359	0.1875
8.5	1.332	0.196	0.0588	0.208	0.103	0.15	0.0394	0.144	0.0532	0.0349	0.0245	0.1	0.0649	0.0572	0.0493	0.0463	0.0363	0.1891
8.583	1.34	0.198	0.0589	0.21	0.104	0.152	0.0396	0.145	0.0535	0.0349	0.0245	0.1	0.0649	0.0576	0.0497	0.0467	0.0367	0.1907
8.667	1.347	0.199	0.059	0.211	0.105	0.153	0.0399	0.145	0.0538	0.0349	0.0245	0.1	0.0649	0.058	0.0501	0.0471	0.0371	0.1923
8.75	1.355	0.2	0.059	0.213	0.105	0.155	0.0401	0.146	0.054	0.0349	0.0245	0.1	0.0649	0.0584	0.0505	0.0475	0.0375	0.1939
8.833	1.363	0.202	0.0591	0.215	0.106	0.156	0.0404	0.146	0.0543	0.0349	0.0245	0.1	0.0649	0.0588	0.0509	0.0479	0.0379	0.1955
8.917	1.371	0.203	0.0592	0.217	0.107	0.158	0.0406	0.147	0.0546	0.0349	0.0245	0.1	0.0649	0.0592	0.0512	0.0483	0.0383	0.197

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
9	1.379	0.204	0.0592	0.218	0.108	0.159	0.0408	0.147	0.0548	0.0349	0.0245	0.1	0.0649	0.0596	0.0516	0.0487	0.0386	0.1985
9.083	1.388	0.206	0.0593	0.22	0.108	0.161	0.0411	0.148	0.0551	0.0349	0.0245	0.1	0.065	0.0599	0.052	0.0491	0.039	0.2
9.167	1.396	0.207	0.0594	0.222	0.109	0.162	0.0413	0.148	0.0553	0.035	0.0245	0.1	0.065	0.0603	0.0524	0.0494	0.0394	0.2015
9.25	1.404	0.208	0.0594	0.224	0.11	0.164	0.0415	0.149	0.0556	0.035	0.0245	0.1	0.0651	0.0607	0.0527	0.0498	0.0398	0.203
9.333	1.413	0.21	0.0595	0.225	0.11	0.165	0.0417	0.149	0.0559	0.035	0.0246	0.1	0.0654	0.061	0.0531	0.0502	0.0401	0.2044
9.417	1.421	0.211	0.0596	0.227	0.111	0.167	0.042	0.15	0.0561	0.0351	0.0247	0.1	0.0656	0.0614	0.0535	0.0505	0.0405	0.2059
9.5	1.43	0.212	0.0597	0.229	0.112	0.168	0.0422	0.15	0.0564	0.0351	0.0247	0.1	0.0659	0.0618	0.0538	0.0509	0.0408	0.2073
9.583	1.439	0.213	0.0598	0.23	0.112	0.169	0.0424	0.151	0.0566	0.0352	0.0248	0.1	0.0664	0.0621	0.0542	0.0512	0.0412	0.2087
9.667	1.448	0.215	0.06	0.232	0.113	0.171	0.0426	0.152	0.0569	0.0353	0.025	0.1	0.0669	0.0625	0.0545	0.0516	0.0416	0.2102
9.75	1.456	0.216	0.0601	0.233	0.114	0.172	0.0429	0.152	0.0571	0.0353	0.0251	0.1	0.0674	0.0628	0.0549	0.052	0.0419	0.2116
9.833	1.466	0.217	0.0602	0.235	0.114	0.174	0.0431	0.153	0.0574	0.0355	0.0252	0.1	0.0679	0.0632	0.0552	0.0523	0.0423	0.213
9.917	1.475	0.219	0.0604	0.237	0.115	0.175	0.0433	0.153	0.0576	0.0356	0.0254	0.1	0.0684	0.0635	0.0556	0.0526	0.0426	0.2143
10	1.484	0.22	0.0606	0.238	0.116	0.177	0.0435	0.154	0.0579	0.0357	0.0256	0.1	0.0689	0.0639	0.0559	0.053	0.043	0.2158
10.083	1.493	0.221	0.0608	0.24	0.116	0.178	0.0438	0.154	0.0581	0.0358	0.0257	0.1	0.0694	0.0642	0.0563	0.0533	0.0433	0.2171
10.167	1.503	0.222	0.0609	0.241	0.117	0.18	0.044	0.155	0.0584	0.036	0.0259	0.1	0.0698	0.0645	0.0566	0.0537	0.0437	0.2185
10.25	1.512	0.224	0.0611	0.243	0.118	0.181	0.0442	0.155	0.0586	0.0361	0.026	0.1	0.0702	0.0649	0.057	0.054	0.044	0.2199
10.333	1.522	0.225	0.0614	0.245	0.118	0.183	0.0444	0.156	0.0589	0.0363	0.0262	0.1	0.0705	0.0652	0.0573	0.0544	0.0443	0.2212
10.417	1.532	0.226	0.0616	0.246	0.119	0.184	0.0446	0.156	0.0591	0.0365	0.0263	0.1	0.0708	0.0656	0.0576	0.0547	0.0447	0.2226
10.5	1.541	0.227	0.0618	0.248	0.12	0.186	0.0449	0.157	0.0594	0.0366	0.0264	0.1	0.0711	0.0659	0.058	0.055	0.045	0.2239
10.583	1.551	0.229	0.0621	0.249	0.12	0.187	0.0451	0.157	0.0596	0.0368	0.0265	0.101	0.0713	0.0662	0.0583	0.0554	0.0454	0.2253
10.667	1.561	0.23	0.0624	0.251	0.121	0.189	0.0453	0.158	0.0599	0.0369	0.0266	0.101	0.0716	0.0666	0.0587	0.0557	0.0457	0.2267
10.75	1.571	0.231	0.0626	0.252	0.122	0.19	0.0455	0.158	0.0601	0.0371	0.0267	0.102	0.0718	0.0669	0.059	0.056	0.046	0.2279
10.833	1.582	0.232	0.0629	0.254	0.122	0.192	0.0457	0.159	0.0604	0.0372	0.0268	0.102	0.0719	0.0672	0.0593	0.0564	0.0464	0.2293
10.917	1.592	0.234	0.0633	0.255	0.123	0.193	0.046	0.16	0.0606	0.0373	0.0268	0.102	0.0721	0.0676	0.0597	0.0567	0.0467	0.2307
11	1.602	0.235	0.0636	0.257	0.124	0.195	0.0462	0.16	0.0608	0.0375	0.0269	0.103	0.0723	0.0679	0.06	0.057	0.047	0.2319
11.083	1.613	0.236	0.0639	0.259	0.124	0.196	0.0464	0.161	0.0611	0.0376	0.027	0.103	0.0724	0.0682	0.0603	0.0574	0.0474	0.2333
11.167	1.624	0.237	0.0642	0.26	0.125	0.197	0.0466	0.161	0.0613	0.0377	0.027	0.103	0.0725	0.0686	0.0607	0.0577	0.0477	0.2347
11.25	1.634	0.239	0.0646	0.262	0.126	0.199	0.0468	0.162	0.0616	0.0378	0.0271	0.104	0.0726	0.0689	0.061	0.0581	0.048	0.236
11.333	1.645	0.24	0.0649	0.263	0.126	0.2	0.0471	0.162	0.0618	0.0379	0.0271	0.104	0.0726	0.0693	0.0613	0.0584	0.0484	0.2374
11.417	1.656	0.241	0.0652	0.265	0.127	0.202	0.0473	0.163	0.0621	0.0379	0.0271	0.104	0.0727	0.0696	0.0617	0.0587	0.0487	0.2387
11.5	1.667	0.242	0.0655	0.266	0.128	0.203	0.0475	0.164	0.0623	0.038	0.0272	0.105	0.0727	0.0699	0.062	0.0591	0.049	0.24
11.583	1.678	0.244	0.0658	0.268	0.128	0.204	0.0477	0.164	0.0626	0.0381	0.0272	0.105	0.0727	0.0703	0.0623	0.0594	0.0494	0.2414
11.667	1.689	0.245	0.0661	0.269	0.129	0.206	0.0479	0.165	0.0628	0.0382	0.0272	0.105	0.0727	0.0706	0.0627	0.0597	0.0497	0.2427
11.75	1.701	0.246	0.0664	0.271	0.129	0.207	0.0481	0.166	0.0631	0.0382	0.0273	0.105	0.0727	0.0709	0.063	0.0601	0.0501	0.2441
11.833	1.712	0.247	0.0667	0.272	0.13	0.209	0.0484	0.166	0.0633	0.0383	0.0273	0.105	0.0727	0.0713	0.0633	0.0604	0.0504	0.2454
11.917	1.724	0.248	0.067	0.274	0.131	0.21	0.0486	0.167	0.0636	0.0384	0.0273	0.106	0.0727	0.0716	0.0637	0.0607	0.0507	0.2467
12	1.735	0.25	0.0673	0.275	0.131	0.211	0.0488	0.168	0.0638	0.0384	0.0273	0.106	0.0727	0.0719	0.064	0.0611	0.0511	0.2481
12.083	1.747	0.251	0.0675	0.277	0.132	0.213	0.049	0.168	0.0641	0.0385	0.0273	0.106	0.0727	0.0723	0.0643	0.0614	0.0514	0.2494
12.167	1.759	0.252	0.0678	0.278	0.133	0.214	0.0492	0.169	0.0644	0.0385	0.0273	0.106	0.0727	0.0726	0.0647	0.0617	0.0517	0.2507
12.25	1.771	0.253	0.068	0.28	0.133	0.215	0.0494	0.17	0.0646	0.0386	0.0273	0.106	0.0727	0.0729	0.065	0.0621	0.0521	0.2521
12.333	1.783	0.255	0.0682	0.282	0.134	0.217	0.0496	0.17	0.0649	0.0386	0.0273	0.106	0.0727	0.0733	0.0653	0.0624	0.0524	0.2534
12.417	1.795	0.256	0.0684	0.283	0.135	0.218	0.0499	0.171	0.0651	0.0387	0.0273	0.106	0.0727	0.0736	0.0657	0.0627	0.0527	0.2547
12.5	1.807	0.257	0.0687	0.285	0.135	0.219	0.0501	0.172	0.0654	0.0387	0.0273	0.106	0.0727	0.0739	0.066	0.0631	0.0531	0.2561
12.583	1.82	0.258	0.0689	0.286	0.136	0.221	0.0503	0.172	0.0657	0.0387	0.0273	0.106	0.0727	0.0743	0.0663	0.0634	0.0534	0.2574
12.667	1.832	0.259	0.0691	0.288	0.137	0.222	0.0505	0.173	0.0659	0.0388	0.0273	0.107	0.0727	0.0746	0.0667	0.0637	0.0537	0.2587
12.75	1.845	0.261	0.0692	0.289	0.137	0.223	0.0507	0.174	0.0662	0.0388	0.0273	0.107	0.0727	0.0749	0.067	0.0641	0.0541	0.2601
12.833	1.858	0.262	0.0694	0.291	0.138	0.225	0.0509	0.174	0.0665	0.0388	0.0273	0.107	0.0727	0.0753	0.0673	0.0644	0.0544	0.2614
12.917	1.871	0.263	0.0696	0.292	0.139	0.226	0.0511	0.175	0.0667	0.0389	0.0273	0.107	0.0727	0.0756	0.0677	0.0647	0.0547	0.2627
13	1.883	0.264	0.0698	0.294	0.14	0.227	0.0514	0.176	0.067	0.0389	0.0273	0.107	0.0727	0.0759	0.068	0.0651	0.0551	0.2641
13.083	1.897	0.266	0.0699	0.295	0.14	0.228	0.0516	0.176	0.0672	0.0389	0.0273	0.107	0.0727	0.0762	0.0683	0.0654	0.0554	0.2653
13.167	1.91	0.267	0.0701	0.297	0.141	0.23	0.0518	0.177	0.0675	0.0389	0.0273	0.107	0.0727	0.0766	0.0687	0.0657	0.0557	0.2667
13.25	1.923	0.268	0.0702	0.298	0.142	0.231	0.052	0.177	0.0678	0.0389	0.0273	0.107	0.0727	0.0769	0.069	0.0661	0.0561	0.2681
13.333	1.936	0.269	0.0703	0.3	0.142	0.232	0.0522	0.178	0.068	0.0389	0.0273	0.107	0.0727	0.0772	0.0693	0.0664	0.0564	0.2693
13.417	1.95	0.271	0.0705	0.301	0.143	0.233	0.0524	0.178	0.0682	0.0389	0.0273	0.107	0.0727	0.0776	0.0697	0.0667	0.0567	0.2707
13.5	1.963	0.272	0.0706	0.303	0.144	0.235	0.0527	0.179	0.0685	0.0389	0.0273	0.107	0.0727	0.0779	0.07	0.067	0.057	0.2719
13.583	1.977	0.273	0.0707	0.304	0.144	0.236	0.0529	0.179	0.0687	0.0389	0.0273	0.107	0.0727	0.0782	0.0703	0.0674	0.0574	0.2733
13.667	1.991	0.274	0.0708	0.306	0.145	0.237	0.0531	0.18	0.0689	0.0389	0.0273	0.107	0.0727	0.0786	0.0706	0.0677	0.0577	0.2746
13.75	2.005	0.276	0.071	0.307	0.146	0.238	0.0533	0.18	0.0691	0.0389	0.0273	0.107	0.0727	0.0789	0.071	0.068	0.058	0.2759
13.833	2.019	0.277	0.0711	0.309	0.146	0.239	0.0535	0.181	0.0693	0.0389	0.0273	0.107	0.0727	0.0792	0.0713	0.0684	0.0584	0.2773
13.917	2.033	0.278	0.0712	0.31	0.147	0.241	0.0538	0.181	0.0695	0.0389	0.0273	0.107	0.0727	0.0795	0.0716	0.0687	0.0587	0.2785
14	2.047	0.279	0.0713	0.312	0.148	0.242	0.054	0.182	0.0697	0.0389	0.0273	0.107	0.0727	0.0799	0.072	0.069	0.059	0.2799
14.083	2.062	0.281	0.0714	0.313	0.148	0.243	0.0542	0.182	0.0699	0.0389	0.0273	0.107	0.0727	0.0802	0.0723	0.0694	0.0594	0.2813
14.167	2.076	0.282	0.0715	0.315	0.149	0.244	0.0544	0.182	0.0701	0.0389	0.0273	0.107	0.0727	0.0805	0.0726	0.0697	0.0597	0.2825
14.25	2.091	0.283	0.0716	0.316	0.149	0.245	0.0546	0.183	0.0703	0.0389	0.0273	0.107	0.0727	0.0809	0.073	0.07	0.06	0.2839
14.333	2.106	0.284	0.0717	0.318	0.15	0.247	0.0548	0.183	0.0705	0.0389	0.0273	0.107	0.0727	0.0812	0.0733	0.0704	0.0604	0.2853
14.417	2.121	0.285	0.0718	0.319	0.15	0.248	0.055	0.184	0.0707	0.0389	0.0273	0.107	0.0727	0.0815	0.0736	0.0707	0.0607	0.2865
14.5	2.136	0.286	0.0719	0.321	0.151	0.249	0.0552	0.184	0.0709	0.0389	0.0273	0.107	0.0727	0.0818	0.0739	0.071	0.061	0.2877

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
14.583	2.151	0.287	0.072	0.322	0.151	0.25	0.0554	0.184	0.071	0.0389	0.0273	0.107	0.0727	0.0822	0.0743	0.0713	0.0613	0.2891
14.667	2.166	0.289	0.072	0.324	0.152	0.251	0.0556	0.185	0.0712	0.0389	0.0273	0.107	0.0727	0.0825	0.0746	0.0716	0.0617	0.2904
14.75	2.181	0.29	0.0721	0.325	0.153	0.252	0.0558	0.185	0.0714	0.0389	0.0273	0.107	0.0727	0.0828	0.0749	0.072	0.062	0.2917
14.833	2.197	0.291	0.0722	0.327	0.153	0.253	0.056	0.185	0.0715	0.0389	0.0273	0.107	0.0727	0.0831	0.0752	0.0723	0.0623	0.2929
14.917	2.212	0.292	0.0723	0.328	0.153	0.255	0.0562	0.186	0.0717	0.0389	0.0273	0.107	0.0727	0.0834	0.0755	0.0726	0.0626	0.2941
15	2.228	0.293	0.0723	0.329	0.154	0.256	0.0564	0.186	0.0719	0.0389	0.0273	0.107	0.0727	0.0837	0.0758	0.0729	0.0629	0.2953
15.083	2.244	0.294	0.0724	0.331	0.154	0.257	0.0565	0.186	0.072	0.0389	0.0273	0.107	0.0727	0.084	0.0761	0.0731	0.0632	0.2964
15.167	2.26	0.295	0.0724	0.332	0.155	0.258	0.0567	0.186	0.0722	0.0389	0.0273	0.107	0.0727	0.0843	0.0764	0.0734	0.0634	0.2975
15.25	2.276	0.296	0.0725	0.333	0.155	0.259	0.0569	0.187	0.0723	0.0389	0.0273	0.107	0.0727	0.0845	0.0766	0.0737	0.0637	0.2985
15.333	2.292	0.297	0.0725	0.335	0.156	0.26	0.057	0.187	0.0725	0.0389	0.0273	0.107	0.0727	0.0848	0.0769	0.074	0.064	0.2997
15.417	2.309	0.297	0.0726	0.336	0.156	0.261	0.0572	0.187	0.0726	0.0389	0.0273	0.107	0.0727	0.0851	0.0772	0.0743	0.0643	0.3009
15.5	2.325	0.298	0.0726	0.337	0.157	0.262	0.0574	0.187	0.0728	0.0389	0.0273	0.107	0.0727	0.0854	0.0775	0.0745	0.0646	0.302
15.583	2.342	0.299	0.0726	0.338	0.157	0.263	0.0575	0.188	0.0729	0.0389	0.0273	0.107	0.0727	0.0856	0.0777	0.0748	0.0648	0.3029
15.667	2.358	0.3	0.0727	0.34	0.157	0.264	0.0577	0.188	0.073	0.0389	0.0273	0.107	0.0727	0.0859	0.078	0.0751	0.0651	0.3041
15.75	2.375	0.301	0.0727	0.341	0.158	0.265	0.0579	0.188	0.0731	0.0389	0.0273	0.107	0.0727	0.0862	0.0783	0.0753	0.0654	0.3052
15.833	2.392	0.302	0.0727	0.342	0.158	0.267	0.058	0.188	0.0733	0.0389	0.0273	0.107	0.0727	0.0864	0.0785	0.0756	0.0656	0.3061
15.917	2.409	0.302	0.0727	0.343	0.158	0.268	0.0581	0.189	0.0734	0.0389	0.0273	0.107	0.0727	0.0867	0.0788	0.0758	0.0658	0.3071
16	2.426	0.303	0.0728	0.344	0.159	0.269	0.0583	0.189	0.0735	0.0389	0.0273	0.107	0.0727	0.0869	0.079	0.0761	0.0661	0.3081
16.083	2.444	0.304	0.0728	0.345	0.159	0.27	0.0584	0.189	0.0736	0.0389	0.0273	0.107	0.0727	0.0871	0.0792	0.0763	0.0663	0.3089
16.167	2.461	0.305	0.0728	0.346	0.16	0.271	0.0586	0.189	0.0737	0.0389	0.0273	0.107	0.0727	0.0874	0.0795	0.0765	0.0666	0.31
16.25	2.479	0.305	0.0728	0.348	0.16	0.272	0.0587	0.189	0.0738	0.0389	0.0273	0.107	0.0727	0.0876	0.0797	0.0768	0.0668	0.3109
16.333	2.496	0.306	0.0728	0.349	0.16	0.273	0.0588	0.19	0.0739	0.0389	0.0273	0.107	0.0727	0.0878	0.0799	0.077	0.067	0.3117
16.417	2.514	0.307	0.0728	0.35	0.161	0.274	0.0589	0.19	0.074	0.0389	0.0273	0.107	0.0727	0.0881	0.0802	0.0772	0.0673	0.3128
16.5	2.532	0.307	0.0728	0.351	0.161	0.275	0.0591	0.19	0.0741	0.0389	0.0273	0.107	0.0727	0.0883	0.0804	0.0775	0.0675	0.3137
16.583	2.55	0.308	0.0728	0.352	0.161	0.275	0.0592	0.19	0.0742	0.0389	0.0273	0.107	0.0727	0.0885	0.0806	0.0777	0.0677	0.3145
16.667	2.569	0.309	0.0728	0.353	0.161	0.276	0.0593	0.19	0.0743	0.0389	0.0273	0.107	0.0727	0.0887	0.0808	0.0779	0.0679	0.3153
16.75	2.587	0.309	0.0728	0.354	0.162	0.277	0.0594	0.191	0.0744	0.0389	0.0273	0.107	0.0727	0.0889	0.081	0.0781	0.0681	0.3161
16.833	2.605	0.31	0.0728	0.355	0.162	0.278	0.0595	0.191	0.0745	0.0389	0.0273	0.107	0.0727	0.0891	0.0812	0.0783	0.0683	0.3169
16.917	2.624	0.311	0.0728	0.355	0.162	0.279	0.0596	0.191	0.0746	0.0389	0.0273	0.107	0.0727	0.0893	0.0814	0.0785	0.0685	0.3177
17	2.643	0.311	0.0728	0.356	0.163	0.28	0.0597	0.191	0.0746	0.0389	0.0273	0.107	0.0727	0.0895	0.0816	0.0787	0.0687	0.3185
17.083	2.662	0.312	0.0728	0.357	0.163	0.281	0.0598	0.191	0.0747	0.0389	0.0273	0.107	0.0727	0.0897	0.0818	0.0789	0.0689	0.3193
17.167	2.681	0.312	0.0728	0.358	0.163	0.281	0.0599	0.191	0.0748	0.0389	0.0273	0.107	0.0727	0.0899	0.082	0.0791	0.0691	0.3201
17.25	2.7	0.313	0.0728	0.359	0.163	0.282	0.06	0.192	0.0749	0.0389	0.0273	0.107	0.0727	0.0901	0.0822	0.0792	0.0693	0.3208
17.333	2.719	0.313	0.0728	0.36	0.164	0.283	0.0601	0.192	0.0749	0.0389	0.0273	0.107	0.0727	0.0902	0.0823	0.0794	0.0694	0.3213
17.417	2.739	0.314	0.0728	0.361	0.164	0.284	0.0602	0.192	0.075	0.0389	0.0273	0.107	0.0727	0.0904	0.0825	0.0796	0.0696	0.3221
17.5	2.758	0.314	0.0728	0.361	0.164	0.284	0.0603	0.192	0.0751	0.0389	0.0273	0.107	0.0727	0.0906	0.0827	0.0797	0.0698	0.3228
17.583	2.778	0.315	0.0728	0.362	0.164	0.285	0.0604	0.192	0.0751	0.0389	0.0273	0.107	0.0727	0.0907	0.0828	0.0799	0.0699	0.3233
17.667	2.798	0.315	0.0728	0.363	0.165	0.286	0.0605	0.192	0.0752	0.0389	0.0273	0.107	0.0727	0.0909	0.083	0.0801	0.0701	0.3241
17.75	2.818	0.316	0.0728	0.364	0.165	0.287	0.0606	0.193	0.0753	0.0389	0.0273	0.107	0.0727	0.0911	0.0832	0.0802	0.0703	0.3248
17.833	2.838	0.316	0.0728	0.364	0.165	0.287	0.0607	0.193	0.0753	0.0389	0.0273	0.107	0.0727	0.0912	0.0833	0.0804	0.0704	0.3253
17.917	2.858	0.317	0.0728	0.365	0.165	0.288	0.0607	0.193	0.0754	0.0389	0.0273	0.107	0.0727	0.0914	0.0835	0.0805	0.0706	0.326
18	2.878	0.317	0.0728	0.366	0.165	0.288	0.0608	0.193	0.0755	0.0389	0.0273	0.107	0.0727	0.0915	0.0836	0.0807	0.0707	0.3265
18.083	2.899	0.317	0.0728	0.366	0.166	0.289	0.0609	0.193	0.0755	0.0389	0.0273	0.107	0.0728	0.0916	0.0837	0.0808	0.0708	0.3269
18.167	2.919	0.318	0.0728	0.367	0.166	0.29	0.061	0.193	0.0756	0.039	0.0273	0.107	0.0728	0.0918	0.0839	0.0809	0.071	0.3276
18.25	2.939	0.318	0.0728	0.368	0.166	0.29	0.061	0.193	0.0757	0.039	0.0273	0.107	0.0729	0.0919	0.084	0.0811	0.0711	0.3281
18.333	2.959	0.319	0.0729	0.368	0.166	0.291	0.0611	0.193	0.0757	0.039	0.0274	0.107	0.0731	0.092	0.0841	0.0812	0.0713	0.3286
18.417	2.979	0.319	0.0729	0.369	0.166	0.292	0.0612	0.194	0.0758	0.039	0.0274	0.107	0.0733	0.0922	0.0843	0.0813	0.0714	0.3292
18.5	2.999	0.32	0.0729	0.369	0.167	0.292	0.0613	0.194	0.0759	0.0391	0.0275	0.107	0.0735	0.0923	0.0844	0.0815	0.0715	0.3297
18.583	3.019	0.32	0.073	0.37	0.167	0.293	0.0614	0.194	0.076	0.0391	0.0276	0.107	0.0739	0.0924	0.0846	0.0816	0.0717	0.3303
18.667	3.039	0.32	0.0731	0.371	0.167	0.293	0.0614	0.194	0.076	0.0392	0.0277	0.108	0.0743	0.0926	0.0847	0.0818	0.0718	0.3309
18.75	3.059	0.321	0.0732	0.371	0.167	0.294	0.0615	0.194	0.0761	0.0393	0.0278	0.108	0.0747	0.0927	0.0848	0.0819	0.0719	0.3313
18.833	3.079	0.321	0.0733	0.372	0.167	0.295	0.0616	0.194	0.0762	0.0394	0.028	0.108	0.0752	0.0929	0.085	0.082	0.0721	0.332
18.917	3.099	0.322	0.0734	0.373	0.168	0.295	0.0617	0.195	0.0763	0.0395	0.0281	0.109	0.0758	0.093	0.0851	0.0822	0.0722	0.3325
19	3.119	0.322	0.0736	0.373	0.168	0.296	0.0617	0.195	0.0764	0.0396	0.0283	0.109	0.0763	0.0931	0.0852	0.0823	0.0723	0.3329
19.083	3.139	0.323	0.0737	0.374	0.168	0.296	0.0618	0.195	0.0765	0.0397	0.0284	0.11	0.0768	0.0933	0.0854	0.0824	0.0725	0.3336
19.167	3.159	0.323	0.0739	0.374	0.168	0.297	0.0619	0.195	0.0766	0.0399	0.0286	0.111	0.0772	0.0934	0.0855	0.0826	0.0726	0.3341
19.25	3.179	0.324	0.0741	0.375	0.169	0.298	0.062	0.196	0.0767	0.04	0.0287	0.111	0.0777	0.0935	0.0856	0.0827	0.0728	0.3346
19.333	3.198	0.324	0.0743	0.376	0.169	0.298	0.0621	0.196	0.0768	0.0402	0.0289	0.112	0.0781	0.0937	0.0858	0.0829	0.0729	0.3353
19.417	3.218	0.325	0.0745	0.376	0.169	0.299	0.0622	0.196	0.0769	0.0403	0.029	0.112	0.0784	0.0938	0.0859	0.083	0.073	0.3357
19.5	3.238	0.325	0.0747	0.377	0.169	0.299	0.0623	0.197	0.077	0.0405	0.0291	0.113	0.0787	0.094	0.0861	0.0831	0.0732	0.3364
19.583	3.258	0.326	0.075	0.378	0.17	0.3	0.0624	0.197	0.0771	0.0406	0.0292	0.113	0.079	0.0941	0.0862	0.0833	0.0733	0.3369
19.667	3.277	0.326	0.0752	0.378	0.17	0.301	0.0624	0.197	0.0772	0.0408	0.0294	0.114	0.0792	0.0942	0.0864	0.0834	0.0735	0.3375
19.75	3.297	0.327	0.0755	0.379	0.17	0.301	0.0625	0.197	0.0774	0.0409	0.0295	0.115	0.0795	0.0944	0.0865	0.0836	0.0736	0.3381
19.833	3.317	0.327	0.0758	0.38	0.17	0.302	0.0626	0.198	0.0775	0.0411	0.0295	0.115	0.0796	0.0945	0.0866	0.0837	0.0738	0.3386
19.917	3.336	0.328	0.0761	0.38	0.171	0.302	0.0627	0.198	0.0776	0.0412	0.0296	0.115	0.0798	0.0947	0.0868	0.0839	0.0739	0.3393
20	3.356	0.328	0.0764	0.381	0.171	0.303	0.0628	0.199	0.0777	0.0413	0.0297	0.116	0.08	0.0948	0.0869	0.084	0.0741	0.3398
20.083	3.375	0.329	0.0767	0.382	0.171	0.304	0.0629	0.199	0.0779	0.0415	0.0297	0.116	0.0801	0.095	0.0871	0.0842	0.0742	0.3405

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
20.167	3.395	0.329	0.0771	0.383	0.172	0.304	0.063	0.199	0.078	0.0416	0.0298	0.117	0.0802	0.0951	0.0872	0.0843	0.0744	0.341
20.25	3.414	0.33	0.0774	0.383	0.172	0.305	0.0631	0.2	0.0781	0.0417	0.0299	0.117	0.0803	0.0953	0.0874	0.0845	0.0745	0.3417
20.333	3.434	0.331	0.0777	0.384	0.172	0.305	0.0632	0.2	0.0783	0.0418	0.0299	0.117	0.0804	0.0955	0.0876	0.0846	0.0747	0.3424
20.417	3.453	0.331	0.0781	0.385	0.173	0.306	0.0633	0.201	0.0784	0.0419	0.03	0.117	0.0805	0.0956	0.0877	0.0848	0.0748	0.3429
20.5	3.473	0.332	0.0784	0.385	0.173	0.306	0.0634	0.201	0.0786	0.042	0.03	0.118	0.0805	0.0958	0.0879	0.0849	0.075	0.3436
20.583	3.492	0.332	0.0787	0.386	0.173	0.307	0.0635	0.202	0.0787	0.042	0.03	0.118	0.0805	0.0959	0.088	0.0851	0.0752	0.3442
20.667	3.511	0.333	0.079	0.387	0.174	0.307	0.0636	0.202	0.0789	0.0421	0.0301	0.118	0.0806	0.0961	0.0882	0.0853	0.0753	0.3449
20.75	3.531	0.334	0.0793	0.388	0.174	0.308	0.0637	0.203	0.079	0.0422	0.0301	0.118	0.0806	0.0963	0.0884	0.0854	0.0755	0.3456
20.833	3.55	0.334	0.0796	0.388	0.174	0.309	0.0639	0.203	0.0792	0.0423	0.0301	0.119	0.0806	0.0964	0.0885	0.0856	0.0757	0.3462
20.917	3.569	0.335	0.0799	0.389	0.175	0.309	0.064	0.204	0.0793	0.0423	0.0301	0.119	0.0806	0.0966	0.0887	0.0858	0.0758	0.3469
21	3.589	0.336	0.0801	0.39	0.175	0.31	0.0641	0.204	0.0795	0.0424	0.0301	0.119	0.0806	0.0968	0.0889	0.0859	0.076	0.3476
21.083	3.608	0.336	0.0804	0.391	0.176	0.31	0.0642	0.205	0.0797	0.0424	0.0301	0.119	0.0806	0.0969	0.089	0.0861	0.0762	0.3482
21.167	3.627	0.337	0.0806	0.392	0.176	0.311	0.0643	0.205	0.0798	0.0425	0.0302	0.119	0.0806	0.0971	0.0892	0.0863	0.0763	0.3489
21.25	3.646	0.338	0.0809	0.392	0.176	0.311	0.0644	0.206	0.08	0.0425	0.0302	0.119	0.0806	0.0973	0.0894	0.0865	0.0765	0.3497
21.333	3.665	0.338	0.0811	0.393	0.177	0.312	0.0646	0.206	0.0802	0.0426	0.0302	0.12	0.0806	0.0975	0.0896	0.0866	0.0767	0.3504
21.417	3.684	0.339	0.0814	0.394	0.177	0.313	0.0647	0.207	0.0804	0.0426	0.0302	0.12	0.0806	0.0976	0.0897	0.0868	0.0769	0.351
21.5	3.703	0.34	0.0816	0.395	0.178	0.313	0.0648	0.208	0.0806	0.0427	0.0302	0.12	0.0806	0.0978	0.0899	0.087	0.077	0.3517
21.583	3.722	0.34	0.0818	0.396	0.178	0.314	0.0649	0.208	0.0807	0.0427	0.0302	0.12	0.0806	0.098	0.0901	0.0872	0.0772	0.3525
21.667	3.741	0.341	0.082	0.396	0.178	0.314	0.0651	0.209	0.0809	0.0427	0.0302	0.12	0.0806	0.0982	0.0903	0.0874	0.0774	0.3533
21.75	3.76	0.342	0.0822	0.397	0.179	0.315	0.0652	0.209	0.0811	0.0428	0.0302	0.12	0.0806	0.0984	0.0905	0.0875	0.0776	0.354
21.833	3.779	0.343	0.0824	0.398	0.179	0.315	0.0653	0.21	0.0813	0.0428	0.0302	0.12	0.0806	0.0986	0.0907	0.0877	0.0778	0.3548
21.917	3.798	0.344	0.0826	0.399	0.18	0.316	0.0654	0.21	0.0815	0.0428	0.0302	0.12	0.0806	0.0987	0.0909	0.0879	0.078	0.3555
22	3.817	0.344	0.0827	0.4	0.18	0.317	0.0656	0.211	0.0817	0.0429	0.0302	0.12	0.0806	0.0989	0.091	0.0881	0.0782	0.3562
22.083	3.836	0.345	0.0829	0.401	0.181	0.317	0.0657	0.212	0.0819	0.0429	0.0302	0.12	0.0806	0.0991	0.0912	0.0883	0.0784	0.357
22.167	3.854	0.346	0.083	0.402	0.181	0.318	0.0658	0.212	0.0821	0.0429	0.0302	0.12	0.0806	0.0993	0.0914	0.0885	0.0786	0.3578
22.25	3.873	0.347	0.0832	0.403	0.182	0.318	0.066	0.213	0.0823	0.0429	0.0302	0.12	0.0806	0.0995	0.0916	0.0887	0.0788	0.3586
22.333	3.892	0.348	0.0833	0.404	0.182	0.319	0.0661	0.213	0.0825	0.0429	0.0302	0.12	0.0806	0.0997	0.0918	0.0889	0.079	0.3594
22.417	3.911	0.348	0.0835	0.405	0.183	0.32	0.0663	0.214	0.0827	0.0429	0.0302	0.12	0.0806	0.0999	0.092	0.0891	0.0792	0.3602
22.5	3.929	0.349	0.0836	0.405	0.183	0.32	0.0664	0.214	0.0829	0.0429	0.0302	0.12	0.0806	0.1	0.0923	0.0893	0.0794	0.361
22.583	3.948	0.35	0.0837	0.406	0.184	0.321	0.0666	0.214	0.083	0.0429	0.0302	0.12	0.0806	0.1	0.0925	0.0895	0.0796	0.3616
22.667	3.967	0.351	0.0839	0.407	0.184	0.321	0.0667	0.215	0.0832	0.0429	0.0302	0.12	0.0806	0.101	0.0927	0.0897	0.0798	0.3632
22.75	3.985	0.352	0.084	0.408	0.185	0.322	0.0669	0.215	0.0834	0.0429	0.0302	0.12	0.0806	0.101	0.0929	0.09	0.08	0.3639
22.833	4.004	0.353	0.0841	0.409	0.185	0.323	0.067	0.216	0.0836	0.0429	0.0302	0.12	0.0806	0.101	0.0931	0.0902	0.0802	0.3645
22.917	4.022	0.354	0.0842	0.41	0.186	0.323	0.0672	0.216	0.0837	0.0429	0.0302	0.12	0.0806	0.101	0.0933	0.0904	0.0804	0.3651
23	4.041	0.354	0.0843	0.411	0.186	0.324	0.0673	0.217	0.0839	0.0429	0.0302	0.12	0.0806	0.101	0.0935	0.0906	0.0807	0.3658
23.083	4.059	0.355	0.0844	0.412	0.186	0.324	0.0675	0.217	0.084	0.0429	0.0302	0.12	0.0806	0.102	0.0938	0.0908	0.0809	0.3675
23.167	4.078	0.356	0.0845	0.413	0.187	0.325	0.0676	0.217	0.0842	0.0429	0.0302	0.12	0.0806	0.102	0.094	0.0911	0.0811	0.3682
23.25	4.096	0.357	0.0846	0.414	0.187	0.326	0.0678	0.218	0.0844	0.0429	0.0302	0.12	0.0806	0.102	0.0942	0.0913	0.0813	0.3688
23.333	4.114	0.358	0.0847	0.415	0.188	0.326	0.0679	0.218	0.0845	0.0429	0.0302	0.12	0.0806	0.102	0.0944	0.0915	0.0816	0.3695
23.417	4.133	0.359	0.0848	0.416	0.188	0.327	0.068	0.219	0.0847	0.0429	0.0302	0.12	0.0806	0.103	0.0947	0.0917	0.0818	0.3712
23.5	4.151	0.359	0.0849	0.417	0.189	0.328	0.0682	0.219	0.0848	0.0429	0.0302	0.12	0.0806	0.103	0.0949	0.0919	0.082	0.3718
23.583	4.169	0.36	0.085	0.418	0.189	0.328	0.0683	0.219	0.085	0.0429	0.0302	0.12	0.0806	0.103	0.0951	0.0922	0.0822	0.3725
23.667	4.187	0.361	0.0851	0.419	0.189	0.329	0.0685	0.22	0.0851	0.0429	0.0302	0.12	0.0806	0.103	0.0953	0.0924	0.0824	0.3731
23.75	4.205	0.362	0.0852	0.42	0.19	0.33	0.0686	0.22	0.0852	0.0429	0.0302	0.12	0.0806	0.103	0.0955	0.0926	0.0827	0.3738
23.833	4.224	0.362	0.0852	0.421	0.19	0.33	0.0687	0.22	0.0854	0.0429	0.0302	0.12	0.0806	0.104	0.0957	0.0928	0.0829	0.3754
23.917	4.242	0.363	0.0853	0.422	0.19	0.331	0.0689	0.221	0.0855	0.0429	0.0302	0.12	0.0806	0.104	0.0959	0.093	0.0831	0.376
24	4.26	0.364	0.0854	0.423	0.191	0.331	0.069	0.221	0.0857	0.0429	0.0302	0.12	0.0806	0.104	0.0961	0.0932	0.0833	0.3766
24.083	4.278	0.365	0.0854	0.424	0.191	0.332	0.0691	0.221	0.0858	0.0429	0.0302	0.12	0.0806	0.104	0.0963	0.0934	0.0835	0.3772
24.167	4.296	0.365	0.0855	0.425	0.192	0.333	0.0692	0.222	0.0859	0.0429	0.0302	0.12	0.0806	0.104	0.0965	0.0936	0.0837	0.3778
24.25	4.314	0.366	0.0856	0.426	0.192	0.333	0.0694	0.222	0.086	0.0429	0.0302	0.12	0.0806	0.105	0.0967	0.0938	0.0839	0.3794
24.333	4.332	0.367	0.0856	0.427	0.192	0.334	0.0695	0.222	0.0862	0.0429	0.0302	0.12	0.0806	0.105	0.0969	0.094	0.0841	0.38
24.417	4.35	0.367	0.0856	0.428	0.193	0.335	0.0696	0.222	0.0863	0.0429	0.0302	0.12	0.0806	0.105	0.0971	0.0942	0.0843	0.3806
24.5	4.367	0.368	0.0857	0.429	0.193	0.335	0.0697	0.223	0.0864	0.0429	0.0302	0.12	0.0806	0.105	0.0973	0.0944	0.0845	0.3812
24.583	4.385	0.369	0.0857	0.43	0.193	0.336	0.0698	0.223	0.0865	0.0429	0.0302	0.12	0.0806	0.105	0.0975	0.0946	0.0846	0.3817
24.667	4.403	0.369	0.0858	0.43	0.194	0.337	0.07	0.223	0.0867	0.0429	0.0302	0.12	0.0806	0.106	0.0977	0.0948	0.0848	0.3833
24.75	4.421	0.37	0.0858	0.431	0.194	0.337	0.0701	0.223	0.0868	0.0429	0.0302	0.12	0.0806	0.106	0.0979	0.0949	0.085	0.3838
24.833	4.438	0.371	0.0858	0.432	0.194	0.338	0.0702	0.224	0.0869	0.0429	0.0302	0.12	0.0806	0.106	0.098	0.0951	0.0852	0.3843
24.917	4.456	0.371	0.0858	0.433	0.194	0.339	0.0703	0.224	0.087	0.0429	0.0302	0.12	0.0806	0.106	0.0982	0.0953	0.0854	0.3849
25	4.474	0.372	0.0859	0.434	0.195	0.339	0.0704	0.224	0.0871	0.0429	0.0302	0.12	0.0806	0.106	0.0984	0.0955	0.0855	0.3854
25.083	4.492	0.372	0.0859	0.434	0.195	0.34	0.0705	0.224	0.0872	0.0429	0.0302	0.12	0.0806	0.106	0.0986	0.0956	0.0857	0.3859
25.167	4.509	0.373	0.0859	0.435	0.195	0.341	0.0706	0.224	0.0873	0.0429	0.0302	0.12	0.0806	0.107	0.0987	0.0958	0.0859	0.3874
25.25	4.527	0.373	0.0859	0.436	0.196	0.341	0.0707	0.225	0.0874	0.0429	0.0302	0.12	0.0806	0.107	0.0989	0.096	0.086	0.3879
25.333	4.545	0.374	0.0859	0.437	0.196	0.342	0.0708	0.225	0.0875	0.0429	0.0302	0.12	0.0806	0.107	0.0991	0.0961	0.0862	0.3884
25.417	4.563	0.375	0.0859	0.438	0.196	0.343	0.0709	0.225	0.0876	0.0429	0.0302	0.12	0.0806	0.107	0.0992	0.0963	0.0864	0.3889
25.5	4.581	0.375	0.0859	0.438	0.196	0.343	0.071	0.225	0.0877	0.0429	0.0302	0.12	0.0806	0.107	0.0994	0.0965	0.0865	0.3894
25.583	4.599	0.376	0.0859	0.439	0.197	0.344	0.0711	0.226	0.0878	0.0429	0.0302	0.12	0.0806	0.107	0.0995	0.0966	0.0867	0.3898
25.667	4.617	0.376	0.0859	0.44	0.197	0.345	0.0712	0.226	0.0879	0.0429	0.0302	0.12	0.0806	0.108	0.0997	0.0968	0.0868	0.3913

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
25.75	4.635	0.377	0.0859	0.44	0.197	0.345	0.0713	0.226	0.0879	0.0429	0.0302	0.12	0.0806	0.108	0.0998	0.0969	0.087	0.3917
25.833	4.653	0.377	0.0859	0.441	0.197	0.346	0.0713	0.226	0.088	0.0429	0.0302	0.12	0.0806	0.108	0.1	0.0971	0.0871	0.3922
25.917	4.672	0.378	0.0859	0.442	0.198	0.346	0.0714	0.226	0.0881	0.0429	0.0302	0.12	0.0806	0.108	0.1	0.0972	0.0873	0.3925
26	4.69	0.378	0.0859	0.442	0.198	0.347	0.0715	0.226	0.0882	0.0429	0.0302	0.12	0.0806	0.108	0.1	0.0973	0.0874	0.3927
26.083	4.708	0.378	0.0859	0.443	0.198	0.348	0.0716	0.227	0.0883	0.0429	0.0302	0.12	0.0806	0.108	0.1	0.0975	0.0876	0.3931
26.167	4.726	0.379	0.0859	0.444	0.198	0.348	0.0717	0.227	0.0883	0.0429	0.0302	0.12	0.0806	0.108	0.101	0.0976	0.0877	0.3943
26.25	4.745	0.379	0.0859	0.444	0.199	0.349	0.0717	0.227	0.0884	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.0978	0.0878	0.3956
26.333	4.763	0.38	0.0859	0.445	0.199	0.349	0.0718	0.227	0.0885	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.0979	0.088	0.3959
26.417	4.782	0.38	0.0859	0.445	0.199	0.35	0.0719	0.227	0.0886	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.098	0.0881	0.3961
26.5	4.8	0.381	0.0859	0.446	0.199	0.35	0.072	0.227	0.0886	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.0981	0.0882	0.3963
26.583	4.819	0.381	0.0859	0.447	0.199	0.351	0.072	0.228	0.0887	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.0983	0.0883	0.3966
26.667	4.837	0.381	0.0859	0.447	0.2	0.351	0.0721	0.228	0.0888	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.0984	0.0885	0.3969
26.75	4.856	0.382	0.0859	0.448	0.2	0.352	0.0722	0.228	0.0888	0.0429	0.0302	0.12	0.0806	0.109	0.101	0.0985	0.0886	0.3971
26.833	4.875	0.382	0.0859	0.448	0.2	0.352	0.0722	0.228	0.0889	0.0429	0.0302	0.12	0.0806	0.109	0.102	0.0986	0.0887	0.3983
26.917	4.894	0.383	0.0859	0.449	0.2	0.353	0.0723	0.228	0.089	0.0429	0.0302	0.12	0.0806	0.11	0.102	0.0987	0.0888	0.3995
27	4.912	0.383	0.0859	0.449	0.2	0.353	0.0724	0.228	0.089	0.0429	0.0302	0.12	0.0806	0.11	0.102	0.0988	0.0889	0.3997
27.083	4.931	0.383	0.0859	0.45	0.201	0.354	0.0724	0.228	0.0891	0.0429	0.0302	0.12	0.0806	0.11	0.102	0.0989	0.089	0.3999
27.167	4.95	0.384	0.0859	0.45	0.201	0.354	0.0725	0.228	0.0892	0.0429	0.0302	0.12	0.0806	0.11	0.102	0.0991	0.0891	0.4002
27.25	4.969	0.384	0.0859	0.451	0.201	0.355	0.0726	0.229	0.0892	0.0429	0.0302	0.12	0.0806	0.11	0.102	0.0992	0.0892	0.4004
27.333	4.988	0.384	0.086	0.451	0.201	0.355	0.0726	0.229	0.0893	0.043	0.0302	0.12	0.0807	0.11	0.102	0.0993	0.0893	0.4006
27.417	5.007	0.385	0.086	0.452	0.201	0.356	0.0727	0.229	0.0894	0.043	0.0302	0.12	0.0809	0.11	0.102	0.0994	0.0894	0.4008
27.5	5.026	0.385	0.086	0.452	0.201	0.356	0.0727	0.229	0.0894	0.043	0.0303	0.12	0.081	0.11	0.102	0.0995	0.0895	0.401
27.583	5.045	0.385	0.0861	0.453	0.202	0.357	0.0728	0.229	0.0895	0.0431	0.0304	0.121	0.0814	0.11	0.103	0.0996	0.0897	0.4023
27.667	5.064	0.386	0.0862	0.453	0.202	0.357	0.0729	0.229	0.0896	0.0431	0.0304	0.121	0.0817	0.11	0.103	0.0997	0.0898	0.4025
27.75	5.084	0.386	0.0862	0.454	0.202	0.358	0.0729	0.229	0.0897	0.0432	0.0305	0.121	0.0821	0.111	0.103	0.0998	0.0899	0.4037
27.833	5.103	0.386	0.0863	0.454	0.202	0.358	0.073	0.23	0.0897	0.0433	0.0307	0.121	0.0826	0.111	0.103	0.0999	0.09	0.4039
27.917	5.122	0.387	0.0864	0.455	0.202	0.359	0.0731	0.23	0.0898	0.0434	0.0308	0.122	0.0831	0.111	0.103	0.1	0.0901	0.4041
28	5.141	0.387	0.0866	0.455	0.203	0.359	0.0732	0.23	0.0899	0.0435	0.0309	0.122	0.0837	0.111	0.103	0.1	0.0902	0.4042
28.083	5.161	0.388	0.0867	0.456	0.203	0.36	0.0732	0.23	0.09	0.0436	0.0311	0.123	0.0842	0.111	0.103	0.1	0.0903	0.4043
28.167	5.18	0.388	0.0869	0.456	0.203	0.36	0.0733	0.231	0.0901	0.0437	0.0313	0.123	0.0847	0.111	0.103	0.1	0.0904	0.4044
28.25	5.2	0.389	0.087	0.457	0.203	0.361	0.0734	0.231	0.0902	0.0439	0.0314	0.124	0.0852	0.111	0.103	0.1	0.0906	0.4046
28.333	5.219	0.389	0.0872	0.457	0.204	0.361	0.0735	0.231	0.0903	0.044	0.0316	0.125	0.0856	0.111	0.104	0.101	0.0907	0.4067
28.417	5.239	0.39	0.0874	0.458	0.204	0.362	0.0735	0.231	0.0904	0.0442	0.0317	0.125	0.086	0.112	0.104	0.101	0.0908	0.4078
28.5	5.259	0.39	0.0876	0.459	0.204	0.362	0.0736	0.232	0.0905	0.0443	0.0319	0.126	0.0863	0.112	0.104	0.101	0.0909	0.4079
28.583	5.278	0.39	0.0879	0.459	0.204	0.363	0.0737	0.232	0.0906	0.0445	0.032	0.126	0.0866	0.112	0.104	0.101	0.091	0.408
28.667	5.298	0.391	0.0881	0.46	0.205	0.363	0.0738	0.232	0.0908	0.0447	0.0321	0.127	0.0869	0.112	0.104	0.101	0.0912	0.4082
28.75	5.318	0.391	0.0884	0.46	0.205	0.364	0.0739	0.233	0.0909	0.0448	0.0322	0.127	0.0871	0.112	0.104	0.101	0.0913	0.4083
28.833	5.338	0.392	0.0886	0.461	0.205	0.364	0.074	0.233	0.091	0.045	0.0323	0.128	0.0873	0.112	0.104	0.101	0.0914	0.4084
28.917	5.358	0.393	0.0889	0.462	0.206	0.365	0.0741	0.233	0.0911	0.0451	0.0324	0.128	0.0875	0.112	0.104	0.101	0.0916	0.4086
29	5.378	0.393	0.0892	0.462	0.206	0.365	0.0742	0.234	0.0912	0.0452	0.0325	0.129	0.0877	0.112	0.105	0.102	0.0917	0.4107
29.083	5.398	0.394	0.0895	0.463	0.206	0.366	0.0743	0.234	0.0914	0.0454	0.0325	0.129	0.0878	0.113	0.105	0.102	0.0918	0.4118
29.167	5.418	0.394	0.0899	0.463	0.206	0.366	0.0744	0.234	0.0915	0.0455	0.0326	0.13	0.088	0.113	0.105	0.102	0.092	0.412
29.25	5.438	0.395	0.0902	0.464	0.207	0.367	0.0745	0.235	0.0916	0.0456	0.0327	0.13	0.0881	0.113	0.105	0.102	0.0921	0.4121
29.333	5.458	0.395	0.0905	0.465	0.207	0.368	0.0746	0.235	0.0918	0.0457	0.0327	0.13	0.0882	0.113	0.105	0.102	0.0923	0.4123
29.417	5.478	0.396	0.0909	0.465	0.207	0.368	0.0747	0.236	0.0919	0.0458	0.0328	0.131	0.0883	0.113	0.105	0.102	0.0924	0.4124
29.5	5.498	0.396	0.0912	0.466	0.208	0.369	0.0748	0.236	0.0921	0.0459	0.0328	0.131	0.0883	0.113	0.105	0.102	0.0926	0.4126
29.583	5.519	0.397	0.0915	0.467	0.208	0.369	0.0749	0.237	0.0922	0.046	0.0328	0.131	0.0884	0.113	0.106	0.103	0.0927	0.4147
29.667	5.539	0.398	0.0918	0.467	0.208	0.37	0.075	0.237	0.0924	0.0461	0.0329	0.131	0.0884	0.114	0.106	0.103	0.0929	0.4159
29.75	5.559	0.398	0.0922	0.468	0.209	0.37	0.0751	0.237	0.0925	0.0461	0.0329	0.132	0.0884	0.114	0.106	0.103	0.093	0.416
29.833	5.58	0.399	0.0924	0.469	0.209	0.371	0.0752	0.238	0.0927	0.0462	0.0329	0.132	0.0884	0.114	0.106	0.103	0.0932	0.4162
29.917	5.6	0.4	0.0927	0.47	0.21	0.371	0.0753	0.239	0.0928	0.0463	0.033	0.132	0.0884	0.114	0.106	0.103	0.0934	0.4164
30	5.621	0.4	0.093	0.47	0.21	0.372	0.0754	0.239	0.093	0.0463	0.033	0.132	0.0884	0.114	0.106	0.103	0.0935	0.4165
30.083	5.642	0.401	0.0933	0.471	0.21	0.373	0.0755	0.24	0.0931	0.0464	0.033	0.132	0.0884	0.114	0.107	0.104	0.0937	0.4187
30.167	5.662	0.402	0.0935	0.472	0.211	0.373	0.0756	0.24	0.0933	0.0464	0.033	0.133	0.0884	0.115	0.107	0.104	0.0939	0.4199
30.25	5.683	0.402	0.0938	0.473	0.211	0.374	0.0758	0.241	0.0935	0.0465	0.033	0.133	0.0884	0.115	0.107	0.104	0.094	0.42
30.333	5.704	0.403	0.0941	0.474	0.212	0.374	0.0759	0.241	0.0937	0.0466	0.033	0.133	0.0885	0.115	0.107	0.104	0.0942	0.4202
30.417	5.725	0.404	0.0943	0.474	0.212	0.375	0.076	0.242	0.0938	0.0466	0.0331	0.133	0.0886	0.115	0.107	0.104	0.0944	0.4204
30.5	5.746	0.404	0.0946	0.475	0.212	0.375	0.0761	0.243	0.094	0.0467	0.0331	0.133	0.0887	0.115	0.107	0.104	0.0946	0.4206
30.583	5.767	0.405	0.0949	0.476	0.213	0.376	0.0763	0.243	0.0942	0.0468	0.0332	0.134	0.0891	0.115	0.108	0.105	0.0948	0.4228
30.667	5.788	0.406	0.0951	0.477	0.213	0.377	0.0764	0.244	0.0944	0.0469	0.0332	0.134	0.0894	0.116	0.108	0.105	0.095	0.424
30.75	5.809	0.407	0.0954	0.478	0.214	0.377	0.0765	0.245	0.0946	0.047	0.0333	0.134	0.0897	0.116	0.108	0.105	0.0952	0.4242
30.833	5.83	0.408	0.0957	0.479	0.214	0.378	0.0767	0.245	0.0949	0.0471	0.0335	0.135	0.0903	0.116	0.108	0.105	0.0954	0.4244
30.917	5.851	0.409	0.096	0.48	0.215	0.379	0.0768	0.246	0.0951	0.0472	0.0336	0.135	0.0908	0.116	0.108	0.105	0.0956	0.4246
31	5.872	0.409	0.0963	0.481	0.215	0.379	0.077	0.247	0.0953	0.0473	0.0337	0.135	0.0914	0.116	0.109	0.106	0.0958	0.4268
31.083	5.893	0.41	0.0966	0.482	0.216	0.38	0.0771	0.247	0.0956	0.0475	0.0339	0.136	0.0919	0.117	0.109	0.106	0.096	0.428
31.167	5.915	0.411	0.0969	0.483	0.216	0.381	0.0773	0.248	0.0958	0.0476	0.0341	0.137	0.0924	0.117	0.109	0.106	0.0962	0.4282
31.25	5.936	0.412	0.0972	0.484	0.217	0.381	0.0775	0.249	0.096	0.0478	0.0342	0.137	0.0929	0.117	0.109	0.106	0.0965	0.4285

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
31.333	5.958	0.413	0.0976	0.485	0.217	0.382	0.0776	0.249	0.0963	0.0479	0.0344	0.138	0.0933	0.117	0.11	0.107	0.0967	0.4307
31.417	5.979	0.414	0.0979	0.486	0.218	0.383	0.0778	0.25	0.0965	0.0481	0.0345	0.138	0.0937	0.118	0.11	0.107	0.097	0.432
31.5	6.001	0.415	0.0982	0.487	0.219	0.383	0.078	0.251	0.0968	0.0483	0.0347	0.139	0.0941	0.118	0.11	0.107	0.0972	0.4322
31.583	6.022	0.416	0.0986	0.488	0.219	0.384	0.0782	0.252	0.097	0.0484	0.0348	0.14	0.0944	0.118	0.11	0.107	0.0975	0.4325
31.667	6.044	0.417	0.099	0.49	0.22	0.385	0.0783	0.252	0.0973	0.0486	0.0349	0.14	0.0946	0.118	0.111	0.108	0.0977	0.4347
31.75	6.066	0.419	0.0993	0.491	0.221	0.385	0.0785	0.253	0.0975	0.0488	0.035	0.141	0.0949	0.119	0.111	0.108	0.098	0.436
31.833	6.087	0.42	0.0997	0.492	0.221	0.386	0.0787	0.254	0.0978	0.0489	0.0351	0.141	0.0951	0.119	0.111	0.108	0.0983	0.4363
31.917	6.109	0.421	0.1	0.493	0.222	0.387	0.0789	0.255	0.098	0.0491	0.0352	0.142	0.0953	0.119	0.111	0.108	0.0985	0.4365
32	6.131	0.422	0.101	0.495	0.222	0.388	0.0791	0.255	0.0983	0.0492	0.0353	0.142	0.0955	0.12	0.112	0.109	0.0988	0.4398
32.083	6.153	0.423	0.101	0.496	0.223	0.389	0.0793	0.256	0.0985	0.0493	0.0354	0.143	0.0956	0.12	0.112	0.109	0.0991	0.4401
32.167	6.175	0.424	0.101	0.497	0.224	0.389	0.0795	0.257	0.0988	0.0495	0.0354	0.143	0.0958	0.12	0.112	0.109	0.0994	0.4404
32.25	6.197	0.425	0.102	0.499	0.224	0.39	0.0797	0.258	0.099	0.0496	0.0355	0.143	0.0959	0.12	0.113	0.11	0.0997	0.4427
32.333	6.219	0.427	0.102	0.5	0.225	0.391	0.0799	0.258	0.0993	0.0497	0.0355	0.144	0.096	0.121	0.113	0.11	0.1	0.444
32.417	6.242	0.428	0.103	0.501	0.226	0.392	0.0801	0.259	0.0995	0.0498	0.0356	0.144	0.0961	0.121	0.113	0.11	0.1	0.444
32.5	6.264	0.429	0.103	0.503	0.226	0.393	0.0803	0.26	0.0998	0.0499	0.0356	0.144	0.0962	0.121	0.113	0.111	0.101	0.446
32.583	6.286	0.43	0.104	0.504	0.227	0.393	0.0805	0.261	0.1	0.05	0.0357	0.144	0.0962	0.122	0.114	0.111	0.101	0.448
32.667	6.309	0.431	0.104	0.506	0.228	0.394	0.0808	0.262	0.1	0.05	0.0357	0.145	0.0962	0.122	0.114	0.111	0.101	0.448
32.75	6.331	0.432	0.104	0.507	0.228	0.395	0.081	0.262	0.101	0.0501	0.0357	0.145	0.0963	0.122	0.114	0.111	0.102	0.449
32.833	6.353	0.434	0.105	0.508	0.229	0.396	0.0812	0.263	0.101	0.0502	0.0358	0.145	0.0963	0.123	0.115	0.112	0.102	0.452
32.917	6.376	0.435	0.105	0.51	0.23	0.397	0.0814	0.264	0.101	0.0503	0.0358	0.145	0.0963	0.123	0.115	0.112	0.102	0.452
33	6.398	0.436	0.105	0.511	0.23	0.398	0.0816	0.265	0.101	0.0503	0.0358	0.146	0.0963	0.123	0.115	0.112	0.102	0.452
33.083	6.421	0.437	0.106	0.513	0.231	0.399	0.0818	0.266	0.102	0.0504	0.0358	0.146	0.0963	0.123	0.116	0.113	0.103	0.455
33.167	6.444	0.438	0.106	0.514	0.231	0.399	0.082	0.267	0.102	0.0504	0.0358	0.146	0.0963	0.124	0.116	0.113	0.103	0.456
33.25	6.467	0.44	0.106	0.515	0.232	0.4	0.0822	0.268	0.102	0.0505	0.0358	0.146	0.0963	0.124	0.116	0.113	0.103	0.456
33.333	6.49	0.441	0.107	0.517	0.233	0.401	0.0824	0.268	0.102	0.0506	0.0359	0.146	0.0964	0.124	0.117	0.114	0.104	0.459
33.417	6.513	0.442	0.107	0.518	0.233	0.402	0.0826	0.269	0.103	0.0506	0.0359	0.146	0.0965	0.125	0.117	0.114	0.104	0.46
33.5	6.535	0.443	0.107	0.52	0.234	0.403	0.0828	0.27	0.103	0.0507	0.0359	0.147	0.0966	0.125	0.117	0.114	0.104	0.46
33.583	6.559	0.444	0.108	0.521	0.235	0.404	0.083	0.271	0.103	0.0508	0.036	0.147	0.0969	0.125	0.117	0.115	0.105	0.462
33.667	6.582	0.446	0.108	0.523	0.235	0.405	0.0832	0.272	0.104	0.0509	0.0361	0.147	0.0972	0.126	0.118	0.115	0.105	0.464
33.75	6.605	0.447	0.108	0.524	0.236	0.406	0.0835	0.273	0.104	0.051	0.0361	0.148	0.0975	0.126	0.118	0.115	0.105	0.464
33.833	6.628	0.448	0.109	0.526	0.237	0.407	0.0837	0.274	0.104	0.0511	0.0363	0.148	0.098	0.126	0.118	0.116	0.106	0.466
33.917	6.651	0.45	0.109	0.527	0.238	0.408	0.0839	0.275	0.105	0.0512	0.0364	0.148	0.0985	0.127	0.119	0.116	0.106	0.468
34	6.675	0.451	0.109	0.529	0.238	0.409	0.0841	0.276	0.105	0.0513	0.0365	0.149	0.0991	0.127	0.119	0.116	0.106	0.468
34.083	6.698	0.452	0.11	0.53	0.239	0.41	0.0844	0.277	0.105	0.0515	0.0367	0.149	0.0996	0.127	0.119	0.117	0.107	0.47
34.167	6.722	0.454	0.11	0.532	0.24	0.411	0.0846	0.278	0.106	0.0516	0.0369	0.15	0.1	0.128	0.12	0.117	0.107	0.472
34.25	6.745	0.455	0.11	0.534	0.241	0.412	0.0848	0.278	0.106	0.0517	0.037	0.15	0.101	0.128	0.12	0.117	0.107	0.472
34.333	6.769	0.456	0.111	0.535	0.241	0.414	0.0851	0.279	0.106	0.0519	0.0372	0.151	0.101	0.128	0.12	0.118	0.108	0.474
34.417	6.792	0.458	0.111	0.537	0.242	0.415	0.0853	0.28	0.107	0.0521	0.0373	0.152	0.101	0.129	0.121	0.118	0.108	0.476
34.5	6.816	0.459	0.111	0.538	0.243	0.416	0.0856	0.281	0.107	0.0522	0.0375	0.152	0.102	0.129	0.121	0.118	0.108	0.476
34.583	6.84	0.461	0.112	0.54	0.244	0.417	0.0858	0.282	0.107	0.0524	0.0376	0.153	0.102	0.129	0.122	0.119	0.109	0.479
34.667	6.864	0.462	0.112	0.542	0.245	0.418	0.086	0.283	0.108	0.0526	0.0377	0.153	0.102	0.13	0.122	0.119	0.109	0.48
34.75	6.888	0.463	0.112	0.544	0.245	0.419	0.0863	0.284	0.108	0.0527	0.0378	0.154	0.103	0.13	0.122	0.119	0.11	0.481
34.833	6.912	0.465	0.113	0.545	0.246	0.42	0.0865	0.285	0.108	0.0529	0.0379	0.154	0.103	0.131	0.123	0.12	0.11	0.484
34.917	6.936	0.466	0.113	0.547	0.247	0.421	0.0868	0.286	0.109	0.053	0.038	0.155	0.103	0.131	0.123	0.12	0.11	0.484
35	6.96	0.468	0.114	0.549	0.248	0.423	0.0871	0.287	0.109	0.0532	0.0381	0.155	0.103	0.131	0.123	0.121	0.111	0.486
35.083	6.984	0.469	0.114	0.551	0.249	0.424	0.0873	0.288	0.109	0.0533	0.0382	0.156	0.103	0.132	0.124	0.121	0.111	0.488
35.167	7.008	0.471	0.114	0.552	0.25	0.425	0.0876	0.289	0.11	0.0534	0.0382	0.156	0.104	0.132	0.124	0.121	0.111	0.488
35.25	7.033	0.472	0.115	0.554	0.25	0.426	0.0878	0.29	0.11	0.0535	0.0383	0.157	0.104	0.132	0.125	0.122	0.112	0.491
35.333	7.057	0.474	0.115	0.556	0.251	0.427	0.0881	0.291	0.11	0.0536	0.0384	0.157	0.104	0.133	0.125	0.122	0.112	0.492
35.417	7.081	0.475	0.116	0.558	0.252	0.428	0.0884	0.292	0.111	0.0538	0.0384	0.157	0.104	0.133	0.125	0.122	0.113	0.493
35.5	7.106	0.477	0.116	0.56	0.253	0.429	0.0886	0.292	0.111	0.0539	0.0385	0.158	0.104	0.134	0.126	0.123	0.113	0.496
35.583	7.131	0.478	0.117	0.561	0.254	0.431	0.0889	0.293	0.111	0.0539	0.0385	0.158	0.104	0.134	0.126	0.123	0.113	0.496
35.667	7.155	0.48	0.117	0.563	0.254	0.432	0.0891	0.294	0.112	0.054	0.0385	0.158	0.104	0.134	0.127	0.124	0.114	0.499
35.75	7.18	0.481	0.117	0.565	0.255	0.433	0.0894	0.295	0.112	0.0541	0.0386	0.158	0.104	0.135	0.127	0.124	0.114	0.5
35.833	7.205	0.483	0.118	0.567	0.256	0.434	0.0897	0.296	0.112	0.0542	0.0386	0.158	0.104	0.135	0.127	0.124	0.115	0.501
35.917	7.23	0.484	0.118	0.568	0.257	0.435	0.0899	0.297	0.113	0.0542	0.0386	0.159	0.104	0.136	0.128	0.125	0.115	0.504
36	7.254	0.486	0.118	0.57	0.258	0.437	0.0902	0.298	0.113	0.0543	0.0387	0.159	0.104	0.136	0.128	0.125	0.115	0.504
36.083	7.279	0.487	0.119	0.572	0.259	0.438	0.0904	0.299	0.113	0.0544	0.0387	0.159	0.104	0.136	0.128	0.126	0.116	0.506
36.167	7.305	0.489	0.119	0.574	0.259	0.439	0.0907	0.3	0.114	0.0544	0.0387	0.159	0.104	0.137	0.129	0.126	0.116	0.508
36.25	7.33	0.49	0.119	0.576	0.26	0.44	0.0909	0.301	0.114	0.0545	0.0387	0.159	0.104	0.137	0.129	0.126	0.116	0.508
36.333	7.355	0.492	0.12	0.577	0.261	0.442	0.0912	0.302	0.114	0.0546	0.0387	0.16	0.104	0.138	0.13	0.127	0.117	0.512
36.417	7.38	0.493	0.12	0.579	0.262	0.443	0.0914	0.303	0.115	0.0547	0.0388	0.16	0.105	0.138	0.13	0.127	0.117	0.512
36.5	7.405	0.495	0.12	0.581	0.263	0.444	0.0917	0.304	0.115	0.0548	0.0389	0.16	0.105	0.138	0.13	0.128	0.118	0.514
36.583	7.431	0.496	0.121	0.583	0.264	0.446	0.092	0.305	0.115	0.055	0.0391	0.161	0.106	0.139	0.131	0.128	0.118	0.516
36.667	7.456	0.498	0.121	0.585	0.265	0.447	0.0922	0.307	0.116	0.0551	0.0393	0.162	0.107	0.139	0.131	0.128	0.119	0.517
36.75	7.482	0.499	0.122	0.587	0.265	0.448	0.0925	0.308	0.116	0.0553	0.0395	0.162	0.107	0.14	0.132	0.129	0.119	0.52
36.833	7.508	0.501	0.122	0.589	0.266	0.45	0.0928	0.309	0.117	0.0556	0.0399	0.163	0.109	0.14	0.132	0.129	0.119	0.52

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
36.917	7.533	0.503	0.123	0.591	0.267	0.451	0.0931	0.31	0.117	0.0559	0.0403	0.165	0.111	0.14	0.133	0.13	0.12	0.523
37	7.559	0.505	0.123	0.593	0.268	0.453	0.0934	0.311	0.117	0.0562	0.0406	0.166	0.112	0.141	0.133	0.13	0.12	0.524
37.083	7.585	0.507	0.124	0.595	0.269	0.454	0.0937	0.313	0.118	0.0565	0.0411	0.167	0.114	0.141	0.133	0.131	0.121	0.526
37.167	7.611	0.508	0.125	0.597	0.271	0.456	0.0941	0.314	0.118	0.0569	0.0416	0.169	0.115	0.142	0.134	0.131	0.121	0.528
37.25	7.637	0.51	0.125	0.599	0.272	0.457	0.0944	0.315	0.119	0.0573	0.0421	0.17	0.117	0.142	0.134	0.131	0.122	0.529
37.333	7.663	0.512	0.126	0.601	0.273	0.459	0.0947	0.317	0.119	0.0577	0.0426	0.172	0.118	0.143	0.135	0.132	0.122	0.532
37.417	7.689	0.514	0.127	0.604	0.274	0.461	0.0951	0.318	0.12	0.0582	0.043	0.174	0.119	0.143	0.135	0.132	0.123	0.533
37.5	7.715	0.516	0.127	0.606	0.275	0.462	0.0954	0.319	0.12	0.0587	0.0435	0.176	0.12	0.144	0.136	0.133	0.123	0.536
37.583	7.741	0.518	0.128	0.608	0.276	0.464	0.0958	0.321	0.121	0.0592	0.0439	0.178	0.121	0.144	0.136	0.133	0.124	0.537
37.667	7.768	0.521	0.129	0.611	0.277	0.466	0.0961	0.322	0.121	0.0597	0.0442	0.179	0.122	0.145	0.137	0.134	0.124	0.54
37.75	7.794	0.523	0.13	0.613	0.279	0.467	0.0965	0.324	0.122	0.0602	0.0446	0.181	0.123	0.145	0.137	0.135	0.125	0.542
37.833	7.821	0.525	0.131	0.616	0.28	0.469	0.0969	0.325	0.122	0.0606	0.0449	0.182	0.124	0.146	0.138	0.135	0.125	0.544
37.917	7.847	0.527	0.132	0.618	0.281	0.471	0.0973	0.327	0.123	0.0611	0.0451	0.184	0.124	0.146	0.139	0.136	0.126	0.547
38	7.874	0.529	0.133	0.621	0.282	0.473	0.0977	0.329	0.123	0.0615	0.0454	0.185	0.125	0.147	0.139	0.136	0.126	0.548
38.083	7.9	0.532	0.134	0.623	0.284	0.474	0.0981	0.33	0.124	0.0619	0.0456	0.187	0.125	0.147	0.14	0.137	0.127	0.551
38.167	7.927	0.534	0.135	0.626	0.285	0.476	0.0985	0.332	0.124	0.0622	0.0458	0.188	0.126	0.148	0.14	0.137	0.127	0.552
38.25	7.954	0.536	0.136	0.629	0.286	0.478	0.0989	0.334	0.125	0.0626	0.046	0.189	0.126	0.149	0.141	0.138	0.128	0.556
38.333	7.981	0.539	0.137	0.631	0.288	0.48	0.0993	0.335	0.126	0.0629	0.0462	0.19	0.127	0.149	0.141	0.139	0.129	0.558
38.417	8.009	0.541	0.138	0.634	0.289	0.482	0.0997	0.337	0.126	0.0633	0.0463	0.191	0.127	0.15	0.142	0.139	0.129	0.56
38.5	8.036	0.544	0.139	0.637	0.29	0.483	0.1	0.339	0.127	0.0636	0.0465	0.192	0.127	0.15	0.143	0.14	0.13	0.563
38.583	8.063	0.546	0.14	0.64	0.292	0.485	0.101	0.341	0.127	0.0638	0.0466	0.193	0.127	0.151	0.143	0.14	0.131	0.565
38.667	8.091	0.549	0.141	0.643	0.293	0.487	0.101	0.343	0.128	0.0641	0.0467	0.193	0.127	0.152	0.144	0.141	0.131	0.568
38.75	8.118	0.551	0.142	0.646	0.295	0.489	0.101	0.345	0.128	0.0643	0.0469	0.194	0.128	0.152	0.144	0.142	0.132	0.57
38.833	8.146	0.554	0.143	0.648	0.296	0.491	0.102	0.347	0.129	0.0645	0.0469	0.195	0.128	0.153	0.145	0.142	0.132	0.572
38.917	8.174	0.556	0.144	0.651	0.298	0.493	0.102	0.349	0.13	0.0648	0.047	0.196	0.128	0.154	0.146	0.143	0.133	0.576
39	8.202	0.559	0.145	0.654	0.299	0.495	0.103	0.351	0.13	0.065	0.0471	0.196	0.128	0.154	0.146	0.144	0.134	0.578
39.083	8.23	0.561	0.146	0.657	0.3	0.497	0.103	0.353	0.131	0.0651	0.0471	0.197	0.128	0.155	0.147	0.144	0.134	0.58
39.167	8.258	0.564	0.147	0.66	0.302	0.499	0.104	0.355	0.132	0.0653	0.0472	0.197	0.128	0.156	0.148	0.145	0.135	0.584
39.25	8.286	0.566	0.148	0.663	0.303	0.501	0.104	0.357	0.132	0.0655	0.0472	0.198	0.128	0.156	0.148	0.145	0.136	0.585
39.333	8.314	0.569	0.149	0.666	0.305	0.503	0.105	0.359	0.133	0.0657	0.0472	0.198	0.128	0.157	0.149	0.146	0.136	0.588
39.417	8.343	0.572	0.149	0.669	0.306	0.505	0.105	0.361	0.134	0.0659	0.0473	0.199	0.128	0.158	0.15	0.147	0.137	0.592
39.5	8.371	0.574	0.15	0.672	0.308	0.507	0.105	0.363	0.134	0.066	0.0473	0.199	0.128	0.158	0.15	0.147	0.138	0.593
39.583	8.4	0.577	0.151	0.676	0.31	0.51	0.106	0.366	0.135	0.0662	0.0475	0.2	0.129	0.159	0.151	0.148	0.138	0.596
39.667	8.429	0.58	0.152	0.679	0.311	0.512	0.106	0.368	0.136	0.0664	0.0476	0.201	0.129	0.16	0.152	0.149	0.139	0.6
39.75	8.457	0.583	0.153	0.682	0.313	0.514	0.107	0.37	0.136	0.0667	0.0477	0.201	0.13	0.16	0.153	0.15	0.14	0.603
39.833	8.486	0.586	0.153	0.686	0.315	0.516	0.107	0.372	0.137	0.0669	0.0479	0.202	0.131	0.161	0.153	0.15	0.141	0.605
39.917	8.516	0.589	0.154	0.689	0.316	0.519	0.108	0.374	0.138	0.0672	0.0482	0.203	0.132	0.162	0.154	0.151	0.141	0.608
40	8.545	0.592	0.155	0.692	0.318	0.521	0.108	0.377	0.139	0.0674	0.0484	0.204	0.133	0.163	0.155	0.152	0.142	0.612
40.083	8.574	0.595	0.156	0.696	0.32	0.523	0.109	0.379	0.14	0.0677	0.0487	0.205	0.134	0.163	0.155	0.153	0.143	0.614
40.167	8.603	0.598	0.157	0.699	0.322	0.526	0.109	0.381	0.14	0.068	0.0491	0.206	0.135	0.164	0.156	0.153	0.144	0.617
40.25	8.633	0.601	0.157	0.703	0.324	0.528	0.11	0.383	0.141	0.0683	0.0494	0.207	0.136	0.165	0.157	0.154	0.144	0.62
40.333	8.663	0.605	0.158	0.707	0.325	0.53	0.111	0.386	0.142	0.0686	0.0497	0.208	0.137	0.166	0.158	0.155	0.145	0.624
40.417	8.692	0.608	0.159	0.71	0.327	0.533	0.111	0.388	0.143	0.069	0.05	0.209	0.137	0.166	0.159	0.156	0.146	0.627
40.5	8.722	0.611	0.16	0.714	0.329	0.535	0.112	0.39	0.144	0.0693	0.0503	0.21	0.138	0.167	0.159	0.157	0.147	0.63
40.583	8.752	0.615	0.161	0.718	0.331	0.538	0.112	0.392	0.144	0.0697	0.0506	0.212	0.139	0.168	0.16	0.157	0.148	0.633
40.667	8.782	0.618	0.162	0.722	0.333	0.54	0.113	0.394	0.145	0.07	0.0508	0.213	0.14	0.169	0.161	0.158	0.148	0.636
40.75	8.812	0.621	0.162	0.725	0.335	0.543	0.113	0.396	0.146	0.0703	0.0511	0.214	0.14	0.17	0.162	0.159	0.149	0.64
40.833	8.843	0.625	0.163	0.729	0.337	0.546	0.114	0.399	0.147	0.0706	0.0513	0.215	0.141	0.171	0.163	0.16	0.15	0.644
40.917	8.873	0.629	0.164	0.733	0.339	0.548	0.115	0.401	0.148	0.0709	0.0515	0.216	0.141	0.171	0.164	0.161	0.151	0.647
41	8.904	0.632	0.165	0.737	0.341	0.551	0.115	0.403	0.148	0.0712	0.0516	0.217	0.141	0.172	0.165	0.162	0.152	0.651
41.083	8.934	0.636	0.166	0.742	0.343	0.553	0.116	0.405	0.149	0.0715	0.0518	0.218	0.142	0.173	0.165	0.163	0.153	0.654
41.167	8.965	0.64	0.167	0.746	0.345	0.556	0.117	0.407	0.15	0.0718	0.0519	0.219	0.142	0.174	0.166	0.163	0.154	0.657
41.25	8.996	0.643	0.168	0.75	0.347	0.559	0.117	0.409	0.151	0.072	0.0521	0.219	0.142	0.175	0.167	0.164	0.155	0.661
41.333	9.027	0.647	0.169	0.754	0.349	0.561	0.118	0.412	0.151	0.0722	0.0522	0.22	0.143	0.176	0.168	0.165	0.156	0.665
41.417	9.058	0.65	0.17	0.758	0.351	0.564	0.118	0.414	0.152	0.0724	0.0523	0.221	0.143	0.177	0.169	0.166	0.156	0.668
41.5	9.089	0.654	0.171	0.763	0.353	0.567	0.119	0.416	0.153	0.0727	0.0524	0.221	0.143	0.178	0.17	0.167	0.157	0.672
41.583	9.12	0.658	0.172	0.767	0.355	0.57	0.12	0.418	0.154	0.0728	0.0525	0.222	0.143	0.179	0.171	0.168	0.158	0.676
41.667	9.152	0.661	0.173	0.771	0.357	0.572	0.12	0.42	0.155	0.073	0.0526	0.222	0.143	0.18	0.172	0.169	0.159	0.68
41.75	9.183	0.665	0.174	0.776	0.359	0.575	0.121	0.422	0.155	0.0732	0.0526	0.223	0.143	0.181	0.173	0.17	0.16	0.684
41.833	9.215	0.668	0.175	0.78	0.361	0.578	0.122	0.424	0.156	0.0733	0.0527	0.223	0.143	0.182	0.174	0.171	0.161	0.688
41.917	9.247	0.672	0.175	0.784	0.363	0.581	0.122	0.427	0.157	0.0735	0.0527	0.224	0.143	0.183	0.175	0.172	0.162	0.692
42	9.279	0.675	0.176	0.788	0.365	0.584	0.123	0.429	0.158	0.0736	0.0528	0.224	0.143	0.183	0.176	0.173	0.163	0.695
42.083	9.311	0.679	0.177	0.793	0.367	0.587	0.123	0.431	0.158	0.0737	0.0528	0.225	0.143	0.184	0.177	0.174	0.164	0.699
42.167	9.343	0.682	0.178	0.797	0.369	0.59	0.124	0.433	0.159	0.0738	0.0529	0.225	0.143	0.185	0.178	0.175	0.165	0.703
42.25	9.375	0.686	0.178	0.801	0.371	0.592	0.125	0.435	0.16	0.074	0.0529	0.225	0.143	0.186	0.178	0.176	0.166	0.706
42.333	9.408	0.689	0.179	0.805	0.372	0.595	0.125	0.437	0.161	0.0741	0.0529	0.226	0.143	0.187	0.179	0.177	0.167	0.71
42.417	9.44	0.693	0.18	0.81	0.374	0.598	0.126	0.439	0.162	0.0742	0.0529	0.226	0.143	0.188	0.18	0.177	0.168	0.713

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
42.5	9.473	0.696	0.18	0.814	0.376	0.601	0.126	0.441	0.162	0.0743	0.0529	0.226	0.144	0.189	0.181	0.178	0.169	0.717
42.583	9.506	0.7	0.181	0.818	0.378	0.604	0.127	0.444	0.163	0.0744	0.053	0.227	0.144	0.19	0.182	0.179	0.17	0.721
42.667	9.539	0.703	0.182	0.822	0.38	0.608	0.128	0.446	0.164	0.0746	0.0531	0.227	0.144	0.191	0.183	0.18	0.17	0.724
42.75	9.572	0.707	0.182	0.826	0.382	0.611	0.128	0.448	0.165	0.0747	0.0531	0.227	0.144	0.192	0.184	0.181	0.171	0.728
42.833	9.605	0.71	0.183	0.831	0.384	0.614	0.129	0.45	0.165	0.0748	0.0532	0.228	0.145	0.193	0.185	0.182	0.172	0.732
42.917	9.638	0.714	0.183	0.835	0.386	0.617	0.129	0.452	0.166	0.075	0.0533	0.228	0.145	0.194	0.186	0.183	0.173	0.736
43	9.671	0.717	0.184	0.839	0.388	0.62	0.13	0.454	0.167	0.0751	0.0535	0.229	0.146	0.195	0.187	0.184	0.174	0.74
43.083	9.705	0.721	0.184	0.843	0.39	0.623	0.131	0.456	0.168	0.0753	0.0536	0.229	0.146	0.195	0.188	0.185	0.175	0.743
43.167	9.739	0.724	0.185	0.848	0.392	0.626	0.131	0.458	0.169	0.0754	0.0538	0.23	0.147	0.196	0.189	0.186	0.176	0.747
43.25	9.772	0.728	0.186	0.852	0.394	0.63	0.132	0.46	0.169	0.0756	0.0539	0.23	0.147	0.197	0.189	0.187	0.177	0.75
43.333	9.806	0.731	0.186	0.856	0.396	0.633	0.133	0.462	0.17	0.0757	0.0541	0.231	0.148	0.198	0.19	0.188	0.178	0.754
43.417	9.84	0.735	0.187	0.86	0.397	0.636	0.133	0.464	0.171	0.0759	0.0542	0.231	0.148	0.199	0.191	0.188	0.179	0.757
43.5	9.874	0.738	0.187	0.864	0.399	0.639	0.134	0.465	0.172	0.0761	0.0544	0.232	0.149	0.2	0.192	0.189	0.18	0.761
43.583	9.909	0.742	0.188	0.869	0.401	0.643	0.134	0.467	0.172	0.0763	0.0545	0.233	0.149	0.201	0.193	0.19	0.181	0.765
43.667	9.943	0.746	0.188	0.873	0.403	0.646	0.135	0.469	0.173	0.0764	0.0547	0.233	0.149	0.202	0.194	0.191	0.182	0.769
43.75	9.977	0.749	0.189	0.877	0.405	0.649	0.136	0.471	0.174	0.0766	0.0548	0.234	0.15	0.203	0.195	0.192	0.182	0.772
43.833	10.012	0.753	0.189	0.881	0.407	0.652	0.136	0.473	0.175	0.0768	0.0549	0.234	0.15	0.204	0.196	0.193	0.183	0.776
43.917	10.047	0.756	0.19	0.886	0.409	0.656	0.137	0.475	0.175	0.0769	0.055	0.235	0.15	0.205	0.197	0.194	0.184	0.78
44	10.082	0.76	0.19	0.89	0.411	0.659	0.137	0.476	0.176	0.0771	0.0551	0.235	0.15	0.206	0.198	0.195	0.185	0.784
44.083	10.117	0.763	0.191	0.894	0.413	0.662	0.138	0.478	0.177	0.0772	0.0552	0.236	0.15	0.207	0.199	0.196	0.186	0.788
44.167	10.152	0.767	0.191	0.899	0.415	0.665	0.139	0.48	0.177	0.0773	0.0552	0.236	0.151	0.207	0.2	0.197	0.187	0.791
44.25	10.187	0.77	0.192	0.903	0.417	0.669	0.139	0.482	0.178	0.0775	0.0553	0.237	0.151	0.208	0.201	0.198	0.188	0.795
44.333	10.223	0.774	0.192	0.907	0.418	0.672	0.14	0.483	0.179	0.0776	0.0554	0.237	0.151	0.209	0.202	0.199	0.189	0.799
44.417	10.258	0.777	0.193	0.911	0.42	0.675	0.14	0.485	0.179	0.0777	0.0554	0.237	0.151	0.21	0.202	0.2	0.19	0.802
44.5	10.294	0.781	0.193	0.916	0.422	0.678	0.141	0.487	0.18	0.0778	0.0555	0.238	0.151	0.211	0.203	0.201	0.191	0.806
44.583	10.33	0.784	0.194	0.92	0.424	0.681	0.142	0.488	0.181	0.0779	0.0555	0.238	0.151	0.212	0.204	0.201	0.192	0.809
44.667	10.366	0.787	0.194	0.924	0.426	0.684	0.142	0.49	0.181	0.078	0.0556	0.238	0.151	0.213	0.205	0.202	0.193	0.813
44.75	10.402	0.791	0.195	0.928	0.427	0.688	0.143	0.492	0.182	0.0781	0.0556	0.238	0.151	0.214	0.206	0.203	0.194	0.817
44.833	10.438	0.794	0.195	0.932	0.429	0.691	0.143	0.493	0.183	0.0781	0.0556	0.239	0.151	0.215	0.207	0.204	0.194	0.82
44.917	10.475	0.797	0.196	0.937	0.431	0.694	0.144	0.495	0.183	0.0782	0.0557	0.239	0.151	0.216	0.208	0.205	0.195	0.824
45	10.511	0.8	0.196	0.941	0.432	0.697	0.145	0.496	0.184	0.0783	0.0557	0.239	0.151	0.217	0.209	0.206	0.196	0.828
45.083	10.548	0.803	0.197	0.945	0.434	0.7	0.145	0.498	0.185	0.0783	0.0557	0.239	0.151	0.217	0.21	0.207	0.197	0.831
45.167	10.584	0.807	0.197	0.949	0.436	0.703	0.146	0.499	0.185	0.0784	0.0557	0.239	0.151	0.218	0.211	0.208	0.198	0.835
45.25	10.621	0.81	0.197	0.953	0.437	0.707	0.146	0.501	0.186	0.0785	0.0557	0.24	0.151	0.219	0.211	0.209	0.199	0.838
45.333	10.658	0.813	0.198	0.957	0.439	0.71	0.147	0.502	0.187	0.0785	0.0558	0.24	0.151	0.22	0.212	0.209	0.2	0.841
45.417	10.695	0.816	0.198	0.96	0.441	0.713	0.147	0.504	0.187	0.0786	0.0558	0.24	0.151	0.221	0.213	0.21	0.201	0.845
45.5	10.733	0.819	0.199	0.964	0.442	0.716	0.148	0.505	0.188	0.0787	0.0558	0.24	0.152	0.222	0.214	0.211	0.201	0.848
45.583	10.77	0.822	0.199	0.968	0.444	0.719	0.148	0.507	0.188	0.0788	0.0559	0.241	0.152	0.223	0.215	0.212	0.202	0.852
45.667	10.808	0.825	0.199	0.972	0.445	0.722	0.149	0.508	0.189	0.0789	0.056	0.241	0.152	0.223	0.216	0.213	0.203	0.855
45.75	10.845	0.828	0.2	0.976	0.447	0.726	0.149	0.51	0.19	0.079	0.0561	0.241	0.153	0.224	0.216	0.214	0.204	0.858
45.833	10.883	0.831	0.2	0.98	0.449	0.729	0.15	0.511	0.19	0.0792	0.0564	0.242	0.154	0.225	0.217	0.214	0.205	0.861
45.917	10.921	0.834	0.201	0.983	0.45	0.732	0.15	0.513	0.191	0.0794	0.0566	0.243	0.155	0.226	0.218	0.215	0.206	0.865
46	10.959	0.837	0.201	0.987	0.452	0.735	0.151	0.514	0.192	0.0796	0.0568	0.243	0.155	0.227	0.219	0.216	0.206	0.868
46.083	10.998	0.84	0.202	0.991	0.454	0.739	0.152	0.516	0.192	0.0798	0.0571	0.244	0.157	0.228	0.22	0.217	0.207	0.872
46.167	11.036	0.843	0.202	0.995	0.455	0.742	0.152	0.517	0.193	0.08	0.0574	0.245	0.158	0.228	0.221	0.218	0.208	0.875
46.25	11.075	0.846	0.202	0.999	0.457	0.745	0.153	0.519	0.193	0.0803	0.0577	0.246	0.159	0.229	0.221	0.219	0.209	0.878
46.333	11.114	0.849	0.203	1.003	0.458	0.748	0.153	0.52	0.194	0.0806	0.058	0.247	0.16	0.23	0.222	0.219	0.21	0.881
46.417	11.152	0.852	0.204	1.006	0.46	0.752	0.154	0.522	0.195	0.0809	0.0584	0.249	0.16	0.231	0.223	0.22	0.211	0.885
46.5	11.191	0.855	0.204	1.01	0.462	0.755	0.154	0.523	0.195	0.0812	0.0587	0.25	0.161	0.232	0.224	0.221	0.211	0.888
46.583	11.23	0.858	0.205	1.014	0.463	0.758	0.155	0.525	0.196	0.0815	0.0589	0.251	0.162	0.232	0.225	0.222	0.212	0.891
46.667	11.27	0.861	0.205	1.018	0.465	0.761	0.155	0.526	0.197	0.0818	0.0592	0.252	0.163	0.233	0.226	0.223	0.213	0.895
46.75	11.309	0.865	0.206	1.021	0.467	0.765	0.156	0.528	0.197	0.0822	0.0595	0.253	0.163	0.234	0.226	0.224	0.214	0.898
46.833	11.349	0.868	0.206	1.025	0.468	0.768	0.156	0.529	0.198	0.0825	0.0597	0.254	0.164	0.235	0.227	0.224	0.215	0.901
46.917	11.389	0.871	0.207	1.029	0.47	0.771	0.157	0.531	0.199	0.0828	0.0599	0.256	0.164	0.236	0.228	0.225	0.216	0.905
47	11.428	0.874	0.208	1.033	0.472	0.774	0.157	0.532	0.199	0.0831	0.0601	0.257	0.165	0.237	0.229	0.226	0.216	0.908
47.083	11.468	0.877	0.208	1.037	0.473	0.777	0.158	0.534	0.2	0.0834	0.0602	0.257	0.165	0.237	0.23	0.227	0.217	0.911
47.167	11.509	0.88	0.209	1.041	0.475	0.781	0.159	0.536	0.2	0.0836	0.0604	0.258	0.165	0.238	0.231	0.228	0.218	0.915
47.25	11.549	0.883	0.21	1.044	0.477	0.784	0.159	0.537	0.201	0.0839	0.0605	0.259	0.166	0.239	0.231	0.228	0.219	0.917
47.333	11.589	0.886	0.211	1.048	0.478	0.787	0.16	0.539	0.202	0.0841	0.0606	0.26	0.166	0.24	0.232	0.229	0.22	0.921
47.417	11.63	0.889	0.211	1.052	0.48	0.79	0.16	0.54	0.202	0.0843	0.0607	0.261	0.166	0.241	0.233	0.23	0.221	0.925
47.5	11.671	0.893	0.212	1.056	0.482	0.793	0.161	0.542	0.203	0.0846	0.0609	0.261	0.166	0.242	0.234	0.231	0.221	0.928
47.583	11.712	0.896	0.213	1.06	0.483	0.796	0.161	0.543	0.203	0.0847	0.0609	0.262	0.167	0.242	0.235	0.232	0.222	0.931
47.667	11.753	0.899	0.214	1.064	0.485	0.799	0.162	0.545	0.204	0.0849	0.061	0.262	0.167	0.243	0.236	0.233	0.223	0.935
47.75	11.794	0.902	0.214	1.068	0.487	0.803	0.162	0.546	0.205	0.0851	0.0611	0.263	0.167	0.244	0.236	0.233	0.224	0.937
47.833	11.835	0.905	0.215	1.071	0.488	0.806	0.163	0.548	0.205	0.0852	0.0612	0.263	0.167	0.245	0.237	0.234	0.225	0.941
47.917	11.877	0.908	0.216	1.075	0.49	0.809	0.163	0.55	0.206	0.0854	0.0612	0.264	0.167	0.246	0.238	0.235	0.226	0.945
48	11.918	0.911	0.216	1.079	0.491	0.812	0.164	0.551	0.207	0.0855	0.0613	0.264	0.167	0.247	0.239	0.236	0.226	0.948

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
48.083	11.96	0.914	0.217	1.083	0.493	0.815	0.164	0.553	0.207	0.0857	0.0613	0.265	0.167	0.247	0.24	0.237	0.227	0.951
48.167	12.002	0.917	0.218	1.086	0.494	0.818	0.165	0.554	0.208	0.0858	0.0614	0.265	0.167	0.248	0.24	0.238	0.228	0.954
48.25	12.044	0.92	0.218	1.09	0.496	0.821	0.166	0.556	0.208	0.0859	0.0614	0.265	0.167	0.249	0.241	0.238	0.229	0.957
48.333	12.087	0.923	0.219	1.094	0.498	0.824	0.166	0.558	0.209	0.0861	0.0615	0.266	0.167	0.25	0.242	0.239	0.23	0.961
48.417	12.129	0.926	0.22	1.098	0.499	0.827	0.167	0.559	0.21	0.0862	0.0615	0.266	0.167	0.251	0.243	0.24	0.23	0.964
48.5	12.171	0.929	0.22	1.101	0.501	0.83	0.167	0.561	0.21	0.0863	0.0616	0.267	0.168	0.251	0.244	0.241	0.231	0.967
48.583	12.214	0.932	0.221	1.105	0.503	0.833	0.168	0.563	0.211	0.0866	0.0618	0.267	0.169	0.252	0.245	0.242	0.232	0.971
48.667	12.257	0.935	0.222	1.109	0.504	0.837	0.168	0.565	0.212	0.0869	0.0621	0.268	0.17	0.253	0.245	0.243	0.233	0.974
48.75	12.3	0.938	0.222	1.113	0.506	0.84	0.169	0.567	0.212	0.0871	0.0623	0.269	0.171	0.254	0.246	0.243	0.234	0.977
48.833	12.343	0.941	0.223	1.117	0.508	0.843	0.169	0.569	0.213	0.0875	0.0628	0.271	0.173	0.255	0.247	0.244	0.235	0.981
48.917	12.387	0.945	0.224	1.121	0.51	0.846	0.17	0.571	0.214	0.0879	0.0633	0.272	0.175	0.256	0.248	0.245	0.236	0.985
49	12.43	0.948	0.225	1.125	0.511	0.849	0.17	0.573	0.215	0.0883	0.0639	0.274	0.177	0.257	0.249	0.246	0.236	0.988
49.083	12.474	0.951	0.226	1.129	0.513	0.853	0.171	0.575	0.215	0.0889	0.0646	0.276	0.179	0.258	0.25	0.247	0.237	0.992
49.167	12.518	0.955	0.227	1.133	0.515	0.856	0.172	0.577	0.216	0.0895	0.0654	0.279	0.182	0.258	0.251	0.248	0.238	0.995
49.25	12.562	0.958	0.228	1.138	0.517	0.859	0.172	0.579	0.217	0.0901	0.0661	0.281	0.185	0.259	0.252	0.249	0.239	0.999
49.333	12.606	0.962	0.229	1.142	0.519	0.863	0.173	0.582	0.218	0.0908	0.0669	0.284	0.187	0.26	0.253	0.25	0.24	1.003
49.417	12.65	0.966	0.23	1.146	0.521	0.866	0.174	0.584	0.219	0.0915	0.0677	0.287	0.189	0.261	0.254	0.251	0.241	1.007
49.5	12.695	0.969	0.231	1.151	0.523	0.87	0.174	0.586	0.22	0.0922	0.0685	0.289	0.192	0.262	0.254	0.252	0.242	1.01
49.583	12.739	0.973	0.233	1.155	0.526	0.873	0.175	0.589	0.22	0.093	0.0692	0.293	0.194	0.263	0.255	0.253	0.243	1.014
49.667	12.784	0.977	0.234	1.16	0.528	0.876	0.176	0.591	0.221	0.0939	0.0699	0.296	0.195	0.264	0.256	0.254	0.244	1.018
49.75	12.829	0.981	0.235	1.164	0.53	0.88	0.176	0.594	0.222	0.0947	0.0706	0.299	0.197	0.265	0.257	0.255	0.245	1.022
49.833	12.874	0.985	0.237	1.169	0.532	0.883	0.177	0.596	0.223	0.0955	0.0711	0.301	0.198	0.266	0.259	0.256	0.246	1.027
49.917	12.919	0.989	0.238	1.174	0.534	0.887	0.178	0.599	0.224	0.0963	0.0716	0.304	0.199	0.267	0.26	0.257	0.247	1.031
50	12.965	0.993	0.24	1.179	0.537	0.89	0.178	0.602	0.225	0.097	0.0721	0.307	0.201	0.268	0.261	0.258	0.248	1.035
50.083	13.01	0.998	0.242	1.184	0.539	0.894	0.179	0.604	0.226	0.0977	0.0725	0.309	0.201	0.269	0.262	0.259	0.249	1.039
50.167	13.056	1.002	0.243	1.189	0.541	0.898	0.18	0.607	0.227	0.0984	0.0729	0.311	0.202	0.27	0.263	0.26	0.25	1.043
50.25	13.102	1.006	0.245	1.194	0.544	0.901	0.181	0.61	0.228	0.0991	0.0733	0.313	0.203	0.272	0.264	0.261	0.251	1.048
50.333	13.148	1.011	0.247	1.199	0.546	0.905	0.181	0.613	0.229	0.0996	0.0735	0.315	0.204	0.273	0.265	0.262	0.253	1.053
50.417	13.195	1.015	0.249	1.204	0.548	0.908	0.182	0.616	0.229	0.1	0.0738	0.317	0.204	0.274	0.266	0.263	0.254	1.057
50.5	13.241	1.019	0.251	1.209	0.551	0.912	0.183	0.619	0.23	0.101	0.0741	0.318	0.205	0.275	0.267	0.264	0.255	1.061
50.583	13.288	1.024	0.253	1.214	0.553	0.916	0.184	0.622	0.231	0.101	0.0744	0.32	0.205	0.276	0.268	0.266	0.256	1.066
50.667	13.334	1.028	0.254	1.22	0.556	0.919	0.184	0.625	0.232	0.102	0.0746	0.321	0.206	0.277	0.27	0.267	0.257	1.071
50.75	13.381	1.032	0.256	1.225	0.558	0.923	0.185	0.628	0.233	0.102	0.0748	0.323	0.206	0.278	0.271	0.268	0.258	1.075
50.833	13.428	1.037	0.258	1.23	0.561	0.927	0.186	0.631	0.234	0.103	0.075	0.324	0.206	0.28	0.272	0.269	0.259	1.08
50.917	13.476	1.041	0.26	1.236	0.563	0.93	0.187	0.634	0.235	0.103	0.0751	0.325	0.206	0.281	0.273	0.27	0.261	1.085
51	13.523	1.046	0.261	1.241	0.565	0.934	0.188	0.638	0.236	0.103	0.0753	0.326	0.206	0.282	0.274	0.271	0.262	1.089
51.083	13.571	1.05	0.263	1.247	0.568	0.938	0.188	0.641	0.237	0.104	0.0754	0.327	0.206	0.283	0.275	0.273	0.263	1.094
51.167	13.619	1.055	0.264	1.252	0.571	0.941	0.189	0.644	0.239	0.104	0.0755	0.328	0.206	0.284	0.277	0.274	0.264	1.099
51.25	13.666	1.06	0.266	1.258	0.573	0.945	0.19	0.648	0.24	0.104	0.0756	0.329	0.206	0.285	0.278	0.275	0.265	1.103
51.333	13.715	1.064	0.267	1.263	0.576	0.949	0.191	0.651	0.241	0.104	0.0756	0.33	0.206	0.287	0.279	0.276	0.267	1.109
51.417	13.763	1.069	0.269	1.269	0.578	0.953	0.191	0.655	0.242	0.105	0.0756	0.33	0.206	0.288	0.28	0.277	0.268	1.113
51.5	13.811	1.074	0.27	1.274	0.581	0.957	0.192	0.658	0.243	0.105	0.0756	0.331	0.206	0.289	0.281	0.279	0.269	1.118
51.583	13.86	1.078	0.271	1.28	0.583	0.96	0.193	0.662	0.244	0.105	0.0756	0.332	0.206	0.29	0.283	0.28	0.27	1.123
51.667	13.909	1.083	0.272	1.285	0.586	0.964	0.194	0.666	0.245	0.105	0.0756	0.332	0.206	0.292	0.284	0.281	0.272	1.129
51.75	13.958	1.088	0.274	1.291	0.589	0.968	0.195	0.669	0.246	0.106	0.0756	0.333	0.206	0.293	0.285	0.282	0.273	1.133
51.833	14.007	1.093	0.275	1.297	0.591	0.972	0.196	0.673	0.247	0.106	0.0756	0.333	0.206	0.294	0.286	0.283	0.274	1.137
51.917	14.056	1.097	0.276	1.302	0.594	0.976	0.196	0.676	0.249	0.106	0.0756	0.333	0.206	0.295	0.288	0.285	0.275	1.143
52	14.106	1.102	0.277	1.308	0.597	0.98	0.197	0.68	0.25	0.106	0.0756	0.334	0.206	0.296	0.289	0.286	0.276	1.147
52.083	14.156	1.107	0.278	1.314	0.6	0.984	0.198	0.683	0.251	0.106	0.0756	0.334	0.206	0.298	0.29	0.287	0.278	1.153
52.167	14.206	1.112	0.279	1.319	0.602	0.988	0.199	0.686	0.252	0.106	0.0756	0.334	0.206	0.299	0.291	0.288	0.279	1.157
52.25	14.255	1.117	0.28	1.325	0.605	0.992	0.2	0.689	0.253	0.107	0.0756	0.334	0.206	0.3	0.293	0.29	0.28	1.163
52.333	14.306	1.122	0.281	1.331	0.608	0.996	0.201	0.692	0.255	0.107	0.0756	0.334	0.206	0.301	0.294	0.291	0.282	1.168
52.417	14.356	1.127	0.281	1.337	0.611	1	0.201	0.695	0.256	0.107	0.0756	0.334	0.206	0.303	0.295	0.292	0.283	1.173
52.5	14.407	1.132	0.282	1.343	0.614	1.004	0.202	0.699	0.257	0.107	0.0756	0.334	0.206	0.304	0.296	0.294	0.284	1.178
52.583	14.458	1.137	0.283	1.349	0.616	1.008	0.203	0.701	0.258	0.107	0.0756	0.334	0.206	0.305	0.298	0.295	0.285	1.183
52.667	14.509	1.142	0.284	1.355	0.619	1.012	0.204	0.704	0.259	0.107	0.0756	0.334	0.206	0.307	0.299	0.296	0.287	1.189
52.75	14.559	1.147	0.284	1.361	0.622	1.016	0.205	0.707	0.26	0.107	0.0756	0.334	0.206	0.308	0.3	0.297	0.288	1.193
52.833	14.611	1.152	0.285	1.367	0.625	1.02	0.206	0.71	0.262	0.107	0.0756	0.334	0.206	0.309	0.302	0.299	0.289	1.199
52.917	14.663	1.157	0.286	1.373	0.628	1.024	0.207	0.713	0.263	0.107	0.0756	0.334	0.206	0.311	0.303	0.3	0.291	1.205
53	14.714	1.163	0.286	1.379	0.631	1.028	0.208	0.715	0.264	0.107	0.0756	0.334	0.206	0.312	0.304	0.301	0.292	1.209
53.083	14.766	1.168	0.287	1.385	0.634	1.032	0.208	0.718	0.265	0.107	0.0756	0.334	0.206	0.313	0.305	0.303	0.293	1.214
53.167	14.818	1.173	0.287	1.391	0.636	1.037	0.209	0.72	0.266	0.107	0.0756	0.334	0.206	0.314	0.307	0.304	0.295	1.22
53.25	14.87	1.178	0.288	1.397	0.639	1.041	0.21	0.723	0.267	0.107	0.0756	0.334	0.206	0.316	0.308	0.305	0.296	1.225
53.333	14.923	1.183	0.288	1.403	0.642	1.045	0.211	0.725	0.268	0.107	0.0756	0.334	0.206	0.317	0.31	0.307	0.297	1.231
53.417	14.975	1.188	0.289	1.409	0.644	1.049	0.212	0.728	0.269	0.107	0.0756	0.334	0.206	0.319	0.311	0.308	0.299	1.237
53.5	15.028	1.193	0.289	1.415	0.647	1.053	0.213	0.73	0.27	0.107	0.0756	0.334	0.206	0.32	0.312	0.309	0.3	1.241
53.583	15.081	1.198	0.29	1.422	0.65	1.057	0.214	0.732	0.271	0.107	0.0756	0.334	0.206	0.321	0.314	0.311	0.301	1.247

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
53.667	15.134	1.203	0.29	1.428	0.652	1.061	0.215	0.734	0.272	0.107	0.0756	0.334	0.206	0.322	0.315	0.312	0.303	1.252
53.75	15.187	1.208	0.291	1.434	0.655	1.065	0.215	0.737	0.273	0.107	0.0756	0.334	0.206	0.324	0.316	0.313	0.304	1.257
53.833	15.241	1.212	0.291	1.44	0.657	1.069	0.216	0.739	0.273	0.107	0.0756	0.334	0.206	0.325	0.317	0.315	0.305	1.262
53.917	15.295	1.217	0.292	1.446	0.66	1.073	0.217	0.741	0.274	0.107	0.0756	0.334	0.206	0.326	0.319	0.316	0.307	1.268
54	15.349	1.221	0.292	1.452	0.662	1.077	0.218	0.743	0.275	0.107	0.0756	0.334	0.206	0.328	0.32	0.317	0.308	1.273
54.083	15.403	1.226	0.292	1.457	0.664	1.081	0.219	0.744	0.276	0.107	0.0756	0.334	0.206	0.329	0.321	0.318	0.309	1.277
54.167	15.457	1.23	0.293	1.463	0.667	1.085	0.219	0.746	0.277	0.107	0.0756	0.334	0.206	0.33	0.322	0.32	0.31	1.282
54.25	15.512	1.235	0.293	1.469	0.669	1.089	0.22	0.748	0.278	0.107	0.0756	0.334	0.206	0.331	0.324	0.321	0.311	1.287
54.333	15.566	1.239	0.293	1.474	0.671	1.093	0.221	0.75	0.279	0.107	0.0756	0.334	0.206	0.333	0.325	0.322	0.313	1.293
54.417	15.621	1.243	0.294	1.479	0.673	1.097	0.222	0.751	0.279	0.107	0.0756	0.334	0.206	0.334	0.326	0.323	0.314	1.297
54.5	15.676	1.247	0.294	1.485	0.675	1.101	0.222	0.753	0.28	0.107	0.0757	0.334	0.206	0.335	0.327	0.324	0.315	1.301
54.583	15.732	1.251	0.294	1.49	0.677	1.105	0.223	0.755	0.281	0.107	0.0757	0.335	0.207	0.336	0.328	0.326	0.316	1.306
54.667	15.787	1.255	0.295	1.495	0.68	1.109	0.224	0.756	0.282	0.107	0.0758	0.335	0.207	0.337	0.33	0.327	0.317	1.311
54.75	15.842	1.259	0.295	1.501	0.682	1.114	0.225	0.758	0.283	0.107	0.0759	0.335	0.207	0.338	0.331	0.328	0.318	1.315
54.833	15.898	1.263	0.295	1.506	0.684	1.118	0.225	0.759	0.283	0.107	0.0761	0.336	0.208	0.339	0.332	0.329	0.32	1.32
54.917	15.954	1.267	0.296	1.511	0.686	1.122	0.226	0.761	0.284	0.107	0.0763	0.336	0.209	0.341	0.333	0.33	0.321	1.325
55	16.01	1.271	0.296	1.516	0.688	1.126	0.227	0.763	0.285	0.108	0.0764	0.337	0.209	0.342	0.334	0.331	0.322	1.329
55.083	16.067	1.275	0.296	1.521	0.69	1.131	0.227	0.764	0.286	0.108	0.0767	0.337	0.21	0.343	0.335	0.332	0.323	1.333
55.167	16.124	1.279	0.297	1.526	0.692	1.135	0.228	0.766	0.286	0.108	0.077	0.338	0.212	0.344	0.336	0.333	0.324	1.337
55.25	16.18	1.283	0.297	1.531	0.694	1.139	0.229	0.767	0.287	0.108	0.0773	0.339	0.213	0.345	0.337	0.334	0.325	1.341
55.333	16.237	1.287	0.297	1.536	0.696	1.143	0.229	0.769	0.288	0.108	0.0776	0.34	0.214	0.346	0.338	0.335	0.326	1.345
55.417	16.295	1.29	0.298	1.541	0.698	1.148	0.23	0.77	0.288	0.109	0.078	0.341	0.215	0.347	0.339	0.337	0.327	1.35
55.5	16.352	1.294	0.298	1.546	0.7	1.152	0.231	0.772	0.289	0.109	0.0783	0.342	0.216	0.348	0.34	0.338	0.328	1.354
55.583	16.41	1.298	0.299	1.55	0.702	1.156	0.231	0.774	0.29	0.109	0.0786	0.344	0.216	0.349	0.341	0.339	0.329	1.358
55.667	16.467	1.302	0.299	1.555	0.704	1.161	0.232	0.775	0.291	0.11	0.0789	0.345	0.217	0.35	0.343	0.34	0.33	1.363
55.75	16.525	1.305	0.299	1.56	0.705	1.165	0.233	0.777	0.291	0.11	0.0791	0.346	0.218	0.351	0.344	0.341	0.331	1.367
55.833	16.584	1.309	0.3	1.565	0.707	1.169	0.233	0.778	0.292	0.11	0.0794	0.347	0.218	0.352	0.345	0.342	0.332	1.371
55.917	16.642	1.312	0.3	1.569	0.709	1.173	0.234	0.78	0.293	0.111	0.0796	0.348	0.219	0.353	0.346	0.343	0.333	1.375
56	16.7	1.316	0.301	1.574	0.711	1.178	0.235	0.782	0.293	0.111	0.0798	0.349	0.219	0.354	0.347	0.344	0.334	1.379
56.083	16.759	1.32	0.301	1.578	0.713	1.182	0.235	0.783	0.294	0.111	0.08	0.35	0.22	0.355	0.348	0.345	0.335	1.383
56.167	16.818	1.323	0.302	1.583	0.715	1.186	0.236	0.785	0.295	0.111	0.0801	0.351	0.22	0.356	0.349	0.346	0.336	1.387
56.25	16.877	1.327	0.303	1.588	0.717	1.19	0.236	0.786	0.295	0.112	0.0803	0.352	0.22	0.357	0.35	0.347	0.337	1.391
56.333	16.937	1.33	0.303	1.592	0.718	1.194	0.237	0.788	0.296	0.112	0.0804	0.353	0.221	0.358	0.35	0.348	0.338	1.394
56.417	16.996	1.334	0.304	1.597	0.72	1.198	0.238	0.79	0.296	0.112	0.0805	0.354	0.221	0.359	0.351	0.349	0.339	1.398
56.5	17.056	1.337	0.305	1.601	0.722	1.202	0.238	0.791	0.297	0.112	0.0807	0.354	0.221	0.36	0.352	0.35	0.34	1.402
56.583	17.116	1.34	0.305	1.605	0.724	1.206	0.239	0.793	0.298	0.113	0.0807	0.355	0.221	0.361	0.353	0.351	0.341	1.406
56.667	17.176	1.344	0.306	1.61	0.725	1.21	0.24	0.795	0.298	0.113	0.0808	0.356	0.222	0.362	0.354	0.352	0.342	1.41
56.75	17.237	1.347	0.307	1.614	0.727	1.214	0.24	0.796	0.299	0.113	0.0809	0.356	0.222	0.363	0.355	0.352	0.343	1.413
56.833	17.297	1.35	0.307	1.619	0.729	1.217	0.241	0.798	0.3	0.113	0.081	0.357	0.222	0.364	0.356	0.353	0.344	1.417
56.917	17.358	1.354	0.308	1.623	0.731	1.221	0.241	0.799	0.3	0.113	0.0811	0.357	0.222	0.365	0.357	0.354	0.345	1.421
57	17.419	1.357	0.308	1.627	0.732	1.225	0.242	0.801	0.301	0.113	0.0811	0.358	0.222	0.366	0.358	0.355	0.346	1.425
57.083	17.48	1.36	0.309	1.631	0.734	1.229	0.242	0.803	0.302	0.114	0.0812	0.358	0.222	0.367	0.359	0.356	0.347	1.429
57.167	17.542	1.364	0.31	1.636	0.736	1.233	0.243	0.805	0.302	0.114	0.0812	0.358	0.222	0.368	0.36	0.357	0.348	1.433
57.25	17.603	1.367	0.31	1.64	0.737	1.236	0.244	0.806	0.303	0.114	0.0813	0.359	0.222	0.368	0.361	0.358	0.349	1.436
57.333	17.665	1.37	0.311	1.644	0.739	1.24	0.244	0.808	0.304	0.114	0.0813	0.359	0.222	0.369	0.362	0.359	0.35	1.44
57.417	17.727	1.373	0.311	1.648	0.741	1.244	0.245	0.81	0.304	0.114	0.0813	0.359	0.222	0.37	0.363	0.36	0.35	1.443
57.5	17.789	1.376	0.312	1.652	0.742	1.247	0.245	0.811	0.305	0.114	0.0813	0.36	0.222	0.371	0.363	0.361	0.351	1.446
57.583	17.852	1.379	0.312	1.656	0.744	1.251	0.246	0.813	0.306	0.114	0.0814	0.36	0.222	0.372	0.364	0.362	0.352	1.45
57.667	17.915	1.383	0.313	1.66	0.746	1.255	0.246	0.815	0.306	0.114	0.0815	0.361	0.222	0.373	0.365	0.362	0.353	1.453
57.75	17.977	1.386	0.313	1.664	0.747	1.258	0.247	0.817	0.307	0.115	0.0815	0.361	0.223	0.374	0.366	0.363	0.354	1.457
57.833	18.041	1.389	0.314	1.668	0.749	1.262	0.247	0.818	0.308	0.115	0.0817	0.362	0.223	0.375	0.367	0.364	0.355	1.461
57.917	18.104	1.392	0.314	1.672	0.751	1.265	0.248	0.82	0.308	0.115	0.0819	0.362	0.224	0.376	0.368	0.365	0.356	1.465
58	18.167	1.395	0.315	1.676	0.753	1.269	0.249	0.822	0.309	0.115	0.082	0.363	0.225	0.376	0.369	0.366	0.357	1.468
58.083	18.231	1.399	0.316	1.681	0.755	1.273	0.249	0.824	0.31	0.115	0.0823	0.364	0.226	0.377	0.37	0.367	0.358	1.472
58.167	18.295	1.402	0.316	1.685	0.756	1.276	0.25	0.826	0.31	0.116	0.0826	0.365	0.227	0.378	0.371	0.368	0.359	1.476
58.25	18.359	1.405	0.317	1.689	0.758	1.28	0.25	0.827	0.311	0.116	0.0829	0.365	0.228	0.379	0.371	0.369	0.359	1.478
58.333	18.423	1.408	0.317	1.693	0.76	1.283	0.251	0.829	0.312	0.116	0.0832	0.367	0.229	0.38	0.372	0.37	0.36	1.482
58.417	18.488	1.412	0.318	1.697	0.762	1.287	0.251	0.831	0.313	0.116	0.0836	0.368	0.23	0.381	0.373	0.37	0.361	1.485
58.5	18.553	1.415	0.319	1.701	0.764	1.29	0.252	0.832	0.313	0.117	0.0839	0.369	0.231	0.382	0.374	0.371	0.362	1.489
58.583	18.618	1.419	0.319	1.705	0.766	1.294	0.253	0.834	0.314	0.117	0.0842	0.37	0.232	0.383	0.375	0.372	0.363	1.493
58.667	18.683	1.422	0.32	1.709	0.767	1.297	0.253	0.836	0.315	0.117	0.0845	0.371	0.233	0.384	0.376	0.373	0.364	1.497
58.75	18.748	1.426	0.321	1.713	0.769	1.301	0.254	0.838	0.316	0.118	0.0848	0.373	0.233	0.384	0.377	0.374	0.365	1.5
58.833	18.814	1.429	0.321	1.718	0.771	1.305	0.254	0.839	0.316	0.118	0.085	0.374	0.234	0.385	0.378	0.375	0.366	1.504
58.917	18.88	1.433	0.322	1.722	0.773	1.308	0.255	0.841	0.317	0.118	0.0852	0.375	0.234	0.386	0.379	0.376	0.367	1.508
59	18.946	1.436	0.323	1.726	0.775	1.312	0.256	0.843	0.318	0.119	0.0854	0.376	0.235	0.387	0.38	0.377	0.368	1.512
59.083	19.012	1.44	0.324	1.73	0.777	1.315	0.256	0.844	0.318	0.119	0.0856	0.377	0.235	0.388	0.381	0.378	0.368	1.515
59.167	19.079	1.443	0.325	1.735	0.779	1.318	0.257	0.846	0.319	0.119	0.0858	0.378	0.236	0.389	0.381	0.379	0.369	1.518

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
59.25	19.145	1.447	0.325	1.739	0.781	1.322	0.258	0.848	0.32	0.12	0.0859	0.379	0.236	0.39	0.382	0.38	0.37	1.522
59.333	19.212	1.45	0.326	1.743	0.783	1.325	0.258	0.849	0.321	0.12	0.0861	0.379	0.236	0.391	0.383	0.381	0.371	1.526
59.417	19.279	1.454	0.327	1.748	0.784	1.329	0.259	0.851	0.321	0.12	0.0862	0.38	0.237	0.392	0.384	0.381	0.372	1.529
59.5	19.346	1.457	0.328	1.752	0.786	1.332	0.259	0.852	0.322	0.12	0.0863	0.381	0.237	0.393	0.385	0.382	0.373	1.533
59.583	19.414	1.461	0.329	1.756	0.788	1.336	0.26	0.854	0.323	0.121	0.0864	0.382	0.237	0.394	0.386	0.383	0.374	1.537
59.667	19.482	1.464	0.33	1.761	0.79	1.339	0.261	0.856	0.323	0.121	0.0865	0.382	0.237	0.395	0.387	0.384	0.375	1.541
59.75	19.549	1.468	0.331	1.765	0.792	1.343	0.261	0.857	0.324	0.121	0.0866	0.383	0.237	0.396	0.388	0.385	0.376	1.545
59.833	19.618	1.471	0.331	1.769	0.794	1.346	0.262	0.859	0.325	0.121	0.0867	0.383	0.237	0.397	0.389	0.386	0.377	1.549
59.917	19.686	1.475	0.332	1.774	0.796	1.349	0.262	0.861	0.325	0.121	0.0867	0.384	0.237	0.398	0.39	0.387	0.378	1.553
60	19.754	1.478	0.333	1.778	0.797	1.353	0.263	0.862	0.326	0.121	0.0868	0.384	0.237	0.399	0.391	0.388	0.379	1.557
60.083	19.823	1.482	0.334	1.782	0.799	1.356	0.264	0.864	0.327	0.122	0.0869	0.385	0.237	0.399	0.392	0.389	0.38	1.56
60.167	19.892	1.485	0.334	1.787	0.801	1.36	0.264	0.866	0.328	0.122	0.0869	0.385	0.237	0.4	0.393	0.39	0.381	1.564
60.25	19.961	1.489	0.335	1.791	0.803	1.363	0.265	0.867	0.328	0.122	0.0869	0.385	0.237	0.401	0.394	0.391	0.382	1.568
60.333	20.031	1.492	0.336	1.795	0.805	1.366	0.266	0.869	0.329	0.122	0.087	0.386	0.237	0.402	0.395	0.392	0.383	1.572
60.417	20.1	1.496	0.336	1.8	0.806	1.37	0.266	0.871	0.33	0.122	0.087	0.386	0.237	0.403	0.396	0.393	0.384	1.576
60.5	20.17	1.499	0.337	1.804	0.808	1.373	0.267	0.872	0.33	0.122	0.087	0.386	0.237	0.404	0.397	0.394	0.385	1.58
60.583	20.24	1.502	0.338	1.808	0.81	1.376	0.267	0.874	0.331	0.122	0.087	0.387	0.237	0.405	0.397	0.395	0.385	1.582
60.667	20.31	1.506	0.338	1.812	0.812	1.38	0.268	0.876	0.332	0.122	0.087	0.387	0.237	0.406	0.398	0.396	0.386	1.586
60.75	20.38	1.509	0.339	1.816	0.813	1.383	0.268	0.878	0.332	0.122	0.087	0.387	0.237	0.407	0.399	0.396	0.387	1.589
60.833	20.45	1.512	0.339	1.82	0.815	1.386	0.269	0.879	0.333	0.123	0.087	0.387	0.237	0.408	0.4	0.397	0.388	1.593
60.917	20.52	1.515	0.34	1.825	0.817	1.39	0.27	0.881	0.334	0.123	0.087	0.387	0.237	0.409	0.401	0.398	0.389	1.597
61	20.591	1.519	0.34	1.829	0.819	1.393	0.27	0.883	0.334	0.123	0.087	0.388	0.237	0.41	0.402	0.399	0.39	1.601
61.083	20.662	1.522	0.341	1.833	0.82	1.396	0.271	0.884	0.335	0.123	0.087	0.388	0.237	0.41	0.403	0.4	0.391	1.604
61.167	20.733	1.525	0.341	1.837	0.822	1.4	0.271	0.886	0.336	0.123	0.087	0.388	0.237	0.411	0.404	0.401	0.392	1.608
61.25	20.804	1.529	0.342	1.841	0.824	1.403	0.272	0.887	0.336	0.123	0.087	0.388	0.237	0.412	0.405	0.402	0.393	1.612
61.333	20.875	1.532	0.342	1.845	0.826	1.406	0.272	0.889	0.337	0.123	0.087	0.388	0.237	0.413	0.406	0.403	0.394	1.616
61.417	20.947	1.535	0.342	1.849	0.827	1.41	0.273	0.89	0.337	0.123	0.087	0.388	0.237	0.414	0.406	0.404	0.394	1.618
61.5	21.018	1.538	0.343	1.853	0.829	1.413	0.274	0.892	0.338	0.123	0.087	0.388	0.237	0.415	0.407	0.405	0.395	1.622
61.583	21.09	1.541	0.343	1.857	0.831	1.416	0.274	0.893	0.339	0.123	0.087	0.388	0.237	0.416	0.408	0.405	0.396	1.625
61.667	21.162	1.545	0.343	1.861	0.832	1.42	0.275	0.895	0.339	0.123	0.087	0.388	0.237	0.417	0.409	0.406	0.397	1.629
61.75	21.234	1.548	0.343	1.865	0.834	1.423	0.275	0.896	0.34	0.123	0.087	0.388	0.237	0.418	0.41	0.407	0.398	1.633
61.833	21.306	1.551	0.344	1.869	0.836	1.426	0.276	0.897	0.34	0.123	0.087	0.388	0.237	0.418	0.411	0.408	0.399	1.636
61.917	21.378	1.554	0.344	1.873	0.837	1.429	0.276	0.899	0.341	0.123	0.087	0.388	0.237	0.419	0.412	0.409	0.4	1.64
62	21.451	1.557	0.344	1.877	0.839	1.432	0.277	0.9	0.342	0.123	0.087	0.388	0.237	0.42	0.413	0.41	0.401	1.644
62.083	21.523	1.56	0.344	1.881	0.841	1.435	0.277	0.901	0.342	0.123	0.087	0.388	0.237	0.421	0.413	0.411	0.401	1.646
62.167	21.596	1.563	0.345	1.885	0.842	1.438	0.278	0.902	0.343	0.123	0.087	0.388	0.237	0.422	0.414	0.411	0.402	1.649
62.25	21.668	1.566	0.345	1.889	0.844	1.442	0.279	0.904	0.343	0.123	0.087	0.388	0.237	0.423	0.415	0.412	0.403	1.653
62.333	21.741	1.569	0.345	1.893	0.845	1.445	0.279	0.905	0.344	0.123	0.087	0.388	0.237	0.423	0.416	0.413	0.404	1.656
62.417	21.814	1.572	0.345	1.897	0.847	1.448	0.28	0.906	0.344	0.123	0.087	0.388	0.237	0.424	0.417	0.414	0.405	1.66
62.5	21.886	1.575	0.346	1.901	0.848	1.451	0.28	0.907	0.344	0.123	0.087	0.388	0.237	0.425	0.418	0.415	0.406	1.664
62.583	21.96	1.578	0.346	1.905	0.85	1.453	0.281	0.908	0.345	0.123	0.087	0.388	0.237	0.426	0.418	0.416	0.407	1.667
62.667	22.033	1.581	0.346	1.908	0.851	1.456	0.281	0.909	0.345	0.123	0.087	0.388	0.237	0.427	0.419	0.417	0.407	1.67
62.75	22.106	1.584	0.346	1.912	0.852	1.459	0.282	0.91	0.346	0.123	0.087	0.388	0.237	0.428	0.42	0.417	0.408	1.673
62.833	22.179	1.586	0.346	1.916	0.854	1.462	0.282	0.911	0.346	0.123	0.087	0.388	0.237	0.428	0.421	0.418	0.409	1.676
62.917	22.253	1.589	0.347	1.92	0.855	1.465	0.283	0.912	0.347	0.123	0.087	0.388	0.237	0.429	0.422	0.419	0.41	1.68
63	22.326	1.592	0.347	1.923	0.856	1.468	0.283	0.913	0.347	0.123	0.087	0.388	0.237	0.43	0.422	0.42	0.411	1.683
63.083	22.4	1.594	0.347	1.927	0.857	1.471	0.284	0.914	0.348	0.123	0.087	0.388	0.237	0.431	0.423	0.42	0.411	1.685
63.167	22.473	1.597	0.347	1.93	0.859	1.473	0.284	0.915	0.348	0.123	0.087	0.388	0.237	0.432	0.424	0.421	0.412	1.689
63.25	22.546	1.599	0.347	1.934	0.86	1.476	0.284	0.916	0.348	0.123	0.087	0.388	0.237	0.432	0.425	0.422	0.413	1.692
63.333	22.62	1.602	0.347	1.937	0.861	1.479	0.285	0.917	0.349	0.123	0.087	0.388	0.237	0.433	0.425	0.423	0.414	1.695
63.417	22.693	1.604	0.347	1.94	0.862	1.482	0.285	0.918	0.349	0.123	0.087	0.388	0.237	0.434	0.426	0.423	0.414	1.697
63.5	22.767	1.606	0.347	1.944	0.863	1.484	0.286	0.919	0.35	0.123	0.087	0.388	0.237	0.434	0.427	0.424	0.415	1.7
63.583	22.84	1.609	0.348	1.947	0.864	1.487	0.286	0.919	0.35	0.123	0.0869	0.388	0.237	0.435	0.428	0.425	0.416	1.704
63.667	22.914	1.611	0.348	1.95	0.865	1.49	0.287	0.92	0.35	0.123	0.0869	0.388	0.237	0.436	0.428	0.425	0.416	1.705
63.75	22.987	1.613	0.348	1.953	0.866	1.492	0.287	0.921	0.351	0.123	0.0868	0.388	0.237	0.436	0.429	0.426	0.417	1.708
63.833	23.061	1.615	0.348	1.956	0.867	1.495	0.287	0.921	0.351	0.123	0.0867	0.387	0.236	0.437	0.43	0.427	0.418	1.712
63.917	23.135	1.617	0.348	1.958	0.868	1.497	0.288	0.922	0.351	0.123	0.0865	0.387	0.236	0.438	0.43	0.427	0.418	1.713
64	23.209	1.619	0.348	1.961	0.869	1.5	0.288	0.922	0.352	0.123	0.0864	0.386	0.235	0.438	0.431	0.428	0.419	1.716
64.083	23.282	1.621	0.347	1.964	0.87	1.502	0.288	0.923	0.352	0.122	0.0861	0.386	0.234	0.439	0.431	0.429	0.419	1.718
64.167	23.356	1.622	0.347	1.966	0.871	1.505	0.289	0.923	0.352	0.122	0.0859	0.385	0.233	0.439	0.432	0.429	0.42	1.72
64.25	23.429	1.624	0.347	1.969	0.871	1.507	0.289	0.924	0.352	0.122	0.0856	0.384	0.232	0.44	0.432	0.43	0.421	1.723
64.333	23.503	1.626	0.347	1.971	0.872	1.509	0.289	0.924	0.353	0.122	0.0853	0.383	0.231	0.44	0.433	0.43	0.421	1.724
64.417	23.576	1.627	0.347	1.974	0.873	1.512	0.29	0.924	0.353	0.122	0.0849	0.382	0.23	0.441	0.433	0.431	0.422	1.727
64.5	23.649	1.629	0.346	1.976	0.874	1.514	0.29	0.924	0.353	0.121	0.0846	0.381	0.229	0.441	0.434	0.431	0.422	1.728
64.583	23.723	1.63	0.346	1.978	0.874	1.516	0.29	0.924	0.353	0.121	0.0843	0.38	0.228	0.442	0.434	0.432	0.423	1.731
64.667	23.796	1.631	0.346	1.981	0.875	1.518	0.29	0.924	0.353	0.121	0.084	0.378	0.227	0.442	0.435	0.432	0.423	1.732
64.75	23.869	1.633	0.345	1.983	0.875	1.521	0.291	0.925	0.354	0.12	0.0837	0.377	0.226	0.443	0.435	0.433	0.423	1.734

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
64.833	23.942	1.634	0.345	1.985	0.876	1.523	0.291	0.925	0.354	0.12	0.0835	0.376	0.226	0.443	0.436	0.433	0.424	1.736
64.917	24.015	1.635	0.344	1.986	0.876	1.525	0.291	0.925	0.354	0.12	0.0832	0.375	0.225	0.444	0.436	0.433	0.424	1.737
65	24.088	1.636	0.344	1.988	0.877	1.527	0.291	0.924	0.354	0.119	0.083	0.374	0.225	0.444	0.437	0.434	0.425	1.74
65.083	24.161	1.637	0.343	1.99	0.877	1.529	0.291	0.924	0.354	0.119	0.0828	0.373	0.224	0.444	0.437	0.434	0.425	1.74
65.167	24.234	1.638	0.343	1.992	0.878	1.531	0.292	0.924	0.354	0.119	0.0826	0.372	0.224	0.445	0.437	0.435	0.425	1.742
65.25	24.307	1.639	0.342	1.993	0.878	1.532	0.292	0.924	0.354	0.119	0.0825	0.371	0.223	0.445	0.438	0.435	0.426	1.744
65.333	24.379	1.64	0.341	1.995	0.879	1.534	0.292	0.924	0.354	0.118	0.0823	0.37	0.223	0.446	0.438	0.435	0.426	1.745
65.417	24.452	1.641	0.341	1.997	0.879	1.536	0.292	0.923	0.354	0.118	0.0822	0.369	0.223	0.446	0.438	0.436	0.426	1.746
65.5	24.524	1.641	0.34	1.998	0.879	1.538	0.292	0.923	0.354	0.118	0.0821	0.368	0.223	0.446	0.439	0.436	0.427	1.748
65.583	24.596	1.642	0.339	1.999	0.879	1.539	0.292	0.922	0.354	0.118	0.082	0.368	0.222	0.446	0.439	0.436	0.427	1.748
65.667	24.668	1.643	0.339	2.001	0.88	1.541	0.292	0.922	0.354	0.117	0.0819	0.367	0.222	0.447	0.439	0.436	0.427	1.749
65.75	24.74	1.643	0.338	2.002	0.88	1.542	0.293	0.921	0.354	0.117	0.0817	0.367	0.222	0.447	0.439	0.437	0.428	1.751
65.833	24.812	1.644	0.337	2.003	0.88	1.544	0.293	0.921	0.354	0.117	0.0817	0.366	0.222	0.447	0.44	0.437	0.428	1.752
65.917	24.884	1.644	0.337	2.004	0.88	1.545	0.293	0.92	0.354	0.117	0.0816	0.366	0.222	0.447	0.44	0.437	0.428	1.752
66	24.955	1.645	0.336	2.005	0.88	1.546	0.293	0.919	0.354	0.117	0.0815	0.365	0.222	0.448	0.44	0.437	0.428	1.753
66.083	25.026	1.645	0.336	2.006	0.88	1.548	0.293	0.919	0.354	0.117	0.0815	0.365	0.222	0.448	0.44	0.438	0.428	1.754
66.167	25.098	1.646	0.335	2.007	0.88	1.549	0.293	0.918	0.354	0.116	0.0814	0.364	0.222	0.448	0.441	0.438	0.429	1.756
66.25	25.169	1.646	0.334	2.008	0.88	1.55	0.293	0.917	0.354	0.116	0.0814	0.364	0.222	0.448	0.441	0.438	0.429	1.756
66.333	25.24	1.646	0.334	2.008	0.88	1.551	0.293	0.916	0.354	0.116	0.0814	0.364	0.222	0.448	0.441	0.438	0.429	1.756
66.417	25.311	1.646	0.333	2.009	0.88	1.552	0.293	0.915	0.354	0.116	0.0813	0.363	0.222	0.448	0.441	0.438	0.429	1.756
66.5	25.381	1.646	0.333	2.01	0.88	1.553	0.293	0.915	0.354	0.116	0.0813	0.363	0.222	0.449	0.441	0.438	0.429	1.757
66.583	25.452	1.646	0.332	2.01	0.88	1.554	0.293	0.914	0.354	0.116	0.0813	0.362	0.222	0.449	0.441	0.438	0.429	1.757
66.667	25.522	1.646	0.332	2.01	0.88	1.555	0.293	0.913	0.354	0.116	0.0812	0.362	0.221	0.449	0.441	0.438	0.429	1.757
66.75	25.592	1.646	0.331	2.011	0.88	1.556	0.293	0.912	0.353	0.116	0.0812	0.362	0.221	0.449	0.441	0.439	0.429	1.758
66.833	25.661	1.646	0.331	2.011	0.88	1.557	0.293	0.91	0.353	0.115	0.081	0.361	0.221	0.449	0.441	0.439	0.429	1.758
66.917	25.731	1.646	0.33	2.011	0.88	1.558	0.293	0.909	0.353	0.115	0.0809	0.361	0.22	0.449	0.441	0.439	0.43	1.759
67	25.8	1.646	0.33	2.011	0.879	1.559	0.293	0.908	0.353	0.115	0.0808	0.36	0.22	0.449	0.441	0.439	0.43	1.759
67.083	25.869	1.645	0.329	2.011	0.879	1.56	0.293	0.907	0.353	0.115	0.0805	0.359	0.219	0.449	0.441	0.439	0.43	1.759
67.167	25.938	1.645	0.329	2.011	0.879	1.56	0.293	0.906	0.352	0.115	0.0803	0.358	0.218	0.449	0.441	0.439	0.43	1.759
67.25	26.007	1.645	0.328	2.011	0.878	1.561	0.293	0.905	0.352	0.114	0.08	0.358	0.217	0.449	0.441	0.439	0.429	1.758
67.333	26.075	1.644	0.327	2.011	0.878	1.561	0.293	0.903	0.352	0.114	0.0797	0.357	0.215	0.449	0.441	0.439	0.429	1.758
67.417	26.143	1.643	0.327	2.01	0.877	1.562	0.293	0.902	0.351	0.114	0.0793	0.355	0.214	0.449	0.441	0.438	0.429	1.757
67.5	26.211	1.643	0.326	2.01	0.877	1.563	0.293	0.901	0.351	0.114	0.079	0.354	0.213	0.449	0.441	0.438	0.429	1.757
67.583	26.279	1.642	0.325	2.01	0.876	1.563	0.293	0.9	0.351	0.113	0.0787	0.353	0.213	0.449	0.441	0.438	0.429	1.757
67.667	26.346	1.641	0.325	2.009	0.876	1.564	0.292	0.898	0.35	0.113	0.0784	0.352	0.212	0.448	0.441	0.438	0.429	1.756
67.75	26.414	1.64	0.324	2.008	0.875	1.564	0.292	0.897	0.35	0.113	0.0781	0.351	0.211	0.448	0.441	0.438	0.429	1.756
67.833	26.48	1.639	0.323	2.008	0.874	1.564	0.292	0.896	0.35	0.112	0.0779	0.35	0.21	0.448	0.441	0.438	0.429	1.756
67.917	26.547	1.638	0.323	2.007	0.874	1.565	0.292	0.894	0.349	0.112	0.0776	0.348	0.21	0.448	0.44	0.438	0.429	1.755
68	26.613	1.637	0.322	2.006	0.873	1.565	0.292	0.893	0.349	0.112	0.0774	0.347	0.209	0.448	0.44	0.438	0.428	1.754
68.083	26.679	1.636	0.321	2.005	0.872	1.565	0.292	0.891	0.349	0.111	0.0772	0.346	0.209	0.448	0.44	0.437	0.428	1.753
68.167	26.745	1.635	0.32	2.004	0.871	1.565	0.291	0.89	0.348	0.111	0.077	0.345	0.208	0.447	0.44	0.437	0.428	1.752
68.25	26.81	1.633	0.32	2.003	0.87	1.565	0.291	0.889	0.348	0.111	0.0768	0.344	0.208	0.447	0.44	0.437	0.428	1.752
68.333	26.875	1.632	0.319	2.002	0.87	1.565	0.291	0.887	0.347	0.11	0.0767	0.343	0.208	0.447	0.439	0.437	0.427	1.75
68.417	26.94	1.631	0.318	2.001	0.869	1.565	0.291	0.886	0.347	0.11	0.0766	0.343	0.207	0.447	0.439	0.436	0.427	1.749
68.5	27.004	1.629	0.317	1.999	0.868	1.565	0.291	0.884	0.346	0.11	0.0764	0.342	0.207	0.446	0.439	0.436	0.427	1.748
68.583	27.068	1.628	0.316	1.998	0.867	1.565	0.29	0.882	0.346	0.11	0.0763	0.341	0.207	0.446	0.439	0.436	0.427	1.748
68.667	27.132	1.627	0.315	1.997	0.866	1.565	0.29	0.881	0.346	0.11	0.0762	0.341	0.207	0.446	0.438	0.435	0.426	1.745
68.75	27.196	1.625	0.314	1.995	0.865	1.565	0.29	0.879	0.345	0.109	0.0761	0.34	0.206	0.445	0.438	0.435	0.426	1.744
68.833	27.259	1.624	0.314	1.994	0.864	1.565	0.29	0.878	0.345	0.109	0.076	0.339	0.206	0.445	0.438	0.435	0.426	1.744
68.917	27.322	1.622	0.313	1.992	0.863	1.565	0.289	0.876	0.344	0.109	0.0759	0.339	0.206	0.445	0.437	0.434	0.425	1.741
69	27.384	1.621	0.312	1.991	0.862	1.564	0.289	0.874	0.344	0.109	0.0759	0.338	0.206	0.444	0.437	0.434	0.425	1.74
69.083	27.446	1.619	0.311	1.989	0.861	1.564	0.289	0.873	0.343	0.109	0.0758	0.338	0.206	0.444	0.437	0.434	0.425	1.74
69.167	27.508	1.618	0.31	1.988	0.86	1.564	0.289	0.871	0.343	0.109	0.0758	0.338	0.206	0.444	0.436	0.433	0.424	1.737
69.25	27.569	1.616	0.31	1.986	0.859	1.563	0.288	0.869	0.342	0.108	0.0757	0.337	0.206	0.443	0.436	0.433	0.424	1.736
69.333	27.63	1.614	0.309	1.984	0.858	1.563	0.288	0.868	0.342	0.108	0.0757	0.337	0.206	0.443	0.435	0.433	0.424	1.735
69.417	27.69	1.613	0.308	1.983	0.857	1.562	0.288	0.866	0.341	0.108	0.0757	0.336	0.206	0.443	0.435	0.432	0.423	1.733
69.5	27.751	1.611	0.308	1.981	0.856	1.562	0.288	0.864	0.341	0.108	0.0756	0.336	0.206	0.442	0.435	0.432	0.423	1.732
69.583	27.81	1.609	0.307	1.979	0.855	1.561	0.287	0.863	0.34	0.108	0.0756	0.336	0.206	0.442	0.434	0.432	0.422	1.73
69.667	27.869	1.608	0.307	1.978	0.854	1.56	0.287	0.861	0.34	0.108	0.0756	0.336	0.206	0.442	0.434	0.431	0.422	1.729
69.75	27.929	1.606	0.306	1.976	0.853	1.56	0.287	0.859	0.339	0.108	0.0756	0.335	0.206	0.441	0.434	0.431	0.422	1.728
69.833	27.987	1.604	0.305	1.974	0.852	1.559	0.286	0.857	0.339	0.108	0.0756	0.335	0.206	0.441	0.433	0.43	0.421	1.725
69.917	28.045	1.602	0.305	1.972	0.851	1.558	0.286	0.856	0.338	0.108	0.0756	0.335	0.206	0.44	0.433	0.43	0.421	1.724
70	28.103	1.6	0.304	1.97	0.85	1.557	0.286	0.854	0.338	0.107	0.0756	0.335	0.206	0.44	0.432	0.43	0.421	1.723
70.083	28.16	1.599	0.304	1.968	0.848	1.556	0.286	0.853	0.337	0.107	0.0756	0.335	0.206	0.44	0.432	0.429	0.42	1.721
70.167	28.217	1.597	0.303	1.967	0.847	1.556	0.285	0.851	0.337	0.107	0.0756	0.335	0.206	0.439	0.432	0.429	0.42	1.72
70.25	28.274	1.595	0.303	1.965	0.846	1.555	0.285	0.849	0.336	0.107	0.0756	0.334	0.206	0.439	0.431	0.428	0.419	1.717
70.333	28.329	1.593	0.303	1.963	0.845	1.554	0.285	0.848	0.336	0.107	0.0756	0.334	0.206	0.438	0.431	0.428	0.419	1.716

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
70.417	28.385	1.591	0.302	1.961	0.844	1.552	0.284	0.846	0.335	0.107	0.0756	0.334	0.206	0.438	0.43	0.428	0.418	1.714
70.5	28.44	1.589	0.302	1.959	0.843	1.551	0.284	0.845	0.334	0.107	0.0756	0.334	0.206	0.437	0.43	0.427	0.418	1.712
70.583	28.494	1.587	0.302	1.957	0.841	1.55	0.284	0.843	0.334	0.107	0.0756	0.334	0.206	0.437	0.429	0.427	0.418	1.711
70.667	28.548	1.585	0.301	1.955	0.84	1.549	0.283	0.842	0.333	0.107	0.0756	0.334	0.206	0.437	0.429	0.426	0.417	1.709
70.75	28.602	1.583	0.301	1.953	0.839	1.548	0.283	0.84	0.333	0.107	0.0756	0.334	0.206	0.436	0.429	0.426	0.417	1.708
70.833	28.655	1.581	0.301	1.95	0.838	1.547	0.283	0.839	0.332	0.107	0.0756	0.334	0.206	0.436	0.428	0.425	0.416	1.705
70.917	28.707	1.579	0.3	1.948	0.836	1.545	0.282	0.838	0.332	0.107	0.0756	0.334	0.206	0.435	0.428	0.425	0.416	1.704
71	28.76	1.577	0.3	1.946	0.835	1.544	0.282	0.836	0.331	0.107	0.0756	0.334	0.206	0.435	0.427	0.424	0.415	1.701
71.083	28.811	1.574	0.3	1.944	0.834	1.543	0.281	0.835	0.331	0.107	0.0756	0.334	0.206	0.434	0.427	0.424	0.415	1.7
71.167	28.863	1.572	0.3	1.942	0.833	1.542	0.281	0.834	0.33	0.107	0.0756	0.334	0.206	0.434	0.426	0.423	0.414	1.697
71.25	28.914	1.57	0.299	1.939	0.831	1.54	0.281	0.833	0.33	0.107	0.0756	0.334	0.206	0.433	0.426	0.423	0.414	1.696
71.333	28.963	1.568	0.299	1.937	0.83	1.539	0.28	0.831	0.329	0.107	0.0756	0.334	0.206	0.433	0.425	0.422	0.413	1.693
71.417	29.013	1.566	0.299	1.935	0.829	1.538	0.28	0.83	0.329	0.107	0.0756	0.334	0.206	0.432	0.425	0.422	0.413	1.692
71.5	29.063	1.564	0.299	1.933	0.828	1.536	0.28	0.829	0.328	0.107	0.0756	0.334	0.206	0.432	0.424	0.421	0.412	1.689
71.583	29.11	1.561	0.299	1.93	0.827	1.535	0.279	0.828	0.328	0.107	0.0756	0.334	0.206	0.431	0.424	0.421	0.412	1.688
71.667	29.158	1.559	0.298	1.928	0.826	1.533	0.279	0.827	0.327	0.107	0.0756	0.334	0.206	0.431	0.423	0.42	0.411	1.685
71.75	29.206	1.557	0.298	1.926	0.824	1.532	0.279	0.826	0.327	0.107	0.0756	0.334	0.206	0.43	0.423	0.42	0.411	1.684
71.833	29.253	1.555	0.298	1.923	0.823	1.53	0.278	0.825	0.326	0.107	0.0756	0.334	0.206	0.43	0.422	0.419	0.41	1.681
71.917	29.299	1.553	0.298	1.921	0.822	1.529	0.278	0.824	0.326	0.107	0.0756	0.334	0.206	0.429	0.422	0.419	0.41	1.68
72	29.345	1.551	0.298	1.919	0.821	1.527	0.278	0.823	0.326	0.107	0.0756	0.334	0.206	0.429	0.421	0.418	0.409	1.677
72.083	29.39	1.549	0.297	1.916	0.82	1.526	0.277	0.822	0.325	0.107	0.0756	0.334	0.206	0.428	0.421	0.418	0.409	1.676
72.167	29.434	1.547	0.297	1.914	0.819	1.524	0.277	0.821	0.325	0.107	0.0756	0.334	0.206	0.428	0.42	0.417	0.408	1.673
72.25	29.479	1.546	0.297	1.912	0.818	1.523	0.277	0.82	0.324	0.107	0.0756	0.334	0.206	0.427	0.42	0.417	0.408	1.672
72.333	29.522	1.544	0.297	1.91	0.817	1.521	0.276	0.819	0.324	0.107	0.0756	0.334	0.206	0.427	0.419	0.416	0.407	1.669
72.417	29.565	1.542	0.297	1.907	0.816	1.519	0.276	0.818	0.324	0.107	0.0756	0.334	0.206	0.426	0.419	0.416	0.407	1.668
72.5	29.608	1.54	0.297	1.905	0.815	1.518	0.276	0.817	0.323	0.107	0.0756	0.334	0.206	0.426	0.418	0.415	0.406	1.665
72.583	29.649	1.538	0.297	1.903	0.814	1.516	0.275	0.816	0.323	0.107	0.0755	0.334	0.206	0.425	0.418	0.415	0.406	1.664
72.667	29.69	1.536	0.296	1.901	0.813	1.514	0.275	0.816	0.322	0.107	0.0755	0.334	0.205	0.425	0.417	0.414	0.405	1.661
72.75	29.731	1.534	0.296	1.898	0.812	1.513	0.275	0.815	0.322	0.107	0.0754	0.334	0.205	0.424	0.417	0.414	0.405	1.66
72.833	29.77	1.533	0.296	1.896	0.811	1.511	0.274	0.814	0.322	0.107	0.0751	0.333	0.204	0.424	0.416	0.413	0.404	1.657
72.917	29.809	1.531	0.296	1.894	0.81	1.509	0.274	0.813	0.321	0.106	0.0748	0.332	0.203	0.423	0.416	0.413	0.404	1.656
73	29.848	1.529	0.295	1.891	0.808	1.507	0.274	0.812	0.321	0.106	0.0745	0.331	0.201	0.423	0.415	0.412	0.403	1.653
73.083	29.885	1.527	0.295	1.889	0.807	1.505	0.273	0.811	0.32	0.106	0.0739	0.33	0.199	0.422	0.415	0.412	0.403	1.652
73.167	29.922	1.524	0.294	1.886	0.806	1.503	0.273	0.81	0.32	0.105	0.0734	0.328	0.197	0.422	0.414	0.411	0.402	1.649
73.25	29.959	1.522	0.294	1.884	0.805	1.501	0.273	0.808	0.319	0.105	0.0728	0.326	0.195	0.421	0.414	0.411	0.402	1.648
73.333	29.995	1.52	0.293	1.881	0.804	1.499	0.272	0.807	0.319	0.105	0.072	0.324	0.192	0.421	0.413	0.41	0.401	1.645
73.417	30.03	1.518	0.292	1.879	0.802	1.497	0.272	0.806	0.318	0.104	0.0712	0.322	0.189	0.42	0.412	0.41	0.4	1.642
73.5	30.065	1.516	0.292	1.876	0.801	1.494	0.271	0.804	0.318	0.103	0.0704	0.319	0.187	0.419	0.412	0.409	0.4	1.64
73.583	30.099	1.513	0.291	1.873	0.8	1.492	0.271	0.803	0.317	0.103	0.0696	0.316	0.184	0.419	0.411	0.409	0.399	1.638
73.667	30.132	1.511	0.29	1.871	0.798	1.49	0.271	0.801	0.317	0.102	0.0688	0.313	0.182	0.418	0.411	0.408	0.399	1.636
73.75	30.165	1.508	0.289	1.868	0.797	1.488	0.27	0.8	0.316	0.101	0.0681	0.31	0.18	0.418	0.41	0.407	0.398	1.633
73.833	30.197	1.506	0.288	1.865	0.796	1.485	0.27	0.798	0.316	0.1	0.0674	0.307	0.178	0.417	0.409	0.407	0.398	1.631
73.917	30.228	1.503	0.287	1.862	0.794	1.483	0.269	0.796	0.315	0.0997	0.0668	0.304	0.177	0.416	0.409	0.406	0.397	1.628
74	30.259	1.501	0.286	1.859	0.793	1.481	0.269	0.794	0.314	0.0988	0.0661	0.301	0.175	0.416	0.408	0.405	0.396	1.625
74.083	30.288	1.498	0.284	1.856	0.791	1.478	0.268	0.793	0.314	0.0981	0.0656	0.299	0.174	0.415	0.408	0.405	0.396	1.624
74.167	30.317	1.495	0.283	1.853	0.79	1.476	0.268	0.791	0.313	0.0973	0.0652	0.296	0.173	0.414	0.407	0.404	0.395	1.62
74.25	30.346	1.493	0.282	1.85	0.788	1.473	0.267	0.789	0.312	0.0966	0.0647	0.294	0.172	0.414	0.406	0.403	0.394	1.617
74.333	30.373	1.49	0.28	1.847	0.787	1.471	0.267	0.787	0.312	0.0959	0.0643	0.292	0.171	0.413	0.406	0.403	0.394	1.616
74.417	30.399	1.487	0.278	1.844	0.785	1.468	0.266	0.784	0.311	0.0953	0.064	0.289	0.17	0.412	0.405	0.402	0.393	1.612
74.5	30.426	1.484	0.277	1.841	0.783	1.466	0.266	0.782	0.31	0.0946	0.0636	0.287	0.169	0.412	0.404	0.401	0.392	1.609
74.583	30.451	1.481	0.275	1.837	0.782	1.463	0.265	0.78	0.31	0.0941	0.0633	0.286	0.169	0.411	0.403	0.401	0.391	1.606
74.667	30.475	1.478	0.274	1.834	0.78	1.461	0.265	0.778	0.309	0.0935	0.063	0.284	0.168	0.41	0.403	0.4	0.391	1.604
74.75	30.5	1.475	0.272	1.83	0.778	1.458	0.264	0.775	0.308	0.093	0.0627	0.282	0.168	0.409	0.402	0.399	0.39	1.6
74.833	30.523	1.472	0.27	1.827	0.777	1.455	0.264	0.773	0.308	0.0925	0.0625	0.281	0.168	0.409	0.401	0.398	0.389	1.597
74.917	30.545	1.469	0.269	1.823	0.775	1.453	0.263	0.77	0.307	0.0921	0.0623	0.28	0.167	0.408	0.4	0.398	0.388	1.594
75	30.568	1.466	0.267	1.82	0.773	1.45	0.263	0.768	0.306	0.0916	0.0621	0.278	0.167	0.407	0.4	0.397	0.388	1.592
75.083	30.588	1.462	0.266	1.816	0.771	1.447	0.262	0.765	0.305	0.0913	0.062	0.277	0.167	0.406	0.399	0.396	0.387	1.588
75.167	30.608	1.459	0.264	1.812	0.769	1.445	0.262	0.762	0.304	0.0909	0.0618	0.276	0.167	0.406	0.398	0.395	0.386	1.585
75.25	30.628	1.456	0.263	1.809	0.767	1.442	0.261	0.76	0.304	0.0906	0.0617	0.275	0.167	0.405	0.397	0.394	0.385	1.581
75.333	30.645	1.452	0.261	1.805	0.765	1.439	0.26	0.757	0.303	0.0902	0.0616	0.274	0.167	0.404	0.396	0.394	0.384	1.578
75.417	30.663	1.449	0.26	1.801	0.763	1.436	0.26	0.754	0.302	0.0899	0.0615	0.273	0.167	0.403	0.395	0.393	0.383	1.574
75.5	30.68	1.445	0.258	1.797	0.762	1.433	0.259	0.751	0.301	0.0896	0.0615	0.272	0.167	0.402	0.395	0.392	0.383	1.572
75.583	30.695	1.442	0.257	1.793	0.759	1.431	0.259	0.747	0.3	0.0894	0.0614	0.272	0.167	0.401	0.394	0.391	0.382	1.568
75.667	30.711	1.438	0.256	1.789	0.757	1.428	0.258	0.744	0.299	0.0891	0.0614	0.271	0.167	0.4	0.393	0.39	0.381	1.564
75.75	30.726	1.435	0.255	1.785	0.755	1.425	0.257	0.741	0.298	0.0888	0.0613	0.27	0.167	0.4	0.392	0.389	0.38	1.561
75.833	30.738	1.431	0.253	1.781	0.753	1.422	0.257	0.738	0.297	0.0885	0.0612	0.269	0.166	0.399	0.391	0.388	0.379	1.557
75.917	30.751	1.427	0.252	1.776	0.751	1.419	0.256	0.735	0.296	0.0882	0.0611	0.268	0.166	0.398	0.39	0.387	0.378	1.553

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
76	30.764	1.424	0.251	1.772	0.749	1.416	0.255	0.731	0.295	0.0879	0.061	0.268	0.165	0.397	0.389	0.386	0.377	1.549
76.083	30.774	1.42	0.25	1.768	0.746	1.413	0.255	0.728	0.294	0.0876	0.0608	0.267	0.164	0.396	0.388	0.385	0.376	1.545
76.167	30.785	1.416	0.249	1.763	0.744	1.41	0.254	0.725	0.293	0.0873	0.0606	0.266	0.163	0.395	0.387	0.384	0.375	1.541
76.25	30.795	1.412	0.247	1.759	0.742	1.407	0.253	0.722	0.292	0.087	0.0604	0.265	0.163	0.394	0.386	0.383	0.374	1.537
76.333	30.802	1.407	0.246	1.754	0.739	1.404	0.253	0.719	0.291	0.0867	0.0601	0.264	0.162	0.393	0.385	0.382	0.373	1.533
76.417	30.81	1.403	0.245	1.749	0.737	1.401	0.252	0.715	0.29	0.0863	0.0597	0.263	0.16	0.392	0.384	0.381	0.372	1.529
76.5	30.818	1.399	0.244	1.745	0.734	1.397	0.251	0.712	0.289	0.086	0.0594	0.262	0.159	0.391	0.383	0.38	0.371	1.525
76.583	30.822	1.394	0.243	1.74	0.732	1.394	0.251	0.709	0.288	0.0856	0.0591	0.261	0.158	0.39	0.382	0.379	0.37	1.521
76.667	30.827	1.39	0.242	1.735	0.729	1.391	0.25	0.706	0.286	0.0853	0.0588	0.259	0.158	0.389	0.381	0.378	0.369	1.517
76.75	30.832	1.385	0.241	1.73	0.726	1.388	0.249	0.703	0.285	0.0849	0.0585	0.258	0.157	0.387	0.38	0.377	0.368	1.512
76.833	30.834	1.381	0.24	1.725	0.724	1.384	0.248	0.7	0.284	0.0846	0.0582	0.257	0.156	0.386	0.379	0.376	0.367	1.508
76.917	30.836	1.376	0.239	1.719	0.721	1.381	0.247	0.697	0.283	0.0842	0.058	0.256	0.155	0.385	0.378	0.375	0.366	1.504
77	30.838	1.371	0.237	1.714	0.718	1.378	0.247	0.694	0.282	0.0839	0.0577	0.255	0.155	0.384	0.377	0.374	0.364	1.499
77.083	30.838	1.366	0.236	1.709	0.715	1.374	0.246	0.691	0.281	0.0835	0.0575	0.254	0.154	0.383	0.375	0.373	0.363	1.494
77.167	30.838	1.361	0.235	1.703	0.712	1.371	0.245	0.688	0.28	0.0832	0.0573	0.252	0.154	0.382	0.374	0.371	0.362	1.489
77.25	30.837	1.356	0.234	1.698	0.71	1.368	0.244	0.685	0.279	0.0829	0.0571	0.251	0.153	0.381	0.373	0.37	0.361	1.485
77.333	30.834	1.351	0.233	1.692	0.707	1.364	0.243	0.683	0.278	0.0826	0.0569	0.251	0.153	0.379	0.372	0.369	0.36	1.48
77.417	30.831	1.346	0.232	1.687	0.704	1.361	0.242	0.68	0.276	0.0824	0.0568	0.25	0.153	0.378	0.37	0.368	0.358	1.474
77.5	30.828	1.341	0.231	1.681	0.701	1.357	0.241	0.677	0.275	0.0821	0.0566	0.249	0.152	0.377	0.369	0.366	0.357	1.469
77.583	30.822	1.336	0.229	1.675	0.699	1.353	0.241	0.674	0.274	0.0819	0.0565	0.248	0.152	0.376	0.368	0.365	0.356	1.465
77.667	30.816	1.331	0.228	1.669	0.696	1.35	0.24	0.671	0.273	0.0817	0.0564	0.247	0.152	0.374	0.367	0.364	0.355	1.46
77.75	30.81	1.326	0.227	1.663	0.693	1.346	0.239	0.669	0.272	0.0814	0.0563	0.247	0.152	0.373	0.365	0.363	0.353	1.454
77.833	30.801	1.321	0.226	1.657	0.691	1.343	0.238	0.666	0.271	0.0813	0.0562	0.246	0.151	0.372	0.364	0.361	0.352	1.449
77.917	30.792	1.316	0.225	1.651	0.688	1.339	0.237	0.663	0.27	0.0811	0.0561	0.246	0.151	0.37	0.363	0.36	0.351	1.444
78	30.783	1.312	0.224	1.646	0.685	1.335	0.236	0.66	0.269	0.0809	0.056	0.245	0.151	0.369	0.362	0.359	0.349	1.439
78.083	30.772	1.307	0.223	1.64	0.683	1.332	0.235	0.658	0.268	0.0807	0.056	0.245	0.151	0.368	0.36	0.357	0.348	1.433
78.167	30.76	1.302	0.222	1.634	0.68	1.328	0.235	0.655	0.267	0.0806	0.0559	0.244	0.151	0.367	0.359	0.356	0.347	1.429
78.25	30.749	1.297	0.221	1.628	0.677	1.324	0.234	0.652	0.266	0.0805	0.0559	0.244	0.151	0.365	0.358	0.355	0.346	1.424
78.333	30.735	1.292	0.22	1.622	0.675	1.32	0.233	0.65	0.265	0.0803	0.0558	0.243	0.151	0.364	0.356	0.354	0.344	1.418
78.417	30.72	1.288	0.219	1.616	0.672	1.316	0.232	0.647	0.264	0.0802	0.0558	0.243	0.151	0.363	0.355	0.352	0.343	1.413
78.5	30.706	1.283	0.218	1.611	0.67	1.312	0.231	0.644	0.263	0.0801	0.0558	0.243	0.151	0.362	0.354	0.351	0.342	1.409
78.583	30.689	1.278	0.217	1.605	0.667	1.308	0.23	0.642	0.262	0.08	0.0557	0.242	0.151	0.36	0.353	0.35	0.341	1.404
78.667	30.673	1.273	0.216	1.599	0.665	1.305	0.23	0.639	0.261	0.0799	0.0557	0.242	0.151	0.359	0.351	0.349	0.339	1.398
78.75	30.656	1.269	0.216	1.594	0.662	1.301	0.229	0.637	0.26	0.0797	0.0557	0.242	0.151	0.358	0.35	0.347	0.338	1.393
78.833	30.636	1.264	0.215	1.588	0.66	1.297	0.228	0.634	0.259	0.0796	0.0557	0.241	0.151	0.357	0.349	0.346	0.337	1.389
78.917	30.617	1.26	0.214	1.582	0.657	1.292	0.227	0.632	0.258	0.0795	0.0556	0.241	0.151	0.355	0.348	0.345	0.336	1.384
79	30.597	1.255	0.213	1.577	0.655	1.288	0.226	0.629	0.257	0.0794	0.0556	0.241	0.15	0.354	0.346	0.344	0.334	1.378
79.083	30.575	1.25	0.213	1.571	0.652	1.284	0.226	0.627	0.256	0.0792	0.0555	0.24	0.15	0.353	0.345	0.342	0.333	1.373
79.167	30.553	1.246	0.212	1.565	0.65	1.28	0.225	0.624	0.255	0.0791	0.0553	0.24	0.15	0.352	0.344	0.341	0.332	1.369
79.25	30.53	1.241	0.212	1.56	0.647	1.276	0.224	0.622	0.254	0.079	0.0552	0.239	0.149	0.35	0.343	0.34	0.331	1.364
79.333	30.506	1.237	0.211	1.554	0.645	1.272	0.223	0.62	0.253	0.0788	0.0551	0.239	0.149	0.349	0.342	0.339	0.329	1.359
79.417	30.481	1.232	0.21	1.549	0.643	1.267	0.222	0.617	0.252	0.0787	0.0549	0.238	0.148	0.348	0.34	0.338	0.328	1.354
79.5	30.456	1.228	0.21	1.543	0.64	1.263	0.222	0.615	0.251	0.0785	0.0548	0.238	0.148	0.347	0.339	0.336	0.327	1.349
79.583	30.428	1.223	0.209	1.538	0.638	1.259	0.221	0.612	0.25	0.0783	0.0546	0.237	0.147	0.346	0.338	0.335	0.326	1.345
79.667	30.401	1.219	0.209	1.532	0.635	1.254	0.22	0.61	0.249	0.0782	0.0545	0.237	0.147	0.344	0.337	0.334	0.325	1.34
79.75	30.374	1.214	0.208	1.526	0.633	1.25	0.219	0.608	0.248	0.078	0.0543	0.236	0.146	0.343	0.336	0.333	0.323	1.335
79.833	30.344	1.21	0.208	1.521	0.63	1.246	0.219	0.606	0.248	0.0778	0.0542	0.236	0.146	0.342	0.334	0.332	0.322	1.33
79.917	30.314	1.205	0.207	1.516	0.628	1.241	0.218	0.603	0.247	0.0776	0.054	0.235	0.146	0.341	0.333	0.33	0.321	1.325
80	30.284	1.201	0.207	1.51	0.626	1.237	0.217	0.601	0.246	0.0775	0.0539	0.234	0.145	0.34	0.332	0.329	0.32	1.321
80.083	30.252	1.196	0.206	1.505	0.623	1.233	0.216	0.599	0.245	0.0773	0.0538	0.234	0.145	0.338	0.331	0.328	0.319	1.316
80.167	30.22	1.192	0.206	1.499	0.621	1.229	0.215	0.597	0.244	0.0771	0.0537	0.233	0.145	0.337	0.33	0.327	0.317	1.311
80.25	30.188	1.188	0.205	1.494	0.618	1.224	0.215	0.595	0.243	0.077	0.0536	0.233	0.144	0.336	0.328	0.326	0.316	1.306
80.333	30.153	1.183	0.205	1.488	0.616	1.22	0.214	0.593	0.242	0.0769	0.0535	0.232	0.144	0.335	0.327	0.324	0.315	1.301
80.417	30.118	1.179	0.204	1.483	0.614	1.216	0.213	0.591	0.242	0.0767	0.0534	0.232	0.144	0.334	0.326	0.323	0.314	1.297
80.5	30.084	1.175	0.204	1.477	0.612	1.212	0.212	0.589	0.241	0.0766	0.0534	0.231	0.144	0.333	0.325	0.322	0.313	1.293
80.583	30.047	1.17	0.203	1.472	0.609	1.208	0.212	0.587	0.24	0.0765	0.0533	0.231	0.144	0.331	0.324	0.321	0.312	1.288
80.667	30.01	1.166	0.202	1.467	0.607	1.204	0.211	0.585	0.239	0.0764	0.0532	0.231	0.144	0.33	0.323	0.32	0.31	1.283
80.75	29.973	1.162	0.202	1.461	0.605	1.199	0.21	0.583	0.238	0.0762	0.0532	0.23	0.144	0.329	0.321	0.319	0.309	1.278
80.833	29.934	1.158	0.201	1.456	0.603	1.195	0.209	0.581	0.238	0.0761	0.0531	0.23	0.144	0.328	0.32	0.318	0.308	1.274
80.917	29.895	1.154	0.201	1.451	0.601	1.191	0.209	0.579	0.237	0.0761	0.0531	0.23	0.143	0.327	0.319	0.316	0.307	1.269
81	29.855	1.15	0.2	1.446	0.599	1.187	0.208	0.577	0.236	0.076	0.0531	0.23	0.143	0.326	0.318	0.315	0.306	1.265
81.083	29.814	1.146	0.2	1.441	0.597	1.183	0.207	0.575	0.235	0.0759	0.053	0.229	0.143	0.325	0.317	0.314	0.305	1.261
81.167	29.773	1.142	0.199	1.436	0.595	1.179	0.207	0.573	0.235	0.0758	0.053	0.229	0.143	0.324	0.316	0.313	0.304	1.257
81.25	29.732	1.138	0.199	1.43	0.593	1.175	0.206	0.571	0.234	0.0757	0.053	0.229	0.143	0.322	0.315	0.312	0.303	1.252
81.333	29.689	1.134	0.199	1.426	0.591	1.171	0.205	0.569	0.233	0.0757	0.0529	0.229	0.143	0.321	0.314	0.311	0.301	1.247
81.417	29.646	1.131	0.198	1.421	0.589	1.167	0.205	0.568	0.232	0.0756	0.0529	0.228	0.143	0.32	0.313	0.31	0.3	1.243
81.5	29.603	1.127	0.198	1.416	0.587	1.163	0.204	0.566	0.232	0.0755	0.0529	0.228	0.143	0.319	0.312	0.309	0.299	1.239

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
81.583	29.558	1.123	0.197	1.411	0.585	1.159	0.203	0.564	0.231	0.0755	0.0529	0.228	0.143	0.318	0.311	0.308	0.298	1.235
81.667	29.513	1.12	0.197	1.406	0.583	1.155	0.203	0.562	0.23	0.0754	0.0529	0.228	0.143	0.317	0.31	0.307	0.297	1.231
81.75	29.468	1.116	0.197	1.402	0.581	1.152	0.202	0.561	0.23	0.0754	0.0528	0.228	0.143	0.316	0.309	0.306	0.296	1.227
81.833	29.421	1.112	0.196	1.397	0.58	1.148	0.201	0.559	0.229	0.0752	0.0528	0.227	0.143	0.315	0.308	0.305	0.295	1.223
81.917	29.374	1.109	0.196	1.392	0.578	1.144	0.201	0.557	0.228	0.0751	0.0527	0.227	0.142	0.314	0.307	0.304	0.294	1.219
82	29.327	1.105	0.195	1.388	0.576	1.14	0.2	0.555	0.227	0.075	0.0526	0.227	0.142	0.313	0.305	0.303	0.293	1.214
82.083	29.279	1.102	0.195	1.383	0.574	1.136	0.2	0.554	0.227	0.0749	0.0524	0.226	0.141	0.312	0.305	0.302	0.292	1.211
82.167	29.23	1.098	0.195	1.379	0.572	1.132	0.199	0.552	0.226	0.0747	0.0522	0.225	0.14	0.311	0.304	0.301	0.291	1.207
82.25	29.182	1.095	0.194	1.374	0.57	1.128	0.198	0.55	0.225	0.0745	0.052	0.225	0.14	0.31	0.303	0.3	0.29	1.203
82.333	29.132	1.091	0.194	1.37	0.568	1.124	0.198	0.549	0.224	0.0743	0.0517	0.224	0.139	0.309	0.302	0.299	0.289	1.199
82.417	29.082	1.088	0.193	1.365	0.566	1.12	0.197	0.547	0.224	0.0741	0.0514	0.223	0.138	0.308	0.301	0.298	0.288	1.195
82.5	29.032	1.084	0.193	1.361	0.565	1.116	0.196	0.545	0.223	0.0739	0.0511	0.222	0.136	0.307	0.3	0.297	0.287	1.191
82.583	28.98	1.081	0.192	1.356	0.563	1.112	0.196	0.544	0.222	0.0736	0.0508	0.221	0.136	0.306	0.299	0.296	0.286	1.187
82.667	28.929	1.077	0.192	1.352	0.561	1.108	0.195	0.542	0.221	0.0733	0.0505	0.22	0.135	0.305	0.298	0.295	0.285	1.183
82.75	28.877	1.074	0.191	1.347	0.559	1.104	0.195	0.54	0.221	0.073	0.0501	0.219	0.134	0.304	0.297	0.294	0.284	1.179
82.833	28.824	1.07	0.191	1.343	0.557	1.1	0.194	0.539	0.22	0.0727	0.0499	0.218	0.133	0.303	0.296	0.293	0.283	1.175
82.917	28.771	1.067	0.19	1.339	0.555	1.096	0.193	0.537	0.219	0.0723	0.0496	0.216	0.132	0.302	0.295	0.292	0.283	1.172
83	28.718	1.063	0.19	1.334	0.553	1.092	0.193	0.536	0.219	0.072	0.0493	0.215	0.131	0.302	0.294	0.291	0.282	1.169
83.083	28.663	1.06	0.189	1.33	0.551	1.089	0.192	0.534	0.218	0.0717	0.0491	0.214	0.131	0.301	0.293	0.29	0.281	1.165
83.167	28.609	1.056	0.188	1.326	0.55	1.085	0.192	0.532	0.217	0.0714	0.0489	0.213	0.13	0.3	0.292	0.289	0.28	1.161
83.25	28.554	1.053	0.188	1.321	0.548	1.081	0.191	0.531	0.216	0.0711	0.0487	0.212	0.13	0.299	0.291	0.288	0.279	1.157
83.333	28.499	1.049	0.187	1.317	0.546	1.077	0.19	0.529	0.216	0.0708	0.0485	0.211	0.13	0.298	0.29	0.287	0.278	1.153
83.417	28.443	1.046	0.186	1.313	0.544	1.073	0.19	0.528	0.215	0.0705	0.0484	0.21	0.129	0.297	0.289	0.286	0.277	1.149
83.5	28.388	1.042	0.186	1.308	0.542	1.07	0.189	0.526	0.214	0.0702	0.0482	0.209	0.129	0.296	0.288	0.285	0.276	1.145
83.583	28.331	1.039	0.185	1.304	0.54	1.066	0.188	0.525	0.214	0.07	0.0481	0.208	0.129	0.295	0.287	0.284	0.275	1.141
83.667	28.274	1.035	0.184	1.299	0.538	1.062	0.188	0.523	0.213	0.0698	0.048	0.208	0.128	0.294	0.286	0.283	0.274	1.137
83.75	28.217	1.032	0.183	1.295	0.537	1.058	0.187	0.521	0.212	0.0695	0.0478	0.207	0.128	0.293	0.285	0.283	0.273	1.134
83.833	28.16	1.028	0.182	1.291	0.535	1.055	0.187	0.52	0.212	0.0694	0.0477	0.206	0.128	0.292	0.284	0.282	0.272	1.13
83.917	28.102	1.025	0.182	1.286	0.533	1.051	0.186	0.518	0.211	0.0692	0.0476	0.206	0.128	0.291	0.283	0.281	0.271	1.126
84	28.044	1.022	0.181	1.282	0.531	1.047	0.185	0.517	0.21	0.069	0.0476	0.205	0.128	0.29	0.283	0.28	0.27	1.123
84.083	27.985	1.018	0.18	1.278	0.529	1.044	0.185	0.515	0.21	0.0688	0.0475	0.205	0.128	0.289	0.282	0.279	0.269	1.119
84.167	27.926	1.015	0.18	1.274	0.528	1.04	0.184	0.514	0.209	0.0687	0.0474	0.204	0.128	0.288	0.281	0.278	0.268	1.115
84.25	27.868	1.011	0.179	1.269	0.526	1.037	0.184	0.512	0.208	0.0685	0.0474	0.204	0.128	0.287	0.28	0.277	0.267	1.111
84.333	27.808	1.008	0.178	1.265	0.524	1.033	0.183	0.51	0.208	0.0684	0.0473	0.203	0.128	0.287	0.279	0.276	0.267	1.109
84.417	27.748	1.005	0.178	1.261	0.522	1.03	0.182	0.509	0.207	0.0683	0.0473	0.203	0.128	0.286	0.278	0.275	0.266	1.105
84.5	27.688	1.001	0.177	1.257	0.52	1.026	0.182	0.507	0.206	0.0681	0.0472	0.203	0.128	0.285	0.277	0.274	0.265	1.101
84.583	27.628	0.998	0.176	1.253	0.519	1.022	0.181	0.505	0.206	0.068	0.0472	0.202	0.128	0.284	0.276	0.273	0.264	1.097
84.667	27.567	0.995	0.176	1.248	0.517	1.019	0.181	0.504	0.205	0.0679	0.0472	0.202	0.128	0.283	0.275	0.272	0.263	1.093
84.75	27.507	0.992	0.175	1.244	0.515	1.015	0.18	0.502	0.204	0.0678	0.0472	0.202	0.127	0.282	0.274	0.271	0.262	1.089
84.833	27.445	0.988	0.175	1.24	0.513	1.012	0.18	0.5	0.203	0.0676	0.047	0.201	0.127	0.281	0.273	0.271	0.261	1.086
84.917	27.384	0.985	0.174	1.236	0.512	1.008	0.179	0.499	0.203	0.0674	0.0469	0.201	0.127	0.28	0.273	0.27	0.26	1.083
85	27.323	0.982	0.173	1.232	0.51	1.005	0.178	0.497	0.202	0.0673	0.0468	0.2	0.126	0.279	0.272	0.269	0.259	1.079
85.083	27.261	0.978	0.173	1.228	0.508	1.001	0.178	0.495	0.201	0.067	0.0465	0.199	0.125	0.278	0.271	0.268	0.258	1.075
85.167	27.199	0.975	0.172	1.223	0.506	0.998	0.177	0.493	0.201	0.0667	0.0463	0.198	0.124	0.277	0.27	0.267	0.257	1.071
85.25	27.137	0.971	0.171	1.219	0.504	0.994	0.177	0.491	0.2	0.0665	0.046	0.197	0.123	0.277	0.269	0.266	0.256	1.068
85.333	27.074	0.968	0.171	1.215	0.502	0.99	0.176	0.489	0.199	0.0661	0.0456	0.196	0.121	0.276	0.268	0.265	0.256	1.065
85.417	27.011	0.964	0.17	1.21	0.5	0.987	0.175	0.488	0.198	0.0658	0.0451	0.195	0.119	0.275	0.267	0.264	0.255	1.061
85.5	26.949	0.961	0.169	1.206	0.498	0.983	0.175	0.486	0.198	0.0655	0.0447	0.193	0.118	0.274	0.266	0.263	0.254	1.057
85.583	26.885	0.957	0.168	1.202	0.496	0.98	0.174	0.484	0.197	0.065	0.0442	0.192	0.116	0.273	0.265	0.262	0.253	1.053
85.667	26.822	0.953	0.168	1.197	0.494	0.976	0.174	0.482	0.196	0.0646	0.0437	0.19	0.115	0.272	0.264	0.261	0.252	1.049
85.75	26.759	0.95	0.167	1.193	0.492	0.972	0.173	0.48	0.195	0.0642	0.0432	0.188	0.113	0.271	0.263	0.26	0.251	1.045
85.833	26.695	0.946	0.166	1.188	0.49	0.969	0.172	0.478	0.195	0.0637	0.0428	0.186	0.112	0.27	0.262	0.259	0.25	1.041
85.917	26.631	0.942	0.165	1.184	0.488	0.965	0.172	0.476	0.194	0.0632	0.0424	0.185	0.111	0.269	0.261	0.258	0.249	1.037
86	26.567	0.939	0.164	1.179	0.486	0.961	0.171	0.474	0.193	0.0627	0.0419	0.183	0.11	0.268	0.26	0.257	0.248	1.033
86.083	26.503	0.935	0.163	1.175	0.484	0.958	0.17	0.472	0.192	0.0622	0.0416	0.181	0.109	0.267	0.259	0.256	0.247	1.029
86.167	26.439	0.931	0.162	1.17	0.482	0.954	0.17	0.47	0.192	0.0617	0.0413	0.179	0.109	0.266	0.258	0.255	0.246	1.025
86.25	26.374	0.927	0.161	1.166	0.48	0.95	0.169	0.468	0.191	0.0612	0.0409	0.178	0.108	0.265	0.257	0.254	0.245	1.021
86.333	26.31	0.923	0.16	1.161	0.478	0.947	0.168	0.466	0.19	0.0608	0.0407	0.176	0.107	0.264	0.256	0.253	0.244	1.017
86.417	26.245	0.919	0.159	1.156	0.476	0.943	0.168	0.464	0.189	0.0604	0.0405	0.175	0.107	0.263	0.255	0.252	0.243	1.013
86.5	26.18	0.915	0.158	1.152	0.474	0.94	0.167	0.462	0.189	0.06	0.0402	0.174	0.106	0.262	0.254	0.251	0.242	1.009
86.583	26.115	0.911	0.157	1.147	0.472	0.936	0.166	0.46	0.188	0.0596	0.04	0.173	0.106	0.261	0.253	0.25	0.241	1.005
86.667	26.05	0.907	0.155	1.142	0.47	0.932	0.165	0.457	0.187	0.0593	0.0399	0.171	0.105	0.26	0.252	0.249	0.24	1.001
86.75	25.985	0.903	0.154	1.137	0.468	0.929	0.165	0.455	0.186	0.0589	0.0397	0.17	0.105	0.259	0.251	0.248	0.239	0.997
86.833	25.919	0.9	0.153	1.132	0.466	0.925	0.164	0.453	0.185	0.0586	0.0395	0.169	0.105	0.258	0.25	0.247	0.237	0.992
86.917	25.854	0.896	0.152	1.127	0.464	0.921	0.163	0.451	0.185	0.0583	0.0394	0.169	0.105	0.257	0.249	0.246	0.236	0.988
87	25.788	0.892	0.151	1.123	0.461	0.918	0.163	0.449	0.184	0.058	0.0392	0.168	0.104	0.256	0.248	0.245	0.235	0.984
87.083	25.722	0.888	0.149	1.118	0.459	0.914	0.162	0.446	0.183	0.0578	0.0391	0.167	0.104	0.254	0.247	0.244	0.234	0.979

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
87.167	25.657	0.884	0.148	1.113	0.457	0.911	0.161	0.444	0.182	0.0576	0.039	0.166	0.104	0.253	0.246	0.243	0.233	0.975
87.25	25.591	0.88	0.147	1.108	0.455	0.907	0.161	0.442	0.182	0.0573	0.0389	0.166	0.104	0.252	0.245	0.242	0.232	0.971
87.333	25.525	0.876	0.146	1.103	0.453	0.903	0.16	0.44	0.181	0.0571	0.0389	0.165	0.104	0.251	0.244	0.241	0.231	0.967
87.417	25.459	0.872	0.145	1.098	0.451	0.9	0.159	0.437	0.18	0.0569	0.0388	0.164	0.104	0.25	0.243	0.24	0.23	0.963
87.5	25.393	0.869	0.144	1.094	0.449	0.896	0.159	0.435	0.179	0.0567	0.0387	0.164	0.104	0.249	0.241	0.239	0.229	0.958
87.583	25.326	0.865	0.143	1.089	0.447	0.893	0.158	0.433	0.178	0.0566	0.0387	0.163	0.104	0.248	0.24	0.238	0.228	0.954
87.667	25.26	0.861	0.142	1.084	0.445	0.889	0.157	0.43	0.178	0.0564	0.0387	0.163	0.104	0.247	0.239	0.237	0.227	0.95
87.75	25.194	0.857	0.142	1.079	0.443	0.885	0.157	0.428	0.177	0.0562	0.0387	0.162	0.104	0.246	0.238	0.235	0.226	0.945
87.833	25.127	0.853	0.141	1.074	0.441	0.882	0.156	0.425	0.176	0.0561	0.0386	0.162	0.104	0.245	0.237	0.234	0.225	0.941
87.917	25.06	0.849	0.14	1.07	0.439	0.878	0.155	0.423	0.175	0.0559	0.0386	0.162	0.104	0.244	0.236	0.233	0.224	0.937
88	24.994	0.846	0.139	1.065	0.437	0.875	0.155	0.42	0.174	0.0558	0.0386	0.161	0.104	0.243	0.235	0.232	0.223	0.933
88.083	24.927	0.842	0.138	1.06	0.435	0.871	0.154	0.418	0.174	0.0556	0.0385	0.161	0.103	0.242	0.234	0.231	0.222	0.929
88.167	24.86	0.838	0.138	1.055	0.433	0.867	0.153	0.416	0.173	0.0554	0.0384	0.16	0.103	0.241	0.233	0.23	0.221	0.925
88.25	24.793	0.834	0.137	1.05	0.431	0.864	0.153	0.413	0.172	0.0553	0.0383	0.16	0.103	0.24	0.232	0.229	0.22	0.921
88.333	24.726	0.83	0.136	1.045	0.429	0.86	0.152	0.411	0.171	0.0551	0.0382	0.159	0.102	0.239	0.231	0.228	0.219	0.917
88.417	24.659	0.826	0.135	1.041	0.427	0.856	0.151	0.409	0.17	0.0549	0.038	0.159	0.102	0.238	0.23	0.227	0.217	0.912
88.5	24.592	0.822	0.135	1.036	0.425	0.853	0.151	0.406	0.169	0.0547	0.0379	0.158	0.101	0.237	0.229	0.226	0.216	0.908
88.583	24.525	0.819	0.134	1.031	0.423	0.849	0.15	0.404	0.168	0.0545	0.0377	0.158	0.1	0.236	0.228	0.225	0.215	0.904
88.667	24.457	0.815	0.133	1.026	0.421	0.845	0.149	0.402	0.167	0.0543	0.0376	0.157	0.1	0.235	0.227	0.224	0.214	0.9
88.75	24.39	0.811	0.133	1.021	0.419	0.842	0.148	0.399	0.167	0.0542	0.0374	0.156	0.0995	0.233	0.226	0.223	0.213	0.895
88.833	24.323	0.807	0.132	1.016	0.416	0.838	0.148	0.397	0.166	0.054	0.0372	0.156	0.0991	0.232	0.225	0.222	0.212	0.891
88.917	24.255	0.803	0.131	1.011	0.414	0.835	0.147	0.395	0.165	0.0538	0.0371	0.155	0.0987	0.231	0.224	0.221	0.211	0.887
89	24.188	0.799	0.131	1.007	0.412	0.831	0.146	0.393	0.164	0.0536	0.037	0.155	0.0983	0.23	0.223	0.22	0.21	0.883
89.083	24.12	0.795	0.13	1.002	0.41	0.827	0.146	0.391	0.163	0.0534	0.0368	0.154	0.0981	0.229	0.221	0.219	0.209	0.878
89.167	24.053	0.791	0.13	0.997	0.408	0.824	0.145	0.389	0.162	0.0533	0.0367	0.153	0.0978	0.228	0.22	0.218	0.208	0.874
89.25	23.985	0.787	0.129	0.992	0.405	0.82	0.144	0.387	0.162	0.0531	0.0366	0.153	0.0976	0.227	0.219	0.216	0.207	0.869
89.333	23.918	0.783	0.128	0.987	0.403	0.817	0.144	0.385	0.161	0.0529	0.0365	0.152	0.0974	0.226	0.218	0.215	0.206	0.865
89.417	23.85	0.779	0.128	0.982	0.401	0.813	0.143	0.383	0.16	0.0528	0.0365	0.152	0.0972	0.225	0.217	0.214	0.205	0.861
89.5	23.782	0.775	0.127	0.977	0.399	0.81	0.142	0.381	0.159	0.0527	0.0364	0.151	0.097	0.224	0.216	0.213	0.204	0.857
89.583	23.714	0.771	0.126	0.972	0.397	0.806	0.142	0.379	0.158	0.0525	0.0363	0.151	0.0968	0.223	0.215	0.212	0.203	0.853
89.667	23.647	0.767	0.126	0.967	0.395	0.803	0.141	0.377	0.158	0.0524	0.0362	0.151	0.0967	0.222	0.214	0.211	0.201	0.848
89.75	23.579	0.763	0.125	0.962	0.393	0.799	0.14	0.375	0.157	0.0523	0.0362	0.15	0.0966	0.221	0.213	0.21	0.2	0.844
89.833	23.511	0.76	0.124	0.957	0.391	0.796	0.14	0.373	0.156	0.0522	0.0361	0.15	0.0965	0.22	0.212	0.209	0.199	0.84
89.917	23.443	0.756	0.124	0.952	0.389	0.793	0.139	0.371	0.155	0.0521	0.0361	0.15	0.0964	0.219	0.211	0.208	0.198	0.836
90	23.375	0.752	0.123	0.947	0.387	0.789	0.138	0.369	0.155	0.052	0.036	0.149	0.0963	0.217	0.21	0.207	0.197	0.831
90.083	23.307	0.749	0.123	0.943	0.385	0.786	0.138	0.367	0.154	0.0519	0.036	0.149	0.0963	0.216	0.209	0.206	0.196	0.827
90.167	23.239	0.745	0.122	0.938	0.383	0.782	0.137	0.366	0.153	0.0518	0.036	0.149	0.0963	0.215	0.208	0.205	0.195	0.823
90.25	23.172	0.741	0.121	0.933	0.381	0.779	0.136	0.364	0.152	0.0518	0.0359	0.149	0.0963	0.214	0.207	0.204	0.194	0.819
90.333	23.104	0.738	0.121	0.928	0.379	0.776	0.136	0.362	0.152	0.0517	0.0359	0.149	0.0963	0.213	0.206	0.203	0.193	0.815
90.417	23.036	0.734	0.12	0.924	0.377	0.772	0.135	0.36	0.151	0.0516	0.0359	0.148	0.0963	0.212	0.205	0.202	0.192	0.811
90.5	22.968	0.731	0.12	0.919	0.376	0.769	0.134	0.359	0.15	0.0516	0.0359	0.148	0.0963	0.211	0.204	0.201	0.191	0.807
90.583	22.9	0.727	0.119	0.915	0.374	0.766	0.134	0.357	0.15	0.0515	0.0359	0.148	0.0963	0.21	0.203	0.2	0.19	0.803
90.667	22.832	0.724	0.119	0.91	0.372	0.762	0.133	0.355	0.149	0.0515	0.0358	0.148	0.0963	0.209	0.202	0.199	0.189	0.799
90.75	22.763	0.72	0.119	0.906	0.37	0.759	0.133	0.353	0.148	0.0514	0.0358	0.148	0.0963	0.209	0.201	0.198	0.188	0.796
90.833	22.695	0.717	0.118	0.902	0.368	0.756	0.132	0.352	0.148	0.0513	0.0358	0.147	0.0962	0.208	0.2	0.197	0.187	0.792
90.917	22.628	0.714	0.118	0.897	0.367	0.752	0.131	0.35	0.147	0.0513	0.0358	0.147	0.096	0.207	0.199	0.196	0.186	0.788
91	22.56	0.71	0.117	0.893	0.365	0.749	0.131	0.349	0.146	0.0512	0.0358	0.147	0.0959	0.206	0.198	0.195	0.185	0.784
91.083	22.492	0.707	0.117	0.889	0.363	0.746	0.13	0.347	0.146	0.0511	0.0357	0.147	0.0956	0.205	0.197	0.194	0.184	0.78
91.167	22.424	0.704	0.117	0.885	0.361	0.742	0.13	0.345	0.145	0.051	0.0356	0.146	0.0953	0.204	0.196	0.193	0.184	0.777
91.25	22.356	0.7	0.116	0.881	0.36	0.739	0.129	0.344	0.144	0.0509	0.0355	0.146	0.0949	0.203	0.195	0.192	0.183	0.773
91.333	22.288	0.697	0.116	0.876	0.358	0.736	0.129	0.342	0.144	0.0508	0.0354	0.146	0.0944	0.202	0.194	0.191	0.182	0.769
91.417	22.22	0.694	0.115	0.872	0.356	0.732	0.128	0.341	0.143	0.0507	0.0352	0.145	0.0938	0.201	0.193	0.191	0.181	0.766
91.5	22.152	0.691	0.115	0.868	0.355	0.729	0.127	0.339	0.142	0.0506	0.0351	0.145	0.0933	0.2	0.193	0.19	0.18	0.763
91.583	22.084	0.687	0.115	0.864	0.353	0.725	0.127	0.338	0.142	0.0504	0.0349	0.144	0.0928	0.199	0.192	0.189	0.179	0.759
91.667	22.016	0.684	0.114	0.86	0.351	0.722	0.126	0.336	0.141	0.0503	0.0348	0.144	0.0923	0.199	0.191	0.188	0.178	0.756
91.75	21.949	0.681	0.114	0.856	0.349	0.718	0.126	0.335	0.14	0.0501	0.0346	0.143	0.0917	0.198	0.19	0.187	0.177	0.752
91.833	21.881	0.678	0.114	0.852	0.348	0.715	0.125	0.333	0.14	0.05	0.0344	0.143	0.0914	0.197	0.189	0.186	0.176	0.748
91.917	21.813	0.675	0.113	0.848	0.346	0.712	0.125	0.332	0.139	0.0498	0.0343	0.142	0.091	0.196	0.188	0.185	0.176	0.745
92	21.745	0.671	0.113	0.844	0.344	0.708	0.124	0.33	0.138	0.0496	0.0342	0.141	0.0906	0.195	0.187	0.184	0.175	0.741
92.083	21.677	0.668	0.113	0.84	0.343	0.705	0.124	0.329	0.138	0.0495	0.034	0.141	0.0903	0.194	0.186	0.184	0.174	0.738
92.167	21.61	0.665	0.112	0.836	0.341	0.702	0.123	0.328	0.137	0.0493	0.0339	0.14	0.09	0.193	0.186	0.183	0.173	0.735
92.25	21.542	0.662	0.112	0.832	0.339	0.698	0.122	0.326	0.137	0.0491	0.0338	0.14	0.0898	0.193	0.185	0.182	0.172	0.732
92.333	21.475	0.659	0.111	0.828	0.338	0.695	0.122	0.325	0.136	0.049	0.0337	0.139	0.0896	0.192	0.184	0.181	0.171	0.728
92.417	21.407	0.656	0.111	0.824	0.336	0.692	0.121	0.323	0.135	0.0488	0.0336	0.139	0.0894	0.191	0.183	0.18	0.17	0.724
92.5	21.34	0.653	0.111	0.821	0.335	0.688	0.121	0.322	0.135	0.0487	0.0336	0.138	0.0892	0.19	0.182	0.179	0.17	0.721
92.583	21.272	0.65	0.11	0.817	0.333	0.685	0.12	0.321	0.134	0.0486	0.0335	0.138	0.089	0.189	0.181	0.178	0.169	0.717
92.667	21.205	0.647	0.11	0.813	0.331	0.682	0.12	0.319	0.134	0.0484	0.0334	0.137	0.0889	0.188	0.181	0.178	0.168	0.715

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
92.75	21.138	0.644	0.109	0.809	0.33	0.679	0.119	0.318	0.133	0.0483	0.0334	0.137	0.0887	0.187	0.18	0.177	0.167	0.711
92.833	21.07	0.641	0.109	0.805	0.328	0.676	0.119	0.317	0.133	0.0482	0.0333	0.137	0.0887	0.187	0.179	0.176	0.166	0.708
92.917	21.003	0.638	0.108	0.801	0.327	0.672	0.118	0.316	0.132	0.0481	0.0333	0.136	0.0886	0.186	0.178	0.175	0.165	0.704
93	20.936	0.635	0.108	0.798	0.325	0.669	0.118	0.314	0.132	0.048	0.0332	0.136	0.0885	0.185	0.177	0.174	0.165	0.701
93.083	20.869	0.632	0.108	0.794	0.324	0.666	0.117	0.313	0.131	0.0479	0.0332	0.136	0.0885	0.184	0.176	0.174	0.164	0.698
93.167	20.802	0.629	0.107	0.79	0.322	0.663	0.117	0.312	0.13	0.0479	0.0331	0.136	0.0884	0.183	0.176	0.173	0.163	0.695
93.25	20.735	0.627	0.107	0.787	0.321	0.66	0.116	0.311	0.13	0.0478	0.0331	0.135	0.0884	0.183	0.175	0.172	0.162	0.692
93.333	20.668	0.624	0.106	0.783	0.32	0.657	0.116	0.309	0.129	0.0477	0.0331	0.135	0.0884	0.182	0.174	0.171	0.161	0.688
93.417	20.601	0.621	0.106	0.779	0.318	0.654	0.115	0.308	0.129	0.0476	0.033	0.135	0.0884	0.181	0.173	0.17	0.161	0.685
93.5	20.534	0.618	0.106	0.776	0.317	0.651	0.115	0.307	0.128	0.0476	0.033	0.135	0.0884	0.18	0.173	0.17	0.16	0.683
93.583	20.468	0.616	0.105	0.772	0.315	0.648	0.114	0.306	0.128	0.0475	0.033	0.135	0.0884	0.18	0.172	0.169	0.159	0.68
93.667	20.401	0.613	0.105	0.769	0.314	0.645	0.114	0.304	0.127	0.0475	0.033	0.134	0.0884	0.179	0.171	0.168	0.158	0.676
93.75	20.335	0.61	0.105	0.766	0.313	0.642	0.113	0.303	0.127	0.0474	0.033	0.134	0.0884	0.178	0.17	0.167	0.158	0.673
93.833	20.268	0.608	0.104	0.762	0.311	0.639	0.113	0.302	0.126	0.0473	0.033	0.134	0.0883	0.177	0.17	0.167	0.157	0.671
93.917	20.202	0.605	0.104	0.759	0.31	0.636	0.112	0.301	0.126	0.0473	0.0329	0.134	0.0882	0.177	0.169	0.166	0.156	0.668
94	20.136	0.603	0.104	0.755	0.309	0.633	0.112	0.3	0.125	0.0472	0.0329	0.134	0.0881	0.176	0.168	0.165	0.155	0.664
94.083	20.07	0.6	0.104	0.752	0.307	0.63	0.111	0.298	0.125	0.0471	0.0328	0.133	0.0878	0.175	0.167	0.164	0.155	0.661
94.167	20.003	0.598	0.103	0.749	0.306	0.628	0.111	0.297	0.124	0.047	0.0328	0.133	0.0875	0.174	0.167	0.164	0.154	0.659
94.25	19.937	0.595	0.103	0.746	0.304	0.625	0.111	0.296	0.124	0.0469	0.0327	0.133	0.0872	0.174	0.166	0.163	0.153	0.656
94.333	19.871	0.593	0.103	0.742	0.303	0.622	0.11	0.295	0.123	0.0468	0.0326	0.132	0.0867	0.173	0.165	0.162	0.153	0.653
94.417	19.806	0.59	0.102	0.739	0.302	0.619	0.11	0.294	0.123	0.0467	0.0324	0.132	0.0861	0.172	0.164	0.162	0.152	0.65
94.5	19.74	0.588	0.102	0.736	0.3	0.616	0.109	0.293	0.122	0.0466	0.0323	0.132	0.0856	0.172	0.164	0.161	0.151	0.648
94.583	19.674	0.585	0.102	0.733	0.299	0.613	0.109	0.291	0.122	0.0464	0.0321	0.131	0.0851	0.171	0.163	0.16	0.15	0.644
94.667	19.609	0.582	0.101	0.729	0.298	0.61	0.108	0.29	0.121	0.0463	0.032	0.13	0.0846	0.17	0.162	0.159	0.15	0.641
94.75	19.543	0.58	0.101	0.726	0.296	0.607	0.108	0.289	0.121	0.0462	0.0318	0.13	0.084	0.17	0.162	0.159	0.149	0.64
94.833	19.478	0.577	0.101	0.723	0.295	0.604	0.107	0.288	0.12	0.046	0.0317	0.129	0.0836	0.169	0.161	0.158	0.148	0.636
94.917	19.413	0.575	0.1	0.72	0.294	0.602	0.107	0.287	0.12	0.0458	0.0315	0.129	0.0832	0.168	0.16	0.157	0.148	0.633
95	19.348	0.572	0.1	0.717	0.292	0.599	0.107	0.286	0.119	0.0457	0.0314	0.128	0.0828	0.167	0.16	0.157	0.147	0.631
95.083	19.283	0.57	0.0996	0.713	0.291	0.596	0.106	0.285	0.119	0.0455	0.0312	0.128	0.0826	0.167	0.159	0.156	0.146	0.628
95.167	19.218	0.567	0.0992	0.71	0.29	0.593	0.106	0.284	0.118	0.0453	0.0311	0.127	0.0823	0.166	0.158	0.155	0.146	0.625
95.25	19.154	0.565	0.0989	0.707	0.288	0.59	0.105	0.283	0.118	0.0452	0.031	0.126	0.082	0.165	0.158	0.155	0.145	0.623
95.333	19.089	0.562	0.0985	0.704	0.287	0.588	0.105	0.282	0.117	0.045	0.0309	0.126	0.0818	0.165	0.157	0.154	0.144	0.62
95.417	19.024	0.56	0.0981	0.701	0.286	0.585	0.104	0.281	0.117	0.0449	0.0308	0.125	0.0816	0.164	0.156	0.153	0.144	0.617
95.5	18.96	0.557	0.0977	0.698	0.284	0.582	0.104	0.28	0.116	0.0447	0.0307	0.125	0.0814	0.163	0.156	0.153	0.143	0.615
95.583	18.896	0.555	0.0972	0.695	0.283	0.58	0.103	0.279	0.116	0.0446	0.0307	0.125	0.0812	0.163	0.155	0.152	0.142	0.612
95.667	18.832	0.552	0.0968	0.691	0.282	0.577	0.103	0.278	0.115	0.0445	0.0306	0.124	0.0811	0.162	0.154	0.151	0.141	0.608
95.75	18.768	0.55	0.0964	0.688	0.281	0.574	0.103	0.277	0.115	0.0444	0.0305	0.124	0.0809	0.161	0.153	0.151	0.141	0.606
95.833	18.704	0.547	0.0959	0.685	0.279	0.572	0.102	0.276	0.115	0.0443	0.0305	0.123	0.0809	0.161	0.153	0.15	0.14	0.604
95.917	18.64	0.545	0.0955	0.682	0.278	0.569	0.102	0.275	0.114	0.0442	0.0304	0.123	0.0808	0.16	0.152	0.149	0.139	0.6
96	18.577	0.542	0.0951	0.679	0.277	0.566	0.101	0.274	0.114	0.044	0.0304	0.123	0.0807	0.159	0.151	0.149	0.139	0.598
96.083	18.513	0.54	0.0946	0.676	0.276	0.564	0.101	0.273	0.113	0.044	0.0303	0.123	0.0806	0.159	0.151	0.148	0.138	0.596
96.167	18.45	0.538	0.0942	0.673	0.274	0.561	0.1	0.272	0.113	0.0439	0.0303	0.122	0.0806	0.158	0.15	0.147	0.137	0.592
96.25	18.387	0.535	0.0938	0.67	0.273	0.559	0.1	0.271	0.112	0.0438	0.0303	0.122	0.0806	0.157	0.149	0.147	0.137	0.59
96.333	18.324	0.533	0.0935	0.667	0.272	0.556	0.0996	0.27	0.112	0.0437	0.0302	0.122	0.0806	0.157	0.149	0.146	0.136	0.588
96.417	18.261	0.531	0.0931	0.664	0.271	0.554	0.0992	0.269	0.112	0.0437	0.0302	0.122	0.0806	0.156	0.148	0.145	0.135	0.584
96.5	18.198	0.529	0.0927	0.661	0.27	0.551	0.0988	0.268	0.111	0.0436	0.0302	0.121	0.0806	0.155	0.147	0.145	0.135	0.582
96.583	18.136	0.526	0.0924	0.658	0.269	0.549	0.0984	0.267	0.111	0.0435	0.0302	0.121	0.0806	0.155	0.147	0.144	0.134	0.58
96.667	18.073	0.524	0.0921	0.655	0.267	0.546	0.098	0.266	0.11	0.0435	0.0302	0.121	0.0806	0.154	0.146	0.143	0.134	0.577
96.75	18.011	0.522	0.0918	0.652	0.266	0.544	0.0976	0.265	0.11	0.0434	0.0302	0.121	0.0806	0.153	0.146	0.143	0.133	0.575
96.833	17.949	0.52	0.0915	0.649	0.265	0.541	0.0973	0.264	0.109	0.0434	0.0302	0.121	0.0806	0.153	0.145	0.142	0.132	0.572
96.917	17.887	0.517	0.0912	0.646	0.264	0.539	0.0969	0.263	0.109	0.0433	0.0302	0.121	0.0806	0.152	0.144	0.141	0.132	0.569
97	17.825	0.515	0.0909	0.644	0.263	0.536	0.0965	0.262	0.109	0.0433	0.0302	0.121	0.0806	0.152	0.144	0.141	0.131	0.568
97.083	17.764	0.513	0.0906	0.641	0.262	0.534	0.0961	0.261	0.108	0.0432	0.0302	0.12	0.0806	0.151	0.143	0.14	0.13	0.564
97.167	17.703	0.511	0.0904	0.638	0.261	0.531	0.0957	0.26	0.108	0.0432	0.0302	0.12	0.0806	0.15	0.143	0.14	0.13	0.563
97.25	17.641	0.509	0.0901	0.635	0.26	0.529	0.0954	0.259	0.107	0.0432	0.0302	0.12	0.0806	0.15	0.142	0.139	0.129	0.56
97.333	17.58	0.507	0.0899	0.633	0.259	0.527	0.095	0.258	0.107	0.0431	0.0302	0.12	0.0806	0.149	0.141	0.138	0.129	0.557
97.417	17.519	0.505	0.0897	0.63	0.258	0.524	0.0946	0.258	0.107	0.0431	0.0302	0.12	0.0806	0.149	0.141	0.138	0.128	0.556
97.5	17.458	0.503	0.0894	0.627	0.257	0.522	0.0943	0.257	0.106	0.0431	0.0302	0.12	0.0806	0.148	0.14	0.137	0.127	0.552
97.583	17.398	0.501	0.0893	0.624	0.256	0.52	0.0939	0.256	0.106	0.043	0.0302	0.12	0.0806	0.147	0.14	0.137	0.127	0.551
97.667	17.338	0.499	0.0891	0.622	0.255	0.517	0.0935	0.255	0.105	0.043	0.0302	0.12	0.0806	0.147	0.139	0.136	0.126	0.548
97.75	17.277	0.497	0.0889	0.619	0.253	0.515	0.0932	0.254	0.105	0.043	0.0302	0.12	0.0806	0.146	0.138	0.136	0.126	0.546
97.833	17.217	0.495	0.0887	0.617	0.252	0.513	0.0928	0.253	0.105	0.043	0.0302	0.12	0.0806	0.146	0.138	0.135	0.125	0.544
97.917	17.157	0.493	0.0886	0.614	0.251	0.511	0.0925	0.253	0.104	0.043	0.0302	0.12	0.0806	0.145	0.137	0.134	0.125	0.541
98	17.097	0.491	0.0884	0.611	0.25	0.508	0.0921	0.252	0.104	0.043	0.0302	0.12	0.0806	0.145	0.137	0.134	0.124	0.54
98.083	17.038	0.489	0.0883	0.609	0.249	0.506	0.0918	0.251	0.104	0.043	0.0302	0.12	0.0806	0.144	0.136	0.133	0.123	0.536
98.167	16.979	0.487	0.0882	0.606	0.248	0.504	0.0915	0.251	0.103	0.0429	0.0302	0.12	0.0806	0.143	0.136	0.133	0.123	0.535
98.25	16.919	0.485	0.0881	0.604	0.247	0.502	0.0911	0.25	0.103	0.0429	0.0302	0.12	0.0806	0.143	0.135	0.132	0.122	0.532

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
98.333	16.861	0.483	0.0879	0.601	0.246	0.5	0.0908	0.249	0.103	0.0429	0.0302	0.12	0.0806	0.142	0.135	0.132	0.122	0.531
98.417	16.802	0.481	0.0878	0.599	0.245	0.498	0.0905	0.248	0.102	0.0429	0.0302	0.12	0.0806	0.142	0.134	0.131	0.121	0.528
98.5	16.743	0.479	0.0877	0.596	0.245	0.495	0.0901	0.248	0.102	0.0429	0.0302	0.12	0.0806	0.141	0.133	0.131	0.121	0.526
98.583	16.685	0.478	0.0876	0.594	0.244	0.493	0.0898	0.247	0.102	0.0429	0.0302	0.12	0.0806	0.141	0.133	0.13	0.12	0.524
98.667	16.627	0.476	0.0875	0.592	0.243	0.491	0.0895	0.247	0.102	0.0429	0.0302	0.12	0.0806	0.14	0.132	0.13	0.12	0.522
98.75	16.568	0.474	0.0874	0.589	0.242	0.489	0.0891	0.246	0.101	0.0429	0.0302	0.12	0.0806	0.14	0.132	0.129	0.119	0.52
98.833	16.511	0.472	0.0873	0.587	0.241	0.487	0.0888	0.245	0.101	0.0429	0.0302	0.12	0.0806	0.139	0.131	0.128	0.119	0.517
98.917	16.453	0.471	0.0872	0.584	0.24	0.485	0.0885	0.245	0.101	0.0429	0.0302	0.12	0.0806	0.139	0.131	0.128	0.118	0.516
99	16.395	0.469	0.0871	0.582	0.239	0.483	0.0882	0.244	0.1	0.0429	0.0302	0.12	0.0806	0.138	0.13	0.127	0.118	0.513
99.083	16.338	0.467	0.087	0.58	0.239	0.482	0.0879	0.244	0.1	0.0429	0.0302	0.12	0.0806	0.138	0.13	0.127	0.117	0.512
99.167	16.281	0.466	0.0869	0.577	0.238	0.48	0.0876	0.243	0.1	0.0429	0.0302	0.12	0.0806	0.137	0.129	0.126	0.117	0.509
99.25	16.224	0.464	0.0868	0.575	0.237	0.478	0.0873	0.243	0.0998	0.0429	0.0302	0.12	0.0806	0.137	0.129	0.126	0.116	0.508
99.333	16.167	0.462	0.0867	0.573	0.236	0.476	0.0871	0.242	0.0995	0.0429	0.0302	0.12	0.0806	0.136	0.128	0.126	0.116	0.506
99.417	16.111	0.461	0.0866	0.571	0.236	0.474	0.0868	0.242	0.0993	0.0429	0.0302	0.12	0.0806	0.136	0.128	0.125	0.115	0.504
99.5	16.054	0.459	0.0866	0.569	0.235	0.472	0.0865	0.241	0.099	0.0429	0.0302	0.12	0.0806	0.135	0.127	0.125	0.115	0.502
99.583	15.998	0.458	0.0865	0.567	0.234	0.471	0.0863	0.241	0.0988	0.0429	0.0302	0.12	0.0806	0.135	0.127	0.124	0.114	0.5
99.667	15.942	0.456	0.0864	0.565	0.233	0.469	0.086	0.241	0.0986	0.0429	0.0302	0.12	0.0806	0.134	0.127	0.124	0.114	0.499
99.75	15.886	0.455	0.0864	0.562	0.233	0.467	0.0857	0.24	0.0984	0.0429	0.0302	0.12	0.0806	0.134	0.126	0.123	0.113	0.496
99.833	15.831	0.454	0.0863	0.561	0.232	0.465	0.0855	0.24	0.0982	0.0429	0.0302	0.12	0.0806	0.134	0.126	0.123	0.113	0.496
99.917	15.775	0.452	0.0863	0.559	0.232	0.464	0.0852	0.239	0.0979	0.0429	0.0302	0.12	0.0806	0.133	0.125	0.122	0.113	0.493
100	15.72	0.451	0.0862	0.557	0.231	0.462	0.085	0.239	0.0977	0.0429	0.0302	0.12	0.0806	0.133	0.125	0.122	0.112	0.492
100.083	15.665	0.45	0.0862	0.555	0.23	0.46	0.0848	0.239	0.0975	0.0429	0.0302	0.12	0.0806	0.132	0.125	0.122	0.112	0.491
100.167	15.61	0.448	0.0861	0.553	0.23	0.459	0.0845	0.238	0.0973	0.0429	0.0302	0.12	0.0806	0.132	0.124	0.121	0.111	0.488
100.25	15.555	0.447	0.0861	0.551	0.229	0.457	0.0843	0.238	0.0971	0.0429	0.0302	0.12	0.0806	0.132	0.124	0.121	0.111	0.488
100.333	15.501	0.446	0.0861	0.55	0.229	0.455	0.0841	0.238	0.0969	0.0429	0.0302	0.12	0.0806	0.131	0.123	0.12	0.111	0.485
100.417	15.446	0.445	0.086	0.548	0.228	0.454	0.0839	0.237	0.0968	0.0429	0.0302	0.12	0.0806	0.131	0.123	0.12	0.11	0.484
100.5	15.392	0.444	0.086	0.546	0.227	0.452	0.0836	0.237	0.0966	0.0429	0.0302	0.12	0.0806	0.13	0.123	0.12	0.11	0.483
100.583	15.338	0.443	0.086	0.544	0.227	0.451	0.0834	0.237	0.0964	0.0429	0.0302	0.12	0.0806	0.13	0.122	0.119	0.109	0.48
100.667	15.285	0.441	0.086	0.543	0.226	0.449	0.0832	0.236	0.0962	0.0429	0.0302	0.12	0.0806	0.13	0.122	0.119	0.109	0.48
100.75	15.231	0.44	0.086	0.541	0.226	0.447	0.083	0.236	0.0961	0.0429	0.0302	0.12	0.0806	0.129	0.122	0.119	0.109	0.479
100.833	15.178	0.439	0.0859	0.54	0.225	0.446	0.0828	0.236	0.0959	0.0429	0.0302	0.12	0.0806	0.129	0.121	0.118	0.108	0.476
100.917	15.125	0.438	0.0859	0.538	0.225	0.444	0.0827	0.236	0.0958	0.0429	0.0302	0.12	0.0806	0.129	0.121	0.118	0.108	0.476
101	15.072	0.437	0.0859	0.537	0.225	0.443	0.0825	0.235	0.0956	0.0429	0.0302	0.12	0.0806	0.128	0.121	0.118	0.108	0.475
101.083	15.019	0.436	0.0859	0.535	0.224	0.441	0.0823	0.235	0.0955	0.0429	0.0302	0.12	0.0806	0.128	0.12	0.117	0.107	0.472
101.167	14.966	0.435	0.0859	0.534	0.224	0.44	0.0821	0.235	0.0953	0.0429	0.0302	0.12	0.0806	0.128	0.12	0.117	0.107	0.472
101.25	14.914	0.434	0.0859	0.532	0.223	0.439	0.082	0.235	0.0952	0.0429	0.0302	0.12	0.0806	0.127	0.12	0.117	0.107	0.471
101.333	14.862	0.434	0.0859	0.531	0.223	0.437	0.0818	0.234	0.095	0.0429	0.0302	0.12	0.0806	0.127	0.119	0.116	0.106	0.468
101.417	14.809	0.433	0.0859	0.529	0.222	0.436	0.0816	0.234	0.0949	0.0429	0.0302	0.12	0.0806	0.127	0.119	0.116	0.106	0.468
101.5	14.757	0.432	0.0859	0.528	0.222	0.435	0.0815	0.234	0.0948	0.0429	0.0302	0.12	0.0806	0.127	0.119	0.116	0.106	0.468
101.583	14.706	0.431	0.0859	0.527	0.221	0.433	0.0813	0.234	0.0947	0.0429	0.0302	0.12	0.0806	0.126	0.118	0.116	0.106	0.466
101.667	14.654	0.43	0.0859	0.525	0.221	0.432	0.0812	0.234	0.0945	0.0429	0.0302	0.12	0.0806	0.126	0.118	0.115	0.105	0.464
101.75	14.603	0.429	0.0859	0.524	0.221	0.431	0.081	0.233	0.0944	0.0429	0.0302	0.12	0.0806	0.126	0.118	0.115	0.105	0.464
101.833	14.552	0.429	0.0859	0.523	0.22	0.43	0.0809	0.233	0.0943	0.0429	0.0302	0.12	0.0806	0.125	0.118	0.115	0.105	0.463
101.917	14.501	0.428	0.0859	0.522	0.22	0.428	0.0807	0.233	0.0942	0.0429	0.0302	0.12	0.0806	0.125	0.117	0.114	0.105	0.461
102	14.45	0.427	0.0859	0.52	0.22	0.427	0.0806	0.233	0.0941	0.0429	0.0302	0.12	0.0806	0.125	0.117	0.114	0.104	0.46
102.083	14.399	0.426	0.0859	0.519	0.219	0.426	0.0805	0.233	0.094	0.0429	0.0302	0.12	0.0806	0.125	0.117	0.114	0.104	0.46
102.167	14.349	0.425	0.0859	0.518	0.219	0.425	0.0803	0.233	0.0939	0.0429	0.0302	0.12	0.0806	0.124	0.117	0.114	0.104	0.459
102.25	14.298	0.425	0.0859	0.517	0.219	0.424	0.0802	0.232	0.0938	0.0429	0.0302	0.12	0.0806	0.124	0.116	0.113	0.104	0.457
102.333	14.248	0.424	0.0859	0.516	0.218	0.423	0.0801	0.232	0.0937	0.0429	0.0302	0.12	0.0806	0.124	0.116	0.113	0.103	0.456
102.417	14.198	0.423	0.0859	0.515	0.218	0.422	0.0799	0.232	0.0936	0.0429	0.0302	0.12	0.0806	0.124	0.116	0.113	0.103	0.456
102.5	14.149	0.423	0.0859	0.514	0.218	0.421	0.0798	0.232	0.0935	0.0429	0.0302	0.12	0.0806	0.124	0.116	0.113	0.103	0.456
102.583	14.099	0.422	0.0859	0.513	0.217	0.42	0.0797	0.232	0.0934	0.0429	0.0302	0.12	0.0806	0.123	0.115	0.113	0.103	0.454
102.667	14.05	0.421	0.0859	0.512	0.217	0.419	0.0796	0.232	0.0933	0.0429	0.0302	0.12	0.0806	0.123	0.115	0.112	0.102	0.452
102.75	14	0.421	0.0859	0.511	0.217	0.418	0.0795	0.232	0.0932	0.0429	0.0302	0.12	0.0806	0.123	0.115	0.112	0.102	0.452
102.833	13.951	0.42	0.0859	0.51	0.216	0.417	0.0793	0.231	0.0931	0.0429	0.0301	0.12	0.0805	0.123	0.115	0.112	0.102	0.452
102.917	13.902	0.419	0.0859	0.509	0.216	0.416	0.0792	0.231	0.093	0.0429	0.0301	0.12	0.0804	0.123	0.115	0.112	0.102	0.452
103	13.853	0.419	0.0859	0.508	0.216	0.415	0.0791	0.231	0.093	0.0429	0.0301	0.12	0.0804	0.122	0.114	0.112	0.102	0.45
103.083	13.805	0.418	0.0858	0.507	0.216	0.414	0.079	0.231	0.0929	0.0429	0.03	0.12	0.0801	0.122	0.114	0.111	0.101	0.448
103.167	13.757	0.418	0.0858	0.506	0.215	0.413	0.0789	0.231	0.0928	0.0428	0.03	0.12	0.0799	0.122	0.114	0.111	0.101	0.448
103.25	13.708	0.417	0.0857	0.506	0.215	0.412	0.0788	0.231	0.0927	0.0428	0.0299	0.119	0.0796	0.122	0.114	0.111	0.101	0.448
103.333	13.66	0.416	0.0857	0.505	0.215	0.412	0.0787	0.231	0.0926	0.0427	0.0298	0.119	0.0792	0.122	0.114	0.111	0.101	0.448
103.417	13.613	0.416	0.0856	0.504	0.214	0.411	0.0786	0.23	0.0925	0.0426	0.0297	0.119	0.0787	0.121	0.113	0.111	0.101	0.446
103.5	13.565	0.415	0.0855	0.503	0.214	0.41	0.0785	0.23	0.0924	0.0426	0.0296	0.118	0.0783	0.121	0.113	0.11	0.1	0.444
103.583	13.518	0.415	0.0853	0.502	0.214	0.409	0.0783	0.23	0.0923	0.0424	0.0294	0.118	0.0777	0.121	0.113	0.11	0.1	0.444
103.667	13.47	0.414	0.0852	0.501	0.213	0.408	0.0782	0.23	0.0922	0.0423	0.0293	0.118	0.0772	0.121	0.113	0.11	0.1	0.444
103.75	13.423	0.413	0.0851	0.5	0.213	0.407	0.0781	0.23	0.0921	0.0422	0.0291	0.117	0.0767	0.121	0.113	0.11	0.0999	0.4439
103.833	13.376	0.413	0.0849	0.499	0.213	0.406	0.078	0.229	0.0919	0.0421	0.029	0.116	0.0762	0.12	0.113	0.11	0.0997	0.4427

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
103.917	13.329	0.412	0.0847	0.499	0.213	0.405	0.0779	0.229	0.0918	0.0419	0.0288	0.116	0.0758	0.12	0.112	0.109	0.0995	0.4405
104	13.282	0.412	0.0845	0.498	0.212	0.405	0.0778	0.229	0.0917	0.0418	0.0286	0.115	0.0753	0.12	0.112	0.109	0.0994	0.4404
104.083	13.236	0.411	0.0843	0.497	0.212	0.404	0.0777	0.228	0.0916	0.0416	0.0285	0.115	0.075	0.12	0.112	0.109	0.0992	0.4402
104.167	13.189	0.41	0.0841	0.496	0.212	0.403	0.0776	0.228	0.0915	0.0415	0.0284	0.114	0.0747	0.12	0.112	0.109	0.099	0.44
104.25	13.143	0.41	0.0839	0.495	0.211	0.402	0.0774	0.228	0.0914	0.0413	0.0283	0.113	0.0744	0.119	0.112	0.109	0.0988	0.4388
104.333	13.097	0.409	0.0836	0.494	0.211	0.401	0.0773	0.228	0.0913	0.0412	0.0282	0.113	0.0742	0.119	0.111	0.108	0.0986	0.4366
104.417	13.051	0.408	0.0833	0.493	0.211	0.4	0.0772	0.227	0.0911	0.041	0.0281	0.112	0.0739	0.119	0.111	0.108	0.0984	0.4364
104.5	13.006	0.408	0.0831	0.492	0.21	0.4	0.0771	0.227	0.091	0.0409	0.028	0.112	0.0737	0.119	0.111	0.108	0.0982	0.4362
104.583	12.96	0.407	0.0828	0.492	0.21	0.399	0.077	0.227	0.0909	0.0407	0.0279	0.112	0.0736	0.119	0.111	0.108	0.098	0.436
104.667	12.915	0.406	0.0825	0.491	0.21	0.398	0.0769	0.226	0.0908	0.0406	0.0278	0.111	0.0734	0.119	0.111	0.108	0.0978	0.4358
104.75	12.87	0.406	0.0821	0.49	0.209	0.397	0.0767	0.226	0.0906	0.0405	0.0278	0.111	0.0732	0.118	0.11	0.108	0.0976	0.4336
104.833	12.825	0.405	0.0818	0.489	0.209	0.397	0.0766	0.225	0.0905	0.0404	0.0277	0.11	0.0731	0.118	0.11	0.107	0.0974	0.4324
104.917	12.78	0.404	0.0815	0.488	0.208	0.396	0.0765	0.225	0.0904	0.0402	0.0276	0.11	0.073	0.118	0.11	0.107	0.0973	0.4323
105	12.735	0.404	0.0811	0.487	0.208	0.395	0.0764	0.225	0.0902	0.0401	0.0276	0.11	0.0729	0.118	0.11	0.107	0.0971	0.4321
105.083	12.69	0.403	0.0808	0.486	0.208	0.394	0.0762	0.224	0.0901	0.04	0.0275	0.109	0.0729	0.118	0.11	0.107	0.0969	0.4319
105.167	12.646	0.402	0.0805	0.485	0.207	0.393	0.0761	0.224	0.0899	0.04	0.0275	0.109	0.0728	0.117	0.109	0.107	0.0967	0.4297
105.25	12.602	0.402	0.0802	0.484	0.207	0.393	0.076	0.223	0.0898	0.0399	0.0275	0.109	0.0728	0.117	0.109	0.106	0.0965	0.4285
105.333	12.558	0.401	0.0799	0.483	0.207	0.392	0.0759	0.223	0.0896	0.0398	0.0274	0.109	0.0727	0.117	0.109	0.106	0.0963	0.4283
105.417	12.514	0.4	0.0796	0.483	0.206	0.391	0.0757	0.222	0.0895	0.0397	0.0274	0.108	0.0727	0.117	0.109	0.106	0.0961	0.4281
105.5	12.47	0.399	0.0793	0.482	0.206	0.391	0.0756	0.222	0.0893	0.0396	0.0274	0.108	0.0727	0.117	0.109	0.106	0.0959	0.4279
105.583	12.426	0.399	0.079	0.481	0.205	0.39	0.0755	0.221	0.0892	0.0396	0.0274	0.108	0.0727	0.116	0.108	0.106	0.0957	0.4257
105.667	12.383	0.398	0.0787	0.48	0.205	0.389	0.0754	0.221	0.089	0.0395	0.0273	0.108	0.0727	0.116	0.108	0.105	0.0955	0.4245
105.75	12.34	0.397	0.0784	0.479	0.205	0.388	0.0752	0.22	0.0888	0.0395	0.0273	0.108	0.0727	0.116	0.108	0.105	0.0953	0.4243
105.833	12.297	0.396	0.0782	0.478	0.204	0.388	0.0751	0.22	0.0887	0.0394	0.0273	0.108	0.0727	0.116	0.108	0.105	0.0951	0.4241
105.917	12.254	0.396	0.0779	0.477	0.204	0.387	0.075	0.219	0.0885	0.0394	0.0273	0.107	0.0727	0.116	0.108	0.105	0.0949	0.4239
106	12.211	0.395	0.0777	0.476	0.203	0.386	0.0748	0.218	0.0883	0.0393	0.0273	0.107	0.0727	0.115	0.107	0.105	0.0947	0.4217
106.083	12.168	0.394	0.0775	0.475	0.203	0.386	0.0747	0.218	0.0881	0.0393	0.0273	0.107	0.0727	0.115	0.107	0.104	0.0944	0.4204
106.167	12.126	0.393	0.0772	0.474	0.203	0.385	0.0746	0.217	0.088	0.0392	0.0273	0.107	0.0727	0.115	0.107	0.104	0.0942	0.4202
106.25	12.083	0.393	0.077	0.473	0.202	0.384	0.0744	0.217	0.0878	0.0392	0.0273	0.107	0.0727	0.115	0.107	0.104	0.094	0.42
106.333	12.041	0.392	0.0768	0.472	0.202	0.383	0.0743	0.216	0.0876	0.0391	0.0273	0.107	0.0727	0.115	0.107	0.104	0.0938	0.4198
106.417	11.999	0.391	0.0766	0.471	0.201	0.383	0.0741	0.215	0.0874	0.0391	0.0273	0.107	0.0727	0.114	0.106	0.104	0.0936	0.4176
106.5	11.957	0.39	0.0764	0.47	0.201	0.382	0.074	0.215	0.0872	0.0391	0.0273	0.107	0.0727	0.114	0.106	0.103	0.0934	0.4164
106.583	11.915	0.389	0.0762	0.469	0.2	0.381	0.0739	0.214	0.087	0.0391	0.0273	0.107	0.0727	0.114	0.106	0.103	0.0932	0.4162
106.667	11.874	0.388	0.0761	0.468	0.2	0.381	0.0737	0.214	0.0868	0.039	0.0273	0.107	0.0727	0.114	0.106	0.103	0.093	0.416
106.75	11.832	0.388	0.0759	0.467	0.2	0.38	0.0736	0.213	0.0866	0.039	0.0273	0.107	0.0727	0.113	0.106	0.103	0.0927	0.4147
106.833	11.791	0.387	0.0758	0.466	0.199	0.379	0.0734	0.213	0.0864	0.039	0.0273	0.107	0.0727	0.113	0.105	0.102	0.0925	0.4125
106.917	11.75	0.386	0.0756	0.465	0.199	0.379	0.0733	0.212	0.0862	0.039	0.0273	0.107	0.0727	0.113	0.105	0.102	0.0923	0.4123
107	11.709	0.385	0.0755	0.464	0.198	0.378	0.0732	0.212	0.086	0.039	0.0273	0.107	0.0727	0.113	0.105	0.102	0.0921	0.4121
107.083	11.668	0.384	0.0753	0.463	0.198	0.377	0.073	0.211	0.0859	0.039	0.0273	0.107	0.0727	0.113	0.105	0.102	0.0919	0.4119
107.167	11.627	0.383	0.0752	0.462	0.197	0.377	0.0729	0.211	0.0857	0.0389	0.0273	0.107	0.0727	0.112	0.104	0.102	0.0916	0.4096
107.25	11.587	0.383	0.075	0.461	0.197	0.376	0.0727	0.21	0.0855	0.0389	0.0273	0.107	0.0727	0.112	0.104	0.101	0.0914	0.4084
107.333	11.546	0.382	0.0749	0.46	0.196	0.375	0.0726	0.21	0.0853	0.0389	0.0273	0.107	0.0727	0.112	0.104	0.101	0.0912	0.4082
107.417	11.506	0.381	0.0748	0.459	0.196	0.375	0.0724	0.209	0.0851	0.0389	0.0273	0.107	0.0727	0.112	0.104	0.101	0.091	0.408
107.5	11.466	0.38	0.0747	0.458	0.195	0.374	0.0723	0.209	0.085	0.0389	0.0273	0.107	0.0727	0.111	0.104	0.101	0.0907	0.4067
107.583	11.426	0.379	0.0746	0.457	0.195	0.373	0.0721	0.209	0.0848	0.0389	0.0273	0.107	0.0727	0.111	0.103	0.1	0.0905	0.4045
107.667	11.386	0.378	0.0745	0.456	0.194	0.373	0.072	0.208	0.0846	0.0389	0.0273	0.107	0.0727	0.111	0.103	0.1	0.0903	0.4043
107.75	11.346	0.377	0.0743	0.455	0.194	0.372	0.0718	0.208	0.0845	0.0389	0.0273	0.107	0.0727	0.111	0.103	0.0999	0.09	0.4039
107.833	11.307	0.377	0.0742	0.454	0.193	0.371	0.0717	0.207	0.0843	0.0389	0.0273	0.107	0.0727	0.111	0.103	0.0997	0.0898	0.4035
107.917	11.267	0.376	0.0741	0.453	0.193	0.371	0.0715	0.207	0.0841	0.0389	0.0273	0.107	0.0727	0.11	0.102	0.0995	0.0896	0.4011
108	11.228	0.375	0.074	0.452	0.193	0.37	0.0714	0.206	0.084	0.0389	0.0273	0.107	0.0727	0.11	0.102	0.0992	0.0893	0.4005
108.083	11.189	0.374	0.0739	0.451	0.192	0.369	0.0712	0.206	0.0838	0.0389	0.0273	0.107	0.0727	0.11	0.102	0.099	0.0891	0.4001
108.167	11.15	0.373	0.0738	0.45	0.192	0.369	0.0711	0.206	0.0837	0.0389	0.0273	0.107	0.0727	0.11	0.102	0.0988	0.0889	0.3997
108.25	11.111	0.372	0.0738	0.448	0.191	0.368	0.0709	0.205	0.0835	0.0389	0.0273	0.107	0.0727	0.109	0.101	0.0986	0.0886	0.3972
108.333	11.073	0.372	0.0737	0.447	0.191	0.367	0.0708	0.205	0.0834	0.0389	0.0273	0.107	0.0727	0.109	0.101	0.0983	0.0884	0.3967
108.417	11.034	0.371	0.0736	0.446	0.19	0.367	0.0707	0.205	0.0833	0.0389	0.0273	0.107	0.0727	0.109	0.101	0.0981	0.0882	0.3963
108.5	10.996	0.37	0.0735	0.445	0.19	0.366	0.0705	0.204	0.0831	0.0389	0.0273	0.107	0.0727	0.109	0.101	0.0979	0.088	0.3959
108.583	10.958	0.369	0.0734	0.444	0.19	0.365	0.0704	0.204	0.083	0.0389	0.0273	0.107	0.0727	0.108	0.101	0.0977	0.0878	0.3945
108.667	10.92	0.369	0.0734	0.444	0.189	0.365	0.0703	0.204	0.0828	0.0389	0.0273	0.107	0.0727	0.108	0.1	0.0975	0.0875	0.393
108.75	10.881	0.368	0.0733	0.443	0.189	0.364	0.0701	0.203	0.0827	0.0389	0.0273	0.107	0.0727	0.108	0.1	0.0973	0.0873	0.3926
108.833	10.844	0.367	0.0733	0.442	0.189	0.363	0.07	0.203	0.0826	0.0389	0.0273	0.107	0.0727	0.108	0.1	0.0971	0.0871	0.3922
108.917	10.806	0.367	0.0732	0.441	0.188	0.363	0.0699	0.203	0.0824	0.0389	0.0273	0.107	0.0727	0.108	0.0998	0.0969	0.0869	0.3916
109	10.768	0.366	0.0731	0.44	0.188	0.362	0.0698	0.203	0.0823	0.0389	0.0273	0.107	0.0727	0.107	0.0996	0.0967	0.0867	0.39
109.083	10.731	0.365	0.0731	0.439	0.188	0.361	0.0696	0.202	0.0822	0.0389	0.0273	0.107	0.0727	0.107	0.0994	0.0965	0.0865	0.3894
109.167	10.694	0.365	0.0731	0.438	0.187	0.361	0.0695	0.202	0.0821	0.0389	0.0273	0.107	0.0727	0.107	0.0992	0.0963	0.0864	0.3889
109.25	10.656	0.364	0.073	0.437	0.187	0.36	0.0694	0.202	0.082	0.0389	0.0273	0.107	0.0727	0.107	0.099	0.0961	0.0862	0.3883
109.333	10.62	0.363	0.073	0.436	0.187	0.359	0.0693	0.202	0.0818	0.0389	0.0273	0.107	0.0727	0.107	0.0988	0.0959	0.086	0.3877
109.417	10.583	0.363	0.073	0.435	0.186	0.359	0.0692	0.201	0.0817	0.0389	0.0273	0.107	0.0727	0.107	0.0987	0.0957	0.0858	0.3872

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
109.5	10.546	0.362	0.0729	0.435	0.186	0.358	0.0691	0.201	0.0816	0.0389	0.0273	0.107	0.0727	0.106	0.0985	0.0955	0.0856	0.3856
109.583	10.51	0.361	0.0729	0.434	0.186	0.357	0.069	0.201	0.0815	0.0389	0.0273	0.107	0.0727	0.106	0.0983	0.0954	0.0854	0.3851
109.667	10.473	0.361	0.0729	0.433	0.185	0.357	0.0688	0.201	0.0814	0.0389	0.0273	0.107	0.0727	0.106	0.0981	0.0952	0.0853	0.3846
109.75	10.437	0.36	0.0728	0.432	0.185	0.356	0.0687	0.2	0.0813	0.0389	0.0273	0.107	0.0727	0.106	0.098	0.095	0.0851	0.3841
109.833	10.401	0.36	0.0728	0.431	0.185	0.355	0.0686	0.2	0.0812	0.0389	0.0273	0.107	0.0727	0.106	0.0978	0.0949	0.0849	0.3836
109.917	10.364	0.359	0.0728	0.431	0.185	0.355	0.0685	0.2	0.0811	0.0389	0.0273	0.107	0.0727	0.105	0.0976	0.0947	0.0848	0.3821
110	10.328	0.359	0.0728	0.43	0.184	0.354	0.0684	0.2	0.081	0.0389	0.0273	0.107	0.0727	0.105	0.0974	0.0945	0.0846	0.3815
110.083	10.293	0.358	0.0728	0.429	0.184	0.353	0.0683	0.2	0.0809	0.0389	0.0273	0.107	0.0727	0.105	0.0973	0.0944	0.0844	0.3811
110.167	10.257	0.357	0.0728	0.428	0.184	0.353	0.0683	0.199	0.0808	0.0389	0.0273	0.107	0.0727	0.105	0.0971	0.0942	0.0843	0.3806
110.25	10.221	0.357	0.0728	0.428	0.183	0.352	0.0682	0.199	0.0807	0.0389	0.0273	0.107	0.0727	0.105	0.097	0.094	0.0841	0.3801
110.333	10.186	0.356	0.0728	0.427	0.183	0.352	0.0681	0.199	0.0806	0.0389	0.0273	0.107	0.0727	0.105	0.0968	0.0939	0.084	0.3797
110.417	10.151	0.356	0.0728	0.426	0.183	0.351	0.068	0.199	0.0805	0.0389	0.0273	0.107	0.0727	0.105	0.0967	0.0937	0.0838	0.3792
110.5	10.116	0.355	0.0728	0.426	0.183	0.35	0.0679	0.199	0.0805	0.0389	0.0273	0.107	0.0727	0.104	0.0965	0.0936	0.0837	0.3778
110.583	10.081	0.355	0.0728	0.425	0.183	0.35	0.0678	0.198	0.0804	0.0389	0.0273	0.107	0.0727	0.104	0.0964	0.0935	0.0835	0.3774
110.667	10.046	0.355	0.0728	0.424	0.182	0.349	0.0677	0.198	0.0803	0.0389	0.0273	0.107	0.0727	0.104	0.0962	0.0933	0.0834	0.3769
110.75	10.011	0.354	0.0728	0.424	0.182	0.349	0.0676	0.198	0.0802	0.0389	0.0273	0.107	0.0727	0.104	0.0961	0.0932	0.0832	0.3765
110.833	9.976	0.354	0.0728	0.423	0.182	0.348	0.0676	0.198	0.0801	0.0389	0.0273	0.107	0.0727	0.104	0.096	0.093	0.0831	0.3761
110.917	9.942	0.353	0.0728	0.422	0.182	0.347	0.0675	0.198	0.0801	0.0389	0.0273	0.107	0.0727	0.104	0.0958	0.0929	0.083	0.3757
111	9.907	0.353	0.0728	0.422	0.181	0.347	0.0674	0.198	0.08	0.0389	0.0273	0.107	0.0727	0.104	0.0957	0.0928	0.0828	0.3753
111.083	9.873	0.352	0.0728	0.421	0.181	0.346	0.0673	0.197	0.0799	0.0389	0.0273	0.107	0.0727	0.103	0.0956	0.0926	0.0827	0.3739
111.167	9.839	0.352	0.0728	0.421	0.181	0.346	0.0673	0.197	0.0798	0.0389	0.0273	0.107	0.0727	0.103	0.0954	0.0925	0.0826	0.3735
111.25	9.805	0.352	0.0728	0.42	0.181	0.345	0.0672	0.197	0.0798	0.0389	0.0273	0.107	0.0727	0.103	0.0953	0.0924	0.0824	0.3731
111.333	9.771	0.351	0.0728	0.419	0.181	0.345	0.0671	0.197	0.0797	0.0389	0.0273	0.107	0.0727	0.103	0.0952	0.0923	0.0823	0.3728
111.417	9.738	0.351	0.0728	0.419	0.18	0.344	0.0671	0.197	0.0796	0.0389	0.0273	0.107	0.0727	0.103	0.0951	0.0921	0.0822	0.3724
111.5	9.704	0.35	0.0728	0.418	0.18	0.344	0.067	0.197	0.0796	0.0389	0.0273	0.107	0.0727	0.103	0.095	0.092	0.0821	0.3721
111.583	9.67	0.35	0.0728	0.418	0.18	0.343	0.0669	0.197	0.0795	0.0389	0.0273	0.107	0.0727	0.103	0.0948	0.0919	0.082	0.3717
111.667	9.637	0.35	0.0728	0.417	0.18	0.343	0.0669	0.196	0.0794	0.0389	0.0273	0.107	0.0727	0.103	0.0947	0.0918	0.0819	0.3714
111.75	9.604	0.349	0.0728	0.417	0.18	0.342	0.0668	0.196	0.0794	0.0389	0.0273	0.107	0.0727	0.103	0.0946	0.0917	0.0818	0.3711
111.833	9.571	0.349	0.0728	0.416	0.179	0.342	0.0667	0.196	0.0793	0.0389	0.0273	0.107	0.0727	0.102	0.0945	0.0916	0.0816	0.3697
111.917	9.538	0.349	0.0728	0.416	0.179	0.341	0.0667	0.196	0.0793	0.0389	0.0273	0.107	0.0727	0.102	0.0944	0.0915	0.0815	0.3694
112	9.505	0.348	0.0728	0.415	0.179	0.341	0.0666	0.196	0.0792	0.0389	0.0273	0.107	0.0726	0.102	0.0943	0.0914	0.0814	0.3691
112.083	9.472	0.348	0.0728	0.415	0.179	0.34	0.0665	0.196	0.0791	0.0389	0.0272	0.106	0.0724	0.102	0.0942	0.0913	0.0813	0.3688
112.167	9.44	0.347	0.0727	0.414	0.179	0.34	0.0665	0.196	0.079	0.0389	0.0272	0.106	0.0723	0.102	0.0941	0.0912	0.0812	0.3685
112.25	9.407	0.347	0.0727	0.414	0.179	0.339	0.0664	0.196	0.079	0.0388	0.0272	0.106	0.0721	0.102	0.094	0.0911	0.0811	0.3682
112.333	9.375	0.347	0.0726	0.413	0.178	0.339	0.0663	0.195	0.0789	0.0388	0.0271	0.106	0.0717	0.102	0.0939	0.091	0.081	0.3679
112.417	9.342	0.346	0.0725	0.413	0.178	0.338	0.0663	0.195	0.0788	0.0387	0.027	0.106	0.0713	0.102	0.0938	0.0908	0.0809	0.3675
112.5	9.31	0.346	0.0724	0.412	0.178	0.338	0.0662	0.195	0.0787	0.0386	0.0269	0.105	0.0709	0.102	0.0937	0.0907	0.0808	0.3672
112.583	9.278	0.346	0.0723	0.412	0.178	0.337	0.0661	0.195	0.0786	0.0385	0.0267	0.105	0.0704	0.101	0.0935	0.0906	0.0807	0.3658
112.667	9.246	0.345	0.0722	0.411	0.177	0.337	0.0661	0.195	0.0786	0.0384	0.0266	0.105	0.0698	0.101	0.0934	0.0905	0.0806	0.3655
112.75	9.214	0.345	0.0721	0.411	0.177	0.336	0.066	0.194	0.0785	0.0383	0.0264	0.104	0.0693	0.101	0.0933	0.0904	0.0805	0.3652
112.833	9.183	0.344	0.0719	0.41	0.177	0.336	0.0659	0.194	0.0784	0.0382	0.0263	0.104	0.0688	0.101	0.0932	0.0903	0.0803	0.3648
112.917	9.151	0.344	0.0718	0.41	0.177	0.335	0.0658	0.194	0.0783	0.0381	0.0261	0.103	0.0683	0.101	0.0931	0.0902	0.0802	0.3645
113	9.12	0.343	0.0716	0.409	0.177	0.335	0.0658	0.194	0.0782	0.0379	0.0259	0.102	0.0679	0.101	0.093	0.09	0.0801	0.3641
113.083	9.089	0.343	0.0714	0.409	0.176	0.334	0.0657	0.193	0.0781	0.0378	0.0258	0.102	0.0675	0.101	0.0929	0.0899	0.08	0.3638
113.167	9.057	0.343	0.0712	0.408	0.176	0.334	0.0656	0.193	0.078	0.0376	0.0257	0.101	0.0671	0.101	0.0927	0.0898	0.0799	0.3634
113.25	9.026	0.342	0.071	0.408	0.176	0.333	0.0655	0.193	0.0778	0.0374	0.0255	0.101	0.0668	0.1	0.0926	0.0897	0.0797	0.362
113.333	8.995	0.342	0.0707	0.407	0.175	0.333	0.0654	0.192	0.0777	0.0373	0.0254	0.1	0.0665	0.1	0.0925	0.0896	0.0796	0.3617
113.417	8.965	0.341	0.0705	0.406	0.175	0.332	0.0653	0.192	0.0776	0.0371	0.0253	0.1	0.0663	0.1	0.0924	0.0894	0.0795	0.3613
113.5	8.934	0.341	0.0702	0.406	0.175	0.332	0.0653	0.192	0.0775	0.037	0.0252	0.1	0.0661	0.1	0.0922	0.0893	0.0794	0.3609
113.583	8.903	0.34	0.0699	0.405	0.175	0.331	0.0652	0.191	0.0774	0.0368	0.0251	0.1	0.0659	0.1	0.0921	0.0892	0.0792	0.3605
113.667	8.873	0.339	0.0696	0.404	0.174	0.331	0.0651	0.191	0.0773	0.0367	0.025	0.1	0.0657	0.0998	0.092	0.089	0.0791	0.3599
113.75	8.842	0.339	0.0693	0.404	0.174	0.33	0.065	0.191	0.0771	0.0366	0.025	0.1	0.0655	0.0997	0.0918	0.0889	0.079	0.3594
113.833	8.812	0.338	0.069	0.403	0.174	0.33	0.0649	0.19	0.077	0.0364	0.0249	0.1	0.0654	0.0996	0.0917	0.0888	0.0788	0.3589
113.917	8.782	0.338	0.0687	0.403	0.173	0.329	0.0648	0.19	0.0769	0.0363	0.0248	0.1	0.0653	0.0994	0.0915	0.0886	0.0787	0.3582
114	8.752	0.337	0.0683	0.402	0.173	0.329	0.0647	0.19	0.0767	0.0362	0.0248	0.1	0.0651	0.0993	0.0914	0.0885	0.0785	0.3577
114.083	8.722	0.337	0.068	0.401	0.173	0.328	0.0646	0.189	0.0766	0.0361	0.0247	0.1	0.0651	0.0991	0.0913	0.0883	0.0784	0.3571
114.167	8.692	0.336	0.0677	0.401	0.172	0.327	0.0645	0.189	0.0764	0.036	0.0247	0.1	0.065	0.099	0.0911	0.0882	0.0782	0.3565
114.25	8.662	0.335	0.0673	0.4	0.172	0.327	0.0644	0.188	0.0763	0.0359	0.0246	0.1	0.0649	0.0988	0.091	0.088	0.0781	0.3559
114.333	8.633	0.335	0.067	0.399	0.172	0.326	0.0643	0.188	0.0761	0.0359	0.0246	0.1	0.0649	0.0987	0.0908	0.0879	0.0779	0.3553
114.417	8.603	0.334	0.0667	0.398	0.171	0.326	0.0642	0.187	0.076	0.0358	0.0246	0.1	0.0649	0.0985	0.0906	0.0877	0.0778	0.3546
114.5	8.574	0.334	0.0664	0.398	0.171	0.325	0.0641	0.187	0.0758	0.0357	0.0245	0.1	0.0649	0.0984	0.0905	0.0876	0.0776	0.3541
114.583	8.545	0.333	0.0661	0.397	0.171	0.325	0.0639	0.186	0.0757	0.0356	0.0245	0.1	0.0649	0.0982	0.0903	0.0874	0.0774	0.3533
114.667	8.515	0.332	0.0658	0.396	0.17	0.324	0.0638	0.186	0.0755	0.0356	0.0245	0.1	0.0649	0.098	0.0902	0.0872	0.0773	0.3527
114.75	8.486	0.332	0.0656	0.396	0.17	0.324	0.0637	0.185	0.0754	0.0355	0.0245	0.1	0.0649	0.0979	0.09	0.0871	0.0771	0.3521
114.833	8.457	0.331	0.0653	0.395	0.17	0.323	0.0636	0.185	0.0752	0.0355	0.0245	0.1	0.0649	0.0977	0.0898	0.0869	0.0769	0.3513
114.917	8.428	0.33	0.065	0.394	0.169	0.322	0.0635	0.184	0.075	0.0354	0.0245	0.1	0.0649	0.0975	0.0897	0.0867	0.0768	0.3507
115	8.4	0.33	0.0648	0.393	0.169	0.322	0.0634	0.183	0.0749	0.0353	0.0245	0.1	0.0649	0.0974	0.0895	0.0866	0.0766	0.3501

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
115.083	8.371	0.329	0.0646	0.392	0.168	0.321	0.0632	0.183	0.0747	0.0353	0.0245	0.1	0.0649	0.0972	0.0893	0.0864	0.0764	0.3493
115.167	8.343	0.328	0.0643	0.392	0.168	0.321	0.0631	0.182	0.0745	0.0353	0.0245	0.1	0.0649	0.097	0.0891	0.0862	0.0762	0.3485
115.25	8.314	0.327	0.0641	0.391	0.167	0.32	0.063	0.182	0.0743	0.0352	0.0245	0.1	0.0649	0.0968	0.089	0.086	0.0761	0.3479
115.333	8.286	0.327	0.0639	0.39	0.167	0.32	0.0629	0.181	0.0741	0.0352	0.0245	0.1	0.0649	0.0967	0.0888	0.0858	0.0759	0.3472
115.417	8.258	0.326	0.0637	0.389	0.167	0.319	0.0628	0.181	0.074	0.0351	0.0245	0.1	0.0649	0.0965	0.0886	0.0857	0.0757	0.3465
115.5	8.23	0.325	0.0635	0.388	0.166	0.318	0.0626	0.18	0.0738	0.0351	0.0245	0.1	0.0649	0.0963	0.0884	0.0855	0.0755	0.3457
115.583	8.202	0.324	0.0633	0.387	0.166	0.318	0.0625	0.179	0.0736	0.0351	0.0245	0.1	0.0649	0.0961	0.0882	0.0853	0.0753	0.3449
115.667	8.174	0.324	0.0631	0.387	0.165	0.317	0.0624	0.179	0.0734	0.035	0.0245	0.1	0.0649	0.0959	0.088	0.0851	0.0751	0.3441
115.75	8.146	0.323	0.0629	0.386	0.165	0.317	0.0622	0.178	0.0732	0.035	0.0245	0.1	0.0649	0.0957	0.0878	0.0849	0.0749	0.3433
115.833	8.118	0.322	0.0628	0.385	0.164	0.316	0.0621	0.178	0.073	0.035	0.0245	0.1	0.0649	0.0955	0.0876	0.0847	0.0747	0.3425
115.917	8.091	0.321	0.0626	0.384	0.164	0.316	0.062	0.177	0.0728	0.035	0.0245	0.1	0.0649	0.0953	0.0874	0.0845	0.0746	0.3418
116	8.063	0.321	0.0625	0.383	0.163	0.315	0.0618	0.177	0.0726	0.035	0.0245	0.1	0.0649	0.0951	0.0872	0.0843	0.0744	0.341
116.083	8.036	0.32	0.0623	0.382	0.163	0.314	0.0617	0.176	0.0724	0.035	0.0245	0.1	0.0649	0.0949	0.087	0.0841	0.0741	0.3401
116.167	8.009	0.319	0.0622	0.381	0.163	0.314	0.0615	0.176	0.0722	0.0349	0.0245	0.1	0.0649	0.0947	0.0868	0.0839	0.0739	0.3393
116.25	7.981	0.318	0.062	0.38	0.162	0.313	0.0614	0.175	0.072	0.0349	0.0245	0.1	0.0649	0.0945	0.0866	0.0837	0.0737	0.3385
116.333	7.954	0.317	0.0619	0.379	0.162	0.313	0.0613	0.175	0.0718	0.0349	0.0245	0.1	0.0649	0.0943	0.0864	0.0835	0.0735	0.3377
116.417	7.927	0.316	0.0618	0.378	0.161	0.312	0.0611	0.174	0.0717	0.0349	0.0245	0.1	0.0649	0.0941	0.0862	0.0833	0.0733	0.3369
116.5	7.9	0.315	0.0617	0.377	0.161	0.311	0.061	0.174	0.0715	0.0349	0.0245	0.1	0.0649	0.0939	0.086	0.0831	0.0731	0.3361
116.583	7.874	0.315	0.0615	0.376	0.16	0.311	0.0608	0.173	0.0713	0.0349	0.0245	0.1	0.0649	0.0937	0.0858	0.0829	0.0729	0.3353
116.667	7.847	0.314	0.0614	0.375	0.16	0.31	0.0607	0.173	0.0712	0.0349	0.0245	0.1	0.0649	0.0935	0.0856	0.0826	0.0727	0.3344
116.75	7.821	0.313	0.0613	0.374	0.159	0.309	0.0605	0.173	0.071	0.0349	0.0245	0.1	0.0649	0.0932	0.0853	0.0824	0.0725	0.3334
116.833	7.794	0.312	0.0612	0.373	0.159	0.309	0.0604	0.172	0.0708	0.0349	0.0245	0.1	0.0649	0.093	0.0851	0.0822	0.0722	0.3325
116.917	7.768	0.311	0.0611	0.372	0.158	0.308	0.0602	0.172	0.0707	0.0349	0.0245	0.1	0.0649	0.0928	0.0849	0.082	0.072	0.3317
117	7.742	0.31	0.061	0.371	0.158	0.308	0.0601	0.171	0.0705	0.0349	0.0245	0.1	0.0649	0.0926	0.0847	0.0817	0.0718	0.3308
117.083	7.715	0.309	0.0609	0.37	0.157	0.307	0.0599	0.171	0.0704	0.0349	0.0245	0.1	0.0649	0.0924	0.0845	0.0815	0.0716	0.33
117.167	7.689	0.309	0.0608	0.369	0.157	0.306	0.0598	0.171	0.0702	0.0349	0.0245	0.1	0.0649	0.0921	0.0842	0.0813	0.0713	0.3289
117.25	7.663	0.308	0.0607	0.368	0.157	0.306	0.0596	0.17	0.0701	0.0349	0.0245	0.1	0.0649	0.0919	0.084	0.0811	0.0711	0.3281
117.333	7.638	0.307	0.0606	0.367	0.156	0.305	0.0595	0.17	0.0699	0.0349	0.0245	0.1	0.0649	0.0917	0.0838	0.0809	0.0709	0.3273
117.417	7.612	0.306	0.0605	0.366	0.156	0.304	0.0593	0.17	0.0698	0.0349	0.0245	0.1	0.0649	0.0915	0.0836	0.0806	0.0707	0.3264
117.5	7.586	0.305	0.0605	0.365	0.155	0.304	0.0592	0.169	0.0696	0.0349	0.0245	0.1	0.0649	0.0913	0.0834	0.0804	0.0705	0.3256
117.583	7.561	0.305	0.0604	0.364	0.155	0.303	0.0591	0.169	0.0695	0.0349	0.0245	0.1	0.0649	0.0911	0.0832	0.0802	0.0703	0.3248
117.667	7.535	0.304	0.0603	0.363	0.155	0.303	0.0589	0.169	0.0693	0.0349	0.0245	0.1	0.0649	0.0908	0.0829	0.08	0.07	0.3237
117.75	7.51	0.303	0.0602	0.362	0.154	0.302	0.0588	0.168	0.0692	0.0349	0.0245	0.1	0.0649	0.0906	0.0827	0.0798	0.0698	0.3229
117.833	7.484	0.303	0.0602	0.361	0.154	0.301	0.0587	0.168	0.0691	0.0349	0.0245	0.1	0.0649	0.0904	0.0825	0.0796	0.0696	0.3221
117.917	7.459	0.302	0.0601	0.36	0.154	0.301	0.0586	0.168	0.0689	0.0349	0.0245	0.1	0.0649	0.0902	0.0823	0.0794	0.0694	0.3213
118	7.434	0.301	0.0601	0.36	0.153	0.3	0.0584	0.167	0.0688	0.0349	0.0245	0.1	0.0648	0.09	0.0821	0.0792	0.0692	0.3205
118.083	7.409	0.3	0.06	0.359	0.153	0.299	0.0583	0.167	0.0687	0.0349	0.0244	0.1	0.0647	0.0898	0.0819	0.079	0.069	0.3197
118.167	7.384	0.3	0.0599	0.358	0.152	0.299	0.0582	0.167	0.0685	0.0349	0.0244	0.1	0.0646	0.0896	0.0817	0.0788	0.0688	0.3189
118.25	7.359	0.299	0.0598	0.357	0.152	0.298	0.0581	0.167	0.0684	0.0349	0.0244	0.1	0.0644	0.0894	0.0815	0.0786	0.0686	0.3181
118.333	7.335	0.298	0.0597	0.356	0.152	0.297	0.0579	0.166	0.0683	0.0348	0.0243	0.1	0.0641	0.0892	0.0813	0.0784	0.0684	0.3173
118.417	7.31	0.298	0.0596	0.355	0.151	0.297	0.0578	0.166	0.0681	0.0347	0.0242	0.1	0.0637	0.089	0.0811	0.0782	0.0682	0.3165
118.5	7.285	0.297	0.0595	0.354	0.151	0.296	0.0577	0.166	0.068	0.0347	0.0241	0.1	0.0634	0.0888	0.0809	0.078	0.068	0.3157
118.583	7.261	0.296	0.0594	0.353	0.151	0.295	0.0576	0.165	0.0679	0.0346	0.024	0.1	0.0628	0.0886	0.0807	0.0778	0.0678	0.3149
118.667	7.237	0.295	0.0593	0.352	0.15	0.294	0.0574	0.165	0.0677	0.0345	0.0238	0.1	0.0623	0.0884	0.0805	0.0776	0.0676	0.3141
118.75	7.212	0.295	0.0591	0.351	0.15	0.294	0.0573	0.164	0.0676	0.0344	0.0237	0.1	0.0618	0.0882	0.0803	0.0774	0.0674	0.3133
118.833	7.188	0.294	0.0589	0.35	0.15	0.293	0.0572	0.164	0.0674	0.0343	0.0235	0.1	0.0613	0.088	0.0801	0.0772	0.0672	0.3125
118.917	7.164	0.293	0.0588	0.349	0.149	0.292	0.057	0.164	0.0673	0.0341	0.0234	0.1	0.0607	0.0878	0.0799	0.077	0.067	0.3117
119	7.14	0.293	0.0586	0.348	0.149	0.291	0.0569	0.163	0.0671	0.034	0.0232	0.1	0.0602	0.0876	0.0797	0.0768	0.0668	0.3109
119.083	7.116	0.292	0.0584	0.348	0.148	0.291	0.0568	0.163	0.067	0.0339	0.023	0.1	0.0599	0.0874	0.0795	0.0766	0.0666	0.3101
119.167	7.093	0.291	0.0582	0.347	0.148	0.29	0.0567	0.162	0.0668	0.0337	0.0229	0.1	0.0595	0.0872	0.0793	0.0764	0.0664	0.3093
119.25	7.069	0.29	0.058	0.346	0.148	0.289	0.0565	0.162	0.0667	0.0335	0.0227	0.1	0.0591	0.087	0.0791	0.0762	0.0662	0.3085
119.333	7.045	0.29	0.0577	0.345	0.147	0.288	0.0564	0.162	0.0665	0.0334	0.0226	0.1	0.0588	0.0868	0.0789	0.076	0.066	0.3077
119.417	7.022	0.289	0.0575	0.344	0.147	0.288	0.0563	0.161	0.0664	0.0332	0.0225	0.1	0.0586	0.0866	0.0787	0.0758	0.0658	0.3069
119.5	6.998	0.288	0.0573	0.343	0.147	0.287	0.0561	0.161	0.0662	0.0331	0.0224	0.1	0.0583	0.0864	0.0785	0.0756	0.0656	0.3061
119.583	6.975	0.288	0.057	0.342	0.146	0.286	0.056	0.16	0.0661	0.0329	0.0223	0.1	0.0581	0.0862	0.0783	0.0754	0.0654	0.3053
119.667	6.952	0.287	0.0567	0.341	0.146	0.285	0.0559	0.16	0.0659	0.0328	0.0222	0.1	0.0579	0.086	0.0781	0.0752	0.0652	0.3045
119.75	6.929	0.286	0.0564	0.34	0.145	0.285	0.0558	0.159	0.0657	0.0326	0.0222	0.1	0.0577	0.0858	0.0779	0.075	0.065	0.3037
119.833	6.905	0.285	0.0561	0.339	0.145	0.284	0.0556	0.159	0.0656	0.0325	0.0221	0.1	0.0576	0.0856	0.0777	0.0748	0.0648	0.3029
119.917	6.882	0.285	0.0557	0.338	0.144	0.283	0.0555	0.158	0.0654	0.0324	0.022	0.1	0.0575	0.0854	0.0775	0.0746	0.0646	0.3021
120	6.859	0.284	0.0554	0.337	0.144	0.282	0.0554	0.157	0.0652	0.0323	0.022	0.1	0.0573	0.0852	0.0773	0.0743	0.0644	0.3012
120.083	6.837	0.283	0.0551	0.336	0.144	0.282	0.0552	0.157	0.065	0.0322	0.0219	0.1	0.0573	0.085	0.0771	0.0741	0.0642	0.3004
120.167	6.814	0.282	0.0547	0.335	0.143	0.281	0.0551	0.156	0.0649	0.0321	0.0219	0.1	0.0572	0.0848	0.0769	0.0739	0.0639	0.2995
120.25	6.791	0.281	0.0544	0.334	0.143	0.28	0.055	0.156	0.0647	0.032	0.0218	0.1	0.0571	0.0846	0.0767	0.0737	0.0637	0.2987
120.333	6.769	0.281	0.0541	0.333	0.142	0.279	0.0548	0.155	0.0645	0.0319	0.0218	0.1	0.0571	0.0843	0.0764	0.0735	0.0635	0.2977
120.417	6.746	0.28	0.0538	0.332	0.142	0.279	0.0547	0.155	0.0643	0.0318	0.0218	0.1	0.0571	0.0841	0.0762	0.0733	0.0633	0.2969
120.5	6.724	0.279	0.0535	0.331	0.141	0.278	0.0545	0.154	0.0641	0.0317	0.0217	0.1	0.057	0.0839	0.076	0.0731	0.0631	0.2961
120.583	6.702	0.278	0.0532	0.33	0.141	0.277	0.0544	0.153	0.0639	0.0317	0.0217	0.1	0.057	0.0837	0.0758	0.0729	0.0629	0.2953

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
120.667	6.679	0.277	0.0529	0.329	0.141	0.277	0.0543	0.153	0.0637	0.0316	0.0217	0.1	0.057	0.0835	0.0756	0.0727	0.0627	0.2945
120.75	6.657	0.277	0.0526	0.328	0.14	0.276	0.0541	0.152	0.0635	0.0315	0.0217	0.1	0.057	0.0833	0.0754	0.0724	0.0625	0.2936
120.833	6.635	0.276	0.0523	0.327	0.14	0.275	0.054	0.151	0.0633	0.0315	0.0216	0.1	0.057	0.0831	0.0752	0.0722	0.0622	0.2927
120.917	6.613	0.275	0.0521	0.326	0.139	0.274	0.0538	0.151	0.0631	0.0314	0.0216	0.1	0.057	0.0829	0.075	0.072	0.062	0.2919
121	6.591	0.274	0.0518	0.325	0.139	0.274	0.0537	0.15	0.0629	0.0314	0.0216	0.1	0.057	0.0826	0.0747	0.0718	0.0618	0.2909
121.083	6.569	0.273	0.0515	0.324	0.138	0.273	0.0536	0.149	0.0627	0.0313	0.0216	0.1	0.0568	0.0824	0.0745	0.0716	0.0616	0.2901
121.167	6.547	0.272	0.0512	0.323	0.138	0.272	0.0534	0.148	0.0625	0.0312	0.0215	0.1	0.0566	0.0822	0.0743	0.0714	0.0614	0.2893
121.25	6.526	0.272	0.051	0.322	0.137	0.271	0.0533	0.148	0.0622	0.0311	0.0215	0.1	0.0564	0.082	0.0741	0.0711	0.0611	0.2883
121.333	6.504	0.271	0.0506	0.321	0.137	0.27	0.0531	0.147	0.062	0.031	0.0213	0.1	0.0557	0.0817	0.0738	0.0709	0.0609	0.2873
121.417	6.482	0.27	0.0503	0.32	0.136	0.27	0.0529	0.146	0.0617	0.0308	0.0211	0.1	0.055	0.0815	0.0736	0.0706	0.0606	0.2863
121.5	6.46	0.269	0.0499	0.319	0.135	0.269	0.0528	0.145	0.0614	0.0307	0.021	0.1	0.0544	0.0812	0.0733	0.0704	0.0604	0.2853
121.583	6.438	0.268	0.0495	0.318	0.135	0.268	0.0526	0.144	0.0612	0.0305	0.0207	0.1	0.0533	0.081	0.0731	0.0701	0.0601	0.2843
121.667	6.417	0.266	0.0491	0.316	0.134	0.267	0.0524	0.143	0.0609	0.0303	0.0204	0.1	0.0522	0.0807	0.0728	0.0698	0.0599	0.2832
121.75	6.395	0.265	0.0487	0.315	0.133	0.266	0.0522	0.143	0.0606	0.03	0.0202	0.1	0.0511	0.0804	0.0725	0.0696	0.0596	0.2821
121.833	6.373	0.264	0.0483	0.314	0.133	0.265	0.052	0.142	0.0602	0.0298	0.0198	0.1	0.0501	0.0801	0.0722	0.0693	0.0593	0.2809
121.917	6.351	0.263	0.0478	0.313	0.132	0.264	0.0518	0.141	0.0599	0.0295	0.0195	0.1	0.049	0.0798	0.0719	0.069	0.059	0.2797
122	6.33	0.262	0.0473	0.311	0.131	0.263	0.0516	0.14	0.0596	0.0292	0.0191	0.1	0.048	0.0796	0.0716	0.0687	0.0587	0.2786
122.083	6.308	0.26	0.0468	0.31	0.131	0.263	0.0514	0.139	0.0593	0.0289	0.0188	0.1	0.0472	0.0792	0.0713	0.0684	0.0584	0.2773
122.167	6.286	0.259	0.0463	0.308	0.13	0.262	0.0511	0.138	0.0589	0.0286	0.0185	0.1	0.0464	0.0789	0.071	0.0681	0.0581	0.2761
122.25	6.265	0.258	0.0457	0.307	0.129	0.261	0.0509	0.137	0.0586	0.0283	0.0183	0.1	0.0457	0.0786	0.0707	0.0678	0.0578	0.2749
122.333	6.243	0.256	0.0451	0.305	0.128	0.26	0.0507	0.136	0.0582	0.0279	0.018	0.1	0.0451	0.0783	0.0704	0.0674	0.0574	0.2735
122.417	6.222	0.255	0.0445	0.304	0.127	0.259	0.0504	0.135	0.0579	0.0276	0.0178	0.1	0.0446	0.0779	0.07	0.0671	0.0571	0.2721
122.5	6.2	0.253	0.0439	0.302	0.127	0.258	0.0502	0.134	0.0575	0.0273	0.0176	0.1	0.044	0.0776	0.0697	0.0667	0.0567	0.2707
122.583	6.179	0.252	0.0432	0.301	0.126	0.256	0.0499	0.133	0.0571	0.027	0.0174	0.1	0.0436	0.0772	0.0693	0.0664	0.0564	0.2693
122.667	6.157	0.25	0.0426	0.299	0.125	0.255	0.0496	0.131	0.0568	0.0267	0.0172	0.1	0.0432	0.0769	0.069	0.066	0.056	0.2679
122.75	6.136	0.249	0.0419	0.297	0.124	0.254	0.0494	0.13	0.0564	0.0264	0.0171	0.1	0.0428	0.0765	0.0686	0.0657	0.0557	0.2665
122.833	6.114	0.247	0.0411	0.295	0.123	0.253	0.0491	0.129	0.056	0.0262	0.0169	0.1	0.0426	0.0761	0.0682	0.0653	0.0553	0.2649
122.917	6.093	0.246	0.0403	0.294	0.122	0.252	0.0488	0.128	0.0556	0.0259	0.0168	0.1	0.0423	0.0757	0.0678	0.0649	0.0549	0.2633
123	6.072	0.244	0.0396	0.292	0.121	0.251	0.0486	0.127	0.0552	0.0257	0.0167	0.1	0.042	0.0754	0.0674	0.0645	0.0545	0.2618
123.083	6.05	0.242	0.0388	0.29	0.12	0.25	0.0483	0.126	0.0548	0.0255	0.0166	0.1	0.0418	0.0749	0.067	0.0641	0.0541	0.2601
123.167	6.029	0.241	0.038	0.288	0.119	0.249	0.048	0.124	0.0544	0.0253	0.0165	0.1	0.0417	0.0745	0.0666	0.0637	0.0537	0.2585
123.25	6.007	0.239	0.0372	0.286	0.118	0.248	0.0477	0.123	0.054	0.0251	0.0164	0.1	0.0415	0.0741	0.0662	0.0633	0.0532	0.2568
123.333	5.986	0.237	0.0365	0.284	0.117	0.246	0.0474	0.122	0.0536	0.0249	0.0163	0.1	0.0414	0.0737	0.0658	0.0628	0.0528	0.2551
123.417	5.965	0.236	0.0358	0.282	0.116	0.245	0.0471	0.121	0.0532	0.0247	0.0162	0.1	0.0414	0.0733	0.0653	0.0624	0.0524	0.2534
123.5	5.944	0.234	0.0351	0.28	0.115	0.244	0.0468	0.119	0.0528	0.0246	0.0161	0.1	0.0413	0.0728	0.0649	0.062	0.052	0.2517
123.583	5.922	0.232	0.0344	0.278	0.114	0.243	0.0465	0.118	0.0524	0.0244	0.0161	0.1	0.0413	0.0724	0.0645	0.0615	0.0515	0.2499
123.667	5.901	0.231	0.0338	0.276	0.114	0.241	0.0462	0.117	0.052	0.0243	0.016	0.1	0.0413	0.072	0.0641	0.0611	0.0511	0.2483
123.75	5.88	0.229	0.0331	0.274	0.113	0.24	0.0459	0.115	0.0515	0.0242	0.016	0.1	0.0413	0.0715	0.0636	0.0607	0.0507	0.2465
123.833	5.859	0.227	0.0325	0.272	0.111	0.239	0.0456	0.114	0.0511	0.0241	0.016	0.1	0.0413	0.0711	0.0632	0.0602	0.0502	0.2447
123.917	5.838	0.225	0.032	0.27	0.11	0.238	0.0453	0.112	0.0507	0.0239	0.016	0.1	0.0413	0.0706	0.0627	0.0598	0.0498	0.2429
124	5.817	0.223	0.0314	0.268	0.109	0.236	0.045	0.111	0.0502	0.0238	0.0159	0.1	0.0413	0.0702	0.0623	0.0593	0.0493	0.2411
124.083	5.795	0.222	0.0308	0.266	0.108	0.235	0.0447	0.11	0.0498	0.0237	0.0159	0.1	0.0413	0.0697	0.0618	0.0589	0.0489	0.2393
124.167	5.774	0.22	0.0303	0.264	0.107	0.234	0.0444	0.108	0.0493	0.0236	0.0159	0.1	0.0413	0.0693	0.0614	0.0584	0.0484	0.2375
124.25	5.753	0.218	0.0298	0.262	0.106	0.232	0.0441	0.107	0.0489	0.0235	0.0159	0.1	0.0413	0.0688	0.0609	0.058	0.048	0.2357
124.333	5.732	0.216	0.0293	0.26	0.105	0.231	0.0438	0.105	0.0484	0.0235	0.0159	0.1	0.0413	0.0684	0.0605	0.0575	0.0475	0.2339
124.417	5.711	0.214	0.0289	0.258	0.104	0.229	0.0434	0.104	0.0479	0.0234	0.0159	0.1	0.0413	0.0679	0.06	0.057	0.047	0.2319
124.5	5.69	0.212	0.0284	0.256	0.103	0.228	0.0431	0.102	0.0475	0.0233	0.0159	0.1	0.0413	0.0674	0.0595	0.0566	0.0466	0.2301
124.583	5.669	0.21	0.028	0.254	0.102	0.227	0.0428	0.101	0.047	0.0233	0.0159	0.1	0.0413	0.067	0.059	0.0561	0.0461	0.2282
124.667	5.648	0.208	0.0276	0.251	0.101	0.225	0.0425	0.0997	0.0465	0.0232	0.0159	0.1	0.0413	0.0665	0.0586	0.0556	0.0456	0.2263
124.75	5.627	0.207	0.0272	0.249	0.0997	0.224	0.0421	0.0983	0.046	0.0231	0.0159	0.1	0.0413	0.066	0.0581	0.0551	0.0451	0.2243
124.833	5.606	0.205	0.0268	0.247	0.0986	0.222	0.0418	0.0971	0.0455	0.0231	0.0159	0.1	0.0413	0.0655	0.0576	0.0547	0.0446	0.2224
124.917	5.585	0.203	0.0265	0.245	0.0975	0.221	0.0415	0.0958	0.045	0.023	0.0159	0.1	0.0413	0.065	0.0571	0.0542	0.0442	0.2205
125	5.565	0.201	0.0261	0.243	0.0963	0.219	0.0411	0.0945	0.0446	0.023	0.0159	0.1	0.0413	0.0646	0.0566	0.0537	0.0437	0.2186
125.083	5.544	0.199	0.0259	0.24	0.0952	0.218	0.0408	0.0933	0.0441	0.023	0.0159	0.1	0.0413	0.0641	0.0561	0.0532	0.0432	0.2166
125.167	5.523	0.197	0.0256	0.238	0.094	0.216	0.0404	0.0921	0.0436	0.023	0.0159	0.1	0.0413	0.0636	0.0556	0.0527	0.0427	0.2146
125.25	5.502	0.195	0.0253	0.236	0.0929	0.215	0.0401	0.0909	0.0431	0.0229	0.0159	0.1	0.0413	0.0631	0.0551	0.0522	0.0422	0.2126
125.333	5.481	0.193	0.025	0.233	0.0917	0.213	0.0397	0.0898	0.0427	0.0229	0.0159	0.1	0.0413	0.0626	0.0546	0.0517	0.0417	0.2106
125.417	5.46	0.19	0.0248	0.231	0.0905	0.212	0.0394	0.0886	0.0422	0.0229	0.0159	0.1	0.0413	0.0621	0.0541	0.0512	0.0412	0.2086
125.5	5.44	0.188	0.0245	0.229	0.0893	0.21	0.039	0.0875	0.0418	0.0229	0.0159	0.1	0.0413	0.0616	0.0536	0.0507	0.0406	0.2065
125.583	5.419	0.186	0.0243	0.226	0.0882	0.209	0.0387	0.0864	0.0414	0.0229	0.0159	0.1	0.0413	0.061	0.0531	0.0502	0.0401	0.2044
125.667	5.398	0.184	0.024	0.224	0.087	0.207	0.0383	0.0853	0.041	0.0229	0.0159	0.1	0.0413	0.0605	0.0526	0.0496	0.0396	0.2023
125.75	5.377	0.182	0.0238	0.222	0.0859	0.205	0.038	0.0843	0.0405	0.0229	0.0159	0.1	0.0413	0.06	0.0521	0.0491	0.0391	0.2003
125.833	5.357	0.18	0.0236	0.219	0.0848	0.204	0.0376	0.0833	0.0401	0.0229	0.0159	0.1	0.0413	0.0595	0.0515	0.0486	0.0386	0.1982
125.917	5.336	0.178	0.0233	0.217	0.0837	0.202	0.0372	0.0823	0.0397	0.0229	0.0159	0.1	0.0413	0.0589	0.051	0.0481	0.038	0.196
126	5.315	0.176	0.0231	0.214	0.0827	0.201	0.0369	0.0813	0.0393	0.0229	0.0159	0.1	0.0413	0.0584	0.0505	0.0475	0.0375	0.1939
126.083	5.295	0.174	0.0229	0.212	0.0816	0.199	0.0365	0.0804	0.0389	0.0229	0.0159	0.1	0.0413	0.0579	0.05	0.047	0.037	0.1919
126.167	5.274	0.172	0.0227	0.209	0.0806	0.198	0.0362	0.0794	0.0386	0.0229	0.0159	0.1	0.0413	0.0574	0.0494	0.0465	0.0364	0.1897

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
126.25	5.254	0.17	0.0225	0.207	0.0795	0.196	0.0358	0.0785	0.0382	0.0229	0.0159	0.1	0.0413	0.0568	0.0489	0.0459	0.0359	0.1875
126.333	5.233	0.168	0.0224	0.205	0.0786	0.194	0.0355	0.0776	0.0378	0.0229	0.0159	0.1	0.0413	0.0563	0.0484	0.0454	0.0354	0.1855
126.417	5.213	0.166	0.0222	0.202	0.0776	0.193	0.0352	0.0768	0.0375	0.0229	0.0159	0.1	0.0413	0.0558	0.0479	0.0449	0.0349	0.1835
126.5	5.192	0.164	0.022	0.2	0.0766	0.191	0.0348	0.0759	0.0371	0.0229	0.0159	0.1	0.0413	0.0553	0.0473	0.0444	0.0343	0.1813
126.583	5.172	0.163	0.0219	0.198	0.0757	0.19	0.0345	0.0751	0.0368	0.0229	0.0159	0.1	0.0413	0.0548	0.0468	0.0439	0.0338	0.1793
126.667	5.151	0.161	0.0217	0.195	0.0747	0.188	0.0342	0.0744	0.0364	0.0229	0.0159	0.1	0.0413	0.0543	0.0464	0.0434	0.0334	0.1775
126.75	5.131	0.159	0.0216	0.193	0.0738	0.186	0.0339	0.0736	0.0361	0.0229	0.0159	0.1	0.0413	0.0538	0.0459	0.0429	0.0329	0.1755
126.833	5.11	0.157	0.0214	0.191	0.0729	0.185	0.0336	0.0728	0.0357	0.0229	0.0159	0.1	0.0413	0.0533	0.0454	0.0424	0.0324	0.1735
126.917	5.09	0.156	0.0213	0.189	0.072	0.183	0.0333	0.0721	0.0354	0.0229	0.0159	0.1	0.0413	0.0528	0.0449	0.0419	0.0319	0.1715
127	5.069	0.154	0.0212	0.186	0.0711	0.182	0.033	0.0714	0.0351	0.0229	0.0159	0.1	0.0413	0.0524	0.0444	0.0415	0.0314	0.1697
127.083	5.049	0.152	0.0211	0.184	0.0703	0.18	0.0327	0.0708	0.0348	0.0229	0.0159	0.1	0.0413	0.0519	0.044	0.041	0.0309	0.1678
127.167	5.029	0.151	0.021	0.182	0.0694	0.178	0.0324	0.0701	0.0344	0.0229	0.0159	0.1	0.0413	0.0514	0.0435	0.0405	0.0305	0.1659
127.25	5.008	0.149	0.0209	0.18	0.0686	0.177	0.0321	0.0695	0.0341	0.0229	0.0159	0.1	0.0413	0.051	0.043	0.0401	0.03	0.1641
127.333	4.988	0.147	0.0208	0.178	0.0678	0.175	0.0318	0.0689	0.0338	0.0229	0.0159	0.1	0.0413	0.0505	0.0426	0.0396	0.0296	0.1623
127.417	4.968	0.146	0.0207	0.176	0.067	0.173	0.0316	0.0683	0.0335	0.0229	0.0159	0.1	0.0413	0.0501	0.0422	0.0392	0.0291	0.1606
127.5	4.947	0.144	0.0206	0.174	0.0662	0.172	0.0313	0.0677	0.0332	0.0229	0.0159	0.1	0.0413	0.0496	0.0417	0.0388	0.0287	0.1588
127.583	4.927	0.143	0.0206	0.172	0.0654	0.17	0.031	0.0671	0.033	0.0229	0.0159	0.1	0.0413	0.0492	0.0413	0.0383	0.0283	0.1571
127.667	4.907	0.141	0.0205	0.17	0.0646	0.168	0.0308	0.0666	0.0327	0.0229	0.0159	0.1	0.0413	0.0488	0.0409	0.0379	0.0278	0.1554
127.75	4.887	0.14	0.0205	0.168	0.0639	0.167	0.0305	0.066	0.0324	0.0229	0.0159	0.1	0.0413	0.0484	0.0404	0.0375	0.0274	0.1537
127.833	4.866	0.138	0.0204	0.166	0.0632	0.165	0.0302	0.0655	0.0321	0.0229	0.0159	0.1	0.0413	0.048	0.04	0.0371	0.027	0.1521
127.917	4.846	0.137	0.0204	0.164	0.0624	0.163	0.03	0.065	0.0319	0.0229	0.0159	0.1	0.0413	0.0476	0.0396	0.0367	0.0266	0.1505
128	4.826	0.136	0.0204	0.162	0.0617	0.162	0.0297	0.0645	0.0316	0.0229	0.0159	0.1	0.0413	0.0472	0.0392	0.0363	0.0262	0.1489
128.083	4.806	0.134	0.0204	0.161	0.061	0.16	0.0295	0.064	0.0314	0.0229	0.0159	0.1	0.0413	0.0468	0.0388	0.0359	0.0258	0.1473
128.167	4.786	0.133	0.0203	0.159	0.0603	0.158	0.0293	0.0635	0.0311	0.0229	0.0159	0.1	0.0413	0.0464	0.0385	0.0355	0.0254	0.1458
128.25	4.766	0.132	0.0203	0.157	0.0597	0.157	0.029	0.063	0.0309	0.0229	0.0159	0.1	0.0413	0.046	0.0381	0.0351	0.025	0.1442
128.333	4.746	0.13	0.0203	0.155	0.059	0.155	0.0288	0.0626	0.0307	0.0229	0.0159	0.1	0.0413	0.0456	0.0377	0.0347	0.0247	0.1427
128.417	4.725	0.129	0.0203	0.154	0.0584	0.154	0.0286	0.0622	0.0304	0.0229	0.0159	0.1	0.0413	0.0453	0.0373	0.0344	0.0243	0.1413
128.5	4.705	0.128	0.0203	0.152	0.0577	0.152	0.0283	0.0617	0.0302	0.0229	0.0159	0.1	0.0413	0.0449	0.037	0.034	0.0239	0.1398
128.583	4.685	0.126	0.0203	0.15	0.0571	0.15	0.0281	0.0613	0.03	0.0229	0.0159	0.1	0.0413	0.0446	0.0366	0.0337	0.0236	0.1385
128.667	4.665	0.125	0.0203	0.149	0.0565	0.149	0.0279	0.0609	0.0298	0.0229	0.0159	0.1	0.0413	0.0442	0.0363	0.0333	0.0232	0.137
128.75	4.645	0.124	0.0203	0.147	0.0558	0.147	0.0277	0.0605	0.0296	0.0229	0.0159	0.1	0.0413	0.0439	0.0359	0.033	0.0229	0.1357
128.833	4.625	0.123	0.0203	0.146	0.0553	0.146	0.0275	0.0602	0.0294	0.0229	0.0159	0.1	0.0413	0.0435	0.0356	0.0326	0.0225	0.1342
128.917	4.605	0.122	0.0203	0.144	0.0547	0.144	0.0273	0.0598	0.0292	0.0229	0.0159	0.1	0.0413	0.0432	0.0352	0.0323	0.0222	0.1329
129	4.585	0.121	0.0203	0.142	0.0541	0.143	0.0271	0.0594	0.029	0.0229	0.0159	0.1	0.0413	0.0428	0.0349	0.0319	0.0219	0.1315
129.083	4.565	0.119	0.0203	0.141	0.0536	0.141	0.0269	0.0591	0.0288	0.0229	0.0159	0.1	0.0413	0.0425	0.0346	0.0316	0.0215	0.1302
129.167	4.546	0.118	0.0203	0.139	0.053	0.14	0.0267	0.0588	0.0286	0.0229	0.0159	0.1	0.0413	0.0422	0.0343	0.0313	0.0212	0.129
129.25	4.526	0.117	0.0203	0.138	0.0525	0.139	0.0265	0.0585	0.0285	0.0229	0.0159	0.1	0.0413	0.0419	0.0339	0.031	0.0209	0.1277
129.333	4.506	0.116	0.0203	0.137	0.0519	0.137	0.0263	0.0582	0.0283	0.0229	0.0159	0.1	0.0413	0.0416	0.0336	0.0307	0.0206	0.1265
129.417	4.486	0.115	0.0203	0.135	0.0514	0.136	0.0261	0.0579	0.0281	0.0229	0.0159	0.1	0.0413	0.0413	0.0333	0.0304	0.0203	0.1253
129.5	4.466	0.114	0.0203	0.134	0.0509	0.134	0.0259	0.0576	0.0279	0.0229	0.0159	0.1	0.0413	0.041	0.033	0.0301	0.02	0.1241
129.583	4.446	0.113	0.0203	0.132	0.0504	0.133	0.0258	0.0573	0.0278	0.0229	0.0159	0.1	0.0413	0.0407	0.0327	0.0298	0.02	0.1232
129.667	4.426	0.112	0.0203	0.131	0.05	0.132	0.0256	0.057	0.0276	0.0229	0.0159	0.1	0.0413	0.0404	0.0324	0.0295	0.02	0.1223
129.75	4.406	0.111	0.0203	0.13	0.0495	0.13	0.0254	0.0568	0.0275	0.0229	0.0159	0.1	0.0413	0.0401	0.0321	0.0292	0.02	0.1214
129.833	4.387	0.11	0.0203	0.128	0.049	0.129	0.0253	0.0565	0.0273	0.0229	0.0159	0.1	0.0413	0.0398	0.0319	0.0289	0.02	0.1206
129.917	4.367	0.109	0.0203	0.127	0.0486	0.128	0.0251	0.0563	0.0271	0.0229	0.0159	0.1	0.0413	0.0395	0.0316	0.0286	0.02	0.1197
130	4.347	0.108	0.0203	0.126	0.0481	0.127	0.0249	0.056	0.027	0.0229	0.0159	0.1	0.0413	0.0393	0.0313	0.0284	0.02	0.119
130.083	4.327	0.108	0.0203	0.125	0.0477	0.125	0.0248	0.0558	0.0268	0.0229	0.0159	0.1	0.0413	0.039	0.0311	0.0281	0.02	0.1182
130.167	4.308	0.107	0.0203	0.123	0.0472	0.124	0.0246	0.0556	0.0267	0.0229	0.0159	0.1	0.0413	0.0387	0.0308	0.0278	0.02	0.1173
130.25	4.288	0.106	0.0203	0.122	0.0468	0.123	0.0245	0.0554	0.0265	0.0229	0.0159	0.1	0.0413	0.0385	0.0305	0.0276	0.02	0.1166
130.333	4.268	0.105	0.0203	0.121	0.0464	0.122	0.0243	0.0552	0.0264	0.0229	0.0159	0.1	0.0413	0.0382	0.0303	0.0273	0.02	0.1158
130.417	4.249	0.104	0.0203	0.12	0.046	0.12	0.0242	0.055	0.0263	0.0229	0.0159	0.1	0.0413	0.038	0.03	0.0271	0.02	0.1151
130.5	4.229	0.103	0.0203	0.119	0.0456	0.119	0.024	0.0548	0.0261	0.0229	0.0159	0.1	0.0413	0.0377	0.0298	0.0268	0.02	0.1143
130.583	4.209	0.103	0.0203	0.118	0.0452	0.118	0.0239	0.0546	0.026	0.0229	0.0159	0.1	0.0413	0.0375	0.0295	0.0266	0.02	0.1136
130.667	4.19	0.102	0.0203	0.117	0.0448	0.117	0.0238	0.0545	0.0259	0.0229	0.0159	0.1	0.0413	0.0373	0.0293	0.0264	0.02	0.113
130.75	4.17	0.101	0.0203	0.116	0.0444	0.116	0.0236	0.0543	0.0257	0.0229	0.0159	0.1	0.0413	0.037	0.0291	0.0261	0.02	0.1122
130.833	4.151	0.1	0.0203	0.115	0.044	0.115	0.0235	0.0542	0.0256	0.0229	0.0159	0.1	0.0413	0.0368	0.0289	0.0259	0.02	0.1116
130.917	4.131	0.0997	0.0203	0.114	0.0436	0.114	0.0233	0.054	0.0255	0.0229	0.0159	0.1	0.0413	0.0366	0.0286	0.0257	0.02	0.1109
131	4.111	0.0989	0.0203	0.113	0.0433	0.112	0.0232	0.0539	0.0254	0.0229	0.0159	0.1	0.0413	0.0364	0.0284	0.0255	0.02	0.1103
131.083	4.092	0.0982	0.0203	0.112	0.0429	0.111	0.0231	0.0538	0.0253	0.0229	0.0159	0.1	0.0413	0.0362	0.0282	0.0252	0.02	0.1096
131.167	4.072	0.0975	0.0203	0.111	0.0426	0.11	0.023	0.0536	0.0252	0.0229	0.0159	0.1	0.0413	0.036	0.028	0.025	0.02	0.109
131.25	4.053	0.0968	0.0203	0.11	0.0422	0.109	0.0228	0.0535	0.0251	0.0229	0.0159	0.1	0.0413	0.0357	0.0278	0.0248	0.02	0.1083
131.333	4.033	0.0961	0.0203	0.109	0.0419	0.108	0.0227	0.0534	0.025	0.0229	0.0159	0.1	0.0413	0.0355	0.0276	0.0246	0.02	0.1077
131.417	4.014	0.0954	0.0203	0.108	0.0415	0.107	0.0226	0.0533	0.0249	0.0229	0.0159	0.1	0.0413	0.0353	0.0274	0.0244	0.02	0.1071
131.5	3.995	0.0947	0.0203	0.107	0.0412	0.106	0.0225	0.0533	0.0248	0.0229	0.0159	0.1	0.0413	0.0351	0.0272	0.0242	0.02	0.1065
131.583	3.975	0.0941	0.0203	0.106	0.0409	0.105	0.0223	0.0532	0.0247	0.0229	0.0159	0.1	0.0413	0.035	0.027	0.024	0.02	0.106
131.667	3.956	0.0934	0.0203	0.105	0.0406	0.104	0.0222	0.0531	0.0246	0.0229	0.0159	0.1	0.0413	0.0348	0.0268	0.0238	0.02	0.1054
131.75	3.936	0.0928	0.0203	0.104	0.0403	0.103	0.0221	0.0531	0.0245	0.0229	0.0159	0.1	0.0413	0.0346	0.0266	0.0237	0.02	0.1049

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
131.833	3.917	0.0922	0.0203	0.103	0.04	0.102	0.022	0.053	0.0244	0.0229	0.0159	0.1	0.0413	0.0344	0.0264	0.0235	0.02	0.1043
131.917	3.897	0.0915	0.0203	0.103	0.0397	0.101	0.0219	0.053	0.0243	0.0229	0.0159	0.1	0.0413	0.0342	0.0262	0.0233	0.02	0.1037
132	3.878	0.0909	0.0203	0.102	0.0394	0.1	0.0218	0.0529	0.0243	0.0229	0.0159	0.1	0.0413	0.034	0.0261	0.0231	0.02	0.1032
132.083	3.859	0.0903	0.0203	0.101	0.0391	0.0993	0.0217	0.0529	0.0242	0.0229	0.0159	0.1	0.0413	0.0338	0.0259	0.0229	0.02	0.1026
132.167	3.839	0.0897	0.0203	0.1	0.0388	0.0984	0.0216	0.0529	0.0241	0.0229	0.0159	0.1	0.0413	0.0337	0.0257	0.0227	0.02	0.1021
132.25	3.82	0.0891	0.0203	0.0993	0.0386	0.0975	0.0214	0.0529	0.024	0.0229	0.0159	0.1	0.0413	0.0335	0.0255	0.0226	0.02	0.1016
132.333	3.801	0.0886	0.0203	0.0985	0.0383	0.0966	0.0213	0.0529	0.024	0.0229	0.0159	0.1	0.0413	0.0333	0.0254	0.0224	0.02	0.1011
132.417	3.782	0.088	0.0203	0.0977	0.0381	0.0957	0.0212	0.0529	0.0239	0.0229	0.0159	0.1	0.0413	0.0332	0.0252	0.0222	0.02	0.1006
132.5	3.762	0.0875	0.0203	0.0969	0.0378	0.0948	0.0211	0.0529	0.0238	0.0229	0.0159	0.1	0.0413	0.033	0.025	0.0221	0.02	0.1001
132.583	3.743	0.0869	0.0203	0.0961	0.0376	0.094	0.021	0.0529	0.0238	0.0229	0.0159	0.1	0.0413	0.0328	0.0249	0.0219	0.02	0.0996
132.667	3.724	0.0864	0.0203	0.0954	0.0373	0.0931	0.0209	0.0529	0.0237	0.0229	0.0159	0.1	0.0413	0.0327	0.0247	0.0217	0.02	0.0991
132.75	3.705	0.0859	0.0203	0.0946	0.0371	0.0923	0.0209	0.0529	0.0237	0.0229	0.0159	0.1	0.0413	0.0325	0.0245	0.0216	0.02	0.0986
132.833	3.685	0.0854	0.0203	0.0939	0.0369	0.0915	0.0208	0.0529	0.0236	0.0229	0.0159	0.1	0.0413	0.0323	0.0244	0.0214	0.02	0.0981
132.917	3.666	0.0849	0.0203	0.0932	0.0367	0.0907	0.0207	0.0529	0.0235	0.0229	0.0159	0.1	0.0413	0.0322	0.0242	0.0213	0.02	0.0977
133	3.647	0.0844	0.0203	0.0925	0.0365	0.0899	0.0206	0.0529	0.0235	0.0229	0.0159	0.1	0.0413	0.032	0.0241	0.0211	0.02	0.0972
133.083	3.628	0.0839	0.0203	0.0918	0.0363	0.0892	0.0205	0.0529	0.0234	0.0229	0.0159	0.1	0.0413	0.0319	0.0239	0.0209	0.02	0.0967
133.167	3.609	0.0835	0.0203	0.0911	0.0361	0.0884	0.0204	0.0529	0.0234	0.0229	0.0159	0.1	0.0413	0.0317	0.0238	0.0208	0.02	0.0963
133.25	3.59	0.083	0.0203	0.0904	0.0359	0.0877	0.0203	0.0529	0.0234	0.0229	0.0159	0.1	0.0413	0.0316	0.0236	0.0207	0.02	0.0959
133.333	3.57	0.0826	0.0203	0.0898	0.0357	0.0869	0.0202	0.0529	0.0233	0.0229	0.0159	0.1	0.0413	0.0314	0.0235	0.0205	0.02	0.0954
133.417	3.551	0.0822	0.0203	0.0891	0.0355	0.0862	0.0202	0.0529	0.0233	0.0229	0.0159	0.1	0.0413	0.0313	0.0233	0.0204	0.02	0.095
133.5	3.532	0.0817	0.0203	0.0885	0.0353	0.0855	0.0201	0.0529	0.0232	0.0229	0.0159	0.1	0.0413	0.0311	0.0232	0.0202	0.02	0.0945
133.583	3.513	0.0813	0.0203	0.0878	0.0352	0.0848	0.02	0.0529	0.0232	0.0229	0.0159	0.1	0.0413	0.031	0.023	0.0201	0.02	0.0941
133.667	3.494	0.0809	0.0203	0.0872	0.035	0.0842	0.0199	0.0529	0.0232	0.0229	0.0159	0.1	0.0413	0.0309	0.0229	0.0199	0.02	0.0937
133.75	3.475	0.0806	0.0203	0.0866	0.0349	0.0835	0.0199	0.0529	0.0231	0.0229	0.0159	0.1	0.0413	0.0307	0.0228	0.0198	0.02	0.0933
133.833	3.456	0.0802	0.0203	0.086	0.0347	0.0828	0.0198	0.0529	0.0231	0.0229	0.0159	0.1	0.0413	0.0306	0.0227	0.0197	0.02	0.093
133.917	3.437	0.0798	0.0203	0.0854	0.0346	0.0822	0.0197	0.0529	0.0231	0.0229	0.0159	0.1	0.0413	0.0305	0.0225	0.0196	0.02	0.0926
134	3.418	0.0795	0.0203	0.0848	0.0344	0.0816	0.0196	0.0529	0.0231	0.0229	0.0159	0.1	0.0413	0.0304	0.0224	0.0194	0.02	0.0922
134.083	3.399	0.0791	0.0203	0.0843	0.0343	0.081	0.0196	0.0529	0.023	0.0229	0.0159	0.1	0.0413	0.0302	0.0223	0.0193	0.02	0.0918
134.167	3.38	0.0788	0.0203	0.0837	0.0342	0.0804	0.0195	0.0529	0.023	0.0229	0.0159	0.1	0.0413	0.0301	0.0222	0.0192	0.02	0.0915
134.25	3.361	0.0785	0.0203	0.0832	0.034	0.0798	0.0195	0.0529	0.023	0.0229	0.0159	0.1	0.0413	0.03	0.022	0.0191	0.02	0.0911
134.333	3.342	0.0782	0.0203	0.0826	0.0339	0.0792	0.0194	0.0529	0.023	0.0229	0.0159	0.1	0.0413	0.0299	0.0219	0.019	0.02	0.0908
134.417	3.323	0.0779	0.0203	0.0821	0.0338	0.0787	0.0193	0.0529	0.023	0.0229	0.0159	0.1	0.0413	0.0298	0.0218	0.0188	0.02	0.0904
134.5	3.304	0.0776	0.0203	0.0816	0.0336	0.0781	0.0193	0.0529	0.023	0.0229	0.0159	0.1	0.0413	0.0297	0.0217	0.0187	0.02	0.0901
134.583	3.285	0.0773	0.0203	0.0811	0.0335	0.0776	0.0192	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0296	0.0216	0.0186	0.02	0.0898
134.667	3.267	0.077	0.0203	0.0806	0.0334	0.0771	0.0192	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0295	0.0215	0.0185	0.02	0.0895
134.75	3.248	0.0768	0.0203	0.0801	0.0333	0.0766	0.0191	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0294	0.0214	0.0184	0.02	0.0892
134.833	3.229	0.0765	0.0203	0.0797	0.0332	0.0761	0.0191	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0293	0.0213	0.0183	0.02	0.0889
134.917	3.21	0.0763	0.0203	0.0792	0.0331	0.0756	0.019	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0291	0.0212	0.0182	0.02	0.0885
135	3.191	0.076	0.0203	0.0788	0.033	0.0752	0.019	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.029	0.0211	0.0181	0.02	0.0882
135.083	3.172	0.0758	0.0203	0.0783	0.0329	0.0747	0.0189	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.029	0.021	0.018	0.02	0.088
135.167	3.154	0.0756	0.0203	0.0779	0.0329	0.0743	0.0189	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0289	0.0209	0.0179	0.02	0.0877
135.25	3.135	0.0754	0.0203	0.0775	0.0328	0.0739	0.0188	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0288	0.0208	0.0178	0.02	0.0874
135.333	3.116	0.0752	0.0203	0.0771	0.0327	0.0735	0.0188	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0287	0.0207	0.0178	0.02	0.0872
135.417	3.097	0.075	0.0203	0.0767	0.0327	0.0731	0.0188	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0286	0.0206	0.0177	0.02	0.0869
135.5	3.078	0.0747	0.0203	0.0763	0.0326	0.0727	0.0187	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0285	0.0206	0.0176	0.02	0.0867
135.583	3.06	0.0746	0.0203	0.076	0.0326	0.0723	0.0187	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0285	0.0205	0.0175	0.02	0.0865
135.667	3.041	0.0744	0.0203	0.0756	0.0325	0.072	0.0187	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0284	0.0204	0.0174	0.02	0.0862
135.75	3.022	0.0742	0.0203	0.0753	0.0325	0.0716	0.0186	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0283	0.0203	0.0174	0.02	0.086
135.833	3.004	0.074	0.0203	0.0749	0.0324	0.0713	0.0186	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0282	0.0203	0.0173	0.02	0.0858
135.917	2.985	0.0739	0.0203	0.0746	0.0324	0.071	0.0185	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0282	0.0202	0.0172	0.02	0.0856
136	2.966	0.0737	0.0203	0.0743	0.0324	0.0707	0.0185	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0281	0.0201	0.0172	0.02	0.0854
136.083	2.948	0.0736	0.0203	0.074	0.0323	0.0704	0.0185	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.028	0.0201	0.0171	0.02	0.0852
136.167	2.929	0.0734	0.0203	0.0737	0.0323	0.0701	0.0185	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.028	0.02	0.017	0.02	0.085
136.25	2.91	0.0733	0.0203	0.0734	0.0323	0.0698	0.0184	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0279	0.0199	0.017	0.02	0.0848
136.333	2.892	0.0732	0.0203	0.0732	0.0323	0.0696	0.0184	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0279	0.0199	0.0169	0.02	0.0847
136.417	2.873	0.0731	0.0203	0.0729	0.0323	0.0693	0.0184	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0278	0.0198	0.0169	0.02	0.0845
136.5	2.855	0.0729	0.0203	0.0726	0.0322	0.069	0.0183	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0277	0.0198	0.0168	0.02	0.0843
136.583	2.836	0.0729	0.0203	0.0724	0.0322	0.0688	0.0183	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0277	0.0197	0.0168	0.02	0.0842
136.667	2.818	0.0728	0.0203	0.0722	0.0322	0.0686	0.0183	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0276	0.0197	0.0167	0.02	0.084
136.75	2.799	0.0727	0.0203	0.0719	0.0322	0.0683	0.0183	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0276	0.0196	0.0167	0.02	0.0839
136.833	2.78	0.0726	0.0203	0.0717	0.0322	0.0681	0.0183	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0275	0.0196	0.0166	0.02	0.0837
136.917	2.762	0.0725	0.0203	0.0715	0.0322	0.0679	0.0183	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0275	0.0195	0.0166	0.02	0.0836
137	2.743	0.0725	0.0203	0.0713	0.0322	0.0677	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0275	0.0195	0.0165	0.02	0.0835
137.083	2.725	0.0724	0.0203	0.0711	0.0322	0.0675	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0274	0.0194	0.0165	0.02	0.0833
137.167	2.706	0.0724	0.0203	0.0709	0.0322	0.0673	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0274	0.0194	0.0164	0.02	0.0832
137.25	2.688	0.0723	0.0203	0.0707	0.0322	0.0672	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0273	0.0194	0.0164	0.02	0.0831
137.333	2.67	0.0723	0.0203	0.0705	0.0322	0.067	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0273	0.0193	0.0164	0.02	0.083

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
137.417	2.651	0.0722	0.0203	0.0703	0.0322	0.0669	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0272	0.0193	0.0163	0.02	0.0828
137.5	2.633	0.0722	0.0203	0.0701	0.0322	0.0667	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0272	0.0192	0.0163	0.02	0.0827
137.583	2.614	0.0722	0.0203	0.07	0.0322	0.0666	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0272	0.0192	0.0163	0.02	0.0827
137.667	2.596	0.0722	0.0203	0.0698	0.0322	0.0664	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0272	0.0192	0.0162	0.02	0.0826
137.75	2.577	0.0722	0.0203	0.0697	0.0322	0.0663	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0271	0.0192	0.0162	0.02	0.0825
137.833	2.559	0.0722	0.0203	0.0696	0.0322	0.0662	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0271	0.0191	0.0162	0.02	0.0824
137.917	2.541	0.0722	0.0203	0.0694	0.0322	0.0661	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0271	0.0191	0.0161	0.02	0.0823
138	2.522	0.0722	0.0203	0.0693	0.0322	0.066	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.027	0.0191	0.0161	0.02	0.0822
138.083	2.504	0.0722	0.0203	0.0692	0.0322	0.0659	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.027	0.019	0.0161	0.02	0.0821
138.167	2.486	0.0722	0.0203	0.0691	0.0322	0.0659	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.027	0.019	0.0161	0.02	0.0821
138.25	2.467	0.0722	0.0203	0.069	0.0322	0.0658	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.027	0.019	0.016	0.02	0.082
138.333	2.449	0.0722	0.0203	0.0689	0.0322	0.0658	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.027	0.019	0.016	0.02	0.082
138.417	2.431	0.0722	0.0203	0.0688	0.0322	0.0657	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.019	0.016	0.02	0.0819
138.5	2.412	0.0722	0.0203	0.0687	0.0322	0.0657	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.019	0.016	0.02	0.0819
138.583	2.394	0.0722	0.0203	0.0687	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.016	0.02	0.0818
138.667	2.376	0.0722	0.0203	0.0686	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.016	0.02	0.0818
138.75	2.358	0.0722	0.0203	0.0685	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.016	0.02	0.0818
138.833	2.339	0.0722	0.0203	0.0685	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
138.917	2.321	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139	2.303	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.083	2.285	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.167	2.268	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.25	2.25	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.333	2.233	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.417	2.215	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.5	2.198	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.583	2.182	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.667	2.165	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.75	2.148	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.833	2.132	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
139.917	2.116	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140	2.1	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.083	2.084	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.167	2.068	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.25	2.053	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.333	2.038	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.417	2.022	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.5	2.007	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.583	1.993	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.667	1.978	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.75	1.963	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.833	1.949	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
140.917	1.935	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141	1.921	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.083	1.907	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.167	1.893	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.25	1.88	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.333	1.866	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.417	1.853	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.5	1.84	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.583	1.827	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.667	1.814	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.75	1.801	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.833	1.789	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
141.917	1.777	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142	1.765	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.083	1.753	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.167	1.741	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.25	1.729	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.333	1.718	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.417	1.706	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.5	1.695	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.583	1.684	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.667	1.673	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.75	1.662	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.833	1.651	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
142.917	1.641	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
143	1.63	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.083	1.62	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.167	1.61	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.25	1.6	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.333	1.59	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.417	1.581	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.5	1.571	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.583	1.562	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.667	1.553	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.75	1.543	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.833	1.535	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
143.917	1.526	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144	1.517	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.083	1.509	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.167	1.5	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.25	1.492	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.333	1.484	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.417	1.476	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.5	1.468	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.583	1.46	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.667	1.453	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.75	1.445	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.833	1.438	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
144.917	1.431	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145	1.424	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.083	1.417	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.167	1.41	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.25	1.403	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.333	1.397	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.417	1.391	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.5	1.384	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.583	1.378	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.667	1.372	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.75	1.366	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.833	1.361	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
145.917	1.355	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146	1.349	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.083	1.344	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.167	1.338	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.25	1.333	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.333	1.328	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.417	1.322	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.5	1.317	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.583	1.312	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.667	1.307	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.75	1.302	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.833	1.296	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
146.917	1.291	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147	1.286	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.083	1.281	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.167	1.277	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.25	1.272	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.333	1.267	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.417	1.262	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.5	1.257	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.583	1.253	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.667	1.248	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.75	1.243	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.833	1.239	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
147.917	1.234	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148	1.23	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.083	1.225	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.167	1.221	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.25	1.217	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.333	1.212	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.417	1.208	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.5	1.204	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
148.583	1.2	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.667	1.196	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.75	1.192	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.833	1.188	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
148.917	1.184	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149	1.18	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.083	1.176	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.167	1.172	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.25	1.168	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.333	1.164	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.417	1.16	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.5	1.157	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.583	1.153	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.667	1.15	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.75	1.146	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.833	1.142	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
149.917	1.139	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150	1.135	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.083	1.132	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.167	1.129	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.25	1.125	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.333	1.122	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.417	1.119	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.5	1.115	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.583	1.112	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.667	1.109	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.75	1.106	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.833	1.103	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
150.917	1.1	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151	1.097	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.083	1.094	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.167	1.091	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.25	1.088	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.333	1.085	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.417	1.082	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.5	1.08	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.583	1.077	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.667	1.074	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.75	1.071	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.833	1.069	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
151.917	1.066	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152	1.064	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.083	1.061	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.167	1.059	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.25	1.056	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.333	1.054	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.417	1.051	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.5	1.049	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.583	1.047	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.667	1.045	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.75	1.042	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.833	1.04	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
152.917	1.038	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153	1.036	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.083	1.034	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.167	1.032	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.25	1.03	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.333	1.028	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.417	1.026	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.5	1.024	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.583	1.022	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.667	1.02	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.75	1.018	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.833	1.016	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
153.917	1.015	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154	1.013	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.083	1.011	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
154.167	1.009	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.25	1.008	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.333	1.006	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.417	1.005	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.5	1.003	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.583	1.002	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.667	1	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.75	0.999	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.833	0.997	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
154.917	0.996	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155	0.995	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.083	0.993	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.167	0.992	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.25	0.991	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.333	0.989	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.417	0.988	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.5	0.987	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.583	0.986	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.667	0.985	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.75	0.984	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.833	0.983	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
155.917	0.982	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156	0.981	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.083	0.98	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.167	0.979	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.25	0.978	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.333	0.977	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.417	0.976	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.5	0.975	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.583	0.975	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.667	0.974	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.75	0.973	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.833	0.973	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
156.917	0.972	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157	0.971	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.083	0.971	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.167	0.97	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.25	0.97	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.333	0.969	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.417	0.969	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.5	0.968	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.583	0.968	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.667	0.967	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.75	0.967	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.833	0.967	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
157.917	0.966	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158	0.966	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.083	0.966	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.167	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.25	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.333	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.417	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.5	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.583	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.667	0.965	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
158.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
159.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
159.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
160.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
161.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
162.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
163.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
164.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
165.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
165.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
166.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
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167.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
167.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
168	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
168.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
168.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
168.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
168.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
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169.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
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169.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
169.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
169.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
170.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
170.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
171.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
172.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
173.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
174.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
175.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
176.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
176.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
177.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
178.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
179.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
180.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
181.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
182.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
182.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
183.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
184.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
185.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
186.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
187.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
187.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
188.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
189.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
190.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
191.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
192.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
193.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
193.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
194.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
195.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
196.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
197.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
198.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
198.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
199.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
200.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
201.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
202.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
203.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
204.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
204.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
205.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
206.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
207.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
208.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
209.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
210	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
210.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
211.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
212.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
213.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
214.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
215.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
215.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
216.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
217.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
218.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
219.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
220.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
221.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
221.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
222.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
223.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
224.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
225.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
226.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
226.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
227.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
228.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
229.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
230.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
231.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
232.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
232.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
233.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
234.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
235.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
236.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
237.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
237.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
238.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
239.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
240.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
241.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
242.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
243.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
243.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
244.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
245.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
246.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
247.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
248.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
249.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
249.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
250.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
251.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
252.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
253.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
254.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
254.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
255.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
256.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
257.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
258.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
259.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
260.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
260.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
261.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
262.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
263.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
264.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
265.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
265.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
266.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
267.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
268.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
269.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
270.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
271.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
271.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
272.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
273.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
274.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
275.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
276.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
277	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
277.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
278.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
279.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
280.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
281.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
282.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
282.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
283.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
284.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
285.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
286.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
287.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
288.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
288.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
289.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
290.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
291.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
292.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
293.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
293.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
294.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
295.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
296.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
297.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
298.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.083	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.167	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.25	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
299.333	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.417	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.5	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.583	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.667	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.75	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.833	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
299.917	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817
300	0.964	0.0722	0.0203	0.0684	0.0322	0.0656	0.0182	0.0529	0.0229	0.0229	0.0159	0.1	0.0413	0.0269	0.0189	0.0159	0.02	0.0817

Output data from file C:\USERS\304490\BOX\PB6582 EDF SZC NNB\EDF SZC NNB TEAM\TECH DATA\E01 CALCULATIONS\EXAMINATION HYDROLOGY\HYDROLOGY CALCS MAY 2021\MDS EA ACTIONS MAY 2021\DESIGN FLOWS\SIZE_T100_121SD.ZZN
Selected output data from time (hr): 0
to time (hr): 300

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
0	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
0.083	0.8	0.0178	0.00448	0.018	0.00831	0.0162	0.00355	0.0101	0.00501	0.00504	0.00363	0.1	0.00969	0.00524	0.00369	0.00311	0.02	0.03204
0.167	0.8	0.0178	0.00454	0.018	0.00833	0.0162	0.00356	0.0101	0.00503	0.00508	0.00369	0.1	0.00991	0.00525	0.0037	0.00312	0.02	0.03207
0.25	0.8	0.0179	0.0046	0.018	0.00835	0.0162	0.00357	0.0102	0.00505	0.00513	0.00375	0.1	0.0101	0.00526	0.00371	0.00313	0.02	0.0321
0.333	0.8	0.018	0.00477	0.0181	0.0084	0.0163	0.00359	0.0104	0.0051	0.00525	0.00393	0.1	0.0108	0.0053	0.00375	0.00317	0.02	0.03222
0.417	0.8	0.0181	0.00494	0.0182	0.00846	0.0164	0.00362	0.0106	0.00516	0.00538	0.00411	0.1	0.0114	0.00534	0.00378	0.00321	0.02	0.03233
0.5	0.8	0.0182	0.00511	0.0183	0.00851	0.0164	0.00365	0.0108	0.00521	0.00551	0.00429	0.1	0.0121	0.00537	0.00382	0.00324	0.02	0.03243
0.583	0.8	0.0184	0.0054	0.0184	0.00861	0.0166	0.0037	0.0111	0.0053	0.00572	0.00459	0.1	0.0132	0.00543	0.00388	0.0033	0.02	0.03261
0.667	0.8	0.0186	0.00569	0.0186	0.0087	0.0167	0.00375	0.0114	0.00538	0.00593	0.00489	0.1	0.0142	0.00548	0.00393	0.00335	0.02	0.03276
0.75	0.8	0.0188	0.00598	0.0187	0.00879	0.0168	0.00379	0.0117	0.00546	0.00613	0.0052	0.1	0.0153	0.00554	0.00399	0.00341	0.02	0.03294
0.833	0.8	0.0191	0.00638	0.019	0.00892	0.0169	0.00386	0.0122	0.00558	0.00643	0.00558	0.1	0.0163	0.00562	0.00407	0.00349	0.02	0.03318
0.917	0.8	0.0193	0.00678	0.0192	0.00905	0.017	0.00393	0.0126	0.0057	0.00672	0.00597	0.1	0.0173	0.00571	0.00415	0.00358	0.02	0.03344
1	0.8	0.0196	0.00718	0.0194	0.00918	0.0172	0.00399	0.0131	0.00582	0.00701	0.00635	0.1	0.0184	0.00579	0.00424	0.00366	0.02	0.03369
1.083	0.8	0.02	0.0077	0.0196	0.00935	0.0174	0.00408	0.0136	0.00598	0.00738	0.00668	0.1	0.0191	0.00589	0.00434	0.00376	0.02	0.03399
1.167	0.8	0.0203	0.00822	0.0199	0.00952	0.0175	0.00416	0.0142	0.00614	0.00775	0.00701	0.1	0.0199	0.00599	0.00444	0.00386	0.02	0.03429
1.25	0.8	0.0207	0.00873	0.0202	0.00969	0.0177	0.00425	0.0148	0.00629	0.00812	0.00734	0.1	0.0206	0.0061	0.00454	0.00397	0.02	0.03461
1.333	0.8	0.0211	0.00937	0.0205	0.00989	0.0179	0.00435	0.0155	0.00648	0.00851	0.0076	0.1	0.0212	0.00623	0.00467	0.0041	0.02	0.035
1.417	0.8	0.0215	0.01	0.0208	0.0101	0.0181	0.00446	0.0162	0.00666	0.00889	0.00786	0.1	0.0217	0.00635	0.0048	0.00423	0.02	0.03538
1.5	0.8	0.0219	0.0106	0.0211	0.0103	0.0183	0.00456	0.0169	0.00685	0.00927	0.00812	0.1	0.0222	0.00648	0.00493	0.00436	0.02	0.03577
1.583	0.8	0.0224	0.0114	0.0215	0.0105	0.0186	0.00469	0.0177	0.00707	0.00961	0.00831	0.1	0.0226	0.00663	0.00508	0.0045	0.02	0.03621
1.667	0.8	0.0229	0.0121	0.0219	0.0108	0.0188	0.00481	0.0185	0.00729	0.00994	0.00849	0.1	0.023	0.00678	0.00523	0.00465	0.02	0.03666
1.75	0.8	0.0234	0.0129	0.0223	0.011	0.0191	0.00493	0.0193	0.00751	0.0103	0.00868	0.1	0.0234	0.00693	0.00538	0.0048	0.02	0.03711
1.833	0.8	0.024	0.0137	0.0227	0.0113	0.0194	0.00508	0.0203	0.00777	0.0106	0.00882	0.1	0.0237	0.0071	0.00555	0.00498	0.02	0.03763
1.917	0.8	0.0246	0.0146	0.0232	0.0116	0.0196	0.00522	0.0212	0.00803	0.0108	0.00897	0.1	0.024	0.00728	0.00573	0.00515	0.02	0.03816
2	0.8	0.0252	0.0155	0.0236	0.0119	0.0199	0.00536	0.0222	0.00828	0.0111	0.00911	0.1	0.0242	0.00746	0.00591	0.00533	0.02	0.0387
2.083	0.8	0.0258	0.0164	0.0241	0.0122	0.0202	0.00552	0.0232	0.00857	0.0114	0.00923	0.1	0.0244	0.00766	0.00611	0.00553	0.02	0.0393
2.167	0.8	0.0265	0.0173	0.0246	0.0125	0.0206	0.00568	0.0243	0.00886	0.0116	0.00934	0.1	0.0246	0.00786	0.00631	0.00574	0.02	0.03991
2.25	0.8	0.0272	0.0182	0.0251	0.0129	0.0209	0.00584	0.0254	0.00914	0.0118	0.00946	0.1	0.0247	0.00807	0.00652	0.00594	0.02	0.04053
2.333	0.8	0.0279	0.019	0.0257	0.0132	0.0212	0.00602	0.0266	0.00946	0.012	0.00954	0.1	0.0248	0.00829	0.00674	0.00616	0.02	0.04119
2.417	0.8	0.0286	0.0199	0.0262	0.0136	0.0216	0.0062	0.0278	0.00979	0.0122	0.00962	0.1	0.0248	0.00851	0.00696	0.00639	0.02	0.04186
2.5	0.8	0.0294	0.0207	0.0268	0.014	0.0219	0.00638	0.029	0.0101	0.0124	0.0097	0.1	0.0249	0.00873	0.00718	0.00661	0.02	0.04252
2.583	0.8	0.0302	0.0215	0.0274	0.0144	0.0223	0.00658	0.0303	0.0105	0.0126	0.00975	0.1	0.0249	0.00898	0.00743	0.00686	0.02	0.04327
2.667	0.8	0.031	0.0222	0.028	0.0148	0.0227	0.00678	0.0317	0.0108	0.0127	0.00981	0.1	0.0249	0.00923	0.00768	0.00711	0.02	0.04402
2.75	0.8	0.0318	0.023	0.0287	0.0152	0.0231	0.00698	0.033	0.0112	0.0129	0.00986	0.1	0.0249	0.00948	0.00793	0.00736	0.02	0.04477
2.833	0.8	0.0327	0.0237	0.0293	0.0156	0.0235	0.00719	0.0345	0.0116	0.013	0.00988	0.1	0.0249	0.00975	0.0082	0.00763	0.02	0.04558
2.917	0.8	0.0336	0.0244	0.03	0.016	0.0239	0.0074	0.0359	0.012	0.0131	0.0099	0.1	0.0249	0.01	0.00847	0.0079	0.02	0.04637
3	0.8	0.0345	0.0251	0.0307	0.0165	0.0243	0.00761	0.0374	0.0123	0.0133	0.00991	0.1	0.0249	0.0103	0.00874	0.00817	0.02	0.04721
3.083	0.8	0.0355	0.0257	0.0314	0.017	0.0248	0.00784	0.039	0.0128	0.0134	0.00994	0.1	0.025	0.0106	0.00904	0.00847	0.02	0.04811
3.167	0.8	0.0364	0.0264	0.0322	0.0174	0.0253	0.00807	0.0405	0.0132	0.0135	0.00997	0.1	0.0251	0.0109	0.00934	0.00877	0.02	0.04901
3.25	0.8	0.0374	0.0271	0.0329	0.0179	0.0258	0.00831	0.0421	0.0136	0.0137	0.01	0.1	0.0252	0.0112	0.00964	0.00907	0.02	0.04991
3.333	0.8	0.0385	0.0277	0.0338	0.0185	0.0263	0.00857	0.0437	0.0141	0.0138	0.0101	0.1	0.0255	0.0115	0.00997	0.0094	0.02	0.05087
3.417	0.8	0.0396	0.0283	0.0346	0.019	0.0268	0.00883	0.0453	0.0146	0.014	0.0102	0.1	0.0258	0.0119	0.0103	0.00973	0.02	0.05193
3.5	0.8	0.0407	0.029	0.0354	0.0195	0.0273	0.00909	0.0469	0.0151	0.0141	0.0102	0.1	0.0261	0.0122	0.0106	0.0101	0.02	0.0529
3.583	0.8	0.0419	0.0296	0.0364	0.0201	0.0279	0.00937	0.0485	0.0156	0.0143	0.0104	0.1	0.0266	0.0126	0.011	0.0104	0.02	0.054
3.667	0.8	0.0431	0.0303	0.0373	0.0207	0.0285	0.00966	0.0501	0.0162	0.0145	0.0105	0.1	0.0271	0.0129	0.0114	0.0108	0.02	0.0551
3.75	0.8	0.0444	0.0309	0.0382	0.0213	0.0291	0.00995	0.0517	0.0167	0.0146	0.0107	0.1	0.0276	0.0133	0.0117	0.0112	0.02	0.0562
3.833	0.8	0.0457	0.0315	0.0392	0.022	0.0297	0.0103	0.0533	0.0173	0.0148	0.0109	0.1	0.0282	0.0137	0.0121	0.0116	0.02	0.0574
3.917	0.8	0.047	0.0322	0.0402	0.0226	0.0303	0.0106	0.0549	0.0178	0.015	0.0111	0.1	0.0287	0.0141	0.0126	0.012	0.02	0.0587
4	0.8	0.0484	0.0328	0.0412	0.0233	0.031	0.0109	0.0565	0.0184	0.0152	0.0112	0.1	0.0292	0.0145	0.013	0.0124	0.02	0.0599
4.083	0.8	0.0498	0.0334	0.0424	0.024	0.0316	0.0112	0.0581	0.019	0.0154	0.0114	0.1	0.0296	0.0149	0.0134	0.0128	0.02	0.0611
4.167	0.8	0.0513	0.034	0.0435	0.0247	0.0323	0.0116	0.0596	0.0196	0.0156	0.0116	0.1	0.03	0.0154	0.0138	0.0133	0.02	0.0625
4.25	0.8	0.0527	0.0347	0.0446	0.0254	0.033	0.0119	0.0612	0.0202	0.0158	0.0118	0.1	0.0304	0.0158	0.0143	0.0137	0.02	0.0638
4.333	0.8	0.0543	0.0353	0.0458	0.0261	0.0337	0.0123	0.0628	0.0207	0.016	0.0119	0.1	0.0306	0.0163	0.0147	0.0142	0.02	0.0652
4.417	0.8	0.0558	0.036	0.0469	0.0269	0.0345	0.0127	0.0643	0.0213	0.0162	0.012	0.1	0.0309	0.0168	0.0152	0.0146	0.02	0.0666
4.5	0.8	0.0574	0.0366	0.0481	0.0276	0.0352	0.0131	0.0659	0.0219	0.0164	0.0122	0.1	0.0312	0.0172	0.0157	0.0151	0.02	0.068
4.583	0.8	0.0591	0.0373	0.0494	0.0284	0.036	0.0135	0.0674	0.0225	0.0166	0.0122	0.1	0.0314	0.0177	0.0162	0.0156	0.02	0.0695
4.667	0.8	0.0607	0.038	0.0507	0.0292	0.0368	0.0139	0.069	0.0231	0.0168	0.0123	0.1	0.0316	0.0182	0.0167	0.0161	0.02	0.071
4.75	0.8	0.0624	0.0387	0.052	0.0299	0.0376	0.0143	0.0705	0.0236	0.0169	0.0124	0.1	0.0318	0.0188	0.0172	0.0166	0.02	0.0726
4.833	0.8	0.0641	0.0394	0.0533	0.0307	0.0384	0.0147	0.0721	0.0242	0.0171	0.0125	0.1	0.0319	0.0193	0.0178	0.0172	0.02	0.0743

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
4.917	0.8	0.0658	0.0401	0.0547	0.0314	0.0393	0.0151	0.0736	0.0248	0.0172	0.0126	0.1	0.0321	0.0198	0.0183	0.0177	0.02	0.0758
5	0.8	0.0675	0.0408	0.0561	0.0322	0.0401	0.0155	0.0751	0.0254	0.0174	0.0127	0.1	0.0322	0.0204	0.0188	0.0183	0.02	0.0775
5.083	0.8	0.0691	0.0415	0.0575	0.0329	0.041	0.016	0.0767	0.0259	0.0175	0.0127	0.1	0.0323	0.0209	0.0194	0.0188	0.02	0.0791
5.167	0.8	0.0708	0.0422	0.0589	0.0337	0.0419	0.0164	0.0782	0.0265	0.0176	0.0128	0.1	0.0324	0.0215	0.02	0.0194	0.02	0.0809
5.25	0.8	0.0725	0.0429	0.0604	0.0344	0.0428	0.0168	0.0797	0.0271	0.0177	0.0128	0.1	0.0325	0.0221	0.0206	0.02	0.02	0.0827
5.333	0.8	0.0742	0.0436	0.0618	0.0352	0.0437	0.0172	0.0813	0.0276	0.0178	0.0129	0.1	0.0325	0.0227	0.0211	0.0206	0.02	0.0844
5.417	0.8	0.0758	0.0442	0.0633	0.0359	0.0447	0.0176	0.0828	0.0282	0.0179	0.0129	0.1	0.0326	0.0232	0.0217	0.0211	0.02	0.086
5.5	0.8	0.0775	0.0449	0.0647	0.0367	0.0456	0.018	0.0843	0.0288	0.018	0.013	0.1	0.0326	0.0238	0.0223	0.0217	0.02	0.0878
5.583	0.8	0.0792	0.0455	0.0661	0.0374	0.0466	0.0184	0.0858	0.0293	0.0181	0.013	0.1	0.0326	0.0244	0.0228	0.0223	0.0205	0.09
5.667	0.8	0.0809	0.0461	0.0676	0.0382	0.0476	0.0189	0.0873	0.0299	0.0182	0.013	0.1	0.0326	0.0249	0.0234	0.0228	0.021	0.0921
5.75	0.8	0.0825	0.0467	0.069	0.0389	0.0486	0.0193	0.0888	0.0305	0.0183	0.0131	0.1	0.0326	0.0255	0.024	0.0234	0.0215	0.0944
5.833	0.8	0.0842	0.0472	0.0704	0.0397	0.0497	0.0197	0.0903	0.031	0.0183	0.0131	0.1	0.0326	0.0261	0.0245	0.024	0.022	0.0966
5.917	0.8	0.0858	0.0477	0.0719	0.0404	0.0507	0.0201	0.0918	0.0316	0.0184	0.0131	0.1	0.0326	0.0266	0.0251	0.0245	0.0226	0.0988
6	0.8	0.0875	0.0482	0.0733	0.0412	0.0518	0.0205	0.0933	0.0321	0.0185	0.0131	0.1	0.0326	0.0272	0.0257	0.0251	0.0232	0.1012
6.083	0.8	0.0892	0.0487	0.0747	0.0419	0.0529	0.0209	0.0948	0.0327	0.0185	0.0131	0.1	0.0326	0.0278	0.0262	0.0257	0.0237	0.1034
6.167	0.8	0.0908	0.0491	0.0762	0.0426	0.054	0.0213	0.0963	0.0333	0.0186	0.0131	0.1	0.0326	0.0283	0.0268	0.0262	0.0243	0.1056
6.25	0.8	0.0925	0.0496	0.0776	0.0434	0.0551	0.0217	0.0977	0.0338	0.0186	0.0131	0.1	0.0326	0.0289	0.0274	0.0268	0.0249	0.108
6.333	0.8	0.0941	0.05	0.079	0.0441	0.0562	0.0221	0.0991	0.0344	0.0187	0.0131	0.1	0.0326	0.0295	0.0279	0.0274	0.0254	0.1102
6.417	0.8	0.0958	0.0503	0.0804	0.0448	0.0574	0.0225	0.101	0.0349	0.0187	0.0131	0.1	0.0326	0.03	0.0285	0.0279	0.026	0.1124
6.5	0.8	0.0974	0.0507	0.0818	0.0456	0.0586	0.0229	0.102	0.0355	0.0188	0.0131	0.1	0.0326	0.0306	0.0291	0.0285	0.0266	0.1148
6.583	0.8	0.099	0.0511	0.0833	0.0463	0.0598	0.0233	0.103	0.0361	0.0188	0.0131	0.1	0.0326	0.0312	0.0296	0.0291	0.0271	0.117
6.667	0.8	0.101	0.0514	0.0847	0.047	0.061	0.0237	0.105	0.0366	0.0188	0.0131	0.1	0.0326	0.0317	0.0302	0.0296	0.0277	0.1192
6.75	0.8	0.102	0.0517	0.0861	0.0478	0.0622	0.0242	0.106	0.0372	0.0189	0.0131	0.1	0.0326	0.0323	0.0307	0.0302	0.0283	0.1215
6.833	0.8	0.104	0.052	0.0875	0.0485	0.0634	0.0246	0.107	0.0377	0.0189	0.0131	0.1	0.0326	0.0328	0.0313	0.0307	0.0288	0.1236
6.917	0.8	0.106	0.0523	0.0889	0.0492	0.0647	0.025	0.108	0.0383	0.0189	0.0131	0.1	0.0326	0.0334	0.0319	0.0313	0.0294	0.126
7	0.8	0.107	0.0525	0.0903	0.05	0.066	0.0254	0.11	0.0388	0.019	0.0131	0.1	0.0326	0.034	0.0324	0.0319	0.0299	0.1282
7.083	0.8	0.109	0.0527	0.0917	0.0507	0.0672	0.0258	0.111	0.0393	0.019	0.0131	0.1	0.0326	0.0345	0.033	0.0324	0.0305	0.1304
7.167	0.8	0.11	0.0529	0.0931	0.0514	0.0685	0.0262	0.112	0.0398	0.019	0.0131	0.1	0.0326	0.0351	0.0335	0.033	0.0311	0.1327
7.25	0.8	0.112	0.0532	0.0945	0.0521	0.0698	0.0266	0.113	0.0404	0.019	0.0131	0.1	0.0326	0.0356	0.0341	0.0335	0.0316	0.1348
7.333	0.8	0.114	0.0533	0.096	0.0528	0.0711	0.027	0.114	0.0409	0.019	0.0131	0.1	0.0326	0.0362	0.0346	0.0341	0.0322	0.1371
7.417	0.8	0.115	0.0535	0.0974	0.0536	0.0724	0.0274	0.116	0.0413	0.019	0.0131	0.1	0.0326	0.0367	0.0352	0.0346	0.0327	0.1392
7.5	0.8	0.117	0.0537	0.0988	0.0543	0.0736	0.0278	0.117	0.0418	0.019	0.0131	0.1	0.0326	0.0373	0.0358	0.0352	0.0333	0.1416
7.583	0.8	0.119	0.0538	0.1	0.055	0.0749	0.0282	0.118	0.0423	0.019	0.0131	0.1	0.0326	0.0378	0.0363	0.0357	0.0338	0.1436
7.667	0.8	0.12	0.054	0.102	0.0556	0.0762	0.0286	0.119	0.0428	0.019	0.0131	0.1	0.0326	0.0384	0.0369	0.0363	0.0344	0.146
7.75	0.8	0.122	0.0542	0.103	0.0563	0.0775	0.029	0.12	0.0432	0.019	0.0131	0.1	0.0326	0.0389	0.0374	0.0368	0.0349	0.148
7.833	0.8	0.123	0.0543	0.104	0.057	0.0787	0.0293	0.121	0.0437	0.019	0.0131	0.1	0.0326	0.0395	0.038	0.0374	0.0355	0.1504
7.917	0.8	0.125	0.0544	0.106	0.0576	0.08	0.0297	0.122	0.0441	0.019	0.0131	0.1	0.0326	0.04	0.0385	0.0379	0.036	0.1524
8	0.8	0.126	0.0546	0.107	0.0583	0.0813	0.0301	0.123	0.0446	0.019	0.0131	0.1	0.0326	0.0406	0.0391	0.0385	0.0366	0.1548
8.083	0.8	0.128	0.0547	0.108	0.0589	0.0825	0.0305	0.124	0.045	0.019	0.0131	0.1	0.0326	0.0411	0.0396	0.039	0.0371	0.1568
8.167	0.8	0.129	0.0549	0.11	0.0595	0.0838	0.0309	0.125	0.0454	0.019	0.0131	0.1	0.0326	0.0417	0.0401	0.0396	0.0377	0.1591
8.25	0.8	0.131	0.055	0.111	0.0602	0.085	0.0313	0.126	0.0458	0.019	0.0131	0.1	0.0326	0.0422	0.0407	0.0401	0.0382	0.1612
8.333	0.8	0.132	0.0551	0.113	0.0608	0.0863	0.0316	0.126	0.0462	0.019	0.0131	0.1	0.0326	0.0427	0.0412	0.0406	0.0387	0.1632
8.417	0.8	0.134	0.0552	0.114	0.0614	0.0876	0.032	0.127	0.0466	0.019	0.0131	0.1	0.0326	0.0433	0.0417	0.0412	0.0393	0.1655
8.5	0.8	0.135	0.0553	0.115	0.0619	0.0888	0.0324	0.128	0.047	0.019	0.0131	0.1	0.0326	0.0438	0.0423	0.0417	0.0398	0.1676
8.583	0.8	0.137	0.0554	0.117	0.0625	0.0901	0.0327	0.129	0.0474	0.019	0.0131	0.1	0.0326	0.0443	0.0428	0.0422	0.0403	0.1696
8.667	0.8	0.138	0.0555	0.118	0.0631	0.0913	0.033	0.13	0.0478	0.019	0.0131	0.1	0.0326	0.0448	0.0433	0.0427	0.0408	0.1716
8.75	0.8	0.139	0.0556	0.119	0.0636	0.0926	0.0334	0.13	0.0481	0.019	0.0131	0.1	0.0326	0.0453	0.0438	0.0432	0.0413	0.1736
8.833	0.8	0.141	0.0557	0.12	0.0641	0.0938	0.0337	0.131	0.0485	0.019	0.0131	0.1	0.0326	0.0458	0.0443	0.0437	0.0418	0.1756
8.917	0.8	0.142	0.0558	0.122	0.0647	0.0951	0.034	0.132	0.0489	0.019	0.0131	0.1	0.0326	0.0463	0.0447	0.0442	0.0423	0.1775
9	0.8	0.143	0.0559	0.123	0.0652	0.0963	0.0343	0.133	0.0492	0.019	0.0131	0.1	0.0326	0.0467	0.0452	0.0447	0.0428	0.1794
9.083	0.8	0.144	0.056	0.124	0.0657	0.0976	0.0347	0.133	0.0496	0.019	0.0131	0.1	0.0327	0.0472	0.0457	0.0451	0.0432	0.1812
9.167	0.8	0.146	0.0561	0.125	0.0663	0.0988	0.035	0.134	0.0499	0.019	0.0131	0.1	0.0328	0.0477	0.0462	0.0456	0.0437	0.1832
9.25	0.8	0.147	0.0562	0.126	0.0668	0.1	0.0353	0.135	0.0503	0.0191	0.0132	0.1	0.0328	0.0482	0.0466	0.0461	0.0442	0.1851
9.333	0.8	0.148	0.0563	0.128	0.0673	0.101	0.0356	0.135	0.0506	0.0191	0.0132	0.1	0.0331	0.0486	0.0471	0.0465	0.0446	0.1868
9.417	0.8	0.149	0.0564	0.129	0.0678	0.103	0.0359	0.136	0.051	0.0192	0.0133	0.1	0.0334	0.0491	0.0476	0.047	0.0451	0.1888
9.5	0.8	0.15	0.0565	0.13	0.0683	0.104	0.0362	0.137	0.0514	0.0192	0.0134	0.1	0.0336	0.0495	0.048	0.0475	0.0456	0.1906
9.583	0.8	0.152	0.0567	0.131	0.0688	0.105	0.0365	0.137	0.0517	0.0193	0.0135	0.1	0.0341	0.05	0.0485	0.0479	0.046	0.1924
9.667	0.8	0.153	0.0569	0.132	0.0693	0.106	0.0368	0.138	0.0521	0.0194	0.0136	0.1	0.0346	0.0504	0.0489	0.0484	0.0465	0.1942
9.75	0.8	0.154	0.057	0.133	0.0699	0.108	0.0371	0.139	0.0524	0.0195	0.0138	0.1	0.035	0.0509	0.0494	0.0488	0.0469	0.196
9.833	0.8	0.155	0.0572	0.134	0.0704	0.109	0.0374	0.139	0.0528	0.0196	0.0139	0.1	0.0356	0.0513	0.0498	0.0493	0.0474	0.1978
9.917	0.8	0.156	0.0574	0.136	0.0709	0.11	0.0377	0.14	0.0531	0.0198	0.0141	0.1	0.0361	0.0518	0.0503	0.0497	0.0478	0.1996
10	0.8	0.158	0.0576	0.137	0.0714	0.112	0.038	0.141	0.0534	0.0199	0.0143	0.1	0.0366	0.0522	0.0507	0.0501	0.0483	0.2013
10.083	0.8	0.159	0.0579	0.138	0.0719	0.113	0.0383	0.141	0.0538	0.0201	0.0145	0.1	0.037	0.0526	0.0511	0.0506	0.0487	0.203

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
10.167	0.8	0.16	0.0582	0.139	0.0724	0.114	0.0386	0.142	0.0541	0.0202	0.0147	0.1	0.0374	0.0531	0.0516	0.051	0.0491	0.2048
10.25	0.8	0.161	0.0584	0.14	0.0729	0.115	0.0389	0.143	0.0545	0.0204	0.0148	0.1	0.0379	0.0535	0.052	0.0514	0.0496	0.2065
10.333	0.8	0.162	0.0587	0.141	0.0734	0.117	0.0392	0.143	0.0548	0.0206	0.015	0.1	0.0382	0.0539	0.0524	0.0519	0.05	0.2082
10.417	0.8	0.164	0.059	0.142	0.0739	0.118	0.0395	0.144	0.0552	0.0208	0.0151	0.1	0.0385	0.0544	0.0529	0.0523	0.0504	0.21
10.5	0.8	0.165	0.0593	0.143	0.0744	0.119	0.0398	0.145	0.0555	0.021	0.0152	0.1	0.0387	0.0548	0.0533	0.0527	0.0509	0.2117
10.583	0.8	0.166	0.0597	0.144	0.0749	0.12	0.0401	0.145	0.0559	0.0212	0.0154	0.1	0.039	0.0552	0.0537	0.0532	0.0513	0.2134
10.667	0.8	0.167	0.06	0.145	0.0754	0.122	0.0404	0.146	0.0562	0.0213	0.0155	0.1	0.0392	0.0557	0.0541	0.0536	0.0517	0.2151
10.75	0.8	0.168	0.0604	0.146	0.0759	0.123	0.0407	0.147	0.0565	0.0215	0.0156	0.1	0.0394	0.0561	0.0546	0.054	0.0521	0.2168
10.833	0.8	0.17	0.0608	0.148	0.0764	0.124	0.041	0.148	0.0569	0.0217	0.0156	0.1	0.0396	0.0565	0.055	0.0544	0.0526	0.2185
10.917	0.8	0.171	0.0612	0.149	0.0768	0.125	0.0413	0.148	0.0572	0.0218	0.0157	0.1	0.0397	0.0569	0.0554	0.0549	0.053	0.2202
11	0.8	0.172	0.0616	0.15	0.0773	0.127	0.0416	0.149	0.0576	0.022	0.0158	0.1	0.0399	0.0573	0.0558	0.0553	0.0534	0.2218
11.083	0.8	0.173	0.0621	0.151	0.0778	0.128	0.0419	0.15	0.0579	0.0221	0.0159	0.1	0.04	0.0578	0.0563	0.0557	0.0538	0.2236
11.167	0.8	0.174	0.0625	0.152	0.0783	0.129	0.0422	0.151	0.0582	0.0222	0.0159	0.1	0.0401	0.0582	0.0567	0.0561	0.0543	0.2253
11.25	0.8	0.175	0.063	0.153	0.0788	0.13	0.0425	0.151	0.0586	0.0223	0.016	0.1	0.0402	0.0586	0.0571	0.0566	0.0547	0.227
11.333	0.8	0.177	0.0634	0.154	0.0793	0.132	0.0428	0.152	0.0589	0.0224	0.016	0.1	0.0402	0.059	0.0575	0.057	0.0551	0.2286
11.417	0.8	0.178	0.0638	0.155	0.0798	0.133	0.0431	0.153	0.0593	0.0225	0.0161	0.1	0.0403	0.0595	0.058	0.0574	0.0555	0.2304
11.5	0.8	0.179	0.0642	0.156	0.0803	0.134	0.0434	0.154	0.0596	0.0226	0.0161	0.1	0.0403	0.0599	0.0584	0.0578	0.056	0.2321
11.583	0.8	0.18	0.0646	0.157	0.0808	0.135	0.0437	0.154	0.06	0.0227	0.0162	0.1	0.0403	0.0603	0.0588	0.0583	0.0564	0.2338
11.667	0.8	0.181	0.065	0.158	0.0813	0.136	0.044	0.155	0.0603	0.0228	0.0162	0.1	0.0403	0.0608	0.0592	0.0587	0.0568	0.2355
11.75	0.8	0.183	0.0654	0.159	0.0818	0.137	0.0443	0.156	0.0607	0.0229	0.0162	0.1	0.0403	0.0612	0.0597	0.0591	0.0572	0.2372
11.833	0.8	0.184	0.0658	0.16	0.0823	0.139	0.0446	0.157	0.061	0.023	0.0162	0.1	0.0403	0.0616	0.0601	0.0595	0.0577	0.2389
11.917	0.8	0.185	0.0661	0.162	0.0828	0.14	0.0449	0.158	0.0614	0.023	0.0162	0.1	0.0403	0.062	0.0605	0.06	0.0581	0.2406
12	0.8	0.186	0.0665	0.163	0.0833	0.141	0.0452	0.159	0.0617	0.0231	0.0163	0.1	0.0403	0.0624	0.0609	0.0604	0.0585	0.2422
12.083	0.8	0.187	0.0668	0.164	0.0838	0.142	0.0454	0.16	0.0621	0.0232	0.0163	0.1	0.0403	0.0629	0.0614	0.0608	0.0589	0.244
12.167	0.8	0.188	0.0672	0.165	0.0843	0.143	0.0457	0.161	0.0624	0.0232	0.0163	0.1	0.0403	0.0633	0.0618	0.0612	0.0594	0.2457
12.25	0.8	0.19	0.0675	0.166	0.0848	0.144	0.046	0.161	0.0628	0.0233	0.0163	0.1	0.0403	0.0637	0.0622	0.0617	0.0598	0.2474
12.333	0.8	0.191	0.0678	0.167	0.0853	0.146	0.0463	0.162	0.0632	0.0233	0.0163	0.1	0.0403	0.0641	0.0626	0.0621	0.0602	0.249
12.417	0.8	0.192	0.0681	0.168	0.0858	0.147	0.0466	0.163	0.0635	0.0234	0.0163	0.1	0.0403	0.0646	0.0631	0.0625	0.0606	0.2508
12.5	0.8	0.193	0.0684	0.169	0.0863	0.148	0.0469	0.164	0.0639	0.0234	0.0163	0.1	0.0403	0.065	0.0635	0.0629	0.0611	0.2525
12.583	0.8	0.194	0.0686	0.17	0.0869	0.149	0.0472	0.165	0.0643	0.0235	0.0163	0.1	0.0403	0.0654	0.0639	0.0634	0.0615	0.2542
12.667	0.8	0.195	0.0689	0.171	0.0874	0.15	0.0475	0.166	0.0646	0.0235	0.0163	0.1	0.0403	0.0658	0.0643	0.0638	0.0619	0.2558
12.75	0.8	0.196	0.0691	0.172	0.0879	0.151	0.0478	0.167	0.065	0.0235	0.0163	0.1	0.0403	0.0663	0.0648	0.0642	0.0623	0.2576
12.833	0.8	0.198	0.0694	0.173	0.0884	0.152	0.0481	0.167	0.0653	0.0236	0.0163	0.1	0.0403	0.0667	0.0652	0.0646	0.0628	0.2593
12.917	0.8	0.199	0.0696	0.174	0.0889	0.153	0.0483	0.168	0.0657	0.0236	0.0163	0.1	0.0403	0.0671	0.0656	0.065	0.0632	0.2609
13	0.8	0.2	0.0698	0.175	0.0894	0.154	0.0486	0.169	0.0661	0.0236	0.0163	0.1	0.0403	0.0675	0.066	0.0654	0.0636	0.2625
13.083	0.806	0.201	0.07	0.176	0.0899	0.156	0.0489	0.17	0.0664	0.0236	0.0163	0.1	0.0403	0.0679	0.0664	0.0659	0.064	0.2642
13.167	0.811	0.202	0.0702	0.177	0.0904	0.157	0.0492	0.17	0.0668	0.0236	0.0163	0.1	0.0403	0.0683	0.0668	0.0663	0.0644	0.2658
13.25	0.817	0.204	0.0704	0.178	0.091	0.158	0.0495	0.171	0.0671	0.0237	0.0163	0.1	0.0403	0.0688	0.0673	0.0667	0.0649	0.2677
13.333	0.825	0.205	0.0706	0.18	0.0915	0.159	0.0498	0.172	0.0675	0.0237	0.0163	0.1	0.0403	0.0692	0.0677	0.0671	0.0653	0.2693
13.417	0.834	0.206	0.0707	0.181	0.092	0.16	0.0501	0.173	0.0678	0.0237	0.0163	0.1	0.0403	0.0696	0.0681	0.0676	0.0657	0.271
13.5	0.842	0.207	0.0709	0.182	0.0925	0.161	0.0504	0.173	0.0681	0.0237	0.0163	0.1	0.0403	0.07	0.0685	0.068	0.0661	0.2726
13.583	0.851	0.208	0.0711	0.183	0.093	0.162	0.0507	0.174	0.0684	0.0237	0.0163	0.1	0.0403	0.0704	0.0689	0.0684	0.0665	0.2742
13.667	0.859	0.21	0.0713	0.184	0.0935	0.163	0.051	0.175	0.0687	0.0237	0.0163	0.1	0.0403	0.0709	0.0694	0.0688	0.067	0.2761
13.75	0.868	0.211	0.0714	0.185	0.094	0.164	0.0513	0.175	0.069	0.0237	0.0163	0.1	0.0403	0.0713	0.0698	0.0692	0.0674	0.2777
13.833	0.876	0.212	0.0716	0.186	0.0945	0.165	0.0516	0.176	0.0693	0.0237	0.0163	0.1	0.0403	0.0717	0.0702	0.0696	0.0678	0.2793
13.917	0.885	0.213	0.0717	0.187	0.095	0.166	0.0519	0.176	0.0696	0.0237	0.0163	0.1	0.0403	0.0721	0.0706	0.0701	0.0682	0.281
14	0.894	0.214	0.0719	0.188	0.0955	0.167	0.0522	0.177	0.0699	0.0237	0.0163	0.1	0.0403	0.0725	0.071	0.0705	0.0686	0.2826
14.083	0.903	0.215	0.072	0.189	0.0959	0.168	0.0525	0.177	0.0702	0.0237	0.0163	0.1	0.0403	0.073	0.0715	0.0709	0.0691	0.2845
14.167	0.912	0.217	0.0721	0.19	0.0963	0.169	0.0528	0.178	0.0704	0.0237	0.0163	0.1	0.0403	0.0734	0.0719	0.0713	0.0695	0.2861
14.25	0.921	0.218	0.0723	0.191	0.0968	0.17	0.0531	0.178	0.0707	0.0237	0.0163	0.1	0.0403	0.0738	0.0723	0.0718	0.0699	0.2878
14.333	0.93	0.219	0.0724	0.192	0.0972	0.171	0.0534	0.179	0.071	0.0237	0.0163	0.1	0.0403	0.0742	0.0727	0.0722	0.0703	0.2894
14.417	0.939	0.22	0.0725	0.193	0.0976	0.172	0.0536	0.179	0.0712	0.0237	0.0163	0.1	0.0403	0.0746	0.0731	0.0726	0.0707	0.291
14.5	0.948	0.221	0.0726	0.194	0.098	0.173	0.0539	0.18	0.0715	0.0237	0.0163	0.1	0.0403	0.075	0.0735	0.073	0.0712	0.2927
14.583	0.958	0.222	0.0727	0.195	0.0984	0.174	0.0542	0.18	0.0717	0.0237	0.0163	0.1	0.0403	0.0754	0.0739	0.0734	0.0716	0.2943
14.667	0.967	0.223	0.0728	0.196	0.0988	0.175	0.0544	0.181	0.0719	0.0237	0.0163	0.1	0.0403	0.0758	0.0743	0.0738	0.072	0.2959
14.75	0.976	0.224	0.0729	0.197	0.0992	0.176	0.0547	0.181	0.0722	0.0237	0.0163	0.1	0.0403	0.0762	0.0748	0.0742	0.0724	0.2976
14.833	0.986	0.225	0.073	0.198	0.0996	0.177	0.0549	0.182	0.0724	0.0237	0.0163	0.1	0.0403	0.0766	0.0751	0.0746	0.0727	0.299
14.917	0.996	0.226	0.0731	0.199	0.1	0.178	0.0552	0.182	0.0726	0.0237	0.0163	0.1	0.0403	0.077	0.0755	0.075	0.0731	0.3006
15	1.005	0.227	0.0732	0.2	0.1	0.179	0.0554	0.182	0.0728	0.0237	0.0163	0.1	0.0403	0.0774	0.0759	0.0753	0.0735	0.3021
15.083	1.015	0.228	0.0733	0.201	0.101	0.18	0.0557	0.183	0.0731	0.0237	0.0163	0.1	0.0403	0.0777	0.0763	0.0757	0.0739	0.3036
15.167	1.025	0.229	0.0733	0.202	0.101	0.181	0.0559	0.183	0.0733	0.0237	0.0163	0.1	0.0403	0.0781	0.0766	0.0761	0.0742	0.305
15.25	1.035	0.23	0.0734	0.203	0.101	0.182	0.0561	0.183	0.0735	0.0237	0.0163	0.1	0.0403	0.0785	0.077	0.0764	0.0746	0.3065
15.333	1.045	0.23	0.0735	0.204	0.102	0.183	0.0564	0.184	0.0737	0.0237	0.0163	0.1	0.0403	0.0788	0.0773	0.0768	0.0749	0.3078

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
15.417	1.055	0.231	0.0735	0.205	0.102	0.184	0.0566	0.184	0.0739	0.0237	0.0163	0.1	0.0403	0.0792	0.0777	0.0771	0.0753	0.3093
15.5	1.065	0.232	0.0736	0.206	0.102	0.185	0.0568	0.184	0.0741	0.0237	0.0163	0.1	0.0403	0.0795	0.078	0.0775	0.0757	0.3107
15.583	1.075	0.233	0.0736	0.207	0.103	0.186	0.057	0.185	0.0742	0.0237	0.0163	0.1	0.0403	0.0799	0.0784	0.0778	0.076	0.3121
15.667	1.085	0.234	0.0737	0.207	0.103	0.186	0.0573	0.185	0.0744	0.0237	0.0163	0.1	0.0403	0.0802	0.0787	0.0782	0.0763	0.3134
15.75	1.096	0.235	0.0737	0.208	0.103	0.187	0.0575	0.185	0.0746	0.0237	0.0163	0.1	0.0403	0.0805	0.079	0.0785	0.0767	0.3147
15.833	1.106	0.235	0.0737	0.209	0.103	0.188	0.0577	0.186	0.0748	0.0237	0.0163	0.1	0.0403	0.0808	0.0793	0.0788	0.077	0.3159
15.917	1.117	0.236	0.0738	0.21	0.104	0.189	0.0579	0.186	0.0749	0.0237	0.0163	0.1	0.0403	0.0811	0.0797	0.0791	0.0773	0.3172
16	1.127	0.237	0.0738	0.211	0.104	0.19	0.0581	0.186	0.0751	0.0237	0.0163	0.1	0.0403	0.0815	0.08	0.0794	0.0776	0.3185
16.083	1.138	0.237	0.0738	0.211	0.104	0.191	0.0582	0.187	0.0753	0.0237	0.0163	0.1	0.0403	0.0818	0.0803	0.0797	0.0779	0.3197
16.167	1.149	0.238	0.0738	0.212	0.105	0.192	0.0584	0.187	0.0754	0.0237	0.0163	0.1	0.0403	0.0821	0.0806	0.08	0.0782	0.3209
16.25	1.16	0.239	0.0738	0.213	0.105	0.193	0.0586	0.187	0.0756	0.0237	0.0163	0.1	0.0403	0.0824	0.0809	0.0803	0.0785	0.3221
16.333	1.171	0.24	0.0738	0.214	0.105	0.193	0.0588	0.187	0.0757	0.0237	0.0163	0.1	0.0403	0.0827	0.0812	0.0806	0.0788	0.3233
16.417	1.182	0.24	0.0738	0.214	0.105	0.194	0.0589	0.188	0.0758	0.0237	0.0163	0.1	0.0403	0.0829	0.0814	0.0809	0.0791	0.3243
16.5	1.193	0.241	0.0738	0.215	0.106	0.195	0.0591	0.188	0.076	0.0237	0.0163	0.1	0.0403	0.0832	0.0817	0.0812	0.0794	0.3255
16.583	1.204	0.241	0.0738	0.216	0.106	0.196	0.0593	0.188	0.0761	0.0237	0.0163	0.1	0.0403	0.0835	0.082	0.0814	0.0796	0.3265
16.667	1.215	0.242	0.0738	0.217	0.106	0.197	0.0594	0.188	0.0762	0.0237	0.0163	0.1	0.0403	0.0837	0.0823	0.0817	0.0799	0.3276
16.75	1.226	0.243	0.0738	0.217	0.106	0.197	0.0596	0.189	0.0763	0.0237	0.0163	0.1	0.0403	0.084	0.0825	0.082	0.0801	0.3286
16.833	1.238	0.243	0.0738	0.218	0.106	0.198	0.0597	0.189	0.0765	0.0237	0.0163	0.1	0.0403	0.0843	0.0828	0.0822	0.0804	0.3297
16.917	1.249	0.244	0.0738	0.218	0.107	0.199	0.0599	0.189	0.0766	0.0237	0.0163	0.1	0.0403	0.0845	0.083	0.0825	0.0807	0.3307
17	1.261	0.244	0.0738	0.219	0.107	0.2	0.06	0.189	0.0767	0.0237	0.0163	0.1	0.0403	0.0848	0.0833	0.0827	0.0809	0.3317
17.083	1.273	0.245	0.0738	0.22	0.107	0.2	0.0602	0.189	0.0768	0.0237	0.0163	0.1	0.0403	0.085	0.0835	0.083	0.0812	0.3327
17.167	1.284	0.245	0.0738	0.22	0.107	0.201	0.0603	0.19	0.0769	0.0237	0.0163	0.1	0.0403	0.0852	0.0838	0.0832	0.0814	0.3336
17.25	1.296	0.246	0.0738	0.221	0.107	0.202	0.0604	0.19	0.077	0.0237	0.0163	0.1	0.0403	0.0855	0.084	0.0834	0.0816	0.3345
17.333	1.308	0.246	0.0738	0.222	0.108	0.202	0.0605	0.19	0.0771	0.0237	0.0163	0.1	0.0403	0.0857	0.0842	0.0837	0.0818	0.3354
17.417	1.32	0.247	0.0738	0.222	0.108	0.203	0.0607	0.19	0.0772	0.0237	0.0163	0.1	0.0403	0.0859	0.0844	0.0839	0.0821	0.3363
17.5	1.332	0.247	0.0738	0.223	0.108	0.204	0.0608	0.19	0.0773	0.0237	0.0163	0.1	0.0403	0.0861	0.0846	0.0841	0.0823	0.3371
17.583	1.344	0.248	0.0738	0.223	0.108	0.204	0.0609	0.191	0.0774	0.0237	0.0163	0.1	0.0403	0.0863	0.0848	0.0843	0.0825	0.3379
17.667	1.356	0.248	0.0738	0.224	0.108	0.205	0.061	0.191	0.0775	0.0237	0.0163	0.1	0.0403	0.0865	0.0851	0.0845	0.0827	0.3388
17.75	1.369	0.249	0.0738	0.224	0.109	0.205	0.0612	0.191	0.0776	0.0237	0.0163	0.1	0.0403	0.0867	0.0853	0.0847	0.0829	0.3396
17.833	1.381	0.249	0.0738	0.225	0.109	0.206	0.0613	0.191	0.0776	0.0237	0.0163	0.1	0.0403	0.0869	0.0854	0.0849	0.0831	0.3403
17.917	1.394	0.25	0.0738	0.225	0.109	0.206	0.0614	0.191	0.0777	0.0237	0.0163	0.1	0.0403	0.0871	0.0856	0.0851	0.0833	0.3411
18	1.406	0.25	0.0738	0.226	0.109	0.207	0.0615	0.192	0.0778	0.0237	0.0163	0.1	0.0403	0.0873	0.0858	0.0853	0.0835	0.3419
18.083	1.419	0.25	0.0739	0.226	0.109	0.208	0.0616	0.192	0.0779	0.0237	0.0163	0.1	0.0404	0.0875	0.086	0.0854	0.0836	0.3425
18.167	1.431	0.251	0.0739	0.227	0.109	0.208	0.0617	0.192	0.078	0.0237	0.0163	0.1	0.0404	0.0876	0.0862	0.0856	0.0838	0.3432
18.25	1.443	0.251	0.0739	0.227	0.109	0.209	0.0618	0.192	0.0781	0.0237	0.0163	0.1	0.0404	0.0878	0.0863	0.0858	0.084	0.3439
18.333	1.456	0.252	0.0739	0.227	0.11	0.209	0.0619	0.192	0.0782	0.0238	0.0164	0.1	0.0406	0.088	0.0865	0.086	0.0841	0.3446
18.417	1.468	0.252	0.074	0.228	0.11	0.21	0.062	0.192	0.0783	0.0238	0.0164	0.1	0.0408	0.0882	0.0867	0.0861	0.0843	0.3453
18.5	1.481	0.252	0.074	0.228	0.11	0.21	0.0621	0.193	0.0784	0.0238	0.0165	0.1	0.041	0.0883	0.0868	0.0863	0.0845	0.3459
18.583	1.493	0.253	0.0741	0.229	0.11	0.211	0.0622	0.193	0.0785	0.0239	0.0166	0.1	0.0414	0.0885	0.087	0.0865	0.0847	0.3467
18.667	1.505	0.253	0.0742	0.229	0.11	0.211	0.0623	0.193	0.0786	0.024	0.0167	0.1	0.0419	0.0887	0.0872	0.0866	0.0848	0.3473
18.75	1.518	0.254	0.0744	0.23	0.11	0.212	0.0624	0.193	0.0787	0.0241	0.0168	0.1	0.0423	0.0888	0.0874	0.0868	0.085	0.348
18.833	1.53	0.254	0.0745	0.23	0.11	0.212	0.0625	0.194	0.0789	0.0242	0.017	0.1	0.0428	0.089	0.0875	0.087	0.0852	0.3487
18.917	1.542	0.254	0.0747	0.23	0.111	0.213	0.0627	0.194	0.079	0.0243	0.0171	0.1	0.0433	0.0892	0.0877	0.0872	0.0853	0.3494
19	1.555	0.255	0.0749	0.231	0.111	0.213	0.0628	0.194	0.0791	0.0244	0.0173	0.1	0.0438	0.0894	0.0879	0.0873	0.0855	0.3501
19.083	1.567	0.255	0.0751	0.231	0.111	0.214	0.0629	0.194	0.0792	0.0246	0.0175	0.1	0.0443	0.0895	0.0881	0.0875	0.0857	0.3508
19.167	1.579	0.256	0.0753	0.232	0.111	0.214	0.063	0.195	0.0794	0.0248	0.0177	0.1	0.0448	0.0897	0.0882	0.0877	0.0859	0.3515
19.25	1.591	0.256	0.0755	0.232	0.111	0.215	0.0631	0.195	0.0795	0.0249	0.0179	0.1	0.0452	0.0899	0.0884	0.0879	0.086	0.3522
19.333	1.603	0.257	0.0758	0.233	0.112	0.215	0.0632	0.195	0.0797	0.0251	0.018	0.1	0.0456	0.0901	0.0886	0.088	0.0862	0.3529
19.417	1.616	0.257	0.0761	0.233	0.112	0.216	0.0633	0.196	0.0798	0.0253	0.0182	0.1	0.0459	0.0902	0.0888	0.0882	0.0864	0.3536
19.5	1.628	0.258	0.0764	0.234	0.112	0.216	0.0635	0.196	0.08	0.0255	0.0183	0.1	0.0462	0.0904	0.0889	0.0884	0.0866	0.3543
19.583	1.64	0.258	0.0767	0.234	0.112	0.217	0.0636	0.197	0.0801	0.0257	0.0184	0.1	0.0465	0.0906	0.0891	0.0886	0.0868	0.3551
19.667	1.652	0.258	0.0771	0.235	0.112	0.217	0.0637	0.197	0.0803	0.0259	0.0185	0.1	0.0467	0.0908	0.0893	0.0888	0.0869	0.3558
19.75	1.664	0.259	0.0774	0.235	0.113	0.218	0.0638	0.197	0.0805	0.026	0.0187	0.1	0.0469	0.091	0.0895	0.0889	0.0871	0.3565
19.833	1.676	0.259	0.0778	0.235	0.113	0.218	0.064	0.198	0.0806	0.0262	0.0187	0.1	0.0471	0.0912	0.0897	0.0891	0.0873	0.3573
19.917	1.688	0.26	0.0782	0.236	0.113	0.219	0.0641	0.198	0.0808	0.0263	0.0188	0.1	0.0473	0.0913	0.0899	0.0893	0.0875	0.358
20	1.7	0.26	0.0786	0.236	0.113	0.219	0.0642	0.199	0.081	0.0265	0.0189	0.1	0.0475	0.0915	0.09	0.0895	0.0877	0.3587
20.083	1.713	0.261	0.079	0.237	0.113	0.22	0.0643	0.199	0.0812	0.0266	0.019	0.1	0.0476	0.0917	0.0902	0.0897	0.0879	0.3595
20.167	1.725	0.262	0.0795	0.237	0.114	0.22	0.0645	0.2	0.0814	0.0268	0.019	0.1	0.0477	0.0919	0.0904	0.0899	0.0881	0.3603
20.25	1.737	0.262	0.0799	0.238	0.114	0.221	0.0646	0.2	0.0815	0.0269	0.0191	0.1	0.0478	0.0921	0.0906	0.0901	0.0883	0.3611
20.333	1.749	0.263	0.0803	0.238	0.114	0.221	0.0648	0.201	0.0817	0.027	0.0192	0.1	0.0479	0.0923	0.0908	0.0903	0.0885	0.3619
20.417	1.761	0.263	0.0808	0.239	0.114	0.222	0.0649	0.202	0.0819	0.0271	0.0192	0.1	0.0479	0.0925	0.091	0.0905	0.0887	0.3627
20.5	1.773	0.264	0.0812	0.239	0.115	0.222	0.065	0.202	0.0821	0.0272	0.0193	0.1	0.048	0.0927	0.0912	0.0907	0.0889	0.3635
20.583	1.784	0.264	0.0816	0.24	0.115	0.223	0.0652	0.203	0.0823	0.0273	0.0193	0.1	0.048	0.0929	0.0914	0.0909	0.0891	0.3643

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
20.667	1.796	0.265	0.082	0.24	0.115	0.223	0.0653	0.203	0.0826	0.0274	0.0193	0.1	0.048	0.0931	0.0917	0.0911	0.0893	0.3652
20.75	1.808	0.266	0.0824	0.241	0.116	0.224	0.0655	0.204	0.0828	0.0275	0.0194	0.1	0.048	0.0933	0.0919	0.0913	0.0895	0.366
20.833	1.82	0.266	0.0828	0.242	0.116	0.224	0.0656	0.205	0.083	0.0276	0.0194	0.1	0.048	0.0936	0.0921	0.0915	0.0897	0.3669
20.917	1.832	0.267	0.0832	0.242	0.116	0.225	0.0658	0.205	0.0832	0.0276	0.0194	0.1	0.048	0.0938	0.0923	0.0917	0.0899	0.3677
21	1.844	0.267	0.0835	0.243	0.116	0.225	0.0659	0.206	0.0834	0.0277	0.0194	0.1	0.048	0.094	0.0925	0.092	0.0902	0.3687
21.083	1.856	0.268	0.0839	0.243	0.117	0.226	0.0661	0.207	0.0837	0.0278	0.0194	0.1	0.048	0.0942	0.0927	0.0922	0.0904	0.3695
21.167	1.868	0.269	0.0842	0.244	0.117	0.226	0.0663	0.208	0.0839	0.0278	0.0194	0.1	0.048	0.0944	0.0929	0.0924	0.0906	0.3703
21.25	1.879	0.269	0.0845	0.244	0.117	0.227	0.0664	0.208	0.0841	0.0279	0.0194	0.1	0.048	0.0946	0.0932	0.0926	0.0908	0.3712
21.333	1.891	0.27	0.0848	0.245	0.118	0.227	0.0666	0.209	0.0844	0.028	0.0194	0.1	0.048	0.0949	0.0934	0.0928	0.091	0.3721
21.417	1.903	0.271	0.0852	0.245	0.118	0.228	0.0667	0.21	0.0846	0.028	0.0194	0.1	0.048	0.0951	0.0936	0.0931	0.0913	0.3731
21.5	1.915	0.271	0.0855	0.246	0.118	0.228	0.0669	0.211	0.0849	0.0281	0.0194	0.1	0.048	0.0953	0.0938	0.0933	0.0915	0.3739
21.583	1.926	0.272	0.0857	0.247	0.119	0.229	0.0671	0.211	0.0851	0.0281	0.0194	0.1	0.048	0.0955	0.0941	0.0935	0.0917	0.3748
21.667	1.938	0.273	0.086	0.247	0.119	0.229	0.0672	0.212	0.0854	0.0281	0.0194	0.1	0.048	0.0958	0.0943	0.0938	0.092	0.3759
21.75	1.95	0.274	0.0863	0.248	0.119	0.23	0.0674	0.213	0.0857	0.0282	0.0194	0.1	0.048	0.096	0.0945	0.094	0.0922	0.3767
21.833	1.961	0.274	0.0865	0.248	0.12	0.23	0.0676	0.214	0.0859	0.0282	0.0194	0.1	0.048	0.0963	0.0948	0.0942	0.0924	0.3777
21.917	1.973	0.275	0.0867	0.249	0.12	0.231	0.0678	0.214	0.0862	0.0282	0.0194	0.1	0.048	0.0965	0.095	0.0945	0.0927	0.3787
22	1.985	0.276	0.087	0.25	0.12	0.231	0.068	0.215	0.0865	0.0283	0.0194	0.1	0.048	0.0967	0.0953	0.0947	0.0929	0.3796
22.083	1.996	0.277	0.0872	0.25	0.121	0.232	0.0681	0.216	0.0867	0.0283	0.0194	0.1	0.048	0.097	0.0955	0.095	0.0932	0.3807
22.167	2.008	0.277	0.0874	0.251	0.121	0.232	0.0683	0.216	0.087	0.0283	0.0194	0.1	0.048	0.0972	0.0958	0.0952	0.0934	0.3816
22.25	2.019	0.278	0.0876	0.251	0.121	0.233	0.0685	0.217	0.0873	0.0283	0.0194	0.1	0.048	0.0975	0.096	0.0955	0.0937	0.3827
22.333	2.031	0.279	0.0878	0.252	0.122	0.233	0.0687	0.218	0.0875	0.0283	0.0194	0.1	0.048	0.0977	0.0963	0.0957	0.0939	0.3836
22.417	2.043	0.28	0.0879	0.253	0.122	0.234	0.0689	0.218	0.0878	0.0283	0.0194	0.1	0.048	0.098	0.0965	0.096	0.0942	0.3847
22.5	2.054	0.28	0.0881	0.253	0.122	0.234	0.0691	0.219	0.0881	0.0284	0.0194	0.1	0.048	0.0983	0.0968	0.0962	0.0944	0.3857
22.583	2.066	0.281	0.0883	0.254	0.123	0.235	0.0693	0.219	0.0883	0.0284	0.0194	0.1	0.048	0.0985	0.0971	0.0965	0.0947	0.3868
22.667	2.077	0.282	0.0885	0.255	0.123	0.235	0.0695	0.22	0.0886	0.0284	0.0194	0.1	0.048	0.0988	0.0973	0.0968	0.095	0.3879
22.75	2.088	0.283	0.0886	0.255	0.123	0.236	0.0697	0.221	0.0888	0.0284	0.0194	0.1	0.048	0.0991	0.0976	0.097	0.0952	0.3889
22.833	2.1	0.284	0.0888	0.256	0.124	0.236	0.0699	0.221	0.089	0.0284	0.0194	0.1	0.048	0.0993	0.0979	0.0973	0.0955	0.39
22.917	2.111	0.285	0.0889	0.257	0.124	0.237	0.0701	0.222	0.0893	0.0284	0.0194	0.1	0.048	0.0996	0.0981	0.0976	0.0958	0.3911
23	2.123	0.285	0.0891	0.258	0.125	0.237	0.0703	0.222	0.0895	0.0284	0.0194	0.1	0.048	0.0999	0.0984	0.0979	0.0961	0.3923
23.083	2.134	0.286	0.0892	0.258	0.125	0.238	0.0705	0.223	0.0897	0.0284	0.0194	0.1	0.048	0.1	0.0987	0.0982	0.0964	0.3933
23.167	2.145	0.287	0.0894	0.259	0.125	0.238	0.0707	0.223	0.0899	0.0284	0.0194	0.1	0.048	0.1	0.099	0.0984	0.0967	0.3941
23.25	2.157	0.288	0.0895	0.26	0.126	0.239	0.0709	0.224	0.0902	0.0284	0.0194	0.1	0.048	0.101	0.0993	0.0987	0.0969	0.3959
23.333	2.168	0.289	0.0896	0.26	0.126	0.239	0.0711	0.224	0.0904	0.0284	0.0194	0.1	0.048	0.101	0.0996	0.099	0.0972	0.3968
23.417	2.179	0.289	0.0897	0.261	0.126	0.24	0.0713	0.225	0.0906	0.0284	0.0194	0.1	0.048	0.101	0.0998	0.0993	0.0975	0.3976
23.5	2.191	0.29	0.0899	0.262	0.126	0.241	0.0715	0.225	0.0908	0.0284	0.0194	0.1	0.048	0.102	0.1	0.0996	0.0978	0.3994
23.583	2.202	0.291	0.09	0.262	0.127	0.241	0.0717	0.226	0.091	0.0284	0.0194	0.1	0.048	0.102	0.1	0.0998	0.0981	0.3999
23.667	2.213	0.292	0.0901	0.263	0.127	0.242	0.0719	0.226	0.0912	0.0284	0.0194	0.1	0.048	0.102	0.101	0.1	0.0983	0.4013
23.75	2.224	0.292	0.0902	0.264	0.127	0.242	0.0721	0.227	0.0914	0.0284	0.0194	0.1	0.048	0.102	0.101	0.1	0.0986	0.4016
23.833	2.235	0.293	0.0903	0.265	0.128	0.243	0.0722	0.227	0.0916	0.0284	0.0194	0.1	0.048	0.103	0.101	0.101	0.0989	0.4039
23.917	2.247	0.294	0.0904	0.265	0.128	0.243	0.0724	0.228	0.0918	0.0284	0.0194	0.1	0.048	0.103	0.101	0.101	0.0991	0.4041
24	2.258	0.294	0.0905	0.266	0.128	0.244	0.0726	0.228	0.092	0.0284	0.0194	0.1	0.048	0.103	0.102	0.101	0.0994	0.4054
24.083	2.269	0.295	0.0905	0.267	0.129	0.244	0.0728	0.228	0.0921	0.0284	0.0194	0.1	0.048	0.103	0.102	0.101	0.0997	0.4057
24.167	2.28	0.296	0.0906	0.267	0.129	0.245	0.0729	0.229	0.0923	0.0284	0.0194	0.1	0.048	0.104	0.102	0.102	0.0999	0.4079
24.25	2.291	0.296	0.0907	0.268	0.129	0.246	0.0731	0.229	0.0925	0.0284	0.0194	0.1	0.048	0.104	0.102	0.102	0.1	0.408
24.333	2.302	0.297	0.0908	0.268	0.129	0.246	0.0733	0.229	0.0927	0.0284	0.0194	0.1	0.048	0.104	0.103	0.102	0.1	0.409
24.417	2.313	0.298	0.0908	0.269	0.13	0.247	0.0734	0.23	0.0928	0.0284	0.0194	0.1	0.048	0.104	0.103	0.102	0.101	0.41
24.5	2.324	0.298	0.0909	0.27	0.13	0.247	0.0736	0.23	0.093	0.0284	0.0194	0.1	0.048	0.105	0.103	0.103	0.101	0.412
24.583	2.335	0.299	0.0909	0.27	0.13	0.248	0.0738	0.23	0.0932	0.0284	0.0194	0.1	0.048	0.105	0.103	0.103	0.101	0.412
24.667	2.346	0.299	0.091	0.271	0.13	0.248	0.0739	0.231	0.0933	0.0284	0.0194	0.1	0.048	0.105	0.104	0.103	0.101	0.413
24.75	2.357	0.3	0.091	0.271	0.131	0.249	0.0741	0.231	0.0935	0.0284	0.0194	0.1	0.048	0.105	0.104	0.103	0.102	0.414
24.833	2.368	0.301	0.0911	0.272	0.131	0.249	0.0742	0.231	0.0937	0.0284	0.0194	0.1	0.048	0.106	0.104	0.104	0.102	0.416
24.917	2.379	0.301	0.0911	0.273	0.131	0.25	0.0744	0.232	0.0938	0.0284	0.0194	0.1	0.048	0.106	0.104	0.104	0.102	0.416
25	2.39	0.302	0.0911	0.273	0.131	0.251	0.0745	0.232	0.094	0.0284	0.0194	0.1	0.048	0.106	0.105	0.104	0.102	0.417
25.083	2.401	0.302	0.0911	0.274	0.131	0.251	0.0746	0.232	0.0941	0.0284	0.0194	0.1	0.048	0.106	0.105	0.104	0.102	0.417
25.167	2.412	0.303	0.0912	0.274	0.132	0.252	0.0748	0.232	0.0942	0.0284	0.0194	0.1	0.048	0.106	0.105	0.104	0.103	0.418
25.25	2.423	0.303	0.0912	0.275	0.132	0.252	0.0749	0.233	0.0944	0.0284	0.0194	0.1	0.048	0.107	0.105	0.105	0.103	0.42
25.333	2.434	0.304	0.0912	0.275	0.132	0.253	0.0751	0.233	0.0945	0.0284	0.0194	0.1	0.048	0.107	0.105	0.105	0.103	0.42
25.417	2.445	0.304	0.0912	0.276	0.132	0.253	0.0752	0.233	0.0946	0.0284	0.0194	0.1	0.048	0.107	0.106	0.105	0.103	0.421
25.5	2.456	0.305	0.0912	0.276	0.132	0.254	0.0753	0.234	0.0948	0.0284	0.0194	0.1	0.048	0.107	0.106	0.105	0.104	0.422
25.583	2.467	0.305	0.0912	0.277	0.133	0.255	0.0754	0.234	0.0949	0.0284	0.0194	0.1	0.048	0.107	0.106	0.105	0.104	0.422
25.667	2.478	0.306	0.0912	0.277	0.133	0.255	0.0756	0.234	0.095	0.0284	0.0194	0.1	0.048	0.108	0.106	0.106	0.104	0.424
25.75	2.489	0.306	0.0912	0.278	0.133	0.256	0.0757	0.234	0.0951	0.0284	0.0194	0.1	0.048	0.108	0.106	0.106	0.104	0.424
25.833	2.5	0.307	0.0912	0.278	0.133	0.256	0.0758	0.235	0.0952	0.0284	0.0194	0.1	0.048	0.108	0.107	0.106	0.104	0.425

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
25.917	2.512	0.307	0.0912	0.279	0.133	0.257	0.0759	0.235	0.0953	0.0284	0.0194	0.1	0.048	0.108	0.107	0.106	0.104	0.425
26	2.523	0.308	0.0912	0.279	0.134	0.257	0.076	0.235	0.0955	0.0284	0.0194	0.1	0.048	0.108	0.107	0.106	0.105	0.426
26.083	2.534	0.308	0.0912	0.28	0.134	0.258	0.0761	0.235	0.0956	0.0284	0.0194	0.1	0.048	0.109	0.107	0.107	0.105	0.428
26.167	2.545	0.309	0.0912	0.28	0.134	0.258	0.0762	0.235	0.0957	0.0284	0.0194	0.1	0.048	0.109	0.107	0.107	0.105	0.428
26.25	2.557	0.309	0.0912	0.281	0.134	0.259	0.0763	0.236	0.0958	0.0284	0.0194	0.1	0.048	0.109	0.107	0.107	0.105	0.428
26.333	2.568	0.309	0.0912	0.281	0.134	0.259	0.0764	0.236	0.0959	0.0284	0.0194	0.1	0.048	0.109	0.108	0.107	0.105	0.429
26.417	2.58	0.31	0.0912	0.281	0.134	0.26	0.0765	0.236	0.096	0.0284	0.0194	0.1	0.048	0.109	0.108	0.107	0.105	0.429
26.5	2.591	0.31	0.0912	0.282	0.135	0.26	0.0766	0.236	0.0961	0.0284	0.0194	0.1	0.048	0.109	0.108	0.107	0.106	0.43
26.583	2.602	0.31	0.0912	0.282	0.135	0.26	0.0767	0.236	0.0962	0.0284	0.0194	0.1	0.048	0.11	0.108	0.108	0.106	0.432
26.667	2.614	0.311	0.0912	0.283	0.135	0.261	0.0768	0.237	0.0963	0.0284	0.0194	0.1	0.048	0.11	0.108	0.108	0.106	0.432
26.75	2.625	0.311	0.0912	0.283	0.135	0.261	0.0769	0.237	0.0964	0.0284	0.0194	0.1	0.048	0.11	0.108	0.108	0.106	0.432
26.833	2.637	0.312	0.0912	0.283	0.135	0.262	0.077	0.237	0.0964	0.0284	0.0194	0.1	0.048	0.11	0.109	0.108	0.106	0.433
26.917	2.648	0.312	0.0912	0.284	0.135	0.262	0.0771	0.237	0.0965	0.0284	0.0194	0.1	0.048	0.11	0.109	0.108	0.106	0.433
27	2.66	0.312	0.0912	0.284	0.135	0.263	0.0772	0.237	0.0966	0.0284	0.0194	0.1	0.048	0.11	0.109	0.108	0.107	0.434
27.083	2.672	0.313	0.0912	0.284	0.136	0.263	0.0773	0.237	0.0967	0.0284	0.0194	0.1	0.048	0.11	0.109	0.108	0.107	0.434
27.167	2.683	0.313	0.0912	0.285	0.136	0.263	0.0774	0.238	0.0968	0.0284	0.0194	0.1	0.0481	0.111	0.109	0.109	0.107	0.436
27.25	2.695	0.313	0.0912	0.285	0.136	0.264	0.0774	0.238	0.0969	0.0284	0.0194	0.1	0.0481	0.111	0.109	0.109	0.107	0.436
27.333	2.707	0.314	0.0912	0.285	0.136	0.264	0.0775	0.238	0.097	0.0284	0.0195	0.1	0.0482	0.111	0.109	0.109	0.107	0.436
27.417	2.718	0.314	0.0913	0.286	0.136	0.265	0.0776	0.238	0.0971	0.0284	0.0195	0.1	0.0483	0.111	0.11	0.109	0.107	0.437
27.5	2.73	0.314	0.0913	0.286	0.136	0.265	0.0777	0.238	0.0972	0.0285	0.0196	0.1	0.0485	0.111	0.11	0.109	0.107	0.437
27.583	2.742	0.315	0.0914	0.286	0.136	0.266	0.0778	0.239	0.0973	0.0285	0.0197	0.1	0.0488	0.111	0.11	0.109	0.107	0.437
27.667	2.754	0.315	0.0915	0.287	0.137	0.266	0.0779	0.239	0.0974	0.0286	0.0198	0.1	0.0491	0.111	0.11	0.109	0.108	0.438
27.75	2.766	0.315	0.0916	0.287	0.137	0.266	0.078	0.239	0.0975	0.0287	0.0198	0.1	0.0495	0.112	0.11	0.11	0.108	0.44
27.833	2.777	0.316	0.0917	0.287	0.137	0.267	0.0781	0.239	0.0976	0.0288	0.02	0.1	0.05	0.112	0.11	0.11	0.108	0.44
27.917	2.789	0.316	0.0919	0.288	0.137	0.267	0.0782	0.239	0.0978	0.0289	0.0202	0.1	0.0506	0.112	0.11	0.11	0.108	0.44
28	2.801	0.316	0.092	0.288	0.137	0.268	0.0783	0.24	0.0979	0.029	0.0203	0.1	0.0511	0.112	0.11	0.11	0.108	0.44
28.083	2.813	0.317	0.0922	0.289	0.137	0.268	0.0784	0.24	0.098	0.0291	0.0205	0.1	0.0516	0.112	0.111	0.11	0.108	0.441
28.167	2.825	0.317	0.0924	0.289	0.138	0.269	0.0785	0.24	0.0981	0.0293	0.0207	0.1	0.0521	0.112	0.111	0.11	0.108	0.441
28.25	2.837	0.318	0.0926	0.289	0.138	0.269	0.0786	0.241	0.0983	0.0294	0.0209	0.1	0.0526	0.112	0.111	0.11	0.109	0.442
28.333	2.849	0.318	0.0929	0.29	0.138	0.269	0.0787	0.241	0.0984	0.0296	0.021	0.1	0.053	0.113	0.111	0.111	0.109	0.444
28.417	2.861	0.319	0.0932	0.29	0.138	0.27	0.0788	0.241	0.0986	0.0298	0.0212	0.1	0.0533	0.113	0.111	0.111	0.109	0.444
28.5	2.873	0.319	0.0934	0.29	0.138	0.27	0.0789	0.242	0.0987	0.03	0.0214	0.1	0.0537	0.113	0.111	0.111	0.109	0.444
28.583	2.886	0.32	0.0938	0.291	0.138	0.271	0.079	0.242	0.0989	0.0302	0.0215	0.1	0.054	0.113	0.112	0.111	0.109	0.445
28.667	2.898	0.32	0.0941	0.291	0.139	0.271	0.0791	0.243	0.099	0.0304	0.0216	0.1	0.0542	0.113	0.112	0.111	0.109	0.445
28.75	2.91	0.32	0.0944	0.292	0.139	0.272	0.0792	0.243	0.0992	0.0306	0.0217	0.1	0.0545	0.113	0.112	0.111	0.11	0.446
28.833	2.922	0.321	0.0948	0.292	0.139	0.272	0.0794	0.243	0.0994	0.0307	0.0218	0.1	0.0547	0.114	0.112	0.112	0.11	0.448
28.917	2.935	0.321	0.0952	0.293	0.139	0.272	0.0795	0.244	0.0995	0.0309	0.0219	0.1	0.0549	0.114	0.112	0.112	0.11	0.448
29	2.947	0.322	0.0955	0.293	0.14	0.273	0.0796	0.244	0.0997	0.0311	0.022	0.1	0.055	0.114	0.112	0.112	0.11	0.448
29.083	2.959	0.322	0.096	0.293	0.14	0.273	0.0798	0.245	0.0999	0.0312	0.0221	0.1	0.0552	0.114	0.113	0.112	0.11	0.449
29.167	2.972	0.323	0.0964	0.294	0.14	0.274	0.0799	0.245	0.1	0.0313	0.0222	0.1	0.0553	0.114	0.113	0.112	0.11	0.449
29.25	2.984	0.324	0.0969	0.294	0.14	0.274	0.08	0.246	0.1	0.0315	0.0222	0.1	0.0554	0.114	0.113	0.112	0.111	0.45
29.333	2.996	0.324	0.0973	0.295	0.141	0.275	0.0802	0.246	0.1	0.0316	0.0223	0.1	0.0555	0.115	0.113	0.113	0.111	0.452
29.417	3.009	0.325	0.0978	0.295	0.141	0.275	0.0803	0.247	0.101	0.0317	0.0223	0.1	0.0556	0.115	0.113	0.113	0.111	0.452
29.5	3.021	0.325	0.0982	0.296	0.141	0.276	0.0804	0.248	0.101	0.0318	0.0224	0.1	0.0557	0.115	0.113	0.113	0.111	0.452
29.583	3.034	0.326	0.0986	0.296	0.141	0.276	0.0806	0.248	0.101	0.0319	0.0224	0.1	0.0557	0.115	0.114	0.113	0.111	0.453
29.667	3.046	0.326	0.099	0.297	0.142	0.277	0.0807	0.249	0.101	0.032	0.0225	0.1	0.0557	0.115	0.114	0.113	0.112	0.454
29.75	3.059	0.327	0.0994	0.297	0.142	0.277	0.0809	0.249	0.101	0.0321	0.0225	0.1	0.0557	0.116	0.114	0.114	0.112	0.456
29.833	3.072	0.328	0.0998	0.298	0.142	0.278	0.081	0.25	0.102	0.0322	0.0225	0.1	0.0557	0.116	0.114	0.114	0.112	0.456
29.917	3.084	0.328	0.1	0.298	0.142	0.278	0.0812	0.251	0.102	0.0323	0.0226	0.1	0.0557	0.116	0.114	0.114	0.112	0.456
30	3.097	0.329	0.101	0.299	0.143	0.279	0.0813	0.251	0.102	0.0323	0.0226	0.1	0.0557	0.116	0.115	0.114	0.112	0.457
30.083	3.11	0.329	0.101	0.299	0.143	0.279	0.0815	0.252	0.102	0.0324	0.0226	0.1	0.0557	0.116	0.115	0.114	0.113	0.458
30.167	3.122	0.33	0.101	0.3	0.143	0.28	0.0816	0.253	0.103	0.0325	0.0226	0.1	0.0557	0.117	0.115	0.115	0.113	0.46
30.25	3.135	0.331	0.102	0.3	0.144	0.28	0.0818	0.254	0.103	0.0325	0.0226	0.1	0.0557	0.117	0.115	0.115	0.113	0.46
30.333	3.148	0.331	0.102	0.301	0.144	0.28	0.082	0.254	0.103	0.0326	0.0226	0.1	0.0559	0.117	0.116	0.115	0.113	0.461
30.417	3.161	0.332	0.102	0.302	0.144	0.281	0.0821	0.255	0.103	0.0327	0.0227	0.1	0.056	0.117	0.116	0.115	0.113	0.461
30.5	3.174	0.333	0.103	0.302	0.144	0.282	0.0823	0.256	0.104	0.0328	0.0227	0.1	0.0561	0.117	0.116	0.115	0.114	0.462
30.583	3.187	0.334	0.103	0.303	0.145	0.282	0.0825	0.257	0.104	0.0329	0.0228	0.1	0.0564	0.118	0.116	0.116	0.114	0.464
30.667	3.2	0.334	0.103	0.303	0.145	0.283	0.0827	0.258	0.104	0.033	0.0229	0.1	0.0567	0.118	0.117	0.116	0.114	0.465
30.75	3.213	0.335	0.104	0.304	0.146	0.283	0.0828	0.259	0.104	0.0331	0.023	0.1	0.057	0.118	0.117	0.116	0.114	0.465
30.833	3.226	0.336	0.104	0.305	0.146	0.284	0.083	0.259	0.105	0.0332	0.0231	0.1	0.0576	0.118	0.117	0.116	0.115	0.466
30.917	3.239	0.337	0.105	0.305	0.146	0.284	0.0833	0.26	0.105	0.0334	0.0233	0.1	0.0581	0.119	0.117	0.117	0.115	0.468
31	3.252	0.338	0.105	0.306	0.147	0.285	0.0835	0.261	0.105	0.0335	0.0234	0.1	0.0587	0.119	0.118	0.117	0.115	0.469
31.083	3.265	0.338	0.105	0.307	0.147	0.285	0.0837	0.262	0.106	0.0337	0.0236	0.1	0.0592	0.119	0.118	0.117	0.116	0.47

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
31.167	3.278	0.339	0.106	0.307	0.148	0.286	0.0839	0.263	0.106	0.0338	0.0238	0.1	0.0597	0.12	0.118	0.118	0.116	0.472
31.25	3.291	0.34	0.106	0.308	0.148	0.286	0.0841	0.264	0.106	0.034	0.024	0.1	0.0602	0.12	0.118	0.118	0.116	0.472
31.333	3.304	0.341	0.107	0.309	0.148	0.287	0.0843	0.265	0.107	0.0342	0.0242	0.1	0.0606	0.12	0.119	0.118	0.116	0.473
31.417	3.318	0.342	0.107	0.31	0.149	0.288	0.0846	0.266	0.107	0.0344	0.0243	0.1	0.061	0.121	0.119	0.119	0.117	0.476
31.5	3.331	0.343	0.107	0.311	0.149	0.288	0.0848	0.267	0.107	0.0346	0.0245	0.1	0.0613	0.121	0.119	0.119	0.117	0.476
31.583	3.344	0.344	0.108	0.311	0.15	0.289	0.0851	0.268	0.108	0.0348	0.0246	0.1	0.0616	0.121	0.12	0.119	0.117	0.477
31.667	3.358	0.345	0.108	0.312	0.15	0.29	0.0853	0.269	0.108	0.035	0.0248	0.1	0.0619	0.121	0.12	0.119	0.118	0.478
31.75	3.371	0.346	0.109	0.313	0.151	0.29	0.0856	0.269	0.108	0.0352	0.0249	0.1	0.0621	0.122	0.12	0.12	0.118	0.48
31.833	3.384	0.347	0.109	0.314	0.151	0.291	0.0858	0.27	0.109	0.0354	0.025	0.1	0.0623	0.122	0.121	0.12	0.118	0.481
31.917	3.398	0.348	0.11	0.315	0.152	0.291	0.0861	0.271	0.109	0.0355	0.0251	0.1	0.0625	0.122	0.121	0.121	0.119	0.483
32	3.411	0.349	0.111	0.316	0.152	0.292	0.0864	0.272	0.109	0.0357	0.0252	0.1	0.0627	0.123	0.121	0.121	0.119	0.484
32.083	3.425	0.35	0.111	0.317	0.153	0.293	0.0866	0.273	0.11	0.0358	0.0252	0.1	0.0629	0.123	0.122	0.121	0.119	0.485
32.167	3.439	0.352	0.112	0.318	0.153	0.293	0.0869	0.274	0.11	0.036	0.0253	0.1	0.063	0.124	0.122	0.122	0.12	0.488
32.25	3.452	0.353	0.112	0.318	0.154	0.294	0.0872	0.275	0.111	0.0361	0.0254	0.1	0.0631	0.124	0.122	0.122	0.12	0.488
32.333	3.466	0.354	0.113	0.319	0.154	0.295	0.0875	0.276	0.111	0.0362	0.0254	0.1	0.0632	0.124	0.123	0.122	0.121	0.49
32.417	3.48	0.355	0.113	0.32	0.155	0.295	0.0877	0.278	0.111	0.0363	0.0255	0.1	0.0633	0.125	0.123	0.123	0.121	0.492
32.5	3.493	0.356	0.114	0.321	0.155	0.296	0.088	0.279	0.112	0.0365	0.0256	0.1	0.0634	0.125	0.124	0.123	0.121	0.493
32.583	3.507	0.357	0.115	0.322	0.156	0.297	0.0883	0.28	0.112	0.0366	0.0256	0.1	0.0634	0.125	0.124	0.124	0.122	0.495
32.667	3.521	0.358	0.115	0.323	0.156	0.298	0.0886	0.281	0.112	0.0367	0.0256	0.1	0.0634	0.126	0.124	0.124	0.122	0.496
32.75	3.535	0.359	0.116	0.324	0.156	0.298	0.0889	0.282	0.113	0.0368	0.0257	0.1	0.0635	0.126	0.125	0.124	0.123	0.498
32.833	3.548	0.36	0.116	0.325	0.157	0.299	0.0891	0.283	0.113	0.0368	0.0257	0.1	0.0635	0.127	0.125	0.125	0.123	0.5
32.917	3.562	0.362	0.117	0.326	0.157	0.3	0.0894	0.284	0.113	0.0369	0.0257	0.1	0.0635	0.127	0.126	0.125	0.123	0.501
33	3.576	0.363	0.117	0.327	0.158	0.301	0.0897	0.285	0.114	0.037	0.0258	0.1	0.0635	0.127	0.126	0.125	0.124	0.502
33.083	3.59	0.364	0.117	0.328	0.158	0.301	0.09	0.286	0.114	0.0371	0.0258	0.1	0.0635	0.128	0.126	0.126	0.124	0.504
33.167	3.604	0.365	0.118	0.329	0.159	0.302	0.0902	0.287	0.115	0.0371	0.0258	0.1	0.0635	0.128	0.127	0.126	0.125	0.506
33.25	3.618	0.366	0.118	0.33	0.159	0.303	0.0905	0.288	0.115	0.0372	0.0258	0.1	0.0635	0.129	0.127	0.127	0.125	0.508
33.333	3.632	0.367	0.119	0.331	0.16	0.304	0.0908	0.289	0.115	0.0373	0.0258	0.1	0.0636	0.129	0.128	0.127	0.125	0.509
33.417	3.647	0.368	0.119	0.332	0.16	0.304	0.0911	0.291	0.116	0.0373	0.0258	0.1	0.0637	0.129	0.128	0.127	0.126	0.51
33.5	3.661	0.37	0.12	0.333	0.161	0.305	0.0914	0.292	0.116	0.0374	0.0259	0.1	0.0637	0.13	0.128	0.128	0.126	0.512
33.583	3.675	0.371	0.12	0.334	0.161	0.306	0.0917	0.293	0.117	0.0375	0.026	0.1	0.0641	0.13	0.129	0.128	0.127	0.514
33.667	3.689	0.372	0.12	0.335	0.162	0.307	0.092	0.294	0.117	0.0376	0.026	0.1	0.0644	0.131	0.129	0.129	0.127	0.516
33.75	3.703	0.373	0.121	0.336	0.163	0.308	0.0923	0.295	0.117	0.0377	0.0261	0.1	0.0647	0.131	0.13	0.129	0.127	0.517
33.833	3.718	0.374	0.121	0.337	0.163	0.309	0.0926	0.296	0.118	0.0379	0.0263	0.1	0.0652	0.131	0.13	0.129	0.128	0.518
33.917	3.732	0.376	0.122	0.338	0.164	0.31	0.0929	0.298	0.118	0.038	0.0264	0.1	0.0657	0.132	0.13	0.13	0.128	0.52
34	3.746	0.377	0.122	0.34	0.164	0.31	0.0932	0.299	0.119	0.0381	0.0266	0.1	0.0662	0.132	0.131	0.13	0.129	0.522
34.083	3.761	0.378	0.122	0.341	0.165	0.311	0.0935	0.3	0.119	0.0383	0.0267	0.1	0.0667	0.133	0.131	0.131	0.129	0.524
34.167	3.775	0.379	0.123	0.342	0.165	0.312	0.0938	0.301	0.12	0.0385	0.0269	0.1	0.0672	0.133	0.132	0.131	0.129	0.525
34.25	3.79	0.381	0.123	0.343	0.166	0.313	0.0941	0.302	0.12	0.0386	0.0271	0.1	0.0677	0.134	0.132	0.132	0.13	0.528
34.333	3.804	0.382	0.124	0.344	0.166	0.314	0.0945	0.304	0.121	0.0388	0.0273	0.1	0.0681	0.134	0.133	0.132	0.13	0.529
34.417	3.819	0.383	0.124	0.345	0.167	0.315	0.0948	0.305	0.121	0.039	0.0275	0.1	0.0685	0.135	0.133	0.133	0.131	0.532
34.5	3.834	0.385	0.125	0.346	0.168	0.316	0.0951	0.306	0.121	0.0392	0.0276	0.1	0.0689	0.135	0.134	0.133	0.131	0.533
34.583	3.848	0.386	0.125	0.347	0.168	0.317	0.0954	0.307	0.122	0.0394	0.0278	0.1	0.0692	0.135	0.134	0.133	0.132	0.534
34.667	3.863	0.387	0.126	0.349	0.169	0.318	0.0958	0.308	0.122	0.0396	0.0279	0.1	0.0695	0.136	0.134	0.134	0.132	0.536
34.75	3.878	0.389	0.126	0.35	0.17	0.319	0.0961	0.31	0.123	0.0398	0.028	0.1	0.0698	0.136	0.135	0.134	0.133	0.538
34.833	3.893	0.39	0.127	0.351	0.17	0.32	0.0965	0.311	0.123	0.04	0.0281	0.1	0.07	0.137	0.135	0.135	0.133	0.54
34.917	3.907	0.392	0.127	0.352	0.171	0.321	0.0968	0.312	0.124	0.0401	0.0282	0.1	0.0702	0.137	0.136	0.135	0.134	0.542
35	3.922	0.393	0.128	0.353	0.171	0.322	0.0972	0.313	0.124	0.0403	0.0283	0.1	0.0704	0.138	0.136	0.136	0.134	0.544
35.083	3.937	0.394	0.128	0.355	0.172	0.323	0.0975	0.314	0.125	0.0405	0.0284	0.1	0.0705	0.138	0.137	0.136	0.135	0.546
35.167	3.952	0.396	0.129	0.356	0.173	0.324	0.0979	0.316	0.125	0.0406	0.0285	0.1	0.0707	0.139	0.137	0.137	0.135	0.548
35.25	3.967	0.397	0.129	0.357	0.173	0.325	0.0982	0.317	0.126	0.0407	0.0285	0.1	0.0708	0.139	0.138	0.137	0.136	0.55
35.333	3.982	0.399	0.13	0.358	0.174	0.326	0.0986	0.318	0.126	0.0409	0.0286	0.1	0.0709	0.14	0.138	0.138	0.136	0.552
35.417	3.997	0.4	0.131	0.36	0.175	0.327	0.0989	0.319	0.126	0.041	0.0287	0.1	0.071	0.14	0.139	0.138	0.137	0.554
35.5	4.012	0.401	0.131	0.361	0.175	0.328	0.0993	0.321	0.127	0.0411	0.0287	0.1	0.0711	0.141	0.139	0.139	0.137	0.556
35.583	4.028	0.403	0.132	0.362	0.176	0.329	0.0996	0.322	0.127	0.0412	0.0288	0.1	0.0711	0.141	0.14	0.139	0.138	0.558
35.667	4.043	0.404	0.132	0.364	0.176	0.33	0.1	0.323	0.128	0.0413	0.0288	0.1	0.0711	0.142	0.14	0.14	0.138	0.56
35.75	4.058	0.406	0.133	0.365	0.177	0.331	0.1	0.324	0.128	0.0414	0.0288	0.1	0.0712	0.142	0.141	0.14	0.139	0.562
35.833	4.073	0.407	0.133	0.366	0.178	0.332	0.101	0.326	0.129	0.0415	0.0289	0.1	0.0712	0.143	0.141	0.141	0.139	0.564
35.917	4.089	0.408	0.134	0.367	0.178	0.333	0.101	0.327	0.129	0.0416	0.0289	0.1	0.0712	0.143	0.142	0.141	0.14	0.566
36	4.104	0.41	0.134	0.369	0.179	0.334	0.101	0.328	0.13	0.0416	0.0289	0.1	0.0712	0.144	0.142	0.142	0.14	0.568
36.083	4.119	0.411	0.135	0.37	0.179	0.335	0.102	0.329	0.13	0.0417	0.0289	0.1	0.0712	0.144	0.143	0.142	0.141	0.57
36.167	4.135	0.413	0.135	0.371	0.18	0.336	0.102	0.331	0.131	0.0418	0.029	0.1	0.0712	0.145	0.143	0.143	0.141	0.572
36.25	4.15	0.414	0.136	0.372	0.181	0.337	0.102	0.332	0.131	0.0418	0.029	0.1	0.0712	0.145	0.144	0.143	0.142	0.574
36.333	4.166	0.415	0.136	0.373	0.181	0.338	0.103	0.333	0.132	0.042	0.029	0.1	0.0714	0.146	0.144	0.144	0.142	0.576

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
36.417	4.181	0.417	0.136	0.375	0.182	0.339	0.103	0.335	0.132	0.0421	0.0291	0.1	0.0717	0.146	0.145	0.144	0.143	0.578
36.5	4.197	0.418	0.137	0.376	0.183	0.34	0.103	0.336	0.133	0.0422	0.0292	0.1	0.072	0.147	0.145	0.145	0.143	0.58
36.583	4.213	0.42	0.137	0.377	0.183	0.342	0.104	0.337	0.133	0.0424	0.0294	0.1	0.0728	0.147	0.146	0.145	0.144	0.582
36.667	4.228	0.421	0.138	0.379	0.184	0.343	0.104	0.339	0.134	0.0426	0.0297	0.1	0.0736	0.148	0.146	0.146	0.144	0.584
36.75	4.244	0.423	0.139	0.38	0.185	0.344	0.105	0.34	0.134	0.0428	0.0299	0.1	0.0745	0.148	0.147	0.146	0.145	0.586
36.833	4.26	0.424	0.139	0.381	0.185	0.345	0.105	0.342	0.135	0.0431	0.0303	0.101	0.076	0.149	0.147	0.147	0.145	0.588
36.917	4.276	0.426	0.14	0.383	0.186	0.346	0.105	0.343	0.135	0.0435	0.0307	0.102	0.0775	0.149	0.148	0.147	0.146	0.59
37	4.292	0.428	0.141	0.384	0.187	0.348	0.106	0.345	0.136	0.0438	0.0311	0.102	0.0789	0.15	0.149	0.148	0.146	0.593
37.083	4.308	0.43	0.141	0.386	0.188	0.349	0.106	0.347	0.137	0.0442	0.0317	0.104	0.0805	0.151	0.149	0.149	0.147	0.596
37.167	4.324	0.431	0.142	0.387	0.189	0.35	0.107	0.348	0.137	0.0447	0.0322	0.105	0.082	0.151	0.15	0.149	0.147	0.597
37.25	4.34	0.433	0.143	0.389	0.189	0.352	0.107	0.35	0.138	0.0451	0.0328	0.106	0.0836	0.152	0.15	0.15	0.148	0.6
37.333	4.356	0.435	0.144	0.39	0.19	0.353	0.108	0.352	0.139	0.0456	0.0333	0.108	0.0848	0.152	0.151	0.15	0.149	0.602
37.417	4.372	0.437	0.145	0.392	0.191	0.355	0.108	0.354	0.139	0.0462	0.0338	0.109	0.086	0.153	0.152	0.151	0.149	0.605
37.5	4.388	0.439	0.146	0.393	0.192	0.356	0.108	0.356	0.14	0.0467	0.0343	0.111	0.0872	0.154	0.152	0.152	0.15	0.608
37.583	4.404	0.441	0.147	0.395	0.193	0.357	0.109	0.358	0.141	0.0473	0.0347	0.112	0.0881	0.154	0.153	0.152	0.151	0.61
37.667	4.42	0.443	0.148	0.397	0.194	0.359	0.109	0.359	0.141	0.0479	0.0352	0.113	0.089	0.155	0.153	0.153	0.151	0.612
37.75	4.437	0.445	0.149	0.398	0.195	0.36	0.11	0.361	0.142	0.0485	0.0356	0.115	0.0898	0.156	0.154	0.154	0.152	0.616
37.833	4.453	0.447	0.15	0.4	0.196	0.362	0.111	0.363	0.143	0.049	0.0359	0.116	0.0905	0.156	0.155	0.154	0.153	0.618
37.917	4.469	0.449	0.152	0.402	0.197	0.363	0.111	0.365	0.144	0.0495	0.0362	0.117	0.0911	0.157	0.156	0.155	0.153	0.621
38	4.486	0.451	0.153	0.404	0.198	0.365	0.112	0.368	0.144	0.05	0.0365	0.118	0.0917	0.158	0.156	0.156	0.154	0.624
38.083	4.502	0.453	0.154	0.406	0.199	0.366	0.112	0.37	0.145	0.0505	0.0367	0.119	0.0922	0.158	0.157	0.156	0.155	0.626
38.167	4.519	0.456	0.156	0.407	0.2	0.368	0.113	0.372	0.146	0.0509	0.0369	0.12	0.0926	0.159	0.158	0.157	0.155	0.629
38.25	4.535	0.458	0.157	0.409	0.2	0.369	0.113	0.374	0.147	0.0513	0.0372	0.121	0.0931	0.16	0.158	0.158	0.156	0.632
38.333	4.552	0.46	0.159	0.411	0.202	0.371	0.114	0.376	0.147	0.0517	0.0373	0.122	0.0934	0.161	0.159	0.159	0.157	0.636
38.417	4.569	0.462	0.16	0.413	0.203	0.372	0.114	0.379	0.148	0.0521	0.0375	0.123	0.0936	0.161	0.16	0.159	0.158	0.638
38.5	4.586	0.465	0.162	0.415	0.204	0.374	0.115	0.381	0.149	0.0524	0.0377	0.123	0.0939	0.162	0.161	0.16	0.159	0.642
38.583	4.603	0.467	0.163	0.417	0.205	0.376	0.116	0.383	0.15	0.0527	0.0378	0.124	0.094	0.163	0.162	0.161	0.159	0.645
38.667	4.619	0.469	0.164	0.419	0.206	0.377	0.116	0.386	0.151	0.053	0.038	0.125	0.0941	0.164	0.162	0.162	0.16	0.648
38.75	4.636	0.472	0.166	0.421	0.207	0.379	0.117	0.388	0.151	0.0533	0.0381	0.125	0.0943	0.165	0.163	0.163	0.161	0.652
38.833	4.654	0.474	0.167	0.423	0.208	0.381	0.117	0.391	0.152	0.0536	0.0382	0.126	0.0943	0.165	0.164	0.163	0.162	0.654
38.917	4.671	0.476	0.168	0.425	0.209	0.382	0.118	0.393	0.153	0.0538	0.0383	0.126	0.0943	0.166	0.165	0.164	0.163	0.658
39	4.688	0.479	0.17	0.427	0.21	0.384	0.118	0.396	0.154	0.0541	0.0384	0.127	0.0943	0.167	0.166	0.165	0.163	0.661
39.083	4.705	0.481	0.171	0.429	0.211	0.386	0.119	0.399	0.155	0.0543	0.0384	0.127	0.0943	0.168	0.166	0.166	0.164	0.664
39.167	4.722	0.484	0.172	0.431	0.212	0.387	0.12	0.401	0.156	0.0545	0.0384	0.128	0.0943	0.169	0.167	0.167	0.165	0.668
39.25	4.74	0.486	0.173	0.433	0.213	0.389	0.12	0.404	0.157	0.0547	0.0385	0.128	0.0943	0.169	0.168	0.168	0.166	0.671
39.333	4.757	0.489	0.174	0.436	0.215	0.391	0.121	0.407	0.157	0.0549	0.0385	0.128	0.0945	0.17	0.169	0.168	0.167	0.674
39.417	4.775	0.491	0.175	0.438	0.216	0.393	0.121	0.41	0.158	0.0551	0.0386	0.129	0.0946	0.171	0.17	0.169	0.168	0.678
39.5	4.792	0.494	0.176	0.44	0.217	0.395	0.122	0.413	0.159	0.0553	0.0386	0.129	0.0948	0.172	0.171	0.17	0.168	0.681
39.583	4.81	0.497	0.177	0.442	0.218	0.396	0.123	0.415	0.16	0.0556	0.0388	0.13	0.0953	0.173	0.171	0.171	0.169	0.684
39.667	4.828	0.499	0.178	0.444	0.219	0.398	0.123	0.418	0.161	0.0558	0.0389	0.13	0.0958	0.174	0.172	0.172	0.17	0.688
39.75	4.846	0.502	0.179	0.447	0.221	0.4	0.124	0.421	0.162	0.056	0.0391	0.131	0.0963	0.175	0.173	0.173	0.171	0.692
39.833	4.863	0.505	0.18	0.449	0.222	0.402	0.125	0.424	0.163	0.0563	0.0393	0.131	0.0973	0.176	0.174	0.174	0.172	0.696
39.917	4.881	0.508	0.182	0.451	0.223	0.404	0.125	0.427	0.164	0.0566	0.0396	0.132	0.0982	0.177	0.175	0.175	0.173	0.7
40	4.899	0.51	0.183	0.454	0.224	0.406	0.126	0.43	0.166	0.0569	0.0399	0.133	0.0992	0.177	0.176	0.176	0.174	0.703
40.083	4.917	0.513	0.184	0.456	0.226	0.408	0.127	0.433	0.167	0.0573	0.0402	0.134	0.1	0.178	0.177	0.177	0.175	0.707
40.167	4.936	0.516	0.185	0.459	0.227	0.41	0.128	0.436	0.168	0.0576	0.0406	0.134	0.101	0.179	0.178	0.178	0.176	0.711
40.25	4.954	0.519	0.186	0.461	0.229	0.412	0.128	0.438	0.169	0.058	0.0409	0.135	0.102	0.18	0.179	0.178	0.177	0.714
40.333	4.972	0.522	0.187	0.464	0.23	0.414	0.129	0.441	0.17	0.0584	0.0413	0.136	0.103	0.181	0.18	0.18	0.178	0.719
40.417	4.99	0.526	0.188	0.466	0.231	0.416	0.13	0.444	0.171	0.0588	0.0416	0.137	0.104	0.182	0.181	0.181	0.179	0.723
40.5	5.009	0.529	0.189	0.469	0.233	0.419	0.131	0.447	0.172	0.0592	0.042	0.138	0.105	0.183	0.182	0.182	0.18	0.727
40.583	5.027	0.532	0.19	0.471	0.234	0.421	0.131	0.45	0.173	0.0596	0.0423	0.139	0.105	0.185	0.183	0.183	0.181	0.732
40.667	5.046	0.535	0.191	0.474	0.236	0.423	0.132	0.453	0.174	0.06	0.0425	0.14	0.106	0.186	0.184	0.184	0.182	0.736
40.75	5.064	0.539	0.192	0.477	0.237	0.425	0.133	0.455	0.176	0.0603	0.0428	0.141	0.107	0.187	0.185	0.185	0.183	0.74
40.833	5.083	0.542	0.194	0.48	0.239	0.427	0.134	0.458	0.177	0.0607	0.043	0.142	0.107	0.188	0.186	0.186	0.184	0.744
40.917	5.102	0.545	0.195	0.482	0.24	0.43	0.135	0.461	0.178	0.0611	0.0432	0.143	0.107	0.189	0.187	0.187	0.185	0.748
41	5.121	0.549	0.196	0.485	0.242	0.432	0.135	0.464	0.179	0.0614	0.0434	0.143	0.108	0.19	0.189	0.188	0.186	0.753
41.083	5.14	0.552	0.197	0.488	0.244	0.434	0.136	0.467	0.18	0.0617	0.0436	0.144	0.108	0.191	0.19	0.189	0.188	0.758
41.167	5.158	0.556	0.198	0.491	0.245	0.436	0.137	0.469	0.181	0.062	0.0438	0.145	0.109	0.192	0.191	0.19	0.189	0.762
41.25	5.177	0.559	0.2	0.494	0.247	0.439	0.138	0.472	0.182	0.0623	0.0439	0.145	0.109	0.193	0.192	0.191	0.19	0.766
41.333	5.197	0.563	0.201	0.497	0.248	0.441	0.139	0.475	0.183	0.0626	0.044	0.146	0.109	0.195	0.193	0.193	0.191	0.772
41.417	5.216	0.566	0.202	0.5	0.25	0.443	0.14	0.478	0.184	0.0628	0.0442	0.146	0.109	0.196	0.194	0.194	0.192	0.776
41.5	5.235	0.569	0.204	0.503	0.251	0.446	0.141	0.481	0.185	0.0631	0.0443	0.147	0.109	0.197	0.196	0.195	0.193	0.781
41.583	5.254	0.573	0.205	0.506	0.252	0.448	0.142	0.483	0.186	0.0633	0.0444	0.147	0.11	0.198	0.197	0.196	0.195	0.786

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
41.667	5.274	0.576	0.206	0.509	0.254	0.45	0.142	0.486	0.188	0.0635	0.0445	0.148	0.11	0.199	0.198	0.197	0.196	0.79
41.75	5.293	0.58	0.207	0.512	0.255	0.453	0.143	0.489	0.189	0.0637	0.0446	0.148	0.11	0.201	0.199	0.199	0.197	0.796
41.833	5.313	0.583	0.208	0.515	0.257	0.455	0.144	0.492	0.19	0.0638	0.0446	0.148	0.11	0.202	0.2	0.2	0.198	0.8
41.917	5.332	0.586	0.209	0.518	0.258	0.458	0.145	0.494	0.191	0.064	0.0447	0.149	0.11	0.203	0.202	0.201	0.199	0.805
42	5.352	0.59	0.211	0.521	0.26	0.46	0.146	0.497	0.192	0.0642	0.0447	0.149	0.11	0.204	0.203	0.202	0.201	0.81
42.083	5.372	0.593	0.212	0.524	0.261	0.462	0.147	0.5	0.193	0.0643	0.0448	0.149	0.11	0.205	0.204	0.203	0.202	0.814
42.167	5.392	0.596	0.212	0.527	0.263	0.465	0.147	0.503	0.194	0.0644	0.0448	0.15	0.11	0.206	0.205	0.205	0.203	0.819
42.25	5.411	0.6	0.213	0.53	0.264	0.467	0.148	0.505	0.195	0.0646	0.0448	0.15	0.11	0.208	0.206	0.206	0.204	0.824
42.333	5.431	0.603	0.214	0.533	0.266	0.47	0.149	0.508	0.196	0.0647	0.0448	0.15	0.11	0.209	0.207	0.207	0.205	0.828
42.417	5.452	0.606	0.215	0.536	0.267	0.473	0.15	0.511	0.197	0.0648	0.0449	0.15	0.11	0.21	0.209	0.208	0.206	0.833
42.5	5.472	0.609	0.216	0.539	0.268	0.475	0.151	0.514	0.198	0.065	0.0449	0.151	0.11	0.211	0.21	0.209	0.208	0.838
42.583	5.492	0.613	0.217	0.542	0.27	0.478	0.151	0.516	0.199	0.0651	0.045	0.151	0.11	0.212	0.211	0.21	0.209	0.842
42.667	5.512	0.616	0.218	0.545	0.271	0.48	0.152	0.519	0.2	0.0653	0.045	0.151	0.11	0.213	0.212	0.212	0.21	0.847
42.75	5.532	0.619	0.219	0.547	0.273	0.483	0.153	0.522	0.201	0.0654	0.0451	0.152	0.111	0.215	0.213	0.213	0.211	0.852
42.833	5.553	0.623	0.219	0.55	0.274	0.486	0.154	0.524	0.203	0.0656	0.0452	0.152	0.111	0.216	0.214	0.214	0.212	0.856
42.917	5.573	0.626	0.22	0.553	0.276	0.488	0.155	0.527	0.204	0.0657	0.0453	0.152	0.112	0.217	0.216	0.215	0.213	0.861
43	5.594	0.629	0.221	0.556	0.277	0.491	0.156	0.53	0.205	0.0659	0.0455	0.153	0.112	0.218	0.217	0.216	0.215	0.866
43.083	5.615	0.633	0.222	0.559	0.279	0.494	0.156	0.532	0.206	0.0661	0.0457	0.153	0.113	0.219	0.218	0.217	0.216	0.87
43.167	5.635	0.636	0.222	0.562	0.28	0.497	0.157	0.535	0.207	0.0663	0.0458	0.153	0.113	0.22	0.219	0.219	0.217	0.875
43.25	5.656	0.639	0.223	0.565	0.282	0.499	0.158	0.537	0.208	0.0665	0.046	0.154	0.114	0.222	0.22	0.22	0.218	0.88
43.333	5.677	0.643	0.224	0.568	0.283	0.502	0.159	0.54	0.209	0.0667	0.0462	0.154	0.114	0.223	0.221	0.221	0.219	0.884
43.417	5.698	0.646	0.224	0.571	0.284	0.505	0.16	0.542	0.21	0.0669	0.0464	0.155	0.114	0.224	0.223	0.222	0.22	0.889
43.5	5.719	0.649	0.225	0.574	0.286	0.508	0.161	0.545	0.211	0.0671	0.0465	0.155	0.115	0.225	0.224	0.223	0.222	0.894
43.583	5.74	0.653	0.226	0.577	0.287	0.51	0.161	0.547	0.212	0.0673	0.0467	0.156	0.115	0.226	0.225	0.224	0.223	0.898
43.667	5.761	0.656	0.226	0.58	0.289	0.513	0.162	0.55	0.213	0.0675	0.0468	0.156	0.115	0.227	0.226	0.226	0.224	0.903
43.75	5.783	0.659	0.227	0.583	0.29	0.516	0.163	0.552	0.214	0.0677	0.047	0.157	0.116	0.229	0.227	0.227	0.225	0.908
43.833	5.804	0.663	0.228	0.586	0.292	0.519	0.164	0.554	0.215	0.0679	0.0471	0.157	0.116	0.23	0.228	0.228	0.226	0.912
43.917	5.825	0.666	0.228	0.589	0.293	0.522	0.165	0.557	0.216	0.068	0.0472	0.158	0.116	0.231	0.23	0.229	0.228	0.918
44	5.847	0.67	0.229	0.592	0.295	0.524	0.166	0.559	0.217	0.0682	0.0473	0.158	0.116	0.232	0.231	0.23	0.229	0.922
44.083	5.869	0.673	0.23	0.595	0.296	0.527	0.166	0.561	0.218	0.0684	0.0474	0.158	0.117	0.233	0.232	0.231	0.23	0.926
44.167	5.89	0.676	0.23	0.598	0.298	0.53	0.167	0.564	0.219	0.0685	0.0474	0.159	0.117	0.234	0.233	0.233	0.231	0.931
44.25	5.912	0.68	0.231	0.601	0.299	0.533	0.168	0.566	0.22	0.0687	0.0475	0.159	0.117	0.236	0.234	0.234	0.232	0.936
44.333	5.934	0.683	0.232	0.604	0.3	0.535	0.169	0.568	0.221	0.0688	0.0476	0.159	0.117	0.237	0.235	0.235	0.233	0.94
44.417	5.956	0.686	0.232	0.607	0.302	0.538	0.17	0.57	0.222	0.0689	0.0477	0.159	0.117	0.238	0.237	0.236	0.235	0.946
44.5	5.978	0.689	0.233	0.61	0.303	0.541	0.171	0.572	0.223	0.0691	0.0477	0.16	0.117	0.239	0.238	0.237	0.236	0.95
44.583	6	0.693	0.234	0.613	0.304	0.544	0.171	0.574	0.224	0.0692	0.0478	0.16	0.117	0.24	0.239	0.239	0.237	0.955
44.667	6.022	0.696	0.235	0.616	0.306	0.546	0.172	0.577	0.225	0.0693	0.0478	0.16	0.117	0.242	0.24	0.24	0.238	0.96
44.75	6.044	0.699	0.235	0.619	0.307	0.549	0.173	0.579	0.226	0.0694	0.0479	0.16	0.117	0.243	0.241	0.241	0.239	0.964
44.833	6.067	0.702	0.236	0.621	0.308	0.552	0.174	0.581	0.227	0.0694	0.0479	0.161	0.117	0.244	0.242	0.242	0.24	0.968
44.917	6.089	0.705	0.236	0.624	0.31	0.554	0.175	0.583	0.227	0.0695	0.0479	0.161	0.117	0.245	0.244	0.243	0.242	0.974
45	6.111	0.708	0.237	0.627	0.311	0.557	0.175	0.585	0.228	0.0696	0.048	0.161	0.117	0.246	0.245	0.244	0.243	0.978
45.083	6.134	0.711	0.238	0.63	0.312	0.56	0.176	0.587	0.229	0.0697	0.048	0.161	0.117	0.247	0.246	0.245	0.244	0.982
45.167	6.157	0.714	0.238	0.633	0.313	0.562	0.177	0.589	0.23	0.0698	0.048	0.161	0.117	0.248	0.247	0.246	0.245	0.986
45.25	6.179	0.717	0.239	0.636	0.315	0.565	0.177	0.591	0.231	0.0698	0.048	0.161	0.117	0.249	0.248	0.248	0.246	0.991
45.333	6.202	0.72	0.239	0.638	0.316	0.568	0.178	0.593	0.232	0.0699	0.048	0.162	0.118	0.25	0.249	0.249	0.247	0.995
45.417	6.225	0.723	0.24	0.641	0.317	0.571	0.179	0.595	0.233	0.07	0.0481	0.162	0.118	0.252	0.25	0.25	0.248	1
45.5	6.248	0.726	0.24	0.644	0.318	0.573	0.18	0.597	0.234	0.0701	0.0481	0.162	0.118	0.253	0.251	0.251	0.249	1.004
45.583	6.271	0.728	0.241	0.646	0.319	0.576	0.18	0.599	0.234	0.0702	0.0482	0.162	0.118	0.254	0.252	0.252	0.25	1.008
45.667	6.295	0.731	0.241	0.649	0.321	0.579	0.181	0.6	0.235	0.0704	0.0484	0.163	0.119	0.255	0.253	0.253	0.251	1.012
45.75	6.318	0.734	0.242	0.652	0.322	0.581	0.182	0.602	0.236	0.0705	0.0485	0.163	0.119	0.256	0.254	0.254	0.252	1.016
45.833	6.341	0.737	0.242	0.654	0.323	0.584	0.183	0.604	0.237	0.0707	0.0487	0.163	0.12	0.257	0.255	0.255	0.254	1.021
45.917	6.365	0.74	0.243	0.657	0.324	0.587	0.183	0.606	0.238	0.0709	0.049	0.164	0.121	0.258	0.257	0.256	0.255	1.026
46	6.388	0.743	0.243	0.66	0.326	0.59	0.184	0.608	0.239	0.0711	0.0492	0.164	0.122	0.259	0.258	0.257	0.256	1.03
46.083	6.412	0.746	0.244	0.662	0.327	0.593	0.185	0.61	0.24	0.0714	0.0495	0.165	0.123	0.26	0.259	0.258	0.257	1.034
46.167	6.435	0.749	0.245	0.665	0.328	0.595	0.185	0.612	0.241	0.0717	0.0499	0.166	0.124	0.261	0.26	0.259	0.258	1.038
46.25	6.459	0.751	0.245	0.668	0.329	0.598	0.186	0.614	0.241	0.0719	0.0502	0.167	0.125	0.262	0.261	0.26	0.259	1.042
46.333	6.483	0.754	0.246	0.67	0.331	0.601	0.187	0.616	0.242	0.0723	0.0506	0.168	0.126	0.263	0.262	0.261	0.26	1.046
46.417	6.507	0.757	0.247	0.673	0.332	0.604	0.188	0.618	0.243	0.0726	0.0509	0.169	0.127	0.264	0.263	0.262	0.261	1.05
46.5	6.531	0.76	0.247	0.676	0.333	0.607	0.188	0.62	0.244	0.073	0.0513	0.17	0.127	0.265	0.264	0.263	0.262	1.054
46.583	6.555	0.763	0.248	0.678	0.334	0.609	0.189	0.622	0.245	0.0734	0.0516	0.17	0.128	0.266	0.265	0.264	0.263	1.058
46.667	6.579	0.766	0.249	0.681	0.336	0.612	0.19	0.624	0.246	0.0738	0.0519	0.171	0.129	0.267	0.266	0.266	0.264	1.063
46.75	6.604	0.769	0.25	0.684	0.337	0.615	0.191	0.626	0.247	0.0742	0.0522	0.172	0.129	0.268	0.267	0.267	0.265	1.067
46.833	6.628	0.772	0.251	0.686	0.338	0.618	0.191	0.628	0.248	0.0745	0.0524	0.173	0.13	0.269	0.268	0.268	0.266	1.071

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
46.917	6.653	0.775	0.251	0.689	0.339	0.62	0.192	0.63	0.249	0.0749	0.0526	0.174	0.13	0.27	0.269	0.269	0.267	1.075
47	6.677	0.778	0.252	0.692	0.341	0.623	0.193	0.632	0.249	0.0752	0.0529	0.175	0.131	0.272	0.27	0.27	0.268	1.08
47.083	6.702	0.781	0.253	0.694	0.342	0.626	0.194	0.634	0.25	0.0755	0.053	0.176	0.131	0.273	0.271	0.271	0.269	1.084
47.167	6.727	0.784	0.254	0.697	0.343	0.629	0.194	0.636	0.251	0.0759	0.0532	0.176	0.131	0.274	0.272	0.272	0.27	1.088
47.25	6.751	0.787	0.255	0.7	0.344	0.631	0.195	0.638	0.252	0.0762	0.0533	0.177	0.132	0.275	0.273	0.273	0.271	1.092
47.333	6.776	0.79	0.256	0.702	0.346	0.634	0.196	0.64	0.253	0.0764	0.0535	0.177	0.132	0.276	0.274	0.274	0.272	1.096
47.417	6.801	0.793	0.257	0.705	0.347	0.637	0.196	0.642	0.254	0.0767	0.0536	0.178	0.132	0.277	0.275	0.275	0.274	1.101
47.5	6.826	0.795	0.258	0.708	0.348	0.639	0.197	0.644	0.254	0.0769	0.0537	0.179	0.132	0.278	0.277	0.276	0.275	1.106
47.583	6.852	0.798	0.259	0.71	0.349	0.642	0.198	0.646	0.255	0.0771	0.0538	0.179	0.133	0.279	0.278	0.277	0.276	1.11
47.667	6.877	0.801	0.26	0.713	0.351	0.645	0.199	0.648	0.256	0.0774	0.0539	0.179	0.133	0.28	0.279	0.278	0.277	1.114
47.75	6.902	0.804	0.261	0.716	0.352	0.647	0.199	0.65	0.257	0.0776	0.054	0.18	0.133	0.281	0.28	0.279	0.278	1.118
47.833	6.928	0.807	0.262	0.718	0.353	0.65	0.2	0.652	0.258	0.0777	0.0541	0.18	0.133	0.282	0.281	0.28	0.279	1.122
47.917	6.953	0.81	0.263	0.721	0.354	0.653	0.201	0.654	0.259	0.0779	0.0542	0.181	0.133	0.283	0.282	0.281	0.28	1.126
48	6.979	0.813	0.264	0.724	0.355	0.655	0.202	0.656	0.26	0.0781	0.0542	0.181	0.133	0.284	0.283	0.282	0.281	1.13
48.083	7.005	0.816	0.265	0.726	0.357	0.658	0.202	0.658	0.26	0.0782	0.0543	0.181	0.133	0.285	0.284	0.283	0.282	1.134
48.167	7.031	0.818	0.265	0.729	0.358	0.661	0.203	0.66	0.261	0.0784	0.0543	0.182	0.133	0.286	0.285	0.284	0.283	1.138
48.25	7.057	0.821	0.266	0.732	0.359	0.663	0.204	0.662	0.262	0.0785	0.0543	0.182	0.133	0.287	0.286	0.285	0.284	1.142
48.333	7.083	0.824	0.267	0.734	0.36	0.666	0.204	0.665	0.263	0.0787	0.0544	0.182	0.133	0.288	0.287	0.287	0.285	1.147
48.417	7.109	0.827	0.268	0.737	0.361	0.668	0.205	0.667	0.264	0.0789	0.0545	0.183	0.133	0.289	0.288	0.288	0.286	1.151
48.5	7.135	0.83	0.269	0.739	0.363	0.671	0.206	0.669	0.265	0.079	0.0546	0.183	0.134	0.29	0.289	0.289	0.287	1.155
48.583	7.162	0.833	0.27	0.742	0.364	0.674	0.207	0.671	0.266	0.0793	0.0548	0.184	0.134	0.291	0.29	0.29	0.288	1.159
48.667	7.188	0.836	0.271	0.745	0.365	0.676	0.207	0.674	0.267	0.0796	0.0551	0.184	0.135	0.292	0.291	0.291	0.289	1.163
48.75	7.214	0.839	0.271	0.747	0.367	0.679	0.208	0.676	0.268	0.0799	0.0554	0.185	0.136	0.294	0.292	0.292	0.29	1.168
48.833	7.241	0.842	0.273	0.75	0.368	0.682	0.209	0.679	0.269	0.0804	0.0559	0.186	0.139	0.295	0.293	0.293	0.291	1.172
48.917	7.268	0.845	0.274	0.753	0.369	0.685	0.21	0.682	0.27	0.0809	0.0565	0.188	0.141	0.296	0.294	0.294	0.293	1.177
49	7.295	0.848	0.275	0.756	0.371	0.688	0.21	0.684	0.271	0.0814	0.0571	0.189	0.143	0.297	0.296	0.295	0.294	1.182
49.083	7.322	0.851	0.276	0.759	0.372	0.69	0.211	0.687	0.272	0.082	0.0579	0.191	0.145	0.298	0.297	0.296	0.295	1.186
49.167	7.349	0.855	0.277	0.762	0.374	0.693	0.212	0.69	0.273	0.0827	0.0588	0.192	0.148	0.299	0.298	0.297	0.296	1.19
49.25	7.376	0.858	0.279	0.765	0.375	0.696	0.213	0.693	0.274	0.0834	0.0596	0.194	0.15	0.3	0.299	0.299	0.297	1.195
49.333	7.403	0.861	0.28	0.768	0.377	0.699	0.214	0.696	0.275	0.0842	0.0605	0.197	0.153	0.302	0.3	0.3	0.298	1.2
49.417	7.43	0.865	0.282	0.771	0.378	0.702	0.215	0.699	0.276	0.085	0.0614	0.199	0.155	0.303	0.301	0.301	0.3	1.205
49.5	7.458	0.868	0.283	0.774	0.38	0.705	0.215	0.702	0.278	0.0859	0.0623	0.201	0.157	0.304	0.303	0.302	0.301	1.21
49.583	7.485	0.872	0.285	0.777	0.381	0.708	0.216	0.705	0.279	0.0869	0.0631	0.204	0.159	0.305	0.304	0.304	0.302	1.215
49.667	7.513	0.876	0.287	0.78	0.383	0.711	0.217	0.708	0.28	0.0878	0.0638	0.206	0.161	0.307	0.305	0.305	0.303	1.22
49.75	7.541	0.88	0.289	0.783	0.385	0.714	0.218	0.711	0.281	0.0888	0.0646	0.208	0.162	0.308	0.307	0.306	0.305	1.226
49.833	7.568	0.883	0.291	0.787	0.386	0.717	0.219	0.715	0.282	0.0897	0.0652	0.21	0.164	0.309	0.308	0.307	0.306	1.23
49.917	7.596	0.887	0.293	0.79	0.388	0.72	0.22	0.718	0.284	0.0906	0.0657	0.213	0.165	0.31	0.309	0.309	0.307	1.235
50	7.624	0.891	0.295	0.794	0.39	0.723	0.221	0.721	0.285	0.0915	0.0663	0.215	0.166	0.312	0.31	0.31	0.309	1.241
50.083	7.652	0.895	0.297	0.797	0.391	0.726	0.222	0.725	0.286	0.0923	0.0667	0.216	0.167	0.313	0.312	0.311	0.31	1.246
50.167	7.681	0.899	0.299	0.8	0.393	0.729	0.223	0.728	0.287	0.0931	0.0672	0.218	0.168	0.314	0.313	0.313	0.311	1.251
50.25	7.709	0.903	0.302	0.804	0.395	0.732	0.224	0.732	0.289	0.0939	0.0676	0.22	0.169	0.316	0.315	0.314	0.313	1.258
50.333	7.737	0.907	0.304	0.808	0.397	0.735	0.225	0.736	0.29	0.0945	0.0679	0.221	0.169	0.317	0.316	0.316	0.314	1.263
50.417	7.766	0.911	0.307	0.811	0.399	0.738	0.226	0.74	0.291	0.0952	0.0682	0.223	0.17	0.319	0.317	0.317	0.316	1.269
50.5	7.794	0.916	0.309	0.815	0.4	0.741	0.227	0.743	0.293	0.0958	0.0686	0.224	0.17	0.32	0.319	0.318	0.317	1.274
50.583	7.823	0.92	0.312	0.818	0.402	0.744	0.228	0.747	0.294	0.0964	0.0688	0.225	0.171	0.322	0.32	0.32	0.318	1.28
50.667	7.852	0.924	0.314	0.822	0.404	0.747	0.229	0.751	0.295	0.0969	0.0691	0.226	0.171	0.323	0.322	0.321	0.32	1.286
50.75	7.881	0.928	0.316	0.826	0.406	0.75	0.23	0.755	0.297	0.0975	0.0693	0.227	0.171	0.325	0.323	0.323	0.321	1.292
50.833	7.91	0.932	0.319	0.83	0.408	0.754	0.231	0.76	0.298	0.0979	0.0695	0.228	0.171	0.326	0.325	0.324	0.323	1.298
50.917	7.939	0.937	0.321	0.833	0.41	0.757	0.233	0.764	0.3	0.0984	0.0697	0.229	0.171	0.328	0.326	0.326	0.324	1.304
51	7.968	0.941	0.323	0.837	0.412	0.76	0.234	0.768	0.301	0.0988	0.0699	0.23	0.171	0.329	0.328	0.327	0.326	1.31
51.083	7.998	0.945	0.325	0.841	0.413	0.763	0.235	0.772	0.302	0.0992	0.07	0.231	0.171	0.331	0.329	0.329	0.327	1.316
51.167	8.027	0.95	0.327	0.845	0.415	0.766	0.236	0.777	0.304	0.0995	0.0701	0.232	0.171	0.332	0.331	0.33	0.329	1.322
51.25	8.057	0.954	0.329	0.849	0.417	0.77	0.237	0.781	0.305	0.0999	0.0702	0.232	0.171	0.334	0.332	0.332	0.33	1.328
51.333	8.087	0.958	0.331	0.852	0.419	0.773	0.238	0.786	0.307	0.1	0.0702	0.233	0.171	0.335	0.334	0.333	0.332	1.334
51.417	8.116	0.963	0.333	0.856	0.421	0.776	0.239	0.79	0.308	0.101	0.0702	0.234	0.171	0.337	0.335	0.335	0.334	1.341
51.5	8.146	0.967	0.335	0.86	0.423	0.779	0.24	0.795	0.31	0.101	0.0702	0.234	0.171	0.338	0.337	0.336	0.335	1.346
51.583	8.176	0.972	0.336	0.864	0.425	0.783	0.241	0.8	0.312	0.101	0.0702	0.235	0.171	0.34	0.338	0.338	0.337	1.353
51.667	8.206	0.976	0.338	0.868	0.427	0.786	0.242	0.804	0.313	0.101	0.0702	0.235	0.171	0.341	0.34	0.34	0.338	1.359
51.75	8.236	0.981	0.34	0.872	0.429	0.789	0.243	0.809	0.315	0.102	0.0702	0.236	0.171	0.343	0.342	0.341	0.34	1.366
51.833	8.267	0.985	0.341	0.876	0.431	0.793	0.245	0.814	0.316	0.102	0.0702	0.236	0.171	0.344	0.343	0.343	0.341	1.371
51.917	8.297	0.99	0.342	0.88	0.433	0.796	0.246	0.818	0.318	0.102	0.0702	0.236	0.171	0.346	0.345	0.344	0.343	1.378
52	8.328	0.994	0.344	0.884	0.435	0.799	0.247	0.822	0.32	0.102	0.0702	0.236	0.171	0.347	0.346	0.346	0.344	1.383
52.083	8.358	0.999	0.345	0.888	0.437	0.803	0.248	0.827	0.321	0.102	0.0702	0.237	0.171	0.349	0.348	0.347	0.346	1.39

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
52.167	8.389	1.003	0.346	0.892	0.439	0.806	0.249	0.831	0.323	0.103	0.0702	0.237	0.171	0.351	0.349	0.349	0.348	1.397
52.25	8.42	1.008	0.348	0.896	0.441	0.81	0.25	0.835	0.325	0.103	0.0702	0.237	0.171	0.352	0.351	0.351	0.349	1.403
52.333	8.451	1.013	0.349	0.9	0.444	0.813	0.251	0.839	0.326	0.103	0.0702	0.237	0.171	0.354	0.353	0.352	0.351	1.41
52.417	8.482	1.018	0.35	0.904	0.446	0.817	0.253	0.843	0.328	0.103	0.0702	0.237	0.171	0.355	0.354	0.354	0.352	1.415
52.5	8.513	1.022	0.351	0.908	0.448	0.82	0.254	0.847	0.33	0.103	0.0702	0.237	0.171	0.357	0.356	0.355	0.354	1.422
52.583	8.545	1.027	0.352	0.912	0.45	0.824	0.255	0.851	0.331	0.103	0.0702	0.237	0.171	0.359	0.358	0.357	0.356	1.43
52.667	8.576	1.032	0.353	0.916	0.452	0.827	0.256	0.855	0.333	0.103	0.0702	0.237	0.171	0.36	0.359	0.359	0.357	1.435
52.75	8.607	1.037	0.354	0.92	0.454	0.83	0.257	0.858	0.334	0.103	0.0702	0.237	0.171	0.362	0.361	0.36	0.359	1.442
52.833	8.639	1.042	0.354	0.925	0.457	0.834	0.258	0.862	0.336	0.103	0.0702	0.237	0.171	0.364	0.362	0.362	0.361	1.449
52.917	8.671	1.047	0.355	0.929	0.459	0.837	0.26	0.865	0.337	0.103	0.0702	0.237	0.171	0.365	0.364	0.364	0.362	1.455
53	8.703	1.052	0.356	0.933	0.461	0.841	0.261	0.869	0.339	0.103	0.0702	0.237	0.171	0.367	0.366	0.365	0.364	1.462
53.083	8.735	1.056	0.357	0.937	0.463	0.844	0.262	0.872	0.34	0.103	0.0702	0.237	0.171	0.369	0.367	0.367	0.366	1.469
53.167	8.767	1.061	0.358	0.942	0.465	0.848	0.263	0.876	0.342	0.103	0.0702	0.237	0.171	0.37	0.369	0.369	0.367	1.475
53.25	8.799	1.066	0.358	0.946	0.467	0.851	0.264	0.879	0.343	0.103	0.0702	0.237	0.171	0.372	0.371	0.37	0.369	1.482
53.333	8.831	1.071	0.359	0.95	0.469	0.855	0.266	0.882	0.345	0.103	0.0702	0.237	0.171	0.374	0.373	0.372	0.371	1.49
53.417	8.864	1.076	0.36	0.955	0.471	0.858	0.267	0.885	0.346	0.103	0.0702	0.237	0.171	0.375	0.374	0.374	0.373	1.496
53.5	8.896	1.08	0.36	0.959	0.473	0.862	0.268	0.888	0.347	0.103	0.0702	0.237	0.171	0.377	0.376	0.376	0.374	1.503
53.583	8.929	1.085	0.361	0.963	0.475	0.865	0.269	0.891	0.349	0.103	0.0702	0.237	0.171	0.379	0.378	0.377	0.376	1.51
53.667	8.962	1.09	0.362	0.967	0.477	0.869	0.27	0.894	0.35	0.103	0.0702	0.237	0.171	0.381	0.379	0.379	0.378	1.517
53.75	8.995	1.094	0.362	0.972	0.479	0.872	0.272	0.896	0.351	0.103	0.0702	0.237	0.171	0.382	0.381	0.381	0.379	1.523
53.833	9.028	1.098	0.363	0.976	0.481	0.875	0.273	0.899	0.352	0.103	0.0702	0.237	0.171	0.384	0.383	0.382	0.381	1.53
53.917	9.061	1.103	0.363	0.98	0.483	0.879	0.274	0.902	0.354	0.103	0.0702	0.237	0.171	0.385	0.384	0.384	0.383	1.536
54	9.094	1.107	0.364	0.984	0.484	0.882	0.275	0.904	0.355	0.103	0.0702	0.237	0.171	0.387	0.386	0.385	0.384	1.542
54.083	9.127	1.111	0.364	0.988	0.486	0.886	0.276	0.907	0.356	0.103	0.0702	0.237	0.171	0.389	0.387	0.387	0.386	1.549
54.167	9.161	1.116	0.365	0.992	0.488	0.889	0.277	0.909	0.357	0.103	0.0702	0.237	0.171	0.39	0.389	0.389	0.387	1.555
54.25	9.194	1.12	0.365	0.996	0.49	0.893	0.278	0.911	0.358	0.103	0.0702	0.237	0.171	0.392	0.391	0.39	0.389	1.562
54.333	9.228	1.124	0.366	1	0.491	0.896	0.279	0.914	0.359	0.103	0.0703	0.237	0.171	0.393	0.392	0.392	0.39	1.567
54.417	9.262	1.128	0.366	1.004	0.493	0.9	0.28	0.916	0.361	0.103	0.0703	0.237	0.172	0.395	0.394	0.393	0.392	1.574
54.5	9.296	1.132	0.366	1.007	0.495	0.903	0.281	0.918	0.362	0.103	0.0703	0.237	0.172	0.396	0.395	0.395	0.393	1.579
54.583	9.33	1.136	0.367	1.011	0.496	0.907	0.282	0.92	0.363	0.103	0.0704	0.237	0.172	0.398	0.396	0.396	0.395	1.585
54.667	9.364	1.139	0.367	1.015	0.498	0.91	0.283	0.922	0.364	0.103	0.0705	0.237	0.172	0.399	0.398	0.398	0.396	1.591
54.75	9.398	1.143	0.368	1.018	0.499	0.914	0.284	0.924	0.365	0.103	0.0705	0.237	0.172	0.401	0.399	0.399	0.398	1.597
54.833	9.433	1.147	0.368	1.022	0.501	0.917	0.285	0.926	0.366	0.104	0.0707	0.238	0.173	0.402	0.401	0.4	0.399	1.602
54.917	9.467	1.151	0.368	1.025	0.503	0.921	0.286	0.928	0.367	0.104	0.0709	0.238	0.174	0.403	0.402	0.402	0.401	1.608
55	9.502	1.155	0.369	1.029	0.504	0.925	0.287	0.93	0.368	0.104	0.0711	0.239	0.175	0.405	0.404	0.403	0.402	1.614
55.083	9.537	1.158	0.369	1.033	0.506	0.928	0.288	0.932	0.369	0.104	0.0715	0.239	0.176	0.406	0.405	0.405	0.403	1.619
55.167	9.572	1.162	0.37	1.036	0.507	0.932	0.289	0.934	0.37	0.104	0.0718	0.24	0.177	0.408	0.406	0.406	0.405	1.625
55.25	9.607	1.166	0.37	1.04	0.509	0.936	0.29	0.936	0.371	0.104	0.0721	0.241	0.178	0.409	0.408	0.407	0.406	1.63
55.333	9.642	1.169	0.371	1.043	0.51	0.939	0.291	0.938	0.372	0.105	0.0725	0.242	0.179	0.41	0.409	0.409	0.407	1.635
55.417	9.677	1.173	0.371	1.046	0.512	0.943	0.291	0.94	0.373	0.105	0.0729	0.242	0.18	0.412	0.41	0.41	0.409	1.641
55.5	9.712	1.176	0.372	1.05	0.513	0.947	0.292	0.942	0.374	0.105	0.0732	0.243	0.181	0.413	0.412	0.411	0.41	1.646
55.583	9.748	1.18	0.372	1.053	0.514	0.95	0.293	0.944	0.375	0.106	0.0735	0.244	0.181	0.414	0.413	0.413	0.411	1.651
55.667	9.784	1.183	0.373	1.056	0.516	0.954	0.294	0.947	0.376	0.106	0.0739	0.245	0.182	0.416	0.414	0.414	0.413	1.657
55.75	9.819	1.187	0.374	1.06	0.517	0.958	0.295	0.949	0.377	0.107	0.0742	0.246	0.183	0.417	0.416	0.415	0.414	1.662
55.833	9.855	1.19	0.374	1.063	0.519	0.961	0.296	0.951	0.378	0.107	0.0744	0.247	0.183	0.418	0.417	0.417	0.415	1.667
55.917	9.891	1.194	0.375	1.066	0.52	0.965	0.297	0.953	0.379	0.107	0.0747	0.248	0.184	0.419	0.418	0.418	0.417	1.672
56	9.927	1.197	0.376	1.07	0.522	0.969	0.298	0.955	0.38	0.108	0.0749	0.249	0.184	0.421	0.42	0.419	0.418	1.678
56.083	9.964	1.2	0.376	1.073	0.523	0.972	0.298	0.957	0.381	0.108	0.0751	0.25	0.185	0.422	0.421	0.42	0.419	1.682
56.167	10	1.204	0.377	1.076	0.524	0.976	0.299	0.959	0.382	0.108	0.0753	0.25	0.185	0.423	0.422	0.422	0.42	1.687
56.25	10.036	1.207	0.378	1.079	0.526	0.979	0.3	0.961	0.382	0.109	0.0754	0.251	0.186	0.425	0.423	0.423	0.422	1.693
56.333	10.073	1.21	0.379	1.082	0.527	0.983	0.301	0.963	0.383	0.109	0.0756	0.252	0.186	0.426	0.425	0.424	0.423	1.698
56.417	10.11	1.214	0.38	1.085	0.528	0.986	0.302	0.965	0.384	0.109	0.0757	0.252	0.186	0.427	0.426	0.425	0.424	1.702
56.5	10.146	1.217	0.38	1.089	0.53	0.989	0.303	0.967	0.385	0.109	0.0759	0.253	0.186	0.428	0.427	0.427	0.425	1.707
56.583	10.184	1.22	0.381	1.092	0.531	0.993	0.303	0.969	0.386	0.11	0.076	0.253	0.186	0.429	0.428	0.428	0.427	1.712
56.667	10.221	1.223	0.382	1.095	0.532	0.996	0.304	0.972	0.387	0.11	0.0761	0.254	0.187	0.431	0.429	0.429	0.428	1.717
56.75	10.258	1.226	0.383	1.098	0.534	0.999	0.305	0.974	0.388	0.11	0.0762	0.254	0.187	0.432	0.431	0.43	0.429	1.722
56.833	10.295	1.23	0.384	1.101	0.535	1.003	0.306	0.976	0.389	0.11	0.0763	0.255	0.187	0.433	0.432	0.431	0.43	1.726
56.917	10.333	1.233	0.385	1.104	0.536	1.006	0.307	0.978	0.39	0.111	0.0763	0.255	0.187	0.434	0.433	0.433	0.431	1.731
57	10.37	1.236	0.386	1.107	0.538	1.009	0.307	0.98	0.39	0.111	0.0764	0.255	0.187	0.435	0.434	0.434	0.433	1.736
57.083	10.408	1.239	0.386	1.11	0.539	1.013	0.308	0.982	0.391	0.111	0.0765	0.256	0.187	0.437	0.435	0.435	0.434	1.741
57.167	10.446	1.242	0.387	1.113	0.54	1.016	0.309	0.984	0.392	0.111	0.0765	0.256	0.187	0.438	0.437	0.436	0.435	1.746
57.25	10.484	1.245	0.388	1.116	0.541	1.019	0.31	0.987	0.393	0.111	0.0765	0.256	0.187	0.439	0.438	0.437	0.436	1.75
57.333	10.522	1.248	0.389	1.118	0.543	1.022	0.311	0.989	0.394	0.111	0.0766	0.257	0.187	0.44	0.439	0.438	0.437	1.754

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
57.417	10.56	1.251	0.389	1.121	0.544	1.025	0.311	0.991	0.395	0.111	0.0766	0.257	0.187	0.441	0.44	0.44	0.438	1.759
57.5	10.599	1.254	0.39	1.124	0.545	1.028	0.312	0.993	0.396	0.112	0.0766	0.257	0.187	0.442	0.441	0.441	0.439	1.763
57.583	10.637	1.257	0.391	1.127	0.547	1.031	0.313	0.996	0.397	0.112	0.0767	0.257	0.187	0.443	0.442	0.442	0.441	1.768
57.667	10.676	1.26	0.391	1.13	0.548	1.035	0.314	0.998	0.398	0.112	0.0768	0.258	0.187	0.444	0.443	0.443	0.442	1.772
57.75	10.714	1.263	0.392	1.133	0.549	1.038	0.314	1	0.399	0.112	0.0768	0.258	0.188	0.446	0.444	0.444	0.443	1.777
57.833	10.753	1.266	0.393	1.135	0.55	1.041	0.315	1.003	0.4	0.112	0.077	0.259	0.188	0.447	0.446	0.445	0.444	1.782
57.917	10.792	1.269	0.393	1.138	0.552	1.044	0.316	1.005	0.401	0.112	0.0772	0.259	0.189	0.448	0.447	0.446	0.445	1.786
58	10.832	1.272	0.394	1.141	0.553	1.047	0.317	1.007	0.402	0.113	0.0774	0.26	0.19	0.449	0.448	0.447	0.446	1.79
58.083	10.871	1.275	0.395	1.144	0.554	1.05	0.317	1.009	0.403	0.113	0.0777	0.26	0.191	0.45	0.449	0.449	0.447	1.795
58.167	10.91	1.278	0.396	1.147	0.556	1.053	0.318	1.012	0.404	0.113	0.078	0.261	0.192	0.451	0.45	0.45	0.449	1.8
58.25	10.95	1.281	0.397	1.15	0.557	1.056	0.319	1.014	0.405	0.114	0.0783	0.262	0.193	0.452	0.451	0.451	0.45	1.804
58.333	10.99	1.285	0.397	1.153	0.559	1.059	0.32	1.016	0.406	0.114	0.0787	0.263	0.194	0.454	0.452	0.452	0.451	1.809
58.417	11.029	1.288	0.398	1.155	0.56	1.062	0.32	1.018	0.407	0.114	0.0791	0.263	0.195	0.455	0.453	0.453	0.452	1.813
58.5	11.069	1.291	0.399	1.158	0.561	1.065	0.321	1.021	0.408	0.115	0.0795	0.264	0.196	0.456	0.455	0.454	0.453	1.818
58.583	11.109	1.294	0.4	1.161	0.563	1.068	0.322	1.023	0.409	0.115	0.0798	0.265	0.197	0.457	0.456	0.455	0.454	1.822
58.667	11.149	1.298	0.401	1.164	0.564	1.071	0.323	1.025	0.41	0.115	0.0801	0.266	0.197	0.458	0.457	0.457	0.455	1.827
58.75	11.19	1.301	0.402	1.167	0.566	1.074	0.324	1.027	0.411	0.116	0.0804	0.267	0.198	0.459	0.458	0.458	0.457	1.832
58.833	11.23	1.304	0.403	1.17	0.567	1.077	0.325	1.03	0.412	0.116	0.0807	0.268	0.199	0.46	0.459	0.459	0.458	1.836
58.917	11.271	1.307	0.404	1.173	0.569	1.08	0.325	1.032	0.413	0.117	0.081	0.269	0.199	0.462	0.46	0.46	0.459	1.841
59	11.311	1.311	0.405	1.176	0.57	1.083	0.326	1.034	0.414	0.117	0.0812	0.27	0.2	0.463	0.462	0.461	0.46	1.846
59.083	11.352	1.314	0.406	1.179	0.571	1.086	0.327	1.036	0.415	0.117	0.0814	0.271	0.2	0.464	0.463	0.462	0.461	1.85
59.167	11.393	1.318	0.407	1.182	0.573	1.089	0.328	1.038	0.416	0.118	0.0816	0.271	0.2	0.465	0.464	0.463	0.462	1.854
59.25	11.434	1.321	0.408	1.185	0.574	1.092	0.329	1.04	0.417	0.118	0.0818	0.272	0.201	0.466	0.465	0.465	0.464	1.86
59.333	11.476	1.324	0.409	1.188	0.576	1.095	0.33	1.042	0.418	0.118	0.0819	0.273	0.201	0.467	0.466	0.466	0.465	1.864
59.417	11.517	1.328	0.41	1.191	0.577	1.098	0.33	1.044	0.419	0.118	0.082	0.273	0.201	0.469	0.467	0.467	0.466	1.869
59.5	11.559	1.331	0.411	1.194	0.579	1.101	0.331	1.047	0.42	0.119	0.0822	0.274	0.202	0.47	0.469	0.468	0.467	1.874
59.583	11.6	1.334	0.412	1.197	0.58	1.104	0.332	1.049	0.421	0.119	0.0823	0.275	0.202	0.471	0.47	0.469	0.468	1.878
59.667	11.642	1.338	0.414	1.2	0.581	1.107	0.333	1.051	0.422	0.119	0.0824	0.275	0.202	0.472	0.471	0.471	0.47	1.884
59.75	11.684	1.341	0.415	1.203	0.583	1.11	0.334	1.053	0.423	0.119	0.0825	0.275	0.202	0.473	0.472	0.472	0.471	1.888
59.833	11.726	1.344	0.416	1.206	0.584	1.113	0.335	1.055	0.423	0.12	0.0826	0.276	0.202	0.475	0.474	0.473	0.472	1.894
59.917	11.768	1.348	0.417	1.209	0.586	1.116	0.335	1.057	0.424	0.12	0.0827	0.276	0.202	0.476	0.475	0.474	0.473	1.898
60	11.81	1.351	0.418	1.212	0.587	1.119	0.336	1.059	0.425	0.12	0.0827	0.277	0.202	0.477	0.476	0.476	0.474	1.903
60.083	11.852	1.354	0.419	1.215	0.588	1.122	0.337	1.061	0.426	0.12	0.0828	0.277	0.202	0.478	0.477	0.477	0.476	1.908
60.167	11.895	1.357	0.42	1.218	0.59	1.125	0.338	1.064	0.427	0.12	0.0828	0.277	0.202	0.479	0.478	0.478	0.477	1.912
60.25	11.937	1.361	0.421	1.221	0.591	1.127	0.339	1.066	0.428	0.12	0.0829	0.278	0.202	0.481	0.48	0.479	0.478	1.918
60.333	11.98	1.364	0.422	1.224	0.592	1.13	0.34	1.068	0.429	0.121	0.0829	0.278	0.202	0.482	0.481	0.48	0.479	1.922
60.417	12.023	1.367	0.422	1.227	0.594	1.133	0.34	1.07	0.43	0.121	0.0829	0.278	0.202	0.483	0.482	0.481	0.48	1.926
60.5	12.066	1.37	0.423	1.23	0.595	1.136	0.341	1.072	0.431	0.121	0.0829	0.278	0.202	0.484	0.483	0.483	0.482	1.932
60.583	12.109	1.374	0.424	1.233	0.596	1.139	0.342	1.075	0.432	0.121	0.0829	0.279	0.202	0.485	0.484	0.484	0.483	1.936
60.667	12.152	1.377	0.425	1.236	0.598	1.142	0.343	1.077	0.433	0.121	0.0829	0.279	0.202	0.486	0.485	0.485	0.484	1.94
60.75	12.195	1.38	0.426	1.239	0.599	1.145	0.344	1.079	0.434	0.121	0.0829	0.279	0.202	0.488	0.486	0.486	0.485	1.945
60.833	12.239	1.383	0.426	1.242	0.6	1.148	0.344	1.081	0.435	0.121	0.0829	0.279	0.202	0.489	0.488	0.487	0.486	1.95
60.917	12.282	1.386	0.427	1.245	0.602	1.15	0.345	1.084	0.436	0.121	0.0829	0.279	0.202	0.49	0.489	0.488	0.487	1.954
61	12.326	1.389	0.428	1.248	0.603	1.153	0.346	1.086	0.437	0.121	0.0829	0.279	0.202	0.491	0.49	0.49	0.488	1.959
61.083	12.369	1.392	0.428	1.25	0.604	1.156	0.347	1.088	0.437	0.122	0.0829	0.279	0.202	0.492	0.491	0.491	0.49	1.964
61.167	12.413	1.395	0.429	1.253	0.606	1.159	0.348	1.09	0.438	0.122	0.0829	0.279	0.202	0.493	0.492	0.492	0.491	1.968
61.25	12.457	1.398	0.429	1.256	0.607	1.162	0.348	1.092	0.439	0.122	0.0829	0.279	0.202	0.494	0.493	0.493	0.492	1.972
61.333	12.501	1.401	0.43	1.259	0.608	1.165	0.349	1.094	0.44	0.122	0.0829	0.28	0.202	0.496	0.494	0.494	0.493	1.977
61.417	12.545	1.405	0.43	1.262	0.609	1.167	0.35	1.096	0.441	0.122	0.0829	0.28	0.202	0.497	0.496	0.495	0.494	1.982
61.5	12.589	1.408	0.431	1.265	0.611	1.17	0.351	1.098	0.442	0.122	0.0829	0.28	0.202	0.498	0.497	0.496	0.495	1.986
61.583	12.633	1.411	0.431	1.267	0.612	1.173	0.351	1.099	0.443	0.122	0.0829	0.28	0.202	0.499	0.498	0.497	0.496	1.99
61.667	12.678	1.414	0.431	1.27	0.613	1.176	0.352	1.101	0.444	0.122	0.0829	0.28	0.202	0.5	0.499	0.499	0.497	1.995
61.75	12.722	1.417	0.432	1.273	0.615	1.179	0.353	1.103	0.444	0.122	0.0829	0.28	0.202	0.501	0.5	0.5	0.499	2
61.833	12.767	1.42	0.432	1.276	0.616	1.181	0.354	1.105	0.445	0.122	0.0829	0.28	0.202	0.502	0.501	0.501	0.5	2.004
61.917	12.811	1.423	0.432	1.279	0.617	1.184	0.354	1.106	0.446	0.122	0.0829	0.28	0.202	0.503	0.502	0.502	0.501	2.008
62	12.856	1.426	0.433	1.281	0.618	1.187	0.355	1.108	0.447	0.122	0.0829	0.28	0.202	0.504	0.503	0.503	0.502	2.012
62.083	12.9	1.428	0.433	1.284	0.62	1.189	0.356	1.11	0.447	0.122	0.0829	0.28	0.202	0.506	0.504	0.504	0.503	2.017
62.167	12.945	1.431	0.433	1.287	0.621	1.192	0.357	1.111	0.448	0.122	0.0829	0.28	0.202	0.507	0.505	0.505	0.504	2.021
62.25	12.99	1.434	0.434	1.29	0.622	1.195	0.357	1.113	0.449	0.122	0.0829	0.28	0.202	0.508	0.507	0.506	0.505	2.026
62.333	13.035	1.437	0.434	1.292	0.623	1.197	0.358	1.115	0.449	0.122	0.0829	0.28	0.202	0.509	0.508	0.507	0.506	2.03
62.417	13.08	1.44	0.434	1.295	0.624	1.2	0.359	1.116	0.45	0.122	0.0829	0.28	0.202	0.51	0.509	0.508	0.507	2.034
62.5	13.124	1.443	0.435	1.298	0.625	1.202	0.36	1.118	0.451	0.122	0.0829	0.28	0.202	0.511	0.51	0.509	0.508	2.038
62.583	13.17	1.445	0.435	1.3	0.626	1.205	0.36	1.119	0.451	0.122	0.0829	0.28	0.202	0.512	0.511	0.51	0.509	2.042

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
62.667	13.215	1.448	0.435	1.303	0.627	1.207	0.361	1.12	0.452	0.122	0.0829	0.28	0.202	0.513	0.512	0.512	0.51	2.047
62.75	13.26	1.451	0.435	1.306	0.629	1.21	0.362	1.122	0.453	0.122	0.0829	0.28	0.202	0.514	0.513	0.513	0.512	2.052
62.833	13.305	1.453	0.436	1.308	0.629	1.212	0.362	1.123	0.453	0.122	0.0829	0.28	0.202	0.515	0.514	0.514	0.513	2.056
62.917	13.35	1.456	0.436	1.311	0.63	1.215	0.363	1.124	0.454	0.122	0.0829	0.28	0.202	0.516	0.515	0.515	0.514	2.06
63	13.396	1.458	0.436	1.313	0.631	1.217	0.364	1.126	0.454	0.122	0.0829	0.28	0.202	0.517	0.516	0.516	0.515	2.064
63.083	13.441	1.461	0.436	1.316	0.632	1.22	0.364	1.127	0.455	0.122	0.0829	0.28	0.202	0.518	0.517	0.517	0.515	2.067
63.167	13.486	1.463	0.436	1.318	0.633	1.222	0.365	1.128	0.456	0.122	0.0829	0.28	0.202	0.519	0.518	0.517	0.516	2.07
63.25	13.531	1.466	0.437	1.321	0.634	1.224	0.365	1.129	0.456	0.122	0.0829	0.28	0.202	0.52	0.519	0.518	0.517	2.074
63.333	13.577	1.468	0.437	1.323	0.635	1.227	0.366	1.13	0.457	0.122	0.0829	0.28	0.202	0.521	0.52	0.519	0.518	2.078
63.417	13.622	1.47	0.437	1.325	0.636	1.229	0.367	1.131	0.457	0.122	0.0829	0.28	0.202	0.522	0.521	0.52	0.519	2.082
63.5	13.667	1.472	0.437	1.328	0.637	1.231	0.367	1.132	0.458	0.122	0.0829	0.28	0.202	0.523	0.522	0.521	0.52	2.086
63.583	13.713	1.474	0.437	1.33	0.637	1.234	0.368	1.133	0.458	0.122	0.0829	0.279	0.202	0.523	0.522	0.522	0.521	2.088
63.667	13.758	1.476	0.437	1.332	0.638	1.236	0.368	1.134	0.459	0.122	0.0828	0.279	0.202	0.524	0.523	0.523	0.522	2.092
63.75	13.803	1.478	0.437	1.334	0.639	1.238	0.369	1.135	0.459	0.122	0.0828	0.279	0.202	0.525	0.524	0.524	0.523	2.096
63.833	13.849	1.48	0.437	1.336	0.64	1.24	0.369	1.136	0.46	0.122	0.0826	0.279	0.201	0.526	0.525	0.524	0.523	2.098
63.917	13.894	1.482	0.437	1.338	0.64	1.242	0.37	1.137	0.46	0.122	0.0824	0.279	0.2	0.527	0.526	0.525	0.524	2.102
64	13.939	1.484	0.437	1.34	0.641	1.245	0.37	1.137	0.461	0.121	0.0823	0.278	0.2	0.528	0.526	0.526	0.525	2.105
64.083	13.985	1.486	0.437	1.342	0.642	1.247	0.371	1.138	0.461	0.121	0.082	0.278	0.199	0.528	0.527	0.527	0.526	2.108
64.167	14.03	1.487	0.437	1.344	0.642	1.249	0.371	1.138	0.461	0.121	0.0817	0.277	0.198	0.529	0.528	0.527	0.526	2.11
64.25	14.076	1.489	0.437	1.346	0.643	1.251	0.371	1.139	0.462	0.121	0.0814	0.276	0.197	0.53	0.529	0.528	0.527	2.114
64.333	14.121	1.49	0.436	1.347	0.643	1.253	0.372	1.139	0.462	0.121	0.081	0.276	0.196	0.53	0.529	0.529	0.528	2.116
64.417	14.166	1.492	0.436	1.349	0.644	1.255	0.372	1.139	0.462	0.12	0.0806	0.275	0.195	0.531	0.53	0.529	0.528	2.118
64.5	14.211	1.493	0.436	1.351	0.645	1.257	0.373	1.14	0.463	0.12	0.0803	0.274	0.194	0.532	0.531	0.53	0.529	2.122
64.583	14.256	1.495	0.435	1.352	0.645	1.259	0.373	1.14	0.463	0.12	0.0799	0.273	0.193	0.532	0.531	0.531	0.53	2.124
64.667	14.301	1.496	0.435	1.354	0.645	1.261	0.373	1.14	0.463	0.119	0.0796	0.272	0.192	0.533	0.532	0.531	0.53	2.126
64.75	14.347	1.497	0.434	1.355	0.646	1.262	0.374	1.14	0.463	0.119	0.0793	0.271	0.191	0.533	0.532	0.532	0.531	2.128
64.833	14.392	1.498	0.433	1.356	0.646	1.264	0.374	1.14	0.464	0.118	0.079	0.27	0.191	0.534	0.533	0.532	0.531	2.13
64.917	14.437	1.499	0.433	1.358	0.647	1.266	0.374	1.14	0.464	0.118	0.0787	0.269	0.19	0.534	0.533	0.533	0.532	2.132
65	14.482	1.5	0.432	1.359	0.647	1.268	0.375	1.14	0.464	0.118	0.0785	0.268	0.19	0.535	0.534	0.533	0.532	2.134
65.083	14.527	1.501	0.432	1.36	0.647	1.269	0.375	1.14	0.464	0.117	0.0783	0.267	0.189	0.535	0.534	0.534	0.533	2.136
65.167	14.571	1.502	0.431	1.361	0.648	1.271	0.375	1.139	0.464	0.117	0.0781	0.267	0.189	0.536	0.535	0.534	0.533	2.138
65.25	14.616	1.503	0.43	1.363	0.648	1.273	0.375	1.139	0.464	0.117	0.0779	0.266	0.188	0.536	0.535	0.535	0.534	2.14
65.333	14.661	1.504	0.429	1.364	0.648	1.274	0.375	1.139	0.465	0.116	0.0777	0.265	0.188	0.537	0.536	0.535	0.534	2.142
65.417	14.706	1.505	0.428	1.365	0.649	1.275	0.376	1.138	0.465	0.116	0.0776	0.265	0.188	0.537	0.536	0.536	0.535	2.144
65.5	14.751	1.505	0.427	1.366	0.649	1.277	0.376	1.138	0.465	0.116	0.0774	0.264	0.188	0.538	0.536	0.536	0.535	2.145
65.583	14.795	1.506	0.427	1.367	0.649	1.278	0.376	1.137	0.465	0.116	0.0773	0.264	0.187	0.538	0.537	0.536	0.535	2.146
65.667	14.839	1.507	0.426	1.368	0.649	1.28	0.376	1.137	0.465	0.115	0.0772	0.263	0.187	0.538	0.537	0.537	0.536	2.148
65.75	14.884	1.507	0.425	1.368	0.649	1.281	0.376	1.136	0.465	0.115	0.0771	0.263	0.187	0.539	0.537	0.537	0.536	2.149
65.833	14.928	1.508	0.424	1.369	0.649	1.282	0.376	1.135	0.465	0.115	0.077	0.262	0.187	0.539	0.538	0.537	0.536	2.15
65.917	14.972	1.508	0.423	1.37	0.65	1.283	0.377	1.134	0.465	0.115	0.0769	0.262	0.187	0.539	0.538	0.538	0.537	2.152
66	15.016	1.509	0.422	1.371	0.65	1.284	0.377	1.133	0.465	0.115	0.0768	0.261	0.187	0.539	0.538	0.538	0.537	2.152
66.083	15.06	1.509	0.421	1.371	0.65	1.286	0.377	1.133	0.464	0.114	0.0768	0.261	0.187	0.54	0.539	0.538	0.537	2.154
66.167	15.104	1.509	0.421	1.372	0.65	1.287	0.377	1.132	0.464	0.114	0.0767	0.261	0.187	0.54	0.539	0.538	0.537	2.154
66.25	15.148	1.51	0.42	1.373	0.65	1.288	0.377	1.131	0.464	0.114	0.0767	0.26	0.187	0.54	0.539	0.539	0.538	2.156
66.333	15.192	1.51	0.419	1.373	0.65	1.289	0.377	1.129	0.464	0.114	0.0766	0.26	0.187	0.54	0.539	0.539	0.538	2.156
66.417	15.235	1.51	0.419	1.373	0.65	1.29	0.377	1.128	0.464	0.114	0.0766	0.26	0.187	0.54	0.539	0.539	0.538	2.156
66.5	15.279	1.51	0.418	1.374	0.65	1.29	0.377	1.127	0.464	0.114	0.0766	0.26	0.187	0.541	0.54	0.539	0.538	2.158
66.583	15.322	1.51	0.417	1.374	0.65	1.291	0.377	1.126	0.464	0.113	0.0765	0.259	0.187	0.541	0.54	0.539	0.538	2.158
66.667	15.366	1.51	0.416	1.374	0.65	1.292	0.377	1.125	0.464	0.113	0.0765	0.259	0.186	0.541	0.54	0.539	0.538	2.158
66.75	15.409	1.51	0.416	1.375	0.649	1.293	0.377	1.123	0.463	0.113	0.0764	0.259	0.186	0.541	0.54	0.54	0.539	2.16
66.833	15.452	1.51	0.415	1.375	0.649	1.294	0.377	1.122	0.463	0.113	0.0763	0.258	0.186	0.541	0.54	0.54	0.539	2.16
66.917	15.494	1.51	0.414	1.375	0.649	1.294	0.377	1.12	0.463	0.113	0.0761	0.258	0.185	0.541	0.54	0.54	0.539	2.16
67	15.537	1.51	0.414	1.375	0.649	1.295	0.377	1.119	0.462	0.113	0.076	0.257	0.185	0.541	0.54	0.54	0.539	2.16
67.083	15.58	1.509	0.413	1.375	0.649	1.296	0.377	1.117	0.462	0.112	0.0757	0.257	0.184	0.541	0.54	0.54	0.539	2.16
67.167	15.622	1.509	0.412	1.375	0.648	1.296	0.377	1.116	0.462	0.112	0.0754	0.256	0.183	0.541	0.54	0.54	0.539	2.16
67.25	15.665	1.508	0.411	1.375	0.648	1.297	0.377	1.114	0.461	0.112	0.0751	0.255	0.182	0.541	0.54	0.54	0.539	2.16
67.333	15.707	1.508	0.41	1.375	0.648	1.297	0.377	1.113	0.461	0.111	0.0748	0.255	0.181	0.541	0.54	0.539	0.538	2.158
67.417	15.749	1.507	0.41	1.374	0.647	1.298	0.377	1.111	0.46	0.111	0.0744	0.254	0.18	0.541	0.54	0.539	0.538	2.158
67.5	15.791	1.507	0.409	1.374	0.647	1.298	0.377	1.109	0.46	0.111	0.074	0.253	0.179	0.541	0.54	0.539	0.538	2.158
67.583	15.832	1.506	0.408	1.374	0.646	1.299	0.376	1.108	0.46	0.11	0.0737	0.252	0.178	0.541	0.539	0.539	0.538	2.157
67.667	15.874	1.505	0.407	1.373	0.646	1.299	0.376	1.106	0.459	0.11	0.0734	0.251	0.177	0.54	0.539	0.539	0.538	2.156
67.75	15.915	1.504	0.406	1.373	0.646	1.3	0.376	1.104	0.459	0.11	0.073	0.25	0.176	0.54	0.539	0.539	0.538	2.156
67.833	15.957	1.503	0.405	1.372	0.645	1.3	0.376	1.103	0.458	0.109	0.0727	0.249	0.176	0.54	0.539	0.539	0.538	2.156

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
67.917	15.998	1.502	0.404	1.372	0.644	1.3	0.376	1.101	0.457	0.109	0.0725	0.248	0.175	0.54	0.539	0.538	0.537	2.154
68	16.039	1.501	0.403	1.371	0.644	1.3	0.375	1.099	0.457	0.108	0.0722	0.247	0.174	0.54	0.539	0.538	0.537	2.154
68.083	16.079	1.5	0.402	1.371	0.643	1.3	0.375	1.097	0.456	0.108	0.072	0.246	0.174	0.539	0.538	0.538	0.537	2.152
68.167	16.119	1.499	0.401	1.37	0.643	1.301	0.375	1.095	0.456	0.108	0.0718	0.246	0.174	0.539	0.538	0.538	0.537	2.152
68.25	16.16	1.498	0.4	1.369	0.642	1.301	0.375	1.093	0.455	0.107	0.0716	0.245	0.173	0.539	0.538	0.537	0.536	2.15
68.333	16.2	1.497	0.399	1.368	0.641	1.301	0.374	1.091	0.455	0.107	0.0714	0.244	0.173	0.538	0.537	0.537	0.536	2.148
68.417	16.24	1.495	0.398	1.368	0.641	1.301	0.374	1.09	0.454	0.107	0.0713	0.244	0.173	0.538	0.537	0.537	0.536	2.148
68.5	16.28	1.494	0.397	1.367	0.64	1.301	0.374	1.088	0.454	0.107	0.0711	0.243	0.172	0.538	0.537	0.536	0.535	2.146
68.583	16.319	1.493	0.396	1.366	0.64	1.301	0.373	1.086	0.453	0.106	0.071	0.242	0.172	0.537	0.536	0.536	0.535	2.144
68.667	16.358	1.491	0.394	1.365	0.639	1.301	0.373	1.083	0.452	0.106	0.0709	0.242	0.172	0.537	0.536	0.536	0.535	2.144
68.75	16.398	1.49	0.393	1.364	0.638	1.301	0.373	1.081	0.452	0.106	0.0708	0.241	0.172	0.537	0.535	0.535	0.534	2.141
68.833	16.436	1.489	0.392	1.363	0.637	1.3	0.372	1.079	0.451	0.106	0.0707	0.241	0.172	0.536	0.535	0.535	0.534	2.14
68.917	16.475	1.487	0.391	1.362	0.637	1.3	0.372	1.077	0.45	0.105	0.0706	0.241	0.172	0.536	0.535	0.534	0.533	2.138
69	16.514	1.486	0.39	1.361	0.636	1.3	0.372	1.075	0.45	0.105	0.0705	0.24	0.171	0.535	0.534	0.534	0.533	2.136
69.083	16.552	1.484	0.389	1.36	0.635	1.3	0.371	1.073	0.449	0.105	0.0704	0.24	0.171	0.535	0.534	0.533	0.532	2.134
69.167	16.59	1.483	0.388	1.358	0.635	1.299	0.371	1.071	0.448	0.105	0.0704	0.239	0.171	0.534	0.533	0.533	0.532	2.132
69.25	16.628	1.481	0.387	1.357	0.634	1.299	0.371	1.069	0.448	0.105	0.0703	0.239	0.171	0.534	0.533	0.533	0.532	2.132
69.333	16.665	1.48	0.386	1.356	0.633	1.299	0.37	1.066	0.447	0.105	0.0703	0.239	0.171	0.534	0.532	0.532	0.531	2.129
69.417	16.702	1.478	0.385	1.355	0.632	1.298	0.37	1.064	0.446	0.104	0.0703	0.239	0.171	0.533	0.532	0.532	0.531	2.128
69.5	16.74	1.477	0.385	1.354	0.631	1.298	0.37	1.062	0.446	0.104	0.0703	0.238	0.171	0.533	0.532	0.531	0.53	2.126
69.583	16.776	1.475	0.384	1.353	0.631	1.297	0.369	1.06	0.445	0.104	0.0702	0.238	0.171	0.532	0.531	0.531	0.53	2.124
69.667	16.813	1.473	0.383	1.351	0.63	1.297	0.369	1.058	0.444	0.104	0.0702	0.238	0.171	0.532	0.531	0.53	0.529	2.122
69.75	16.849	1.472	0.382	1.35	0.629	1.296	0.368	1.055	0.444	0.104	0.0702	0.238	0.171	0.531	0.53	0.53	0.529	2.12
69.833	16.885	1.47	0.381	1.349	0.628	1.295	0.368	1.053	0.443	0.104	0.0702	0.238	0.171	0.531	0.53	0.529	0.528	2.118
69.917	16.921	1.468	0.381	1.348	0.627	1.295	0.368	1.051	0.442	0.104	0.0702	0.237	0.171	0.53	0.529	0.529	0.528	2.116
70	16.957	1.467	0.38	1.346	0.626	1.294	0.367	1.049	0.441	0.104	0.0702	0.237	0.171	0.53	0.529	0.528	0.527	2.114
70.083	16.992	1.465	0.38	1.345	0.626	1.293	0.367	1.047	0.441	0.104	0.0702	0.237	0.171	0.529	0.528	0.528	0.527	2.112
70.167	17.027	1.463	0.379	1.344	0.625	1.292	0.366	1.045	0.44	0.104	0.0702	0.237	0.171	0.529	0.528	0.527	0.526	2.11
70.25	17.062	1.461	0.378	1.342	0.624	1.292	0.366	1.043	0.439	0.103	0.0702	0.237	0.171	0.528	0.527	0.527	0.526	2.108
70.333	17.096	1.459	0.378	1.341	0.623	1.291	0.365	1.041	0.438	0.103	0.0702	0.237	0.171	0.528	0.526	0.526	0.525	2.105
70.417	17.131	1.458	0.377	1.34	0.622	1.29	0.365	1.039	0.438	0.103	0.0702	0.237	0.171	0.527	0.526	0.525	0.524	2.102
70.5	17.165	1.456	0.377	1.338	0.621	1.289	0.365	1.037	0.437	0.103	0.0702	0.237	0.171	0.526	0.525	0.525	0.524	2.1
70.583	17.198	1.454	0.376	1.337	0.62	1.288	0.364	1.035	0.436	0.103	0.0702	0.237	0.171	0.526	0.525	0.524	0.523	2.098
70.667	17.231	1.452	0.376	1.335	0.619	1.287	0.364	1.033	0.435	0.103	0.0702	0.237	0.171	0.525	0.524	0.524	0.523	2.096
70.75	17.265	1.45	0.376	1.334	0.618	1.286	0.363	1.031	0.435	0.103	0.0702	0.237	0.171	0.525	0.524	0.523	0.522	2.094
70.833	17.297	1.448	0.375	1.332	0.617	1.285	0.363	1.029	0.434	0.103	0.0702	0.237	0.171	0.524	0.523	0.523	0.522	2.092
70.917	17.329	1.446	0.375	1.331	0.616	1.284	0.362	1.028	0.433	0.103	0.0702	0.237	0.171	0.524	0.522	0.522	0.521	2.089
71	17.362	1.444	0.375	1.329	0.615	1.283	0.362	1.026	0.432	0.103	0.0702	0.237	0.171	0.523	0.522	0.521	0.52	2.086
71.083	17.394	1.442	0.374	1.328	0.614	1.282	0.361	1.024	0.432	0.103	0.0702	0.237	0.171	0.522	0.521	0.521	0.52	2.084
71.167	17.425	1.44	0.374	1.326	0.614	1.28	0.361	1.023	0.431	0.103	0.0702	0.237	0.171	0.522	0.521	0.52	0.519	2.082
71.25	17.457	1.438	0.374	1.325	0.613	1.279	0.36	1.021	0.43	0.103	0.0702	0.237	0.171	0.521	0.52	0.52	0.519	2.08
71.333	17.487	1.436	0.373	1.323	0.612	1.278	0.36	1.019	0.43	0.103	0.0702	0.237	0.171	0.52	0.519	0.519	0.518	2.076
71.417	17.518	1.434	0.373	1.322	0.611	1.277	0.359	1.018	0.429	0.103	0.0702	0.237	0.171	0.52	0.519	0.518	0.517	2.074
71.5	17.548	1.432	0.373	1.32	0.61	1.276	0.359	1.016	0.428	0.103	0.0702	0.237	0.171	0.519	0.518	0.518	0.517	2.072
71.583	17.578	1.43	0.372	1.318	0.609	1.275	0.358	1.015	0.428	0.103	0.0702	0.237	0.171	0.519	0.517	0.517	0.516	2.069
71.667	17.608	1.428	0.372	1.317	0.608	1.273	0.358	1.013	0.427	0.103	0.0702	0.237	0.171	0.518	0.517	0.516	0.515	2.066
71.75	17.637	1.426	0.372	1.315	0.607	1.272	0.357	1.012	0.426	0.103	0.0702	0.237	0.171	0.517	0.516	0.516	0.515	2.064
71.833	17.666	1.424	0.372	1.314	0.606	1.271	0.357	1.011	0.426	0.103	0.0702	0.237	0.171	0.517	0.516	0.515	0.514	2.062
71.917	17.694	1.422	0.371	1.312	0.606	1.27	0.356	1.009	0.425	0.103	0.0702	0.237	0.171	0.516	0.515	0.514	0.513	2.058
72	17.723	1.42	0.371	1.31	0.605	1.268	0.356	1.008	0.425	0.103	0.0702	0.237	0.171	0.515	0.514	0.514	0.513	2.056
72.083	17.75	1.418	0.371	1.309	0.604	1.267	0.355	1.007	0.424	0.103	0.0702	0.237	0.171	0.515	0.514	0.513	0.512	2.054
72.167	17.778	1.416	0.371	1.307	0.603	1.266	0.355	1.006	0.424	0.103	0.0702	0.237	0.171	0.514	0.513	0.513	0.512	2.052
72.25	17.805	1.415	0.371	1.306	0.602	1.264	0.355	1.004	0.423	0.103	0.0702	0.237	0.171	0.513	0.512	0.512	0.511	2.048
72.333	17.831	1.413	0.37	1.304	0.602	1.263	0.354	1.003	0.422	0.103	0.0702	0.237	0.171	0.513	0.512	0.511	0.51	2.046
72.417	17.858	1.411	0.37	1.302	0.601	1.261	0.354	1.002	0.422	0.103	0.0702	0.237	0.171	0.512	0.511	0.511	0.51	2.044
72.5	17.884	1.409	0.37	1.301	0.6	1.26	0.353	1.001	0.421	0.103	0.0702	0.237	0.171	0.512	0.51	0.51	0.509	2.041
72.583	17.91	1.408	0.37	1.299	0.599	1.259	0.353	1	0.421	0.103	0.0701	0.237	0.171	0.511	0.51	0.509	0.508	2.038
72.667	17.935	1.406	0.37	1.298	0.599	1.257	0.352	0.999	0.42	0.103	0.0701	0.236	0.171	0.51	0.509	0.509	0.508	2.036
72.75	17.96	1.404	0.369	1.296	0.598	1.256	0.352	0.998	0.42	0.103	0.07	0.236	0.17	0.51	0.509	0.508	0.507	2.034
72.833	17.984	1.402	0.369	1.295	0.597	1.254	0.351	0.996	0.419	0.103	0.0696	0.236	0.169	0.509	0.508	0.508	0.507	2.032
72.917	18.009	1.4	0.369	1.293	0.596	1.252	0.351	0.995	0.418	0.102	0.0693	0.235	0.168	0.508	0.507	0.507	0.506	2.028
73	18.033	1.399	0.368	1.291	0.595	1.251	0.351	0.994	0.418	0.102	0.069	0.234	0.167	0.508	0.507	0.506	0.505	2.026
73.083	18.056	1.397	0.367	1.29	0.594	1.249	0.35	0.992	0.417	0.102	0.0683	0.233	0.165	0.507	0.506	0.506	0.505	2.024

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
73.167	18.078	1.395	0.367	1.288	0.593	1.247	0.35	0.991	0.417	0.101	0.0677	0.232	0.162	0.506	0.505	0.505	0.504	2.02
73.25	18.101	1.393	0.366	1.286	0.593	1.246	0.349	0.989	0.416	0.101	0.0671	0.231	0.16	0.506	0.505	0.504	0.503	2.018
73.333	18.123	1.39	0.365	1.284	0.592	1.244	0.349	0.988	0.415	0.1	0.0662	0.229	0.157	0.505	0.504	0.504	0.502	2.015
73.417	18.145	1.388	0.364	1.282	0.591	1.242	0.348	0.986	0.414	0.0997	0.0653	0.227	0.155	0.504	0.503	0.503	0.502	2.012
73.5	18.167	1.386	0.363	1.281	0.59	1.24	0.347	0.984	0.414	0.099	0.0644	0.225	0.152	0.504	0.502	0.502	0.501	2.009
73.583	18.187	1.384	0.362	1.279	0.589	1.238	0.347	0.982	0.413	0.0982	0.0635	0.222	0.15	0.503	0.502	0.501	0.5	2.006
73.667	18.208	1.382	0.361	1.277	0.588	1.236	0.346	0.98	0.412	0.0973	0.0627	0.22	0.148	0.502	0.501	0.501	0.5	2.004
73.75	18.228	1.379	0.36	1.275	0.587	1.234	0.346	0.978	0.411	0.0965	0.0618	0.218	0.146	0.501	0.5	0.5	0.499	2
73.833	18.247	1.377	0.358	1.273	0.586	1.232	0.345	0.976	0.411	0.0955	0.0611	0.215	0.144	0.501	0.499	0.499	0.498	1.997
73.917	18.267	1.374	0.357	1.271	0.585	1.23	0.345	0.974	0.41	0.0946	0.0603	0.213	0.143	0.5	0.499	0.498	0.497	1.994
74	18.286	1.372	0.355	1.269	0.583	1.228	0.344	0.971	0.409	0.0936	0.0596	0.211	0.141	0.499	0.498	0.497	0.496	1.99
74.083	18.304	1.369	0.353	1.267	0.582	1.226	0.343	0.969	0.408	0.0927	0.0591	0.209	0.14	0.498	0.497	0.497	0.496	1.988
74.167	18.322	1.367	0.352	1.265	0.581	1.224	0.343	0.966	0.407	0.0918	0.0586	0.207	0.139	0.497	0.496	0.496	0.495	1.984
74.25	18.34	1.364	0.35	1.262	0.58	1.222	0.342	0.964	0.406	0.091	0.058	0.204	0.138	0.496	0.495	0.495	0.494	1.98
74.333	18.356	1.362	0.348	1.26	0.579	1.22	0.341	0.961	0.405	0.0902	0.0576	0.203	0.137	0.496	0.494	0.494	0.493	1.977
74.417	18.373	1.359	0.346	1.258	0.578	1.218	0.341	0.958	0.405	0.0894	0.0572	0.201	0.136	0.495	0.494	0.493	0.492	1.974
74.5	18.389	1.356	0.344	1.256	0.576	1.215	0.34	0.956	0.404	0.0887	0.0568	0.199	0.135	0.494	0.493	0.492	0.491	1.97
74.583	18.404	1.353	0.342	1.253	0.575	1.213	0.339	0.953	0.403	0.0881	0.0565	0.198	0.135	0.493	0.492	0.491	0.49	1.966
74.667	18.419	1.35	0.339	1.251	0.574	1.211	0.339	0.95	0.402	0.0874	0.0562	0.197	0.134	0.492	0.491	0.49	0.489	1.962
74.75	18.435	1.348	0.337	1.249	0.573	1.209	0.338	0.947	0.401	0.0868	0.0559	0.195	0.134	0.491	0.49	0.489	0.488	1.958
74.833	18.449	1.345	0.335	1.246	0.571	1.207	0.337	0.943	0.4	0.0863	0.0556	0.194	0.133	0.49	0.489	0.488	0.487	1.954
74.917	18.462	1.342	0.333	1.244	0.57	1.204	0.336	0.94	0.399	0.0857	0.0554	0.193	0.133	0.489	0.488	0.487	0.486	1.95
75	18.476	1.339	0.331	1.241	0.568	1.202	0.336	0.937	0.397	0.0852	0.0551	0.192	0.133	0.488	0.487	0.487	0.485	1.947
75.083	18.489	1.336	0.329	1.239	0.567	1.2	0.335	0.933	0.396	0.0848	0.055	0.191	0.133	0.487	0.486	0.485	0.484	1.942
75.167	18.501	1.332	0.327	1.236	0.566	1.197	0.334	0.93	0.395	0.0844	0.0548	0.191	0.133	0.486	0.485	0.484	0.483	1.938
75.25	18.513	1.329	0.325	1.233	0.564	1.195	0.333	0.926	0.394	0.0839	0.0547	0.19	0.133	0.485	0.484	0.483	0.482	1.934
75.333	18.524	1.326	0.323	1.231	0.563	1.193	0.333	0.922	0.393	0.0836	0.0546	0.189	0.133	0.484	0.483	0.482	0.481	1.93
75.417	18.535	1.323	0.321	1.228	0.561	1.19	0.332	0.918	0.392	0.0832	0.0545	0.188	0.133	0.483	0.482	0.481	0.48	1.926
75.5	18.546	1.32	0.319	1.225	0.56	1.188	0.331	0.915	0.39	0.0829	0.0544	0.187	0.133	0.482	0.481	0.48	0.479	1.922
75.583	18.555	1.316	0.318	1.223	0.558	1.185	0.33	0.911	0.389	0.0825	0.0544	0.187	0.133	0.481	0.479	0.479	0.478	1.917
75.667	18.564	1.313	0.316	1.22	0.557	1.183	0.329	0.906	0.388	0.0822	0.0543	0.186	0.133	0.479	0.478	0.478	0.477	1.912
75.75	18.574	1.31	0.314	1.217	0.555	1.18	0.329	0.902	0.387	0.0819	0.0543	0.186	0.133	0.478	0.477	0.477	0.476	1.908
75.833	18.582	1.306	0.313	1.214	0.553	1.178	0.328	0.898	0.385	0.0816	0.0542	0.185	0.132	0.477	0.476	0.476	0.475	1.904
75.917	18.59	1.302	0.311	1.211	0.552	1.175	0.327	0.894	0.384	0.0812	0.054	0.184	0.132	0.476	0.475	0.474	0.473	1.898
76	18.597	1.299	0.309	1.208	0.55	1.173	0.326	0.89	0.383	0.0809	0.0539	0.184	0.131	0.475	0.474	0.473	0.472	1.894
76.083	18.604	1.295	0.308	1.205	0.548	1.17	0.325	0.885	0.381	0.0805	0.0537	0.183	0.13	0.474	0.472	0.472	0.471	1.889
76.167	18.61	1.291	0.306	1.202	0.547	1.168	0.324	0.881	0.38	0.0802	0.0534	0.182	0.13	0.472	0.471	0.471	0.47	1.884
76.25	18.616	1.288	0.305	1.199	0.545	1.165	0.323	0.877	0.378	0.0798	0.0532	0.181	0.129	0.471	0.47	0.47	0.468	1.879
76.333	18.621	1.283	0.303	1.195	0.543	1.162	0.322	0.873	0.377	0.0794	0.0528	0.181	0.128	0.47	0.469	0.468	0.467	1.874
76.417	18.626	1.279	0.302	1.192	0.541	1.16	0.321	0.869	0.375	0.079	0.0525	0.18	0.127	0.468	0.467	0.467	0.466	1.868
76.5	18.63	1.275	0.3	1.189	0.539	1.157	0.32	0.865	0.373	0.0786	0.0522	0.179	0.126	0.467	0.466	0.466	0.464	1.863
76.583	18.633	1.271	0.299	1.185	0.537	1.154	0.319	0.861	0.372	0.0782	0.0518	0.178	0.125	0.466	0.465	0.464	0.463	1.858
76.667	18.636	1.267	0.297	1.182	0.535	1.151	0.318	0.857	0.37	0.0778	0.0514	0.177	0.124	0.464	0.463	0.463	0.462	1.852
76.75	18.639	1.263	0.296	1.178	0.533	1.149	0.317	0.853	0.369	0.0774	0.0511	0.176	0.123	0.463	0.462	0.461	0.46	1.846
76.833	18.641	1.258	0.295	1.175	0.531	1.146	0.316	0.849	0.367	0.077	0.0508	0.175	0.122	0.462	0.46	0.46	0.459	1.841
76.917	18.642	1.254	0.293	1.171	0.529	1.143	0.315	0.845	0.366	0.0765	0.0505	0.174	0.122	0.46	0.459	0.459	0.457	1.835
77	18.643	1.249	0.292	1.168	0.527	1.14	0.314	0.841	0.364	0.0761	0.0502	0.173	0.121	0.459	0.458	0.457	0.456	1.83
77.083	18.643	1.245	0.29	1.164	0.525	1.137	0.313	0.838	0.363	0.0758	0.05	0.172	0.12	0.457	0.456	0.456	0.455	1.824
77.167	18.643	1.24	0.289	1.16	0.523	1.134	0.312	0.834	0.361	0.0754	0.0498	0.172	0.12	0.456	0.455	0.454	0.453	1.818
77.25	18.642	1.235	0.287	1.156	0.521	1.131	0.311	0.83	0.359	0.075	0.0495	0.171	0.12	0.454	0.453	0.453	0.452	1.812
77.333	18.64	1.23	0.286	1.152	0.518	1.128	0.309	0.826	0.358	0.0747	0.0494	0.17	0.119	0.453	0.452	0.451	0.45	1.806
77.417	18.638	1.226	0.284	1.148	0.516	1.125	0.308	0.823	0.356	0.0744	0.0492	0.169	0.119	0.451	0.45	0.45	0.448	1.799
77.5	18.637	1.221	0.282	1.144	0.514	1.122	0.307	0.819	0.355	0.0741	0.049	0.169	0.119	0.45	0.448	0.448	0.447	1.793
77.583	18.633	1.216	0.281	1.14	0.512	1.119	0.306	0.815	0.353	0.0738	0.0489	0.168	0.118	0.448	0.447	0.446	0.445	1.786
77.667	18.629	1.211	0.279	1.136	0.51	1.116	0.305	0.812	0.352	0.0736	0.0488	0.168	0.118	0.446	0.445	0.445	0.444	1.78
77.75	18.626	1.207	0.278	1.132	0.508	1.113	0.303	0.808	0.351	0.0733	0.0486	0.167	0.118	0.445	0.443	0.443	0.442	1.773
77.833	18.62	1.202	0.276	1.128	0.506	1.11	0.302	0.805	0.349	0.0731	0.0485	0.167	0.118	0.443	0.442	0.441	0.44	1.766
77.917	18.615	1.197	0.275	1.124	0.504	1.107	0.301	0.801	0.348	0.0729	0.0484	0.166	0.118	0.441	0.44	0.44	0.439	1.76
78	18.609	1.193	0.273	1.12	0.502	1.104	0.3	0.798	0.346	0.0727	0.0484	0.166	0.118	0.44	0.439	0.438	0.437	1.754
78.083	18.602	1.188	0.272	1.115	0.5	1.101	0.299	0.794	0.345	0.0725	0.0483	0.165	0.117	0.438	0.437	0.437	0.435	1.747
78.167	18.595	1.184	0.271	1.111	0.498	1.097	0.298	0.791	0.343	0.0723	0.0482	0.165	0.117	0.436	0.435	0.435	0.434	1.74
78.25	18.588	1.179	0.269	1.107	0.496	1.094	0.296	0.787	0.342	0.0722	0.0481	0.165	0.117	0.435	0.434	0.433	0.432	1.734
78.333	18.579	1.174	0.268	1.103	0.494	1.091	0.295	0.784	0.341	0.072	0.0481	0.164	0.117	0.433	0.432	0.432	0.43	1.727

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
78.417	18.571	1.17	0.267	1.099	0.492	1.087	0.294	0.78	0.339	0.0719	0.0481	0.164	0.117	0.432	0.43	0.43	0.429	1.721
78.5	18.562	1.165	0.266	1.095	0.49	1.084	0.293	0.777	0.338	0.0717	0.048	0.164	0.117	0.43	0.429	0.428	0.427	1.714
78.583	18.551	1.161	0.265	1.091	0.489	1.081	0.292	0.774	0.337	0.0716	0.048	0.164	0.117	0.429	0.427	0.427	0.426	1.709
78.667	18.541	1.157	0.264	1.087	0.487	1.077	0.291	0.77	0.335	0.0715	0.048	0.163	0.117	0.427	0.426	0.425	0.424	1.702
78.75	18.531	1.152	0.263	1.083	0.485	1.074	0.29	0.767	0.334	0.0713	0.048	0.163	0.117	0.425	0.424	0.424	0.423	1.696
78.833	18.519	1.148	0.262	1.079	0.483	1.071	0.289	0.764	0.332	0.0712	0.0479	0.163	0.117	0.424	0.423	0.422	0.421	1.69
78.917	18.507	1.143	0.261	1.075	0.481	1.067	0.288	0.76	0.331	0.071	0.0479	0.163	0.117	0.422	0.421	0.421	0.419	1.683
79	18.495	1.139	0.26	1.071	0.479	1.064	0.286	0.757	0.33	0.0709	0.0478	0.162	0.117	0.421	0.419	0.419	0.418	1.677
79.083	18.481	1.135	0.259	1.068	0.477	1.06	0.285	0.754	0.328	0.0707	0.0477	0.162	0.116	0.419	0.418	0.417	0.416	1.67
79.167	18.467	1.13	0.258	1.064	0.475	1.056	0.284	0.751	0.327	0.0706	0.0476	0.162	0.116	0.418	0.416	0.416	0.415	1.665
79.25	18.453	1.126	0.257	1.06	0.474	1.053	0.283	0.748	0.326	0.0704	0.0475	0.161	0.115	0.416	0.415	0.414	0.413	1.658
79.333	18.438	1.122	0.257	1.056	0.472	1.049	0.282	0.745	0.324	0.0702	0.0473	0.161	0.115	0.414	0.413	0.413	0.412	1.652
79.417	18.423	1.117	0.256	1.052	0.47	1.046	0.281	0.742	0.323	0.0701	0.0471	0.16	0.114	0.413	0.412	0.411	0.41	1.646
79.5	18.407	1.113	0.255	1.048	0.468	1.042	0.28	0.738	0.322	0.0699	0.047	0.16	0.114	0.411	0.41	0.41	0.409	1.64
79.583	18.391	1.109	0.254	1.044	0.466	1.038	0.279	0.735	0.32	0.0697	0.0468	0.16	0.113	0.41	0.409	0.408	0.407	1.634
79.667	18.374	1.105	0.254	1.04	0.464	1.034	0.278	0.733	0.319	0.0695	0.0466	0.159	0.113	0.408	0.407	0.407	0.406	1.628
79.75	18.357	1.1	0.253	1.036	0.462	1.031	0.277	0.73	0.318	0.0693	0.0464	0.159	0.113	0.407	0.406	0.405	0.404	1.622
79.833	18.338	1.096	0.252	1.033	0.461	1.027	0.276	0.727	0.316	0.0691	0.0463	0.158	0.112	0.405	0.404	0.404	0.402	1.615
79.917	18.32	1.092	0.252	1.029	0.459	1.023	0.275	0.724	0.315	0.0689	0.0461	0.158	0.112	0.404	0.403	0.402	0.401	1.61
80	18.302	1.088	0.251	1.025	0.457	1.02	0.274	0.721	0.314	0.0687	0.046	0.157	0.112	0.402	0.401	0.401	0.399	1.603
80.083	18.282	1.084	0.25	1.021	0.455	1.016	0.273	0.718	0.313	0.0685	0.0459	0.157	0.111	0.401	0.4	0.399	0.398	1.598
80.167	18.262	1.079	0.25	1.017	0.453	1.012	0.272	0.715	0.312	0.0683	0.0457	0.156	0.111	0.399	0.398	0.398	0.396	1.591
80.25	18.242	1.075	0.249	1.013	0.452	1.009	0.27	0.713	0.31	0.0681	0.0456	0.156	0.111	0.398	0.397	0.396	0.395	1.586
80.333	18.221	1.071	0.248	1.01	0.45	1.005	0.269	0.71	0.309	0.0679	0.0455	0.156	0.111	0.396	0.395	0.395	0.393	1.579
80.417	18.199	1.067	0.247	1.006	0.448	1.002	0.268	0.707	0.308	0.0678	0.0455	0.155	0.11	0.395	0.394	0.393	0.392	1.574
80.5	18.178	1.063	0.247	1.002	0.446	0.998	0.267	0.704	0.307	0.0676	0.0454	0.155	0.11	0.393	0.392	0.392	0.39	1.567
80.583	18.155	1.059	0.246	0.998	0.445	0.994	0.266	0.702	0.306	0.0675	0.0453	0.155	0.11	0.392	0.391	0.39	0.389	1.562
80.667	18.132	1.055	0.245	0.995	0.443	0.991	0.265	0.699	0.305	0.0674	0.0452	0.154	0.11	0.39	0.389	0.389	0.388	1.556
80.75	18.11	1.051	0.245	0.991	0.442	0.987	0.264	0.697	0.304	0.0672	0.0452	0.154	0.11	0.389	0.388	0.387	0.386	1.55
80.833	18.085	1.047	0.244	0.987	0.44	0.984	0.263	0.694	0.303	0.0671	0.0451	0.154	0.11	0.388	0.386	0.386	0.385	1.545
80.917	18.061	1.043	0.243	0.984	0.438	0.98	0.262	0.692	0.302	0.067	0.0451	0.154	0.11	0.386	0.385	0.384	0.383	1.538
81	18.037	1.039	0.243	0.98	0.437	0.977	0.261	0.689	0.301	0.0669	0.045	0.153	0.11	0.385	0.383	0.383	0.382	1.533
81.083	18.012	1.036	0.242	0.976	0.435	0.973	0.26	0.687	0.3	0.0668	0.045	0.153	0.11	0.383	0.382	0.382	0.38	1.527
81.167	17.987	1.032	0.241	0.973	0.434	0.97	0.26	0.684	0.299	0.0667	0.045	0.153	0.11	0.382	0.381	0.38	0.379	1.522
81.25	17.961	1.028	0.241	0.969	0.432	0.967	0.259	0.682	0.298	0.0666	0.0449	0.153	0.11	0.38	0.379	0.379	0.378	1.516
81.333	17.935	1.025	0.24	0.966	0.431	0.963	0.258	0.68	0.297	0.0666	0.0449	0.153	0.11	0.379	0.378	0.377	0.376	1.51
81.417	17.908	1.021	0.24	0.962	0.429	0.96	0.257	0.677	0.295	0.0665	0.0449	0.153	0.11	0.378	0.377	0.376	0.375	1.506
81.5	17.882	1.018	0.239	0.959	0.428	0.956	0.256	0.675	0.294	0.0664	0.0449	0.152	0.11	0.376	0.375	0.375	0.373	1.499
81.583	17.854	1.014	0.239	0.956	0.426	0.953	0.255	0.673	0.293	0.0664	0.0448	0.152	0.11	0.375	0.374	0.373	0.372	1.494
81.667	17.826	1.011	0.238	0.952	0.425	0.95	0.254	0.67	0.292	0.0663	0.0448	0.152	0.11	0.374	0.373	0.372	0.371	1.49
81.75	17.798	1.007	0.238	0.949	0.424	0.946	0.253	0.668	0.291	0.0662	0.0448	0.152	0.11	0.373	0.371	0.371	0.37	1.485
81.833	17.769	1.004	0.237	0.946	0.422	0.943	0.252	0.666	0.29	0.0661	0.0447	0.152	0.109	0.371	0.37	0.37	0.368	1.479
81.917	17.741	1.001	0.237	0.943	0.421	0.94	0.252	0.664	0.289	0.066	0.0446	0.151	0.109	0.37	0.369	0.368	0.367	1.474
82	17.712	0.997	0.236	0.94	0.419	0.936	0.251	0.662	0.288	0.0658	0.0445	0.151	0.108	0.369	0.367	0.367	0.366	1.469
82.083	17.682	0.994	0.235	0.936	0.418	0.933	0.25	0.659	0.287	0.0656	0.0443	0.151	0.108	0.367	0.366	0.366	0.364	1.463
82.167	17.652	0.991	0.235	0.933	0.416	0.929	0.249	0.657	0.286	0.0654	0.0441	0.15	0.107	0.366	0.365	0.364	0.363	1.458
82.25	17.622	0.987	0.234	0.93	0.415	0.926	0.248	0.655	0.285	0.0653	0.0438	0.15	0.106	0.365	0.364	0.363	0.362	1.454
82.333	17.591	0.984	0.234	0.927	0.414	0.923	0.247	0.653	0.284	0.065	0.0435	0.149	0.105	0.364	0.362	0.362	0.361	1.449
82.417	17.56	0.981	0.233	0.924	0.412	0.919	0.247	0.651	0.283	0.0647	0.0432	0.148	0.104	0.362	0.361	0.361	0.359	1.443
82.5	17.529	0.977	0.232	0.921	0.411	0.916	0.246	0.649	0.282	0.0645	0.0429	0.147	0.103	0.361	0.36	0.36	0.358	1.439
82.583	17.498	0.974	0.232	0.917	0.409	0.913	0.245	0.646	0.281	0.0641	0.0425	0.147	0.102	0.36	0.359	0.358	0.357	1.434
82.667	17.466	0.971	0.231	0.914	0.408	0.909	0.244	0.644	0.28	0.0638	0.0421	0.146	0.101	0.359	0.358	0.357	0.356	1.43
82.75	17.434	0.967	0.23	0.911	0.407	0.906	0.243	0.642	0.279	0.0635	0.0418	0.145	0.1	0.358	0.356	0.356	0.355	1.425
82.833	17.401	0.964	0.23	0.908	0.405	0.902	0.242	0.64	0.278	0.0631	0.0414	0.144	0.0995	0.356	0.355	0.355	0.353	1.419
82.917	17.369	0.961	0.229	0.905	0.404	0.899	0.242	0.638	0.277	0.0627	0.0411	0.143	0.0988	0.355	0.354	0.353	0.352	1.414
83	17.336	0.957	0.228	0.902	0.402	0.896	0.241	0.636	0.276	0.0623	0.0408	0.142	0.0981	0.354	0.353	0.352	0.351	1.41
83.083	17.302	0.954	0.227	0.899	0.401	0.892	0.24	0.634	0.275	0.0619	0.0406	0.141	0.0976	0.353	0.351	0.351	0.35	1.405
83.167	17.269	0.951	0.227	0.896	0.399	0.889	0.239	0.632	0.274	0.0616	0.0404	0.14	0.0971	0.352	0.35	0.35	0.349	1.401
83.25	17.235	0.947	0.226	0.893	0.398	0.886	0.238	0.63	0.273	0.0612	0.0401	0.139	0.0966	0.35	0.349	0.349	0.347	1.395
83.333	17.201	0.944	0.225	0.89	0.397	0.883	0.237	0.628	0.272	0.0609	0.0399	0.139	0.0963	0.349	0.348	0.347	0.346	1.39
83.417	17.167	0.941	0.224	0.887	0.395	0.879	0.237	0.626	0.271	0.0605	0.0398	0.138	0.0959	0.348	0.347	0.346	0.345	1.386
83.5	17.132	0.937	0.223	0.884	0.394	0.876	0.236	0.624	0.27	0.0602	0.0396	0.137	0.0955	0.347	0.346	0.345	0.344	1.382
83.583	17.097	0.934	0.222	0.881	0.392	0.873	0.235	0.622	0.269	0.06	0.0395	0.137	0.0953	0.346	0.344	0.344	0.343	1.377

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
83.667	17.062	0.931	0.221	0.878	0.391	0.87	0.234	0.62	0.268	0.0597	0.0393	0.136	0.095	0.344	0.343	0.343	0.341	1.371
83.75	17.027	0.928	0.22	0.875	0.39	0.867	0.233	0.618	0.267	0.0594	0.0392	0.135	0.0948	0.343	0.342	0.341	0.34	1.366
83.833	16.992	0.924	0.219	0.872	0.388	0.863	0.232	0.615	0.267	0.0592	0.0391	0.135	0.0947	0.342	0.341	0.34	0.339	1.362
83.917	16.956	0.921	0.218	0.869	0.387	0.86	0.232	0.613	0.266	0.059	0.039	0.134	0.0945	0.341	0.34	0.339	0.338	1.358
84	16.921	0.918	0.217	0.866	0.386	0.857	0.231	0.611	0.265	0.0588	0.0389	0.134	0.0944	0.34	0.338	0.338	0.337	1.353
84.083	16.884	0.915	0.216	0.863	0.384	0.854	0.23	0.609	0.264	0.0586	0.0388	0.134	0.0944	0.338	0.337	0.337	0.335	1.347
84.167	16.848	0.911	0.215	0.86	0.383	0.851	0.229	0.607	0.263	0.0584	0.0387	0.133	0.0943	0.337	0.336	0.336	0.334	1.343
84.25	16.812	0.908	0.214	0.857	0.382	0.848	0.228	0.605	0.262	0.0582	0.0387	0.133	0.0943	0.336	0.335	0.334	0.333	1.338
84.333	16.775	0.905	0.213	0.854	0.38	0.845	0.228	0.603	0.261	0.0581	0.0386	0.133	0.0943	0.335	0.334	0.333	0.332	1.334
84.417	16.738	0.902	0.212	0.851	0.379	0.842	0.227	0.601	0.26	0.0579	0.0386	0.132	0.0943	0.334	0.332	0.332	0.331	1.329
84.5	16.701	0.899	0.212	0.848	0.377	0.839	0.226	0.599	0.259	0.0578	0.0385	0.132	0.0943	0.333	0.331	0.331	0.329	1.324
84.583	16.664	0.896	0.211	0.845	0.376	0.836	0.225	0.597	0.258	0.0576	0.0385	0.132	0.0942	0.331	0.33	0.33	0.328	1.319
84.667	16.627	0.892	0.21	0.842	0.375	0.833	0.224	0.595	0.257	0.0575	0.0385	0.131	0.0942	0.33	0.329	0.329	0.327	1.315
84.75	16.589	0.889	0.209	0.839	0.373	0.83	0.224	0.592	0.256	0.0573	0.0384	0.131	0.0941	0.329	0.328	0.327	0.326	1.31
84.833	16.551	0.886	0.208	0.836	0.372	0.827	0.223	0.59	0.255	0.0571	0.0383	0.131	0.0936	0.328	0.327	0.326	0.325	1.306
84.917	16.514	0.883	0.208	0.833	0.371	0.824	0.222	0.588	0.254	0.057	0.0382	0.13	0.0932	0.327	0.326	0.325	0.324	1.302
85	16.476	0.88	0.207	0.831	0.369	0.821	0.221	0.586	0.253	0.0568	0.038	0.13	0.0927	0.326	0.324	0.324	0.323	1.297
85.083	16.438	0.877	0.206	0.828	0.368	0.817	0.22	0.583	0.252	0.0565	0.0377	0.129	0.0916	0.325	0.323	0.323	0.321	1.292
85.167	16.399	0.873	0.205	0.825	0.367	0.814	0.22	0.581	0.251	0.0562	0.0374	0.128	0.0905	0.323	0.322	0.322	0.32	1.287
85.25	16.361	0.87	0.204	0.822	0.365	0.811	0.219	0.578	0.25	0.0559	0.0371	0.128	0.0894	0.322	0.321	0.32	0.319	1.282
85.333	16.323	0.867	0.203	0.819	0.364	0.808	0.218	0.576	0.249	0.0555	0.0367	0.127	0.0878	0.321	0.32	0.319	0.318	1.278
85.417	16.284	0.863	0.202	0.816	0.362	0.805	0.217	0.574	0.248	0.055	0.0362	0.126	0.0862	0.32	0.319	0.318	0.317	1.274
85.5	16.245	0.86	0.201	0.813	0.361	0.802	0.216	0.571	0.247	0.0546	0.0357	0.125	0.0846	0.319	0.317	0.317	0.315	1.268
85.583	16.206	0.857	0.2	0.81	0.359	0.799	0.215	0.569	0.246	0.0541	0.0351	0.123	0.0832	0.317	0.316	0.316	0.314	1.263
85.667	16.167	0.853	0.199	0.806	0.358	0.796	0.215	0.566	0.245	0.0536	0.0346	0.122	0.0817	0.316	0.315	0.314	0.313	1.258
85.75	16.128	0.85	0.198	0.803	0.356	0.793	0.214	0.564	0.244	0.0531	0.034	0.12	0.0803	0.315	0.314	0.313	0.312	1.254
85.833	16.089	0.846	0.197	0.8	0.355	0.79	0.213	0.561	0.243	0.0526	0.0335	0.119	0.0792	0.314	0.312	0.312	0.311	1.249
85.917	16.049	0.843	0.196	0.797	0.353	0.787	0.212	0.559	0.242	0.052	0.0331	0.118	0.0781	0.312	0.311	0.311	0.309	1.243
86	16.01	0.839	0.195	0.794	0.352	0.783	0.211	0.556	0.241	0.0514	0.0326	0.116	0.0771	0.311	0.31	0.309	0.308	1.238
86.083	15.97	0.835	0.193	0.791	0.35	0.78	0.21	0.553	0.24	0.0508	0.0322	0.115	0.0763	0.31	0.309	0.308	0.307	1.234
86.167	15.931	0.832	0.192	0.788	0.348	0.777	0.209	0.551	0.239	0.0503	0.0319	0.113	0.0756	0.309	0.307	0.307	0.306	1.229
86.25	15.891	0.828	0.191	0.784	0.347	0.774	0.208	0.548	0.238	0.0497	0.0315	0.112	0.0748	0.307	0.306	0.306	0.304	1.223
86.333	15.851	0.824	0.189	0.781	0.345	0.771	0.207	0.545	0.237	0.0492	0.0312	0.111	0.0743	0.306	0.305	0.304	0.303	1.218
86.417	15.811	0.821	0.188	0.778	0.344	0.768	0.206	0.543	0.236	0.0487	0.031	0.11	0.0737	0.305	0.304	0.303	0.302	1.214
86.5	15.772	0.817	0.186	0.775	0.342	0.765	0.206	0.54	0.235	0.0482	0.0307	0.109	0.0731	0.304	0.302	0.302	0.3	1.208
86.583	15.731	0.813	0.185	0.771	0.341	0.762	0.205	0.537	0.234	0.0478	0.0305	0.108	0.0728	0.302	0.301	0.3	0.299	1.202
86.667	15.691	0.81	0.183	0.768	0.339	0.759	0.204	0.534	0.232	0.0474	0.0303	0.107	0.0724	0.301	0.3	0.299	0.298	1.198
86.75	15.651	0.806	0.181	0.764	0.338	0.755	0.203	0.532	0.231	0.047	0.0301	0.106	0.072	0.3	0.298	0.298	0.296	1.192
86.833	15.611	0.802	0.18	0.761	0.336	0.752	0.202	0.529	0.23	0.0467	0.0299	0.105	0.0718	0.298	0.297	0.296	0.295	1.186
86.917	15.57	0.798	0.178	0.758	0.334	0.749	0.201	0.526	0.229	0.0463	0.0297	0.105	0.0716	0.297	0.296	0.295	0.294	1.182
87	15.53	0.795	0.177	0.754	0.333	0.746	0.2	0.523	0.228	0.046	0.0296	0.104	0.0713	0.296	0.294	0.294	0.292	1.176
87.083	15.489	0.791	0.175	0.751	0.331	0.743	0.199	0.52	0.227	0.0457	0.0295	0.104	0.0713	0.294	0.293	0.292	0.291	1.17
87.167	15.449	0.787	0.174	0.747	0.33	0.74	0.198	0.517	0.226	0.0454	0.0294	0.103	0.0712	0.293	0.292	0.291	0.29	1.166
87.25	15.408	0.784	0.172	0.744	0.328	0.737	0.197	0.514	0.225	0.0452	0.0292	0.102	0.0712	0.292	0.29	0.29	0.288	1.16
87.333	15.367	0.78	0.171	0.741	0.327	0.734	0.196	0.511	0.224	0.0449	0.0292	0.102	0.0712	0.29	0.289	0.288	0.287	1.154
87.417	15.327	0.776	0.17	0.737	0.325	0.731	0.195	0.508	0.223	0.0447	0.0291	0.101	0.0712	0.289	0.288	0.287	0.286	1.15
87.5	15.286	0.773	0.168	0.734	0.324	0.728	0.194	0.505	0.222	0.0445	0.029	0.101	0.0712	0.287	0.286	0.286	0.284	1.143
87.583	15.245	0.769	0.167	0.731	0.322	0.725	0.193	0.502	0.221	0.0443	0.029	0.101	0.0712	0.286	0.285	0.284	0.283	1.138
87.667	15.204	0.765	0.166	0.727	0.321	0.721	0.193	0.499	0.22	0.0441	0.029	0.1	0.0711	0.285	0.284	0.283	0.282	1.134
87.75	15.163	0.762	0.165	0.724	0.319	0.718	0.192	0.496	0.218	0.0439	0.029	0.1	0.0711	0.284	0.282	0.282	0.28	1.128
87.833	15.122	0.758	0.164	0.721	0.318	0.715	0.191	0.493	0.217	0.0437	0.0289	0.1	0.071	0.282	0.281	0.28	0.279	1.122
87.917	15.081	0.755	0.163	0.717	0.316	0.712	0.19	0.49	0.216	0.0435	0.0289	0.1	0.0709	0.281	0.28	0.279	0.278	1.118
88	15.04	0.751	0.162	0.714	0.315	0.709	0.189	0.486	0.215	0.0433	0.0288	0.1	0.0707	0.28	0.278	0.278	0.276	1.112
88.083	14.999	0.747	0.16	0.711	0.313	0.706	0.188	0.483	0.214	0.0431	0.0287	0.1	0.0704	0.278	0.277	0.276	0.275	1.106
88.167	14.958	0.744	0.159	0.707	0.311	0.703	0.187	0.48	0.213	0.0429	0.0287	0.1	0.07	0.277	0.276	0.275	0.274	1.102
88.25	14.916	0.74	0.158	0.704	0.31	0.7	0.186	0.477	0.211	0.0427	0.0286	0.1	0.0697	0.276	0.274	0.274	0.272	1.096
88.333	14.875	0.736	0.158	0.7	0.308	0.697	0.185	0.474	0.21	0.0425	0.0284	0.1	0.0692	0.274	0.273	0.272	0.271	1.09
88.417	14.834	0.733	0.157	0.697	0.307	0.694	0.184	0.471	0.209	0.0423	0.0282	0.1	0.0686	0.273	0.272	0.271	0.27	1.086
88.5	14.792	0.729	0.156	0.694	0.305	0.69	0.183	0.468	0.208	0.0421	0.0281	0.1	0.0681	0.272	0.27	0.27	0.268	1.08
88.583	14.751	0.725	0.155	0.69	0.304	0.687	0.182	0.465	0.207	0.0419	0.0279	0.1	0.0676	0.27	0.269	0.268	0.267	1.074
88.667	14.709	0.722	0.154	0.687	0.302	0.684	0.182	0.462	0.205	0.0417	0.0277	0.1	0.0671	0.269	0.268	0.267	0.266	1.07
88.75	14.668	0.718	0.153	0.683	0.3	0.681	0.181	0.459	0.204	0.0415	0.0275	0.1	0.0666	0.268	0.266	0.266	0.264	1.064
88.833	14.626	0.714	0.152	0.68	0.299	0.678	0.18	0.457	0.203	0.0412	0.0274	0.1	0.0662	0.266	0.265	0.264	0.263	1.058

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
88.917	14.585	0.711	0.151	0.677	0.297	0.675	0.179	0.454	0.202	0.041	0.0272	0.1	0.0659	0.265	0.264	0.263	0.262	1.054
89	14.543	0.707	0.151	0.673	0.295	0.672	0.178	0.451	0.201	0.0408	0.027	0.1	0.0655	0.263	0.262	0.262	0.26	1.047
89.083	14.502	0.703	0.15	0.67	0.294	0.669	0.177	0.448	0.199	0.0406	0.0269	0.1	0.0652	0.262	0.261	0.26	0.259	1.042
89.167	14.46	0.699	0.149	0.666	0.292	0.666	0.176	0.445	0.198	0.0404	0.0268	0.1	0.065	0.261	0.259	0.259	0.257	1.036
89.25	14.418	0.696	0.148	0.663	0.291	0.663	0.175	0.443	0.197	0.0402	0.0267	0.1	0.0647	0.259	0.258	0.258	0.256	1.031
89.333	14.377	0.692	0.147	0.66	0.289	0.66	0.174	0.44	0.196	0.04	0.0266	0.1	0.0645	0.258	0.257	0.256	0.255	1.026
89.417	14.335	0.688	0.146	0.656	0.287	0.657	0.173	0.438	0.195	0.0399	0.0265	0.1	0.0643	0.257	0.255	0.255	0.253	1.02
89.5	14.293	0.684	0.145	0.653	0.286	0.654	0.172	0.435	0.194	0.0397	0.0264	0.1	0.0642	0.255	0.254	0.254	0.252	1.015
89.583	14.251	0.681	0.145	0.649	0.284	0.651	0.171	0.432	0.193	0.0396	0.0263	0.1	0.064	0.254	0.253	0.252	0.251	1.01
89.667	14.209	0.677	0.144	0.646	0.283	0.648	0.17	0.43	0.192	0.0394	0.0262	0.1	0.0639	0.253	0.251	0.251	0.249	1.004
89.75	14.168	0.673	0.143	0.642	0.281	0.645	0.169	0.427	0.191	0.0393	0.0262	0.1	0.0638	0.251	0.25	0.249	0.248	0.998
89.833	14.126	0.67	0.142	0.639	0.28	0.642	0.168	0.425	0.19	0.0392	0.0261	0.1	0.0637	0.25	0.249	0.248	0.247	0.994
89.917	14.084	0.666	0.141	0.635	0.278	0.639	0.168	0.422	0.189	0.0391	0.0261	0.1	0.0636	0.249	0.247	0.247	0.245	0.988
90	14.042	0.662	0.14	0.632	0.277	0.636	0.167	0.42	0.188	0.0389	0.026	0.1	0.0635	0.247	0.246	0.245	0.244	0.982
90.083	14	0.659	0.14	0.629	0.275	0.633	0.166	0.418	0.187	0.0389	0.026	0.1	0.0635	0.246	0.245	0.244	0.243	0.978
90.167	13.959	0.655	0.139	0.625	0.274	0.63	0.165	0.415	0.186	0.0388	0.0259	0.1	0.0635	0.245	0.243	0.243	0.241	0.972
90.25	13.917	0.652	0.138	0.622	0.272	0.627	0.164	0.413	0.185	0.0387	0.0259	0.1	0.0635	0.243	0.242	0.241	0.24	0.966
90.333	13.875	0.649	0.138	0.619	0.271	0.624	0.163	0.411	0.184	0.0386	0.0259	0.1	0.0635	0.242	0.241	0.24	0.239	0.962
90.417	13.833	0.645	0.137	0.615	0.269	0.622	0.162	0.408	0.183	0.0385	0.0258	0.1	0.0635	0.241	0.239	0.239	0.237	0.956
90.5	13.791	0.642	0.136	0.612	0.268	0.619	0.162	0.406	0.182	0.0384	0.0258	0.1	0.0635	0.239	0.238	0.238	0.236	0.951
90.583	13.749	0.639	0.136	0.609	0.267	0.616	0.161	0.404	0.181	0.0384	0.0258	0.1	0.0635	0.238	0.237	0.236	0.235	0.946
90.667	13.707	0.635	0.135	0.606	0.265	0.613	0.16	0.402	0.18	0.0383	0.0258	0.1	0.0635	0.237	0.236	0.235	0.234	0.942
90.75	13.665	0.632	0.134	0.603	0.264	0.61	0.159	0.4	0.179	0.0382	0.0258	0.1	0.0635	0.236	0.234	0.234	0.232	0.936
90.833	13.623	0.629	0.134	0.6	0.263	0.607	0.158	0.398	0.178	0.0382	0.0258	0.1	0.0633	0.235	0.233	0.233	0.231	0.932
90.917	13.581	0.626	0.133	0.597	0.261	0.605	0.157	0.395	0.177	0.0381	0.0257	0.1	0.0632	0.234	0.232	0.232	0.23	0.928
91	13.539	0.623	0.133	0.594	0.26	0.602	0.157	0.393	0.176	0.038	0.0257	0.1	0.0631	0.232	0.231	0.23	0.229	0.922
91.083	13.497	0.619	0.132	0.591	0.259	0.599	0.156	0.391	0.175	0.0379	0.0256	0.1	0.0628	0.231	0.23	0.229	0.228	0.918
91.167	13.456	0.616	0.132	0.588	0.257	0.596	0.155	0.389	0.174	0.0378	0.0255	0.1	0.0625	0.23	0.229	0.228	0.227	0.914
91.25	13.414	0.613	0.131	0.585	0.256	0.593	0.154	0.387	0.173	0.0377	0.0254	0.1	0.0621	0.229	0.227	0.227	0.225	0.908
91.333	13.372	0.61	0.131	0.582	0.255	0.59	0.154	0.385	0.172	0.0375	0.0253	0.1	0.0616	0.228	0.226	0.226	0.224	0.904
91.417	13.33	0.607	0.13	0.579	0.253	0.587	0.153	0.383	0.171	0.0374	0.0251	0.1	0.0611	0.227	0.225	0.225	0.223	0.9
91.5	13.288	0.604	0.13	0.577	0.252	0.584	0.152	0.381	0.17	0.0373	0.025	0.1	0.0605	0.225	0.224	0.224	0.222	0.895
91.583	13.246	0.601	0.129	0.574	0.251	0.581	0.151	0.379	0.169	0.0371	0.0248	0.1	0.06	0.224	0.223	0.222	0.221	0.89
91.667	13.205	0.598	0.129	0.571	0.249	0.578	0.15	0.377	0.169	0.0369	0.0246	0.1	0.0595	0.223	0.222	0.221	0.22	0.886
91.75	13.163	0.595	0.128	0.568	0.248	0.575	0.15	0.375	0.168	0.0368	0.0244	0.1	0.059	0.222	0.221	0.22	0.219	0.882
91.833	13.121	0.592	0.128	0.565	0.247	0.572	0.149	0.374	0.167	0.0366	0.0242	0.1	0.0586	0.221	0.22	0.219	0.218	0.878
91.917	13.079	0.589	0.127	0.563	0.246	0.57	0.148	0.372	0.166	0.0364	0.0241	0.1	0.0582	0.22	0.219	0.218	0.216	0.873
92	13.037	0.586	0.127	0.56	0.244	0.567	0.147	0.37	0.165	0.0362	0.0239	0.1	0.0579	0.219	0.217	0.217	0.215	0.868
92.083	12.996	0.583	0.126	0.557	0.243	0.564	0.147	0.368	0.164	0.036	0.0238	0.1	0.0576	0.218	0.216	0.216	0.214	0.864
92.167	12.954	0.58	0.126	0.554	0.242	0.561	0.146	0.366	0.163	0.0358	0.0236	0.1	0.0573	0.217	0.215	0.215	0.213	0.86
92.25	12.912	0.577	0.126	0.551	0.241	0.558	0.145	0.364	0.163	0.0356	0.0235	0.1	0.0571	0.216	0.214	0.214	0.212	0.856
92.333	12.871	0.574	0.125	0.549	0.239	0.555	0.144	0.363	0.162	0.0354	0.0234	0.1	0.0569	0.214	0.213	0.213	0.211	0.851
92.417	12.829	0.571	0.124	0.546	0.238	0.552	0.144	0.361	0.161	0.0352	0.0233	0.1	0.0567	0.213	0.212	0.212	0.21	0.847
92.5	12.787	0.568	0.124	0.543	0.237	0.55	0.143	0.359	0.16	0.0351	0.0232	0.1	0.0565	0.212	0.211	0.21	0.209	0.842
92.583	12.746	0.565	0.123	0.541	0.236	0.547	0.142	0.357	0.159	0.0349	0.0232	0.1	0.0563	0.211	0.21	0.209	0.208	0.838
92.667	12.704	0.563	0.123	0.538	0.235	0.544	0.142	0.356	0.159	0.0348	0.0231	0.1	0.0562	0.21	0.209	0.208	0.207	0.834
92.75	12.663	0.56	0.122	0.535	0.233	0.541	0.141	0.354	0.158	0.0347	0.023	0.1	0.0561	0.209	0.208	0.207	0.206	0.83
92.833	12.621	0.557	0.122	0.533	0.232	0.539	0.14	0.352	0.157	0.0345	0.023	0.1	0.056	0.208	0.207	0.206	0.205	0.826
92.917	12.58	0.554	0.121	0.53	0.231	0.536	0.139	0.351	0.156	0.0344	0.0229	0.1	0.0559	0.207	0.206	0.205	0.204	0.822
93	12.538	0.551	0.12	0.527	0.23	0.533	0.139	0.349	0.156	0.0343	0.0228	0.1	0.0558	0.206	0.205	0.204	0.203	0.818
93.083	12.497	0.549	0.12	0.525	0.229	0.531	0.138	0.347	0.155	0.0342	0.0228	0.1	0.0558	0.205	0.204	0.203	0.202	0.814
93.167	12.456	0.546	0.119	0.522	0.228	0.528	0.137	0.346	0.154	0.0341	0.0228	0.1	0.0558	0.204	0.203	0.202	0.201	0.81
93.25	12.414	0.543	0.119	0.52	0.227	0.525	0.137	0.344	0.153	0.034	0.0227	0.1	0.0557	0.203	0.202	0.201	0.2	0.806
93.333	12.373	0.541	0.118	0.517	0.226	0.523	0.136	0.342	0.153	0.0339	0.0227	0.1	0.0557	0.202	0.201	0.2	0.199	0.802
93.417	12.332	0.538	0.118	0.515	0.225	0.52	0.135	0.341	0.152	0.0339	0.0227	0.1	0.0557	0.201	0.2	0.199	0.198	0.798
93.5	12.291	0.536	0.117	0.512	0.223	0.518	0.135	0.339	0.151	0.0338	0.0226	0.1	0.0557	0.2	0.199	0.198	0.197	0.794
93.583	12.25	0.533	0.117	0.51	0.222	0.515	0.134	0.338	0.15	0.0337	0.0226	0.1	0.0557	0.199	0.198	0.197	0.196	0.79
93.667	12.209	0.531	0.117	0.507	0.221	0.513	0.133	0.336	0.15	0.0336	0.0226	0.1	0.0557	0.198	0.197	0.196	0.195	0.786
93.75	12.168	0.528	0.116	0.505	0.22	0.51	0.133	0.335	0.149	0.0336	0.0226	0.1	0.0557	0.197	0.196	0.195	0.194	0.782
93.833	12.127	0.526	0.116	0.503	0.219	0.508	0.132	0.333	0.148	0.0335	0.0226	0.1	0.0556	0.196	0.195	0.194	0.193	0.778
93.917	12.086	0.523	0.115	0.5	0.218	0.505	0.132	0.331	0.148	0.0334	0.0226	0.1	0.0555	0.195	0.194	0.193	0.192	0.774
94	12.045	0.521	0.115	0.498	0.217	0.502	0.131	0.33	0.147	0.0333	0.0225	0.1	0.0554	0.194	0.193	0.193	0.191	0.771
94.083	12.004	0.518	0.114	0.496	0.216	0.5	0.13	0.328	0.146	0.0332	0.0224	0.1	0.0551	0.194	0.192	0.192	0.19	0.768

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
94.167	11.964	0.516	0.114	0.493	0.215	0.497	0.13	0.327	0.145	0.0331	0.0224	0.1	0.0548	0.193	0.191	0.191	0.189	0.764
94.25	11.923	0.514	0.114	0.491	0.214	0.495	0.129	0.325	0.145	0.033	0.0223	0.1	0.0545	0.192	0.19	0.19	0.188	0.76
94.333	11.882	0.511	0.113	0.489	0.213	0.493	0.129	0.324	0.144	0.0329	0.0221	0.1	0.054	0.191	0.189	0.189	0.187	0.756
94.417	11.842	0.509	0.113	0.486	0.212	0.49	0.128	0.322	0.143	0.0328	0.022	0.1	0.0535	0.19	0.188	0.188	0.186	0.752
94.5	11.801	0.506	0.112	0.484	0.211	0.488	0.127	0.321	0.143	0.0326	0.0218	0.1	0.053	0.189	0.188	0.187	0.185	0.749
94.583	11.761	0.504	0.112	0.482	0.21	0.485	0.127	0.319	0.142	0.0325	0.0217	0.1	0.0525	0.188	0.187	0.186	0.185	0.746
94.667	11.72	0.501	0.112	0.48	0.209	0.483	0.126	0.318	0.141	0.0323	0.0215	0.1	0.052	0.187	0.186	0.185	0.184	0.742
94.75	11.68	0.499	0.111	0.477	0.208	0.48	0.125	0.316	0.14	0.0321	0.0213	0.1	0.0514	0.186	0.185	0.184	0.183	0.738
94.833	11.64	0.497	0.111	0.475	0.207	0.478	0.125	0.315	0.14	0.0319	0.0211	0.1	0.0511	0.185	0.184	0.184	0.182	0.735
94.917	11.6	0.494	0.11	0.473	0.206	0.475	0.124	0.314	0.139	0.0317	0.0209	0.1	0.0507	0.185	0.183	0.183	0.181	0.732
95	11.559	0.492	0.11	0.471	0.205	0.473	0.124	0.312	0.138	0.0315	0.0208	0.1	0.0503	0.184	0.182	0.182	0.18	0.728
95.083	11.52	0.489	0.109	0.469	0.204	0.47	0.123	0.311	0.138	0.0314	0.0206	0.1	0.05	0.183	0.181	0.181	0.179	0.724
95.167	11.48	0.487	0.109	0.466	0.203	0.468	0.122	0.309	0.137	0.0312	0.0205	0.1	0.0497	0.182	0.181	0.18	0.178	0.721
95.25	11.44	0.485	0.108	0.464	0.202	0.466	0.122	0.308	0.136	0.031	0.0204	0.1	0.0494	0.181	0.18	0.179	0.178	0.718
95.333	11.4	0.482	0.108	0.462	0.201	0.463	0.121	0.307	0.136	0.0308	0.0203	0.1	0.0492	0.18	0.179	0.178	0.177	0.714
95.417	11.36	0.48	0.107	0.46	0.2	0.461	0.121	0.305	0.135	0.0306	0.0202	0.1	0.049	0.179	0.178	0.177	0.176	0.71
95.5	11.32	0.478	0.107	0.458	0.199	0.459	0.12	0.304	0.134	0.0304	0.0201	0.1	0.0488	0.178	0.177	0.177	0.175	0.707
95.583	11.281	0.475	0.106	0.455	0.198	0.456	0.119	0.303	0.134	0.0303	0.02	0.1	0.0487	0.178	0.176	0.176	0.174	0.704
95.667	11.241	0.473	0.106	0.453	0.197	0.454	0.119	0.301	0.133	0.0302	0.0199	0.1	0.0485	0.177	0.175	0.175	0.173	0.7
95.75	11.202	0.47	0.105	0.451	0.196	0.452	0.118	0.3	0.133	0.03	0.0199	0.1	0.0484	0.176	0.175	0.174	0.172	0.697
95.833	11.162	0.468	0.104	0.449	0.195	0.45	0.118	0.299	0.132	0.0299	0.0198	0.1	0.0483	0.175	0.174	0.173	0.171	0.693
95.917	11.123	0.466	0.104	0.447	0.194	0.447	0.117	0.298	0.131	0.0298	0.0197	0.1	0.0482	0.174	0.173	0.172	0.171	0.69
96	11.084	0.464	0.103	0.444	0.193	0.445	0.117	0.296	0.131	0.0297	0.0197	0.1	0.0481	0.173	0.172	0.171	0.17	0.686
96.083	11.045	0.461	0.103	0.442	0.192	0.443	0.116	0.295	0.13	0.0296	0.0196	0.1	0.0481	0.172	0.171	0.171	0.169	0.683
96.167	11.006	0.459	0.102	0.44	0.191	0.441	0.115	0.294	0.13	0.0295	0.0196	0.1	0.0481	0.172	0.17	0.17	0.168	0.68
96.25	10.967	0.457	0.102	0.438	0.191	0.438	0.115	0.293	0.129	0.0294	0.0196	0.1	0.048	0.171	0.169	0.169	0.167	0.676
96.333	10.928	0.455	0.101	0.436	0.19	0.436	0.114	0.291	0.128	0.0293	0.0195	0.1	0.048	0.17	0.169	0.168	0.166	0.673
96.417	10.889	0.453	0.101	0.434	0.189	0.434	0.114	0.29	0.128	0.0292	0.0195	0.1	0.048	0.169	0.168	0.167	0.166	0.67
96.5	10.851	0.45	0.1	0.432	0.188	0.432	0.113	0.289	0.127	0.0291	0.0195	0.1	0.048	0.168	0.167	0.166	0.165	0.666
96.583	10.812	0.448	0.0998	0.43	0.187	0.43	0.113	0.288	0.127	0.0291	0.0195	0.1	0.048	0.168	0.166	0.166	0.164	0.664
96.667	10.774	0.446	0.0993	0.428	0.186	0.428	0.112	0.286	0.126	0.029	0.0195	0.1	0.048	0.167	0.165	0.165	0.163	0.66
96.75	10.735	0.444	0.0989	0.426	0.185	0.426	0.112	0.285	0.125	0.0289	0.0194	0.1	0.048	0.166	0.164	0.164	0.162	0.656
96.833	10.697	0.442	0.0985	0.424	0.184	0.423	0.111	0.284	0.125	0.0289	0.0194	0.1	0.048	0.165	0.164	0.163	0.162	0.654
96.917	10.659	0.44	0.0981	0.422	0.184	0.421	0.11	0.283	0.124	0.0288	0.0194	0.1	0.048	0.164	0.163	0.162	0.161	0.65
97	10.621	0.438	0.0977	0.42	0.183	0.419	0.11	0.281	0.124	0.0288	0.0194	0.1	0.048	0.164	0.162	0.162	0.16	0.648
97.083	10.583	0.436	0.0974	0.418	0.182	0.417	0.109	0.28	0.123	0.0287	0.0194	0.1	0.048	0.163	0.161	0.161	0.159	0.644
97.167	10.545	0.434	0.0971	0.416	0.181	0.415	0.109	0.279	0.123	0.0287	0.0194	0.1	0.048	0.162	0.161	0.16	0.158	0.641
97.25	10.507	0.432	0.0967	0.414	0.18	0.413	0.108	0.278	0.122	0.0286	0.0194	0.1	0.048	0.161	0.16	0.159	0.158	0.638
97.333	10.47	0.43	0.0964	0.412	0.18	0.411	0.108	0.277	0.122	0.0286	0.0194	0.1	0.048	0.161	0.159	0.159	0.157	0.636
97.417	10.432	0.428	0.0961	0.41	0.179	0.409	0.107	0.275	0.121	0.0285	0.0194	0.1	0.048	0.16	0.158	0.158	0.156	0.632
97.5	10.395	0.426	0.0958	0.408	0.178	0.407	0.107	0.274	0.12	0.0285	0.0194	0.1	0.048	0.159	0.158	0.157	0.155	0.629
97.583	10.357	0.424	0.0956	0.406	0.177	0.405	0.106	0.273	0.12	0.0285	0.0194	0.1	0.048	0.158	0.157	0.156	0.155	0.626
97.667	10.32	0.422	0.0954	0.405	0.176	0.403	0.106	0.272	0.119	0.0285	0.0194	0.1	0.048	0.158	0.156	0.156	0.154	0.624
97.75	10.283	0.42	0.0951	0.403	0.176	0.401	0.105	0.271	0.119	0.0284	0.0194	0.1	0.048	0.157	0.155	0.155	0.153	0.62
97.833	10.246	0.418	0.0949	0.401	0.175	0.399	0.105	0.27	0.118	0.0284	0.0194	0.1	0.048	0.156	0.155	0.154	0.152	0.617
97.917	10.209	0.417	0.0947	0.399	0.174	0.397	0.105	0.269	0.118	0.0284	0.0194	0.1	0.048	0.155	0.154	0.153	0.152	0.614
98	10.172	0.415	0.0945	0.397	0.173	0.395	0.104	0.268	0.117	0.0284	0.0194	0.1	0.048	0.155	0.153	0.153	0.151	0.612
98.083	10.135	0.413	0.0943	0.395	0.173	0.393	0.104	0.267	0.117	0.0284	0.0194	0.1	0.048	0.154	0.153	0.152	0.15	0.609
98.167	10.099	0.411	0.0942	0.394	0.172	0.392	0.103	0.266	0.117	0.0284	0.0194	0.1	0.048	0.153	0.152	0.151	0.15	0.606
98.25	10.062	0.409	0.094	0.392	0.171	0.39	0.103	0.265	0.116	0.0284	0.0194	0.1	0.048	0.153	0.151	0.151	0.149	0.604
98.333	10.026	0.407	0.0938	0.39	0.17	0.388	0.102	0.264	0.116	0.0284	0.0194	0.1	0.048	0.152	0.15	0.15	0.148	0.6
98.417	9.99	0.406	0.0937	0.388	0.17	0.386	0.102	0.264	0.115	0.0284	0.0194	0.1	0.048	0.151	0.15	0.149	0.148	0.598
98.5	9.954	0.404	0.0935	0.387	0.169	0.384	0.101	0.263	0.115	0.0284	0.0194	0.1	0.048	0.151	0.149	0.149	0.147	0.596
98.583	9.918	0.402	0.0934	0.385	0.168	0.383	0.101	0.262	0.114	0.0284	0.0194	0.1	0.048	0.15	0.148	0.148	0.146	0.592
98.667	9.882	0.4	0.0932	0.383	0.167	0.381	0.1	0.261	0.114	0.0284	0.0194	0.1	0.048	0.149	0.148	0.147	0.146	0.59
98.75	9.846	0.399	0.0931	0.382	0.167	0.379	0.1	0.26	0.114	0.0284	0.0194	0.1	0.048	0.149	0.147	0.147	0.145	0.588
98.833	9.81	0.397	0.093	0.38	0.166	0.377	0.0996	0.26	0.113	0.0284	0.0194	0.1	0.048	0.148	0.146	0.146	0.144	0.584
98.917	9.775	0.395	0.0928	0.378	0.166	0.376	0.0991	0.259	0.113	0.0284	0.0194	0.1	0.048	0.147	0.146	0.145	0.144	0.582
99	9.739	0.394	0.0927	0.377	0.165	0.374	0.0987	0.258	0.113	0.0284	0.0194	0.1	0.048	0.147	0.145	0.145	0.143	0.58
99.083	9.704	0.392	0.0926	0.375	0.164	0.372	0.0983	0.258	0.112	0.0284	0.0194	0.1	0.048	0.146	0.145	0.144	0.142	0.577
99.167	9.669	0.391	0.0925	0.373	0.164	0.371	0.0979	0.257	0.112	0.0284	0.0194	0.1	0.048	0.145	0.144	0.143	0.142	0.574
99.25	9.633	0.389	0.0923	0.372	0.163	0.369	0.0975	0.256	0.111	0.0284	0.0194	0.1	0.048	0.145	0.143	0.143	0.141	0.572
99.333	9.599	0.388	0.0922	0.37	0.163	0.368	0.0972	0.256	0.111	0.0284	0.0194	0.1	0.048	0.144	0.143	0.142	0.14	0.569

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
99.417	9.564	0.386	0.0921	0.369	0.162	0.366	0.0968	0.255	0.111	0.0284	0.0194	0.1	0.048	0.144	0.142	0.142	0.14	0.568
99.5	9.529	0.385	0.092	0.367	0.161	0.365	0.0964	0.254	0.111	0.0284	0.0194	0.1	0.048	0.143	0.142	0.141	0.139	0.565
99.583	9.494	0.383	0.092	0.366	0.161	0.363	0.0961	0.254	0.11	0.0284	0.0194	0.1	0.048	0.142	0.141	0.14	0.139	0.562
99.667	9.46	0.382	0.0919	0.365	0.16	0.362	0.0957	0.253	0.11	0.0284	0.0194	0.1	0.048	0.142	0.14	0.14	0.138	0.56
99.75	9.425	0.381	0.0918	0.363	0.16	0.36	0.0953	0.253	0.11	0.0284	0.0194	0.1	0.048	0.141	0.14	0.139	0.138	0.558
99.833	9.391	0.379	0.0917	0.362	0.159	0.359	0.095	0.252	0.109	0.0284	0.0194	0.1	0.048	0.141	0.139	0.139	0.137	0.556
99.917	9.357	0.378	0.0917	0.36	0.159	0.357	0.0947	0.252	0.109	0.0284	0.0194	0.1	0.048	0.14	0.139	0.138	0.137	0.554
100	9.323	0.377	0.0916	0.359	0.159	0.356	0.0943	0.251	0.109	0.0284	0.0194	0.1	0.048	0.14	0.138	0.138	0.136	0.552
100.083	9.289	0.376	0.0915	0.358	0.158	0.354	0.094	0.251	0.108	0.0284	0.0194	0.1	0.048	0.139	0.138	0.137	0.135	0.549
100.167	9.255	0.375	0.0915	0.357	0.158	0.353	0.0937	0.25	0.108	0.0284	0.0194	0.1	0.048	0.139	0.137	0.137	0.135	0.548
100.25	9.221	0.373	0.0914	0.355	0.157	0.351	0.0934	0.25	0.108	0.0284	0.0194	0.1	0.048	0.138	0.137	0.136	0.134	0.545
100.333	9.188	0.372	0.0914	0.354	0.157	0.35	0.0931	0.25	0.108	0.0284	0.0194	0.1	0.048	0.138	0.136	0.136	0.134	0.544
100.417	9.154	0.371	0.0913	0.353	0.156	0.349	0.0928	0.249	0.107	0.0284	0.0194	0.1	0.048	0.137	0.136	0.135	0.134	0.542
100.5	9.121	0.37	0.0913	0.352	0.156	0.347	0.0925	0.249	0.107	0.0284	0.0194	0.1	0.048	0.137	0.135	0.135	0.133	0.54
100.583	9.088	0.369	0.0913	0.35	0.156	0.346	0.0922	0.248	0.107	0.0284	0.0194	0.1	0.048	0.136	0.135	0.134	0.133	0.538
100.667	9.054	0.368	0.0913	0.349	0.155	0.345	0.092	0.248	0.107	0.0284	0.0194	0.1	0.048	0.136	0.134	0.134	0.132	0.536
100.75	9.021	0.367	0.0912	0.348	0.155	0.343	0.0917	0.248	0.106	0.0284	0.0194	0.1	0.048	0.135	0.134	0.133	0.132	0.534
100.833	8.989	0.366	0.0912	0.347	0.154	0.342	0.0914	0.247	0.106	0.0284	0.0194	0.1	0.048	0.135	0.134	0.133	0.131	0.533
100.917	8.956	0.365	0.0912	0.346	0.154	0.341	0.0912	0.247	0.106	0.0284	0.0194	0.1	0.048	0.135	0.133	0.133	0.131	0.532
101	8.923	0.364	0.0912	0.345	0.154	0.339	0.0909	0.246	0.106	0.0284	0.0194	0.1	0.048	0.134	0.133	0.132	0.13	0.529
101.083	8.891	0.363	0.0912	0.344	0.153	0.338	0.0907	0.246	0.106	0.0284	0.0194	0.1	0.048	0.134	0.132	0.132	0.13	0.528
101.167	8.858	0.362	0.0912	0.343	0.153	0.337	0.0904	0.246	0.105	0.0284	0.0194	0.1	0.048	0.133	0.132	0.131	0.13	0.526
101.25	8.826	0.361	0.0912	0.342	0.153	0.336	0.0902	0.246	0.105	0.0284	0.0194	0.1	0.048	0.133	0.131	0.131	0.129	0.524
101.333	8.794	0.36	0.0912	0.341	0.152	0.334	0.09	0.245	0.105	0.0284	0.0194	0.1	0.048	0.133	0.131	0.131	0.129	0.524
101.417	8.761	0.36	0.0912	0.34	0.152	0.333	0.0898	0.245	0.105	0.0284	0.0194	0.1	0.048	0.132	0.131	0.13	0.128	0.521
101.5	8.729	0.359	0.0912	0.339	0.152	0.332	0.0895	0.245	0.105	0.0284	0.0194	0.1	0.048	0.132	0.13	0.13	0.128	0.52
101.583	8.698	0.358	0.0912	0.338	0.151	0.331	0.0893	0.244	0.104	0.0284	0.0194	0.1	0.048	0.131	0.13	0.129	0.128	0.518
101.667	8.666	0.357	0.0912	0.337	0.151	0.33	0.0891	0.244	0.104	0.0284	0.0194	0.1	0.048	0.131	0.13	0.129	0.127	0.517
101.75	8.634	0.356	0.0912	0.336	0.151	0.329	0.0889	0.244	0.104	0.0284	0.0194	0.1	0.048	0.131	0.129	0.129	0.127	0.516
101.833	8.603	0.356	0.0912	0.335	0.15	0.328	0.0887	0.244	0.104	0.0284	0.0194	0.1	0.048	0.13	0.129	0.128	0.127	0.514
101.917	8.571	0.355	0.0912	0.335	0.15	0.327	0.0886	0.244	0.104	0.0284	0.0194	0.1	0.048	0.13	0.129	0.128	0.126	0.513
102	8.54	0.354	0.0912	0.334	0.15	0.326	0.0884	0.243	0.104	0.0284	0.0194	0.1	0.048	0.13	0.128	0.128	0.126	0.512
102.083	8.509	0.353	0.0912	0.333	0.15	0.325	0.0882	0.243	0.104	0.0284	0.0194	0.1	0.048	0.129	0.128	0.127	0.126	0.51
102.167	8.477	0.353	0.0912	0.332	0.149	0.324	0.088	0.243	0.103	0.0284	0.0194	0.1	0.048	0.129	0.128	0.127	0.125	0.509
102.25	8.446	0.352	0.0912	0.331	0.149	0.323	0.0878	0.243	0.103	0.0284	0.0194	0.1	0.048	0.129	0.127	0.127	0.125	0.508
102.333	8.416	0.351	0.0912	0.331	0.149	0.322	0.0876	0.243	0.103	0.0284	0.0194	0.1	0.048	0.129	0.127	0.127	0.125	0.508
102.417	8.385	0.351	0.0912	0.33	0.149	0.321	0.0875	0.242	0.103	0.0284	0.0194	0.1	0.048	0.128	0.127	0.126	0.125	0.506
102.5	8.354	0.35	0.0912	0.329	0.148	0.32	0.0873	0.242	0.103	0.0284	0.0194	0.1	0.048	0.128	0.127	0.126	0.124	0.505
102.583	8.324	0.349	0.0912	0.328	0.148	0.32	0.0871	0.242	0.103	0.0284	0.0194	0.1	0.048	0.128	0.126	0.126	0.124	0.504
102.667	8.293	0.349	0.0912	0.328	0.148	0.319	0.087	0.242	0.103	0.0284	0.0194	0.1	0.048	0.127	0.126	0.125	0.124	0.502
102.75	8.263	0.348	0.0912	0.327	0.148	0.318	0.0868	0.242	0.102	0.0284	0.0194	0.1	0.048	0.127	0.126	0.125	0.123	0.501
102.833	8.232	0.348	0.0912	0.326	0.148	0.317	0.0867	0.242	0.102	0.0284	0.0194	0.1	0.048	0.127	0.125	0.125	0.123	0.5
102.917	8.202	0.347	0.0912	0.326	0.147	0.316	0.0865	0.241	0.102	0.0283	0.0194	0.1	0.0479	0.127	0.125	0.125	0.123	0.5
103	8.172	0.346	0.0911	0.325	0.147	0.316	0.0864	0.241	0.102	0.0283	0.0194	0.1	0.0478	0.126	0.125	0.124	0.123	0.498
103.083	8.142	0.346	0.0911	0.325	0.147	0.315	0.0862	0.241	0.102	0.0283	0.0193	0.1	0.0476	0.126	0.125	0.124	0.122	0.497
103.167	8.112	0.345	0.091	0.324	0.147	0.314	0.0861	0.241	0.102	0.0282	0.0193	0.1	0.0474	0.126	0.124	0.124	0.122	0.496
103.25	8.083	0.345	0.091	0.323	0.146	0.313	0.0859	0.241	0.102	0.0282	0.0192	0.1	0.0471	0.126	0.124	0.124	0.122	0.496
103.333	8.053	0.344	0.0908	0.323	0.146	0.312	0.0858	0.24	0.102	0.0281	0.0191	0.1	0.0467	0.125	0.124	0.123	0.122	0.494
103.417	8.024	0.344	0.0907	0.322	0.146	0.312	0.0856	0.24	0.101	0.028	0.0189	0.1	0.0462	0.125	0.124	0.123	0.121	0.493
103.5	7.994	0.343	0.0906	0.321	0.146	0.311	0.0855	0.24	0.101	0.0279	0.0188	0.1	0.0458	0.125	0.124	0.123	0.121	0.493
103.583	7.965	0.342	0.0904	0.321	0.146	0.31	0.0853	0.24	0.101	0.0278	0.0186	0.1	0.0452	0.125	0.123	0.123	0.121	0.492
103.667	7.936	0.342	0.0902	0.32	0.145	0.309	0.0852	0.239	0.101	0.0277	0.0185	0.1	0.0447	0.124	0.123	0.123	0.121	0.491
103.75	7.907	0.341	0.0901	0.32	0.145	0.309	0.085	0.239	0.101	0.0275	0.0183	0.1	0.0442	0.124	0.123	0.122	0.121	0.49
103.833	7.878	0.341	0.0898	0.319	0.145	0.308	0.0849	0.239	0.101	0.0274	0.0181	0.1	0.0438	0.124	0.123	0.122	0.12	0.489
103.917	7.849	0.34	0.0896	0.318	0.145	0.307	0.0847	0.238	0.101	0.0272	0.0179	0.1	0.0433	0.124	0.122	0.122	0.12	0.488
104	7.82	0.339	0.0893	0.318	0.144	0.306	0.0846	0.238	0.1	0.027	0.0177	0.1	0.0429	0.124	0.122	0.122	0.12	0.488
104.083	7.791	0.339	0.0891	0.317	0.144	0.306	0.0844	0.238	0.1	0.0268	0.0176	0.1	0.0426	0.123	0.122	0.121	0.12	0.486
104.167	7.763	0.338	0.0888	0.317	0.144	0.305	0.0842	0.237	0.1	0.0266	0.0175	0.1	0.0423	0.123	0.122	0.121	0.119	0.485
104.25	7.734	0.338	0.0885	0.316	0.144	0.304	0.0841	0.237	0.0999	0.0265	0.0173	0.1	0.042	0.123	0.121	0.121	0.119	0.484
104.333	7.706	0.337	0.0881	0.315	0.143	0.304	0.0839	0.236	0.0997	0.0263	0.0172	0.1	0.0417	0.123	0.121	0.121	0.119	0.484
104.417	7.678	0.336	0.0878	0.315	0.143	0.303	0.0838	0.236	0.0995	0.0261	0.0171	0.1	0.0415	0.122	0.121	0.12	0.119	0.482
104.5	7.649	0.336	0.0874	0.314	0.143	0.302	0.0836	0.236	0.0994	0.0259	0.017	0.1	0.0413	0.122	0.121	0.12	0.118	0.481
104.583	7.621	0.335	0.087	0.314	0.143	0.302	0.0834	0.235	0.0992	0.0258	0.0169	0.1	0.0411	0.122	0.12	0.12	0.118	0.48

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
104.667	7.594	0.335	0.0866	0.313	0.142	0.301	0.0833	0.235	0.099	0.0256	0.0168	0.1	0.041	0.122	0.12	0.12	0.118	0.48
104.75	7.566	0.334	0.0862	0.312	0.142	0.3	0.0831	0.234	0.0988	0.0255	0.0168	0.1	0.0408	0.121	0.12	0.119	0.118	0.478
104.833	7.538	0.333	0.0857	0.312	0.142	0.3	0.083	0.234	0.0987	0.0253	0.0167	0.1	0.0407	0.121	0.12	0.119	0.117	0.477
104.917	7.51	0.333	0.0853	0.311	0.142	0.299	0.0828	0.233	0.0985	0.0252	0.0166	0.1	0.0406	0.121	0.119	0.119	0.117	0.476
105	7.483	0.332	0.0849	0.31	0.141	0.298	0.0826	0.233	0.0983	0.0251	0.0166	0.1	0.0405	0.121	0.119	0.119	0.117	0.476
105.083	7.455	0.331	0.0844	0.31	0.141	0.298	0.0825	0.232	0.0981	0.025	0.0165	0.1	0.0404	0.12	0.119	0.118	0.117	0.474
105.167	7.428	0.331	0.084	0.309	0.141	0.297	0.0823	0.231	0.0979	0.0249	0.0165	0.1	0.0404	0.12	0.119	0.118	0.116	0.473
105.25	7.4	0.33	0.0836	0.309	0.14	0.296	0.0821	0.231	0.0977	0.0248	0.0164	0.1	0.0403	0.12	0.118	0.118	0.116	0.472
105.333	7.373	0.329	0.0832	0.308	0.14	0.296	0.0819	0.23	0.0975	0.0247	0.0164	0.1	0.0403	0.12	0.118	0.118	0.116	0.472
105.417	7.346	0.329	0.0828	0.307	0.14	0.295	0.0818	0.23	0.0973	0.0246	0.0164	0.1	0.0403	0.119	0.118	0.117	0.116	0.47
105.5	7.319	0.328	0.0824	0.307	0.14	0.294	0.0816	0.229	0.097	0.0245	0.0163	0.1	0.0403	0.119	0.118	0.117	0.115	0.469
105.583	7.292	0.327	0.082	0.306	0.139	0.294	0.0814	0.228	0.0968	0.0244	0.0163	0.1	0.0403	0.119	0.117	0.117	0.115	0.468
105.667	7.266	0.327	0.0816	0.305	0.139	0.293	0.0812	0.228	0.0966	0.0244	0.0163	0.1	0.0403	0.119	0.117	0.117	0.115	0.468
105.75	7.239	0.326	0.0813	0.305	0.139	0.293	0.0811	0.227	0.0964	0.0243	0.0163	0.1	0.0403	0.118	0.117	0.116	0.115	0.466
105.833	7.212	0.325	0.081	0.304	0.138	0.292	0.0809	0.226	0.0961	0.0242	0.0163	0.1	0.0403	0.118	0.117	0.116	0.114	0.465
105.917	7.186	0.324	0.0806	0.303	0.138	0.291	0.0807	0.225	0.0959	0.0242	0.0163	0.1	0.0403	0.118	0.116	0.116	0.114	0.464
106	7.159	0.324	0.0803	0.303	0.138	0.291	0.0805	0.225	0.0957	0.0241	0.0163	0.1	0.0403	0.118	0.116	0.116	0.114	0.464
106.083	7.133	0.323	0.08	0.302	0.137	0.29	0.0803	0.224	0.0954	0.0241	0.0163	0.1	0.0403	0.117	0.116	0.115	0.114	0.462
106.167	7.107	0.322	0.0797	0.301	0.137	0.29	0.0802	0.223	0.0951	0.024	0.0163	0.1	0.0403	0.117	0.116	0.115	0.113	0.461
106.25	7.081	0.321	0.0794	0.301	0.137	0.289	0.08	0.222	0.0949	0.024	0.0163	0.1	0.0403	0.117	0.115	0.115	0.113	0.46
106.333	7.055	0.321	0.0791	0.3	0.136	0.288	0.0798	0.222	0.0946	0.0239	0.0163	0.1	0.0403	0.117	0.115	0.115	0.113	0.46
106.417	7.029	0.32	0.0789	0.299	0.136	0.288	0.0796	0.221	0.0944	0.0239	0.0163	0.1	0.0403	0.116	0.115	0.114	0.112	0.457
106.5	7.003	0.319	0.0786	0.299	0.136	0.287	0.0794	0.22	0.0941	0.0239	0.0163	0.1	0.0403	0.116	0.115	0.114	0.112	0.457
106.583	6.977	0.318	0.0784	0.298	0.135	0.287	0.0792	0.219	0.0938	0.0238	0.0163	0.1	0.0403	0.116	0.114	0.114	0.112	0.456
106.667	6.952	0.318	0.0782	0.297	0.135	0.286	0.079	0.219	0.0936	0.0238	0.0163	0.1	0.0403	0.115	0.114	0.113	0.112	0.454
106.75	6.926	0.317	0.0779	0.297	0.135	0.285	0.0788	0.218	0.0933	0.0238	0.0163	0.1	0.0403	0.115	0.114	0.113	0.111	0.453
106.833	6.901	0.316	0.0777	0.296	0.134	0.285	0.0786	0.217	0.093	0.0238	0.0163	0.1	0.0403	0.115	0.113	0.113	0.111	0.452
106.917	6.875	0.315	0.0775	0.295	0.134	0.284	0.0785	0.217	0.0928	0.0237	0.0163	0.1	0.0403	0.115	0.113	0.113	0.111	0.452
107	6.85	0.314	0.0773	0.295	0.134	0.284	0.0783	0.216	0.0925	0.0237	0.0163	0.1	0.0403	0.114	0.113	0.112	0.111	0.45
107.083	6.825	0.314	0.0772	0.294	0.133	0.283	0.0781	0.215	0.0922	0.0237	0.0163	0.1	0.0403	0.114	0.113	0.112	0.11	0.449
107.167	6.8	0.313	0.077	0.293	0.133	0.282	0.0779	0.215	0.092	0.0237	0.0163	0.1	0.0403	0.114	0.112	0.112	0.11	0.448
107.25	6.775	0.312	0.0768	0.292	0.133	0.282	0.0777	0.214	0.0917	0.0237	0.0163	0.1	0.0403	0.113	0.112	0.111	0.11	0.446
107.333	6.75	0.311	0.0766	0.292	0.132	0.281	0.0774	0.213	0.0915	0.0237	0.0163	0.1	0.0403	0.113	0.112	0.111	0.109	0.445
107.417	6.725	0.31	0.0765	0.291	0.132	0.281	0.0772	0.213	0.0912	0.0237	0.0163	0.1	0.0403	0.113	0.111	0.111	0.109	0.444
107.5	6.7	0.31	0.0763	0.29	0.132	0.28	0.077	0.212	0.091	0.0237	0.0163	0.1	0.0403	0.113	0.111	0.111	0.109	0.444
107.583	6.676	0.309	0.0762	0.289	0.131	0.28	0.0768	0.212	0.0908	0.0237	0.0163	0.1	0.0403	0.112	0.111	0.11	0.109	0.442
107.667	6.651	0.308	0.076	0.289	0.131	0.279	0.0766	0.211	0.0905	0.0237	0.0163	0.1	0.0403	0.112	0.111	0.11	0.108	0.441
107.75	6.626	0.307	0.0759	0.288	0.13	0.278	0.0764	0.211	0.0903	0.0237	0.0163	0.1	0.0403	0.112	0.11	0.11	0.108	0.44
107.833	6.602	0.306	0.0757	0.287	0.13	0.278	0.0762	0.21	0.0901	0.0237	0.0163	0.1	0.0403	0.111	0.11	0.109	0.108	0.438
107.917	6.578	0.305	0.0756	0.286	0.13	0.277	0.076	0.21	0.0899	0.0237	0.0163	0.1	0.0403	0.111	0.11	0.109	0.107	0.437
108	6.554	0.305	0.0755	0.286	0.129	0.277	0.0758	0.209	0.0896	0.0237	0.0163	0.1	0.0403	0.111	0.109	0.109	0.107	0.436
108.083	6.53	0.304	0.0753	0.285	0.129	0.276	0.0756	0.209	0.0894	0.0237	0.0163	0.1	0.0403	0.111	0.109	0.109	0.107	0.436
108.167	6.506	0.303	0.0752	0.284	0.129	0.276	0.0754	0.208	0.0892	0.0237	0.0163	0.1	0.0403	0.11	0.109	0.108	0.106	0.433
108.25	6.482	0.302	0.0751	0.283	0.129	0.275	0.0752	0.208	0.089	0.0237	0.0163	0.1	0.0403	0.11	0.108	0.108	0.106	0.432
108.333	6.458	0.302	0.075	0.283	0.128	0.275	0.075	0.207	0.0888	0.0237	0.0163	0.1	0.0403	0.11	0.108	0.108	0.106	0.432
108.417	6.434	0.301	0.0749	0.282	0.128	0.274	0.0749	0.207	0.0886	0.0237	0.0163	0.1	0.0403	0.109	0.108	0.107	0.106	0.43
108.5	6.41	0.3	0.0748	0.281	0.128	0.273	0.0747	0.206	0.0884	0.0237	0.0163	0.1	0.0403	0.109	0.108	0.107	0.105	0.429
108.583	6.387	0.3	0.0747	0.281	0.127	0.273	0.0745	0.206	0.0882	0.0237	0.0163	0.1	0.0403	0.109	0.107	0.107	0.105	0.428
108.667	6.363	0.299	0.0746	0.28	0.127	0.272	0.0743	0.206	0.0881	0.0237	0.0163	0.1	0.0403	0.109	0.107	0.107	0.105	0.428
108.75	6.34	0.298	0.0745	0.279	0.127	0.272	0.0742	0.205	0.0879	0.0237	0.0163	0.1	0.0403	0.108	0.107	0.106	0.105	0.426
108.833	6.317	0.297	0.0744	0.279	0.127	0.271	0.074	0.205	0.0877	0.0237	0.0163	0.1	0.0403	0.108	0.107	0.106	0.104	0.425
108.917	6.293	0.297	0.0744	0.278	0.126	0.271	0.0738	0.204	0.0875	0.0237	0.0163	0.1	0.0403	0.108	0.106	0.106	0.104	0.424
109	6.27	0.296	0.0743	0.277	0.126	0.27	0.0736	0.204	0.0873	0.0237	0.0163	0.1	0.0403	0.108	0.106	0.106	0.104	0.424
109.083	6.247	0.296	0.0742	0.277	0.126	0.27	0.0735	0.204	0.0872	0.0237	0.0163	0.1	0.0403	0.107	0.106	0.105	0.104	0.422
109.167	6.224	0.295	0.0742	0.276	0.126	0.269	0.0733	0.203	0.087	0.0237	0.0163	0.1	0.0403	0.107	0.106	0.105	0.103	0.421
109.25	6.201	0.294	0.0741	0.276	0.125	0.268	0.0732	0.203	0.0868	0.0237	0.0163	0.1	0.0403	0.107	0.105	0.105	0.103	0.42
109.333	6.179	0.294	0.0741	0.275	0.125	0.268	0.073	0.203	0.0867	0.0237	0.0163	0.1	0.0403	0.107	0.105	0.105	0.103	0.42
109.417	6.156	0.293	0.074	0.274	0.125	0.267	0.0728	0.202	0.0865	0.0237	0.0163	0.1	0.0403	0.106	0.105	0.104	0.103	0.418
109.5	6.133	0.292	0.074	0.274	0.125	0.267	0.0727	0.202	0.0863	0.0237	0.0163	0.1	0.0403	0.106	0.105	0.104	0.102	0.417
109.583	6.111	0.292	0.074	0.273	0.124	0.266	0.0725	0.202	0.0862	0.0237	0.0163	0.1	0.0403	0.106	0.104	0.104	0.102	0.416
109.667	6.088	0.291	0.0739	0.273	0.124	0.266	0.0724	0.202	0.086	0.0237	0.0163	0.1	0.0403	0.106	0.104	0.104	0.102	0.416
109.75	6.066	0.291	0.0739	0.272	0.124	0.265	0.0723	0.201	0.0859	0.0237	0.0163	0.1	0.0403	0.105	0.104	0.103	0.102	0.414
109.833	6.043	0.29	0.0739	0.272	0.124	0.264	0.0721	0.201	0.0858	0.0237	0.0163	0.1	0.0403	0.105	0.104	0.103	0.101	0.413

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
109.917	6.021	0.29	0.0739	0.271	0.123	0.264	0.072	0.201	0.0856	0.0237	0.0163	0.1	0.0403	0.105	0.104	0.103	0.101	0.413
110	5.999	0.289	0.0739	0.27	0.123	0.263	0.0718	0.2	0.0855	0.0237	0.0163	0.1	0.0403	0.105	0.103	0.103	0.101	0.412
110.083	5.977	0.289	0.0738	0.27	0.123	0.263	0.0717	0.2	0.0854	0.0237	0.0163	0.1	0.0403	0.105	0.103	0.103	0.101	0.412
110.167	5.955	0.288	0.0738	0.269	0.123	0.262	0.0716	0.2	0.0852	0.0237	0.0163	0.1	0.0403	0.104	0.103	0.102	0.101	0.41
110.25	5.933	0.288	0.0738	0.269	0.123	0.262	0.0715	0.2	0.0851	0.0237	0.0163	0.1	0.0403	0.104	0.103	0.102	0.1	0.409
110.333	5.911	0.287	0.0738	0.268	0.122	0.261	0.0714	0.199	0.085	0.0237	0.0163	0.1	0.0403	0.104	0.103	0.102	0.1	0.409
110.417	5.889	0.287	0.0738	0.268	0.122	0.261	0.0712	0.199	0.0849	0.0237	0.0163	0.1	0.0403	0.104	0.102	0.102	0.1	0.408
110.5	5.868	0.286	0.0738	0.267	0.122	0.26	0.0711	0.199	0.0847	0.0237	0.0163	0.1	0.0403	0.104	0.102	0.102	0.0999	0.4079
110.583	5.846	0.286	0.0738	0.267	0.122	0.26	0.071	0.199	0.0846	0.0237	0.0163	0.1	0.0403	0.103	0.102	0.101	0.0997	0.4057
110.667	5.825	0.285	0.0738	0.267	0.122	0.259	0.0709	0.198	0.0845	0.0237	0.0163	0.1	0.0403	0.103	0.102	0.101	0.0995	0.4055
110.75	5.803	0.285	0.0738	0.266	0.122	0.258	0.0708	0.198	0.0844	0.0237	0.0163	0.1	0.0403	0.103	0.102	0.101	0.0993	0.4053
110.833	5.782	0.285	0.0738	0.266	0.121	0.258	0.0707	0.198	0.0843	0.0237	0.0163	0.1	0.0403	0.103	0.101	0.101	0.0992	0.4042
110.917	5.761	0.284	0.0738	0.265	0.121	0.258	0.0706	0.198	0.0842	0.0237	0.0163	0.1	0.0403	0.103	0.101	0.101	0.099	0.404
111	5.74	0.284	0.0738	0.265	0.121	0.257	0.0705	0.198	0.0841	0.0237	0.0163	0.1	0.0403	0.103	0.101	0.101	0.0988	0.4038
111.083	5.718	0.283	0.0738	0.264	0.121	0.257	0.0704	0.197	0.084	0.0237	0.0163	0.1	0.0403	0.102	0.101	0.1	0.0987	0.4017
111.167	5.697	0.283	0.0738	0.264	0.121	0.256	0.0703	0.197	0.0839	0.0237	0.0163	0.1	0.0403	0.102	0.101	0.1	0.0985	0.4015
111.25	5.676	0.283	0.0738	0.264	0.121	0.256	0.0702	0.197	0.0838	0.0237	0.0163	0.1	0.0403	0.102	0.101	0.1	0.0983	0.4013
111.333	5.656	0.282	0.0738	0.263	0.12	0.255	0.0701	0.197	0.0837	0.0237	0.0163	0.1	0.0403	0.102	0.101	0.1	0.0982	0.4012
111.417	5.635	0.282	0.0738	0.263	0.12	0.255	0.07	0.197	0.0836	0.0237	0.0163	0.1	0.0403	0.102	0.1	0.0998	0.098	0.3998
111.5	5.614	0.281	0.0738	0.262	0.12	0.254	0.0699	0.196	0.0835	0.0237	0.0163	0.1	0.0403	0.102	0.1	0.0997	0.0979	0.3996
111.583	5.593	0.281	0.0738	0.262	0.12	0.254	0.0698	0.196	0.0834	0.0237	0.0163	0.1	0.0403	0.102	0.1	0.0995	0.0977	0.3992
111.667	5.573	0.281	0.0738	0.262	0.12	0.254	0.0697	0.196	0.0833	0.0237	0.0163	0.1	0.0403	0.101	0.0999	0.0994	0.0976	0.3979
111.75	5.552	0.28	0.0738	0.261	0.12	0.253	0.0696	0.196	0.0833	0.0237	0.0163	0.1	0.0403	0.101	0.0998	0.0993	0.0975	0.3976
111.833	5.532	0.28	0.0738	0.261	0.12	0.253	0.0695	0.196	0.0832	0.0237	0.0163	0.1	0.0403	0.101	0.0997	0.0991	0.0973	0.3971
111.917	5.512	0.28	0.0738	0.261	0.119	0.252	0.0694	0.196	0.0831	0.0237	0.0162	0.1	0.0403	0.101	0.0995	0.099	0.0972	0.3967
112	5.491	0.279	0.0738	0.26	0.119	0.252	0.0694	0.195	0.083	0.0237	0.0162	0.1	0.0402	0.101	0.0994	0.0989	0.0971	0.3964
112.083	5.471	0.279	0.0738	0.26	0.119	0.251	0.0693	0.195	0.0829	0.0236	0.0162	0.1	0.04	0.101	0.0993	0.0987	0.0969	0.3959
112.167	5.451	0.279	0.0737	0.26	0.119	0.251	0.0692	0.195	0.0828	0.0236	0.0161	0.1	0.0399	0.101	0.0991	0.0986	0.0968	0.3955
112.25	5.431	0.278	0.0737	0.259	0.119	0.251	0.0691	0.195	0.0827	0.0236	0.0161	0.1	0.0397	0.1	0.099	0.0985	0.0967	0.3942
112.333	5.411	0.278	0.0736	0.259	0.119	0.25	0.069	0.195	0.0826	0.0235	0.016	0.1	0.0393	0.1	0.0989	0.0983	0.0965	0.3937
112.417	5.391	0.278	0.0735	0.259	0.119	0.25	0.0689	0.194	0.0825	0.0234	0.0159	0.1	0.0389	0.1	0.0987	0.0982	0.0964	0.3933
112.5	5.371	0.277	0.0734	0.258	0.118	0.249	0.0688	0.194	0.0824	0.0233	0.0158	0.1	0.0385	0.1	0.0986	0.098	0.0962	0.3928
112.583	5.352	0.277	0.0732	0.258	0.118	0.249	0.0687	0.194	0.0822	0.0232	0.0156	0.1	0.038	0.0999	0.0984	0.0979	0.0961	0.3923
112.667	5.332	0.277	0.073	0.257	0.118	0.248	0.0686	0.194	0.0821	0.0231	0.0154	0.1	0.0375	0.0998	0.0983	0.0977	0.096	0.3918
112.75	5.312	0.276	0.0729	0.257	0.118	0.248	0.0685	0.193	0.082	0.023	0.0153	0.1	0.0369	0.0996	0.0981	0.0976	0.0958	0.3911
112.833	5.293	0.276	0.0727	0.257	0.118	0.248	0.0684	0.193	0.0818	0.0228	0.0151	0.1	0.0365	0.0995	0.098	0.0975	0.0957	0.3907
112.917	5.273	0.275	0.0724	0.256	0.118	0.247	0.0683	0.193	0.0817	0.0227	0.0149	0.1	0.036	0.0993	0.0979	0.0973	0.0955	0.39
113	5.254	0.275	0.0722	0.256	0.117	0.247	0.0682	0.192	0.0816	0.0225	0.0147	0.1	0.0355	0.0992	0.0977	0.0972	0.0954	0.3895
113.083	5.235	0.274	0.072	0.256	0.117	0.246	0.0681	0.192	0.0814	0.0223	0.0146	0.1	0.0352	0.099	0.0976	0.097	0.0952	0.3888
113.167	5.215	0.274	0.0717	0.255	0.117	0.246	0.068	0.192	0.0813	0.0221	0.0144	0.1	0.0348	0.0989	0.0974	0.0969	0.0951	0.3883
113.25	5.196	0.274	0.0714	0.255	0.117	0.245	0.0679	0.191	0.0811	0.022	0.0143	0.1	0.0345	0.0987	0.0972	0.0967	0.0949	0.3875
113.333	5.177	0.273	0.0711	0.254	0.117	0.245	0.0678	0.191	0.081	0.0218	0.0141	0.1	0.0342	0.0986	0.0971	0.0965	0.0947	0.3869
113.417	5.158	0.273	0.0707	0.254	0.116	0.245	0.0676	0.19	0.0808	0.0216	0.014	0.1	0.034	0.0984	0.0969	0.0964	0.0946	0.3863
113.5	5.139	0.272	0.0704	0.254	0.116	0.244	0.0675	0.19	0.0807	0.0214	0.0139	0.1	0.0338	0.0982	0.0968	0.0962	0.0944	0.3856
113.583	5.12	0.272	0.07	0.253	0.116	0.244	0.0674	0.19	0.0805	0.0212	0.0138	0.1	0.0336	0.0981	0.0966	0.096	0.0942	0.3849
113.667	5.102	0.271	0.0696	0.253	0.116	0.243	0.0673	0.189	0.0803	0.0211	0.0137	0.1	0.0334	0.0979	0.0964	0.0959	0.0941	0.3843
113.75	5.083	0.271	0.0692	0.252	0.116	0.243	0.0672	0.189	0.0801	0.0209	0.0136	0.1	0.0332	0.0977	0.0963	0.0957	0.0939	0.3836
113.833	5.064	0.27	0.0688	0.252	0.115	0.242	0.067	0.188	0.0799	0.0208	0.0136	0.1	0.0331	0.0975	0.0961	0.0955	0.0937	0.3828
113.917	5.045	0.27	0.0683	0.251	0.115	0.242	0.0669	0.188	0.0798	0.0207	0.0135	0.1	0.033	0.0974	0.0959	0.0953	0.0935	0.3821
114	5.027	0.269	0.0679	0.251	0.115	0.241	0.0668	0.187	0.0796	0.0205	0.0134	0.1	0.0329	0.0972	0.0957	0.0952	0.0934	0.3815
114.083	5.009	0.268	0.0675	0.25	0.115	0.241	0.0666	0.187	0.0794	0.0204	0.0134	0.1	0.0328	0.097	0.0955	0.095	0.0932	0.3807
114.167	4.99	0.268	0.067	0.25	0.114	0.24	0.0665	0.186	0.0792	0.0203	0.0133	0.1	0.0327	0.0968	0.0953	0.0948	0.093	0.3799
114.25	4.972	0.267	0.0666	0.25	0.114	0.24	0.0663	0.185	0.079	0.0202	0.0133	0.1	0.0327	0.0966	0.0951	0.0946	0.0928	0.3791
114.333	4.954	0.267	0.0662	0.249	0.114	0.239	0.0662	0.185	0.0788	0.0201	0.0132	0.1	0.0326	0.0964	0.0949	0.0944	0.0926	0.3783
114.417	4.935	0.266	0.0658	0.249	0.114	0.239	0.066	0.184	0.0786	0.02	0.0132	0.1	0.0326	0.0962	0.0947	0.0942	0.0924	0.3775
114.5	4.917	0.266	0.0654	0.248	0.113	0.239	0.0659	0.184	0.0784	0.0199	0.0132	0.1	0.0326	0.096	0.0945	0.094	0.0922	0.3767
114.583	4.899	0.265	0.065	0.247	0.113	0.238	0.0657	0.183	0.0781	0.0198	0.0132	0.1	0.0326	0.0958	0.0943	0.0938	0.092	0.3759
114.667	4.881	0.264	0.0646	0.247	0.113	0.238	0.0656	0.182	0.0779	0.0198	0.0131	0.1	0.0326	0.0956	0.0941	0.0936	0.0918	0.3751
114.75	4.863	0.264	0.0642	0.246	0.112	0.237	0.0654	0.182	0.0777	0.0197	0.0131	0.1	0.0326	0.0954	0.0939	0.0934	0.0916	0.3743
114.833	4.845	0.263	0.0639	0.246	0.112	0.237	0.0653	0.181	0.0775	0.0196	0.0131	0.1	0.0326	0.0952	0.0937	0.0932	0.0914	0.3735
114.917	4.828	0.262	0.0636	0.245	0.112	0.236	0.0651	0.18	0.0772	0.0196	0.0131	0.1	0.0326	0.095	0.0935	0.0929	0.0911	0.3725
115	4.81	0.262	0.0632	0.245	0.112	0.236	0.065	0.179	0.077	0.0195	0.0131	0.1	0.0326	0.0948	0.0933	0.0927	0.0909	0.3717
115.083	4.792	0.261	0.0629	0.244	0.111	0.235	0.0648	0.179	0.0767	0.0194	0.0131	0.1	0.0326	0.0945	0.0931	0.0925	0.0907	0.3708

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
115.167	4.775	0.26	0.0626	0.244	0.111	0.235	0.0646	0.178	0.0765	0.0194	0.0131	0.1	0.0326	0.0943	0.0928	0.0923	0.0905	0.3699
115.25	4.757	0.26	0.0623	0.243	0.111	0.234	0.0645	0.177	0.0762	0.0193	0.0131	0.1	0.0326	0.0941	0.0926	0.0921	0.0902	0.369
115.333	4.74	0.259	0.062	0.243	0.11	0.234	0.0643	0.176	0.076	0.0193	0.0131	0.1	0.0326	0.0938	0.0924	0.0918	0.09	0.368
115.417	4.722	0.258	0.0618	0.242	0.11	0.233	0.0641	0.176	0.0757	0.0193	0.0131	0.1	0.0326	0.0936	0.0921	0.0916	0.0898	0.3671
115.5	4.705	0.258	0.0615	0.241	0.11	0.233	0.064	0.175	0.0755	0.0192	0.0131	0.1	0.0326	0.0934	0.0919	0.0914	0.0895	0.3662
115.583	4.688	0.257	0.0613	0.241	0.109	0.232	0.0638	0.174	0.0752	0.0192	0.0131	0.1	0.0326	0.0931	0.0917	0.0911	0.0893	0.3652
115.667	4.671	0.256	0.061	0.24	0.109	0.232	0.0636	0.173	0.0749	0.0192	0.0131	0.1	0.0326	0.0929	0.0914	0.0909	0.0891	0.3643
115.75	4.654	0.255	0.0608	0.24	0.109	0.231	0.0634	0.173	0.0747	0.0191	0.0131	0.1	0.0326	0.0927	0.0912	0.0906	0.0888	0.3633
115.833	4.637	0.255	0.0606	0.239	0.108	0.231	0.0632	0.172	0.0744	0.0191	0.0131	0.1	0.0326	0.0924	0.0909	0.0904	0.0886	0.3623
115.917	4.62	0.254	0.0604	0.238	0.108	0.23	0.0631	0.171	0.0741	0.0191	0.0131	0.1	0.0326	0.0922	0.0907	0.0901	0.0883	0.3613
116	4.603	0.253	0.0602	0.238	0.108	0.23	0.0629	0.171	0.0738	0.0191	0.0131	0.1	0.0326	0.0919	0.0904	0.0899	0.0881	0.3603
116.083	4.586	0.252	0.06	0.237	0.107	0.229	0.0627	0.17	0.0736	0.019	0.0131	0.1	0.0326	0.0916	0.0902	0.0896	0.0878	0.3592
116.167	4.569	0.252	0.0598	0.236	0.107	0.229	0.0625	0.169	0.0733	0.019	0.0131	0.1	0.0326	0.0914	0.0899	0.0894	0.0876	0.3583
116.25	4.552	0.251	0.0596	0.236	0.106	0.228	0.0623	0.169	0.0731	0.019	0.0131	0.1	0.0326	0.0911	0.0897	0.0891	0.0873	0.3572
116.333	4.535	0.25	0.0594	0.235	0.106	0.228	0.0621	0.168	0.0728	0.019	0.0131	0.1	0.0326	0.0909	0.0894	0.0888	0.087	0.3561
116.417	4.519	0.249	0.0593	0.234	0.106	0.227	0.0619	0.168	0.0726	0.019	0.0131	0.1	0.0326	0.0906	0.0891	0.0886	0.0868	0.3551
116.5	4.502	0.248	0.0591	0.234	0.105	0.227	0.0617	0.167	0.0723	0.019	0.0131	0.1	0.0326	0.0903	0.0889	0.0883	0.0865	0.354
116.583	4.486	0.248	0.0589	0.233	0.105	0.226	0.0615	0.166	0.0721	0.019	0.0131	0.1	0.0326	0.0901	0.0886	0.088	0.0862	0.3529
116.667	4.469	0.247	0.0588	0.232	0.105	0.226	0.0613	0.166	0.0718	0.019	0.0131	0.1	0.0326	0.0898	0.0883	0.0878	0.0859	0.3518
116.75	4.453	0.246	0.0586	0.232	0.104	0.225	0.0611	0.165	0.0716	0.019	0.0131	0.1	0.0326	0.0895	0.088	0.0875	0.0857	0.3507
116.833	4.437	0.245	0.0585	0.231	0.104	0.224	0.0609	0.165	0.0714	0.019	0.0131	0.1	0.0326	0.0892	0.0877	0.0872	0.0854	0.3495
116.917	4.42	0.244	0.0584	0.23	0.104	0.224	0.0607	0.164	0.0712	0.019	0.0131	0.1	0.0326	0.0889	0.0875	0.0869	0.0851	0.3484
117	4.404	0.243	0.0582	0.229	0.103	0.223	0.0605	0.164	0.0709	0.019	0.0131	0.1	0.0326	0.0887	0.0872	0.0866	0.0848	0.3473
117.083	4.388	0.243	0.0581	0.229	0.103	0.223	0.0603	0.163	0.0707	0.019	0.0131	0.1	0.0326	0.0884	0.0869	0.0863	0.0845	0.3461
117.167	4.372	0.242	0.058	0.228	0.103	0.222	0.0601	0.163	0.0705	0.019	0.0131	0.1	0.0326	0.0881	0.0866	0.0861	0.0842	0.345
117.25	4.356	0.241	0.0578	0.227	0.102	0.222	0.0599	0.162	0.0703	0.019	0.0131	0.1	0.0326	0.0878	0.0863	0.0858	0.084	0.3439
117.333	4.34	0.24	0.0577	0.227	0.102	0.221	0.0597	0.162	0.0701	0.019	0.0131	0.1	0.0326	0.0875	0.0861	0.0855	0.0837	0.3428
117.417	4.324	0.24	0.0576	0.226	0.102	0.221	0.0595	0.161	0.0699	0.019	0.0131	0.1	0.0326	0.0873	0.0858	0.0852	0.0834	0.3417
117.5	4.308	0.239	0.0575	0.225	0.101	0.22	0.0593	0.161	0.0697	0.019	0.0131	0.1	0.0326	0.087	0.0855	0.085	0.0831	0.3406
117.583	4.293	0.238	0.0574	0.225	0.101	0.22	0.0591	0.16	0.0695	0.019	0.0131	0.1	0.0326	0.0867	0.0852	0.0847	0.0829	0.3395
117.667	4.277	0.238	0.0573	0.224	0.101	0.219	0.059	0.16	0.0693	0.019	0.0131	0.1	0.0326	0.0865	0.085	0.0844	0.0826	0.3385
117.75	4.261	0.237	0.0572	0.223	0.101	0.219	0.0588	0.16	0.0692	0.019	0.0131	0.1	0.0326	0.0862	0.0847	0.0842	0.0823	0.3374
117.833	4.246	0.236	0.0572	0.223	0.1	0.218	0.0586	0.159	0.069	0.019	0.0131	0.1	0.0326	0.0859	0.0845	0.0839	0.0821	0.3364
117.917	4.23	0.235	0.0571	0.222	0.1	0.217	0.0584	0.159	0.0688	0.019	0.0131	0.1	0.0326	0.0857	0.0842	0.0837	0.0818	0.3354
118	4.215	0.235	0.057	0.221	0.0997	0.217	0.0583	0.158	0.0686	0.019	0.0131	0.1	0.0326	0.0854	0.0839	0.0834	0.0816	0.3343
118.083	4.199	0.234	0.0569	0.221	0.0995	0.216	0.0581	0.158	0.0684	0.019	0.013	0.1	0.0324	0.0852	0.0837	0.0832	0.0813	0.3334
118.167	4.184	0.233	0.0568	0.22	0.0992	0.216	0.0579	0.158	0.0682	0.019	0.013	0.1	0.0323	0.0849	0.0834	0.0829	0.0811	0.3323
118.25	4.169	0.233	0.0567	0.219	0.0989	0.215	0.0578	0.157	0.0681	0.0189	0.013	0.1	0.0322	0.0847	0.0832	0.0826	0.0808	0.3313
118.333	4.153	0.232	0.0566	0.219	0.0987	0.215	0.0576	0.157	0.0679	0.0189	0.0129	0.1	0.0318	0.0844	0.0829	0.0824	0.0806	0.3303
118.417	4.138	0.231	0.0564	0.218	0.0984	0.214	0.0574	0.156	0.0677	0.0188	0.0128	0.1	0.0315	0.0842	0.0827	0.0821	0.0803	0.3293
118.5	4.123	0.231	0.0563	0.217	0.0981	0.213	0.0572	0.156	0.0675	0.0187	0.0127	0.1	0.0311	0.0839	0.0824	0.0819	0.0801	0.3283
118.583	4.108	0.23	0.0561	0.217	0.0979	0.213	0.0571	0.156	0.0673	0.0186	0.0125	0.1	0.0306	0.0837	0.0822	0.0816	0.0798	0.3273
118.667	4.093	0.229	0.0559	0.216	0.0976	0.212	0.0569	0.155	0.0671	0.0185	0.0124	0.1	0.0301	0.0834	0.0819	0.0814	0.0796	0.3263
118.75	4.078	0.229	0.0557	0.216	0.0973	0.211	0.0567	0.155	0.0669	0.0184	0.0122	0.1	0.0295	0.0832	0.0817	0.0811	0.0793	0.3253
118.833	4.063	0.228	0.0555	0.215	0.097	0.211	0.0565	0.154	0.0667	0.0183	0.012	0.1	0.029	0.0829	0.0814	0.0809	0.079	0.3242
118.917	4.048	0.227	0.0553	0.214	0.0967	0.21	0.0564	0.154	0.0665	0.0181	0.0118	0.1	0.0285	0.0826	0.0812	0.0806	0.0788	0.3232
119	4.034	0.227	0.055	0.214	0.0965	0.209	0.0562	0.153	0.0663	0.018	0.0116	0.1	0.028	0.0824	0.0809	0.0804	0.0785	0.3222
119.083	4.019	0.226	0.0548	0.213	0.0962	0.209	0.056	0.153	0.0661	0.0178	0.0115	0.1	0.0277	0.0821	0.0806	0.0801	0.0783	0.3211
119.167	4.004	0.225	0.0545	0.212	0.0959	0.208	0.0559	0.152	0.0659	0.0176	0.0113	0.1	0.0273	0.0819	0.0804	0.0798	0.078	0.3201
119.25	3.99	0.225	0.0542	0.212	0.0956	0.208	0.0557	0.151	0.0657	0.0174	0.0112	0.1	0.0269	0.0816	0.0801	0.0796	0.0778	0.3191
119.333	3.975	0.224	0.0539	0.211	0.0953	0.207	0.0555	0.151	0.0654	0.0172	0.011	0.1	0.0267	0.0814	0.0799	0.0793	0.0775	0.3181
119.417	3.961	0.223	0.0536	0.21	0.095	0.206	0.0553	0.15	0.0652	0.017	0.0109	0.1	0.0264	0.0811	0.0796	0.0791	0.0772	0.317
119.5	3.946	0.223	0.0533	0.21	0.0947	0.206	0.0552	0.15	0.065	0.0168	0.0108	0.1	0.0262	0.0808	0.0794	0.0788	0.077	0.316
119.583	3.932	0.222	0.0529	0.209	0.0944	0.205	0.055	0.149	0.0648	0.0167	0.0107	0.1	0.026	0.0806	0.0791	0.0785	0.0767	0.3149
119.667	3.917	0.221	0.0525	0.208	0.0941	0.204	0.0548	0.148	0.0646	0.0165	0.0106	0.1	0.0258	0.0803	0.0788	0.0783	0.0765	0.3139
119.75	3.903	0.221	0.0521	0.208	0.0938	0.204	0.0546	0.148	0.0643	0.0163	0.0105	0.1	0.0256	0.0801	0.0786	0.078	0.0762	0.3129
119.833	3.889	0.22	0.0517	0.207	0.0935	0.203	0.0544	0.147	0.0641	0.0162	0.0104	0.1	0.0255	0.0798	0.0783	0.0778	0.0759	0.3118
119.917	3.875	0.219	0.0513	0.206	0.0932	0.202	0.0543	0.146	0.0639	0.0161	0.0104	0.1	0.0253	0.0795	0.078	0.0775	0.0757	0.3107
120	3.86	0.218	0.0508	0.206	0.0928	0.202	0.0541	0.146	0.0636	0.0159	0.0103	0.1	0.0252	0.0793	0.0778	0.0772	0.0754	0.3097
120.083	3.846	0.218	0.0504	0.205	0.0925	0.201	0.0539	0.145	0.0634	0.0158	0.0102	0.1	0.0251	0.079	0.0775	0.077	0.0751	0.3086
120.167	3.832	0.217	0.0499	0.204	0.0922	0.201	0.0537	0.144	0.0631	0.0157	0.0102	0.1	0.025	0.0787	0.0773	0.0767	0.0749	0.3076
120.25	3.818	0.216	0.0495	0.204	0.0919	0.2	0.0535	0.143	0.0629	0.0156	0.0101	0.1	0.025	0.0785	0.077	0.0764	0.0746	0.3065
120.333	3.805	0.215	0.0491	0.203	0.0915	0.199	0.0533	0.143	0.0626	0.0155	0.0101	0.1	0.0249	0.0782	0.0767	0.0762	0.0743	0.3054

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
120.417	3.791	0.215	0.0487	0.202	0.0912	0.199	0.0532	0.142	0.0624	0.0154	0.0101	0.1	0.0249	0.0779	0.0765	0.0759	0.0741	0.3044
120.5	3.777	0.214	0.0482	0.202	0.0909	0.198	0.053	0.141	0.0621	0.0153	0.01	0.1	0.0249	0.0777	0.0762	0.0756	0.0738	0.3033
120.583	3.763	0.213	0.0479	0.201	0.0905	0.197	0.0528	0.14	0.0618	0.0152	0.00999	0.1	0.0249	0.0774	0.0759	0.0754	0.0735	0.3022
120.667	3.749	0.212	0.0475	0.2	0.0902	0.197	0.0526	0.139	0.0616	0.0151	0.00996	0.1	0.0249	0.0771	0.0756	0.0751	0.0733	0.3011
120.75	3.736	0.212	0.0471	0.2	0.0898	0.196	0.0524	0.138	0.0613	0.0151	0.00994	0.1	0.0249	0.0769	0.0754	0.0748	0.073	0.3001
120.833	3.722	0.211	0.0468	0.199	0.0895	0.196	0.0522	0.138	0.061	0.015	0.00993	0.1	0.0249	0.0766	0.0751	0.0746	0.0727	0.299
120.917	3.709	0.21	0.0464	0.198	0.0891	0.195	0.052	0.137	0.0607	0.0149	0.00992	0.1	0.0249	0.0763	0.0748	0.0743	0.0724	0.2978
121	3.695	0.209	0.0461	0.197	0.0888	0.194	0.0518	0.136	0.0605	0.0149	0.00991	0.1	0.0249	0.0761	0.0746	0.074	0.0722	0.2969
121.083	3.682	0.208	0.0457	0.197	0.0884	0.194	0.0516	0.135	0.0601	0.0148	0.00985	0.1	0.0247	0.0758	0.0743	0.0737	0.0719	0.2957
121.167	3.668	0.208	0.0453	0.196	0.088	0.193	0.0514	0.134	0.0598	0.0147	0.00979	0.1	0.0245	0.0755	0.074	0.0734	0.0716	0.2945
121.25	3.655	0.207	0.045	0.195	0.0876	0.192	0.0512	0.133	0.0595	0.0146	0.00973	0.1	0.0242	0.0752	0.0737	0.0732	0.0713	0.2934
121.333	3.641	0.206	0.0445	0.195	0.0872	0.192	0.051	0.132	0.0591	0.0144	0.00955	0.1	0.0236	0.0749	0.0734	0.0728	0.071	0.2921
121.417	3.628	0.205	0.044	0.194	0.0867	0.191	0.0508	0.131	0.0588	0.0142	0.00937	0.1	0.0229	0.0746	0.0731	0.0725	0.0707	0.2909
121.5	3.614	0.204	0.0436	0.193	0.0863	0.19	0.0505	0.13	0.0584	0.014	0.00919	0.1	0.0223	0.0743	0.0728	0.0722	0.0704	0.2897
121.583	3.601	0.203	0.0431	0.192	0.0858	0.189	0.0503	0.128	0.058	0.0138	0.00889	0.1	0.0212	0.0739	0.0724	0.0719	0.07	0.2882
121.667	3.587	0.202	0.0425	0.191	0.0853	0.189	0.05	0.127	0.0576	0.0136	0.00858	0.1	0.0201	0.0736	0.0721	0.0715	0.0697	0.2869
121.75	3.574	0.201	0.042	0.19	0.0848	0.188	0.0498	0.126	0.0572	0.0133	0.00828	0.1	0.0191	0.0732	0.0717	0.0712	0.0693	0.2854
121.833	3.561	0.2	0.0414	0.189	0.0843	0.187	0.0495	0.125	0.0567	0.013	0.0079	0.1	0.018	0.0729	0.0714	0.0708	0.069	0.2841
121.917	3.547	0.199	0.0408	0.188	0.0838	0.186	0.0492	0.124	0.0563	0.0127	0.00751	0.1	0.017	0.0725	0.071	0.0704	0.0686	0.2825
122	3.534	0.197	0.0402	0.188	0.0832	0.186	0.0489	0.123	0.0558	0.0124	0.00713	0.1	0.016	0.0721	0.0706	0.0701	0.0682	0.281
122.083	3.521	0.196	0.0395	0.187	0.0826	0.185	0.0486	0.121	0.0553	0.012	0.0068	0.1	0.0152	0.0717	0.0702	0.0697	0.0678	0.2794
122.167	3.507	0.195	0.0387	0.186	0.0821	0.184	0.0483	0.12	0.0549	0.0116	0.00647	0.1	0.0145	0.0713	0.0698	0.0693	0.0674	0.2778
122.25	3.494	0.194	0.038	0.185	0.0815	0.183	0.048	0.119	0.0544	0.0112	0.00614	0.1	0.0137	0.0709	0.0694	0.0689	0.067	0.2762
122.333	3.481	0.192	0.0372	0.183	0.0808	0.182	0.0477	0.117	0.0539	0.0108	0.00588	0.1	0.0132	0.0705	0.069	0.0685	0.0666	0.2746
122.417	3.467	0.191	0.0364	0.182	0.0802	0.181	0.0474	0.116	0.0534	0.0104	0.00562	0.1	0.0127	0.0701	0.0686	0.068	0.0662	0.2729
122.5	3.454	0.19	0.0356	0.181	0.0796	0.181	0.047	0.115	0.0529	0.0101	0.00536	0.1	0.0121	0.0696	0.0681	0.0676	0.0657	0.271
122.583	3.441	0.188	0.0347	0.18	0.0789	0.18	0.0467	0.113	0.0524	0.00972	0.00517	0.1	0.0117	0.0692	0.0677	0.0671	0.0653	0.2693
122.667	3.428	0.187	0.0338	0.179	0.0783	0.179	0.0463	0.112	0.0519	0.00939	0.00498	0.1	0.0113	0.0687	0.0672	0.0667	0.0648	0.2674
122.75	3.414	0.185	0.0329	0.178	0.0776	0.178	0.046	0.11	0.0514	0.00905	0.0048	0.1	0.011	0.0683	0.0668	0.0662	0.0644	0.2657
122.833	3.401	0.184	0.0319	0.177	0.0769	0.177	0.0456	0.109	0.0508	0.00877	0.00465	0.1	0.0107	0.0678	0.0663	0.0657	0.0639	0.2637
122.917	3.388	0.182	0.0309	0.175	0.0762	0.176	0.0452	0.107	0.0503	0.00849	0.00451	0.1	0.0104	0.0673	0.0658	0.0652	0.0634	0.2617
123	3.375	0.181	0.0299	0.174	0.0756	0.175	0.0448	0.106	0.0498	0.00821	0.00437	0.1	0.0101	0.0668	0.0653	0.0647	0.0629	0.2597
123.083	3.362	0.179	0.0289	0.173	0.0748	0.174	0.0444	0.104	0.0492	0.00797	0.00425	0.1	0.00996	0.0663	0.0648	0.0642	0.0624	0.2577
123.167	3.348	0.178	0.0278	0.171	0.0741	0.173	0.0441	0.103	0.0487	0.00773	0.00413	0.1	0.00979	0.0657	0.0642	0.0637	0.0618	0.2554
123.25	3.335	0.176	0.0268	0.17	0.0734	0.172	0.0437	0.101	0.0481	0.0075	0.00402	0.1	0.00962	0.0652	0.0637	0.0632	0.0613	0.2534
123.333	3.322	0.174	0.0259	0.169	0.0727	0.171	0.0433	0.0995	0.0476	0.00731	0.00394	0.1	0.00957	0.0647	0.0632	0.0626	0.0608	0.2513
123.417	3.309	0.173	0.0249	0.167	0.072	0.17	0.0429	0.0978	0.047	0.00712	0.00386	0.1	0.00952	0.0641	0.0626	0.0621	0.0602	0.249
123.5	3.296	0.171	0.024	0.166	0.0712	0.169	0.0425	0.0961	0.0464	0.00693	0.00378	0.1	0.00947	0.0636	0.0621	0.0615	0.0597	0.2469
123.583	3.283	0.17	0.0231	0.165	0.0705	0.168	0.0421	0.0944	0.0458	0.00677	0.00372	0.1	0.00947	0.0631	0.0616	0.061	0.0591	0.2448
123.667	3.27	0.168	0.0222	0.163	0.0697	0.167	0.0417	0.0926	0.0452	0.00662	0.00367	0.1	0.00947	0.0625	0.061	0.0604	0.0586	0.2425
123.75	3.257	0.166	0.0214	0.162	0.069	0.166	0.0413	0.0909	0.0446	0.00646	0.00362	0.1	0.00947	0.0619	0.0604	0.0599	0.058	0.2402
123.833	3.244	0.165	0.0206	0.16	0.0682	0.165	0.0408	0.0891	0.044	0.00633	0.0036	0.1	0.00947	0.0614	0.0599	0.0593	0.0575	0.2381
123.917	3.23	0.163	0.0198	0.159	0.0674	0.163	0.0404	0.0872	0.0434	0.00619	0.00358	0.1	0.00947	0.0608	0.0593	0.0588	0.0569	0.2358
124	3.217	0.161	0.019	0.158	0.0667	0.162	0.04	0.0854	0.0428	0.00605	0.00356	0.1	0.00947	0.0603	0.0588	0.0582	0.0563	0.2336
124.083	3.204	0.159	0.0183	0.156	0.0659	0.161	0.0396	0.0835	0.0422	0.00594	0.00356	0.1	0.00947	0.0597	0.0582	0.0576	0.0557	0.2312
124.167	3.191	0.158	0.0176	0.155	0.0651	0.16	0.0392	0.0816	0.0416	0.00583	0.00356	0.1	0.00947	0.0591	0.0576	0.057	0.0552	0.2289
124.25	3.178	0.156	0.0169	0.153	0.0643	0.159	0.0388	0.0797	0.0409	0.00573	0.00356	0.1	0.00947	0.0585	0.057	0.0565	0.0546	0.2266
124.333	3.165	0.154	0.0163	0.152	0.0635	0.158	0.0383	0.0778	0.0403	0.00563	0.00356	0.1	0.00947	0.0579	0.0564	0.0559	0.054	0.2242
124.417	3.153	0.152	0.0157	0.15	0.0627	0.156	0.0379	0.076	0.0396	0.00554	0.00356	0.1	0.00947	0.0573	0.0558	0.0553	0.0534	0.2218
124.5	3.14	0.151	0.0151	0.149	0.0618	0.155	0.0375	0.0742	0.039	0.00545	0.00356	0.1	0.00947	0.0568	0.0552	0.0547	0.0528	0.2195
124.583	3.127	0.149	0.0146	0.147	0.061	0.154	0.037	0.0724	0.0383	0.00538	0.00356	0.1	0.00947	0.0562	0.0546	0.0541	0.0522	0.2171
124.667	3.114	0.147	0.014	0.146	0.0602	0.153	0.0366	0.0707	0.0377	0.00531	0.00356	0.1	0.00947	0.0555	0.054	0.0535	0.0516	0.2146
124.75	3.101	0.145	0.0135	0.144	0.0593	0.152	0.0361	0.0689	0.037	0.00524	0.00356	0.1	0.00947	0.0549	0.0534	0.0529	0.051	0.2122
124.833	3.088	0.143	0.013	0.143	0.0585	0.15	0.0357	0.0673	0.0363	0.00519	0.00356	0.1	0.00947	0.0543	0.0528	0.0523	0.0504	0.2098
124.917	3.075	0.141	0.0126	0.141	0.0576	0.149	0.0352	0.0656	0.0356	0.00514	0.00356	0.1	0.00947	0.0537	0.0522	0.0516	0.0498	0.2073
125	3.062	0.14	0.0121	0.14	0.0568	0.148	0.0347	0.064	0.035	0.0051	0.00356	0.1	0.00947	0.0531	0.0516	0.051	0.0491	0.2048
125.083	3.049	0.138	0.0117	0.138	0.0559	0.146	0.0343	0.0624	0.0343	0.00507	0.00356	0.1	0.00947	0.0525	0.051	0.0504	0.0485	0.2024
125.167	3.036	0.136	0.0114	0.136	0.055	0.145	0.0338	0.0608	0.0337	0.00504	0.00356	0.1	0.00947	0.0518	0.0503	0.0498	0.0479	0.1998
125.25	3.024	0.134	0.011	0.135	0.0541	0.144	0.0333	0.0593	0.033	0.00502	0.00356	0.1	0.00947	0.0512	0.0497	0.0491	0.0472	0.1972
125.333	3.011	0.132	0.0106	0.133	0.0532	0.143	0.0329	0.0578	0.0324	0.00501	0.00356	0.1	0.00947	0.0506	0.049	0.0485	0.0466	0.1947
125.417	2.998	0.13	0.0103	0.132	0.0523	0.141	0.0324	0.0563	0.0318	0.005	0.00356	0.1	0.00947	0.0499	0.0484	0.0478	0.046	0.1921
125.5	2.985	0.128	0.00994	0.13	0.0514	0.14	0.0319	0.0548	0.0312	0.00499	0.00356	0.1	0.00947	0.0493	0.0478	0.0472	0.0453	0.1896
125.583	2.972	0.126	0.00963	0.128	0.0506	0.139	0.0314	0.0535	0.0306	0.00499	0.00356	0.1	0.00947	0.0486	0.0471	0.0465	0.0447	0.1869

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
125.667	2.96	0.124	0.00931	0.127	0.0497	0.137	0.0309	0.0521	0.03	0.00499	0.00356	0.1	0.00947	0.048	0.0464	0.0459	0.044	0.1843
125.75	2.947	0.122	0.00899	0.125	0.0489	0.136	0.0305	0.0507	0.0294	0.00499	0.00356	0.1	0.00947	0.0473	0.0458	0.0452	0.0433	0.1816
125.833	2.934	0.12	0.00871	0.123	0.0481	0.135	0.03	0.0494	0.0288	0.00499	0.00356	0.1	0.00947	0.0466	0.0451	0.0446	0.0427	0.179
125.917	2.921	0.118	0.00842	0.122	0.0472	0.133	0.0295	0.0481	0.0283	0.00499	0.00356	0.1	0.00947	0.046	0.0445	0.0439	0.042	0.1764
126	2.909	0.116	0.00813	0.12	0.0464	0.132	0.029	0.0468	0.0277	0.00499	0.00356	0.1	0.00947	0.0453	0.0438	0.0432	0.0413	0.1736
126.083	2.896	0.114	0.00787	0.118	0.0456	0.131	0.0285	0.0456	0.0272	0.00499	0.00356	0.1	0.00947	0.0446	0.0431	0.0425	0.0406	0.1708
126.167	2.883	0.112	0.00761	0.116	0.0448	0.129	0.028	0.0444	0.0267	0.00499	0.00356	0.1	0.00947	0.044	0.0424	0.0419	0.04	0.1683
126.25	2.87	0.111	0.00736	0.115	0.0441	0.128	0.0276	0.0432	0.0261	0.00499	0.00356	0.1	0.00947	0.0433	0.0418	0.0412	0.0393	0.1656
126.333	2.858	0.109	0.00713	0.113	0.0433	0.126	0.0271	0.0421	0.0256	0.00499	0.00356	0.1	0.00947	0.0426	0.0411	0.0405	0.0386	0.1628
126.417	2.845	0.107	0.0069	0.111	0.0426	0.125	0.0267	0.041	0.0251	0.00499	0.00356	0.1	0.00947	0.042	0.0404	0.0399	0.038	0.1603
126.5	2.833	0.105	0.00667	0.11	0.0418	0.124	0.0262	0.0399	0.0246	0.00499	0.00356	0.1	0.00947	0.0413	0.0398	0.0392	0.0373	0.1576
126.583	2.82	0.103	0.00647	0.108	0.0411	0.122	0.0258	0.0388	0.0242	0.00499	0.00356	0.1	0.00947	0.0407	0.0392	0.0386	0.0367	0.1552
126.667	2.807	0.102	0.00626	0.107	0.0404	0.121	0.0254	0.0378	0.0237	0.00499	0.00356	0.1	0.00947	0.0401	0.0385	0.038	0.0361	0.1527
126.75	2.795	0.1	0.00606	0.105	0.0397	0.12	0.0249	0.0368	0.0232	0.00499	0.00356	0.1	0.00947	0.0394	0.0379	0.0373	0.0354	0.15
126.833	2.782	0.0984	0.0059	0.103	0.039	0.118	0.0245	0.0359	0.0227	0.00499	0.00356	0.1	0.00947	0.0388	0.0373	0.0367	0.0348	0.1476
126.917	2.769	0.0968	0.00574	0.102	0.0384	0.117	0.0241	0.0349	0.0223	0.00499	0.00356	0.1	0.00947	0.0382	0.0367	0.0361	0.0342	0.1452
127	2.757	0.0952	0.00557	0.1	0.0377	0.115	0.0237	0.034	0.0218	0.00499	0.00356	0.1	0.00947	0.0376	0.0361	0.0355	0.0336	0.1428
127.083	2.744	0.0936	0.00544	0.0989	0.0371	0.114	0.0233	0.0332	0.0214	0.00499	0.00356	0.1	0.00947	0.037	0.0355	0.0349	0.033	0.1404
127.167	2.732	0.0921	0.00531	0.0974	0.0364	0.113	0.0229	0.0323	0.021	0.00499	0.00356	0.1	0.00947	0.0364	0.0349	0.0343	0.0324	0.138
127.25	2.719	0.0905	0.00517	0.0959	0.0358	0.111	0.0225	0.0315	0.0205	0.00499	0.00356	0.1	0.00947	0.0359	0.0343	0.0338	0.0318	0.1358
127.333	2.707	0.0891	0.00507	0.0945	0.0352	0.11	0.0221	0.0307	0.0201	0.00499	0.00356	0.1	0.00947	0.0353	0.0338	0.0332	0.0313	0.1336
127.417	2.694	0.0876	0.00496	0.0931	0.0346	0.108	0.0218	0.03	0.0197	0.00499	0.00356	0.1	0.00947	0.0347	0.0332	0.0326	0.0307	0.1312
127.5	2.682	0.0861	0.00486	0.0917	0.0339	0.107	0.0214	0.0292	0.0193	0.00499	0.00356	0.1	0.00947	0.0342	0.0326	0.0321	0.0302	0.1291
127.583	2.669	0.0847	0.00478	0.0903	0.0334	0.106	0.021	0.0285	0.0189	0.00499	0.00356	0.1	0.00947	0.0336	0.0321	0.0315	0.0296	0.1268
127.667	2.657	0.0833	0.0047	0.089	0.0328	0.104	0.0207	0.0278	0.0185	0.00499	0.00356	0.1	0.00947	0.0331	0.0316	0.031	0.0291	0.1248
127.75	2.644	0.0819	0.00463	0.0876	0.0322	0.103	0.0203	0.027	0.0181	0.00499	0.00356	0.1	0.00947	0.0326	0.031	0.0305	0.0285	0.1226
127.833	2.632	0.0805	0.00458	0.0863	0.0317	0.101	0.02	0.0264	0.0177	0.00499	0.00356	0.1	0.00947	0.032	0.0305	0.0299	0.028	0.1204
127.917	2.619	0.0792	0.00453	0.085	0.0311	0.0999	0.0196	0.0257	0.0174	0.00499	0.00356	0.1	0.00947	0.0315	0.03	0.0294	0.0275	0.1184
128	2.607	0.0779	0.00448	0.0837	0.0306	0.0985	0.0193	0.025	0.017	0.00499	0.00356	0.1	0.00947	0.031	0.0295	0.0289	0.027	0.1164
128.083	2.594	0.0766	0.00446	0.0825	0.0301	0.0971	0.0189	0.0244	0.0167	0.00499	0.00356	0.1	0.00947	0.0305	0.029	0.0284	0.0265	0.1144
128.167	2.582	0.0753	0.00444	0.0812	0.0295	0.0957	0.0186	0.0238	0.0164	0.00499	0.00356	0.1	0.00947	0.03	0.0285	0.0279	0.026	0.1124
128.25	2.57	0.074	0.00443	0.08	0.029	0.0942	0.0183	0.0232	0.016	0.00499	0.00356	0.1	0.00947	0.0296	0.028	0.0275	0.0255	0.1106
128.333	2.557	0.0728	0.00443	0.0788	0.0285	0.0929	0.018	0.0226	0.0157	0.00499	0.00356	0.1	0.00947	0.0291	0.0276	0.027	0.0251	0.1088
128.417	2.545	0.0716	0.00443	0.0776	0.028	0.0915	0.0177	0.022	0.0154	0.00499	0.00356	0.1	0.00947	0.0286	0.0271	0.0265	0.0246	0.1068
128.5	2.532	0.0704	0.00443	0.0764	0.0275	0.0901	0.0174	0.0215	0.0151	0.00499	0.00356	0.1	0.00947	0.0281	0.0266	0.026	0.0241	0.1048
128.583	2.52	0.0692	0.00443	0.0753	0.0271	0.0888	0.0171	0.0209	0.0148	0.00499	0.00356	0.1	0.00947	0.0277	0.0262	0.0256	0.0237	0.1032
128.667	2.508	0.0681	0.00443	0.0741	0.0266	0.0875	0.0168	0.0204	0.0145	0.00499	0.00356	0.1	0.00947	0.0273	0.0257	0.0252	0.0232	0.1014
128.75	2.495	0.0669	0.00443	0.073	0.0261	0.0862	0.0165	0.0199	0.0142	0.00499	0.00356	0.1	0.00947	0.0268	0.0253	0.0247	0.0228	0.0996
128.833	2.483	0.0658	0.00443	0.0719	0.0257	0.0849	0.0162	0.0194	0.0139	0.00499	0.00356	0.1	0.00947	0.0264	0.0248	0.0243	0.0223	0.0978
128.917	2.471	0.0647	0.00443	0.0708	0.0253	0.0836	0.0159	0.019	0.0137	0.00499	0.00356	0.1	0.00947	0.026	0.0244	0.0238	0.0219	0.0961
129	2.458	0.0636	0.00443	0.0697	0.0248	0.0823	0.0157	0.0185	0.0134	0.00499	0.00356	0.1	0.00947	0.0255	0.024	0.0234	0.0215	0.0944
129.083	2.446	0.0626	0.00443	0.0687	0.0244	0.0811	0.0154	0.0181	0.0132	0.00499	0.00356	0.1	0.00947	0.0251	0.0236	0.023	0.0211	0.0928
129.167	2.434	0.0615	0.00443	0.0676	0.024	0.0799	0.0151	0.0176	0.0129	0.00499	0.00356	0.1	0.00947	0.0247	0.0232	0.0226	0.0207	0.0912
129.25	2.422	0.0605	0.00443	0.0666	0.0236	0.0786	0.0149	0.0172	0.0127	0.00499	0.00356	0.1	0.00947	0.0243	0.0228	0.0222	0.0203	0.0896
129.333	2.409	0.0595	0.00443	0.0656	0.0232	0.0775	0.0146	0.0168	0.0124	0.00499	0.00356	0.1	0.00947	0.0239	0.0224	0.0218	0.0202	0.0883
129.417	2.397	0.0585	0.00443	0.0646	0.0228	0.0763	0.0144	0.0165	0.0122	0.00499	0.00356	0.1	0.00947	0.0235	0.022	0.0214	0.0201	0.087
129.5	2.385	0.0576	0.00443	0.0636	0.0224	0.0751	0.0141	0.0161	0.0119	0.00499	0.00356	0.1	0.00947	0.0231	0.0216	0.021	0.02	0.0857
129.583	2.373	0.0566	0.00443	0.0627	0.022	0.074	0.0139	0.0157	0.0117	0.00499	0.00356	0.1	0.00947	0.0228	0.0212	0.0207	0.02	0.0847
129.667	2.36	0.0557	0.00443	0.0617	0.0217	0.0728	0.0136	0.0154	0.0115	0.00499	0.00356	0.1	0.00947	0.0224	0.0209	0.0203	0.02	0.0836
129.75	2.348	0.0548	0.00443	0.0608	0.0213	0.0717	0.0134	0.015	0.0113	0.00499	0.00356	0.1	0.00947	0.022	0.0205	0.0199	0.02	0.0824
129.833	2.336	0.0539	0.00443	0.0599	0.021	0.0706	0.0132	0.0147	0.011	0.00499	0.00356	0.1	0.00947	0.0217	0.0201	0.0196	0.02	0.0814
129.917	2.324	0.053	0.00443	0.059	0.0206	0.0695	0.013	0.0144	0.0108	0.00499	0.00356	0.1	0.00947	0.0213	0.0198	0.0192	0.02	0.0803
130	2.312	0.0521	0.00443	0.0581	0.0203	0.0684	0.0127	0.0141	0.0106	0.00499	0.00356	0.1	0.00947	0.021	0.0194	0.0189	0.02	0.0793
130.083	2.299	0.0513	0.00443	0.0573	0.02	0.0673	0.0125	0.0138	0.0104	0.00499	0.00356	0.1	0.00947	0.0207	0.0191	0.0185	0.02	0.0783
130.167	2.287	0.0505	0.00443	0.0564	0.0196	0.0663	0.0123	0.0135	0.0102	0.00499	0.00356	0.1	0.00947	0.0203	0.0188	0.0182	0.02	0.0773
130.25	2.275	0.0497	0.00443	0.0556	0.0193	0.0652	0.0121	0.0132	0.01	0.00499	0.00356	0.1	0.00947	0.02	0.0184	0.0179	0.02	0.0763
130.333	2.263	0.0489	0.00443	0.0548	0.019	0.0642	0.0119	0.013	0.00981	0.00499	0.00356	0.1	0.00947	0.0197	0.0181	0.0176	0.02	0.0754
130.417	2.251	0.0482	0.00443	0.054	0.0187	0.0631	0.0117	0.0127	0.00962	0.00499	0.00356	0.1	0.00947	0.0194	0.0178	0.0172	0.02	0.0744
130.5	2.239	0.0474	0.00443	0.0532	0.0184	0.0621	0.0115	0.0125	0.00942	0.00499	0.00356	0.1	0.00947	0.019	0.0175	0.0169	0.02	0.0734
130.583	2.227	0.0467	0.00443	0.0524	0.0181	0.0611	0.0113	0.0123	0.00925	0.00499	0.00356	0.1	0.00947	0.0187	0.0172	0.0166	0.02	0.0725
130.667	2.215	0.046	0.00443	0.0517	0.0178	0.0601	0.0111	0.012	0.00907	0.00499	0.00356	0.1	0.00947	0.0184	0.0169	0.0163	0.02	0.0716
130.75	2.202	0.0452	0.00443	0.0509	0.0175	0.0591	0.011	0.0118	0.00889	0.00499	0.00356	0.1	0.00947	0.0181	0.0166	0.016	0.02	0.0707
130.833	2.19	0.0445	0.00443	0.0502	0.0172	0.0582	0.0108	0.0116	0.00872	0.00499	0.00356	0.1	0.00947	0.0179	0.0163	0.0158	0.02	0.07

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
130.917	2.178	0.0438	0.00443	0.0495	0.0169	0.0572	0.0106	0.0115	0.00856	0.00499	0.00356	0.1	0.00947	0.0176	0.016	0.0155	0.02	0.0691
131	2.166	0.0431	0.00443	0.0488	0.0166	0.0562	0.0104	0.0113	0.00839	0.00499	0.00356	0.1	0.00947	0.0173	0.0158	0.0152	0.02	0.0683
131.083	2.154	0.0424	0.00443	0.0481	0.0163	0.0553	0.0102	0.0111	0.00824	0.00499	0.00356	0.1	0.00947	0.017	0.0155	0.0149	0.02	0.0674
131.167	2.142	0.0417	0.00443	0.0475	0.0161	0.0544	0.0101	0.011	0.00809	0.00499	0.00356	0.1	0.00947	0.0168	0.0152	0.0147	0.02	0.0667
131.25	2.13	0.0411	0.00443	0.0468	0.0158	0.0535	0.00989	0.0108	0.00794	0.00499	0.00356	0.1	0.00947	0.0165	0.015	0.0144	0.02	0.0659
131.333	2.118	0.0404	0.00443	0.0462	0.0156	0.0526	0.00972	0.0107	0.0078	0.00499	0.00356	0.1	0.00947	0.0163	0.0147	0.0141	0.02	0.0651
131.417	2.106	0.0398	0.00443	0.0455	0.0153	0.0517	0.00955	0.0106	0.00766	0.00499	0.00356	0.1	0.00947	0.016	0.0145	0.0139	0.02	0.0644
131.5	2.094	0.0391	0.00443	0.0449	0.0151	0.0508	0.00938	0.0105	0.00752	0.00499	0.00356	0.1	0.00947	0.0157	0.0142	0.0136	0.02	0.0635
131.583	2.082	0.0385	0.00443	0.0443	0.0148	0.0499	0.00922	0.0104	0.0074	0.00499	0.00356	0.1	0.00947	0.0155	0.014	0.0134	0.02	0.0629
131.667	2.07	0.0379	0.00443	0.0437	0.0146	0.0491	0.00907	0.0103	0.00727	0.00499	0.00356	0.1	0.00947	0.0153	0.0137	0.0131	0.02	0.0621
131.75	2.058	0.0373	0.00443	0.043	0.0144	0.0482	0.00891	0.0102	0.00715	0.00499	0.00356	0.1	0.00947	0.015	0.0135	0.0129	0.02	0.0614
131.833	2.046	0.0367	0.00443	0.0424	0.0141	0.0474	0.00875	0.0102	0.00704	0.00499	0.00356	0.1	0.00947	0.0148	0.0132	0.0127	0.02	0.0607
131.917	2.034	0.0361	0.00443	0.0418	0.0139	0.0466	0.0086	0.0101	0.00693	0.00499	0.00356	0.1	0.00947	0.0146	0.013	0.0124	0.02	0.06
132	2.022	0.0355	0.00443	0.0413	0.0137	0.0458	0.00844	0.0101	0.00682	0.00499	0.00356	0.1	0.00947	0.0143	0.0128	0.0122	0.02	0.0593
132.083	2.011	0.0349	0.00443	0.0407	0.0135	0.045	0.0083	0.01	0.00672	0.00499	0.00356	0.1	0.00947	0.0141	0.0126	0.012	0.02	0.0587
132.167	1.999	0.0344	0.00443	0.0401	0.0133	0.0442	0.00816	0.01	0.00662	0.00499	0.00356	0.1	0.00947	0.0139	0.0123	0.0118	0.02	0.058
132.25	1.987	0.0338	0.00443	0.0395	0.0131	0.0434	0.00801	0.01	0.00651	0.00499	0.00356	0.1	0.00947	0.0136	0.0121	0.0115	0.02	0.0572
132.333	1.975	0.0333	0.00443	0.039	0.0129	0.0427	0.00787	0.01	0.00642	0.00499	0.00356	0.1	0.00947	0.0134	0.0119	0.0113	0.02	0.0566
132.417	1.963	0.0328	0.00443	0.0384	0.0127	0.0419	0.00773	0.01	0.00633	0.00499	0.00356	0.1	0.00947	0.0132	0.0117	0.0111	0.02	0.056
132.5	1.951	0.0322	0.00443	0.0379	0.0125	0.0412	0.00759	0.01	0.00624	0.00499	0.00356	0.1	0.00947	0.013	0.0115	0.0109	0.02	0.0554
132.583	1.939	0.0317	0.00443	0.0374	0.0123	0.0404	0.00746	0.01	0.00615	0.00499	0.00356	0.1	0.00947	0.0128	0.0113	0.0107	0.02	0.0548
132.667	1.927	0.0312	0.00443	0.0368	0.0121	0.0397	0.00733	0.01	0.00607	0.00499	0.00356	0.1	0.00947	0.0126	0.011	0.0105	0.02	0.0541
132.75	1.915	0.0307	0.00443	0.0363	0.012	0.039	0.0072	0.01	0.00599	0.00499	0.00356	0.1	0.00947	0.0124	0.0108	0.0103	0.02	0.0535
132.833	1.904	0.0303	0.00443	0.0358	0.0118	0.0383	0.00708	0.01	0.00592	0.00499	0.00356	0.1	0.00947	0.0122	0.0106	0.0101	0.02	0.0529
132.917	1.892	0.0298	0.00443	0.0353	0.0116	0.0376	0.00695	0.01	0.00584	0.00499	0.00356	0.1	0.00947	0.012	0.0104	0.00985	0.02	0.05225
133	1.88	0.0293	0.00443	0.0348	0.0115	0.037	0.00682	0.01	0.00577	0.00499	0.00356	0.1	0.00947	0.0118	0.0102	0.00966	0.02	0.05166
133.083	1.868	0.0289	0.00443	0.0343	0.0113	0.0363	0.00671	0.01	0.0057	0.00499	0.00356	0.1	0.00947	0.0116	0.01	0.00947	0.02	0.05107
133.167	1.856	0.0284	0.00443	0.0338	0.0112	0.0357	0.00659	0.01	0.00564	0.00499	0.00356	0.1	0.00947	0.0114	0.00986	0.00928	0.02	0.05054
133.25	1.845	0.028	0.00443	0.0333	0.011	0.035	0.00648	0.01	0.00557	0.00499	0.00356	0.1	0.00947	0.0112	0.00967	0.0091	0.02	0.04997
133.333	1.833	0.0276	0.00443	0.0329	0.0109	0.0344	0.00637	0.01	0.00552	0.00499	0.00356	0.1	0.00947	0.011	0.00949	0.00891	0.02	0.0494
133.417	1.821	0.0272	0.00443	0.0324	0.0108	0.0338	0.00625	0.01	0.00546	0.00499	0.00356	0.1	0.00947	0.0109	0.00931	0.00873	0.02	0.04894
133.5	1.809	0.0268	0.00443	0.032	0.0106	0.0332	0.00614	0.01	0.00541	0.00499	0.00356	0.1	0.00947	0.0107	0.00912	0.00854	0.02	0.04836
133.583	1.797	0.0264	0.00443	0.0316	0.0105	0.0326	0.00604	0.01	0.00536	0.00499	0.00356	0.1	0.00947	0.0105	0.00895	0.00837	0.02	0.04782
133.667	1.786	0.0261	0.00443	0.0311	0.0104	0.032	0.00594	0.01	0.00532	0.00499	0.00356	0.1	0.00947	0.0103	0.00878	0.0082	0.02	0.04728
133.75	1.774	0.0257	0.00443	0.0307	0.0103	0.0314	0.00584	0.01	0.00527	0.00499	0.00356	0.1	0.00947	0.0102	0.00861	0.00803	0.02	0.04684
133.833	1.762	0.0254	0.00443	0.0303	0.0102	0.0309	0.00575	0.01	0.00523	0.00499	0.00356	0.1	0.00947	0.01	0.00845	0.00787	0.02	0.04632
133.917	1.751	0.025	0.00443	0.0299	0.01	0.0304	0.00565	0.01	0.0052	0.00499	0.00356	0.1	0.00947	0.00984	0.00829	0.00772	0.02	0.04585
134	1.739	0.0247	0.00443	0.0295	0.00994	0.0298	0.00556	0.01	0.00516	0.00499	0.00356	0.1	0.00947	0.00968	0.00813	0.00756	0.02	0.04537
134.083	1.727	0.0244	0.00443	0.0291	0.00984	0.0293	0.00547	0.01	0.00513	0.00499	0.00356	0.1	0.00947	0.00953	0.00798	0.0074	0.02	0.04491
134.167	1.715	0.024	0.00443	0.0287	0.00973	0.0288	0.00539	0.01	0.0051	0.00499	0.00356	0.1	0.00947	0.00937	0.00782	0.00724	0.02	0.04443
134.25	1.704	0.0237	0.00443	0.0283	0.00963	0.0283	0.0053	0.01	0.00508	0.00499	0.00356	0.1	0.00947	0.00921	0.00766	0.00709	0.02	0.04396
134.333	1.692	0.0234	0.00443	0.0279	0.00954	0.0278	0.00522	0.01	0.00506	0.00499	0.00356	0.1	0.00947	0.00907	0.00752	0.00694	0.02	0.04353
134.417	1.68	0.0232	0.00443	0.0276	0.00944	0.0273	0.00514	0.01	0.00504	0.00499	0.00356	0.1	0.00947	0.00893	0.00738	0.0068	0.02	0.04311
134.5	1.669	0.0229	0.00443	0.0272	0.00935	0.0269	0.00506	0.01	0.00502	0.00499	0.00356	0.1	0.00947	0.00878	0.00723	0.00666	0.02	0.04267
134.583	1.657	0.0226	0.00443	0.0269	0.00927	0.0264	0.00499	0.01	0.00501	0.00499	0.00356	0.1	0.00947	0.00865	0.0071	0.00653	0.02	0.04228
134.667	1.645	0.0224	0.00443	0.0265	0.00918	0.026	0.00492	0.01	0.005	0.00499	0.00356	0.1	0.00947	0.00852	0.00697	0.0064	0.02	0.04189
134.75	1.634	0.0221	0.00443	0.0262	0.0091	0.0255	0.00485	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00839	0.00685	0.00627	0.02	0.04151
134.833	1.622	0.0219	0.00443	0.0259	0.00903	0.0251	0.00478	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00827	0.00672	0.00614	0.02	0.04113
134.917	1.611	0.0216	0.00443	0.0255	0.00895	0.0247	0.00471	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00814	0.00659	0.00601	0.02	0.04074
135	1.599	0.0214	0.00443	0.0252	0.00888	0.0243	0.00465	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00801	0.00646	0.00588	0.02	0.04035
135.083	1.587	0.0212	0.00443	0.0249	0.00882	0.024	0.00459	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00789	0.00634	0.00577	0.02	0.04
135.167	1.576	0.021	0.00443	0.0246	0.00876	0.0236	0.00453	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00778	0.00623	0.00565	0.02	0.03966
135.25	1.564	0.0208	0.00443	0.0243	0.00871	0.0232	0.00448	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00766	0.00611	0.00553	0.02	0.0393
135.333	1.553	0.0206	0.00443	0.0241	0.00866	0.0229	0.00442	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00756	0.00601	0.00543	0.02	0.039
135.417	1.541	0.0204	0.00443	0.0238	0.00862	0.0226	0.00436	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00746	0.00591	0.00533	0.02	0.0387
135.5	1.529	0.0202	0.00443	0.0235	0.00857	0.0222	0.00431	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00736	0.00581	0.00523	0.02	0.0384
135.583	1.518	0.02	0.00443	0.0233	0.00853	0.0219	0.00426	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00725	0.0057	0.00513	0.02	0.03808
135.667	1.506	0.0198	0.00443	0.023	0.00849	0.0216	0.00421	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00715	0.0056	0.00503	0.02	0.03778
135.75	1.495	0.0197	0.00443	0.0228	0.00846	0.0213	0.00416	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00705	0.0055	0.00492	0.02	0.03747
135.833	1.483	0.0195	0.00443	0.0225	0.00843	0.021	0.00412	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00696	0.00541	0.00484	0.02	0.03721
135.917	1.472	0.0194	0.00443	0.0223	0.0084	0.0208	0.00407	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00688	0.00533	0.00475	0.02	0.03696
136	1.46	0.0192	0.00443	0.0221	0.00837	0.0205	0.00402	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00679	0.00524	0.00466	0.02	0.03669
136.083	1.449	0.0191	0.00443	0.0219	0.00835	0.0202	0.00398	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00672	0.00516	0.00459	0.02	0.03647

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
136.167	1.437	0.0189	0.00443	0.0217	0.00834	0.02	0.00395	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00664	0.00509	0.00451	0.02	0.03624
136.25	1.426	0.0188	0.00443	0.0215	0.00832	0.0198	0.00391	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00657	0.00502	0.00444	0.02	0.03603
136.333	1.414	0.0187	0.00443	0.0213	0.00831	0.0195	0.00387	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00649	0.00494	0.00437	0.02	0.0358
136.417	1.403	0.0186	0.00443	0.0211	0.0083	0.0193	0.00383	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00642	0.00487	0.00429	0.02	0.03558
136.5	1.391	0.0185	0.00443	0.0209	0.00829	0.0191	0.00379	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00635	0.00479	0.00422	0.02	0.03536
136.583	1.38	0.0184	0.00443	0.0208	0.00829	0.0189	0.00377	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00628	0.00473	0.00415	0.02	0.03516
136.667	1.369	0.0183	0.00443	0.0206	0.00829	0.0187	0.00374	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00622	0.00466	0.00409	0.02	0.03497
136.75	1.357	0.0182	0.00443	0.0204	0.00829	0.0185	0.00371	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00615	0.0046	0.00402	0.02	0.03477
136.833	1.346	0.0181	0.00443	0.0203	0.00829	0.0183	0.00369	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0061	0.00454	0.00397	0.02	0.03461
136.917	1.334	0.0181	0.00443	0.0201	0.00829	0.0181	0.00367	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00604	0.00449	0.00391	0.02	0.03444
137	1.323	0.018	0.00443	0.02	0.00829	0.0179	0.00365	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00598	0.00443	0.00386	0.02	0.03427
137.083	1.312	0.018	0.00443	0.0198	0.00829	0.0178	0.00363	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00593	0.00438	0.0038	0.02	0.03411
137.167	1.3	0.0179	0.00443	0.0197	0.00829	0.0176	0.00361	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00587	0.00432	0.00374	0.02	0.03393
137.25	1.289	0.0179	0.00443	0.0196	0.00829	0.0175	0.00359	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00582	0.00427	0.00369	0.02	0.03378
137.333	1.277	0.0178	0.00443	0.0194	0.00829	0.0173	0.00359	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00577	0.00422	0.00364	0.02	0.03363
137.417	1.266	0.0178	0.00443	0.0193	0.00829	0.0172	0.00358	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00573	0.00417	0.0036	0.02	0.0335
137.5	1.255	0.0178	0.00443	0.0192	0.00829	0.0171	0.00357	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00568	0.00413	0.00355	0.02	0.03336
137.583	1.243	0.0178	0.00443	0.0191	0.00829	0.017	0.00356	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00564	0.00409	0.00351	0.02	0.03324
137.667	1.232	0.0178	0.00443	0.019	0.00829	0.0169	0.00355	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0056	0.00405	0.00348	0.02	0.03313
137.75	1.221	0.0178	0.00443	0.0189	0.00829	0.0167	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00557	0.00402	0.00344	0.02	0.03303
137.833	1.209	0.0178	0.00443	0.0188	0.00829	0.0167	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00553	0.00398	0.0034	0.02	0.03291
137.917	1.198	0.0178	0.00443	0.0187	0.00829	0.0166	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00549	0.00394	0.00336	0.02	0.03279
138	1.187	0.0178	0.00443	0.0186	0.00829	0.0165	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00546	0.0039	0.00333	0.02	0.03269
138.083	1.175	0.0178	0.00443	0.0185	0.00829	0.0164	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00543	0.00388	0.0033	0.02	0.03261
138.167	1.164	0.0178	0.00443	0.0185	0.00829	0.0164	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0054	0.00385	0.00327	0.02	0.03252
138.25	1.153	0.0178	0.00443	0.0184	0.00829	0.0163	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00537	0.00382	0.00324	0.02	0.03243
138.333	1.141	0.0178	0.00443	0.0183	0.00829	0.0163	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00535	0.0038	0.00323	0.02	0.03238
138.417	1.13	0.0178	0.00443	0.0183	0.00829	0.0162	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00534	0.00378	0.00321	0.02	0.03233
138.5	1.119	0.0178	0.00443	0.0182	0.00829	0.0162	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00532	0.00377	0.00319	0.02	0.03228
138.583	1.108	0.0178	0.00443	0.0182	0.00829	0.0162	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0053	0.00375	0.00317	0.02	0.03222
138.667	1.096	0.0178	0.00443	0.0181	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00528	0.00373	0.00315	0.02	0.03216
138.75	1.085	0.0178	0.00443	0.0181	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00526	0.00371	0.00313	0.02	0.0321
138.833	1.074	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00525	0.0037	0.00312	0.02	0.03207
138.917	1.063	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00524	0.00369	0.00311	0.02	0.03204
139	1.051	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.083	1.04	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.167	1.03	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.25	1.019	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.333	1.008	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.417	0.997	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.5	0.987	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.583	0.977	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.667	0.966	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.75	0.956	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.833	0.946	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.917	0.936	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140	0.926	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.083	0.916	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.167	0.907	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.25	0.897	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.333	0.888	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.417	0.878	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.5	0.869	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.583	0.86	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.667	0.851	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.75	0.842	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.833	0.833	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.917	0.824	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141	0.816	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.083	0.81	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.167	0.805	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
141.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
146.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
151.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
157.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
162.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
167.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
172.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
178.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
183.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
188.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
193.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
199.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
204.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
209.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
214.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
220.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
225.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
230.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
235.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
241.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
246.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
251.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
256.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
262.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
267.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
272.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
277.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
283.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
288.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
293.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
298.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
300	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Output data from file C:\USERS\304490\BOX\PB6582 EDF SZC NNB\EDF SZC NNB TEAM\TECH DATA\E01 CALCULATIONS\EXAMINATION HYDROLOGY\HYDROLOGY CALCS MAY 2021\MDS EA ACTIONS MAY 2021\DESIGN FLOWS\SIZE_T100_121SD_PR75PC.ZZN
Selected output data from time (hr): 0
to time (hr): 300

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
0	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
0.083	0.8	0.0178	0.00451	0.018	0.00832	0.0162	0.00355	0.0101	0.00502	0.00506	0.00366	0.1	0.0098	0.00525	0.0037	0.00312	0.02	0.03207
0.167	0.8	0.0179	0.0046	0.018	0.00835	0.0162	0.00357	0.0102	0.00505	0.00513	0.00375	0.1	0.0101	0.00526	0.00371	0.00313	0.02	0.0321
0.25	0.8	0.0179	0.00468	0.0181	0.00837	0.0163	0.00358	0.0103	0.00508	0.00519	0.00384	0.1	0.0104	0.00528	0.00372	0.00315	0.02	0.03215
0.333	0.8	0.0181	0.00494	0.0182	0.00846	0.0164	0.00362	0.0106	0.00516	0.00539	0.00411	0.1	0.0114	0.00533	0.00378	0.0032	0.02	0.03231
0.417	0.8	0.0183	0.0052	0.0183	0.00854	0.0165	0.00367	0.0109	0.00524	0.00558	0.00438	0.1	0.0124	0.00539	0.00384	0.00326	0.02	0.03249
0.5	0.8	0.0184	0.00546	0.0185	0.00862	0.0166	0.00371	0.0112	0.00533	0.00577	0.00465	0.1	0.0134	0.00544	0.00389	0.00331	0.02	0.03264
0.583	0.8	0.0187	0.00589	0.0187	0.00876	0.0168	0.00378	0.0116	0.00545	0.00608	0.0051	0.1	0.015	0.00553	0.00397	0.0034	0.02	0.0329
0.667	0.8	0.019	0.00632	0.0189	0.0089	0.0169	0.00385	0.0121	0.00557	0.00639	0.00556	0.1	0.0166	0.00561	0.00406	0.00348	0.02	0.03315
0.75	0.8	0.0193	0.00675	0.0191	0.00904	0.0171	0.00392	0.0126	0.0057	0.00671	0.00601	0.1	0.0182	0.00569	0.00414	0.00356	0.02	0.03339
0.833	0.8	0.0197	0.00736	0.0194	0.00924	0.0173	0.00402	0.0133	0.00588	0.00714	0.00659	0.1	0.0197	0.00582	0.00427	0.00369	0.02	0.03378
0.917	0.8	0.0201	0.00796	0.0198	0.00943	0.0175	0.00412	0.0139	0.00606	0.00758	0.00717	0.1	0.0213	0.00594	0.00439	0.00381	0.02	0.03414
1	0.8	0.0205	0.00856	0.0201	0.00963	0.0177	0.00422	0.0146	0.00624	0.00802	0.00774	0.1	0.0228	0.00607	0.00452	0.00394	0.02	0.03453
1.083	0.8	0.0211	0.00934	0.0205	0.00988	0.018	0.00435	0.0154	0.00647	0.00857	0.00824	0.1	0.024	0.00622	0.00467	0.00409	0.02	0.03498
1.167	0.8	0.0216	0.0101	0.0209	0.0101	0.0182	0.00448	0.0163	0.00671	0.00913	0.00873	0.1	0.0251	0.00637	0.00482	0.00424	0.02	0.03543
1.25	0.8	0.0221	0.0109	0.0213	0.0104	0.0185	0.00461	0.0172	0.00694	0.00969	0.00923	0.1	0.0262	0.00653	0.00497	0.0044	0.02	0.0359
1.333	0.8	0.0227	0.0118	0.0217	0.0107	0.0188	0.00476	0.0182	0.00722	0.0103	0.00962	0.1	0.027	0.00672	0.00517	0.00459	0.02	0.03648
1.417	0.8	0.0234	0.0128	0.0222	0.011	0.0191	0.00492	0.0192	0.0075	0.0108	0.01	0.1	0.0278	0.00691	0.00536	0.00479	0.02	0.03706
1.5	0.8	0.024	0.0137	0.0227	0.0113	0.0194	0.00508	0.0203	0.00777	0.0114	0.0104	0.1	0.0286	0.00711	0.00556	0.00498	0.02	0.03765
1.583	0.8	0.0248	0.0149	0.0233	0.0117	0.0198	0.00526	0.0215	0.0081	0.0119	0.0107	0.1	0.0292	0.00733	0.00578	0.0052	0.02	0.03831
1.667	0.8	0.0255	0.016	0.0239	0.012	0.0202	0.00545	0.0227	0.00844	0.0124	0.011	0.1	0.0298	0.00755	0.006	0.00543	0.02	0.03898
1.75	0.8	0.0263	0.0171	0.0245	0.0124	0.0206	0.00563	0.024	0.00877	0.0129	0.0112	0.1	0.0304	0.00778	0.00623	0.00565	0.02	0.03966
1.833	0.8	0.0272	0.0184	0.0251	0.0128	0.021	0.00584	0.0254	0.00915	0.0133	0.0115	0.1	0.0308	0.00804	0.00649	0.00591	0.02	0.04044
1.917	0.8	0.028	0.0197	0.0258	0.0133	0.0214	0.00606	0.0268	0.00954	0.0138	0.0117	0.1	0.0312	0.0083	0.00675	0.00618	0.02	0.04123
2	0.8	0.0289	0.021	0.0264	0.0137	0.0218	0.00627	0.0282	0.00993	0.0142	0.0119	0.1	0.0316	0.00857	0.00702	0.00644	0.02	0.04203
2.083	0.8	0.0299	0.0224	0.0272	0.0142	0.0223	0.00651	0.0299	0.0104	0.0145	0.0121	0.1	0.0319	0.00887	0.00732	0.00675	0.02	0.04294
2.167	0.8	0.0309	0.0237	0.0279	0.0147	0.0228	0.00676	0.0315	0.0108	0.0149	0.0122	0.1	0.0321	0.00918	0.00763	0.00705	0.02	0.04386
2.25	0.8	0.0319	0.0251	0.0287	0.0152	0.0232	0.007	0.0331	0.0112	0.0153	0.0124	0.1	0.0324	0.00948	0.00793	0.00736	0.02	0.04477
2.333	0.8	0.033	0.0263	0.0295	0.0157	0.0238	0.00727	0.0349	0.0117	0.0155	0.0125	0.1	0.0325	0.00982	0.00827	0.00769	0.02	0.04578
2.417	0.8	0.0341	0.0276	0.0304	0.0163	0.0243	0.00754	0.0367	0.0122	0.0158	0.0126	0.1	0.0325	0.0102	0.0086	0.00803	0.02	0.04683
2.5	0.8	0.0352	0.0288	0.0312	0.0168	0.0248	0.00781	0.0385	0.0127	0.0161	0.0128	0.1	0.0326	0.0105	0.00894	0.00836	0.02	0.0478
2.583	0.8	0.0364	0.03	0.0322	0.0174	0.0254	0.00811	0.0405	0.0132	0.0163	0.0128	0.1	0.0326	0.0109	0.00931	0.00874	0.02	0.04895
2.667	0.8	0.0376	0.0311	0.0331	0.018	0.026	0.00841	0.0425	0.0137	0.0166	0.0129	0.1	0.0326	0.0112	0.00969	0.00911	0.02	0.05
2.75	0.8	0.0388	0.0323	0.034	0.0186	0.0266	0.00871	0.0445	0.0143	0.0168	0.013	0.1	0.0326	0.0116	0.0101	0.00949	0.02	0.05119
2.833	0.8	0.0402	0.0333	0.035	0.0193	0.0272	0.00902	0.0467	0.0149	0.017	0.013	0.1	0.0326	0.012	0.0105	0.00989	0.02	0.05239
2.917	0.8	0.0415	0.0344	0.036	0.0199	0.0278	0.00933	0.0489	0.0154	0.0172	0.0131	0.1	0.0326	0.0124	0.0109	0.0103	0.02	0.0536
3	0.8	0.0428	0.0354	0.0371	0.0206	0.0285	0.00964	0.051	0.016	0.0174	0.0131	0.1	0.0326	0.0128	0.0113	0.0107	0.02	0.0548
3.083	0.8	0.0443	0.0364	0.0382	0.0213	0.0292	0.00999	0.0534	0.0167	0.0176	0.0131	0.1	0.0328	0.0133	0.0117	0.0111	0.02	0.0561
3.167	0.8	0.0458	0.0374	0.0393	0.022	0.0299	0.0103	0.0558	0.0173	0.0178	0.0132	0.1	0.0329	0.0137	0.0122	0.0116	0.02	0.0575
3.25	0.8	0.0473	0.0384	0.0404	0.0227	0.0306	0.0107	0.0582	0.018	0.018	0.0132	0.1	0.033	0.0142	0.0126	0.012	0.02	0.0588
3.333	0.8	0.0489	0.0393	0.0417	0.0236	0.0314	0.0111	0.0606	0.0187	0.0182	0.0133	0.1	0.0335	0.0147	0.0131	0.0125	0.02	0.0603
3.417	0.8	0.0506	0.0403	0.0429	0.0244	0.0322	0.0115	0.063	0.0194	0.0185	0.0135	0.1	0.034	0.0152	0.0136	0.013	0.02	0.0618
3.5	0.8	0.0522	0.0413	0.0442	0.0252	0.0329	0.0119	0.0654	0.0202	0.0187	0.0136	0.1	0.0344	0.0157	0.0141	0.0135	0.02	0.0633
3.583	0.8	0.054	0.0422	0.0456	0.0261	0.0338	0.0123	0.0678	0.021	0.0189	0.0138	0.1	0.0352	0.0162	0.0147	0.0141	0.02	0.065
3.667	0.8	0.0558	0.0432	0.047	0.0269	0.0347	0.0127	0.0702	0.0217	0.0192	0.014	0.1	0.036	0.0168	0.0152	0.0147	0.02	0.0667
3.75	0.8	0.0577	0.0441	0.0483	0.0278	0.0355	0.0132	0.0726	0.0225	0.0195	0.0142	0.1	0.0367	0.0173	0.0158	0.0152	0.02	0.0683
3.833	0.8	0.0597	0.0451	0.0499	0.0288	0.0365	0.0136	0.075	0.0234	0.0197	0.0145	0.1	0.0375	0.0179	0.0164	0.0158	0.02	0.0701
3.917	0.8	0.0617	0.046	0.0514	0.0298	0.0374	0.0141	0.0773	0.0243	0.02	0.0148	0.1	0.0383	0.0185	0.017	0.0164	0.02	0.0719
4	0.8	0.0637	0.047	0.0529	0.0308	0.0384	0.0146	0.0797	0.0251	0.0203	0.0151	0.1	0.039	0.0191	0.0176	0.017	0.02	0.0737
4.083	0.8	0.0658	0.0479	0.0545	0.0318	0.0394	0.0151	0.0821	0.026	0.0206	0.0153	0.1	0.0396	0.0198	0.0182	0.0177	0.02	0.0757
4.167	0.8	0.068	0.0488	0.0562	0.0329	0.0404	0.0156	0.0844	0.0269	0.0209	0.0156	0.1	0.0402	0.0204	0.0189	0.0183	0.02	0.0776
4.25	0.8	0.0702	0.0498	0.0579	0.0339	0.0414	0.0161	0.0868	0.0277	0.0212	0.0158	0.1	0.0408	0.0211	0.0196	0.019	0.02	0.0797
4.333	0.8	0.0725	0.0508	0.0597	0.0351	0.0425	0.0167	0.0891	0.0286	0.0215	0.016	0.1	0.0412	0.0218	0.0203	0.0197	0.02	0.0818
4.417	0.8	0.0749	0.0517	0.0614	0.0362	0.0437	0.0173	0.0915	0.0295	0.0218	0.0162	0.1	0.0416	0.0225	0.021	0.0204	0.02	0.0839
4.5	0.8	0.0772	0.0527	0.0632	0.0373	0.0448	0.0178	0.0938	0.0304	0.0221	0.0164	0.1	0.0421	0.0232	0.0217	0.0211	0.02	0.086
4.583	0.8	0.0797	0.0537	0.0652	0.0385	0.0459	0.0184	0.0961	0.0312	0.0224	0.0166	0.1	0.0424	0.024	0.0224	0.0219	0.0205	0.0888
4.667	0.8	0.0822	0.0548	0.0671	0.0396	0.0471	0.019	0.0985	0.0321	0.0227	0.0167	0.1	0.0427	0.0247	0.0232	0.0226	0.021	0.0915
4.75	0.8	0.0847	0.0558	0.069	0.0407	0.0483	0.0196	0.101	0.033	0.0229	0.0169	0.1	0.043	0.0255	0.024	0.0234	0.0215	0.0944
4.833	0.8	0.0873	0.0569	0.071	0.0419	0.0496	0.0203	0.103	0.0338	0.0231	0.017	0.1	0.0432	0.0263	0.0248	0.0242	0.0223	0.0976

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
4.917	0.8	0.0898	0.058	0.0731	0.043	0.0508	0.0209	0.105	0.0347	0.0233	0.0171	0.1	0.0434	0.0271	0.0256	0.025	0.0231	0.1008
5	0.8	0.0923	0.059	0.0751	0.0441	0.0521	0.0215	0.108	0.0356	0.0236	0.0172	0.1	0.0436	0.0279	0.0264	0.0258	0.0239	0.104
5.083	0.8	0.0948	0.0601	0.0773	0.0453	0.0534	0.0222	0.11	0.0364	0.0237	0.0173	0.1	0.0438	0.0288	0.0273	0.0267	0.0248	0.1076
5.167	0.8	0.0974	0.0611	0.0794	0.0464	0.0548	0.0228	0.112	0.0373	0.0239	0.0174	0.1	0.0439	0.0297	0.0281	0.0276	0.0256	0.111
5.25	0.8	0.0999	0.0622	0.0816	0.0475	0.0561	0.0234	0.115	0.0381	0.0241	0.0175	0.1	0.044	0.0305	0.029	0.0284	0.0265	0.1144
5.333	0.8	0.102	0.0632	0.0838	0.0487	0.0575	0.024	0.117	0.039	0.0242	0.0175	0.1	0.0441	0.0314	0.0298	0.0293	0.0274	0.1179
5.417	0.8	0.105	0.0642	0.0859	0.0498	0.0589	0.0247	0.119	0.0398	0.0244	0.0176	0.1	0.0441	0.0322	0.0307	0.0301	0.0282	0.1212
5.5	0.8	0.107	0.0651	0.0881	0.0509	0.0604	0.0253	0.121	0.0406	0.0245	0.0177	0.1	0.0442	0.0331	0.0316	0.031	0.0291	0.1248
5.583	0.8	0.11	0.066	0.0902	0.052	0.0619	0.0259	0.124	0.0415	0.0247	0.0177	0.1	0.0442	0.0339	0.0324	0.0319	0.0299	0.1281
5.667	0.8	0.112	0.0669	0.0924	0.0531	0.0634	0.0265	0.126	0.0423	0.0248	0.0178	0.1	0.0442	0.0348	0.0333	0.0327	0.0308	0.1316
5.75	0.8	0.115	0.0678	0.0945	0.0543	0.0649	0.0271	0.128	0.0432	0.0249	0.0178	0.1	0.0442	0.0357	0.0341	0.0336	0.0316	0.135
5.833	0.8	0.117	0.0686	0.0967	0.0554	0.0664	0.0277	0.13	0.044	0.025	0.0178	0.1	0.0442	0.0365	0.035	0.0344	0.0325	0.1384
5.917	0.8	0.12	0.0693	0.0988	0.0565	0.068	0.0284	0.133	0.0449	0.0251	0.0178	0.1	0.0442	0.0374	0.0358	0.0353	0.0334	0.1419
6	0.8	0.122	0.0701	0.101	0.0576	0.0696	0.029	0.135	0.0457	0.0252	0.0178	0.1	0.0442	0.0382	0.0367	0.0361	0.0342	0.1452
6.083	0.8	0.125	0.0708	0.103	0.0587	0.0712	0.0296	0.137	0.0466	0.0253	0.0178	0.1	0.0442	0.0391	0.0375	0.037	0.0351	0.1487
6.167	0.8	0.127	0.0715	0.105	0.0598	0.0729	0.0302	0.139	0.0474	0.0254	0.0179	0.1	0.0442	0.0399	0.0384	0.0378	0.0359	0.152
6.25	0.8	0.13	0.0721	0.107	0.0609	0.0746	0.0308	0.142	0.0482	0.0255	0.0179	0.1	0.0442	0.0407	0.0392	0.0387	0.0368	0.1554
6.333	0.8	0.132	0.0727	0.11	0.062	0.0763	0.0314	0.144	0.0491	0.0255	0.0179	0.1	0.0442	0.0416	0.0401	0.0395	0.0376	0.1588
6.417	0.8	0.135	0.0733	0.112	0.0631	0.078	0.032	0.146	0.0499	0.0256	0.0179	0.1	0.0442	0.0424	0.0409	0.0403	0.0384	0.162
6.5	0.8	0.137	0.0739	0.114	0.0642	0.0798	0.0326	0.148	0.0508	0.0257	0.0179	0.1	0.0442	0.0433	0.0418	0.0412	0.0393	0.1656
6.583	0.8	0.14	0.0744	0.116	0.0653	0.0816	0.0332	0.15	0.0516	0.0257	0.0179	0.1	0.0442	0.0441	0.0426	0.042	0.0401	0.1688
6.667	0.8	0.142	0.0749	0.118	0.0664	0.0834	0.0339	0.152	0.0524	0.0258	0.0179	0.1	0.0442	0.045	0.0434	0.0429	0.041	0.1723
6.75	0.8	0.145	0.0754	0.12	0.0675	0.0852	0.0345	0.154	0.0533	0.0258	0.0179	0.1	0.0442	0.0458	0.0443	0.0437	0.0418	0.1756
6.833	0.8	0.147	0.0758	0.122	0.0686	0.0871	0.0351	0.156	0.0541	0.0259	0.0179	0.1	0.0442	0.0466	0.0451	0.0446	0.0427	0.179
6.917	0.8	0.15	0.0762	0.124	0.0697	0.089	0.0357	0.158	0.0549	0.0259	0.0179	0.1	0.0442	0.0475	0.046	0.0454	0.0435	0.1824
7	0.8	0.152	0.0766	0.127	0.0708	0.0909	0.0363	0.16	0.0557	0.0259	0.0179	0.1	0.0442	0.0483	0.0468	0.0462	0.0443	0.1856
7.083	0.8	0.154	0.0769	0.129	0.0719	0.0928	0.0369	0.161	0.0565	0.026	0.0179	0.1	0.0442	0.0491	0.0476	0.0471	0.0452	0.189
7.167	0.8	0.157	0.0772	0.131	0.073	0.0947	0.0375	0.163	0.0573	0.026	0.0179	0.1	0.0442	0.05	0.0485	0.0479	0.046	0.1924
7.25	0.8	0.159	0.0775	0.133	0.074	0.0967	0.0381	0.165	0.058	0.026	0.0179	0.1	0.0442	0.0508	0.0493	0.0487	0.0468	0.1956
7.333	0.8	0.162	0.0778	0.135	0.0751	0.0986	0.0387	0.167	0.0588	0.026	0.0179	0.1	0.0442	0.0516	0.0501	0.0496	0.0477	0.199
7.417	0.8	0.164	0.078	0.137	0.0762	0.1	0.0393	0.168	0.0595	0.026	0.0179	0.1	0.0442	0.0525	0.051	0.0504	0.0485	0.2024
7.5	0.8	0.167	0.0783	0.139	0.0773	0.102	0.0399	0.17	0.0603	0.026	0.0179	0.1	0.0442	0.0533	0.0518	0.0512	0.0493	0.2056
7.583	0.8	0.169	0.0785	0.141	0.0783	0.104	0.0405	0.172	0.061	0.026	0.0179	0.1	0.0442	0.0541	0.0526	0.0521	0.0502	0.209
7.667	0.8	0.171	0.0788	0.143	0.0793	0.106	0.0411	0.173	0.0617	0.026	0.0179	0.1	0.0442	0.0549	0.0534	0.0529	0.051	0.2122
7.75	0.8	0.174	0.079	0.145	0.0804	0.108	0.0417	0.175	0.0624	0.026	0.0179	0.1	0.0442	0.0558	0.0543	0.0537	0.0518	0.2156
7.833	0.8	0.176	0.0792	0.148	0.0813	0.11	0.0423	0.176	0.063	0.026	0.0179	0.1	0.0442	0.0566	0.0551	0.0545	0.0527	0.2189
7.917	0.8	0.179	0.0795	0.15	0.0823	0.112	0.0428	0.178	0.0637	0.026	0.0179	0.1	0.0442	0.0574	0.0559	0.0554	0.0535	0.2222
8	0.8	0.181	0.0797	0.152	0.0833	0.114	0.0434	0.179	0.0643	0.026	0.0179	0.1	0.0442	0.0582	0.0567	0.0562	0.0543	0.2254
8.083	0.8	0.183	0.0799	0.154	0.0842	0.116	0.044	0.181	0.065	0.026	0.0179	0.1	0.0442	0.0591	0.0575	0.057	0.0551	0.2287
8.167	0.8	0.185	0.0801	0.156	0.0852	0.118	0.0446	0.182	0.0656	0.026	0.0179	0.1	0.0442	0.0599	0.0584	0.0578	0.0559	0.232
8.25	0.8	0.188	0.0803	0.158	0.0861	0.12	0.0451	0.183	0.0662	0.026	0.0179	0.1	0.0442	0.0607	0.0592	0.0586	0.0567	0.2352
8.333	0.8	0.19	0.0804	0.16	0.087	0.121	0.0457	0.185	0.0668	0.026	0.0179	0.1	0.0442	0.0615	0.06	0.0594	0.0575	0.2384
8.417	0.8	0.192	0.0806	0.162	0.0879	0.123	0.0462	0.186	0.0674	0.026	0.0179	0.1	0.0442	0.0623	0.0608	0.0602	0.0583	0.2416
8.5	0.8	0.194	0.0808	0.164	0.0888	0.125	0.0468	0.187	0.068	0.026	0.0179	0.1	0.0442	0.0631	0.0616	0.061	0.0591	0.2448
8.583	0.8	0.196	0.0809	0.166	0.0896	0.127	0.0473	0.188	0.0686	0.026	0.0179	0.1	0.0442	0.0638	0.0623	0.0617	0.0599	0.2477
8.667	0.8	0.198	0.0811	0.168	0.0904	0.129	0.0478	0.19	0.0691	0.026	0.0179	0.1	0.0442	0.0646	0.0631	0.0625	0.0606	0.2508
8.75	0.8	0.2	0.0812	0.17	0.0913	0.131	0.0483	0.191	0.0697	0.026	0.0179	0.1	0.0442	0.0653	0.0638	0.0633	0.0614	0.2538
8.833	0.8	0.202	0.0814	0.172	0.0921	0.133	0.0488	0.192	0.0702	0.026	0.0179	0.1	0.0442	0.066	0.0645	0.064	0.0621	0.2566
8.917	0.8	0.204	0.0815	0.173	0.0929	0.135	0.0493	0.193	0.0708	0.026	0.0179	0.1	0.0442	0.0668	0.0653	0.0647	0.0629	0.2597
9	0.8	0.206	0.0816	0.175	0.0937	0.136	0.0497	0.194	0.0713	0.026	0.0179	0.1	0.0442	0.0675	0.066	0.0654	0.0636	0.2625
9.083	0.8	0.208	0.0817	0.177	0.0945	0.138	0.0502	0.195	0.0719	0.0261	0.0179	0.1	0.0443	0.0682	0.0667	0.0662	0.0643	0.2654
9.167	0.8	0.21	0.0819	0.179	0.0952	0.14	0.0507	0.196	0.0724	0.0261	0.0179	0.1	0.0444	0.0689	0.0674	0.0669	0.065	0.2682
9.25	0.8	0.211	0.082	0.181	0.096	0.142	0.0511	0.197	0.0729	0.0261	0.0179	0.1	0.0445	0.0696	0.0681	0.0676	0.0657	0.271
9.333	0.8	0.213	0.0822	0.182	0.0968	0.144	0.0516	0.198	0.0735	0.0262	0.0181	0.1	0.0449	0.0703	0.0688	0.0683	0.0664	0.2738
9.417	0.8	0.215	0.0824	0.184	0.0976	0.146	0.0521	0.199	0.074	0.0263	0.0182	0.1	0.0453	0.071	0.0695	0.0689	0.0671	0.2765
9.5	0.8	0.217	0.0826	0.186	0.0983	0.148	0.0525	0.2	0.0745	0.0263	0.0183	0.1	0.0457	0.0717	0.0702	0.0696	0.0678	0.2793
9.583	0.8	0.219	0.0828	0.188	0.0991	0.15	0.053	0.201	0.0751	0.0265	0.0185	0.1	0.0464	0.0724	0.0709	0.0703	0.0685	0.2821
9.667	0.8	0.22	0.0831	0.189	0.0999	0.152	0.0534	0.202	0.0756	0.0266	0.0187	0.1	0.0471	0.073	0.0715	0.071	0.0691	0.2846
9.75	0.8	0.222	0.0833	0.191	0.101	0.153	0.0539	0.203	0.0761	0.0267	0.0189	0.1	0.0478	0.0737	0.0722	0.0717	0.0698	0.2874
9.833	0.8	0.224	0.0836	0.193	0.101	0.155	0.0543	0.204	0.0766	0.0269	0.0191	0.1	0.0486	0.0744	0.0729	0.0723	0.0705	0.2901
9.917	0.8	0.226	0.0839	0.194	0.102	0.157	0.0548	0.205	0.0772	0.0271	0.0194	0.1	0.0494	0.075	0.0735	0.073	0.0712	0.2927
10	0.8	0.228	0.0843	0.196	0.103	0.159	0.0553	0.206	0.0777	0.0273	0.0197	0.1	0.0502	0.0757	0.0742	0.0737	0.0718	0.2954
10.083	0.8	0.229	0.0846	0.198	0.104	0.161	0.0557	0.207	0.0782	0.0276	0.0199	0.1	0.0508	0.0764	0.0749	0.0743	0.0725	0.2981

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
10.167	0.8	0.231	0.085	0.199	0.104	0.163	0.0561	0.208	0.0787	0.0279	0.0202	0.1	0.0514	0.077	0.0755	0.075	0.0731	0.3006
10.25	0.8	0.233	0.0854	0.201	0.105	0.165	0.0566	0.209	0.0792	0.0281	0.0205	0.1	0.052	0.0777	0.0762	0.0756	0.0738	0.3033
10.333	0.8	0.235	0.0858	0.203	0.106	0.167	0.057	0.21	0.0797	0.0284	0.0207	0.1	0.0525	0.0783	0.0768	0.0763	0.0744	0.3058
10.417	0.8	0.237	0.0863	0.204	0.107	0.169	0.0575	0.211	0.0803	0.0287	0.0209	0.1	0.0529	0.0789	0.0775	0.0769	0.0751	0.3084
10.5	0.8	0.238	0.0867	0.206	0.107	0.171	0.058	0.212	0.0808	0.029	0.0211	0.1	0.0534	0.0796	0.0781	0.0776	0.0757	0.311
10.583	0.8	0.24	0.0873	0.207	0.108	0.173	0.0584	0.213	0.0813	0.0292	0.0212	0.1	0.0537	0.0802	0.0787	0.0782	0.0764	0.3135
10.667	0.8	0.242	0.0878	0.209	0.109	0.174	0.0588	0.214	0.0818	0.0295	0.0214	0.1	0.054	0.0809	0.0794	0.0788	0.077	0.3161
10.75	0.8	0.244	0.0883	0.211	0.11	0.176	0.0593	0.215	0.0823	0.0298	0.0216	0.1	0.0544	0.0815	0.08	0.0795	0.0776	0.3186
10.833	0.805	0.245	0.089	0.212	0.11	0.178	0.0597	0.216	0.0828	0.03	0.0217	0.1	0.0546	0.0821	0.0806	0.0801	0.0783	0.3211
10.917	0.811	0.247	0.0896	0.214	0.111	0.18	0.0602	0.218	0.0833	0.0302	0.0218	0.1	0.0548	0.0828	0.0813	0.0807	0.0789	0.3237
11	0.816	0.249	0.0902	0.216	0.112	0.182	0.0606	0.219	0.0838	0.0304	0.0219	0.1	0.0551	0.0834	0.0819	0.0814	0.0795	0.3262
11.083	0.826	0.251	0.0909	0.217	0.113	0.184	0.0611	0.22	0.0844	0.0306	0.022	0.1	0.0552	0.084	0.0826	0.082	0.0802	0.3288
11.167	0.836	0.253	0.0916	0.219	0.113	0.186	0.0615	0.221	0.0849	0.0308	0.0221	0.1	0.0554	0.0847	0.0832	0.0826	0.0808	0.3313
11.25	0.846	0.254	0.0922	0.22	0.114	0.187	0.062	0.222	0.0854	0.031	0.0222	0.1	0.0555	0.0853	0.0838	0.0833	0.0815	0.3339
11.333	0.856	0.256	0.0929	0.222	0.115	0.189	0.0624	0.223	0.0859	0.0312	0.0223	0.1	0.0556	0.086	0.0845	0.0839	0.0821	0.3365
11.417	0.866	0.258	0.0935	0.224	0.116	0.191	0.0629	0.224	0.0864	0.0313	0.0223	0.1	0.0556	0.0866	0.0851	0.0846	0.0827	0.339
11.5	0.876	0.26	0.0941	0.225	0.116	0.193	0.0633	0.225	0.0869	0.0315	0.0224	0.1	0.0557	0.0872	0.0857	0.0852	0.0834	0.3415
11.583	0.886	0.261	0.0947	0.227	0.117	0.195	0.0638	0.227	0.0875	0.0316	0.0224	0.1	0.0557	0.0879	0.0864	0.0858	0.084	0.3441
11.667	0.897	0.263	0.0953	0.228	0.118	0.196	0.0642	0.228	0.088	0.0317	0.0225	0.1	0.0557	0.0885	0.087	0.0865	0.0847	0.3467
11.75	0.907	0.265	0.0959	0.23	0.119	0.198	0.0646	0.229	0.0885	0.0318	0.0225	0.1	0.0557	0.0892	0.0877	0.0871	0.0853	0.3493
11.833	0.918	0.267	0.0965	0.232	0.119	0.2	0.0651	0.23	0.089	0.0319	0.0226	0.1	0.0557	0.0898	0.0883	0.0878	0.0859	0.3518
11.917	0.928	0.268	0.097	0.233	0.12	0.202	0.0655	0.232	0.0896	0.032	0.0226	0.1	0.0557	0.0904	0.0889	0.0884	0.0866	0.3543
12	0.939	0.27	0.0975	0.235	0.121	0.203	0.066	0.233	0.0901	0.0322	0.0226	0.1	0.0557	0.0911	0.0896	0.089	0.0872	0.3569
12.083	0.95	0.272	0.098	0.237	0.122	0.205	0.0664	0.234	0.0906	0.0322	0.0226	0.1	0.0557	0.0917	0.0902	0.0897	0.0879	0.3595
12.167	0.961	0.274	0.0985	0.238	0.122	0.207	0.0668	0.236	0.0912	0.0323	0.0226	0.1	0.0557	0.0923	0.0908	0.0903	0.0885	0.3619
12.25	0.972	0.275	0.099	0.24	0.123	0.209	0.0673	0.237	0.0917	0.0324	0.0226	0.1	0.0557	0.093	0.0915	0.0909	0.0891	0.3645
12.333	0.983	0.277	0.0994	0.241	0.124	0.21	0.0677	0.238	0.0922	0.0325	0.0226	0.1	0.0557	0.0936	0.0921	0.0916	0.0898	0.3671
12.417	0.994	0.279	0.0999	0.243	0.125	0.212	0.0681	0.24	0.0928	0.0326	0.0226	0.1	0.0557	0.0942	0.0928	0.0922	0.0904	0.3696
12.5	1.006	0.281	0.1	0.244	0.125	0.214	0.0686	0.241	0.0933	0.0326	0.0226	0.1	0.0557	0.0949	0.0934	0.0928	0.091	0.3721
12.583	1.017	0.282	0.101	0.246	0.126	0.215	0.069	0.242	0.0939	0.0327	0.0226	0.1	0.0557	0.0955	0.094	0.0935	0.0917	0.3747
12.667	1.029	0.284	0.101	0.248	0.127	0.217	0.0694	0.244	0.0944	0.0328	0.0226	0.1	0.0557	0.0961	0.0947	0.0941	0.0923	0.3772
12.75	1.04	0.286	0.101	0.249	0.128	0.219	0.0699	0.245	0.095	0.0328	0.0226	0.1	0.0557	0.0968	0.0953	0.0947	0.0929	0.3797
12.833	1.052	0.288	0.102	0.251	0.128	0.22	0.0703	0.246	0.0955	0.0329	0.0226	0.1	0.0557	0.0974	0.0959	0.0954	0.0936	0.3823
12.917	1.064	0.289	0.102	0.252	0.129	0.222	0.0708	0.247	0.0961	0.0329	0.0226	0.1	0.0557	0.098	0.0965	0.096	0.0942	0.3847
13	1.076	0.291	0.103	0.254	0.13	0.224	0.0712	0.249	0.0966	0.0329	0.0226	0.1	0.0557	0.0986	0.0972	0.0966	0.0948	0.3872
13.083	1.088	0.293	0.103	0.256	0.131	0.225	0.0716	0.25	0.0971	0.033	0.0226	0.1	0.0557	0.0993	0.0978	0.0972	0.0955	0.3898
13.167	1.1	0.295	0.103	0.257	0.132	0.227	0.0721	0.251	0.0977	0.033	0.0226	0.1	0.0557	0.0999	0.0984	0.0979	0.0961	0.3923
13.25	1.112	0.296	0.103	0.259	0.132	0.228	0.0725	0.252	0.0982	0.033	0.0226	0.1	0.0557	0.101	0.0991	0.0985	0.0967	0.3953
13.333	1.125	0.298	0.104	0.26	0.133	0.23	0.073	0.253	0.0987	0.033	0.0226	0.1	0.0557	0.101	0.0997	0.0991	0.0974	0.3972
13.417	1.137	0.3	0.104	0.262	0.134	0.232	0.0734	0.254	0.0992	0.033	0.0226	0.1	0.0557	0.102	0.1	0.0998	0.098	0.3998
13.5	1.15	0.302	0.104	0.263	0.135	0.233	0.0739	0.255	0.0997	0.033	0.0226	0.1	0.0557	0.102	0.101	0.1	0.0986	0.4016
13.583	1.163	0.304	0.104	0.265	0.135	0.235	0.0743	0.256	0.1	0.033	0.0226	0.1	0.0557	0.103	0.102	0.101	0.0992	0.4052
13.667	1.175	0.305	0.105	0.267	0.136	0.236	0.0748	0.257	0.101	0.033	0.0226	0.1	0.0557	0.104	0.102	0.102	0.0999	0.4079
13.75	1.188	0.307	0.105	0.268	0.137	0.238	0.0752	0.258	0.101	0.033	0.0226	0.1	0.0557	0.104	0.103	0.102	0.1	0.409
13.833	1.201	0.309	0.105	0.27	0.138	0.24	0.0757	0.259	0.101	0.033	0.0226	0.1	0.0557	0.105	0.103	0.103	0.101	0.412
13.917	1.214	0.311	0.105	0.271	0.138	0.241	0.0761	0.259	0.102	0.033	0.0226	0.1	0.0557	0.106	0.104	0.104	0.102	0.416
14	1.228	0.313	0.106	0.273	0.139	0.243	0.0766	0.26	0.102	0.033	0.0226	0.1	0.0557	0.106	0.105	0.104	0.102	0.417
14.083	1.241	0.314	0.106	0.275	0.14	0.244	0.077	0.261	0.103	0.033	0.0226	0.1	0.0557	0.107	0.105	0.105	0.103	0.42
14.167	1.254	0.316	0.106	0.276	0.14	0.246	0.0774	0.262	0.103	0.033	0.0226	0.1	0.0557	0.107	0.106	0.105	0.104	0.422
14.25	1.268	0.318	0.106	0.278	0.141	0.247	0.0778	0.263	0.104	0.033	0.0226	0.1	0.0557	0.108	0.107	0.106	0.104	0.425
14.333	1.282	0.319	0.106	0.279	0.142	0.249	0.0783	0.263	0.104	0.033	0.0226	0.1	0.0557	0.109	0.107	0.107	0.105	0.428
14.417	1.295	0.321	0.107	0.281	0.142	0.25	0.0787	0.264	0.104	0.033	0.0226	0.1	0.0557	0.109	0.108	0.107	0.106	0.43
14.5	1.309	0.322	0.107	0.283	0.143	0.252	0.0791	0.265	0.105	0.033	0.0226	0.1	0.0557	0.11	0.108	0.108	0.106	0.432
14.583	1.323	0.324	0.107	0.284	0.144	0.253	0.0795	0.265	0.105	0.033	0.0226	0.1	0.0557	0.111	0.109	0.109	0.107	0.436
14.667	1.337	0.325	0.107	0.286	0.144	0.255	0.0799	0.266	0.105	0.033	0.0226	0.1	0.0557	0.111	0.11	0.109	0.107	0.437
14.75	1.351	0.327	0.107	0.287	0.145	0.256	0.0803	0.267	0.106	0.033	0.0226	0.1	0.0557	0.112	0.11	0.11	0.108	0.44
14.833	1.366	0.328	0.107	0.289	0.145	0.258	0.0806	0.267	0.106	0.033	0.0226	0.1	0.0557	0.112	0.111	0.11	0.109	0.442
14.917	1.38	0.33	0.107	0.29	0.146	0.259	0.081	0.268	0.106	0.033	0.0226	0.1	0.0557	0.113	0.111	0.111	0.109	0.444
15	1.395	0.331	0.108	0.291	0.146	0.26	0.0814	0.269	0.107	0.033	0.0226	0.1	0.0557	0.113	0.112	0.111	0.11	0.446
15.083	1.409	0.333	0.108	0.293	0.147	0.262	0.0818	0.269	0.107	0.033	0.0226	0.1	0.0557	0.114	0.113	0.112	0.11	0.449
15.167	1.424	0.334	0.108	0.294	0.147	0.263	0.0821	0.27	0.107	0.033	0.0226	0.1	0.0557	0.115	0.113	0.113	0.111	0.452
15.25	1.439	0.335	0.108	0.296	0.148	0.265	0.0825	0.27	0.108	0.033	0.0226	0.1	0.0557	0.115	0.114	0.113	0.111	0.453
15.333	1.454	0.337	0.108	0.297	0.148	0.266	0.0828	0.271	0.108	0.033	0.0226	0.1	0.0557	0.116	0.114	0.114	0.112	0.456

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
15.417	1.469	0.338	0.108	0.298	0.149	0.267	0.0831	0.271	0.108	0.033	0.0226	0.1	0.0557	0.116	0.115	0.114	0.112	0.457
15.5	1.484	0.339	0.108	0.3	0.149	0.269	0.0835	0.272	0.109	0.033	0.0226	0.1	0.0557	0.117	0.115	0.115	0.113	0.46
15.583	1.5	0.341	0.108	0.301	0.15	0.27	0.0838	0.272	0.109	0.033	0.0226	0.1	0.0557	0.117	0.116	0.115	0.113	0.461
15.667	1.515	0.342	0.108	0.302	0.15	0.272	0.0841	0.273	0.109	0.033	0.0226	0.1	0.0557	0.118	0.116	0.116	0.114	0.464
15.75	1.531	0.343	0.108	0.303	0.151	0.273	0.0844	0.273	0.109	0.033	0.0226	0.1	0.0557	0.118	0.117	0.116	0.114	0.465
15.833	1.546	0.344	0.108	0.305	0.151	0.274	0.0847	0.273	0.11	0.033	0.0226	0.1	0.0557	0.119	0.117	0.117	0.115	0.468
15.917	1.562	0.345	0.108	0.306	0.151	0.276	0.085	0.274	0.11	0.033	0.0226	0.1	0.0557	0.119	0.118	0.117	0.115	0.469
16	1.578	0.346	0.108	0.307	0.152	0.277	0.0853	0.274	0.11	0.033	0.0226	0.1	0.0557	0.12	0.118	0.118	0.116	0.472
16.083	1.594	0.347	0.108	0.308	0.152	0.278	0.0856	0.275	0.11	0.033	0.0226	0.1	0.0557	0.12	0.119	0.118	0.116	0.473
16.167	1.61	0.348	0.109	0.309	0.153	0.28	0.0859	0.275	0.111	0.033	0.0226	0.1	0.0557	0.12	0.119	0.118	0.117	0.474
16.25	1.626	0.349	0.109	0.31	0.153	0.281	0.0861	0.276	0.111	0.033	0.0226	0.1	0.0557	0.121	0.119	0.119	0.117	0.476
16.333	1.643	0.35	0.109	0.312	0.153	0.282	0.0864	0.276	0.111	0.033	0.0226	0.1	0.0557	0.121	0.12	0.119	0.118	0.478
16.417	1.659	0.351	0.109	0.313	0.154	0.283	0.0866	0.276	0.111	0.033	0.0226	0.1	0.0557	0.122	0.12	0.12	0.118	0.48
16.5	1.676	0.352	0.109	0.314	0.154	0.285	0.0869	0.277	0.111	0.033	0.0226	0.1	0.0557	0.122	0.121	0.12	0.118	0.481
16.583	1.693	0.353	0.109	0.315	0.155	0.286	0.0871	0.277	0.112	0.033	0.0226	0.1	0.0557	0.123	0.121	0.121	0.119	0.484
16.667	1.71	0.354	0.109	0.316	0.155	0.287	0.0874	0.278	0.112	0.033	0.0226	0.1	0.0557	0.123	0.122	0.121	0.119	0.485
16.75	1.726	0.355	0.109	0.317	0.155	0.288	0.0876	0.278	0.112	0.033	0.0226	0.1	0.0557	0.123	0.122	0.121	0.12	0.486
16.833	1.744	0.356	0.109	0.318	0.156	0.289	0.0878	0.278	0.112	0.033	0.0226	0.1	0.0557	0.124	0.122	0.122	0.12	0.488
16.917	1.761	0.357	0.109	0.319	0.156	0.29	0.088	0.279	0.112	0.033	0.0226	0.1	0.0557	0.124	0.123	0.122	0.12	0.489
17	1.778	0.358	0.109	0.32	0.156	0.291	0.0883	0.279	0.113	0.033	0.0226	0.1	0.0557	0.125	0.123	0.123	0.121	0.492
17.083	1.796	0.358	0.109	0.321	0.156	0.292	0.0885	0.279	0.113	0.033	0.0226	0.1	0.0557	0.125	0.123	0.123	0.121	0.492
17.167	1.813	0.359	0.109	0.322	0.157	0.293	0.0887	0.28	0.113	0.033	0.0226	0.1	0.0557	0.125	0.124	0.123	0.122	0.494
17.25	1.831	0.36	0.109	0.322	0.157	0.294	0.0889	0.28	0.113	0.033	0.0226	0.1	0.0557	0.126	0.124	0.124	0.122	0.496
17.333	1.849	0.361	0.109	0.323	0.157	0.295	0.0891	0.28	0.113	0.033	0.0226	0.1	0.0557	0.126	0.124	0.124	0.122	0.496
17.417	1.867	0.361	0.109	0.324	0.158	0.296	0.0892	0.28	0.113	0.033	0.0226	0.1	0.0557	0.126	0.125	0.124	0.123	0.498
17.5	1.885	0.362	0.109	0.325	0.158	0.297	0.0894	0.281	0.113	0.033	0.0226	0.1	0.0557	0.127	0.125	0.125	0.123	0.5
17.583	1.903	0.363	0.109	0.326	0.158	0.298	0.0896	0.281	0.114	0.033	0.0226	0.1	0.0557	0.127	0.125	0.125	0.123	0.5
17.667	1.922	0.363	0.109	0.327	0.158	0.299	0.0898	0.281	0.114	0.033	0.0226	0.1	0.0557	0.127	0.126	0.125	0.123	0.501
17.75	1.94	0.364	0.109	0.327	0.159	0.3	0.09	0.282	0.114	0.033	0.0226	0.1	0.0557	0.127	0.126	0.126	0.124	0.503
17.833	1.959	0.365	0.109	0.328	0.159	0.301	0.0901	0.282	0.114	0.033	0.0226	0.1	0.0557	0.128	0.126	0.126	0.124	0.504
17.917	1.977	0.365	0.109	0.329	0.159	0.302	0.0903	0.282	0.114	0.033	0.0226	0.1	0.0557	0.128	0.127	0.126	0.124	0.505
18	1.996	0.366	0.109	0.329	0.159	0.302	0.0905	0.282	0.114	0.033	0.0226	0.1	0.0557	0.128	0.127	0.126	0.125	0.506
18.083	2.015	0.367	0.109	0.33	0.16	0.303	0.0906	0.283	0.114	0.0331	0.0226	0.1	0.0558	0.129	0.127	0.127	0.125	0.508
18.167	2.033	0.367	0.109	0.331	0.16	0.304	0.0908	0.283	0.115	0.0331	0.0227	0.1	0.0559	0.129	0.127	0.127	0.125	0.508
18.25	2.052	0.368	0.109	0.331	0.16	0.305	0.0909	0.283	0.115	0.0331	0.0227	0.1	0.0559	0.129	0.128	0.127	0.125	0.509
18.333	2.071	0.368	0.109	0.332	0.16	0.306	0.0911	0.283	0.115	0.0331	0.0228	0.1	0.0562	0.129	0.128	0.127	0.126	0.51
18.417	2.089	0.369	0.109	0.333	0.16	0.306	0.0912	0.284	0.115	0.0332	0.0228	0.1	0.0565	0.13	0.128	0.128	0.126	0.512
18.5	2.108	0.37	0.109	0.333	0.161	0.307	0.0914	0.284	0.115	0.0333	0.0229	0.1	0.0568	0.13	0.128	0.128	0.126	0.512
18.583	2.126	0.37	0.109	0.334	0.161	0.308	0.0916	0.284	0.115	0.0334	0.0231	0.1	0.0574	0.13	0.129	0.128	0.126	0.513
18.667	2.145	0.371	0.109	0.335	0.161	0.309	0.0917	0.285	0.115	0.0335	0.0233	0.1	0.0581	0.13	0.129	0.128	0.127	0.514
18.75	2.163	0.371	0.109	0.335	0.161	0.31	0.0919	0.285	0.116	0.0336	0.0234	0.1	0.0587	0.131	0.129	0.129	0.127	0.516
18.833	2.182	0.372	0.11	0.336	0.162	0.31	0.092	0.285	0.116	0.0338	0.0237	0.1	0.0595	0.131	0.129	0.129	0.127	0.516
18.917	2.2	0.373	0.11	0.337	0.162	0.311	0.0922	0.286	0.116	0.034	0.0239	0.1	0.0602	0.131	0.13	0.129	0.127	0.517
19	2.219	0.373	0.11	0.337	0.162	0.312	0.0924	0.286	0.116	0.0342	0.0242	0.1	0.061	0.131	0.13	0.129	0.128	0.518
19.083	2.237	0.374	0.11	0.338	0.162	0.313	0.0925	0.287	0.116	0.0344	0.0245	0.1	0.0617	0.132	0.13	0.13	0.128	0.52
19.167	2.255	0.375	0.111	0.339	0.163	0.314	0.0927	0.287	0.117	0.0346	0.0247	0.1	0.0624	0.132	0.13	0.13	0.128	0.52
19.25	2.274	0.375	0.111	0.339	0.163	0.314	0.0929	0.288	0.117	0.0349	0.025	0.1	0.0631	0.132	0.131	0.13	0.128	0.521
19.333	2.292	0.376	0.112	0.34	0.163	0.315	0.0931	0.288	0.117	0.0352	0.0252	0.1	0.0636	0.132	0.131	0.131	0.129	0.523
19.417	2.31	0.377	0.112	0.341	0.163	0.316	0.0932	0.289	0.117	0.0355	0.0255	0.1	0.0641	0.133	0.131	0.131	0.129	0.524
19.5	2.329	0.377	0.112	0.341	0.164	0.317	0.0934	0.289	0.117	0.0357	0.0257	0.1	0.0646	0.133	0.132	0.131	0.129	0.525
19.583	2.347	0.378	0.113	0.342	0.164	0.317	0.0936	0.29	0.118	0.036	0.0259	0.1	0.065	0.133	0.132	0.131	0.13	0.526
19.667	2.365	0.379	0.113	0.343	0.164	0.318	0.0938	0.291	0.118	0.0363	0.026	0.1	0.0653	0.134	0.132	0.132	0.13	0.528
19.75	2.383	0.38	0.114	0.343	0.165	0.319	0.094	0.291	0.118	0.0366	0.0262	0.1	0.0657	0.134	0.132	0.132	0.13	0.528
19.833	2.401	0.38	0.114	0.344	0.165	0.32	0.0942	0.292	0.118	0.0368	0.0263	0.1	0.0659	0.134	0.133	0.132	0.13	0.529
19.917	2.42	0.381	0.115	0.345	0.165	0.32	0.0944	0.293	0.119	0.037	0.0265	0.1	0.0662	0.134	0.133	0.132	0.131	0.53
20	2.438	0.382	0.116	0.346	0.166	0.321	0.0945	0.293	0.119	0.0373	0.0266	0.1	0.0664	0.135	0.133	0.133	0.131	0.532
20.083	2.456	0.383	0.116	0.346	0.166	0.322	0.0947	0.294	0.119	0.0375	0.0267	0.1	0.0666	0.135	0.134	0.133	0.131	0.533
20.167	2.474	0.383	0.117	0.347	0.166	0.323	0.0949	0.295	0.12	0.0377	0.0268	0.1	0.0668	0.135	0.134	0.133	0.132	0.534
20.25	2.492	0.384	0.118	0.348	0.167	0.323	0.0951	0.296	0.12	0.0379	0.0269	0.1	0.067	0.136	0.134	0.134	0.132	0.536
20.333	2.51	0.385	0.118	0.349	0.167	0.324	0.0954	0.296	0.12	0.038	0.027	0.1	0.0671	0.136	0.134	0.134	0.132	0.536
20.417	2.528	0.386	0.119	0.349	0.168	0.325	0.0956	0.297	0.12	0.0382	0.027	0.1	0.0672	0.136	0.135	0.134	0.132	0.537
20.5	2.546	0.387	0.12	0.35	0.168	0.325	0.0958	0.298	0.121	0.0383	0.0271	0.1	0.0672	0.136	0.135	0.134	0.133	0.538
20.583	2.564	0.388	0.12	0.351	0.168	0.326	0.096	0.299	0.121	0.0385	0.0272	0.1	0.0673	0.137	0.135	0.135	0.133	0.54

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
20.667	2.581	0.389	0.121	0.352	0.169	0.327	0.0962	0.3	0.121	0.0386	0.0272	0.1	0.0673	0.137	0.136	0.135	0.133	0.541
20.75	2.599	0.389	0.121	0.353	0.169	0.328	0.0964	0.301	0.122	0.0387	0.0273	0.1	0.0673	0.137	0.136	0.135	0.134	0.542
20.833	2.617	0.39	0.122	0.353	0.17	0.328	0.0967	0.302	0.122	0.0389	0.0273	0.1	0.0673	0.138	0.136	0.136	0.134	0.544
20.917	2.635	0.391	0.123	0.354	0.17	0.329	0.0969	0.303	0.122	0.039	0.0273	0.1	0.0673	0.138	0.137	0.136	0.134	0.545
21	2.653	0.392	0.123	0.355	0.17	0.33	0.0971	0.304	0.123	0.0391	0.0274	0.1	0.0673	0.138	0.137	0.136	0.135	0.546
21.083	2.67	0.393	0.124	0.356	0.171	0.331	0.0974	0.305	0.123	0.0392	0.0274	0.1	0.0673	0.139	0.137	0.137	0.135	0.548
21.167	2.688	0.394	0.124	0.357	0.171	0.331	0.0976	0.306	0.123	0.0393	0.0274	0.1	0.0673	0.139	0.138	0.137	0.135	0.549
21.25	2.706	0.395	0.125	0.357	0.172	0.332	0.0978	0.307	0.124	0.0394	0.0274	0.1	0.0673	0.139	0.138	0.137	0.136	0.55
21.333	2.724	0.396	0.125	0.358	0.172	0.333	0.0981	0.309	0.124	0.0394	0.0274	0.1	0.0673	0.14	0.138	0.138	0.136	0.552
21.417	2.741	0.397	0.126	0.359	0.173	0.333	0.0983	0.31	0.124	0.0395	0.0274	0.1	0.0673	0.14	0.139	0.138	0.136	0.553
21.5	2.759	0.398	0.126	0.36	0.173	0.334	0.0986	0.311	0.125	0.0396	0.0274	0.1	0.0673	0.14	0.139	0.138	0.137	0.554
21.583	2.776	0.399	0.126	0.361	0.174	0.335	0.0988	0.312	0.125	0.0396	0.0274	0.1	0.0673	0.141	0.139	0.139	0.137	0.556
21.667	2.794	0.4	0.127	0.362	0.174	0.336	0.0991	0.313	0.126	0.0397	0.0274	0.1	0.0673	0.141	0.14	0.139	0.137	0.557
21.75	2.812	0.401	0.127	0.363	0.175	0.336	0.0994	0.314	0.126	0.0398	0.0274	0.1	0.0673	0.141	0.14	0.139	0.138	0.558
21.833	2.829	0.403	0.128	0.364	0.175	0.337	0.0996	0.315	0.126	0.0398	0.0274	0.1	0.0673	0.142	0.14	0.14	0.138	0.56
21.917	2.846	0.404	0.128	0.364	0.176	0.338	0.0999	0.316	0.127	0.0399	0.0274	0.1	0.0673	0.142	0.141	0.14	0.138	0.561
22	2.864	0.405	0.128	0.365	0.176	0.339	0.1	0.317	0.127	0.0399	0.0274	0.1	0.0673	0.142	0.141	0.141	0.139	0.563
22.083	2.881	0.406	0.129	0.366	0.177	0.339	0.1	0.318	0.128	0.0399	0.0274	0.1	0.0673	0.143	0.141	0.141	0.139	0.564
22.167	2.899	0.407	0.129	0.367	0.177	0.34	0.101	0.319	0.128	0.04	0.0274	0.1	0.0673	0.143	0.142	0.141	0.14	0.566
22.25	2.916	0.408	0.129	0.368	0.178	0.341	0.101	0.32	0.128	0.04	0.0274	0.1	0.0673	0.144	0.142	0.142	0.14	0.568
22.333	2.933	0.409	0.129	0.369	0.178	0.342	0.101	0.321	0.129	0.04	0.0274	0.1	0.0673	0.144	0.143	0.142	0.14	0.569
22.417	2.951	0.411	0.13	0.37	0.179	0.342	0.102	0.322	0.129	0.04	0.0274	0.1	0.0673	0.144	0.143	0.142	0.141	0.57
22.5	2.968	0.412	0.13	0.371	0.179	0.343	0.102	0.323	0.13	0.04	0.0274	0.1	0.0673	0.145	0.143	0.143	0.141	0.572
22.583	2.985	0.413	0.13	0.372	0.18	0.344	0.102	0.324	0.13	0.04	0.0274	0.1	0.0673	0.145	0.144	0.143	0.142	0.574
22.667	3.002	0.414	0.13	0.373	0.181	0.345	0.102	0.325	0.13	0.0401	0.0274	0.1	0.0673	0.146	0.144	0.144	0.142	0.576
22.75	3.02	0.415	0.131	0.374	0.181	0.346	0.103	0.326	0.131	0.0401	0.0274	0.1	0.0673	0.146	0.145	0.144	0.142	0.577
22.833	3.037	0.417	0.131	0.375	0.182	0.346	0.103	0.327	0.131	0.0401	0.0274	0.1	0.0673	0.146	0.145	0.144	0.143	0.578
22.917	3.054	0.418	0.131	0.376	0.182	0.347	0.103	0.328	0.131	0.0401	0.0274	0.1	0.0673	0.147	0.145	0.145	0.143	0.58
23	3.071	0.419	0.131	0.377	0.183	0.348	0.104	0.329	0.132	0.0401	0.0274	0.1	0.0673	0.147	0.146	0.145	0.144	0.582
23.083	3.088	0.42	0.132	0.378	0.183	0.349	0.104	0.329	0.132	0.0401	0.0274	0.1	0.0673	0.148	0.146	0.146	0.144	0.584
23.167	3.105	0.422	0.132	0.379	0.184	0.35	0.104	0.33	0.132	0.0401	0.0274	0.1	0.0673	0.148	0.147	0.146	0.144	0.585
23.25	3.122	0.423	0.132	0.38	0.184	0.35	0.105	0.331	0.133	0.0401	0.0274	0.1	0.0673	0.148	0.147	0.147	0.145	0.587
23.333	3.139	0.424	0.132	0.382	0.185	0.351	0.105	0.332	0.133	0.0401	0.0274	0.1	0.0673	0.149	0.147	0.147	0.145	0.588
23.417	3.156	0.425	0.132	0.383	0.185	0.352	0.105	0.332	0.133	0.0401	0.0274	0.1	0.0673	0.149	0.148	0.147	0.146	0.59
23.5	3.173	0.426	0.133	0.384	0.186	0.353	0.105	0.333	0.134	0.0401	0.0274	0.1	0.0673	0.15	0.148	0.148	0.146	0.592
23.583	3.19	0.427	0.133	0.385	0.186	0.354	0.106	0.334	0.134	0.0401	0.0274	0.1	0.0673	0.15	0.149	0.148	0.147	0.594
23.667	3.206	0.428	0.133	0.386	0.186	0.354	0.106	0.334	0.134	0.0401	0.0274	0.1	0.0673	0.151	0.149	0.149	0.147	0.596
23.75	3.223	0.43	0.133	0.387	0.187	0.355	0.106	0.335	0.135	0.0401	0.0274	0.1	0.0673	0.151	0.15	0.149	0.147	0.597
23.833	3.24	0.431	0.133	0.388	0.187	0.356	0.107	0.336	0.135	0.0401	0.0274	0.1	0.0673	0.151	0.15	0.149	0.148	0.598
23.917	3.257	0.432	0.133	0.389	0.188	0.357	0.107	0.336	0.135	0.0401	0.0274	0.1	0.0673	0.152	0.15	0.15	0.148	0.6
24	3.274	0.433	0.133	0.39	0.188	0.358	0.107	0.337	0.135	0.0401	0.0274	0.1	0.0673	0.152	0.151	0.15	0.149	0.602
24.083	3.29	0.434	0.134	0.391	0.189	0.359	0.107	0.337	0.136	0.0401	0.0274	0.1	0.0673	0.153	0.151	0.151	0.149	0.604
24.167	3.307	0.435	0.134	0.392	0.189	0.359	0.108	0.338	0.136	0.0401	0.0274	0.1	0.0673	0.153	0.152	0.151	0.149	0.605
24.25	3.323	0.436	0.134	0.393	0.189	0.36	0.108	0.339	0.136	0.0401	0.0274	0.1	0.0673	0.153	0.152	0.151	0.15	0.606
24.333	3.34	0.437	0.134	0.394	0.19	0.361	0.108	0.339	0.137	0.0401	0.0274	0.1	0.0673	0.154	0.152	0.152	0.15	0.608
24.417	3.357	0.438	0.134	0.395	0.19	0.362	0.108	0.34	0.137	0.0401	0.0274	0.1	0.0673	0.154	0.153	0.152	0.15	0.609
24.5	3.373	0.439	0.134	0.395	0.191	0.363	0.109	0.34	0.137	0.0401	0.0274	0.1	0.0673	0.154	0.153	0.152	0.151	0.61
24.583	3.39	0.439	0.134	0.396	0.191	0.364	0.109	0.341	0.137	0.0401	0.0274	0.1	0.0673	0.155	0.153	0.153	0.151	0.612
24.667	3.406	0.44	0.134	0.397	0.191	0.364	0.109	0.341	0.138	0.0401	0.0274	0.1	0.0673	0.155	0.154	0.153	0.151	0.613
24.75	3.422	0.441	0.134	0.398	0.192	0.365	0.109	0.342	0.138	0.0401	0.0274	0.1	0.0673	0.155	0.154	0.154	0.152	0.615
24.833	3.439	0.442	0.134	0.399	0.192	0.366	0.11	0.342	0.138	0.0401	0.0274	0.1	0.0673	0.156	0.154	0.154	0.152	0.616
24.917	3.455	0.443	0.134	0.4	0.192	0.367	0.11	0.342	0.138	0.0401	0.0274	0.1	0.0673	0.156	0.155	0.154	0.152	0.617
25	3.471	0.444	0.134	0.401	0.193	0.368	0.11	0.343	0.138	0.0401	0.0274	0.1	0.0673	0.156	0.155	0.155	0.153	0.619
25.083	3.488	0.445	0.134	0.402	0.193	0.369	0.11	0.343	0.139	0.0401	0.0274	0.1	0.0673	0.157	0.155	0.155	0.153	0.62
25.167	3.504	0.445	0.135	0.402	0.193	0.37	0.11	0.344	0.139	0.0401	0.0274	0.1	0.0673	0.157	0.156	0.155	0.153	0.621
25.25	3.521	0.446	0.135	0.403	0.194	0.37	0.111	0.344	0.139	0.0401	0.0274	0.1	0.0673	0.157	0.156	0.155	0.154	0.622
25.333	3.537	0.447	0.135	0.404	0.194	0.371	0.111	0.345	0.139	0.0401	0.0274	0.1	0.0673	0.158	0.156	0.156	0.154	0.624
25.417	3.554	0.448	0.135	0.405	0.194	0.372	0.111	0.345	0.139	0.0401	0.0274	0.1	0.0673	0.158	0.157	0.156	0.154	0.625
25.5	3.571	0.449	0.135	0.405	0.195	0.373	0.111	0.345	0.14	0.0401	0.0274	0.1	0.0673	0.158	0.157	0.156	0.155	0.626
25.583	3.587	0.449	0.135	0.406	0.195	0.374	0.111	0.346	0.14	0.0401	0.0274	0.1	0.0673	0.159	0.157	0.157	0.155	0.628
25.667	3.604	0.45	0.135	0.407	0.195	0.375	0.112	0.346	0.14	0.0401	0.0274	0.1	0.0673	0.159	0.157	0.157	0.155	0.628
25.75	3.621	0.451	0.135	0.408	0.195	0.375	0.112	0.346	0.14	0.0401	0.0274	0.1	0.0673	0.159	0.158	0.157	0.156	0.63
25.833	3.638	0.451	0.135	0.408	0.196	0.376	0.112	0.347	0.14	0.0401	0.0274	0.1	0.0673	0.159	0.158	0.158	0.156	0.631

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
25.917	3.654	0.452	0.135	0.409	0.196	0.377	0.112	0.347	0.141	0.0401	0.0274	0.1	0.0673	0.16	0.158	0.158	0.156	0.632
26	3.671	0.453	0.135	0.41	0.196	0.378	0.112	0.347	0.141	0.0401	0.0274	0.1	0.0673	0.16	0.159	0.158	0.156	0.633
26.083	3.688	0.453	0.135	0.41	0.196	0.378	0.112	0.348	0.141	0.0401	0.0274	0.1	0.0673	0.16	0.159	0.158	0.157	0.634
26.167	3.705	0.454	0.135	0.411	0.197	0.379	0.113	0.348	0.141	0.0401	0.0274	0.1	0.0673	0.161	0.159	0.159	0.157	0.636
26.25	3.722	0.455	0.135	0.412	0.197	0.38	0.113	0.348	0.141	0.0401	0.0274	0.1	0.0673	0.161	0.159	0.159	0.157	0.636
26.333	3.739	0.455	0.135	0.412	0.197	0.381	0.113	0.349	0.141	0.0401	0.0274	0.1	0.0673	0.161	0.16	0.159	0.157	0.637
26.417	3.756	0.456	0.135	0.413	0.197	0.381	0.113	0.349	0.141	0.0401	0.0274	0.1	0.0673	0.161	0.16	0.159	0.158	0.638
26.5	3.773	0.456	0.135	0.414	0.198	0.382	0.113	0.349	0.142	0.0401	0.0274	0.1	0.0673	0.162	0.16	0.16	0.158	0.64
26.583	3.79	0.457	0.135	0.414	0.198	0.383	0.113	0.35	0.142	0.0401	0.0274	0.1	0.0673	0.162	0.16	0.16	0.158	0.64
26.667	3.808	0.457	0.135	0.415	0.198	0.383	0.113	0.35	0.142	0.0401	0.0274	0.1	0.0673	0.162	0.161	0.16	0.158	0.641
26.75	3.825	0.458	0.135	0.415	0.198	0.384	0.114	0.35	0.142	0.0401	0.0274	0.1	0.0673	0.162	0.161	0.16	0.159	0.642
26.833	3.842	0.459	0.135	0.416	0.199	0.385	0.114	0.35	0.142	0.0401	0.0274	0.1	0.0673	0.162	0.161	0.161	0.159	0.643
26.917	3.86	0.459	0.135	0.417	0.199	0.385	0.114	0.351	0.142	0.0401	0.0274	0.1	0.0673	0.163	0.161	0.161	0.159	0.644
27	3.877	0.46	0.135	0.417	0.199	0.386	0.114	0.351	0.142	0.0401	0.0274	0.1	0.0673	0.163	0.161	0.161	0.159	0.644
27.083	3.894	0.46	0.135	0.418	0.199	0.386	0.114	0.351	0.143	0.0401	0.0274	0.1	0.0673	0.163	0.162	0.161	0.159	0.645
27.167	3.912	0.461	0.135	0.418	0.199	0.387	0.114	0.351	0.143	0.0401	0.0274	0.1	0.0673	0.163	0.162	0.161	0.16	0.646
27.25	3.929	0.461	0.135	0.419	0.2	0.388	0.114	0.352	0.143	0.0401	0.0274	0.1	0.0674	0.163	0.162	0.162	0.16	0.647
27.333	3.947	0.462	0.135	0.419	0.2	0.388	0.115	0.352	0.143	0.0401	0.0274	0.1	0.0676	0.164	0.162	0.162	0.16	0.648
27.417	3.964	0.462	0.135	0.42	0.2	0.389	0.115	0.352	0.143	0.0401	0.0275	0.1	0.0678	0.164	0.162	0.162	0.16	0.648
27.5	3.982	0.463	0.135	0.42	0.2	0.39	0.115	0.352	0.143	0.0402	0.0276	0.1	0.0679	0.164	0.163	0.162	0.16	0.649
27.583	4	0.463	0.135	0.421	0.2	0.39	0.115	0.353	0.143	0.0403	0.0277	0.1	0.0685	0.164	0.163	0.162	0.161	0.65
27.667	4.018	0.464	0.135	0.421	0.201	0.391	0.115	0.353	0.144	0.0404	0.0278	0.1	0.069	0.164	0.163	0.163	0.161	0.651
27.75	4.035	0.464	0.135	0.422	0.201	0.391	0.115	0.353	0.144	0.0405	0.028	0.1	0.0695	0.165	0.163	0.163	0.161	0.652
27.833	4.053	0.465	0.135	0.422	0.201	0.392	0.115	0.354	0.144	0.0407	0.0282	0.1	0.0703	0.165	0.163	0.163	0.161	0.652
27.917	4.071	0.465	0.136	0.423	0.201	0.393	0.115	0.354	0.144	0.0408	0.0285	0.1	0.0711	0.165	0.164	0.163	0.162	0.654
28	4.089	0.466	0.136	0.423	0.202	0.393	0.116	0.355	0.144	0.041	0.0287	0.1	0.0719	0.165	0.164	0.163	0.162	0.654
28.083	4.107	0.466	0.136	0.424	0.202	0.394	0.116	0.355	0.145	0.0412	0.029	0.1	0.0727	0.166	0.164	0.164	0.162	0.656
28.167	4.125	0.467	0.136	0.424	0.202	0.395	0.116	0.356	0.145	0.0414	0.0293	0.1	0.0734	0.166	0.164	0.164	0.162	0.656
28.25	4.143	0.468	0.137	0.425	0.202	0.395	0.116	0.356	0.145	0.0417	0.0295	0.1	0.0742	0.166	0.165	0.164	0.162	0.657
28.333	4.161	0.468	0.137	0.426	0.203	0.396	0.116	0.357	0.145	0.0419	0.0298	0.1	0.0747	0.166	0.165	0.164	0.163	0.658
28.417	4.179	0.469	0.138	0.426	0.203	0.397	0.116	0.357	0.145	0.0422	0.03	0.1	0.0753	0.166	0.165	0.165	0.163	0.659
28.5	4.197	0.47	0.138	0.427	0.203	0.397	0.117	0.358	0.146	0.0425	0.0303	0.1	0.0758	0.167	0.165	0.165	0.163	0.66
28.583	4.215	0.47	0.138	0.427	0.204	0.398	0.117	0.358	0.146	0.0428	0.0305	0.101	0.0762	0.167	0.165	0.165	0.163	0.66
28.667	4.234	0.471	0.139	0.428	0.204	0.399	0.117	0.359	0.146	0.0431	0.0306	0.101	0.0766	0.167	0.166	0.165	0.164	0.662
28.75	4.252	0.472	0.139	0.429	0.204	0.399	0.117	0.359	0.146	0.0433	0.0308	0.102	0.077	0.167	0.166	0.165	0.164	0.662
28.833	4.27	0.473	0.14	0.429	0.205	0.4	0.117	0.36	0.147	0.0436	0.031	0.102	0.0773	0.168	0.166	0.166	0.164	0.664
28.917	4.289	0.473	0.141	0.43	0.205	0.401	0.117	0.361	0.147	0.0438	0.0311	0.103	0.0775	0.168	0.166	0.166	0.164	0.664
29	4.307	0.474	0.141	0.43	0.205	0.401	0.118	0.362	0.147	0.0441	0.0312	0.103	0.0778	0.168	0.167	0.166	0.165	0.666
29.083	4.326	0.475	0.142	0.431	0.206	0.402	0.118	0.362	0.147	0.0443	0.0314	0.104	0.078	0.168	0.167	0.166	0.165	0.666
29.167	4.344	0.476	0.142	0.432	0.206	0.403	0.118	0.363	0.148	0.0445	0.0315	0.104	0.0782	0.169	0.167	0.167	0.165	0.668
29.25	4.363	0.476	0.143	0.433	0.206	0.403	0.118	0.364	0.148	0.0447	0.0316	0.105	0.0784	0.169	0.168	0.167	0.165	0.669
29.333	4.381	0.477	0.144	0.433	0.207	0.404	0.118	0.365	0.148	0.0449	0.0316	0.105	0.0785	0.169	0.168	0.167	0.166	0.67
29.417	4.4	0.478	0.144	0.434	0.207	0.405	0.119	0.365	0.148	0.0451	0.0317	0.105	0.0787	0.17	0.168	0.168	0.166	0.672
29.5	4.419	0.479	0.145	0.435	0.207	0.406	0.119	0.366	0.149	0.0452	0.0318	0.106	0.0788	0.17	0.168	0.168	0.166	0.672
29.583	4.438	0.48	0.146	0.435	0.208	0.406	0.119	0.367	0.149	0.0454	0.0319	0.106	0.0788	0.17	0.169	0.168	0.166	0.673
29.667	4.456	0.481	0.146	0.436	0.208	0.407	0.119	0.368	0.149	0.0455	0.0319	0.106	0.0788	0.17	0.169	0.168	0.167	0.674
29.75	4.475	0.482	0.147	0.437	0.209	0.408	0.12	0.369	0.15	0.0457	0.032	0.107	0.0789	0.171	0.169	0.169	0.167	0.676
29.833	4.494	0.482	0.148	0.438	0.209	0.408	0.12	0.37	0.15	0.0458	0.032	0.107	0.0789	0.171	0.17	0.169	0.167	0.677
29.917	4.513	0.483	0.148	0.438	0.209	0.409	0.12	0.371	0.15	0.0459	0.0321	0.107	0.0789	0.171	0.17	0.169	0.168	0.678
30	4.532	0.484	0.149	0.439	0.21	0.41	0.12	0.372	0.151	0.046	0.0321	0.107	0.0789	0.172	0.17	0.17	0.168	0.68
30.083	4.551	0.485	0.149	0.44	0.21	0.41	0.12	0.373	0.151	0.0461	0.0321	0.108	0.0789	0.172	0.171	0.17	0.168	0.681
30.167	4.57	0.486	0.15	0.441	0.211	0.411	0.121	0.374	0.151	0.0462	0.0321	0.108	0.0789	0.172	0.171	0.17	0.169	0.682
30.25	4.59	0.487	0.15	0.442	0.211	0.412	0.121	0.375	0.152	0.0463	0.0321	0.108	0.0789	0.173	0.171	0.171	0.169	0.684
30.333	4.609	0.488	0.151	0.442	0.212	0.413	0.121	0.377	0.152	0.0464	0.0322	0.108	0.079	0.173	0.171	0.171	0.169	0.684
30.417	4.628	0.489	0.151	0.443	0.212	0.413	0.121	0.378	0.152	0.0465	0.0322	0.108	0.0792	0.173	0.172	0.171	0.17	0.686
30.5	4.647	0.49	0.152	0.444	0.213	0.414	0.122	0.379	0.153	0.0466	0.0323	0.109	0.0794	0.174	0.172	0.172	0.17	0.688
30.583	4.667	0.491	0.152	0.445	0.213	0.415	0.122	0.38	0.153	0.0468	0.0324	0.109	0.0799	0.174	0.173	0.172	0.17	0.689
30.667	4.686	0.493	0.153	0.446	0.214	0.416	0.122	0.382	0.154	0.047	0.0325	0.109	0.0803	0.174	0.173	0.172	0.171	0.69
30.75	4.706	0.494	0.153	0.447	0.214	0.417	0.123	0.383	0.154	0.0471	0.0327	0.11	0.0808	0.175	0.173	0.173	0.171	0.692
30.833	4.725	0.495	0.154	0.448	0.215	0.417	0.123	0.384	0.155	0.0473	0.0329	0.11	0.0816	0.175	0.174	0.173	0.172	0.694
30.917	4.745	0.496	0.155	0.449	0.215	0.418	0.123	0.385	0.155	0.0475	0.0331	0.111	0.0824	0.176	0.174	0.174	0.172	0.696
31	4.764	0.497	0.155	0.45	0.216	0.419	0.123	0.387	0.156	0.0478	0.0334	0.111	0.0832	0.176	0.175	0.174	0.172	0.697
31.083	4.784	0.499	0.156	0.451	0.217	0.42	0.124	0.388	0.156	0.048	0.0337	0.112	0.084	0.176	0.175	0.174	0.173	0.698

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
31.167	4.804	0.5	0.156	0.452	0.217	0.421	0.124	0.389	0.157	0.0483	0.0339	0.113	0.0848	0.177	0.175	0.175	0.173	0.7
31.25	4.824	0.501	0.157	0.453	0.218	0.422	0.124	0.391	0.157	0.0485	0.0342	0.113	0.0855	0.177	0.176	0.175	0.174	0.702
31.333	4.844	0.503	0.158	0.454	0.218	0.423	0.125	0.392	0.158	0.0488	0.0345	0.114	0.0861	0.178	0.176	0.176	0.174	0.704
31.417	4.863	0.504	0.158	0.456	0.219	0.423	0.125	0.394	0.158	0.0491	0.0347	0.115	0.0867	0.178	0.177	0.176	0.175	0.706
31.5	4.883	0.506	0.159	0.457	0.22	0.424	0.125	0.395	0.159	0.0494	0.035	0.115	0.0873	0.179	0.177	0.177	0.175	0.708
31.583	4.903	0.507	0.16	0.458	0.22	0.425	0.126	0.396	0.159	0.0497	0.0352	0.116	0.0877	0.179	0.178	0.177	0.176	0.71
31.667	4.923	0.509	0.16	0.459	0.221	0.426	0.126	0.398	0.16	0.05	0.0354	0.117	0.0881	0.18	0.178	0.178	0.176	0.712
31.75	4.943	0.51	0.161	0.461	0.222	0.427	0.127	0.399	0.16	0.0503	0.0356	0.117	0.0884	0.18	0.179	0.178	0.177	0.714
31.833	4.964	0.512	0.162	0.462	0.223	0.428	0.127	0.401	0.161	0.0505	0.0357	0.118	0.0887	0.181	0.179	0.179	0.177	0.716
31.917	4.984	0.514	0.163	0.463	0.223	0.429	0.127	0.402	0.161	0.0508	0.0358	0.119	0.089	0.181	0.18	0.179	0.178	0.718
32	5.004	0.515	0.164	0.465	0.224	0.43	0.128	0.404	0.162	0.051	0.036	0.119	0.0893	0.182	0.18	0.18	0.178	0.72
32.083	5.024	0.517	0.164	0.466	0.225	0.431	0.128	0.405	0.162	0.0512	0.0361	0.12	0.0895	0.182	0.181	0.18	0.179	0.722
32.167	5.045	0.519	0.165	0.467	0.225	0.432	0.129	0.407	0.163	0.0515	0.0362	0.12	0.0897	0.183	0.181	0.181	0.179	0.724
32.25	5.065	0.52	0.166	0.469	0.226	0.433	0.129	0.408	0.163	0.0517	0.0363	0.121	0.09	0.183	0.182	0.181	0.18	0.726
32.333	5.086	0.522	0.167	0.47	0.227	0.434	0.129	0.41	0.164	0.0518	0.0364	0.121	0.0901	0.184	0.182	0.182	0.18	0.728
32.417	5.106	0.523	0.168	0.472	0.228	0.435	0.13	0.411	0.164	0.052	0.0365	0.121	0.0902	0.184	0.183	0.183	0.181	0.731
32.5	5.127	0.525	0.169	0.473	0.228	0.436	0.13	0.413	0.165	0.0522	0.0366	0.122	0.0903	0.185	0.184	0.183	0.181	0.733
32.583	5.147	0.527	0.17	0.475	0.229	0.437	0.131	0.414	0.165	0.0523	0.0366	0.122	0.0904	0.186	0.184	0.184	0.182	0.736
32.667	5.168	0.528	0.17	0.476	0.23	0.438	0.131	0.416	0.166	0.0525	0.0367	0.122	0.0904	0.186	0.185	0.184	0.183	0.738
32.75	5.189	0.53	0.171	0.477	0.231	0.439	0.132	0.418	0.166	0.0526	0.0367	0.123	0.0904	0.187	0.185	0.185	0.183	0.74
32.833	5.21	0.532	0.172	0.479	0.231	0.441	0.132	0.419	0.167	0.0527	0.0368	0.123	0.0904	0.187	0.186	0.185	0.184	0.742
32.917	5.23	0.534	0.173	0.48	0.232	0.442	0.132	0.421	0.168	0.0529	0.0368	0.123	0.0904	0.188	0.187	0.186	0.184	0.745
33	5.251	0.535	0.173	0.482	0.233	0.443	0.133	0.422	0.168	0.053	0.0369	0.123	0.0904	0.189	0.187	0.187	0.185	0.748
33.083	5.272	0.537	0.174	0.483	0.234	0.444	0.133	0.424	0.169	0.0531	0.0369	0.123	0.0904	0.189	0.188	0.187	0.186	0.75
33.167	5.293	0.539	0.175	0.485	0.234	0.445	0.134	0.426	0.169	0.0532	0.0369	0.124	0.0904	0.19	0.188	0.188	0.186	0.752
33.25	5.314	0.54	0.175	0.486	0.235	0.446	0.134	0.427	0.17	0.0533	0.0369	0.124	0.0904	0.19	0.189	0.188	0.187	0.754
33.333	5.336	0.542	0.176	0.488	0.236	0.447	0.134	0.429	0.17	0.0534	0.0369	0.124	0.0906	0.191	0.19	0.189	0.187	0.757
33.417	5.357	0.544	0.176	0.489	0.237	0.449	0.135	0.431	0.171	0.0535	0.037	0.124	0.0907	0.192	0.19	0.19	0.188	0.76
33.5	5.378	0.545	0.177	0.491	0.237	0.45	0.135	0.433	0.172	0.0536	0.037	0.125	0.0909	0.192	0.191	0.19	0.189	0.762
33.583	5.399	0.547	0.178	0.492	0.238	0.451	0.136	0.434	0.172	0.0538	0.0372	0.125	0.0913	0.193	0.191	0.191	0.189	0.764
33.667	5.421	0.549	0.178	0.494	0.239	0.452	0.136	0.436	0.173	0.0539	0.0373	0.125	0.0918	0.193	0.192	0.191	0.19	0.766
33.75	5.442	0.551	0.179	0.496	0.24	0.454	0.137	0.438	0.174	0.0541	0.0374	0.126	0.0923	0.194	0.193	0.192	0.19	0.769
33.833	5.464	0.553	0.18	0.497	0.24	0.455	0.137	0.44	0.174	0.0543	0.0376	0.126	0.093	0.195	0.193	0.193	0.191	0.772
33.917	5.485	0.554	0.18	0.499	0.241	0.456	0.138	0.441	0.175	0.0545	0.0378	0.127	0.0938	0.195	0.194	0.193	0.192	0.774
34	5.507	0.556	0.181	0.5	0.242	0.458	0.138	0.443	0.176	0.0547	0.0381	0.127	0.0946	0.196	0.194	0.194	0.192	0.776
34.083	5.528	0.558	0.182	0.502	0.243	0.459	0.138	0.445	0.176	0.055	0.0383	0.128	0.0953	0.197	0.195	0.195	0.193	0.78
34.167	5.55	0.56	0.182	0.504	0.244	0.46	0.139	0.447	0.177	0.0552	0.0386	0.128	0.0961	0.197	0.196	0.195	0.194	0.782
34.25	5.572	0.562	0.183	0.505	0.245	0.462	0.139	0.449	0.178	0.0554	0.0389	0.129	0.0969	0.198	0.196	0.196	0.194	0.784
34.333	5.594	0.564	0.183	0.507	0.246	0.463	0.14	0.45	0.178	0.0557	0.0392	0.13	0.0975	0.198	0.197	0.197	0.195	0.787
34.417	5.615	0.566	0.184	0.509	0.246	0.465	0.14	0.452	0.179	0.056	0.0394	0.13	0.0981	0.199	0.198	0.197	0.196	0.79
34.5	5.637	0.568	0.185	0.51	0.247	0.466	0.141	0.454	0.18	0.0563	0.0397	0.131	0.0987	0.2	0.198	0.198	0.196	0.792
34.583	5.659	0.57	0.186	0.512	0.248	0.467	0.141	0.456	0.18	0.0566	0.0399	0.132	0.0991	0.201	0.199	0.199	0.197	0.796
34.667	5.681	0.572	0.186	0.514	0.249	0.469	0.142	0.458	0.181	0.0569	0.0401	0.133	0.0995	0.201	0.2	0.199	0.198	0.798
34.75	5.704	0.574	0.187	0.516	0.25	0.47	0.142	0.459	0.182	0.0572	0.0403	0.133	0.0999	0.202	0.201	0.2	0.198	0.801
34.833	5.726	0.576	0.188	0.518	0.251	0.472	0.143	0.461	0.182	0.0575	0.0404	0.134	0.1	0.203	0.201	0.201	0.199	0.804
34.917	5.748	0.578	0.189	0.519	0.252	0.473	0.143	0.463	0.183	0.0577	0.0406	0.134	0.101	0.203	0.202	0.201	0.2	0.806
35	5.77	0.581	0.189	0.521	0.253	0.475	0.144	0.465	0.184	0.058	0.0407	0.135	0.101	0.204	0.203	0.202	0.201	0.81
35.083	5.793	0.583	0.19	0.523	0.254	0.476	0.144	0.467	0.184	0.0582	0.0408	0.136	0.101	0.205	0.203	0.203	0.201	0.812
35.167	5.815	0.585	0.191	0.525	0.255	0.478	0.145	0.469	0.185	0.0584	0.0409	0.136	0.101	0.206	0.204	0.204	0.202	0.816
35.25	5.838	0.587	0.192	0.527	0.256	0.479	0.146	0.47	0.186	0.0586	0.041	0.136	0.101	0.206	0.205	0.204	0.203	0.818
35.333	5.86	0.589	0.193	0.529	0.257	0.481	0.146	0.472	0.187	0.0588	0.0411	0.137	0.102	0.207	0.206	0.205	0.204	0.822
35.417	5.883	0.591	0.194	0.531	0.258	0.482	0.147	0.474	0.187	0.059	0.0412	0.137	0.102	0.208	0.206	0.206	0.204	0.824
35.5	5.905	0.593	0.195	0.533	0.259	0.484	0.147	0.476	0.188	0.0592	0.0413	0.138	0.102	0.209	0.207	0.207	0.205	0.828
35.583	5.928	0.595	0.195	0.534	0.259	0.485	0.148	0.478	0.189	0.0593	0.0414	0.138	0.102	0.209	0.208	0.207	0.206	0.83
35.667	5.951	0.597	0.196	0.536	0.26	0.487	0.148	0.48	0.189	0.0595	0.0414	0.138	0.102	0.21	0.209	0.208	0.207	0.834
35.75	5.974	0.6	0.197	0.538	0.261	0.488	0.149	0.482	0.19	0.0596	0.0415	0.138	0.102	0.211	0.209	0.209	0.207	0.836
35.833	5.997	0.602	0.198	0.54	0.262	0.49	0.149	0.483	0.191	0.0597	0.0415	0.139	0.102	0.212	0.21	0.21	0.208	0.84
35.917	6.02	0.604	0.198	0.542	0.263	0.491	0.15	0.485	0.191	0.0598	0.0416	0.139	0.102	0.212	0.211	0.21	0.209	0.842
36	6.043	0.606	0.199	0.544	0.264	0.493	0.15	0.487	0.192	0.06	0.0416	0.139	0.102	0.213	0.212	0.211	0.21	0.846
36.083	6.066	0.608	0.2	0.546	0.265	0.494	0.151	0.489	0.193	0.0601	0.0416	0.139	0.102	0.214	0.212	0.212	0.21	0.848
36.167	6.089	0.61	0.2	0.547	0.266	0.496	0.151	0.491	0.193	0.0602	0.0416	0.14	0.102	0.214	0.213	0.213	0.211	0.851
36.25	6.112	0.612	0.201	0.549	0.267	0.498	0.152	0.493	0.194	0.0603	0.0417	0.14	0.102	0.215	0.214	0.213	0.212	0.854
36.333	6.136	0.614	0.202	0.551	0.268	0.499	0.152	0.495	0.195	0.0604	0.0418	0.14	0.102	0.216	0.215	0.214	0.212	0.857

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
36.417	6.159	0.616	0.202	0.553	0.269	0.501	0.153	0.497	0.196	0.0606	0.0419	0.141	0.103	0.217	0.215	0.215	0.213	0.86
36.5	6.182	0.618	0.203	0.555	0.27	0.502	0.153	0.499	0.196	0.0608	0.042	0.141	0.103	0.217	0.216	0.216	0.214	0.863
36.583	6.206	0.621	0.204	0.557	0.271	0.504	0.154	0.501	0.197	0.0611	0.0424	0.142	0.104	0.218	0.217	0.216	0.215	0.866
36.667	6.229	0.623	0.205	0.559	0.272	0.506	0.155	0.503	0.198	0.0614	0.0427	0.143	0.106	0.219	0.218	0.217	0.216	0.87
36.75	6.253	0.625	0.206	0.561	0.273	0.508	0.155	0.506	0.199	0.0617	0.0431	0.143	0.107	0.22	0.218	0.218	0.216	0.872
36.833	6.277	0.628	0.207	0.563	0.274	0.51	0.156	0.508	0.2	0.0622	0.0437	0.145	0.109	0.221	0.219	0.219	0.217	0.876
36.917	6.301	0.63	0.208	0.565	0.275	0.512	0.156	0.51	0.201	0.0627	0.0443	0.146	0.111	0.221	0.22	0.22	0.218	0.879
37	6.324	0.633	0.209	0.567	0.276	0.513	0.157	0.513	0.201	0.0632	0.0449	0.147	0.114	0.222	0.221	0.22	0.219	0.882
37.083	6.348	0.635	0.21	0.57	0.277	0.515	0.158	0.515	0.202	0.0638	0.0458	0.149	0.116	0.223	0.222	0.221	0.22	0.886
37.167	6.372	0.638	0.211	0.572	0.279	0.518	0.158	0.518	0.203	0.0645	0.0466	0.151	0.118	0.224	0.223	0.222	0.221	0.89
37.25	6.396	0.641	0.212	0.574	0.28	0.52	0.159	0.52	0.204	0.0652	0.0474	0.153	0.121	0.225	0.224	0.223	0.222	0.894
37.333	6.42	0.644	0.214	0.576	0.281	0.522	0.16	0.523	0.205	0.066	0.0482	0.155	0.122	0.226	0.225	0.224	0.222	0.897
37.417	6.444	0.646	0.215	0.579	0.282	0.524	0.16	0.526	0.206	0.0668	0.049	0.157	0.124	0.227	0.225	0.225	0.223	0.9
37.5	6.469	0.649	0.217	0.581	0.284	0.526	0.161	0.528	0.207	0.0676	0.0497	0.159	0.126	0.228	0.226	0.226	0.224	0.904
37.583	6.493	0.652	0.218	0.584	0.285	0.528	0.162	0.531	0.208	0.0685	0.0503	0.161	0.127	0.229	0.227	0.227	0.225	0.908
37.667	6.517	0.655	0.22	0.586	0.286	0.53	0.162	0.534	0.21	0.0693	0.0509	0.164	0.129	0.23	0.228	0.228	0.226	0.912
37.75	6.542	0.658	0.222	0.589	0.288	0.532	0.163	0.537	0.211	0.0702	0.0516	0.166	0.13	0.231	0.229	0.229	0.227	0.916
37.833	6.566	0.662	0.223	0.591	0.289	0.535	0.164	0.54	0.212	0.071	0.052	0.167	0.131	0.232	0.23	0.23	0.228	0.92
37.917	6.591	0.665	0.225	0.594	0.291	0.537	0.165	0.543	0.213	0.0718	0.0525	0.169	0.132	0.233	0.231	0.231	0.229	0.924
38	6.615	0.668	0.227	0.597	0.292	0.539	0.166	0.546	0.214	0.0725	0.0529	0.171	0.133	0.234	0.232	0.232	0.23	0.928
38.083	6.64	0.671	0.229	0.599	0.294	0.541	0.166	0.55	0.215	0.0732	0.0533	0.172	0.134	0.235	0.234	0.233	0.232	0.934
38.167	6.665	0.675	0.231	0.602	0.295	0.544	0.167	0.553	0.216	0.0739	0.0536	0.174	0.134	0.236	0.235	0.234	0.233	0.938
38.25	6.69	0.678	0.234	0.605	0.297	0.546	0.168	0.556	0.217	0.0745	0.054	0.175	0.135	0.237	0.236	0.235	0.234	0.942
38.333	6.715	0.681	0.236	0.608	0.298	0.548	0.169	0.56	0.218	0.0751	0.0542	0.176	0.135	0.238	0.237	0.236	0.235	0.946
38.417	6.74	0.685	0.238	0.611	0.3	0.551	0.17	0.563	0.22	0.0756	0.0545	0.178	0.136	0.239	0.238	0.238	0.236	0.951
38.5	6.765	0.688	0.24	0.614	0.301	0.553	0.171	0.566	0.221	0.0762	0.0548	0.179	0.136	0.241	0.239	0.239	0.237	0.956
38.583	6.791	0.692	0.242	0.617	0.303	0.555	0.171	0.57	0.222	0.0766	0.055	0.18	0.136	0.242	0.24	0.24	0.238	0.96
38.667	6.816	0.695	0.244	0.62	0.304	0.558	0.172	0.574	0.223	0.0771	0.0552	0.181	0.136	0.243	0.242	0.241	0.24	0.966
38.75	6.842	0.699	0.246	0.623	0.306	0.56	0.173	0.577	0.225	0.0775	0.0554	0.181	0.137	0.244	0.243	0.242	0.241	0.97
38.833	6.867	0.702	0.248	0.626	0.308	0.563	0.174	0.581	0.226	0.0779	0.0555	0.182	0.137	0.245	0.244	0.244	0.242	0.975
38.917	6.893	0.706	0.25	0.629	0.309	0.565	0.175	0.585	0.227	0.0783	0.0556	0.183	0.137	0.247	0.245	0.245	0.243	0.98
39	6.919	0.709	0.252	0.632	0.311	0.568	0.176	0.589	0.228	0.0786	0.0558	0.184	0.137	0.248	0.246	0.246	0.244	0.984
39.083	6.945	0.713	0.254	0.635	0.313	0.571	0.177	0.593	0.23	0.0789	0.0558	0.184	0.137	0.249	0.248	0.247	0.246	0.99
39.167	6.971	0.717	0.256	0.638	0.314	0.573	0.178	0.597	0.231	0.0792	0.0559	0.185	0.137	0.25	0.249	0.248	0.247	0.994
39.25	6.997	0.721	0.257	0.641	0.316	0.576	0.179	0.601	0.232	0.0796	0.0559	0.186	0.137	0.252	0.25	0.25	0.248	1
39.333	7.023	0.724	0.259	0.644	0.318	0.578	0.18	0.605	0.234	0.0799	0.056	0.186	0.137	0.253	0.251	0.251	0.249	1.004
39.417	7.049	0.728	0.261	0.648	0.319	0.581	0.18	0.61	0.235	0.0802	0.0561	0.187	0.137	0.254	0.253	0.252	0.251	1.01
39.5	7.075	0.732	0.262	0.651	0.321	0.584	0.181	0.614	0.237	0.0805	0.0562	0.187	0.137	0.255	0.254	0.254	0.252	1.015
39.583	7.102	0.736	0.264	0.654	0.323	0.587	0.182	0.618	0.238	0.0808	0.0564	0.188	0.138	0.257	0.255	0.255	0.253	1.02
39.667	7.129	0.74	0.265	0.658	0.325	0.589	0.183	0.622	0.24	0.0812	0.0566	0.189	0.139	0.258	0.257	0.256	0.255	1.026
39.75	7.155	0.744	0.267	0.661	0.327	0.592	0.184	0.627	0.241	0.0816	0.0568	0.19	0.14	0.259	0.258	0.258	0.256	1.031
39.833	7.182	0.748	0.269	0.665	0.329	0.595	0.185	0.631	0.243	0.082	0.0572	0.191	0.141	0.261	0.259	0.259	0.257	1.036
39.917	7.209	0.752	0.27	0.668	0.331	0.598	0.186	0.635	0.244	0.0825	0.0576	0.192	0.143	0.262	0.261	0.26	0.259	1.042
40	7.236	0.757	0.272	0.672	0.333	0.601	0.187	0.64	0.246	0.0829	0.058	0.193	0.144	0.264	0.262	0.262	0.26	1.048
40.083	7.263	0.761	0.273	0.675	0.335	0.604	0.189	0.644	0.247	0.0834	0.0585	0.194	0.146	0.265	0.264	0.263	0.262	1.054
40.167	7.29	0.766	0.275	0.679	0.337	0.607	0.19	0.648	0.249	0.0839	0.0591	0.195	0.147	0.267	0.265	0.265	0.263	1.06
40.25	7.317	0.77	0.276	0.683	0.339	0.61	0.191	0.653	0.251	0.0845	0.0596	0.196	0.149	0.268	0.267	0.266	0.265	1.066
40.333	7.345	0.775	0.278	0.687	0.341	0.613	0.192	0.657	0.253	0.0851	0.0601	0.198	0.15	0.27	0.268	0.268	0.266	1.072
40.417	7.372	0.779	0.28	0.69	0.343	0.617	0.193	0.661	0.254	0.0856	0.0607	0.199	0.151	0.271	0.27	0.269	0.268	1.078
40.5	7.4	0.784	0.281	0.694	0.345	0.62	0.194	0.665	0.256	0.0862	0.0612	0.201	0.152	0.273	0.271	0.271	0.269	1.084
40.583	7.428	0.789	0.283	0.698	0.348	0.623	0.195	0.67	0.258	0.0868	0.0616	0.202	0.153	0.274	0.273	0.272	0.271	1.09
40.667	7.455	0.794	0.285	0.702	0.35	0.626	0.197	0.674	0.259	0.0874	0.062	0.204	0.154	0.276	0.274	0.274	0.272	1.096
40.75	7.483	0.799	0.286	0.706	0.352	0.63	0.198	0.678	0.261	0.088	0.0624	0.205	0.155	0.277	0.276	0.276	0.274	1.103
40.833	7.511	0.804	0.288	0.71	0.354	0.633	0.199	0.682	0.263	0.0886	0.0627	0.206	0.156	0.279	0.278	0.277	0.276	1.11
40.917	7.54	0.809	0.29	0.715	0.357	0.636	0.2	0.687	0.264	0.0891	0.0631	0.207	0.156	0.281	0.279	0.279	0.277	1.116
41	7.568	0.814	0.292	0.719	0.359	0.64	0.201	0.691	0.266	0.0896	0.0634	0.209	0.157	0.282	0.281	0.281	0.279	1.123
41.083	7.596	0.819	0.294	0.723	0.361	0.643	0.203	0.695	0.267	0.0901	0.0636	0.21	0.158	0.284	0.283	0.282	0.281	1.13
41.167	7.625	0.825	0.296	0.728	0.363	0.646	0.204	0.699	0.269	0.0905	0.0638	0.211	0.158	0.286	0.284	0.284	0.283	1.137
41.25	7.653	0.83	0.297	0.732	0.366	0.65	0.205	0.703	0.271	0.091	0.0641	0.212	0.159	0.287	0.286	0.286	0.284	1.143
41.333	7.682	0.835	0.299	0.736	0.368	0.653	0.207	0.707	0.272	0.0913	0.0643	0.212	0.159	0.289	0.288	0.287	0.286	1.15
41.417	7.711	0.84	0.301	0.741	0.37	0.657	0.208	0.712	0.274	0.0917	0.0645	0.213	0.159	0.291	0.29	0.289	0.288	1.158
41.5	7.739	0.845	0.303	0.745	0.372	0.66	0.209	0.716	0.276	0.0921	0.0646	0.214	0.159	0.293	0.292	0.291	0.29	1.166
41.583	7.768	0.85	0.305	0.75	0.375	0.664	0.21	0.72	0.277	0.0924	0.0648	0.215	0.16	0.295	0.293	0.293	0.291	1.172

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
41.667	7.797	0.855	0.307	0.754	0.377	0.667	0.212	0.724	0.279	0.0927	0.0649	0.215	0.16	0.296	0.295	0.295	0.293	1.179
41.75	7.827	0.86	0.309	0.759	0.379	0.671	0.213	0.728	0.28	0.093	0.065	0.216	0.16	0.298	0.297	0.296	0.295	1.186
41.833	7.856	0.865	0.31	0.763	0.381	0.675	0.214	0.732	0.282	0.0933	0.0651	0.216	0.16	0.3	0.299	0.298	0.297	1.194
41.917	7.885	0.871	0.312	0.768	0.383	0.678	0.216	0.737	0.284	0.0935	0.0652	0.217	0.16	0.302	0.3	0.3	0.299	1.201
42	7.915	0.876	0.314	0.772	0.386	0.682	0.217	0.741	0.285	0.0937	0.0653	0.217	0.16	0.304	0.302	0.302	0.3	1.208
42.083	7.945	0.881	0.315	0.777	0.388	0.686	0.218	0.745	0.287	0.094	0.0654	0.218	0.16	0.305	0.304	0.304	0.302	1.215
42.167	7.974	0.886	0.317	0.781	0.39	0.689	0.219	0.749	0.288	0.0942	0.0654	0.218	0.16	0.307	0.306	0.305	0.304	1.222
42.25	8.004	0.891	0.318	0.786	0.392	0.693	0.221	0.753	0.29	0.0944	0.0655	0.219	0.16	0.309	0.307	0.307	0.306	1.229
42.333	8.034	0.895	0.319	0.79	0.394	0.697	0.222	0.757	0.292	0.0946	0.0655	0.219	0.16	0.311	0.309	0.309	0.307	1.236
42.417	8.064	0.9	0.321	0.795	0.396	0.701	0.223	0.761	0.293	0.0948	0.0655	0.219	0.16	0.312	0.311	0.311	0.309	1.243
42.5	8.094	0.905	0.322	0.799	0.399	0.705	0.224	0.766	0.295	0.095	0.0656	0.22	0.16	0.314	0.313	0.312	0.311	1.25
42.583	8.125	0.91	0.323	0.803	0.401	0.708	0.225	0.77	0.296	0.0952	0.0657	0.22	0.161	0.316	0.314	0.314	0.313	1.257
42.667	8.155	0.915	0.324	0.808	0.403	0.712	0.227	0.774	0.298	0.0954	0.0658	0.221	0.161	0.318	0.316	0.316	0.314	1.264
42.75	8.185	0.92	0.326	0.812	0.405	0.716	0.228	0.778	0.3	0.0956	0.0659	0.221	0.161	0.319	0.318	0.318	0.316	1.271
42.833	8.216	0.925	0.327	0.817	0.407	0.72	0.229	0.782	0.301	0.0959	0.0661	0.222	0.162	0.321	0.32	0.319	0.318	1.278
42.917	8.247	0.93	0.328	0.821	0.409	0.724	0.23	0.786	0.303	0.0961	0.0662	0.222	0.163	0.323	0.321	0.321	0.32	1.285
43	8.278	0.935	0.329	0.825	0.412	0.728	0.232	0.79	0.305	0.0964	0.0664	0.223	0.163	0.325	0.323	0.323	0.321	1.292
43.083	8.309	0.94	0.33	0.83	0.414	0.733	0.233	0.793	0.306	0.0966	0.0667	0.223	0.164	0.326	0.325	0.325	0.323	1.299
43.167	8.34	0.945	0.331	0.834	0.416	0.737	0.234	0.797	0.308	0.0969	0.067	0.224	0.165	0.328	0.327	0.326	0.325	1.306
43.25	8.371	0.95	0.332	0.839	0.418	0.741	0.235	0.801	0.309	0.0972	0.0672	0.224	0.166	0.33	0.328	0.328	0.327	1.313
43.333	8.402	0.955	0.333	0.843	0.42	0.745	0.237	0.805	0.311	0.0975	0.0675	0.225	0.166	0.332	0.33	0.33	0.328	1.32
43.417	8.434	0.96	0.334	0.848	0.423	0.749	0.238	0.809	0.313	0.0978	0.0678	0.226	0.167	0.333	0.332	0.332	0.33	1.327
43.5	8.465	0.965	0.335	0.852	0.425	0.753	0.239	0.812	0.314	0.0981	0.068	0.227	0.168	0.335	0.334	0.333	0.332	1.334
43.583	8.497	0.97	0.336	0.856	0.427	0.758	0.24	0.816	0.316	0.0984	0.0682	0.227	0.168	0.337	0.336	0.335	0.334	1.342
43.667	8.529	0.975	0.337	0.861	0.429	0.762	0.242	0.819	0.317	0.0987	0.0684	0.228	0.168	0.339	0.337	0.337	0.335	1.348
43.75	8.561	0.98	0.338	0.865	0.431	0.766	0.243	0.823	0.319	0.099	0.0687	0.229	0.169	0.34	0.339	0.339	0.337	1.355
43.833	8.593	0.985	0.339	0.87	0.434	0.77	0.244	0.827	0.32	0.0993	0.0688	0.229	0.169	0.342	0.341	0.34	0.339	1.362
43.917	8.625	0.99	0.34	0.874	0.436	0.774	0.245	0.83	0.322	0.0996	0.069	0.23	0.17	0.344	0.343	0.342	0.341	1.37
44	8.657	0.996	0.341	0.879	0.438	0.778	0.247	0.834	0.323	0.0998	0.0691	0.231	0.17	0.346	0.344	0.344	0.342	1.376
44.083	8.69	1.001	0.342	0.883	0.44	0.783	0.248	0.837	0.325	0.1	0.0693	0.231	0.17	0.347	0.346	0.346	0.344	1.383
44.167	8.722	1.006	0.343	0.888	0.442	0.787	0.249	0.84	0.326	0.1	0.0694	0.232	0.17	0.349	0.348	0.347	0.346	1.39
44.25	8.755	1.011	0.344	0.892	0.444	0.791	0.25	0.844	0.328	0.101	0.0695	0.232	0.171	0.351	0.35	0.349	0.348	1.398
44.333	8.788	1.015	0.345	0.897	0.446	0.795	0.252	0.847	0.329	0.101	0.0696	0.232	0.171	0.353	0.351	0.351	0.35	1.405
44.417	8.821	1.02	0.347	0.901	0.448	0.799	0.253	0.85	0.331	0.101	0.0697	0.233	0.171	0.354	0.353	0.353	0.351	1.411
44.5	8.853	1.025	0.348	0.906	0.45	0.803	0.254	0.853	0.332	0.101	0.0698	0.233	0.171	0.356	0.355	0.354	0.353	1.418
44.583	8.887	1.03	0.349	0.91	0.452	0.807	0.255	0.857	0.333	0.101	0.0699	0.234	0.171	0.358	0.357	0.356	0.355	1.426
44.667	8.92	1.035	0.35	0.915	0.454	0.811	0.256	0.86	0.335	0.101	0.0699	0.234	0.171	0.36	0.358	0.358	0.357	1.433
44.75	8.953	1.039	0.351	0.919	0.456	0.815	0.258	0.863	0.336	0.102	0.07	0.234	0.171	0.361	0.36	0.36	0.358	1.439
44.833	8.987	1.044	0.352	0.923	0.458	0.819	0.259	0.866	0.337	0.102	0.0701	0.234	0.171	0.363	0.362	0.361	0.36	1.446
44.917	9.02	1.049	0.352	0.928	0.46	0.824	0.26	0.869	0.339	0.102	0.0701	0.235	0.171	0.365	0.364	0.363	0.362	1.454
45	9.054	1.053	0.353	0.932	0.462	0.828	0.261	0.872	0.34	0.102	0.0702	0.235	0.171	0.366	0.365	0.365	0.363	1.459
45.083	9.088	1.058	0.354	0.936	0.464	0.832	0.262	0.875	0.341	0.102	0.0702	0.235	0.171	0.368	0.367	0.366	0.365	1.466
45.167	9.122	1.062	0.355	0.94	0.466	0.836	0.263	0.878	0.343	0.102	0.0702	0.235	0.171	0.37	0.369	0.368	0.367	1.474
45.25	9.156	1.067	0.356	0.944	0.468	0.84	0.264	0.881	0.344	0.102	0.0702	0.236	0.171	0.371	0.37	0.37	0.368	1.479
45.333	9.19	1.071	0.356	0.948	0.47	0.844	0.266	0.884	0.345	0.102	0.0703	0.236	0.172	0.373	0.372	0.371	0.37	1.486
45.417	9.225	1.075	0.357	0.953	0.471	0.848	0.267	0.887	0.346	0.103	0.0703	0.236	0.172	0.375	0.373	0.373	0.372	1.493
45.5	9.259	1.08	0.358	0.957	0.473	0.852	0.268	0.89	0.348	0.103	0.0704	0.236	0.172	0.376	0.375	0.375	0.373	1.499
45.583	9.294	1.084	0.359	0.961	0.475	0.856	0.269	0.893	0.349	0.103	0.0706	0.237	0.173	0.378	0.377	0.376	0.375	1.506
45.667	9.329	1.088	0.36	0.965	0.477	0.86	0.27	0.896	0.35	0.103	0.0707	0.237	0.173	0.379	0.378	0.378	0.376	1.511
45.75	9.364	1.092	0.36	0.969	0.479	0.864	0.271	0.899	0.352	0.103	0.0709	0.238	0.174	0.381	0.38	0.379	0.378	1.518
45.833	9.399	1.097	0.361	0.973	0.481	0.868	0.272	0.902	0.353	0.104	0.0713	0.239	0.175	0.383	0.381	0.381	0.38	1.525
45.917	9.434	1.101	0.362	0.977	0.482	0.872	0.273	0.904	0.354	0.104	0.0716	0.239	0.176	0.384	0.383	0.383	0.381	1.531
46	9.469	1.105	0.363	0.981	0.484	0.877	0.274	0.907	0.356	0.104	0.072	0.24	0.178	0.386	0.385	0.384	0.383	1.538
46.083	9.504	1.11	0.364	0.985	0.486	0.881	0.275	0.91	0.357	0.105	0.0725	0.241	0.179	0.387	0.386	0.386	0.384	1.543
46.167	9.54	1.114	0.365	0.989	0.488	0.885	0.276	0.913	0.358	0.105	0.073	0.243	0.181	0.389	0.388	0.387	0.386	1.55
46.25	9.576	1.118	0.366	0.993	0.49	0.889	0.278	0.916	0.36	0.105	0.0736	0.244	0.182	0.391	0.389	0.389	0.388	1.557
46.333	9.611	1.123	0.367	0.997	0.492	0.893	0.279	0.919	0.361	0.106	0.0741	0.245	0.184	0.392	0.391	0.39	0.389	1.562
46.417	9.647	1.127	0.368	1.001	0.494	0.898	0.28	0.922	0.362	0.106	0.0746	0.246	0.185	0.394	0.392	0.392	0.391	1.569
46.5	9.683	1.131	0.369	1.005	0.496	0.902	0.281	0.925	0.364	0.107	0.0752	0.248	0.186	0.395	0.394	0.394	0.392	1.575
46.583	9.72	1.136	0.37	1.009	0.497	0.906	0.282	0.928	0.365	0.108	0.0756	0.249	0.187	0.397	0.396	0.395	0.394	1.582
46.667	9.756	1.14	0.371	1.013	0.499	0.91	0.283	0.931	0.366	0.108	0.076	0.251	0.188	0.398	0.397	0.397	0.395	1.587
46.75	9.792	1.145	0.372	1.017	0.501	0.914	0.284	0.934	0.368	0.109	0.0765	0.252	0.189	0.4	0.399	0.398	0.397	1.594
46.833	9.829	1.149	0.374	1.021	0.503	0.918	0.285	0.937	0.369	0.109	0.0768	0.253	0.19	0.402	0.4	0.4	0.399	1.601

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
46.917	9.866	1.153	0.375	1.025	0.505	0.923	0.286	0.94	0.37	0.11	0.0772	0.255	0.191	0.403	0.402	0.401	0.4	1.606
47	9.902	1.158	0.376	1.029	0.507	0.927	0.287	0.943	0.372	0.11	0.0775	0.256	0.191	0.405	0.403	0.403	0.402	1.613
47.083	9.94	1.162	0.378	1.033	0.509	0.931	0.289	0.946	0.373	0.111	0.0777	0.257	0.192	0.406	0.405	0.405	0.403	1.619
47.167	9.977	1.167	0.379	1.037	0.511	0.935	0.29	0.949	0.374	0.111	0.078	0.258	0.192	0.408	0.407	0.406	0.405	1.626
47.25	10.014	1.171	0.38	1.041	0.512	0.939	0.291	0.952	0.375	0.112	0.0782	0.259	0.193	0.409	0.408	0.408	0.407	1.632
47.333	10.051	1.176	0.382	1.045	0.514	0.943	0.292	0.955	0.377	0.112	0.0784	0.26	0.193	0.411	0.41	0.409	0.408	1.638
47.417	10.089	1.18	0.384	1.049	0.516	0.947	0.293	0.958	0.378	0.113	0.0786	0.261	0.194	0.413	0.411	0.411	0.41	1.645
47.5	10.126	1.184	0.385	1.053	0.518	0.951	0.294	0.961	0.379	0.113	0.0788	0.261	0.194	0.414	0.413	0.413	0.411	1.651
47.583	10.164	1.189	0.387	1.057	0.52	0.955	0.295	0.964	0.381	0.113	0.079	0.262	0.194	0.416	0.415	0.414	0.413	1.658
47.667	10.202	1.193	0.388	1.061	0.522	0.959	0.296	0.967	0.382	0.114	0.0791	0.263	0.194	0.417	0.416	0.416	0.414	1.663
47.75	10.24	1.197	0.389	1.065	0.524	0.963	0.297	0.97	0.383	0.114	0.0793	0.263	0.194	0.419	0.418	0.417	0.416	1.67
47.833	10.279	1.202	0.391	1.069	0.525	0.967	0.298	0.973	0.384	0.114	0.0794	0.264	0.194	0.42	0.419	0.419	0.418	1.676
47.917	10.317	1.206	0.392	1.073	0.527	0.971	0.3	0.976	0.386	0.114	0.0795	0.264	0.195	0.422	0.421	0.42	0.419	1.682
48	10.355	1.21	0.394	1.077	0.529	0.975	0.301	0.979	0.387	0.115	0.0796	0.265	0.195	0.424	0.422	0.422	0.421	1.689
48.083	10.394	1.215	0.395	1.081	0.531	0.979	0.302	0.982	0.388	0.115	0.0796	0.265	0.195	0.425	0.424	0.424	0.422	1.695
48.167	10.433	1.219	0.396	1.085	0.533	0.983	0.303	0.985	0.389	0.115	0.0797	0.266	0.195	0.427	0.426	0.425	0.424	1.702
48.25	10.472	1.223	0.397	1.088	0.534	0.987	0.304	0.988	0.391	0.115	0.0797	0.266	0.195	0.428	0.427	0.427	0.425	1.707
48.333	10.511	1.227	0.398	1.092	0.536	0.991	0.305	0.992	0.392	0.116	0.0798	0.267	0.195	0.43	0.429	0.428	0.427	1.714
48.417	10.55	1.232	0.4	1.096	0.538	0.995	0.306	0.995	0.393	0.116	0.0799	0.267	0.195	0.431	0.43	0.43	0.429	1.72
48.5	10.59	1.236	0.401	1.1	0.54	0.999	0.307	0.998	0.395	0.116	0.08	0.268	0.196	0.433	0.432	0.431	0.43	1.726
48.583	10.629	1.24	0.402	1.104	0.542	1.003	0.308	1.002	0.396	0.117	0.0805	0.269	0.197	0.435	0.433	0.433	0.432	1.733
48.667	10.669	1.245	0.404	1.108	0.544	1.007	0.309	1.006	0.398	0.117	0.0809	0.27	0.198	0.436	0.435	0.435	0.433	1.739
48.75	10.709	1.249	0.405	1.112	0.546	1.011	0.31	1.009	0.399	0.117	0.0813	0.271	0.2	0.438	0.437	0.436	0.435	1.746
48.833	10.749	1.254	0.407	1.116	0.548	1.015	0.312	1.013	0.401	0.118	0.0821	0.273	0.203	0.439	0.438	0.438	0.437	1.752
48.917	10.789	1.258	0.408	1.121	0.55	1.019	0.313	1.017	0.402	0.119	0.083	0.275	0.206	0.441	0.44	0.439	0.438	1.758
49	10.829	1.263	0.41	1.125	0.552	1.023	0.314	1.021	0.404	0.12	0.0838	0.277	0.209	0.443	0.442	0.441	0.44	1.766
49.083	10.869	1.268	0.412	1.129	0.554	1.027	0.315	1.025	0.405	0.121	0.0851	0.279	0.213	0.444	0.443	0.443	0.442	1.772
49.167	10.91	1.273	0.414	1.134	0.556	1.032	0.316	1.03	0.407	0.122	0.0864	0.282	0.217	0.446	0.445	0.445	0.443	1.779
49.25	10.95	1.278	0.416	1.138	0.558	1.036	0.318	1.034	0.409	0.123	0.0876	0.285	0.221	0.448	0.447	0.446	0.445	1.786
49.333	10.991	1.283	0.418	1.143	0.561	1.04	0.319	1.038	0.41	0.124	0.089	0.288	0.224	0.45	0.449	0.448	0.447	1.794
49.417	11.032	1.289	0.421	1.147	0.563	1.045	0.32	1.043	0.412	0.125	0.0903	0.292	0.228	0.452	0.45	0.45	0.449	1.801
49.5	11.073	1.294	0.423	1.152	0.565	1.049	0.321	1.047	0.414	0.126	0.0917	0.295	0.231	0.453	0.452	0.452	0.451	1.808
49.583	11.115	1.299	0.426	1.157	0.568	1.054	0.323	1.052	0.416	0.128	0.0928	0.299	0.234	0.455	0.454	0.454	0.453	1.816
49.667	11.156	1.305	0.428	1.161	0.57	1.058	0.324	1.057	0.417	0.129	0.094	0.303	0.236	0.457	0.456	0.456	0.454	1.823
49.75	11.198	1.31	0.431	1.166	0.573	1.062	0.326	1.062	0.419	0.131	0.0951	0.306	0.239	0.459	0.458	0.458	0.456	1.831
49.833	11.24	1.316	0.434	1.171	0.575	1.067	0.327	1.067	0.421	0.132	0.096	0.309	0.241	0.461	0.46	0.459	0.458	1.838
49.917	11.281	1.322	0.437	1.176	0.578	1.071	0.328	1.072	0.423	0.133	0.0968	0.313	0.242	0.463	0.462	0.461	0.46	1.846
50	11.323	1.328	0.44	1.181	0.58	1.076	0.33	1.077	0.425	0.135	0.0977	0.316	0.244	0.465	0.464	0.463	0.462	1.854
50.083	11.366	1.334	0.443	1.187	0.583	1.08	0.331	1.082	0.427	0.136	0.0983	0.318	0.245	0.467	0.466	0.465	0.464	1.862
50.167	11.408	1.34	0.447	1.192	0.586	1.085	0.333	1.088	0.429	0.137	0.099	0.321	0.247	0.469	0.468	0.468	0.466	1.871
50.25	11.45	1.346	0.45	1.197	0.588	1.09	0.334	1.093	0.431	0.138	0.0996	0.324	0.248	0.471	0.47	0.47	0.468	1.879
50.333	11.493	1.352	0.454	1.202	0.591	1.094	0.336	1.099	0.433	0.139	0.1	0.326	0.249	0.473	0.472	0.472	0.471	1.888
50.417	11.536	1.358	0.458	1.208	0.594	1.099	0.338	1.104	0.435	0.14	0.101	0.328	0.25	0.475	0.474	0.474	0.473	1.896
50.5	11.579	1.364	0.461	1.213	0.596	1.103	0.339	1.11	0.436	0.141	0.101	0.33	0.251	0.478	0.476	0.476	0.475	1.905
50.583	11.622	1.371	0.465	1.219	0.599	1.108	0.341	1.116	0.439	0.142	0.101	0.332	0.251	0.48	0.479	0.478	0.477	1.914
50.667	11.665	1.377	0.469	1.224	0.602	1.113	0.342	1.122	0.441	0.143	0.102	0.333	0.252	0.482	0.481	0.48	0.479	1.922
50.75	11.708	1.383	0.472	1.23	0.605	1.118	0.344	1.128	0.443	0.144	0.102	0.335	0.252	0.484	0.483	0.483	0.482	1.932
50.833	11.752	1.39	0.476	1.236	0.608	1.122	0.345	1.134	0.445	0.144	0.102	0.336	0.252	0.486	0.485	0.485	0.484	1.94
50.917	11.796	1.396	0.479	1.241	0.61	1.127	0.347	1.141	0.447	0.145	0.103	0.338	0.252	0.489	0.488	0.487	0.486	1.95
51	11.84	1.402	0.482	1.247	0.613	1.132	0.349	1.147	0.449	0.146	0.103	0.339	0.252	0.491	0.49	0.489	0.488	1.958
51.083	11.884	1.409	0.485	1.252	0.616	1.137	0.35	1.154	0.451	0.146	0.103	0.34	0.252	0.493	0.492	0.492	0.491	1.968
51.167	11.928	1.415	0.489	1.258	0.619	1.141	0.352	1.16	0.453	0.147	0.103	0.341	0.252	0.495	0.494	0.494	0.493	1.976
51.25	11.972	1.422	0.492	1.264	0.622	1.146	0.354	1.167	0.456	0.147	0.103	0.342	0.252	0.498	0.497	0.496	0.495	1.986
51.333	12.017	1.429	0.494	1.27	0.625	1.151	0.355	1.174	0.458	0.148	0.103	0.343	0.252	0.5	0.499	0.498	0.497	1.994
51.417	12.061	1.435	0.497	1.275	0.628	1.156	0.357	1.181	0.46	0.148	0.104	0.344	0.252	0.502	0.501	0.501	0.5	2.004
51.5	12.106	1.442	0.5	1.281	0.63	1.161	0.358	1.188	0.462	0.149	0.104	0.345	0.252	0.505	0.503	0.503	0.502	2.013
51.583	12.151	1.448	0.502	1.287	0.633	1.166	0.36	1.195	0.465	0.149	0.104	0.346	0.252	0.507	0.506	0.505	0.504	2.022
51.667	12.196	1.455	0.505	1.293	0.636	1.171	0.362	1.202	0.467	0.15	0.104	0.346	0.252	0.509	0.508	0.508	0.507	2.032
51.75	12.242	1.462	0.507	1.299	0.639	1.176	0.363	1.209	0.47	0.15	0.104	0.347	0.252	0.512	0.51	0.51	0.509	2.041
51.833	12.287	1.469	0.509	1.305	0.643	1.181	0.365	1.215	0.472	0.15	0.104	0.347	0.252	0.514	0.513	0.512	0.511	2.05
51.917	12.333	1.476	0.511	1.311	0.646	1.186	0.367	1.222	0.474	0.151	0.104	0.348	0.252	0.516	0.515	0.515	0.514	2.06
52	12.378	1.482	0.514	1.317	0.649	1.191	0.368	1.229	0.477	0.151	0.104	0.348	0.252	0.519	0.518	0.517	0.516	2.07
52.083	12.425	1.489	0.515	1.323	0.652	1.196	0.37	1.235	0.479	0.151	0.104	0.348	0.252	0.521	0.52	0.52	0.518	2.079

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
52.167	12.471	1.496	0.517	1.329	0.655	1.201	0.372	1.241	0.482	0.151	0.104	0.349	0.252	0.523	0.522	0.522	0.521	2.088
52.25	12.517	1.503	0.519	1.335	0.658	1.206	0.374	1.248	0.484	0.152	0.104	0.349	0.252	0.526	0.525	0.524	0.523	2.098
52.333	12.563	1.51	0.521	1.341	0.661	1.212	0.375	1.254	0.487	0.152	0.104	0.349	0.252	0.528	0.527	0.527	0.526	2.108
52.417	12.61	1.518	0.522	1.347	0.664	1.217	0.377	1.26	0.489	0.152	0.104	0.349	0.252	0.531	0.53	0.529	0.528	2.118
52.5	12.657	1.525	0.524	1.353	0.668	1.222	0.379	1.266	0.492	0.152	0.104	0.349	0.252	0.533	0.532	0.532	0.531	2.128
52.583	12.704	1.532	0.525	1.359	0.671	1.227	0.381	1.271	0.494	0.152	0.104	0.349	0.252	0.536	0.534	0.534	0.533	2.137
52.667	12.751	1.539	0.527	1.366	0.674	1.232	0.382	1.277	0.497	0.152	0.104	0.349	0.252	0.538	0.537	0.536	0.536	2.147
52.75	12.798	1.546	0.528	1.372	0.678	1.238	0.384	1.283	0.499	0.152	0.104	0.349	0.252	0.54	0.539	0.539	0.538	2.156
52.833	12.846	1.554	0.529	1.378	0.681	1.243	0.386	1.288	0.501	0.152	0.104	0.349	0.252	0.543	0.542	0.541	0.54	2.166
52.917	12.893	1.561	0.531	1.384	0.684	1.248	0.388	1.293	0.504	0.152	0.104	0.349	0.252	0.545	0.544	0.544	0.543	2.176
53	12.941	1.568	0.532	1.391	0.687	1.253	0.389	1.298	0.506	0.152	0.104	0.349	0.252	0.548	0.547	0.546	0.545	2.186
53.083	12.989	1.576	0.533	1.397	0.69	1.258	0.391	1.303	0.508	0.152	0.104	0.349	0.252	0.55	0.549	0.549	0.548	2.196
53.167	13.037	1.583	0.534	1.403	0.694	1.264	0.393	1.308	0.51	0.152	0.104	0.349	0.252	0.553	0.552	0.552	0.551	2.208
53.25	13.085	1.59	0.535	1.41	0.697	1.269	0.395	1.313	0.512	0.152	0.104	0.349	0.252	0.555	0.554	0.554	0.553	2.216
53.333	13.134	1.598	0.536	1.416	0.7	1.274	0.397	1.318	0.514	0.152	0.104	0.349	0.252	0.558	0.557	0.557	0.556	2.228
53.417	13.183	1.605	0.537	1.423	0.703	1.279	0.399	1.322	0.516	0.152	0.104	0.349	0.252	0.561	0.56	0.559	0.558	2.238
53.5	13.231	1.612	0.538	1.429	0.706	1.284	0.4	1.327	0.518	0.152	0.104	0.349	0.252	0.563	0.562	0.562	0.561	2.248
53.583	13.28	1.619	0.539	1.436	0.709	1.29	0.402	1.331	0.52	0.152	0.104	0.349	0.252	0.566	0.565	0.564	0.563	2.258
53.667	13.33	1.625	0.54	1.442	0.712	1.295	0.404	1.335	0.522	0.152	0.104	0.349	0.252	0.568	0.567	0.567	0.566	2.268
53.75	13.379	1.632	0.541	1.449	0.714	1.3	0.406	1.34	0.524	0.152	0.104	0.349	0.252	0.571	0.57	0.569	0.568	2.278
53.833	13.428	1.639	0.542	1.455	0.717	1.305	0.407	1.344	0.526	0.152	0.104	0.349	0.252	0.573	0.572	0.572	0.571	2.288
53.917	13.478	1.645	0.543	1.461	0.72	1.31	0.409	1.347	0.528	0.152	0.104	0.349	0.252	0.576	0.575	0.574	0.573	2.298
54	13.528	1.652	0.544	1.467	0.723	1.315	0.41	1.351	0.53	0.152	0.104	0.349	0.252	0.578	0.577	0.577	0.576	2.308
54.083	13.578	1.658	0.544	1.473	0.725	1.321	0.412	1.355	0.532	0.152	0.104	0.349	0.252	0.58	0.579	0.579	0.578	2.316
54.167	13.628	1.664	0.545	1.479	0.728	1.326	0.414	1.358	0.533	0.152	0.104	0.349	0.252	0.583	0.582	0.581	0.58	2.326
54.25	13.678	1.671	0.546	1.485	0.73	1.331	0.415	1.362	0.535	0.152	0.104	0.349	0.252	0.585	0.584	0.584	0.583	2.336
54.333	13.729	1.677	0.546	1.491	0.733	1.336	0.417	1.365	0.537	0.152	0.104	0.349	0.252	0.587	0.586	0.586	0.585	2.344
54.417	13.78	1.683	0.547	1.496	0.735	1.341	0.418	1.369	0.538	0.152	0.104	0.349	0.253	0.59	0.588	0.588	0.587	2.353
54.5	13.831	1.689	0.547	1.502	0.738	1.347	0.42	1.372	0.54	0.152	0.104	0.349	0.253	0.592	0.591	0.59	0.589	2.362
54.583	13.882	1.694	0.548	1.507	0.74	1.352	0.421	1.375	0.542	0.152	0.104	0.349	0.253	0.594	0.593	0.593	0.592	2.372
54.667	13.933	1.7	0.549	1.513	0.743	1.357	0.423	1.378	0.543	0.152	0.104	0.35	0.254	0.596	0.595	0.595	0.594	2.38
54.75	13.984	1.706	0.549	1.518	0.745	1.363	0.424	1.381	0.545	0.153	0.104	0.35	0.254	0.598	0.597	0.597	0.596	2.388
54.833	14.036	1.712	0.55	1.524	0.747	1.368	0.426	1.384	0.546	0.153	0.104	0.35	0.255	0.6	0.599	0.599	0.598	2.396
54.917	14.088	1.717	0.55	1.529	0.75	1.373	0.427	1.387	0.548	0.153	0.105	0.351	0.256	0.603	0.601	0.601	0.6	2.405
55	14.14	1.723	0.551	1.535	0.752	1.379	0.428	1.39	0.55	0.153	0.105	0.352	0.257	0.605	0.604	0.603	0.602	2.414
55.083	14.192	1.728	0.552	1.54	0.754	1.384	0.43	1.393	0.551	0.154	0.105	0.353	0.259	0.607	0.606	0.605	0.604	2.422
55.167	14.244	1.734	0.552	1.545	0.757	1.39	0.431	1.396	0.553	0.154	0.106	0.354	0.26	0.609	0.608	0.607	0.607	2.431
55.25	14.297	1.739	0.553	1.55	0.759	1.395	0.433	1.399	0.554	0.154	0.106	0.355	0.262	0.611	0.61	0.609	0.609	2.439
55.333	14.35	1.745	0.554	1.555	0.761	1.401	0.434	1.402	0.556	0.155	0.107	0.356	0.264	0.613	0.612	0.611	0.611	2.447
55.417	14.403	1.75	0.555	1.561	0.763	1.407	0.435	1.405	0.557	0.155	0.107	0.357	0.265	0.615	0.614	0.613	0.613	2.455
55.5	14.455	1.756	0.556	1.566	0.765	1.412	0.437	1.409	0.559	0.156	0.108	0.359	0.266	0.617	0.616	0.616	0.615	2.464
55.583	14.509	1.761	0.556	1.571	0.768	1.418	0.438	1.412	0.56	0.156	0.109	0.36	0.267	0.619	0.618	0.617	0.617	2.471
55.667	14.562	1.766	0.557	1.576	0.77	1.423	0.439	1.415	0.562	0.157	0.109	0.362	0.269	0.621	0.62	0.619	0.619	2.479
55.75	14.616	1.771	0.558	1.581	0.772	1.429	0.441	1.418	0.563	0.157	0.109	0.363	0.27	0.623	0.622	0.621	0.621	2.487
55.833	14.67	1.776	0.559	1.586	0.774	1.434	0.442	1.421	0.564	0.158	0.11	0.364	0.27	0.625	0.624	0.623	0.623	2.495
55.917	14.724	1.782	0.56	1.59	0.776	1.439	0.443	1.424	0.566	0.158	0.11	0.366	0.271	0.627	0.626	0.625	0.624	2.502
56	14.778	1.787	0.561	1.595	0.778	1.445	0.445	1.427	0.567	0.159	0.111	0.367	0.272	0.629	0.628	0.627	0.626	2.51
56.083	14.832	1.792	0.562	1.6	0.78	1.45	0.446	1.43	0.568	0.159	0.111	0.368	0.272	0.63	0.629	0.629	0.628	2.516
56.167	14.887	1.797	0.563	1.605	0.782	1.455	0.447	1.433	0.57	0.16	0.111	0.369	0.273	0.632	0.631	0.631	0.63	2.524
56.25	14.941	1.802	0.565	1.61	0.785	1.461	0.448	1.436	0.571	0.16	0.111	0.37	0.274	0.634	0.633	0.633	0.632	2.532
56.333	14.996	1.807	0.566	1.614	0.787	1.466	0.45	1.44	0.573	0.161	0.112	0.371	0.274	0.636	0.635	0.635	0.634	2.54
56.417	15.051	1.811	0.567	1.619	0.789	1.471	0.451	1.443	0.574	0.161	0.112	0.372	0.274	0.638	0.637	0.637	0.636	2.548
56.5	15.107	1.816	0.568	1.624	0.791	1.476	0.452	1.446	0.575	0.162	0.112	0.373	0.275	0.64	0.639	0.638	0.638	2.555
56.583	15.162	1.821	0.57	1.628	0.793	1.481	0.453	1.449	0.577	0.162	0.112	0.374	0.275	0.642	0.641	0.64	0.639	2.562
56.667	15.218	1.826	0.571	1.633	0.795	1.486	0.455	1.452	0.578	0.162	0.112	0.374	0.275	0.643	0.642	0.642	0.641	2.568
56.75	15.274	1.831	0.572	1.638	0.797	1.491	0.456	1.455	0.579	0.163	0.112	0.375	0.275	0.645	0.644	0.644	0.643	2.576
56.833	15.33	1.835	0.574	1.642	0.799	1.496	0.457	1.459	0.581	0.163	0.113	0.375	0.275	0.647	0.646	0.646	0.645	2.584
56.917	15.386	1.84	0.575	1.647	0.8	1.501	0.458	1.462	0.582	0.163	0.113	0.376	0.275	0.649	0.648	0.647	0.647	2.591
57	15.442	1.845	0.576	1.651	0.802	1.506	0.459	1.465	0.583	0.164	0.113	0.377	0.276	0.65	0.649	0.649	0.648	2.596
57.083	15.499	1.85	0.577	1.656	0.804	1.511	0.461	1.468	0.585	0.164	0.113	0.377	0.276	0.652	0.651	0.651	0.65	2.604
57.167	15.556	1.854	0.578	1.66	0.806	1.515	0.462	1.472	0.586	0.164	0.113	0.378	0.276	0.654	0.653	0.653	0.652	2.612
57.25	15.613	1.859	0.58	1.664	0.808	1.52	0.463	1.475	0.587	0.164	0.113	0.378	0.276	0.656	0.655	0.654	0.654	2.619
57.333	15.67	1.863	0.581	1.669	0.81	1.525	0.464	1.478	0.589	0.164	0.113	0.378	0.276	0.657	0.656	0.656	0.655	2.624

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
57.417	15.727	1.868	0.582	1.673	0.812	1.53	0.465	1.482	0.59	0.165	0.113	0.379	0.276	0.659	0.658	0.658	0.657	2.632
57.5	15.785	1.872	0.583	1.677	0.814	1.534	0.466	1.485	0.591	0.165	0.113	0.379	0.276	0.661	0.66	0.659	0.659	2.639
57.583	15.843	1.877	0.584	1.681	0.816	1.539	0.467	1.489	0.593	0.165	0.113	0.38	0.276	0.662	0.661	0.661	0.66	2.644
57.667	15.901	1.881	0.585	1.686	0.818	1.544	0.469	1.492	0.594	0.165	0.113	0.38	0.276	0.664	0.663	0.663	0.662	2.652
57.75	15.959	1.886	0.586	1.69	0.82	1.548	0.47	1.495	0.596	0.166	0.113	0.381	0.277	0.666	0.665	0.664	0.664	2.659
57.833	16.017	1.89	0.587	1.694	0.822	1.553	0.471	1.499	0.597	0.166	0.114	0.381	0.278	0.668	0.667	0.666	0.665	2.666
57.917	16.076	1.895	0.588	1.699	0.824	1.558	0.472	1.502	0.598	0.166	0.114	0.382	0.279	0.669	0.668	0.668	0.667	2.672
58	16.134	1.899	0.589	1.703	0.826	1.562	0.473	1.506	0.6	0.167	0.114	0.383	0.28	0.671	0.67	0.67	0.669	2.68
58.083	16.193	1.904	0.59	1.707	0.828	1.567	0.474	1.509	0.601	0.167	0.115	0.384	0.282	0.673	0.672	0.671	0.671	2.687
58.167	16.252	1.909	0.591	1.711	0.83	1.572	0.475	1.513	0.603	0.167	0.115	0.385	0.283	0.674	0.673	0.673	0.672	2.692
58.25	16.311	1.913	0.593	1.716	0.832	1.576	0.477	1.516	0.604	0.168	0.116	0.386	0.285	0.676	0.675	0.675	0.674	2.7
58.333	16.371	1.918	0.594	1.72	0.834	1.581	0.478	1.519	0.606	0.168	0.116	0.387	0.286	0.678	0.677	0.676	0.676	2.707
58.417	16.431	1.923	0.595	1.724	0.836	1.585	0.479	1.523	0.608	0.169	0.117	0.389	0.288	0.679	0.678	0.678	0.677	2.712
58.5	16.491	1.928	0.596	1.729	0.838	1.59	0.48	1.526	0.609	0.169	0.117	0.39	0.289	0.681	0.68	0.68	0.679	2.72
58.583	16.551	1.933	0.598	1.733	0.84	1.594	0.481	1.529	0.611	0.17	0.118	0.392	0.29	0.683	0.682	0.681	0.681	2.727
58.667	16.611	1.937	0.599	1.737	0.842	1.599	0.483	1.533	0.612	0.171	0.118	0.393	0.291	0.685	0.684	0.683	0.682	2.734
58.75	16.671	1.942	0.6	1.741	0.844	1.603	0.484	1.536	0.614	0.171	0.119	0.395	0.293	0.686	0.685	0.685	0.684	2.74
58.833	16.732	1.947	0.602	1.746	0.846	1.608	0.485	1.539	0.615	0.172	0.119	0.396	0.293	0.688	0.687	0.687	0.686	2.748
58.917	16.793	1.952	0.603	1.75	0.849	1.612	0.486	1.543	0.617	0.172	0.12	0.397	0.294	0.69	0.689	0.688	0.688	2.755
59	16.854	1.957	0.605	1.755	0.851	1.617	0.488	1.546	0.618	0.173	0.12	0.399	0.295	0.691	0.69	0.69	0.689	2.76
59.083	16.916	1.962	0.606	1.759	0.853	1.621	0.489	1.549	0.62	0.173	0.12	0.4	0.295	0.693	0.692	0.692	0.691	2.768
59.167	16.977	1.967	0.608	1.764	0.855	1.626	0.49	1.552	0.621	0.174	0.121	0.401	0.296	0.695	0.694	0.694	0.693	2.776
59.25	17.039	1.973	0.61	1.768	0.857	1.63	0.491	1.555	0.623	0.174	0.121	0.402	0.297	0.697	0.696	0.695	0.695	2.783
59.333	17.101	1.978	0.611	1.773	0.859	1.635	0.493	1.559	0.624	0.175	0.121	0.403	0.297	0.699	0.698	0.697	0.697	2.791
59.417	17.163	1.983	0.613	1.777	0.862	1.639	0.494	1.562	0.626	0.175	0.121	0.404	0.297	0.7	0.699	0.699	0.698	2.796
59.5	17.225	1.988	0.615	1.782	0.864	1.644	0.495	1.565	0.627	0.176	0.121	0.405	0.298	0.702	0.701	0.701	0.7	2.804
59.583	17.287	1.993	0.617	1.786	0.866	1.648	0.496	1.568	0.628	0.176	0.122	0.405	0.298	0.704	0.703	0.703	0.702	2.812
59.667	17.35	1.998	0.618	1.791	0.868	1.653	0.498	1.571	0.63	0.176	0.122	0.406	0.298	0.706	0.705	0.704	0.704	2.819
59.75	17.412	2.003	0.62	1.796	0.87	1.657	0.499	1.574	0.631	0.177	0.122	0.407	0.298	0.708	0.707	0.706	0.706	2.827
59.833	17.476	2.008	0.622	1.8	0.872	1.661	0.5	1.578	0.633	0.177	0.122	0.407	0.299	0.709	0.708	0.708	0.707	2.832
59.917	17.539	2.013	0.623	1.805	0.874	1.666	0.501	1.581	0.634	0.177	0.122	0.408	0.299	0.711	0.71	0.71	0.709	2.84
60	17.602	2.017	0.625	1.809	0.876	1.67	0.503	1.584	0.636	0.177	0.122	0.408	0.299	0.713	0.712	0.712	0.711	2.848
60.083	17.666	2.022	0.626	1.814	0.878	1.674	0.504	1.587	0.637	0.178	0.122	0.409	0.299	0.715	0.714	0.714	0.713	2.856
60.167	17.729	2.027	0.628	1.818	0.88	1.679	0.505	1.59	0.638	0.178	0.122	0.409	0.299	0.717	0.716	0.715	0.715	2.863
60.25	17.793	2.032	0.629	1.823	0.882	1.683	0.506	1.594	0.64	0.178	0.123	0.41	0.299	0.718	0.717	0.717	0.716	2.868
60.333	17.857	2.037	0.63	1.827	0.884	1.687	0.508	1.597	0.641	0.178	0.123	0.41	0.299	0.72	0.719	0.719	0.718	2.876
60.417	17.922	2.042	0.632	1.832	0.886	1.692	0.509	1.6	0.643	0.179	0.123	0.411	0.299	0.722	0.721	0.721	0.72	2.884
60.5	17.986	2.047	0.633	1.836	0.888	1.696	0.51	1.604	0.644	0.179	0.123	0.411	0.299	0.724	0.723	0.722	0.722	2.891
60.583	18.051	2.051	0.634	1.841	0.89	1.7	0.511	1.607	0.645	0.179	0.123	0.411	0.299	0.725	0.724	0.724	0.723	2.896
60.667	18.115	2.056	0.635	1.845	0.892	1.705	0.512	1.61	0.647	0.179	0.123	0.412	0.299	0.727	0.726	0.726	0.725	2.904
60.75	18.18	2.061	0.636	1.849	0.894	1.709	0.514	1.614	0.648	0.179	0.123	0.412	0.299	0.729	0.728	0.728	0.727	2.912
60.833	18.245	2.066	0.637	1.854	0.896	1.713	0.515	1.617	0.65	0.179	0.123	0.412	0.299	0.731	0.73	0.729	0.729	2.919
60.917	18.31	2.07	0.638	1.858	0.898	1.718	0.516	1.62	0.651	0.18	0.123	0.412	0.299	0.732	0.731	0.731	0.73	2.924
61	18.375	2.075	0.639	1.862	0.9	1.722	0.517	1.623	0.652	0.18	0.123	0.413	0.299	0.734	0.733	0.733	0.732	2.932
61.083	18.441	2.08	0.64	1.867	0.902	1.726	0.518	1.627	0.654	0.18	0.123	0.413	0.299	0.736	0.735	0.734	0.734	2.939
61.167	18.507	2.084	0.641	1.871	0.904	1.73	0.52	1.63	0.655	0.18	0.123	0.413	0.299	0.737	0.736	0.736	0.736	2.945
61.25	18.572	2.089	0.642	1.875	0.906	1.735	0.521	1.633	0.656	0.18	0.123	0.413	0.299	0.739	0.738	0.738	0.737	2.952
61.333	18.638	2.093	0.642	1.879	0.908	1.739	0.522	1.636	0.658	0.18	0.123	0.413	0.299	0.741	0.74	0.74	0.739	2.96
61.417	18.704	2.098	0.643	1.884	0.91	1.743	0.523	1.638	0.659	0.18	0.123	0.413	0.299	0.742	0.742	0.741	0.741	2.966
61.5	18.771	2.103	0.644	1.888	0.912	1.747	0.524	1.641	0.66	0.18	0.123	0.413	0.299	0.744	0.743	0.743	0.742	2.972
61.583	18.837	2.107	0.644	1.892	0.914	1.752	0.525	1.644	0.662	0.18	0.123	0.413	0.299	0.746	0.745	0.745	0.744	2.98
61.667	18.904	2.112	0.645	1.896	0.916	1.756	0.526	1.647	0.663	0.18	0.123	0.413	0.299	0.747	0.747	0.746	0.746	2.986
61.75	18.97	2.116	0.646	1.901	0.918	1.76	0.528	1.65	0.664	0.18	0.123	0.413	0.299	0.749	0.748	0.748	0.747	2.992
61.833	19.037	2.121	0.646	1.905	0.92	1.764	0.529	1.652	0.665	0.18	0.123	0.413	0.299	0.751	0.75	0.75	0.749	3
61.917	19.104	2.125	0.647	1.909	0.922	1.768	0.53	1.655	0.666	0.18	0.123	0.413	0.299	0.752	0.751	0.751	0.751	3.005
62	19.17	2.129	0.647	1.913	0.923	1.772	0.531	1.657	0.668	0.18	0.123	0.413	0.299	0.754	0.753	0.753	0.752	3.012
62.083	19.237	2.134	0.648	1.917	0.925	1.776	0.532	1.66	0.669	0.18	0.123	0.413	0.299	0.756	0.755	0.754	0.754	3.019
62.167	19.305	2.138	0.648	1.921	0.927	1.78	0.533	1.662	0.67	0.18	0.123	0.413	0.299	0.757	0.756	0.756	0.756	3.025
62.25	19.372	2.143	0.648	1.925	0.929	1.784	0.534	1.665	0.671	0.18	0.123	0.413	0.299	0.759	0.758	0.758	0.757	3.032
62.333	19.439	2.147	0.649	1.93	0.931	1.788	0.535	1.667	0.672	0.18	0.123	0.413	0.299	0.761	0.76	0.759	0.759	3.039
62.417	19.506	2.151	0.649	1.934	0.932	1.792	0.536	1.669	0.673	0.18	0.123	0.413	0.299	0.762	0.761	0.761	0.76	3.044
62.5	19.574	2.155	0.65	1.938	0.934	1.796	0.537	1.671	0.674	0.18	0.123	0.413	0.299	0.764	0.763	0.763	0.762	3.052
62.583	19.641	2.159	0.65	1.942	0.935	1.799	0.539	1.673	0.675	0.18	0.123	0.413	0.299	0.765	0.764	0.764	0.764	3.057

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
62.667	19.709	2.163	0.651	1.946	0.937	1.803	0.54	1.676	0.676	0.18	0.123	0.413	0.299	0.767	0.766	0.766	0.765	3.064
62.75	19.777	2.167	0.651	1.95	0.939	1.807	0.541	1.678	0.677	0.18	0.123	0.413	0.299	0.768	0.768	0.767	0.767	3.07
62.833	19.844	2.171	0.651	1.954	0.94	1.811	0.542	1.68	0.677	0.18	0.123	0.413	0.299	0.77	0.769	0.769	0.768	3.076
62.917	19.912	2.175	0.652	1.957	0.942	1.814	0.543	1.682	0.678	0.18	0.123	0.413	0.299	0.771	0.771	0.77	0.77	3.082
63	19.98	2.179	0.652	1.961	0.943	1.818	0.544	1.683	0.679	0.18	0.123	0.413	0.299	0.773	0.772	0.772	0.771	3.088
63.083	20.048	2.182	0.652	1.965	0.944	1.821	0.544	1.685	0.68	0.18	0.123	0.413	0.299	0.774	0.774	0.773	0.773	3.094
63.167	20.116	2.186	0.652	1.968	0.946	1.825	0.545	1.687	0.681	0.18	0.123	0.413	0.299	0.776	0.775	0.775	0.774	3.1
63.25	20.184	2.189	0.653	1.972	0.947	1.829	0.546	1.689	0.682	0.18	0.123	0.413	0.299	0.777	0.776	0.776	0.776	3.105
63.333	20.252	2.193	0.653	1.976	0.948	1.832	0.547	1.69	0.683	0.18	0.123	0.413	0.299	0.779	0.778	0.777	0.777	3.111
63.417	20.32	2.196	0.653	1.979	0.95	1.836	0.548	1.692	0.683	0.18	0.123	0.413	0.299	0.78	0.779	0.779	0.778	3.116
63.5	20.388	2.2	0.654	1.983	0.951	1.839	0.549	1.694	0.684	0.18	0.123	0.413	0.299	0.781	0.78	0.78	0.78	3.121
63.583	20.456	2.203	0.654	1.986	0.952	1.842	0.55	1.695	0.685	0.18	0.123	0.413	0.298	0.783	0.782	0.781	0.781	3.127
63.667	20.524	2.206	0.654	1.989	0.953	1.846	0.55	1.696	0.686	0.18	0.122	0.413	0.298	0.784	0.783	0.783	0.782	3.132
63.75	20.592	2.209	0.654	1.992	0.954	1.849	0.551	1.698	0.686	0.18	0.122	0.412	0.298	0.785	0.784	0.784	0.783	3.136
63.833	20.66	2.212	0.654	1.995	0.955	1.852	0.552	1.699	0.687	0.18	0.122	0.412	0.297	0.786	0.785	0.785	0.785	3.141
63.917	20.728	2.214	0.654	1.998	0.957	1.856	0.553	1.7	0.688	0.18	0.122	0.411	0.296	0.788	0.787	0.786	0.786	3.147
64	20.796	2.217	0.654	2.001	0.958	1.859	0.554	1.701	0.688	0.18	0.122	0.411	0.295	0.789	0.788	0.788	0.787	3.152
64.083	20.864	2.22	0.653	2.004	0.958	1.862	0.554	1.702	0.689	0.179	0.121	0.41	0.294	0.79	0.789	0.789	0.788	3.156
64.167	20.932	2.222	0.653	2.007	0.959	1.865	0.555	1.702	0.69	0.179	0.121	0.409	0.292	0.791	0.79	0.79	0.789	3.16
64.25	21	2.225	0.653	2.009	0.96	1.868	0.555	1.703	0.69	0.179	0.12	0.408	0.29	0.792	0.791	0.791	0.79	3.164
64.333	21.068	2.227	0.652	2.012	0.961	1.871	0.556	1.704	0.691	0.178	0.12	0.407	0.289	0.793	0.792	0.792	0.791	3.168
64.417	21.136	2.229	0.652	2.014	0.962	1.874	0.557	1.704	0.691	0.178	0.119	0.406	0.287	0.794	0.793	0.793	0.792	3.172
64.5	21.204	2.231	0.651	2.017	0.963	1.877	0.557	1.705	0.692	0.177	0.119	0.405	0.286	0.795	0.794	0.794	0.793	3.176
64.583	21.271	2.233	0.65	2.019	0.963	1.88	0.558	1.705	0.692	0.177	0.118	0.403	0.285	0.796	0.795	0.795	0.794	3.18
64.667	21.339	2.235	0.65	2.021	0.964	1.883	0.558	1.705	0.692	0.176	0.118	0.402	0.283	0.797	0.796	0.795	0.795	3.183
64.75	21.407	2.237	0.649	2.024	0.965	1.886	0.559	1.705	0.693	0.176	0.117	0.4	0.282	0.797	0.797	0.796	0.796	3.186
64.833	21.474	2.239	0.648	2.026	0.965	1.888	0.559	1.705	0.693	0.175	0.117	0.399	0.281	0.798	0.797	0.797	0.797	3.189
64.917	21.542	2.24	0.647	2.028	0.966	1.891	0.56	1.705	0.693	0.175	0.116	0.397	0.281	0.799	0.798	0.798	0.797	3.192
65	21.609	2.242	0.646	2.03	0.966	1.894	0.56	1.705	0.694	0.174	0.116	0.396	0.28	0.8	0.799	0.799	0.798	3.196
65.083	21.677	2.243	0.645	2.031	0.967	1.896	0.56	1.705	0.694	0.174	0.116	0.395	0.279	0.801	0.8	0.799	0.799	3.199
65.167	21.744	2.245	0.644	2.033	0.967	1.898	0.561	1.704	0.694	0.173	0.115	0.394	0.279	0.801	0.8	0.8	0.8	3.201
65.25	21.812	2.246	0.643	2.035	0.968	1.901	0.561	1.704	0.694	0.173	0.115	0.392	0.278	0.802	0.801	0.801	0.8	3.204
65.333	21.879	2.247	0.642	2.036	0.968	1.903	0.561	1.703	0.694	0.172	0.115	0.392	0.278	0.803	0.802	0.801	0.801	3.207
65.417	21.946	2.248	0.64	2.038	0.969	1.905	0.562	1.702	0.694	0.172	0.115	0.391	0.277	0.803	0.802	0.802	0.801	3.208
65.5	22.013	2.249	0.639	2.04	0.969	1.907	0.562	1.702	0.694	0.171	0.114	0.39	0.277	0.804	0.803	0.803	0.802	3.212
65.583	22.079	2.25	0.638	2.041	0.969	1.909	0.562	1.701	0.694	0.171	0.114	0.389	0.276	0.804	0.803	0.803	0.803	3.213
65.667	22.146	2.251	0.636	2.042	0.97	1.911	0.562	1.7	0.695	0.171	0.114	0.388	0.276	0.805	0.804	0.804	0.803	3.216
65.75	22.213	2.252	0.635	2.044	0.97	1.913	0.563	1.699	0.695	0.17	0.114	0.387	0.276	0.805	0.804	0.804	0.804	3.217
65.833	22.279	2.253	0.634	2.045	0.97	1.915	0.563	1.698	0.694	0.17	0.114	0.387	0.276	0.806	0.805	0.805	0.804	3.22
65.917	22.345	2.253	0.632	2.046	0.97	1.917	0.563	1.696	0.694	0.17	0.114	0.386	0.276	0.806	0.805	0.805	0.804	3.22
66	22.411	2.254	0.631	2.047	0.97	1.919	0.563	1.695	0.694	0.169	0.113	0.386	0.276	0.807	0.806	0.805	0.805	3.223
66.083	22.477	2.255	0.63	2.048	0.97	1.92	0.563	1.694	0.694	0.169	0.113	0.385	0.276	0.807	0.806	0.806	0.805	3.224
66.167	22.543	2.255	0.629	2.049	0.97	1.922	0.564	1.692	0.694	0.169	0.113	0.385	0.276	0.807	0.806	0.806	0.806	3.225
66.25	22.609	2.256	0.628	2.05	0.97	1.923	0.564	1.691	0.694	0.169	0.113	0.384	0.276	0.808	0.807	0.806	0.806	3.227
66.333	22.674	2.256	0.627	2.05	0.97	1.925	0.564	1.689	0.694	0.168	0.113	0.384	0.276	0.808	0.807	0.807	0.806	3.228
66.417	22.74	2.256	0.626	2.051	0.97	1.926	0.564	1.687	0.694	0.168	0.113	0.383	0.276	0.808	0.807	0.807	0.806	3.228
66.5	22.805	2.256	0.625	2.052	0.97	1.928	0.564	1.686	0.693	0.168	0.113	0.383	0.276	0.808	0.808	0.807	0.807	3.23
66.583	22.87	2.256	0.623	2.052	0.97	1.929	0.564	1.684	0.693	0.168	0.113	0.382	0.275	0.809	0.808	0.807	0.807	3.231
66.667	22.935	2.256	0.622	2.053	0.97	1.93	0.564	1.682	0.693	0.168	0.113	0.382	0.275	0.809	0.808	0.808	0.807	3.232
66.75	23	2.256	0.621	2.053	0.97	1.931	0.564	1.68	0.692	0.167	0.113	0.382	0.275	0.809	0.808	0.808	0.807	3.232
66.833	23.064	2.256	0.62	2.053	0.97	1.933	0.564	1.678	0.692	0.167	0.113	0.381	0.274	0.809	0.808	0.808	0.807	3.232
66.917	23.129	2.256	0.619	2.053	0.969	1.934	0.564	1.676	0.692	0.167	0.112	0.38	0.273	0.809	0.808	0.808	0.807	3.232
67	23.193	2.256	0.618	2.054	0.969	1.935	0.564	1.673	0.691	0.166	0.112	0.38	0.272	0.809	0.808	0.808	0.807	3.232
67.083	23.257	2.255	0.617	2.054	0.969	1.936	0.564	1.671	0.691	0.166	0.112	0.379	0.271	0.809	0.808	0.808	0.807	3.232
67.167	23.32	2.254	0.616	2.053	0.968	1.937	0.564	1.669	0.69	0.166	0.111	0.378	0.269	0.809	0.808	0.808	0.807	3.232
67.25	23.384	2.254	0.615	2.053	0.968	1.937	0.564	1.666	0.69	0.165	0.111	0.377	0.268	0.809	0.808	0.808	0.807	3.232
67.333	23.447	2.253	0.613	2.053	0.967	1.938	0.563	1.664	0.689	0.165	0.11	0.375	0.266	0.809	0.808	0.808	0.807	3.232
67.417	23.51	2.252	0.612	2.053	0.967	1.939	0.563	1.662	0.688	0.164	0.11	0.374	0.265	0.809	0.808	0.807	0.807	3.231
67.5	23.573	2.251	0.611	2.052	0.966	1.94	0.563	1.659	0.688	0.164	0.109	0.373	0.263	0.808	0.808	0.807	0.807	3.23
67.583	23.635	2.25	0.61	2.052	0.966	1.94	0.563	1.657	0.687	0.163	0.109	0.371	0.262	0.808	0.807	0.807	0.807	3.229
67.667	23.698	2.249	0.608	2.051	0.965	1.941	0.563	1.654	0.686	0.163	0.108	0.37	0.261	0.808	0.807	0.807	0.806	3.228
67.75	23.76	2.248	0.607	2.051	0.964	1.941	0.562	1.652	0.685	0.162	0.108	0.369	0.259	0.808	0.807	0.807	0.806	3.228
67.833	23.822	2.246	0.606	2.05	0.963	1.942	0.562	1.649	0.685	0.161	0.107	0.367	0.259	0.807	0.807	0.806	0.806	3.226

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
67.917	23.883	2.245	0.604	2.049	0.963	1.942	0.562	1.646	0.684	0.161	0.107	0.366	0.258	0.807	0.806	0.806	0.806	3.225
68	23.945	2.243	0.603	2.048	0.962	1.942	0.561	1.644	0.683	0.16	0.107	0.364	0.257	0.807	0.806	0.806	0.805	3.224
68.083	24.005	2.241	0.601	2.047	0.961	1.943	0.561	1.641	0.682	0.16	0.106	0.363	0.256	0.806	0.806	0.805	0.805	3.222
68.167	24.066	2.24	0.6	2.046	0.96	1.943	0.561	1.638	0.681	0.159	0.106	0.362	0.256	0.806	0.805	0.805	0.804	3.22
68.25	24.127	2.238	0.598	2.045	0.959	1.943	0.56	1.635	0.68	0.159	0.106	0.361	0.255	0.806	0.805	0.804	0.804	3.219
68.333	24.187	2.236	0.596	2.044	0.958	1.943	0.56	1.632	0.68	0.158	0.105	0.36	0.255	0.805	0.804	0.804	0.803	3.216
68.417	24.246	2.234	0.595	2.042	0.957	1.943	0.559	1.629	0.679	0.158	0.105	0.359	0.254	0.805	0.804	0.803	0.803	3.215
68.5	24.306	2.232	0.593	2.041	0.956	1.943	0.559	1.626	0.678	0.157	0.105	0.358	0.254	0.804	0.803	0.803	0.802	3.212
68.583	24.365	2.23	0.591	2.04	0.955	1.943	0.558	1.623	0.677	0.157	0.105	0.357	0.253	0.803	0.803	0.802	0.802	3.21
68.667	24.424	2.228	0.59	2.038	0.954	1.943	0.558	1.62	0.676	0.157	0.105	0.356	0.253	0.803	0.802	0.802	0.801	3.208
68.75	24.483	2.226	0.588	2.037	0.953	1.943	0.557	1.617	0.675	0.156	0.104	0.356	0.253	0.802	0.801	0.801	0.801	3.205
68.833	24.542	2.224	0.586	2.035	0.952	1.942	0.557	1.614	0.674	0.156	0.104	0.355	0.253	0.802	0.801	0.8	0.8	3.203
68.917	24.6	2.222	0.585	2.034	0.951	1.942	0.556	1.611	0.673	0.156	0.104	0.354	0.253	0.801	0.8	0.8	0.799	3.2
69	24.658	2.22	0.583	2.032	0.95	1.942	0.556	1.608	0.672	0.155	0.104	0.354	0.252	0.8	0.799	0.799	0.799	3.197
69.083	24.715	2.218	0.581	2.03	0.949	1.941	0.555	1.604	0.671	0.155	0.104	0.353	0.252	0.8	0.799	0.799	0.798	3.196
69.167	24.772	2.215	0.58	2.029	0.948	1.941	0.555	1.601	0.67	0.155	0.104	0.353	0.252	0.799	0.798	0.798	0.797	3.192
69.25	24.829	2.213	0.579	2.027	0.946	1.94	0.554	1.598	0.669	0.155	0.104	0.352	0.252	0.798	0.798	0.797	0.797	3.19
69.333	24.885	2.211	0.577	2.025	0.945	1.94	0.554	1.595	0.668	0.154	0.104	0.352	0.252	0.798	0.797	0.797	0.796	3.188
69.417	24.941	2.208	0.576	2.024	0.944	1.939	0.553	1.591	0.667	0.154	0.104	0.351	0.252	0.797	0.796	0.796	0.795	3.184
69.5	24.997	2.206	0.575	2.022	0.943	1.938	0.553	1.588	0.666	0.154	0.104	0.351	0.252	0.796	0.795	0.795	0.795	3.181
69.583	25.051	2.204	0.573	2.02	0.942	1.938	0.552	1.585	0.665	0.154	0.104	0.351	0.252	0.796	0.795	0.794	0.794	3.179
69.667	25.106	2.201	0.572	2.018	0.941	1.937	0.551	1.581	0.664	0.154	0.104	0.35	0.252	0.795	0.794	0.794	0.793	3.176
69.75	25.161	2.199	0.571	2.016	0.939	1.936	0.551	1.578	0.663	0.153	0.104	0.35	0.252	0.794	0.793	0.793	0.792	3.172
69.833	25.215	2.196	0.57	2.014	0.938	1.935	0.55	1.575	0.662	0.153	0.104	0.35	0.252	0.793	0.793	0.792	0.792	3.17
69.917	25.269	2.194	0.569	2.013	0.937	1.934	0.55	1.571	0.661	0.153	0.104	0.35	0.252	0.793	0.792	0.791	0.791	3.167
70	25.322	2.191	0.568	2.011	0.935	1.933	0.549	1.568	0.66	0.153	0.104	0.349	0.252	0.792	0.791	0.791	0.79	3.164
70.083	25.375	2.188	0.567	2.009	0.934	1.932	0.548	1.565	0.659	0.153	0.104	0.349	0.252	0.791	0.79	0.79	0.789	3.16
70.167	25.428	2.186	0.566	2.007	0.933	1.93	0.548	1.562	0.657	0.153	0.104	0.349	0.252	0.79	0.789	0.789	0.789	3.157
70.25	25.48	2.183	0.565	2.005	0.931	1.929	0.547	1.559	0.656	0.153	0.104	0.349	0.252	0.79	0.789	0.788	0.788	3.155
70.333	25.532	2.18	0.565	2.003	0.93	1.928	0.546	1.556	0.655	0.153	0.104	0.349	0.252	0.789	0.788	0.788	0.787	3.152
70.417	25.583	2.177	0.564	2.001	0.929	1.927	0.546	1.553	0.654	0.153	0.104	0.349	0.252	0.788	0.787	0.787	0.786	3.148
70.5	25.634	2.175	0.563	1.998	0.927	1.925	0.545	1.55	0.653	0.152	0.104	0.349	0.252	0.787	0.786	0.786	0.785	3.144
70.583	25.684	2.172	0.562	1.996	0.926	1.924	0.544	1.547	0.652	0.152	0.104	0.349	0.252	0.786	0.785	0.785	0.784	3.14
70.667	25.734	2.169	0.562	1.994	0.925	1.922	0.544	1.544	0.651	0.152	0.104	0.349	0.252	0.785	0.784	0.784	0.784	3.137
70.75	25.784	2.166	0.561	1.992	0.923	1.921	0.543	1.542	0.65	0.152	0.104	0.349	0.252	0.784	0.784	0.783	0.783	3.134
70.833	25.833	2.163	0.561	1.99	0.922	1.919	0.542	1.539	0.648	0.152	0.104	0.349	0.252	0.784	0.783	0.782	0.782	3.131
70.917	25.881	2.16	0.56	1.987	0.92	1.918	0.542	1.536	0.647	0.152	0.104	0.349	0.252	0.783	0.782	0.782	0.781	3.128
71	25.93	2.157	0.56	1.985	0.919	1.916	0.541	1.534	0.646	0.152	0.104	0.349	0.252	0.782	0.781	0.781	0.78	3.124
71.083	25.977	2.154	0.559	1.983	0.918	1.914	0.54	1.531	0.645	0.152	0.104	0.349	0.252	0.781	0.78	0.78	0.779	3.12
71.167	26.025	2.151	0.559	1.981	0.916	1.913	0.539	1.529	0.644	0.152	0.104	0.349	0.252	0.78	0.779	0.779	0.778	3.116
71.25	26.072	2.148	0.558	1.978	0.915	1.911	0.539	1.526	0.643	0.152	0.104	0.349	0.252	0.779	0.778	0.778	0.777	3.112
71.333	26.118	2.145	0.558	1.976	0.913	1.909	0.538	1.524	0.642	0.152	0.104	0.349	0.252	0.778	0.777	0.777	0.776	3.108
71.417	26.164	2.142	0.557	1.974	0.912	1.907	0.537	1.522	0.641	0.152	0.104	0.349	0.252	0.777	0.776	0.776	0.775	3.104
71.5	26.21	2.139	0.557	1.971	0.911	1.906	0.536	1.519	0.64	0.152	0.104	0.349	0.252	0.776	0.775	0.775	0.774	3.1
71.583	26.254	2.136	0.556	1.969	0.909	1.904	0.536	1.517	0.639	0.152	0.104	0.349	0.252	0.775	0.774	0.774	0.774	3.097
71.667	26.298	2.133	0.556	1.966	0.908	1.902	0.535	1.515	0.638	0.152	0.104	0.349	0.252	0.774	0.773	0.773	0.773	3.093
71.75	26.342	2.13	0.556	1.964	0.907	1.9	0.534	1.513	0.637	0.152	0.104	0.349	0.252	0.773	0.772	0.772	0.772	3.089
71.833	26.385	2.127	0.555	1.961	0.906	1.898	0.533	1.511	0.636	0.152	0.104	0.349	0.252	0.772	0.771	0.771	0.771	3.085
71.917	26.428	2.124	0.555	1.959	0.904	1.896	0.533	1.509	0.635	0.152	0.104	0.349	0.252	0.771	0.77	0.77	0.77	3.081
72	26.471	2.121	0.555	1.956	0.903	1.894	0.532	1.507	0.635	0.152	0.104	0.349	0.252	0.77	0.769	0.769	0.769	3.077
72.083	26.512	2.118	0.554	1.954	0.902	1.892	0.531	1.505	0.634	0.152	0.104	0.349	0.252	0.769	0.769	0.768	0.768	3.074
72.167	26.553	2.116	0.554	1.952	0.901	1.89	0.531	1.503	0.633	0.152	0.104	0.349	0.252	0.769	0.768	0.767	0.767	3.071
72.25	26.594	2.113	0.554	1.949	0.899	1.888	0.53	1.502	0.632	0.152	0.104	0.349	0.252	0.768	0.767	0.766	0.766	3.067
72.333	26.634	2.11	0.553	1.947	0.898	1.886	0.529	1.5	0.631	0.152	0.104	0.349	0.252	0.767	0.766	0.765	0.765	3.063
72.417	26.674	2.108	0.553	1.945	0.897	1.884	0.529	1.498	0.63	0.152	0.104	0.349	0.252	0.766	0.765	0.765	0.764	3.06
72.5	26.714	2.105	0.553	1.942	0.896	1.882	0.528	1.497	0.629	0.152	0.104	0.349	0.252	0.765	0.764	0.764	0.763	3.056
72.583	26.752	2.102	0.553	1.94	0.895	1.88	0.527	1.495	0.629	0.152	0.103	0.349	0.252	0.764	0.763	0.763	0.762	3.052
72.667	26.789	2.1	0.552	1.938	0.894	1.878	0.527	1.493	0.628	0.152	0.103	0.348	0.251	0.763	0.762	0.762	0.761	3.048
72.75	26.827	2.097	0.552	1.935	0.892	1.875	0.526	1.492	0.627	0.152	0.103	0.348	0.251	0.762	0.761	0.761	0.76	3.044
72.833	26.864	2.094	0.551	1.933	0.891	1.873	0.525	1.49	0.626	0.152	0.103	0.347	0.249	0.761	0.76	0.76	0.759	3.04
72.917	26.9	2.092	0.551	1.93	0.89	1.871	0.525	1.488	0.625	0.151	0.102	0.346	0.247	0.76	0.759	0.759	0.758	3.036
73	26.936	2.089	0.55	1.928	0.889	1.868	0.524	1.486	0.624	0.151	0.102	0.345	0.246	0.759	0.758	0.758	0.757	3.032
73.083	26.97	2.086	0.549	1.925	0.887	1.866	0.523	1.484	0.623	0.15	0.101	0.343	0.242	0.758	0.757	0.757	0.756	3.028

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
73.167	27.005	2.083	0.548	1.923	0.886	1.863	0.523	1.481	0.622	0.15	0.0998	0.341	0.239	0.757	0.756	0.756	0.755	3.024
73.25	27.039	2.08	0.547	1.92	0.885	1.86	0.522	1.479	0.621	0.149	0.0988	0.339	0.235	0.756	0.755	0.755	0.754	3.02
73.333	27.072	2.077	0.545	1.917	0.883	1.858	0.521	1.477	0.62	0.148	0.0975	0.337	0.231	0.755	0.754	0.754	0.753	3.016
73.417	27.104	2.074	0.544	1.915	0.882	1.855	0.52	1.474	0.619	0.147	0.0962	0.334	0.228	0.754	0.753	0.753	0.752	3.012
73.5	27.137	2.07	0.543	1.912	0.88	1.852	0.519	1.471	0.618	0.146	0.0949	0.331	0.224	0.753	0.752	0.752	0.751	3.008
73.583	27.168	2.067	0.541	1.909	0.879	1.849	0.519	1.468	0.617	0.145	0.0935	0.327	0.22	0.752	0.751	0.75	0.75	3.003
73.667	27.198	2.064	0.539	1.906	0.877	1.846	0.518	1.465	0.616	0.143	0.0922	0.324	0.217	0.751	0.75	0.749	0.749	2.999
73.75	27.229	2.06	0.537	1.903	0.876	1.843	0.517	1.462	0.615	0.142	0.0909	0.32	0.214	0.749	0.749	0.748	0.748	2.994
73.833	27.258	2.056	0.535	1.9	0.874	1.84	0.516	1.459	0.613	0.141	0.0898	0.317	0.212	0.748	0.747	0.747	0.746	2.988
73.917	27.287	2.053	0.533	1.897	0.873	1.837	0.515	1.455	0.612	0.139	0.0887	0.313	0.209	0.747	0.746	0.746	0.745	2.984
74	27.316	2.049	0.531	1.894	0.871	1.834	0.514	1.452	0.611	0.138	0.0877	0.31	0.207	0.746	0.745	0.745	0.744	2.98
74.083	27.343	2.045	0.528	1.891	0.869	1.831	0.513	1.448	0.61	0.137	0.0869	0.306	0.205	0.745	0.744	0.743	0.743	2.975
74.167	27.369	2.041	0.525	1.888	0.868	1.828	0.512	1.445	0.608	0.135	0.086	0.303	0.204	0.743	0.742	0.742	0.741	2.968
74.25	27.396	2.038	0.523	1.885	0.866	1.825	0.511	1.441	0.607	0.134	0.0852	0.3	0.202	0.742	0.741	0.741	0.74	2.964
74.333	27.421	2.033	0.52	1.881	0.864	1.822	0.51	1.437	0.606	0.133	0.0846	0.298	0.201	0.741	0.74	0.74	0.739	2.96
74.417	27.446	2.029	0.517	1.878	0.862	1.818	0.509	1.433	0.604	0.132	0.084	0.295	0.199	0.739	0.738	0.738	0.738	2.953
74.5	27.47	2.025	0.513	1.875	0.86	1.815	0.508	1.428	0.603	0.131	0.0834	0.293	0.198	0.738	0.737	0.737	0.736	2.948
74.583	27.493	2.021	0.51	1.871	0.858	1.812	0.507	1.424	0.601	0.13	0.0829	0.291	0.197	0.737	0.736	0.735	0.735	2.943
74.667	27.516	2.017	0.507	1.868	0.857	1.809	0.506	1.419	0.6	0.129	0.0825	0.289	0.197	0.735	0.734	0.734	0.733	2.936
74.75	27.539	2.013	0.504	1.864	0.855	1.805	0.505	1.415	0.598	0.128	0.082	0.287	0.196	0.734	0.733	0.733	0.732	2.932
74.833	27.56	2.008	0.5	1.86	0.853	1.802	0.504	1.41	0.597	0.127	0.0816	0.285	0.196	0.732	0.731	0.731	0.731	2.925
74.917	27.58	2.004	0.497	1.857	0.851	1.798	0.503	1.405	0.595	0.126	0.0813	0.284	0.195	0.731	0.73	0.73	0.729	2.92
75	27.601	1.999	0.494	1.853	0.849	1.795	0.502	1.4	0.594	0.125	0.0809	0.282	0.195	0.729	0.729	0.728	0.728	2.914
75.083	27.62	1.994	0.491	1.849	0.846	1.791	0.501	1.395	0.592	0.125	0.0807	0.281	0.195	0.728	0.727	0.727	0.726	2.908
75.167	27.638	1.99	0.488	1.845	0.844	1.788	0.499	1.39	0.59	0.124	0.0805	0.279	0.195	0.726	0.725	0.725	0.724	2.9
75.25	27.657	1.985	0.485	1.841	0.842	1.784	0.498	1.384	0.589	0.123	0.0802	0.278	0.195	0.725	0.724	0.724	0.723	2.896
75.333	27.673	1.98	0.482	1.837	0.84	1.781	0.497	1.378	0.587	0.123	0.0801	0.277	0.195	0.723	0.722	0.722	0.721	2.888
75.417	27.689	1.975	0.479	1.833	0.838	1.777	0.496	1.373	0.585	0.122	0.08	0.276	0.195	0.722	0.721	0.72	0.72	2.883
75.5	27.705	1.971	0.477	1.829	0.836	1.774	0.495	1.367	0.583	0.122	0.0798	0.275	0.195	0.72	0.719	0.719	0.718	2.876
75.583	27.719	1.966	0.474	1.825	0.833	1.77	0.494	1.361	0.581	0.121	0.0798	0.274	0.194	0.718	0.717	0.717	0.716	2.868
75.667	27.733	1.961	0.472	1.821	0.831	1.766	0.492	1.355	0.579	0.121	0.0797	0.273	0.194	0.717	0.716	0.715	0.715	2.863
75.75	27.747	1.955	0.469	1.816	0.829	1.763	0.491	1.348	0.577	0.12	0.0796	0.272	0.194	0.715	0.714	0.714	0.713	2.856
75.833	27.759	1.95	0.467	1.812	0.826	1.759	0.49	1.342	0.575	0.12	0.0794	0.271	0.193	0.713	0.712	0.712	0.711	2.848
75.917	27.771	1.945	0.464	1.808	0.824	1.755	0.488	1.336	0.573	0.119	0.0793	0.27	0.193	0.711	0.71	0.71	0.709	2.84
76	27.783	1.939	0.462	1.803	0.821	1.751	0.487	1.329	0.571	0.119	0.0791	0.269	0.192	0.71	0.709	0.708	0.708	2.835
76.083	27.793	1.934	0.46	1.798	0.818	1.747	0.486	1.323	0.569	0.118	0.0787	0.268	0.191	0.708	0.707	0.706	0.706	2.827
76.167	27.802	1.928	0.457	1.794	0.816	1.743	0.484	1.317	0.567	0.118	0.0784	0.267	0.19	0.706	0.705	0.705	0.704	2.82
76.25	27.811	1.922	0.455	1.789	0.813	1.739	0.483	1.311	0.565	0.117	0.078	0.266	0.188	0.704	0.703	0.703	0.702	2.812
76.333	27.818	1.916	0.453	1.784	0.81	1.735	0.482	1.305	0.562	0.117	0.0775	0.265	0.187	0.702	0.701	0.701	0.7	2.804
76.417	27.825	1.91	0.451	1.779	0.807	1.731	0.48	1.299	0.56	0.116	0.077	0.263	0.185	0.7	0.699	0.699	0.698	2.796
76.5	27.832	1.904	0.448	1.774	0.805	1.727	0.479	1.292	0.558	0.115	0.0765	0.262	0.184	0.698	0.697	0.697	0.696	2.788
76.583	27.837	1.898	0.446	1.769	0.802	1.723	0.477	1.286	0.555	0.115	0.0759	0.261	0.182	0.696	0.695	0.695	0.694	2.78
76.667	27.841	1.892	0.444	1.764	0.799	1.719	0.476	1.281	0.553	0.114	0.0754	0.259	0.181	0.694	0.693	0.693	0.692	2.772
76.75	27.846	1.885	0.442	1.759	0.796	1.715	0.474	1.275	0.551	0.114	0.0748	0.258	0.18	0.692	0.691	0.691	0.69	2.764
76.833	27.848	1.878	0.44	1.753	0.792	1.711	0.472	1.269	0.548	0.113	0.0744	0.256	0.179	0.69	0.689	0.689	0.688	2.756
76.917	27.85	1.872	0.437	1.748	0.789	1.706	0.471	1.263	0.546	0.112	0.074	0.255	0.178	0.688	0.687	0.686	0.686	2.747
77	27.852	1.865	0.435	1.742	0.786	1.702	0.469	1.257	0.544	0.112	0.0735	0.254	0.177	0.686	0.685	0.684	0.684	2.739
77.083	27.851	1.858	0.433	1.737	0.783	1.698	0.467	1.251	0.541	0.111	0.0732	0.252	0.176	0.683	0.682	0.682	0.681	2.728
77.167	27.851	1.851	0.431	1.731	0.78	1.693	0.466	1.246	0.539	0.111	0.0728	0.251	0.175	0.681	0.68	0.68	0.679	2.72
77.25	27.85	1.844	0.428	1.725	0.777	1.689	0.464	1.24	0.537	0.11	0.0725	0.25	0.175	0.679	0.678	0.677	0.677	2.711
77.333	27.848	1.837	0.426	1.719	0.774	1.684	0.462	1.235	0.534	0.11	0.0723	0.249	0.174	0.676	0.675	0.675	0.674	2.7
77.417	27.845	1.829	0.424	1.713	0.77	1.68	0.46	1.229	0.532	0.109	0.072	0.248	0.174	0.674	0.673	0.673	0.672	2.692
77.5	27.842	1.822	0.421	1.708	0.767	1.676	0.459	1.223	0.53	0.109	0.0718	0.247	0.173	0.672	0.671	0.67	0.67	2.683
77.583	27.836	1.815	0.419	1.701	0.764	1.671	0.457	1.218	0.528	0.108	0.0716	0.246	0.173	0.669	0.668	0.668	0.667	2.672
77.667	27.831	1.808	0.417	1.695	0.761	1.666	0.455	1.213	0.526	0.108	0.0714	0.245	0.172	0.667	0.666	0.666	0.665	2.664
77.75	27.825	1.801	0.414	1.689	0.758	1.662	0.453	1.207	0.523	0.107	0.0712	0.244	0.172	0.664	0.663	0.663	0.662	2.652
77.833	27.817	1.794	0.412	1.683	0.755	1.657	0.452	1.202	0.521	0.107	0.071	0.244	0.172	0.662	0.661	0.661	0.66	2.644
77.917	27.809	1.787	0.41	1.677	0.752	1.652	0.45	1.197	0.519	0.107	0.0709	0.243	0.172	0.659	0.658	0.658	0.657	2.632
78	27.801	1.78	0.408	1.67	0.749	1.648	0.448	1.191	0.517	0.107	0.0707	0.242	0.172	0.657	0.656	0.656	0.655	2.624
78.083	27.79	1.773	0.406	1.664	0.746	1.643	0.446	1.186	0.515	0.106	0.0706	0.242	0.171	0.655	0.654	0.653	0.652	2.614
78.167	27.78	1.766	0.404	1.658	0.743	1.638	0.445	1.181	0.513	0.106	0.0705	0.241	0.171	0.652	0.651	0.651	0.65	2.604
78.25	27.769	1.76	0.402	1.652	0.74	1.633	0.443	1.176	0.511	0.106	0.0704	0.241	0.171	0.65	0.649	0.648	0.648	2.595
78.333	27.756	1.753	0.4	1.646	0.737	1.628	0.441	1.171	0.508	0.106	0.0704	0.24	0.171	0.647	0.646	0.646	0.645	2.584

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
78.417	27.743	1.746	0.398	1.64	0.734	1.623	0.44	1.166	0.506	0.105	0.0703	0.24	0.171	0.645	0.644	0.644	0.643	2.576
78.5	27.73	1.739	0.397	1.634	0.731	1.618	0.438	1.16	0.504	0.105	0.0703	0.239	0.171	0.642	0.641	0.641	0.64	2.564
78.583	27.714	1.733	0.395	1.628	0.729	1.613	0.436	1.155	0.502	0.105	0.0702	0.239	0.171	0.64	0.639	0.639	0.638	2.556
78.667	27.698	1.726	0.393	1.622	0.726	1.608	0.435	1.15	0.5	0.105	0.0702	0.239	0.171	0.638	0.637	0.636	0.636	2.547
78.75	27.683	1.719	0.392	1.616	0.723	1.603	0.433	1.145	0.498	0.104	0.0702	0.238	0.171	0.635	0.634	0.634	0.633	2.536
78.833	27.665	1.713	0.39	1.61	0.72	1.598	0.431	1.14	0.496	0.104	0.0701	0.238	0.171	0.633	0.632	0.632	0.631	2.528
78.917	27.647	1.706	0.389	1.604	0.717	1.593	0.43	1.136	0.494	0.104	0.07	0.237	0.171	0.631	0.63	0.629	0.629	2.519
79	27.629	1.7	0.388	1.598	0.714	1.587	0.428	1.131	0.492	0.104	0.0699	0.237	0.17	0.628	0.627	0.627	0.626	2.508
79.083	27.608	1.693	0.386	1.592	0.712	1.582	0.426	1.126	0.49	0.104	0.0698	0.236	0.17	0.626	0.625	0.625	0.624	2.5
79.167	27.588	1.687	0.385	1.586	0.709	1.577	0.425	1.121	0.488	0.103	0.0696	0.236	0.169	0.624	0.623	0.622	0.622	2.491
79.25	27.567	1.68	0.384	1.581	0.706	1.571	0.423	1.116	0.486	0.103	0.0694	0.235	0.168	0.621	0.62	0.62	0.619	2.48
79.333	27.544	1.674	0.383	1.575	0.703	1.566	0.421	1.112	0.484	0.103	0.0692	0.235	0.168	0.619	0.618	0.618	0.617	2.472
79.417	27.521	1.667	0.381	1.569	0.701	1.56	0.42	1.107	0.482	0.103	0.0689	0.234	0.167	0.617	0.616	0.615	0.615	2.463
79.5	27.498	1.661	0.38	1.563	0.698	1.555	0.418	1.103	0.48	0.102	0.0687	0.234	0.166	0.615	0.613	0.613	0.612	2.453
79.583	27.473	1.654	0.379	1.557	0.695	1.549	0.417	1.098	0.478	0.102	0.0684	0.233	0.165	0.612	0.611	0.611	0.61	2.444
79.667	27.447	1.648	0.378	1.551	0.692	1.544	0.415	1.094	0.476	0.102	0.0681	0.232	0.165	0.61	0.609	0.609	0.608	2.436
79.75	27.422	1.642	0.377	1.546	0.69	1.538	0.413	1.089	0.474	0.101	0.0679	0.232	0.164	0.608	0.607	0.606	0.605	2.426
79.833	27.394	1.635	0.376	1.54	0.687	1.532	0.412	1.085	0.472	0.101	0.0676	0.231	0.164	0.605	0.604	0.604	0.603	2.416
79.917	27.367	1.629	0.375	1.534	0.684	1.527	0.41	1.081	0.47	0.101	0.0674	0.23	0.163	0.603	0.602	0.602	0.601	2.408
80	27.339	1.623	0.374	1.528	0.681	1.521	0.409	1.076	0.468	0.101	0.0672	0.229	0.163	0.601	0.6	0.599	0.599	2.399
80.083	27.31	1.616	0.373	1.523	0.679	1.516	0.407	1.072	0.467	0.1	0.067	0.229	0.162	0.599	0.598	0.597	0.596	2.39
80.167	27.28	1.61	0.372	1.517	0.676	1.51	0.406	1.068	0.465	0.0999	0.0668	0.228	0.162	0.596	0.595	0.595	0.594	2.38
80.25	27.25	1.604	0.371	1.511	0.673	1.505	0.404	1.064	0.463	0.0997	0.0667	0.227	0.161	0.594	0.593	0.593	0.592	2.372
80.333	27.218	1.598	0.37	1.506	0.671	1.5	0.402	1.06	0.461	0.0994	0.0665	0.227	0.161	0.592	0.591	0.59	0.59	2.363
80.417	27.186	1.592	0.369	1.5	0.668	1.494	0.401	1.056	0.46	0.0992	0.0664	0.226	0.161	0.59	0.589	0.588	0.587	2.354
80.5	27.154	1.585	0.368	1.494	0.666	1.489	0.399	1.052	0.458	0.099	0.0663	0.226	0.161	0.587	0.586	0.586	0.585	2.344
80.583	27.12	1.579	0.367	1.489	0.663	1.484	0.398	1.048	0.456	0.0988	0.0662	0.225	0.161	0.585	0.584	0.584	0.583	2.336
80.667	27.085	1.573	0.366	1.483	0.661	1.478	0.396	1.044	0.455	0.0986	0.0661	0.225	0.16	0.583	0.582	0.582	0.581	2.328
80.75	27.051	1.567	0.365	1.477	0.658	1.473	0.395	1.04	0.453	0.0984	0.066	0.225	0.16	0.581	0.58	0.579	0.578	2.318
80.833	27.015	1.562	0.364	1.472	0.656	1.468	0.393	1.036	0.452	0.0982	0.0659	0.224	0.16	0.579	0.578	0.577	0.576	2.31
80.917	26.979	1.556	0.363	1.466	0.653	1.463	0.392	1.032	0.45	0.098	0.0658	0.224	0.16	0.577	0.575	0.575	0.574	2.301
81	26.943	1.55	0.362	1.461	0.651	1.457	0.39	1.029	0.448	0.0979	0.0657	0.224	0.16	0.574	0.573	0.573	0.572	2.292
81.083	26.905	1.545	0.361	1.456	0.649	1.452	0.389	1.025	0.447	0.0977	0.0657	0.223	0.16	0.572	0.571	0.571	0.57	2.284
81.167	26.867	1.539	0.36	1.45	0.646	1.447	0.388	1.021	0.445	0.0976	0.0656	0.223	0.16	0.57	0.569	0.569	0.568	2.276
81.25	26.829	1.534	0.359	1.445	0.644	1.442	0.386	1.018	0.444	0.0975	0.0656	0.223	0.16	0.568	0.567	0.567	0.566	2.268
81.333	26.789	1.528	0.358	1.44	0.642	1.437	0.385	1.014	0.442	0.0974	0.0656	0.223	0.16	0.566	0.565	0.565	0.564	2.26
81.417	26.749	1.523	0.357	1.435	0.64	1.432	0.383	1.011	0.441	0.0973	0.0655	0.222	0.16	0.564	0.563	0.563	0.562	2.252
81.5	26.709	1.518	0.356	1.43	0.638	1.427	0.382	1.007	0.439	0.0971	0.0655	0.222	0.16	0.562	0.561	0.561	0.56	2.244
81.583	26.668	1.512	0.356	1.425	0.635	1.422	0.381	1.004	0.438	0.097	0.0655	0.222	0.16	0.56	0.559	0.559	0.558	2.236
81.667	26.626	1.507	0.355	1.42	0.633	1.416	0.38	1.001	0.436	0.0969	0.0654	0.222	0.16	0.558	0.557	0.557	0.556	2.228
81.75	26.584	1.502	0.354	1.415	0.631	1.411	0.378	0.997	0.435	0.0968	0.0654	0.221	0.16	0.556	0.555	0.555	0.554	2.22
81.833	26.541	1.497	0.353	1.41	0.629	1.406	0.377	0.994	0.433	0.0966	0.0652	0.221	0.159	0.554	0.553	0.553	0.552	2.212
81.917	26.498	1.492	0.353	1.405	0.627	1.401	0.376	0.991	0.432	0.0964	0.0651	0.221	0.159	0.552	0.551	0.551	0.55	2.204
82	26.454	1.487	0.352	1.4	0.625	1.396	0.374	0.987	0.43	0.0963	0.065	0.22	0.158	0.55	0.549	0.549	0.548	2.196
82.083	26.409	1.482	0.351	1.396	0.623	1.391	0.373	0.984	0.429	0.096	0.0646	0.219	0.157	0.549	0.547	0.547	0.546	2.189
82.167	26.365	1.477	0.35	1.391	0.621	1.386	0.372	0.981	0.427	0.0957	0.0643	0.219	0.156	0.547	0.546	0.545	0.544	2.182
82.25	26.32	1.472	0.349	1.386	0.618	1.381	0.371	0.977	0.426	0.0954	0.064	0.218	0.154	0.545	0.544	0.543	0.542	2.174
82.333	26.274	1.467	0.348	1.381	0.616	1.376	0.369	0.974	0.424	0.095	0.0635	0.217	0.153	0.543	0.542	0.541	0.54	2.166
82.417	26.227	1.462	0.347	1.377	0.614	1.371	0.368	0.971	0.422	0.0946	0.063	0.216	0.151	0.541	0.54	0.54	0.539	2.16
82.5	26.181	1.457	0.346	1.372	0.612	1.366	0.367	0.968	0.421	0.0942	0.0625	0.215	0.15	0.539	0.538	0.538	0.537	2.152
82.583	26.133	1.452	0.345	1.367	0.61	1.361	0.366	0.965	0.419	0.0937	0.062	0.213	0.148	0.537	0.536	0.536	0.535	2.144
82.667	26.086	1.447	0.344	1.363	0.608	1.356	0.364	0.961	0.418	0.0932	0.0614	0.212	0.147	0.536	0.534	0.534	0.533	2.137
82.75	26.038	1.442	0.343	1.358	0.606	1.351	0.363	0.958	0.416	0.0927	0.0609	0.211	0.145	0.534	0.533	0.532	0.531	2.13
82.833	25.989	1.437	0.342	1.353	0.604	1.346	0.362	0.955	0.415	0.0921	0.0604	0.209	0.144	0.532	0.531	0.53	0.529	2.122
82.917	25.94	1.432	0.341	1.349	0.601	1.341	0.361	0.952	0.413	0.0915	0.0599	0.208	0.143	0.53	0.529	0.529	0.528	2.116
83	25.891	1.427	0.34	1.344	0.599	1.336	0.359	0.949	0.412	0.091	0.0595	0.206	0.142	0.528	0.527	0.527	0.526	2.108
83.083	25.84	1.422	0.339	1.34	0.597	1.331	0.358	0.946	0.41	0.0904	0.0591	0.205	0.142	0.527	0.525	0.525	0.524	2.101
83.167	25.79	1.417	0.338	1.335	0.595	1.326	0.357	0.943	0.409	0.0898	0.0587	0.204	0.141	0.525	0.524	0.523	0.522	2.094
83.25	25.74	1.412	0.336	1.331	0.593	1.321	0.356	0.94	0.407	0.0893	0.0584	0.202	0.14	0.523	0.522	0.521	0.52	2.086
83.333	25.688	1.407	0.335	1.326	0.591	1.316	0.354	0.936	0.406	0.0888	0.0581	0.201	0.14	0.521	0.52	0.52	0.519	2.08
83.417	25.637	1.402	0.334	1.321	0.589	1.311	0.353	0.933	0.405	0.0883	0.0579	0.2	0.139	0.519	0.518	0.518	0.517	2.072
83.5	25.585	1.397	0.332	1.317	0.587	1.306	0.352	0.93	0.403	0.0878	0.0576	0.199	0.139	0.518	0.516	0.516	0.515	2.065
83.583	25.533	1.392	0.331	1.312	0.585	1.301	0.351	0.927	0.402	0.0874	0.0574	0.198	0.138	0.516	0.515	0.514	0.513	2.058

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
83.667	25.48	1.387	0.329	1.308	0.582	1.297	0.349	0.924	0.4	0.087	0.0572	0.198	0.138	0.514	0.513	0.512	0.511	2.05
83.75	25.428	1.382	0.328	1.303	0.58	1.292	0.348	0.921	0.399	0.0866	0.057	0.197	0.137	0.512	0.511	0.511	0.51	2.044
83.833	25.375	1.378	0.326	1.299	0.578	1.287	0.347	0.918	0.397	0.0863	0.0568	0.196	0.137	0.51	0.509	0.509	0.508	2.036
83.917	25.321	1.373	0.325	1.294	0.576	1.282	0.346	0.915	0.396	0.086	0.0567	0.195	0.137	0.509	0.507	0.507	0.506	2.029
84	25.268	1.368	0.323	1.29	0.574	1.278	0.344	0.912	0.395	0.0856	0.0565	0.195	0.137	0.507	0.506	0.505	0.504	2.022
84.083	25.213	1.363	0.322	1.285	0.572	1.273	0.343	0.909	0.393	0.0854	0.0564	0.194	0.137	0.505	0.504	0.504	0.502	2.015
84.167	25.159	1.358	0.32	1.281	0.57	1.268	0.342	0.906	0.392	0.0851	0.0563	0.194	0.137	0.503	0.502	0.502	0.501	2.008
84.25	25.105	1.353	0.319	1.276	0.568	1.264	0.341	0.903	0.39	0.0848	0.0562	0.193	0.137	0.501	0.5	0.5	0.499	2
84.333	25.049	1.349	0.318	1.272	0.566	1.259	0.34	0.9	0.389	0.0846	0.0561	0.193	0.137	0.5	0.499	0.498	0.497	1.994
84.417	24.994	1.344	0.316	1.267	0.564	1.255	0.338	0.897	0.387	0.0844	0.0561	0.192	0.137	0.498	0.497	0.496	0.495	1.986
84.5	24.939	1.339	0.315	1.263	0.562	1.25	0.337	0.893	0.386	0.0842	0.056	0.192	0.137	0.496	0.495	0.495	0.494	1.98
84.583	24.883	1.334	0.314	1.259	0.56	1.246	0.336	0.89	0.385	0.0839	0.056	0.191	0.137	0.495	0.493	0.493	0.492	1.973
84.667	24.827	1.33	0.313	1.254	0.558	1.241	0.335	0.887	0.383	0.0837	0.0559	0.191	0.137	0.493	0.492	0.491	0.49	1.966
84.75	24.771	1.325	0.312	1.25	0.556	1.236	0.334	0.884	0.382	0.0835	0.0559	0.19	0.136	0.491	0.49	0.49	0.489	1.96
84.833	24.714	1.32	0.31	1.246	0.554	1.232	0.333	0.88	0.38	0.0832	0.0557	0.19	0.136	0.489	0.488	0.488	0.487	1.952
84.917	24.657	1.316	0.309	1.241	0.552	1.227	0.331	0.877	0.379	0.0829	0.0555	0.189	0.135	0.488	0.487	0.486	0.485	1.946
85	24.601	1.311	0.308	1.237	0.55	1.223	0.33	0.873	0.378	0.0826	0.0553	0.188	0.134	0.486	0.485	0.484	0.483	1.938
85.083	24.543	1.306	0.307	1.232	0.548	1.218	0.329	0.87	0.376	0.0822	0.0548	0.187	0.133	0.484	0.483	0.483	0.482	1.932
85.167	24.486	1.301	0.305	1.228	0.546	1.214	0.328	0.866	0.375	0.0817	0.0544	0.186	0.131	0.482	0.481	0.481	0.48	1.924
85.25	24.429	1.296	0.304	1.224	0.544	1.209	0.327	0.863	0.373	0.0813	0.0539	0.185	0.129	0.481	0.48	0.479	0.478	1.918
85.333	24.371	1.291	0.303	1.219	0.541	1.204	0.325	0.859	0.371	0.0807	0.0532	0.184	0.127	0.479	0.478	0.477	0.476	1.91
85.417	24.313	1.286	0.301	1.215	0.539	1.2	0.324	0.855	0.37	0.0801	0.0525	0.182	0.125	0.477	0.476	0.476	0.474	1.903
85.5	24.255	1.281	0.3	1.21	0.537	1.195	0.323	0.852	0.368	0.0795	0.0518	0.18	0.122	0.475	0.474	0.474	0.473	1.896
85.583	24.196	1.276	0.298	1.205	0.535	1.19	0.321	0.848	0.367	0.0787	0.0509	0.178	0.12	0.473	0.472	0.472	0.471	1.888
85.667	24.138	1.271	0.296	1.201	0.533	1.186	0.32	0.844	0.365	0.078	0.0501	0.176	0.118	0.472	0.47	0.47	0.469	1.881
85.75	24.079	1.266	0.295	1.196	0.53	1.181	0.319	0.84	0.364	0.0772	0.0492	0.174	0.116	0.47	0.469	0.468	0.467	1.874
85.833	24.02	1.26	0.293	1.191	0.528	1.176	0.318	0.837	0.362	0.0763	0.0485	0.172	0.114	0.468	0.467	0.466	0.465	1.866
85.917	23.961	1.255	0.291	1.187	0.526	1.172	0.316	0.833	0.36	0.0755	0.0478	0.17	0.112	0.466	0.465	0.465	0.463	1.859
86	23.902	1.25	0.29	1.182	0.523	1.167	0.315	0.829	0.359	0.0746	0.0471	0.168	0.111	0.464	0.463	0.463	0.462	1.852
86.083	23.843	1.244	0.288	1.177	0.521	1.162	0.314	0.825	0.357	0.0737	0.0466	0.166	0.11	0.462	0.461	0.461	0.46	1.844
86.167	23.783	1.239	0.286	1.172	0.519	1.158	0.312	0.821	0.356	0.0729	0.046	0.164	0.109	0.46	0.459	0.459	0.458	1.836
86.25	23.724	1.233	0.284	1.168	0.516	1.153	0.311	0.817	0.354	0.0721	0.0455	0.162	0.107	0.459	0.457	0.457	0.456	1.829
86.333	23.664	1.228	0.281	1.163	0.514	1.148	0.309	0.813	0.353	0.0713	0.045	0.16	0.107	0.457	0.455	0.455	0.454	1.821
86.417	23.604	1.222	0.279	1.158	0.511	1.144	0.308	0.809	0.351	0.0706	0.0446	0.158	0.106	0.455	0.453	0.453	0.452	1.813
86.5	23.544	1.217	0.277	1.153	0.509	1.139	0.307	0.805	0.349	0.0699	0.0442	0.157	0.105	0.453	0.452	0.451	0.45	1.806
86.583	23.484	1.211	0.275	1.148	0.507	1.134	0.305	0.801	0.348	0.0692	0.0439	0.156	0.104	0.451	0.45	0.449	0.448	1.798
86.667	23.424	1.205	0.272	1.143	0.504	1.13	0.304	0.797	0.346	0.0686	0.0436	0.154	0.104	0.449	0.448	0.447	0.446	1.79
86.75	23.364	1.2	0.27	1.138	0.502	1.125	0.302	0.793	0.345	0.068	0.0433	0.153	0.103	0.447	0.446	0.445	0.444	1.782
86.833	23.303	1.194	0.267	1.133	0.5	1.12	0.301	0.788	0.343	0.0675	0.0431	0.152	0.103	0.445	0.444	0.443	0.442	1.774
86.917	23.242	1.189	0.265	1.128	0.497	1.116	0.299	0.784	0.342	0.067	0.0428	0.151	0.103	0.443	0.442	0.441	0.44	1.766
87	23.182	1.183	0.263	1.122	0.495	1.111	0.298	0.78	0.34	0.0665	0.0426	0.15	0.102	0.441	0.44	0.439	0.438	1.758
87.083	23.121	1.178	0.261	1.117	0.493	1.107	0.297	0.775	0.338	0.0661	0.0424	0.149	0.102	0.439	0.437	0.437	0.436	1.749
87.167	23.06	1.172	0.258	1.112	0.491	1.102	0.295	0.771	0.337	0.0657	0.0422	0.148	0.102	0.437	0.435	0.435	0.434	1.741
87.25	22.999	1.167	0.256	1.107	0.488	1.097	0.294	0.767	0.335	0.0652	0.0421	0.147	0.102	0.435	0.433	0.433	0.432	1.733
87.333	22.938	1.161	0.254	1.102	0.486	1.093	0.292	0.762	0.333	0.0649	0.042	0.147	0.102	0.433	0.431	0.431	0.43	1.725
87.417	22.877	1.156	0.252	1.097	0.484	1.088	0.291	0.758	0.332	0.0646	0.0419	0.146	0.102	0.431	0.429	0.429	0.428	1.717
87.5	22.816	1.15	0.25	1.092	0.481	1.083	0.29	0.753	0.33	0.0642	0.0418	0.145	0.102	0.429	0.427	0.427	0.426	1.709
87.583	22.754	1.145	0.249	1.087	0.479	1.079	0.288	0.748	0.328	0.0639	0.0417	0.145	0.102	0.427	0.425	0.425	0.424	1.701
87.667	22.693	1.139	0.247	1.082	0.477	1.074	0.287	0.744	0.327	0.0636	0.0417	0.144	0.102	0.425	0.423	0.423	0.422	1.693
87.75	22.632	1.134	0.245	1.077	0.475	1.07	0.286	0.739	0.325	0.0633	0.0417	0.143	0.102	0.423	0.421	0.421	0.42	1.685
87.833	22.57	1.128	0.243	1.072	0.472	1.065	0.284	0.734	0.323	0.0631	0.0416	0.143	0.102	0.421	0.419	0.419	0.418	1.677
87.917	22.509	1.123	0.242	1.067	0.47	1.06	0.283	0.729	0.322	0.0628	0.0415	0.142	0.102	0.419	0.418	0.417	0.416	1.67
88	22.447	1.118	0.24	1.062	0.468	1.056	0.282	0.725	0.32	0.0625	0.0415	0.142	0.101	0.417	0.416	0.415	0.414	1.662
88.083	22.385	1.112	0.239	1.057	0.465	1.051	0.28	0.72	0.318	0.0622	0.0413	0.141	0.101	0.415	0.414	0.413	0.412	1.654
88.167	22.323	1.107	0.237	1.052	0.463	1.046	0.279	0.715	0.316	0.0619	0.0412	0.141	0.1	0.413	0.411	0.411	0.41	1.645
88.25	22.261	1.101	0.235	1.047	0.461	1.042	0.277	0.711	0.315	0.0616	0.0411	0.14	0.0998	0.411	0.409	0.409	0.408	1.637
88.333	22.199	1.096	0.234	1.042	0.458	1.037	0.276	0.706	0.313	0.0613	0.0408	0.139	0.099	0.409	0.407	0.407	0.406	1.629
88.417	22.137	1.09	0.233	1.037	0.456	1.032	0.275	0.702	0.311	0.061	0.0406	0.139	0.0982	0.407	0.406	0.405	0.404	1.622
88.5	22.075	1.085	0.231	1.032	0.454	1.028	0.273	0.697	0.309	0.0607	0.0404	0.138	0.0974	0.405	0.404	0.403	0.402	1.614
88.583	22.013	1.079	0.23	1.026	0.451	1.023	0.272	0.693	0.307	0.0603	0.0401	0.138	0.0967	0.403	0.401	0.401	0.4	1.605
88.667	21.951	1.074	0.229	1.021	0.449	1.018	0.271	0.688	0.306	0.06	0.0398	0.137	0.0959	0.401	0.399	0.399	0.398	1.597
88.75	21.889	1.068	0.227	1.016	0.446	1.013	0.269	0.684	0.304	0.0597	0.0395	0.136	0.0952	0.399	0.397	0.397	0.396	1.589
88.833	21.826	1.062	0.226	1.011	0.444	1.009	0.268	0.68	0.302	0.0594	0.0393	0.135	0.0946	0.397	0.395	0.395	0.394	1.581

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
88.917	21.764	1.057	0.225	1.006	0.442	1.004	0.266	0.676	0.3	0.059	0.039	0.135	0.0941	0.395	0.393	0.393	0.392	1.573
89	21.702	1.051	0.224	1.001	0.439	1	0.265	0.671	0.298	0.0587	0.0388	0.134	0.0935	0.393	0.391	0.391	0.39	1.565
89.083	21.639	1.046	0.222	0.996	0.437	0.995	0.264	0.667	0.297	0.0584	0.0386	0.133	0.0931	0.391	0.389	0.389	0.388	1.557
89.167	21.577	1.04	0.221	0.991	0.434	0.99	0.262	0.663	0.295	0.0581	0.0384	0.133	0.0927	0.389	0.387	0.387	0.386	1.549
89.25	21.514	1.034	0.22	0.985	0.432	0.986	0.261	0.659	0.293	0.0578	0.0382	0.132	0.0924	0.387	0.385	0.385	0.384	1.541
89.333	21.452	1.029	0.219	0.98	0.429	0.981	0.259	0.655	0.292	0.0576	0.0381	0.131	0.0921	0.385	0.383	0.383	0.382	1.533
89.417	21.389	1.023	0.217	0.975	0.427	0.977	0.258	0.651	0.29	0.0573	0.0379	0.131	0.0918	0.382	0.381	0.381	0.38	1.524
89.5	21.327	1.017	0.216	0.97	0.424	0.972	0.257	0.647	0.288	0.0571	0.0378	0.13	0.0915	0.38	0.379	0.379	0.378	1.516
89.583	21.264	1.012	0.215	0.965	0.422	0.968	0.255	0.644	0.287	0.0569	0.0377	0.13	0.0913	0.378	0.377	0.377	0.375	1.507
89.667	21.201	1.006	0.213	0.96	0.42	0.963	0.254	0.64	0.285	0.0567	0.0376	0.129	0.0911	0.376	0.375	0.375	0.373	1.499
89.75	21.138	1.001	0.212	0.954	0.417	0.959	0.252	0.636	0.284	0.0564	0.0375	0.129	0.0909	0.374	0.373	0.373	0.371	1.491
89.833	21.076	0.995	0.211	0.949	0.415	0.954	0.251	0.632	0.282	0.0563	0.0374	0.129	0.0908	0.372	0.371	0.371	0.369	1.483
89.917	21.013	0.99	0.21	0.944	0.413	0.95	0.25	0.629	0.28	0.0561	0.0373	0.128	0.0907	0.37	0.369	0.369	0.367	1.475
90	20.95	0.985	0.208	0.939	0.411	0.946	0.248	0.625	0.279	0.0559	0.0372	0.128	0.0905	0.368	0.367	0.367	0.365	1.467
90.083	20.887	0.98	0.207	0.934	0.408	0.941	0.247	0.622	0.277	0.0558	0.0372	0.128	0.0905	0.366	0.365	0.365	0.363	1.459
90.167	20.825	0.974	0.206	0.929	0.406	0.937	0.246	0.618	0.276	0.0556	0.0371	0.127	0.0905	0.364	0.363	0.363	0.361	1.451
90.25	20.762	0.969	0.205	0.924	0.404	0.933	0.244	0.614	0.274	0.0555	0.0371	0.127	0.0904	0.362	0.361	0.361	0.359	1.443
90.333	20.699	0.964	0.204	0.919	0.402	0.929	0.243	0.611	0.273	0.0554	0.037	0.127	0.0904	0.36	0.359	0.359	0.357	1.435
90.417	20.636	0.959	0.203	0.914	0.4	0.924	0.242	0.608	0.271	0.0553	0.037	0.127	0.0904	0.359	0.357	0.357	0.356	1.429
90.5	20.573	0.954	0.202	0.909	0.398	0.92	0.241	0.604	0.27	0.0552	0.0369	0.126	0.0904	0.357	0.355	0.355	0.354	1.421
90.583	20.51	0.949	0.201	0.905	0.396	0.916	0.239	0.601	0.269	0.0551	0.0369	0.126	0.0904	0.355	0.354	0.353	0.352	1.414
90.667	20.447	0.944	0.2	0.9	0.394	0.912	0.238	0.598	0.267	0.055	0.0369	0.126	0.0904	0.353	0.352	0.351	0.35	1.406
90.75	20.385	0.939	0.199	0.896	0.392	0.907	0.237	0.595	0.266	0.0549	0.0369	0.126	0.0904	0.351	0.35	0.349	0.348	1.398
90.833	20.322	0.935	0.199	0.891	0.39	0.903	0.236	0.591	0.264	0.0547	0.0369	0.125	0.0903	0.349	0.348	0.348	0.346	1.391
90.917	20.259	0.93	0.198	0.887	0.388	0.899	0.234	0.588	0.263	0.0546	0.0368	0.125	0.0901	0.348	0.346	0.346	0.345	1.385
91	20.196	0.925	0.197	0.882	0.386	0.894	0.233	0.585	0.261	0.0545	0.0368	0.125	0.09	0.346	0.345	0.344	0.343	1.378
91.083	20.133	0.92	0.196	0.878	0.384	0.89	0.232	0.582	0.26	0.0544	0.0366	0.125	0.0895	0.344	0.343	0.342	0.341	1.37
91.167	20.07	0.916	0.195	0.873	0.382	0.886	0.231	0.579	0.259	0.0542	0.0365	0.124	0.089	0.342	0.341	0.341	0.339	1.363
91.25	20.007	0.911	0.195	0.869	0.38	0.881	0.23	0.576	0.257	0.054	0.0364	0.124	0.0885	0.341	0.339	0.339	0.338	1.357
91.333	19.945	0.906	0.194	0.865	0.378	0.877	0.228	0.573	0.256	0.0538	0.0361	0.123	0.0877	0.339	0.338	0.337	0.336	1.35
91.417	19.882	0.902	0.193	0.86	0.376	0.873	0.227	0.57	0.254	0.0536	0.0359	0.123	0.0869	0.337	0.336	0.336	0.334	1.343
91.5	19.819	0.897	0.192	0.856	0.374	0.868	0.226	0.567	0.253	0.0534	0.0357	0.122	0.0861	0.336	0.334	0.334	0.332	1.336
91.583	19.756	0.893	0.192	0.852	0.372	0.864	0.225	0.564	0.252	0.0531	0.0354	0.122	0.0853	0.334	0.333	0.332	0.331	1.33
91.667	19.694	0.888	0.191	0.847	0.37	0.859	0.224	0.561	0.25	0.0529	0.0351	0.121	0.0845	0.332	0.331	0.33	0.329	1.322
91.75	19.631	0.883	0.19	0.843	0.368	0.855	0.223	0.558	0.249	0.0526	0.0348	0.12	0.0838	0.331	0.329	0.329	0.327	1.316
91.833	19.568	0.879	0.19	0.839	0.366	0.851	0.222	0.555	0.248	0.0523	0.0346	0.12	0.0832	0.329	0.328	0.327	0.326	1.31
91.917	19.506	0.874	0.189	0.835	0.364	0.846	0.22	0.552	0.246	0.052	0.0343	0.119	0.0826	0.327	0.326	0.325	0.324	1.302
92	19.443	0.87	0.188	0.831	0.362	0.842	0.219	0.55	0.245	0.0518	0.0341	0.118	0.0821	0.326	0.324	0.324	0.322	1.296
92.083	19.38	0.866	0.188	0.827	0.36	0.838	0.218	0.547	0.244	0.0515	0.0339	0.117	0.0817	0.324	0.323	0.322	0.321	1.29
92.167	19.318	0.861	0.187	0.822	0.359	0.833	0.217	0.544	0.243	0.0512	0.0337	0.117	0.0813	0.322	0.321	0.321	0.319	1.283
92.25	19.255	0.857	0.186	0.818	0.357	0.829	0.216	0.541	0.241	0.0509	0.0335	0.116	0.0809	0.321	0.319	0.319	0.318	1.277
92.333	19.193	0.852	0.185	0.814	0.355	0.825	0.215	0.539	0.24	0.0506	0.0333	0.116	0.0806	0.319	0.318	0.317	0.316	1.27
92.417	19.13	0.848	0.184	0.81	0.353	0.821	0.214	0.536	0.239	0.0504	0.0332	0.115	0.0803	0.317	0.316	0.316	0.314	1.263
92.5	19.068	0.844	0.184	0.806	0.351	0.816	0.213	0.534	0.238	0.0501	0.0331	0.114	0.08	0.316	0.315	0.314	0.313	1.258
92.583	19.006	0.839	0.183	0.802	0.349	0.812	0.212	0.531	0.237	0.0499	0.033	0.114	0.0798	0.314	0.313	0.313	0.311	1.251
92.667	18.943	0.835	0.182	0.798	0.348	0.808	0.211	0.528	0.235	0.0497	0.0328	0.113	0.0796	0.313	0.311	0.311	0.31	1.245
92.75	18.881	0.831	0.181	0.794	0.346	0.804	0.209	0.526	0.234	0.0495	0.0327	0.113	0.0794	0.311	0.31	0.309	0.308	1.238
92.833	18.819	0.827	0.18	0.79	0.344	0.8	0.208	0.523	0.233	0.0493	0.0327	0.113	0.0792	0.31	0.308	0.308	0.306	1.232
92.917	18.757	0.822	0.179	0.786	0.342	0.796	0.207	0.521	0.232	0.0491	0.0326	0.112	0.0791	0.308	0.307	0.306	0.305	1.226
93	18.695	0.818	0.178	0.782	0.341	0.792	0.206	0.518	0.231	0.049	0.0325	0.112	0.079	0.306	0.305	0.305	0.303	1.219
93.083	18.633	0.814	0.178	0.778	0.339	0.788	0.205	0.516	0.23	0.0488	0.0324	0.112	0.079	0.305	0.304	0.303	0.302	1.214
93.167	18.571	0.81	0.177	0.774	0.337	0.784	0.204	0.514	0.229	0.0487	0.0324	0.111	0.0789	0.303	0.302	0.302	0.3	1.207
93.25	18.508	0.806	0.176	0.77	0.336	0.78	0.203	0.511	0.227	0.0485	0.0323	0.111	0.0789	0.302	0.301	0.3	0.299	1.202
93.333	18.447	0.802	0.175	0.767	0.334	0.776	0.202	0.509	0.226	0.0484	0.0323	0.111	0.0789	0.3	0.299	0.299	0.297	1.195
93.417	18.385	0.798	0.175	0.763	0.333	0.772	0.201	0.506	0.225	0.0483	0.0322	0.111	0.0789	0.299	0.298	0.297	0.296	1.19
93.5	18.323	0.795	0.174	0.759	0.331	0.768	0.2	0.504	0.224	0.0482	0.0322	0.11	0.0789	0.297	0.296	0.296	0.294	1.183
93.583	18.262	0.791	0.173	0.756	0.329	0.765	0.199	0.502	0.223	0.0481	0.0322	0.11	0.0789	0.296	0.295	0.294	0.293	1.178
93.667	18.2	0.787	0.173	0.752	0.328	0.761	0.198	0.499	0.222	0.048	0.0322	0.11	0.0789	0.295	0.293	0.293	0.291	1.172
93.75	18.139	0.783	0.172	0.748	0.326	0.757	0.197	0.497	0.221	0.0479	0.0321	0.11	0.0789	0.293	0.292	0.291	0.29	1.166
93.833	18.077	0.78	0.171	0.745	0.325	0.753	0.197	0.494	0.22	0.0478	0.0321	0.11	0.0787	0.292	0.291	0.29	0.289	1.162
93.917	18.016	0.776	0.171	0.741	0.323	0.749	0.196	0.492	0.219	0.0476	0.0321	0.109	0.0786	0.29	0.289	0.289	0.287	1.155
94	17.955	0.772	0.17	0.738	0.322	0.746	0.195	0.49	0.218	0.0475	0.032	0.109	0.0784	0.289	0.288	0.288	0.287	0.286	1.15
94.083	17.893	0.769	0.17	0.734	0.32	0.742	0.194	0.487	0.217	0.0474	0.0319	0.109	0.078	0.288	0.286	0.286	0.284	1.144

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
94.167	17.832	0.765	0.169	0.731	0.319	0.738	0.193	0.485	0.216	0.0472	0.0318	0.108	0.0775	0.286	0.285	0.284	0.283	1.138
94.25	17.771	0.761	0.168	0.727	0.317	0.734	0.192	0.483	0.215	0.0471	0.0316	0.108	0.0771	0.285	0.284	0.283	0.282	1.134
94.333	17.71	0.758	0.168	0.724	0.316	0.731	0.191	0.481	0.213	0.0469	0.0314	0.108	0.0763	0.284	0.282	0.282	0.28	1.128
94.417	17.649	0.754	0.167	0.721	0.314	0.727	0.19	0.478	0.212	0.0466	0.0312	0.107	0.0755	0.282	0.281	0.28	0.279	1.122
94.5	17.588	0.751	0.166	0.717	0.313	0.723	0.189	0.476	0.211	0.0464	0.031	0.107	0.0747	0.281	0.28	0.279	0.278	1.118
94.583	17.528	0.747	0.166	0.714	0.311	0.72	0.188	0.474	0.21	0.0462	0.0307	0.106	0.074	0.28	0.278	0.278	0.276	1.112
94.667	17.467	0.743	0.165	0.71	0.309	0.716	0.187	0.472	0.209	0.046	0.0304	0.105	0.0732	0.278	0.277	0.276	0.275	1.106
94.75	17.407	0.74	0.164	0.707	0.308	0.712	0.186	0.47	0.208	0.0457	0.0301	0.105	0.0724	0.277	0.276	0.275	0.274	1.102
94.833	17.347	0.736	0.164	0.704	0.306	0.708	0.186	0.467	0.207	0.0454	0.0299	0.104	0.0718	0.276	0.274	0.274	0.272	1.096
94.917	17.286	0.733	0.163	0.7	0.305	0.705	0.185	0.465	0.206	0.0451	0.0296	0.103	0.0713	0.274	0.273	0.272	0.271	1.09
95	17.226	0.729	0.162	0.697	0.303	0.701	0.184	0.463	0.205	0.0448	0.0294	0.102	0.0707	0.273	0.272	0.271	0.27	1.086
95.083	17.166	0.725	0.162	0.694	0.302	0.698	0.183	0.461	0.204	0.0445	0.0292	0.102	0.0703	0.272	0.27	0.27	0.268	1.08
95.167	17.106	0.722	0.161	0.691	0.3	0.694	0.182	0.459	0.203	0.0442	0.029	0.101	0.0698	0.27	0.269	0.269	0.267	1.075
95.25	17.046	0.718	0.16	0.687	0.299	0.69	0.181	0.457	0.202	0.0439	0.0288	0.1	0.0694	0.269	0.268	0.267	0.266	1.07
95.333	16.987	0.715	0.159	0.684	0.297	0.687	0.18	0.455	0.201	0.0437	0.0286	0.1	0.0691	0.268	0.266	0.266	0.264	1.064
95.417	16.927	0.711	0.159	0.681	0.296	0.683	0.179	0.453	0.2	0.0434	0.0285	0.1	0.0688	0.266	0.265	0.265	0.263	1.059
95.5	16.867	0.707	0.158	0.677	0.294	0.68	0.178	0.451	0.199	0.0432	0.0283	0.1	0.0685	0.265	0.264	0.263	0.262	1.054
95.583	16.808	0.704	0.157	0.674	0.293	0.676	0.177	0.449	0.198	0.043	0.0282	0.1	0.0683	0.264	0.263	0.262	0.261	1.05
95.667	16.749	0.7	0.156	0.671	0.291	0.673	0.177	0.447	0.197	0.0427	0.0281	0.1	0.0681	0.263	0.261	0.261	0.259	1.044
95.75	16.689	0.697	0.155	0.667	0.29	0.67	0.176	0.445	0.196	0.0425	0.028	0.1	0.0679	0.261	0.26	0.259	0.258	1.038
95.833	16.631	0.693	0.154	0.664	0.289	0.666	0.175	0.443	0.195	0.0424	0.0279	0.1	0.0677	0.26	0.259	0.258	0.257	1.034
95.917	16.572	0.69	0.154	0.661	0.287	0.663	0.174	0.441	0.195	0.0422	0.0278	0.1	0.0676	0.259	0.257	0.257	0.255	1.028
96	16.513	0.687	0.153	0.658	0.286	0.659	0.173	0.44	0.194	0.042	0.0277	0.1	0.0675	0.257	0.256	0.256	0.254	1.023
96.083	16.454	0.683	0.152	0.654	0.284	0.656	0.172	0.438	0.193	0.0418	0.0277	0.1	0.0674	0.256	0.255	0.254	0.253	1.018
96.167	16.396	0.68	0.151	0.651	0.283	0.653	0.171	0.436	0.192	0.0417	0.0276	0.1	0.0674	0.255	0.254	0.253	0.252	1.014
96.25	16.337	0.677	0.15	0.648	0.282	0.65	0.17	0.434	0.191	0.0416	0.0276	0.1	0.0673	0.254	0.252	0.252	0.25	1.008
96.333	16.279	0.673	0.15	0.645	0.28	0.646	0.17	0.432	0.19	0.0414	0.0275	0.1	0.0673	0.252	0.251	0.251	0.249	1.003
96.417	16.221	0.67	0.149	0.642	0.279	0.643	0.169	0.43	0.189	0.0413	0.0275	0.1	0.0673	0.251	0.25	0.249	0.248	0.998
96.5	16.163	0.667	0.148	0.639	0.278	0.64	0.168	0.428	0.188	0.0412	0.0274	0.1	0.0673	0.25	0.249	0.248	0.247	0.994
96.583	16.105	0.663	0.147	0.636	0.276	0.637	0.167	0.426	0.187	0.0411	0.0274	0.1	0.0673	0.249	0.247	0.247	0.245	0.988
96.667	16.048	0.66	0.147	0.633	0.275	0.633	0.166	0.425	0.187	0.041	0.0274	0.1	0.0673	0.247	0.246	0.246	0.244	0.983
96.75	15.99	0.657	0.146	0.629	0.274	0.63	0.166	0.423	0.186	0.0409	0.0274	0.1	0.0673	0.246	0.245	0.244	0.243	0.978
96.833	15.933	0.654	0.146	0.627	0.273	0.627	0.165	0.421	0.185	0.0408	0.0274	0.1	0.0673	0.245	0.244	0.243	0.242	0.974
96.917	15.875	0.651	0.145	0.624	0.271	0.624	0.164	0.419	0.184	0.0407	0.0274	0.1	0.0673	0.244	0.243	0.242	0.241	0.97
97	15.818	0.648	0.144	0.621	0.27	0.621	0.163	0.417	0.183	0.0406	0.0274	0.1	0.0673	0.243	0.241	0.241	0.239	0.964
97.083	15.761	0.645	0.144	0.618	0.269	0.618	0.162	0.415	0.182	0.0406	0.0274	0.1	0.0673	0.242	0.24	0.24	0.238	0.96
97.167	15.704	0.642	0.143	0.615	0.268	0.615	0.162	0.413	0.182	0.0405	0.0274	0.1	0.0673	0.24	0.239	0.239	0.237	0.955
97.25	15.648	0.639	0.143	0.612	0.266	0.612	0.161	0.412	0.181	0.0404	0.0274	0.1	0.0673	0.239	0.238	0.237	0.236	0.95
97.333	15.591	0.636	0.142	0.609	0.265	0.609	0.16	0.41	0.18	0.0404	0.0274	0.1	0.0673	0.238	0.237	0.236	0.235	0.946
97.417	15.535	0.633	0.142	0.606	0.264	0.606	0.159	0.408	0.179	0.0403	0.0274	0.1	0.0673	0.237	0.236	0.235	0.234	0.942
97.5	15.479	0.63	0.142	0.603	0.263	0.603	0.159	0.406	0.178	0.0403	0.0274	0.1	0.0673	0.236	0.235	0.234	0.233	0.938
97.583	15.423	0.627	0.141	0.601	0.262	0.6	0.158	0.405	0.177	0.0402	0.0274	0.1	0.0673	0.235	0.233	0.233	0.231	0.932
97.667	15.367	0.624	0.141	0.598	0.26	0.597	0.157	0.403	0.177	0.0402	0.0274	0.1	0.0673	0.234	0.232	0.232	0.23	0.928
97.75	15.311	0.622	0.14	0.595	0.259	0.594	0.156	0.402	0.176	0.0401	0.0274	0.1	0.0673	0.233	0.231	0.231	0.229	0.924
97.833	15.256	0.619	0.14	0.592	0.258	0.591	0.156	0.4	0.175	0.0401	0.0274	0.1	0.0673	0.232	0.23	0.23	0.228	0.92
97.917	15.2	0.616	0.14	0.59	0.257	0.588	0.155	0.399	0.174	0.0401	0.0274	0.1	0.0673	0.23	0.229	0.229	0.227	0.915
98	15.145	0.613	0.14	0.587	0.256	0.585	0.154	0.397	0.174	0.0401	0.0274	0.1	0.0673	0.229	0.228	0.228	0.226	0.911
98.083	15.09	0.61	0.139	0.584	0.255	0.582	0.154	0.396	0.173	0.0401	0.0274	0.1	0.0673	0.228	0.227	0.227	0.225	0.907
98.167	15.035	0.608	0.139	0.582	0.253	0.579	0.153	0.394	0.172	0.0401	0.0274	0.1	0.0673	0.227	0.226	0.225	0.224	0.902
98.25	14.98	0.605	0.139	0.579	0.252	0.577	0.152	0.393	0.172	0.0401	0.0274	0.1	0.0673	0.226	0.225	0.224	0.223	0.898
98.333	14.926	0.602	0.139	0.576	0.251	0.574	0.152	0.392	0.171	0.0401	0.0274	0.1	0.0673	0.225	0.224	0.223	0.222	0.894
98.417	14.872	0.6	0.138	0.574	0.25	0.571	0.151	0.39	0.17	0.0401	0.0274	0.1	0.0673	0.224	0.223	0.222	0.221	0.89
98.5	14.817	0.597	0.138	0.571	0.249	0.568	0.15	0.389	0.17	0.0401	0.0274	0.1	0.0673	0.223	0.222	0.221	0.22	0.886
98.583	14.763	0.594	0.138	0.569	0.248	0.566	0.15	0.388	0.169	0.0401	0.0274	0.1	0.0673	0.222	0.221	0.22	0.219	0.882
98.667	14.71	0.592	0.138	0.566	0.247	0.563	0.149	0.387	0.169	0.0401	0.0274	0.1	0.0673	0.221	0.22	0.219	0.218	0.878
98.75	14.656	0.589	0.137	0.564	0.246	0.561	0.148	0.386	0.168	0.0401	0.0274	0.1	0.0673	0.22	0.219	0.218	0.217	0.874
98.833	14.602	0.587	0.137	0.561	0.245	0.558	0.148	0.384	0.167	0.0401	0.0274	0.1	0.0673	0.219	0.218	0.217	0.216	0.87
98.917	14.549	0.584	0.137	0.559	0.244	0.556	0.147	0.383	0.167	0.0401	0.0274	0.1	0.0673	0.218	0.217	0.216	0.215	0.866
99	14.496	0.582	0.137	0.556	0.243	0.553	0.146	0.382	0.166	0.0401	0.0274	0.1	0.0673	0.217	0.216	0.215	0.214	0.862
99.083	14.443	0.58	0.137	0.554	0.242	0.551	0.146	0.381	0.166	0.0401	0.0274	0.1	0.0673	0.216	0.215	0.214	0.213	0.858
99.167	14.39	0.577	0.136	0.551	0.241	0.548	0.145	0.38	0.165	0.0401	0.0274	0.1	0.0673	0.215	0.214	0.214	0.212	0.855
99.25	14.337	0.575	0.136	0.549	0.241	0.546	0.145	0.379	0.165	0.0401	0.0274	0.1	0.0673	0.214	0.213	0.213	0.211	0.851
99.333	14.285	0.573	0.136	0.547	0.24	0.543	0.144	0.378	0.164	0.0401	0.0274	0.1	0.0673	0.214	0.212	0.212	0.21	0.848

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
99.417	14.232	0.571	0.136	0.544	0.239	0.541	0.143	0.378	0.164	0.0401	0.0274	0.1	0.0673	0.213	0.211	0.211	0.209	0.844
99.5	14.18	0.568	0.136	0.542	0.238	0.539	0.143	0.377	0.163	0.0401	0.0274	0.1	0.0673	0.212	0.21	0.21	0.208	0.84
99.583	14.128	0.566	0.136	0.54	0.237	0.536	0.142	0.376	0.163	0.0401	0.0274	0.1	0.0673	0.211	0.21	0.209	0.207	0.837
99.667	14.077	0.564	0.136	0.538	0.237	0.534	0.142	0.375	0.162	0.0401	0.0274	0.1	0.0673	0.21	0.209	0.208	0.207	0.834
99.75	14.025	0.562	0.135	0.536	0.236	0.532	0.141	0.374	0.162	0.0401	0.0274	0.1	0.0673	0.209	0.208	0.207	0.206	0.83
99.833	13.974	0.56	0.135	0.534	0.235	0.53	0.141	0.373	0.161	0.0401	0.0274	0.1	0.0673	0.208	0.207	0.207	0.205	0.827
99.917	13.922	0.558	0.135	0.532	0.234	0.528	0.14	0.373	0.161	0.0401	0.0274	0.1	0.0673	0.208	0.206	0.206	0.204	0.824
100	13.871	0.556	0.135	0.53	0.234	0.525	0.14	0.372	0.161	0.0401	0.0274	0.1	0.0673	0.207	0.206	0.205	0.203	0.821
100.083	13.82	0.555	0.135	0.528	0.233	0.523	0.139	0.371	0.16	0.0401	0.0274	0.1	0.0673	0.206	0.205	0.204	0.203	0.818
100.167	13.77	0.553	0.135	0.526	0.232	0.521	0.139	0.371	0.16	0.0401	0.0274	0.1	0.0673	0.205	0.204	0.204	0.202	0.815
100.25	13.719	0.551	0.135	0.524	0.232	0.519	0.138	0.37	0.159	0.0401	0.0274	0.1	0.0673	0.205	0.203	0.203	0.201	0.812
100.333	13.668	0.549	0.135	0.522	0.231	0.517	0.138	0.369	0.159	0.0401	0.0274	0.1	0.0673	0.204	0.203	0.202	0.2	0.809
100.417	13.618	0.548	0.135	0.52	0.23	0.515	0.137	0.369	0.159	0.0401	0.0274	0.1	0.0673	0.203	0.202	0.201	0.2	0.806
100.5	13.568	0.546	0.135	0.518	0.23	0.513	0.137	0.368	0.158	0.0401	0.0274	0.1	0.0673	0.203	0.201	0.201	0.199	0.804
100.583	13.518	0.544	0.135	0.517	0.229	0.511	0.137	0.367	0.158	0.0401	0.0274	0.1	0.0673	0.202	0.2	0.2	0.198	0.8
100.667	13.469	0.543	0.135	0.515	0.229	0.509	0.136	0.367	0.157	0.0401	0.0274	0.1	0.0673	0.201	0.2	0.199	0.198	0.798
100.75	13.419	0.541	0.135	0.513	0.228	0.507	0.136	0.366	0.157	0.0401	0.0274	0.1	0.0673	0.201	0.199	0.199	0.197	0.796
100.833	13.37	0.54	0.135	0.512	0.227	0.505	0.135	0.366	0.157	0.0401	0.0274	0.1	0.0673	0.2	0.198	0.198	0.196	0.792
100.917	13.321	0.538	0.135	0.51	0.227	0.503	0.135	0.365	0.156	0.0401	0.0274	0.1	0.0673	0.199	0.198	0.197	0.196	0.79
101	13.272	0.537	0.135	0.508	0.226	0.501	0.135	0.365	0.156	0.0401	0.0274	0.1	0.0673	0.199	0.197	0.197	0.195	0.788
101.083	13.223	0.536	0.135	0.507	0.226	0.499	0.134	0.364	0.156	0.0401	0.0274	0.1	0.0673	0.198	0.197	0.196	0.194	0.785
101.167	13.174	0.534	0.135	0.505	0.225	0.497	0.134	0.364	0.156	0.0401	0.0274	0.1	0.0673	0.197	0.196	0.195	0.194	0.782
101.25	13.126	0.533	0.135	0.504	0.225	0.495	0.134	0.363	0.155	0.0401	0.0274	0.1	0.0673	0.197	0.195	0.195	0.193	0.78
101.333	13.077	0.532	0.135	0.502	0.224	0.494	0.133	0.363	0.155	0.0401	0.0274	0.1	0.0673	0.196	0.195	0.194	0.193	0.778
101.417	13.029	0.53	0.135	0.501	0.224	0.492	0.133	0.362	0.155	0.0401	0.0274	0.1	0.0673	0.196	0.194	0.194	0.192	0.776
101.5	12.981	0.529	0.135	0.5	0.223	0.49	0.133	0.362	0.154	0.0401	0.0274	0.1	0.0673	0.195	0.194	0.193	0.192	0.774
101.583	12.933	0.528	0.135	0.498	0.223	0.489	0.132	0.362	0.154	0.0401	0.0274	0.1	0.0673	0.195	0.193	0.193	0.191	0.772
101.667	12.886	0.527	0.135	0.497	0.222	0.487	0.132	0.361	0.154	0.0401	0.0274	0.1	0.0673	0.194	0.193	0.192	0.191	0.77
101.75	12.838	0.526	0.135	0.495	0.222	0.485	0.132	0.361	0.154	0.0401	0.0274	0.1	0.0673	0.193	0.192	0.192	0.19	0.767
101.833	12.791	0.524	0.135	0.494	0.222	0.484	0.131	0.361	0.153	0.0401	0.0274	0.1	0.0673	0.193	0.192	0.191	0.189	0.765
101.917	12.744	0.523	0.135	0.493	0.221	0.482	0.131	0.36	0.153	0.0401	0.0274	0.1	0.0673	0.193	0.191	0.191	0.189	0.764
102	12.696	0.522	0.135	0.492	0.221	0.481	0.131	0.36	0.153	0.0401	0.0274	0.1	0.0673	0.192	0.191	0.19	0.188	0.761
102.083	12.65	0.521	0.135	0.49	0.22	0.479	0.13	0.36	0.153	0.0401	0.0274	0.1	0.0673	0.192	0.19	0.19	0.188	0.76
102.167	12.603	0.52	0.135	0.489	0.22	0.478	0.13	0.359	0.153	0.0401	0.0274	0.1	0.0673	0.191	0.19	0.189	0.188	0.758
102.25	12.556	0.519	0.135	0.488	0.22	0.477	0.13	0.359	0.152	0.0401	0.0274	0.1	0.0673	0.191	0.189	0.189	0.187	0.756
102.333	12.51	0.518	0.135	0.487	0.219	0.475	0.13	0.359	0.152	0.0401	0.0274	0.1	0.0673	0.19	0.189	0.188	0.187	0.754
102.417	12.464	0.517	0.135	0.486	0.219	0.474	0.129	0.359	0.152	0.0401	0.0274	0.1	0.0673	0.19	0.188	0.188	0.186	0.752
102.5	12.418	0.516	0.135	0.485	0.218	0.473	0.129	0.358	0.152	0.0401	0.0274	0.1	0.0673	0.189	0.188	0.187	0.186	0.75
102.583	12.372	0.515	0.135	0.484	0.218	0.471	0.129	0.358	0.152	0.0401	0.0274	0.1	0.0673	0.189	0.188	0.187	0.185	0.749
102.667	12.326	0.514	0.135	0.483	0.218	0.47	0.129	0.358	0.151	0.0401	0.0274	0.1	0.0673	0.189	0.187	0.187	0.185	0.748
102.75	12.281	0.513	0.135	0.482	0.217	0.469	0.128	0.358	0.151	0.0401	0.0274	0.1	0.0673	0.188	0.187	0.186	0.185	0.746
102.833	12.236	0.513	0.135	0.481	0.217	0.468	0.128	0.357	0.151	0.04	0.0273	0.1	0.0672	0.188	0.186	0.186	0.184	0.744
102.917	12.19	0.512	0.135	0.48	0.217	0.466	0.128	0.357	0.151	0.04	0.0273	0.1	0.0671	0.187	0.186	0.185	0.184	0.742
103	12.145	0.511	0.134	0.479	0.217	0.465	0.128	0.357	0.151	0.04	0.0273	0.1	0.067	0.187	0.186	0.185	0.183	0.741
103.083	12.1	0.51	0.134	0.478	0.216	0.464	0.128	0.357	0.15	0.0399	0.0272	0.1	0.0667	0.187	0.185	0.185	0.183	0.74
103.167	12.056	0.509	0.134	0.477	0.216	0.463	0.127	0.356	0.15	0.0399	0.0271	0.1	0.0663	0.186	0.185	0.184	0.183	0.738
103.25	12.011	0.508	0.134	0.476	0.216	0.462	0.127	0.356	0.15	0.0398	0.027	0.1	0.0659	0.186	0.185	0.184	0.182	0.737
103.333	11.967	0.507	0.134	0.475	0.215	0.461	0.127	0.356	0.15	0.0397	0.0268	0.1	0.0653	0.186	0.184	0.184	0.182	0.736
103.417	11.922	0.507	0.134	0.474	0.215	0.459	0.127	0.355	0.15	0.0395	0.0266	0.1	0.0646	0.185	0.184	0.183	0.182	0.734
103.5	11.878	0.506	0.134	0.473	0.215	0.458	0.126	0.355	0.149	0.0394	0.0264	0.1	0.0639	0.185	0.183	0.183	0.181	0.732
103.583	11.834	0.505	0.133	0.472	0.214	0.457	0.126	0.354	0.149	0.0392	0.0262	0.1	0.0631	0.184	0.183	0.183	0.181	0.731
103.667	11.791	0.504	0.133	0.471	0.214	0.456	0.126	0.354	0.149	0.039	0.0259	0.1	0.0623	0.184	0.183	0.182	0.181	0.73
103.75	11.747	0.503	0.133	0.47	0.214	0.455	0.126	0.354	0.149	0.0388	0.0256	0.1	0.0616	0.184	0.182	0.182	0.18	0.728
103.833	11.704	0.502	0.133	0.47	0.213	0.454	0.126	0.353	0.149	0.0386	0.0254	0.1	0.0609	0.183	0.182	0.181	0.18	0.726
103.917	11.66	0.501	0.132	0.469	0.213	0.453	0.125	0.353	0.148	0.0383	0.0251	0.1	0.0603	0.183	0.182	0.181	0.179	0.725
104	11.617	0.5	0.132	0.468	0.212	0.452	0.125	0.352	0.148	0.038	0.0248	0.1	0.0596	0.183	0.181	0.181	0.179	0.724
104.083	11.574	0.499	0.131	0.467	0.212	0.451	0.125	0.351	0.148	0.0378	0.0246	0.1	0.0591	0.182	0.181	0.18	0.179	0.722
104.167	11.531	0.499	0.131	0.466	0.212	0.45	0.125	0.351	0.148	0.0375	0.0244	0.1	0.0587	0.182	0.181	0.18	0.178	0.721
104.25	11.488	0.498	0.13	0.465	0.211	0.448	0.124	0.35	0.147	0.0372	0.0242	0.1	0.0582	0.182	0.18	0.18	0.178	0.72
104.333	11.446	0.497	0.13	0.464	0.211	0.447	0.124	0.35	0.147	0.0369	0.024	0.1	0.0579	0.181	0.18	0.179	0.178	0.718
104.417	11.403	0.496	0.129	0.463	0.211	0.446	0.124	0.349	0.147	0.0367	0.0239	0.1	0.0575	0.181	0.179	0.179	0.177	0.716
104.5	11.361	0.495	0.129	0.462	0.21	0.445	0.124	0.348	0.147	0.0364	0.0237	0.1	0.0572	0.181	0.179	0.179	0.177	0.716
104.583	11.319	0.494	0.128	0.461	0.21	0.444	0.123	0.348	0.146	0.0362	0.0236	0.1	0.057	0.18	0.179	0.178	0.177	0.714

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
104.667	11.277	0.493	0.128	0.46	0.209	0.443	0.123	0.347	0.146	0.0359	0.0235	0.1	0.0567	0.18	0.178	0.178	0.176	0.712
104.75	11.235	0.492	0.127	0.459	0.209	0.442	0.123	0.346	0.146	0.0357	0.0233	0.1	0.0565	0.179	0.178	0.178	0.176	0.711
104.833	11.194	0.491	0.126	0.459	0.209	0.441	0.123	0.345	0.145	0.0355	0.0233	0.1	0.0563	0.179	0.178	0.177	0.175	0.709
104.917	11.152	0.49	0.126	0.458	0.208	0.44	0.122	0.345	0.145	0.0353	0.0232	0.1	0.0562	0.179	0.177	0.177	0.175	0.708
105	11.111	0.489	0.125	0.457	0.208	0.439	0.122	0.344	0.145	0.0351	0.0231	0.1	0.056	0.178	0.177	0.176	0.175	0.706
105.083	11.07	0.488	0.124	0.456	0.207	0.438	0.122	0.343	0.145	0.035	0.023	0.1	0.0559	0.178	0.177	0.176	0.174	0.705
105.167	11.029	0.487	0.124	0.455	0.207	0.437	0.122	0.342	0.144	0.0348	0.0229	0.1	0.0559	0.178	0.176	0.176	0.174	0.704
105.25	10.987	0.486	0.123	0.454	0.207	0.436	0.121	0.341	0.144	0.0347	0.0228	0.1	0.0558	0.177	0.176	0.175	0.174	0.702
105.333	10.947	0.485	0.123	0.453	0.206	0.435	0.121	0.34	0.144	0.0345	0.0228	0.1	0.0558	0.177	0.175	0.175	0.173	0.7
105.417	10.906	0.484	0.122	0.452	0.206	0.435	0.121	0.339	0.143	0.0344	0.0228	0.1	0.0558	0.176	0.175	0.175	0.173	0.699
105.5	10.866	0.483	0.121	0.451	0.205	0.434	0.121	0.338	0.143	0.0343	0.0227	0.1	0.0557	0.176	0.175	0.174	0.172	0.697
105.583	10.825	0.482	0.121	0.45	0.205	0.433	0.12	0.337	0.143	0.0342	0.0227	0.1	0.0557	0.176	0.174	0.174	0.172	0.696
105.667	10.785	0.481	0.12	0.449	0.204	0.432	0.12	0.336	0.142	0.0341	0.0227	0.1	0.0557	0.175	0.174	0.173	0.172	0.694
105.75	10.745	0.48	0.12	0.448	0.204	0.431	0.12	0.335	0.142	0.034	0.0226	0.1	0.0557	0.175	0.173	0.173	0.171	0.692
105.833	10.705	0.479	0.119	0.447	0.203	0.43	0.12	0.334	0.142	0.0339	0.0226	0.1	0.0557	0.175	0.173	0.173	0.171	0.692
105.917	10.666	0.478	0.119	0.446	0.203	0.429	0.119	0.333	0.141	0.0338	0.0226	0.1	0.0557	0.174	0.173	0.172	0.171	0.69
106	10.626	0.477	0.118	0.445	0.202	0.428	0.119	0.332	0.141	0.0337	0.0226	0.1	0.0557	0.174	0.172	0.172	0.17	0.688
106.083	10.587	0.475	0.118	0.444	0.202	0.427	0.119	0.331	0.141	0.0336	0.0226	0.1	0.0557	0.173	0.172	0.171	0.17	0.686
106.167	10.547	0.474	0.117	0.443	0.202	0.426	0.118	0.33	0.14	0.0335	0.0226	0.1	0.0557	0.173	0.172	0.171	0.169	0.685
106.25	10.508	0.473	0.117	0.442	0.201	0.425	0.118	0.328	0.14	0.0335	0.0226	0.1	0.0557	0.173	0.171	0.171	0.169	0.684
106.333	10.469	0.472	0.117	0.441	0.201	0.424	0.118	0.327	0.139	0.0334	0.0226	0.1	0.0557	0.172	0.171	0.17	0.169	0.682
106.417	10.43	0.471	0.116	0.44	0.2	0.424	0.118	0.326	0.139	0.0334	0.0226	0.1	0.0557	0.172	0.17	0.17	0.168	0.68
106.5	10.391	0.47	0.116	0.439	0.2	0.423	0.117	0.325	0.139	0.0333	0.0226	0.1	0.0557	0.171	0.17	0.169	0.168	0.678
106.583	10.353	0.469	0.115	0.438	0.199	0.422	0.117	0.324	0.138	0.0333	0.0226	0.1	0.0557	0.171	0.17	0.169	0.167	0.677
106.667	10.314	0.468	0.115	0.437	0.199	0.421	0.117	0.323	0.138	0.0332	0.0226	0.1	0.0557	0.171	0.169	0.169	0.167	0.676
106.75	10.276	0.466	0.115	0.436	0.198	0.42	0.116	0.322	0.137	0.0332	0.0226	0.1	0.0557	0.17	0.169	0.168	0.167	0.674
106.833	10.238	0.465	0.114	0.435	0.197	0.419	0.116	0.321	0.137	0.0331	0.0226	0.1	0.0557	0.17	0.168	0.168	0.166	0.672
106.917	10.2	0.464	0.114	0.434	0.197	0.418	0.116	0.32	0.137	0.0331	0.0226	0.1	0.0557	0.169	0.168	0.167	0.166	0.67
107	10.162	0.463	0.114	0.433	0.196	0.417	0.116	0.319	0.136	0.0331	0.0226	0.1	0.0557	0.169	0.167	0.167	0.165	0.668
107.083	10.124	0.462	0.114	0.432	0.196	0.417	0.115	0.318	0.136	0.0331	0.0226	0.1	0.0557	0.168	0.167	0.167	0.165	0.667
107.167	10.087	0.46	0.113	0.431	0.195	0.416	0.115	0.317	0.135	0.0331	0.0226	0.1	0.0557	0.168	0.167	0.166	0.164	0.665
107.25	10.049	0.459	0.113	0.43	0.195	0.415	0.115	0.316	0.135	0.0331	0.0226	0.1	0.0557	0.168	0.166	0.166	0.164	0.664
107.333	10.012	0.458	0.113	0.428	0.194	0.414	0.114	0.315	0.135	0.033	0.0226	0.1	0.0557	0.167	0.166	0.165	0.164	0.662
107.417	9.974	0.457	0.113	0.427	0.194	0.413	0.114	0.314	0.134	0.033	0.0226	0.1	0.0557	0.167	0.165	0.165	0.163	0.66
107.5	9.937	0.455	0.112	0.426	0.193	0.412	0.114	0.313	0.134	0.033	0.0226	0.1	0.0557	0.166	0.165	0.164	0.163	0.658
107.583	9.9	0.454	0.112	0.425	0.193	0.411	0.113	0.313	0.134	0.033	0.0226	0.1	0.0557	0.166	0.164	0.164	0.162	0.656
107.667	9.863	0.453	0.112	0.424	0.192	0.41	0.113	0.312	0.133	0.033	0.0226	0.1	0.0557	0.165	0.164	0.163	0.162	0.654
107.75	9.827	0.452	0.112	0.423	0.192	0.41	0.113	0.311	0.133	0.033	0.0226	0.1	0.0557	0.165	0.164	0.163	0.161	0.653
107.833	9.79	0.451	0.111	0.422	0.191	0.409	0.113	0.31	0.133	0.033	0.0226	0.1	0.0557	0.165	0.163	0.163	0.161	0.652
107.917	9.754	0.449	0.111	0.421	0.191	0.408	0.112	0.309	0.132	0.033	0.0226	0.1	0.0557	0.164	0.163	0.162	0.16	0.649
108	9.717	0.448	0.111	0.42	0.19	0.407	0.112	0.309	0.132	0.033	0.0226	0.1	0.0557	0.164	0.162	0.162	0.16	0.648
108.083	9.681	0.447	0.111	0.418	0.19	0.406	0.112	0.308	0.132	0.033	0.0226	0.1	0.0557	0.163	0.162	0.161	0.16	0.646
108.167	9.645	0.446	0.111	0.417	0.189	0.405	0.111	0.307	0.131	0.033	0.0226	0.1	0.0557	0.163	0.161	0.161	0.159	0.644
108.25	9.609	0.445	0.11	0.416	0.189	0.405	0.111	0.307	0.131	0.033	0.0226	0.1	0.0557	0.162	0.161	0.16	0.159	0.642
108.333	9.574	0.444	0.11	0.415	0.188	0.404	0.111	0.306	0.131	0.033	0.0226	0.1	0.0557	0.162	0.16	0.16	0.158	0.64
108.417	9.538	0.443	0.11	0.414	0.188	0.403	0.111	0.305	0.13	0.033	0.0226	0.1	0.0557	0.161	0.16	0.16	0.158	0.639
108.5	9.503	0.441	0.11	0.413	0.187	0.402	0.11	0.305	0.13	0.033	0.0226	0.1	0.0557	0.161	0.16	0.159	0.157	0.637
108.583	9.467	0.44	0.11	0.412	0.187	0.401	0.11	0.304	0.13	0.033	0.0226	0.1	0.0557	0.161	0.159	0.159	0.157	0.636
108.667	9.432	0.439	0.11	0.411	0.186	0.4	0.11	0.303	0.13	0.033	0.0226	0.1	0.0557	0.16	0.159	0.158	0.157	0.634
108.75	9.397	0.438	0.11	0.41	0.186	0.4	0.109	0.303	0.129	0.033	0.0226	0.1	0.0557	0.16	0.158	0.158	0.156	0.632
108.833	9.362	0.437	0.109	0.409	0.186	0.399	0.109	0.302	0.129	0.033	0.0226	0.1	0.0557	0.159	0.158	0.158	0.156	0.631
108.917	9.327	0.436	0.109	0.408	0.185	0.398	0.109	0.302	0.129	0.033	0.0226	0.1	0.0557	0.159	0.158	0.157	0.155	0.629
109	9.292	0.435	0.109	0.407	0.185	0.397	0.109	0.301	0.128	0.033	0.0226	0.1	0.0557	0.159	0.157	0.157	0.155	0.628
109.083	9.258	0.434	0.109	0.406	0.185	0.396	0.108	0.301	0.128	0.033	0.0226	0.1	0.0557	0.158	0.157	0.156	0.155	0.626
109.167	9.223	0.433	0.109	0.405	0.184	0.395	0.108	0.3	0.128	0.033	0.0226	0.1	0.0557	0.158	0.157	0.156	0.154	0.625
109.25	9.189	0.433	0.109	0.404	0.184	0.395	0.108	0.3	0.128	0.033	0.0226	0.1	0.0557	0.158	0.156	0.156	0.154	0.624
109.333	9.155	0.432	0.109	0.403	0.183	0.394	0.108	0.299	0.127	0.033	0.0226	0.1	0.0557	0.157	0.156	0.155	0.154	0.622
109.417	9.121	0.431	0.109	0.403	0.183	0.393	0.108	0.299	0.127	0.033	0.0226	0.1	0.0557	0.157	0.156	0.155	0.153	0.621
109.5	9.087	0.43	0.109	0.402	0.183	0.392	0.107	0.298	0.127	0.033	0.0226	0.1	0.0557	0.157	0.155	0.155	0.153	0.62
109.583	9.053	0.429	0.109	0.401	0.182	0.391	0.107	0.298	0.127	0.033	0.0226	0.1	0.0557	0.156	0.155	0.154	0.153	0.618
109.667	9.019	0.428	0.109	0.4	0.182	0.39	0.107	0.297	0.127	0.033	0.0226	0.1	0.0557	0.156	0.155	0.154	0.152	0.617
109.75	8.985	0.427	0.109	0.399	0.182	0.389	0.107	0.297	0.126	0.033	0.0226	0.1	0.0557	0.156	0.154	0.154	0.152	0.616
109.833	8.952	0.427	0.109	0.398	0.181	0.389	0.106	0.296	0.126	0.033	0.0226	0.1	0.0557	0.155	0.154	0.153	0.152	0.614

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
109.917	8.919	0.426	0.109	0.398	0.181	0.388	0.106	0.296	0.126	0.033	0.0226	0.1	0.0557	0.155	0.154	0.153	0.151	0.613
110	8.885	0.425	0.109	0.397	0.181	0.387	0.106	0.296	0.126	0.033	0.0226	0.1	0.0557	0.155	0.153	0.153	0.151	0.612
110.083	8.852	0.424	0.109	0.396	0.18	0.386	0.106	0.295	0.126	0.033	0.0226	0.1	0.0557	0.154	0.153	0.152	0.151	0.61
110.167	8.819	0.423	0.109	0.395	0.18	0.385	0.106	0.295	0.125	0.033	0.0226	0.1	0.0557	0.154	0.153	0.152	0.15	0.609
110.25	8.786	0.423	0.109	0.394	0.18	0.384	0.105	0.294	0.125	0.033	0.0226	0.1	0.0557	0.154	0.152	0.152	0.15	0.608
110.333	8.754	0.422	0.109	0.394	0.18	0.384	0.105	0.294	0.125	0.033	0.0226	0.1	0.0557	0.153	0.152	0.152	0.15	0.607
110.417	8.721	0.421	0.109	0.393	0.179	0.383	0.105	0.294	0.125	0.033	0.0226	0.1	0.0557	0.153	0.152	0.151	0.15	0.606
110.5	8.689	0.421	0.109	0.392	0.179	0.382	0.105	0.293	0.125	0.033	0.0226	0.1	0.0557	0.153	0.151	0.151	0.149	0.604
110.583	8.656	0.42	0.109	0.392	0.179	0.381	0.105	0.293	0.124	0.033	0.0226	0.1	0.0557	0.153	0.151	0.151	0.149	0.604
110.667	8.624	0.419	0.109	0.391	0.178	0.38	0.105	0.293	0.124	0.033	0.0226	0.1	0.0557	0.152	0.151	0.15	0.149	0.602
110.75	8.592	0.419	0.109	0.39	0.178	0.38	0.104	0.292	0.124	0.033	0.0226	0.1	0.0557	0.152	0.151	0.15	0.148	0.601
110.833	8.56	0.418	0.109	0.389	0.178	0.379	0.104	0.292	0.124	0.033	0.0226	0.1	0.0557	0.152	0.15	0.15	0.148	0.6
110.917	8.528	0.417	0.109	0.389	0.178	0.378	0.104	0.292	0.124	0.033	0.0226	0.1	0.0557	0.152	0.15	0.15	0.148	0.6
111	8.496	0.417	0.109	0.388	0.177	0.378	0.104	0.291	0.124	0.033	0.0226	0.1	0.0557	0.151	0.15	0.149	0.148	0.598
111.083	8.465	0.416	0.109	0.388	0.177	0.377	0.104	0.291	0.124	0.033	0.0226	0.1	0.0557	0.151	0.15	0.149	0.147	0.597
111.167	8.433	0.416	0.109	0.387	0.177	0.376	0.104	0.291	0.123	0.033	0.0226	0.1	0.0557	0.151	0.149	0.149	0.147	0.596
111.25	8.401	0.415	0.109	0.386	0.177	0.375	0.103	0.29	0.123	0.033	0.0226	0.1	0.0557	0.151	0.149	0.149	0.147	0.596
111.333	8.37	0.414	0.109	0.386	0.177	0.375	0.103	0.29	0.123	0.033	0.0226	0.1	0.0557	0.15	0.149	0.148	0.147	0.594
111.417	8.339	0.414	0.109	0.385	0.176	0.374	0.103	0.29	0.123	0.033	0.0226	0.1	0.0557	0.15	0.149	0.148	0.146	0.593
111.5	8.308	0.413	0.109	0.385	0.176	0.373	0.103	0.29	0.123	0.033	0.0226	0.1	0.0557	0.15	0.148	0.148	0.146	0.592
111.583	8.277	0.413	0.109	0.384	0.176	0.373	0.103	0.289	0.123	0.033	0.0226	0.1	0.0557	0.15	0.148	0.148	0.146	0.592
111.667	8.246	0.412	0.109	0.383	0.176	0.372	0.103	0.289	0.123	0.033	0.0226	0.1	0.0557	0.149	0.148	0.148	0.146	0.591
111.75	8.215	0.412	0.109	0.383	0.175	0.372	0.103	0.289	0.122	0.033	0.0226	0.1	0.0557	0.149	0.148	0.147	0.146	0.59
111.833	8.185	0.411	0.109	0.382	0.175	0.371	0.103	0.289	0.122	0.033	0.0226	0.1	0.0557	0.149	0.148	0.147	0.145	0.589
111.917	8.154	0.411	0.109	0.382	0.175	0.37	0.102	0.288	0.122	0.033	0.0226	0.1	0.0556	0.149	0.147	0.147	0.145	0.588
112	8.124	0.41	0.109	0.381	0.175	0.37	0.102	0.288	0.122	0.033	0.0226	0.1	0.0556	0.149	0.147	0.147	0.145	0.588
112.083	8.094	0.41	0.108	0.381	0.175	0.369	0.102	0.288	0.122	0.033	0.0225	0.1	0.0553	0.148	0.147	0.147	0.145	0.587
112.167	8.064	0.409	0.108	0.38	0.174	0.368	0.102	0.288	0.122	0.0329	0.0224	0.1	0.0551	0.148	0.147	0.146	0.145	0.586
112.25	8.033	0.409	0.108	0.38	0.174	0.368	0.102	0.287	0.122	0.0329	0.0224	0.1	0.0548	0.148	0.147	0.146	0.144	0.585
112.333	8.003	0.408	0.108	0.379	0.174	0.367	0.102	0.287	0.121	0.0327	0.0222	0.1	0.0542	0.148	0.146	0.146	0.144	0.584
112.417	7.974	0.408	0.108	0.379	0.174	0.367	0.102	0.287	0.121	0.0326	0.022	0.1	0.0536	0.148	0.146	0.146	0.144	0.584
112.5	7.944	0.407	0.108	0.378	0.174	0.366	0.101	0.286	0.121	0.0325	0.0219	0.1	0.0531	0.147	0.146	0.145	0.144	0.582
112.583	7.914	0.407	0.108	0.378	0.173	0.365	0.101	0.286	0.121	0.0323	0.0216	0.1	0.0523	0.147	0.146	0.145	0.144	0.582
112.667	7.885	0.406	0.107	0.377	0.173	0.365	0.101	0.285	0.121	0.0322	0.0214	0.1	0.0515	0.147	0.146	0.145	0.143	0.581
112.75	7.855	0.405	0.107	0.377	0.173	0.364	0.101	0.285	0.12	0.032	0.0211	0.1	0.0507	0.147	0.145	0.145	0.143	0.58
112.833	7.826	0.405	0.107	0.376	0.172	0.363	0.101	0.285	0.12	0.0318	0.0209	0.1	0.05	0.147	0.145	0.145	0.143	0.58
112.917	7.797	0.404	0.106	0.376	0.172	0.363	0.101	0.284	0.12	0.0315	0.0206	0.1	0.0493	0.146	0.145	0.144	0.143	0.578
113	7.768	0.404	0.106	0.375	0.172	0.362	0.101	0.284	0.12	0.0313	0.0203	0.1	0.0486	0.146	0.145	0.144	0.142	0.577
113.083	7.739	0.403	0.106	0.374	0.172	0.361	0.1	0.283	0.12	0.031	0.0201	0.1	0.048	0.146	0.144	0.144	0.142	0.576
113.167	7.71	0.402	0.105	0.374	0.171	0.361	0.1	0.283	0.119	0.0307	0.0198	0.1	0.0475	0.146	0.144	0.144	0.142	0.576
113.25	7.681	0.402	0.105	0.373	0.171	0.36	0.1	0.282	0.119	0.0304	0.0196	0.1	0.047	0.145	0.144	0.143	0.142	0.574
113.333	7.653	0.401	0.104	0.373	0.171	0.359	0.0999	0.281	0.119	0.0302	0.0194	0.1	0.0466	0.145	0.144	0.143	0.142	0.574
113.417	7.624	0.4	0.104	0.372	0.17	0.359	0.0997	0.281	0.119	0.0299	0.0192	0.1	0.0463	0.145	0.144	0.143	0.141	0.573
113.5	7.596	0.399	0.103	0.371	0.17	0.358	0.0995	0.28	0.118	0.0296	0.0191	0.1	0.0459	0.145	0.143	0.143	0.141	0.572
113.583	7.567	0.399	0.103	0.371	0.17	0.357	0.0993	0.279	0.118	0.0294	0.0189	0.1	0.0456	0.144	0.143	0.143	0.141	0.571
113.667	7.539	0.398	0.102	0.37	0.169	0.357	0.0991	0.279	0.118	0.0291	0.0188	0.1	0.0454	0.144	0.143	0.142	0.141	0.57
113.75	7.511	0.397	0.102	0.369	0.169	0.356	0.099	0.278	0.118	0.0289	0.0187	0.1	0.0451	0.144	0.143	0.142	0.14	0.569
113.833	7.483	0.396	0.101	0.369	0.169	0.355	0.0988	0.277	0.117	0.0287	0.0186	0.1	0.0449	0.144	0.142	0.142	0.14	0.568
113.917	7.455	0.396	0.1	0.368	0.168	0.355	0.0986	0.276	0.117	0.0285	0.0185	0.1	0.0447	0.143	0.142	0.141	0.14	0.566
114	7.427	0.395	0.0996	0.367	0.168	0.354	0.0984	0.276	0.117	0.0283	0.0184	0.1	0.0446	0.143	0.142	0.141	0.139	0.565
114.083	7.4	0.394	0.099	0.367	0.168	0.353	0.0982	0.275	0.117	0.0281	0.0183	0.1	0.0445	0.143	0.141	0.141	0.139	0.564
114.167	7.372	0.393	0.0983	0.366	0.167	0.353	0.0979	0.274	0.116	0.0279	0.0182	0.1	0.0444	0.143	0.141	0.141	0.139	0.564
114.25	7.345	0.392	0.0977	0.365	0.167	0.352	0.0977	0.273	0.116	0.0278	0.0181	0.1	0.0443	0.142	0.141	0.14	0.139	0.562
114.333	7.317	0.391	0.0971	0.365	0.167	0.351	0.0975	0.272	0.116	0.0276	0.0181	0.1	0.0442	0.142	0.141	0.14	0.138	0.561
114.417	7.29	0.39	0.0964	0.364	0.166	0.35	0.0973	0.271	0.115	0.0275	0.018	0.1	0.0442	0.142	0.14	0.14	0.138	0.56
114.5	7.263	0.39	0.0958	0.363	0.166	0.35	0.0971	0.27	0.115	0.0274	0.018	0.1	0.0442	0.141	0.14	0.139	0.138	0.558
114.583	7.236	0.389	0.0953	0.362	0.165	0.349	0.0968	0.269	0.115	0.0273	0.0179	0.1	0.0442	0.141	0.14	0.139	0.137	0.557
114.667	7.209	0.388	0.0947	0.361	0.165	0.348	0.0966	0.268	0.114	0.0272	0.0179	0.1	0.0442	0.141	0.139	0.139	0.137	0.556
114.75	7.182	0.387	0.0942	0.361	0.164	0.348	0.0964	0.267	0.114	0.027	0.0179	0.1	0.0442	0.14	0.139	0.139	0.137	0.555
114.833	7.155	0.386	0.0936	0.36	0.164	0.347	0.0961	0.266	0.114	0.0269	0.0179	0.1	0.0442	0.14	0.139	0.138	0.136	0.553
114.917	7.128	0.385	0.0931	0.359	0.164	0.346	0.0959	0.265	0.113	0.0268	0.0179	0.1	0.0442	0.14	0.138	0.138	0.136	0.552
115	7.102	0.384	0.0926	0.358	0.163	0.345	0.0957	0.264	0.113	0.0268	0.0179	0.1	0.0442	0.14	0.138	0.138	0.136	0.552
115.083	7.075	0.383	0.0922	0.357	0.163	0.345	0.0954	0.263	0.113	0.0267	0.0179	0.1	0.0442	0.139	0.138	0.137	0.135	0.549

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
115.167	7.049	0.382	0.0917	0.357	0.162	0.344	0.0952	0.262	0.112	0.0266	0.0179	0.1	0.0442	0.139	0.137	0.137	0.135	0.548
115.25	7.023	0.381	0.0912	0.356	0.162	0.343	0.0949	0.26	0.112	0.0265	0.0179	0.1	0.0442	0.138	0.137	0.137	0.135	0.547
115.333	6.997	0.38	0.0908	0.355	0.161	0.342	0.0947	0.259	0.111	0.0265	0.0179	0.1	0.0442	0.138	0.137	0.136	0.134	0.545
115.417	6.971	0.379	0.0904	0.354	0.161	0.342	0.0944	0.258	0.111	0.0264	0.0179	0.1	0.0442	0.138	0.136	0.136	0.134	0.544
115.5	6.945	0.378	0.09	0.353	0.16	0.341	0.0942	0.257	0.111	0.0263	0.0179	0.1	0.0442	0.137	0.136	0.135	0.134	0.542
115.583	6.919	0.377	0.0897	0.352	0.16	0.34	0.0939	0.256	0.11	0.0263	0.0179	0.1	0.0442	0.137	0.136	0.135	0.133	0.541
115.667	6.893	0.375	0.0893	0.351	0.159	0.339	0.0936	0.255	0.11	0.0262	0.0179	0.1	0.0442	0.137	0.135	0.135	0.133	0.54
115.75	6.867	0.374	0.0889	0.35	0.159	0.339	0.0934	0.254	0.109	0.0262	0.0179	0.1	0.0442	0.136	0.135	0.134	0.133	0.538
115.833	6.842	0.373	0.0886	0.349	0.158	0.338	0.0931	0.253	0.109	0.0262	0.0179	0.1	0.0442	0.136	0.135	0.134	0.132	0.537
115.917	6.816	0.372	0.0883	0.348	0.158	0.337	0.0928	0.252	0.109	0.0261	0.0179	0.1	0.0442	0.136	0.134	0.134	0.132	0.536
116	6.791	0.371	0.088	0.348	0.157	0.336	0.0925	0.251	0.108	0.0261	0.0179	0.1	0.0442	0.135	0.134	0.133	0.132	0.534
116.083	6.765	0.37	0.0877	0.347	0.157	0.336	0.0922	0.25	0.108	0.0261	0.0179	0.1	0.0442	0.135	0.133	0.133	0.131	0.532
116.167	6.74	0.369	0.0875	0.346	0.156	0.335	0.092	0.249	0.107	0.0261	0.0179	0.1	0.0442	0.134	0.133	0.132	0.131	0.53
116.25	6.715	0.367	0.0872	0.345	0.156	0.334	0.0917	0.248	0.107	0.026	0.0179	0.1	0.0442	0.134	0.133	0.132	0.13	0.529
116.333	6.69	0.366	0.0869	0.344	0.155	0.333	0.0914	0.247	0.107	0.026	0.0179	0.1	0.0442	0.134	0.132	0.132	0.13	0.528
116.417	6.665	0.365	0.0867	0.343	0.154	0.333	0.0911	0.246	0.106	0.026	0.0179	0.1	0.0442	0.133	0.132	0.131	0.13	0.526
116.5	6.64	0.364	0.0864	0.342	0.154	0.332	0.0908	0.245	0.106	0.026	0.0179	0.1	0.0442	0.133	0.131	0.131	0.129	0.524
116.583	6.616	0.362	0.0862	0.341	0.153	0.331	0.0905	0.245	0.106	0.026	0.0179	0.1	0.0442	0.132	0.131	0.13	0.129	0.522
116.667	6.591	0.361	0.086	0.34	0.153	0.33	0.0901	0.244	0.105	0.026	0.0179	0.1	0.0442	0.132	0.131	0.13	0.128	0.521
116.75	6.566	0.36	0.0857	0.338	0.152	0.329	0.0898	0.243	0.105	0.026	0.0179	0.1	0.0442	0.132	0.13	0.13	0.128	0.52
116.833	6.542	0.359	0.0855	0.337	0.152	0.329	0.0895	0.242	0.105	0.026	0.0179	0.1	0.0442	0.131	0.13	0.129	0.128	0.518
116.917	6.518	0.358	0.0853	0.336	0.151	0.328	0.0892	0.241	0.104	0.026	0.0179	0.1	0.0442	0.131	0.129	0.129	0.127	0.516
117	6.493	0.356	0.0851	0.335	0.151	0.327	0.0889	0.24	0.104	0.026	0.0179	0.1	0.0442	0.13	0.129	0.128	0.127	0.514
117.083	6.469	0.355	0.0849	0.334	0.15	0.326	0.0886	0.24	0.104	0.026	0.0179	0.1	0.0442	0.13	0.129	0.128	0.126	0.513
117.167	6.445	0.354	0.0847	0.333	0.15	0.325	0.0883	0.239	0.103	0.026	0.0179	0.1	0.0442	0.13	0.128	0.128	0.126	0.512
117.25	6.421	0.353	0.0846	0.332	0.149	0.325	0.088	0.238	0.103	0.026	0.0179	0.1	0.0442	0.129	0.128	0.127	0.125	0.509
117.333	6.397	0.352	0.0844	0.331	0.149	0.324	0.0878	0.238	0.103	0.026	0.0179	0.1	0.0442	0.129	0.127	0.127	0.125	0.508
117.417	6.373	0.351	0.0842	0.33	0.148	0.323	0.0875	0.237	0.102	0.026	0.0179	0.1	0.0442	0.128	0.127	0.126	0.125	0.506
117.5	6.349	0.35	0.0841	0.329	0.148	0.322	0.0872	0.236	0.102	0.026	0.0179	0.1	0.0442	0.128	0.126	0.126	0.124	0.504
117.583	6.326	0.348	0.0839	0.328	0.148	0.321	0.0869	0.236	0.102	0.026	0.0179	0.1	0.0442	0.127	0.126	0.125	0.124	0.502
117.667	6.302	0.347	0.0838	0.327	0.147	0.321	0.0867	0.235	0.102	0.026	0.0179	0.1	0.0442	0.127	0.126	0.125	0.123	0.501
117.75	6.279	0.346	0.0836	0.326	0.147	0.32	0.0864	0.234	0.101	0.026	0.0179	0.1	0.0442	0.127	0.125	0.125	0.123	0.5
117.833	6.255	0.345	0.0835	0.325	0.146	0.319	0.0861	0.234	0.101	0.026	0.0178	0.1	0.0442	0.126	0.125	0.124	0.123	0.498
117.917	6.232	0.344	0.0834	0.324	0.146	0.318	0.0859	0.233	0.101	0.026	0.0178	0.1	0.0441	0.126	0.124	0.124	0.122	0.496
118	6.209	0.343	0.0833	0.323	0.145	0.317	0.0856	0.233	0.1	0.026	0.0178	0.1	0.0441	0.126	0.124	0.124	0.122	0.496
118.083	6.186	0.342	0.0831	0.322	0.145	0.316	0.0854	0.232	0.1	0.026	0.0178	0.1	0.0439	0.125	0.124	0.123	0.121	0.493
118.167	6.163	0.341	0.083	0.321	0.145	0.315	0.0851	0.232	0.0999	0.0259	0.0177	0.1	0.0437	0.125	0.123	0.123	0.121	0.492
118.25	6.14	0.34	0.0828	0.32	0.144	0.315	0.0849	0.231	0.0996	0.0259	0.0177	0.1	0.0435	0.124	0.123	0.122	0.121	0.49
118.333	6.117	0.339	0.0826	0.319	0.144	0.314	0.0846	0.23	0.0993	0.0258	0.0175	0.1	0.043	0.124	0.123	0.122	0.12	0.489
118.417	6.094	0.338	0.0824	0.318	0.143	0.313	0.0843	0.23	0.099	0.0257	0.0174	0.1	0.0425	0.124	0.122	0.122	0.12	0.488
118.5	6.071	0.337	0.0822	0.317	0.143	0.312	0.0841	0.229	0.0987	0.0256	0.0172	0.1	0.042	0.123	0.122	0.121	0.12	0.486
118.583	6.049	0.336	0.0819	0.316	0.143	0.311	0.0838	0.228	0.0984	0.0254	0.017	0.1	0.0412	0.123	0.121	0.121	0.119	0.484
118.667	6.026	0.335	0.0817	0.315	0.142	0.31	0.0836	0.228	0.0981	0.0253	0.0168	0.1	0.0404	0.123	0.121	0.121	0.119	0.484
118.75	6.004	0.334	0.0814	0.314	0.142	0.309	0.0833	0.227	0.0978	0.0251	0.0165	0.1	0.0396	0.122	0.121	0.12	0.118	0.481
118.833	5.982	0.333	0.081	0.313	0.141	0.308	0.083	0.226	0.0975	0.0249	0.0163	0.1	0.0388	0.122	0.12	0.12	0.118	0.48
118.917	5.959	0.332	0.0807	0.312	0.141	0.307	0.0828	0.225	0.0972	0.0247	0.016	0.1	0.0381	0.121	0.12	0.119	0.118	0.478
119	5.937	0.331	0.0804	0.311	0.141	0.306	0.0825	0.225	0.0969	0.0244	0.0157	0.1	0.0373	0.121	0.12	0.119	0.117	0.477
119.083	5.915	0.33	0.08	0.31	0.14	0.305	0.0823	0.224	0.0966	0.0242	0.0154	0.1	0.0368	0.121	0.119	0.119	0.117	0.476
119.167	5.893	0.329	0.0795	0.309	0.14	0.304	0.082	0.223	0.0963	0.0239	0.0152	0.1	0.0362	0.12	0.119	0.118	0.116	0.473
119.25	5.871	0.328	0.0791	0.308	0.139	0.303	0.0818	0.222	0.096	0.0236	0.015	0.1	0.0357	0.12	0.118	0.118	0.116	0.472
119.333	5.849	0.327	0.0787	0.307	0.139	0.302	0.0815	0.221	0.0957	0.0233	0.0148	0.1	0.0353	0.119	0.118	0.117	0.116	0.47
119.417	5.828	0.326	0.0782	0.306	0.138	0.301	0.0812	0.22	0.0953	0.023	0.0146	0.1	0.0349	0.119	0.118	0.117	0.115	0.469
119.5	5.806	0.325	0.0777	0.305	0.138	0.3	0.081	0.219	0.095	0.0227	0.0144	0.1	0.0345	0.119	0.117	0.117	0.115	0.468
119.583	5.784	0.324	0.0771	0.304	0.137	0.299	0.0807	0.218	0.0947	0.0225	0.0143	0.1	0.0342	0.118	0.117	0.116	0.115	0.466
119.667	5.763	0.323	0.0766	0.303	0.137	0.298	0.0804	0.217	0.0943	0.0222	0.0141	0.1	0.0339	0.118	0.116	0.116	0.114	0.464
119.75	5.741	0.322	0.076	0.302	0.137	0.297	0.0802	0.217	0.094	0.022	0.014	0.1	0.0337	0.117	0.116	0.115	0.114	0.462
119.833	5.72	0.321	0.0753	0.301	0.136	0.297	0.0799	0.215	0.0936	0.0218	0.0139	0.1	0.0335	0.117	0.116	0.115	0.113	0.461
119.917	5.699	0.32	0.0747	0.3	0.136	0.296	0.0796	0.214	0.0933	0.0216	0.0138	0.1	0.0333	0.117	0.115	0.115	0.113	0.46
120	5.678	0.319	0.074	0.299	0.135	0.295	0.0794	0.213	0.0929	0.0214	0.0137	0.1	0.0331	0.116	0.115	0.114	0.113	0.458
120.083	5.657	0.318	0.0733	0.298	0.135	0.294	0.0791	0.212	0.0926	0.0212	0.0136	0.1	0.0329	0.116	0.114	0.114	0.112	0.456
120.167	5.636	0.316	0.0727	0.297	0.134	0.293	0.0788	0.211	0.0922	0.021	0.0135	0.1	0.0328	0.115	0.114	0.114	0.112	0.455
120.25	5.615	0.315	0.072	0.296	0.134	0.292	0.0785	0.21	0.0918	0.0209	0.0134	0.1	0.0327	0.115	0.114	0.113	0.111	0.453
120.333	5.594	0.314	0.0714	0.295	0.133	0.291	0.0782	0.209	0.0915	0.0207	0.0134	0.1	0.0327	0.115	0.113	0.113	0.111	0.452

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
120.417	5.573	0.313	0.0708	0.294	0.133	0.29	0.078	0.208	0.0911	0.0206	0.0133	0.1	0.0326	0.114	0.113	0.112	0.111	0.45
120.5	5.552	0.312	0.0701	0.293	0.132	0.289	0.0777	0.206	0.0907	0.0204	0.0132	0.1	0.0326	0.114	0.112	0.112	0.11	0.448
120.583	5.532	0.311	0.0696	0.292	0.132	0.288	0.0774	0.205	0.0903	0.0203	0.0132	0.1	0.0326	0.113	0.112	0.111	0.11	0.446
120.667	5.511	0.31	0.069	0.291	0.131	0.287	0.0771	0.204	0.0899	0.0202	0.0132	0.1	0.0326	0.113	0.112	0.111	0.109	0.445
120.75	5.491	0.309	0.0684	0.29	0.131	0.286	0.0768	0.203	0.0895	0.0201	0.0131	0.1	0.0326	0.113	0.111	0.111	0.109	0.444
120.833	5.47	0.307	0.0679	0.289	0.13	0.285	0.0765	0.201	0.089	0.02	0.0131	0.1	0.0326	0.112	0.111	0.11	0.109	0.442
120.917	5.45	0.306	0.0674	0.288	0.13	0.284	0.0763	0.2	0.0886	0.0199	0.0131	0.1	0.0326	0.112	0.11	0.11	0.108	0.44
121	5.429	0.305	0.0669	0.287	0.129	0.283	0.076	0.199	0.0882	0.0198	0.0131	0.1	0.0326	0.111	0.11	0.109	0.108	0.438
121.083	5.409	0.304	0.0663	0.286	0.128	0.282	0.0757	0.197	0.0877	0.0196	0.013	0.1	0.0323	0.111	0.11	0.109	0.107	0.437
121.167	5.389	0.303	0.0658	0.285	0.128	0.281	0.0754	0.196	0.0872	0.0195	0.0129	0.1	0.032	0.111	0.109	0.109	0.107	0.436
121.25	5.369	0.301	0.0652	0.284	0.127	0.28	0.0751	0.194	0.0867	0.0193	0.0128	0.1	0.0316	0.11	0.109	0.108	0.106	0.433
121.333	5.349	0.3	0.0645	0.283	0.127	0.279	0.0747	0.193	0.0862	0.0191	0.0125	0.1	0.0306	0.11	0.108	0.108	0.106	0.432
121.417	5.328	0.298	0.0639	0.282	0.126	0.278	0.0744	0.191	0.0856	0.0188	0.0123	0.1	0.0297	0.109	0.108	0.107	0.105	0.429
121.5	5.308	0.297	0.0632	0.28	0.125	0.277	0.074	0.189	0.0851	0.0186	0.012	0.1	0.0287	0.109	0.107	0.107	0.105	0.428
121.583	5.288	0.296	0.0624	0.279	0.125	0.276	0.0737	0.188	0.0845	0.0182	0.0115	0.1	0.0271	0.108	0.107	0.106	0.104	0.425
121.667	5.268	0.294	0.0616	0.278	0.124	0.275	0.0733	0.186	0.0839	0.0178	0.0111	0.1	0.0255	0.108	0.106	0.106	0.104	0.424
121.75	5.248	0.292	0.0608	0.277	0.123	0.274	0.0729	0.184	0.0833	0.0175	0.0106	0.1	0.0239	0.107	0.106	0.105	0.103	0.421
121.833	5.228	0.291	0.0599	0.275	0.122	0.273	0.0725	0.182	0.0826	0.017	0.0101	0.1	0.0223	0.107	0.105	0.105	0.103	0.42
121.917	5.208	0.289	0.0589	0.274	0.122	0.272	0.0721	0.181	0.0819	0.0165	0.00948	0.1	0.0208	0.106	0.105	0.104	0.102	0.417
122	5.188	0.287	0.058	0.272	0.121	0.27	0.0716	0.179	0.0812	0.0161	0.00891	0.1	0.0193	0.106	0.104	0.104	0.102	0.416
122.083	5.168	0.285	0.057	0.271	0.12	0.269	0.0712	0.177	0.0805	0.0155	0.00841	0.1	0.0181	0.105	0.104	0.103	0.101	0.413
122.167	5.148	0.283	0.0559	0.269	0.119	0.268	0.0707	0.175	0.0798	0.0149	0.00792	0.1	0.017	0.104	0.103	0.102	0.101	0.41
122.25	5.128	0.282	0.0549	0.268	0.118	0.267	0.0703	0.173	0.0791	0.0143	0.00742	0.1	0.0158	0.104	0.102	0.102	0.1	0.408
122.333	5.108	0.28	0.0537	0.266	0.117	0.265	0.0698	0.171	0.0784	0.0138	0.00703	0.1	0.015	0.103	0.102	0.101	0.0993	0.4053
122.417	5.088	0.278	0.0524	0.265	0.116	0.264	0.0693	0.169	0.0776	0.0132	0.00664	0.1	0.0143	0.102	0.101	0.1	0.0987	0.4017
122.5	5.068	0.275	0.0512	0.263	0.115	0.263	0.0688	0.167	0.0769	0.0126	0.00626	0.1	0.0135	0.102	0.1	0.0998	0.098	0.3998
122.583	5.048	0.273	0.0499	0.261	0.114	0.261	0.0682	0.165	0.0761	0.0121	0.00597	0.1	0.0129	0.101	0.0997	0.0991	0.0974	0.3972
122.667	5.028	0.271	0.0485	0.259	0.113	0.26	0.0677	0.163	0.0753	0.0116	0.00569	0.1	0.0123	0.1	0.099	0.0985	0.0967	0.3942
122.75	5.008	0.269	0.0472	0.258	0.112	0.259	0.0672	0.161	0.0746	0.0111	0.00541	0.1	0.0117	0.0998	0.0983	0.0978	0.096	0.3919
122.833	4.989	0.267	0.0457	0.256	0.111	0.257	0.0666	0.158	0.0738	0.0107	0.0052	0.1	0.0113	0.099	0.0976	0.097	0.0952	0.3888
122.917	4.969	0.264	0.0441	0.254	0.11	0.256	0.066	0.156	0.073	0.0102	0.00498	0.1	0.0109	0.0983	0.0968	0.0963	0.0945	0.3859
123	4.949	0.262	0.0426	0.252	0.109	0.254	0.0655	0.154	0.0722	0.00982	0.00477	0.1	0.0104	0.0976	0.0961	0.0956	0.0938	0.3831
123.083	4.929	0.26	0.0411	0.25	0.108	0.253	0.0649	0.151	0.0713	0.00946	0.00459	0.1	0.0102	0.0968	0.0953	0.0948	0.093	0.3799
123.167	4.909	0.257	0.0395	0.248	0.107	0.251	0.0643	0.149	0.0705	0.00911	0.00442	0.1	0.00995	0.096	0.0945	0.094	0.0922	0.3767
123.25	4.89	0.255	0.038	0.246	0.106	0.25	0.0637	0.147	0.0697	0.00875	0.00425	0.1	0.0097	0.0952	0.0937	0.0932	0.0914	0.3735
123.333	4.87	0.253	0.0366	0.244	0.105	0.248	0.0631	0.144	0.0688	0.00847	0.00413	0.1	0.00962	0.0944	0.0929	0.0924	0.0906	0.3703
123.417	4.85	0.25	0.0351	0.242	0.104	0.247	0.0625	0.142	0.068	0.00818	0.00401	0.1	0.00955	0.0936	0.0921	0.0916	0.0898	0.3671
123.5	4.831	0.248	0.0337	0.24	0.103	0.245	0.0619	0.139	0.0671	0.00789	0.00388	0.1	0.00947	0.0928	0.0913	0.0908	0.089	0.3639
123.583	4.811	0.245	0.0324	0.238	0.102	0.244	0.0613	0.137	0.0663	0.00766	0.0038	0.1	0.00947	0.092	0.0905	0.0899	0.0881	0.3605
123.667	4.791	0.243	0.0311	0.236	0.1	0.242	0.0607	0.134	0.0654	0.00743	0.00372	0.1	0.00947	0.0911	0.0897	0.0891	0.0873	0.3572
123.75	4.772	0.24	0.0298	0.234	0.0993	0.24	0.0601	0.131	0.0645	0.0072	0.00364	0.1	0.00947	0.0903	0.0888	0.0883	0.0865	0.3539
123.833	4.752	0.238	0.0287	0.232	0.0982	0.239	0.0595	0.129	0.0636	0.00699	0.00362	0.1	0.00947	0.0895	0.088	0.0874	0.0856	0.3505
123.917	4.733	0.235	0.0275	0.23	0.097	0.237	0.0589	0.126	0.0627	0.00679	0.00359	0.1	0.00947	0.0886	0.0871	0.0866	0.0848	0.3471
124	4.713	0.233	0.0263	0.227	0.0959	0.235	0.0583	0.123	0.0617	0.00658	0.00356	0.1	0.00947	0.0878	0.0863	0.0857	0.0839	0.3437
124.083	4.694	0.23	0.0253	0.225	0.0947	0.234	0.0576	0.12	0.0608	0.00642	0.00356	0.1	0.00947	0.0869	0.0854	0.0849	0.0831	0.3403
124.167	4.674	0.228	0.0242	0.223	0.0935	0.232	0.057	0.117	0.0599	0.00626	0.00356	0.1	0.00947	0.086	0.0846	0.084	0.0822	0.3368
124.25	4.655	0.225	0.0232	0.221	0.0923	0.23	0.0564	0.114	0.0589	0.00609	0.00356	0.1	0.00947	0.0852	0.0837	0.0831	0.0813	0.3333
124.333	4.635	0.222	0.0223	0.219	0.0911	0.228	0.0557	0.112	0.0579	0.00596	0.00356	0.1	0.00947	0.0843	0.0828	0.0823	0.0804	0.3298
124.417	4.616	0.22	0.0213	0.216	0.0898	0.227	0.0551	0.109	0.057	0.00582	0.00356	0.1	0.00947	0.0834	0.0819	0.0814	0.0795	0.3262
124.5	4.596	0.217	0.0204	0.214	0.0886	0.225	0.0544	0.106	0.056	0.00568	0.00356	0.1	0.00947	0.0825	0.081	0.0805	0.0787	0.3227
124.583	4.577	0.214	0.0196	0.212	0.0874	0.223	0.0537	0.104	0.055	0.00558	0.00356	0.1	0.00947	0.0816	0.0801	0.0796	0.0777	0.319
124.667	4.557	0.212	0.0188	0.21	0.0861	0.221	0.0531	0.101	0.054	0.00547	0.00356	0.1	0.00947	0.0807	0.0792	0.0787	0.0768	0.3154
124.75	4.538	0.209	0.018	0.207	0.0849	0.219	0.0524	0.0984	0.053	0.00536	0.00356	0.1	0.00947	0.0798	0.0783	0.0778	0.0759	0.3118
124.833	4.519	0.206	0.0173	0.205	0.0836	0.217	0.0517	0.0959	0.052	0.00529	0.00356	0.1	0.00947	0.0789	0.0774	0.0768	0.075	0.3081
124.917	4.499	0.203	0.0167	0.203	0.0823	0.215	0.051	0.0934	0.051	0.00522	0.00356	0.1	0.00947	0.078	0.0765	0.0759	0.0741	0.3045
125	4.48	0.2	0.016	0.2	0.081	0.214	0.0503	0.0909	0.05	0.00515	0.00356	0.1	0.00947	0.077	0.0755	0.075	0.0731	0.3006
125.083	4.461	0.198	0.0154	0.198	0.0797	0.212	0.0496	0.0886	0.049	0.00511	0.00356	0.1	0.00947	0.0761	0.0746	0.074	0.0722	0.2969
125.167	4.442	0.195	0.0148	0.196	0.0784	0.21	0.049	0.0863	0.048	0.00507	0.00356	0.1	0.00947	0.0751	0.0736	0.0731	0.0712	0.293
125.25	4.422	0.192	0.0143	0.193	0.077	0.208	0.0483	0.0839	0.047	0.00503	0.00356	0.1	0.00947	0.0742	0.0727	0.0721	0.0703	0.2893
125.333	4.403	0.189	0.0137	0.191	0.0757	0.206	0.0475	0.0817	0.0461	0.00502	0.00356	0.1	0.00947	0.0732	0.0717	0.0712	0.0693	0.2854
125.417	4.384	0.186	0.0132	0.188	0.0744	0.204	0.0468	0.0795	0.0452	0.005	0.00356	0.1	0.00947	0.0723	0.0708	0.0702	0.0684	0.2817
125.5	4.365	0.183	0.0127	0.186	0.073	0.202	0.0461	0.0773	0.0442	0.00499	0.00356	0.1	0.00947	0.0713	0.0698	0.0692	0.0674	0.2777
125.583	4.345	0.18	0.0122	0.183	0.0717	0.2	0.0454	0.0752	0.0433	0.00499	0.00356	0.1	0.00947	0.0703	0.0688	0.0683	0.0664	0.2738

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
125.667	4.326	0.177	0.0118	0.181	0.0705	0.198	0.0446	0.0731	0.0425	0.00499	0.00356	0.1	0.00947	0.0693	0.0678	0.0673	0.0654	0.2698
125.75	4.307	0.174	0.0113	0.178	0.0692	0.196	0.0439	0.071	0.0416	0.00499	0.00356	0.1	0.00947	0.0683	0.0668	0.0663	0.0644	0.2658
125.833	4.288	0.171	0.0108	0.176	0.0679	0.194	0.0432	0.0691	0.0408	0.00499	0.00356	0.1	0.00947	0.0673	0.0658	0.0653	0.0634	0.2618
125.917	4.269	0.168	0.0104	0.173	0.0667	0.192	0.0424	0.0672	0.0399	0.00499	0.00356	0.1	0.00947	0.0663	0.0648	0.0643	0.0624	0.2578
126	4.25	0.165	0.00998	0.171	0.0655	0.19	0.0417	0.0652	0.0391	0.00499	0.00356	0.1	0.00947	0.0653	0.0638	0.0633	0.0614	0.2538
126.083	4.231	0.163	0.0096	0.168	0.0643	0.188	0.041	0.0634	0.0383	0.00499	0.00356	0.1	0.00947	0.0643	0.0628	0.0623	0.0604	0.2498
126.167	4.212	0.16	0.00921	0.166	0.0631	0.186	0.0403	0.0616	0.0375	0.00499	0.00356	0.1	0.00947	0.0633	0.0618	0.0613	0.0594	0.2458
126.25	4.193	0.157	0.00882	0.163	0.0619	0.184	0.0396	0.0598	0.0367	0.00499	0.00356	0.1	0.00947	0.0623	0.0608	0.0602	0.0584	0.2417
126.333	4.174	0.154	0.00848	0.161	0.0608	0.182	0.0389	0.0581	0.036	0.00499	0.00356	0.1	0.00947	0.0613	0.0598	0.0593	0.0574	0.2378
126.417	4.155	0.152	0.00813	0.158	0.0597	0.18	0.0382	0.0565	0.0352	0.00499	0.00356	0.1	0.00947	0.0603	0.0588	0.0583	0.0564	0.2338
126.5	4.136	0.149	0.00779	0.156	0.0586	0.178	0.0375	0.0548	0.0345	0.00499	0.00356	0.1	0.00947	0.0593	0.0578	0.0573	0.0554	0.2298
126.583	4.117	0.146	0.00749	0.153	0.0575	0.175	0.0369	0.0533	0.0337	0.00499	0.00356	0.1	0.00947	0.0584	0.0569	0.0563	0.0545	0.2261
126.667	4.098	0.144	0.00718	0.151	0.0565	0.173	0.0363	0.0517	0.033	0.00499	0.00356	0.1	0.00947	0.0575	0.056	0.0554	0.0535	0.2224
126.75	4.079	0.141	0.00688	0.149	0.0554	0.171	0.0356	0.0502	0.0323	0.00499	0.00356	0.1	0.00947	0.0565	0.055	0.0545	0.0526	0.2186
126.833	4.06	0.139	0.00664	0.146	0.0544	0.169	0.035	0.0488	0.0316	0.00499	0.00356	0.1	0.00947	0.0556	0.0541	0.0535	0.0517	0.2149
126.917	4.041	0.136	0.00639	0.144	0.0534	0.167	0.0344	0.0474	0.0309	0.00499	0.00356	0.1	0.00947	0.0547	0.0532	0.0526	0.0507	0.2112
127	4.022	0.134	0.00615	0.142	0.0524	0.165	0.0338	0.046	0.0303	0.00499	0.00356	0.1	0.00947	0.0538	0.0523	0.0517	0.0498	0.2076
127.083	4.003	0.132	0.00595	0.139	0.0515	0.163	0.0332	0.0448	0.0296	0.00499	0.00356	0.1	0.00947	0.0529	0.0514	0.0508	0.049	0.2041
127.167	3.984	0.129	0.00575	0.137	0.0505	0.161	0.0326	0.0435	0.0289	0.00499	0.00356	0.1	0.00947	0.052	0.0505	0.05	0.0481	0.2006
127.25	3.966	0.127	0.00555	0.135	0.0495	0.159	0.032	0.0422	0.0283	0.00499	0.00356	0.1	0.00947	0.0512	0.0496	0.0491	0.0472	0.1971
127.333	3.947	0.125	0.00539	0.133	0.0486	0.157	0.0314	0.0411	0.0277	0.00499	0.00356	0.1	0.00947	0.0503	0.0488	0.0482	0.0464	0.1937
127.417	3.928	0.122	0.00523	0.131	0.0477	0.155	0.0309	0.0399	0.027	0.00499	0.00356	0.1	0.00947	0.0495	0.048	0.0474	0.0455	0.1904
127.5	3.909	0.12	0.00507	0.129	0.0468	0.153	0.0303	0.0388	0.0264	0.00499	0.00356	0.1	0.00947	0.0486	0.0471	0.0466	0.0447	0.187
127.583	3.891	0.118	0.00496	0.127	0.0459	0.15	0.0298	0.0377	0.0258	0.00499	0.00356	0.1	0.00947	0.0478	0.0463	0.0457	0.0439	0.1837
127.667	3.872	0.116	0.00484	0.124	0.045	0.148	0.0292	0.0366	0.0252	0.00499	0.00356	0.1	0.00947	0.047	0.0455	0.0449	0.0431	0.1805
127.75	3.853	0.114	0.00473	0.122	0.0442	0.146	0.0287	0.0356	0.0247	0.00499	0.00356	0.1	0.00947	0.0462	0.0447	0.0441	0.0422	0.1772
127.833	3.835	0.112	0.00466	0.12	0.0434	0.144	0.0282	0.0346	0.0241	0.00499	0.00356	0.1	0.00947	0.0455	0.0439	0.0434	0.0415	0.1743
127.917	3.816	0.11	0.00458	0.119	0.0425	0.142	0.0277	0.0335	0.0236	0.00499	0.00356	0.1	0.00947	0.0447	0.0432	0.0426	0.0407	0.1712
128	3.797	0.108	0.00451	0.117	0.0417	0.14	0.0271	0.0325	0.023	0.00499	0.00356	0.1	0.00947	0.0439	0.0424	0.0418	0.0399	0.168
128.083	3.779	0.106	0.00448	0.115	0.0409	0.138	0.0267	0.0316	0.0225	0.00499	0.00356	0.1	0.00947	0.0432	0.0417	0.0411	0.0392	0.1652
128.167	3.76	0.104	0.00445	0.113	0.0402	0.135	0.0262	0.0307	0.022	0.00499	0.00356	0.1	0.00947	0.0424	0.0409	0.0404	0.0385	0.1622
128.25	3.741	0.102	0.00443	0.111	0.0394	0.133	0.0257	0.0297	0.0215	0.00499	0.00356	0.1	0.00947	0.0417	0.0402	0.0396	0.0377	0.1592
128.333	3.723	0.1	0.00443	0.109	0.0386	0.131	0.0252	0.0289	0.0211	0.00499	0.00356	0.1	0.00947	0.041	0.0395	0.0389	0.037	0.1564
128.417	3.704	0.0985	0.00443	0.107	0.0379	0.129	0.0248	0.028	0.0206	0.00499	0.00356	0.1	0.00947	0.0403	0.0388	0.0382	0.0363	0.1536
128.5	3.686	0.0967	0.00443	0.106	0.0372	0.127	0.0243	0.0272	0.0201	0.00499	0.00356	0.1	0.00947	0.0396	0.0381	0.0375	0.0356	0.1508
128.583	3.667	0.0949	0.00443	0.104	0.0365	0.125	0.0239	0.0264	0.0197	0.00499	0.00356	0.1	0.00947	0.0389	0.0374	0.0368	0.0349	0.148
128.667	3.649	0.0932	0.00443	0.102	0.0358	0.123	0.0234	0.0256	0.0193	0.00499	0.00356	0.1	0.00947	0.0383	0.0367	0.0362	0.0343	0.1455
128.75	3.63	0.0915	0.00443	0.1	0.0351	0.121	0.023	0.0248	0.0188	0.00499	0.00356	0.1	0.00947	0.0376	0.0361	0.0355	0.0336	0.1428
128.833	3.612	0.0899	0.00443	0.0989	0.0344	0.119	0.0226	0.0241	0.0184	0.00499	0.00356	0.1	0.00947	0.037	0.0354	0.0349	0.033	0.1403
128.917	3.593	0.0882	0.00443	0.0972	0.0337	0.117	0.0221	0.0234	0.018	0.00499	0.00356	0.1	0.00947	0.0363	0.0348	0.0342	0.0323	0.1376
129	3.575	0.0866	0.00443	0.0956	0.0331	0.115	0.0217	0.0227	0.0176	0.00499	0.00356	0.1	0.00947	0.0357	0.0341	0.0336	0.0317	0.1351
129.083	3.556	0.085	0.00443	0.094	0.0325	0.114	0.0213	0.0221	0.0172	0.00499	0.00356	0.1	0.00947	0.0351	0.0335	0.033	0.0311	0.1327
129.167	3.538	0.0834	0.00443	0.0925	0.0318	0.112	0.0209	0.0215	0.0169	0.00499	0.00356	0.1	0.00947	0.0345	0.0329	0.0324	0.0304	0.1302
129.25	3.519	0.0819	0.00443	0.0909	0.0312	0.11	0.0205	0.0208	0.0165	0.00499	0.00356	0.1	0.00947	0.0338	0.0323	0.0317	0.0298	0.1276
129.333	3.501	0.0804	0.00443	0.0894	0.0306	0.108	0.0201	0.0203	0.0161	0.00499	0.00356	0.1	0.00947	0.0333	0.0317	0.0312	0.0292	0.1254
129.417	3.483	0.0789	0.00443	0.0879	0.03	0.106	0.0198	0.0197	0.0158	0.00499	0.00356	0.1	0.00947	0.0327	0.0311	0.0306	0.0287	0.1231
129.5	3.464	0.0775	0.00443	0.0864	0.0295	0.105	0.0194	0.0191	0.0154	0.00499	0.00356	0.1	0.00947	0.0321	0.0306	0.03	0.0281	0.1208
129.583	3.446	0.0761	0.00443	0.085	0.0289	0.103	0.019	0.0186	0.0151	0.00499	0.00356	0.1	0.00947	0.0315	0.03	0.0294	0.0275	0.1184
129.667	3.427	0.0747	0.00443	0.0836	0.0284	0.101	0.0187	0.0181	0.0147	0.00499	0.00356	0.1	0.00947	0.031	0.0295	0.0289	0.027	0.1164
129.75	3.409	0.0733	0.00443	0.0822	0.0278	0.0995	0.0183	0.0175	0.0144	0.00499	0.00356	0.1	0.00947	0.0304	0.0289	0.0283	0.0264	0.114
129.833	3.391	0.072	0.00443	0.0809	0.0273	0.0978	0.018	0.0171	0.0141	0.00499	0.00356	0.1	0.00947	0.0299	0.0284	0.0278	0.0259	0.112
129.917	3.373	0.0707	0.00443	0.0795	0.0268	0.0962	0.0177	0.0166	0.0138	0.00499	0.00356	0.1	0.00947	0.0294	0.0279	0.0273	0.0254	0.11
130	3.354	0.0693	0.00443	0.0782	0.0263	0.0945	0.0173	0.0161	0.0134	0.00499	0.00356	0.1	0.00947	0.0289	0.0273	0.0268	0.0248	0.1078
130.083	3.336	0.0681	0.00443	0.0769	0.0258	0.0929	0.017	0.0157	0.0131	0.00499	0.00356	0.1	0.00947	0.0284	0.0268	0.0263	0.0243	0.1058
130.167	3.318	0.0669	0.00443	0.0756	0.0253	0.0913	0.0167	0.0153	0.0128	0.00499	0.00356	0.1	0.00947	0.0279	0.0263	0.0258	0.0238	0.1038
130.25	3.3	0.0657	0.00443	0.0744	0.0248	0.0897	0.0164	0.0149	0.0125	0.00499	0.00356	0.1	0.00947	0.0274	0.0258	0.0253	0.0233	0.1018
130.333	3.281	0.0645	0.00443	0.0732	0.0243	0.0882	0.0161	0.0145	0.0122	0.00499	0.00356	0.1	0.00947	0.0269	0.0254	0.0248	0.0229	0.1
130.417	3.263	0.0634	0.00443	0.072	0.0239	0.0866	0.0158	0.0141	0.0119	0.00499	0.00356	0.1	0.00947	0.0264	0.0249	0.0243	0.0224	0.098
130.5	3.245	0.0623	0.00443	0.0708	0.0234	0.0851	0.0155	0.0137	0.0116	0.00499	0.00356	0.1	0.00947	0.0259	0.0244	0.0238	0.0219	0.096
130.583	3.227	0.0612	0.00443	0.0697	0.0229	0.0836	0.0152	0.0134	0.0114	0.00499	0.00356	0.1	0.00947	0.0255	0.024	0.0234	0.0215	0.0944
130.667	3.209	0.0601	0.00443	0.0685	0.0225	0.0821	0.0149	0.0131	0.0111	0.00499	0.00356	0.1	0.00947	0.025	0.0235	0.0229	0.021	0.0924
130.75	3.191	0.059	0.00443	0.0674	0.022	0.0806	0.0147	0.0127	0.0108	0.00499	0.00356	0.1	0.00947	0.0246	0.0231	0.0225	0.0206	0.0908
130.833	3.173	0.0579	0.00443	0.0663	0.0216	0.0792	0.0144	0.0125	0.0106	0.00499	0.00356	0.1	0.00947	0.0242	0.0226	0.0221	0.0204	0.0893

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
130.917	3.154	0.0568	0.00443	0.0653	0.0212	0.0777	0.0141	0.0122	0.0103	0.00499	0.00356	0.1	0.00947	0.0238	0.0222	0.0217	0.0202	0.0879
131	3.136	0.0558	0.00443	0.0642	0.0208	0.0763	0.0138	0.0119	0.0101	0.00499	0.00356	0.1	0.00947	0.0233	0.0218	0.0212	0.02	0.0863
131.083	3.118	0.0548	0.00443	0.0632	0.0204	0.0749	0.0136	0.0117	0.00986	0.00499	0.00356	0.1	0.00947	0.0229	0.0214	0.0208	0.02	0.0851
131.167	3.1	0.0537	0.00443	0.0622	0.02	0.0735	0.0133	0.0114	0.00963	0.00499	0.00356	0.1	0.00947	0.0225	0.021	0.0204	0.02	0.0839
131.25	3.082	0.0527	0.00443	0.0612	0.0196	0.0721	0.0131	0.0112	0.00941	0.00499	0.00356	0.1	0.00947	0.0221	0.0206	0.02	0.02	0.0827
131.333	3.064	0.0518	0.00443	0.0603	0.0192	0.0708	0.0128	0.011	0.0092	0.00499	0.00356	0.1	0.00947	0.0218	0.0202	0.0197	0.02	0.0817
131.417	3.046	0.0508	0.00443	0.0593	0.0188	0.0695	0.0126	0.0109	0.00899	0.00499	0.00356	0.1	0.00947	0.0214	0.0198	0.0193	0.02	0.0805
131.5	3.028	0.0498	0.00443	0.0583	0.0185	0.0681	0.0123	0.0107	0.00879	0.00499	0.00356	0.1	0.00947	0.021	0.0195	0.0189	0.02	0.0794
131.583	3.01	0.0489	0.00443	0.0574	0.0181	0.0669	0.0121	0.0106	0.0086	0.00499	0.00356	0.1	0.00947	0.0206	0.0191	0.0185	0.02	0.0782
131.667	2.992	0.048	0.00443	0.0565	0.0177	0.0656	0.0118	0.0104	0.00841	0.00499	0.00356	0.1	0.00947	0.0203	0.0187	0.0182	0.02	0.0772
131.75	2.974	0.047	0.00443	0.0556	0.0174	0.0643	0.0116	0.0103	0.00823	0.00499	0.00356	0.1	0.00947	0.0199	0.0184	0.0178	0.02	0.0761
131.833	2.956	0.0462	0.00443	0.0547	0.0171	0.0631	0.0114	0.0102	0.00806	0.00499	0.00356	0.1	0.00947	0.0196	0.018	0.0175	0.02	0.0751
131.917	2.938	0.0453	0.00443	0.0538	0.0167	0.0618	0.0111	0.0102	0.0079	0.00499	0.00356	0.1	0.00947	0.0192	0.0177	0.0171	0.02	0.074
132	2.921	0.0444	0.00443	0.0529	0.0164	0.0606	0.0109	0.0101	0.00773	0.00499	0.00356	0.1	0.00947	0.0189	0.0173	0.0168	0.02	0.073
132.083	2.903	0.0435	0.00443	0.052	0.0161	0.0594	0.0107	0.0101	0.00758	0.00499	0.00356	0.1	0.00947	0.0185	0.017	0.0164	0.02	0.0719
132.167	2.885	0.0427	0.00443	0.0512	0.0158	0.0582	0.0105	0.01	0.00743	0.00499	0.00356	0.1	0.00947	0.0182	0.0167	0.0161	0.02	0.071
132.25	2.867	0.0419	0.00443	0.0503	0.0155	0.0571	0.0103	0.01	0.00727	0.00499	0.00356	0.1	0.00947	0.0179	0.0163	0.0157	0.02	0.0699
132.333	2.849	0.0411	0.00443	0.0495	0.0152	0.0559	0.01	0.01	0.00714	0.00499	0.00356	0.1	0.00947	0.0175	0.016	0.0154	0.02	0.0689
132.417	2.831	0.0403	0.00443	0.0487	0.0149	0.0548	0.00983	0.01	0.007	0.00499	0.00356	0.1	0.00947	0.0172	0.0157	0.0151	0.02	0.068
132.5	2.813	0.0395	0.00443	0.0478	0.0146	0.0537	0.00961	0.01	0.00686	0.00499	0.00356	0.1	0.00947	0.0169	0.0154	0.0148	0.02	0.0671
132.583	2.796	0.0387	0.00443	0.047	0.0143	0.0526	0.00942	0.01	0.00674	0.00499	0.00356	0.1	0.00947	0.0166	0.015	0.0145	0.02	0.0661
132.667	2.778	0.038	0.00443	0.0463	0.0141	0.0515	0.00923	0.01	0.00661	0.00499	0.00356	0.1	0.00947	0.0163	0.0147	0.0141	0.02	0.0651
132.75	2.76	0.0372	0.00443	0.0455	0.0138	0.0505	0.00904	0.01	0.00649	0.00499	0.00356	0.1	0.00947	0.0159	0.0144	0.0138	0.02	0.0641
132.833	2.742	0.0365	0.00443	0.0447	0.0136	0.0494	0.00884	0.01	0.00638	0.00499	0.00356	0.1	0.00947	0.0156	0.0141	0.0135	0.02	0.0632
132.917	2.725	0.0358	0.00443	0.044	0.0133	0.0484	0.00865	0.01	0.00627	0.00499	0.00356	0.1	0.00947	0.0153	0.0138	0.0132	0.02	0.0623
133	2.707	0.0351	0.00443	0.0432	0.0131	0.0474	0.00846	0.01	0.00615	0.00499	0.00356	0.1	0.00947	0.015	0.0135	0.0129	0.02	0.0614
133.083	2.689	0.0344	0.00443	0.0425	0.0129	0.0464	0.00829	0.01	0.00606	0.00499	0.00356	0.1	0.00947	0.0148	0.0132	0.0127	0.02	0.0607
133.167	2.671	0.0338	0.00443	0.0418	0.0126	0.0454	0.00812	0.01	0.00596	0.00499	0.00356	0.1	0.00947	0.0145	0.0129	0.0124	0.02	0.0598
133.25	2.654	0.0331	0.00443	0.041	0.0124	0.0445	0.00795	0.01	0.00586	0.00499	0.00356	0.1	0.00947	0.0142	0.0127	0.0121	0.02	0.059
133.333	2.636	0.0325	0.00443	0.0404	0.0122	0.0435	0.00778	0.01	0.00578	0.00499	0.00356	0.1	0.00947	0.0139	0.0124	0.0118	0.02	0.0581
133.417	2.618	0.0319	0.00443	0.0397	0.012	0.0426	0.00761	0.01	0.0057	0.00499	0.00356	0.1	0.00947	0.0137	0.0121	0.0115	0.02	0.0573
133.5	2.601	0.0313	0.00443	0.039	0.0118	0.0417	0.00744	0.01	0.00562	0.00499	0.00356	0.1	0.00947	0.0134	0.0118	0.0113	0.02	0.0565
133.583	2.583	0.0308	0.00443	0.0384	0.0116	0.0408	0.00729	0.01	0.00555	0.00499	0.00356	0.1	0.00947	0.0131	0.0116	0.011	0.02	0.0557
133.667	2.565	0.0302	0.00443	0.0377	0.0114	0.04	0.00714	0.01	0.00548	0.00499	0.00356	0.1	0.00947	0.0129	0.0113	0.0108	0.02	0.055
133.75	2.548	0.0297	0.00443	0.0371	0.0113	0.0391	0.00699	0.01	0.00541	0.00499	0.00356	0.1	0.00947	0.0126	0.0111	0.0105	0.02	0.0542
133.833	2.53	0.0291	0.00443	0.0364	0.0111	0.0383	0.00685	0.01	0.00535	0.00499	0.00356	0.1	0.00947	0.0124	0.0108	0.0103	0.02	0.0535
133.917	2.513	0.0286	0.00443	0.0358	0.0109	0.0375	0.00671	0.01	0.0053	0.00499	0.00356	0.1	0.00947	0.0121	0.0106	0.01	0.02	0.0527
134	2.495	0.0281	0.00443	0.0352	0.0108	0.0367	0.00657	0.01	0.00524	0.00499	0.00356	0.1	0.00947	0.0119	0.0104	0.00979	0.02	0.05209
134.083	2.478	0.0277	0.00443	0.0346	0.0106	0.0359	0.00644	0.01	0.0052	0.00499	0.00356	0.1	0.00947	0.0117	0.0101	0.00955	0.02	0.05135
134.167	2.46	0.0272	0.00443	0.034	0.0105	0.0351	0.00631	0.01	0.00516	0.00499	0.00356	0.1	0.00947	0.0114	0.00989	0.00931	0.02	0.0506
134.25	2.442	0.0267	0.00443	0.0335	0.0103	0.0344	0.00618	0.01	0.00512	0.00499	0.00356	0.1	0.00947	0.0112	0.00965	0.00908	0.02	0.04993
134.333	2.425	0.0263	0.00443	0.0329	0.0102	0.0337	0.00606	0.01	0.00509	0.00499	0.00356	0.1	0.00947	0.011	0.00944	0.00886	0.02	0.0493
134.417	2.407	0.0259	0.00443	0.0324	0.01	0.0329	0.00594	0.01	0.00506	0.00499	0.00356	0.1	0.00947	0.0108	0.00923	0.00865	0.02	0.04868
134.5	2.39	0.0254	0.00443	0.0318	0.00988	0.0322	0.00582	0.01	0.00504	0.00499	0.00356	0.1	0.00947	0.0106	0.00901	0.00843	0.02	0.04804
134.583	2.373	0.025	0.00443	0.0313	0.00976	0.0316	0.00571	0.01	0.00502	0.00499	0.00356	0.1	0.00947	0.0104	0.00882	0.00824	0.02	0.04746
134.667	2.355	0.0247	0.00443	0.0308	0.00963	0.0309	0.00561	0.01	0.00501	0.00499	0.00356	0.1	0.00947	0.0102	0.00862	0.00805	0.02	0.04687
134.75	2.338	0.0243	0.00443	0.0303	0.0095	0.0303	0.0055	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00998	0.00843	0.00785	0.02	0.04626
134.833	2.32	0.0239	0.00443	0.0298	0.00939	0.0296	0.0054	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00978	0.00823	0.00766	0.02	0.04567
134.917	2.303	0.0236	0.00443	0.0293	0.00928	0.029	0.0053	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00959	0.00804	0.00746	0.02	0.04509
135	2.285	0.0232	0.00443	0.0289	0.00917	0.0284	0.0052	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00939	0.00785	0.00727	0.02	0.04451
135.083	2.268	0.0229	0.00443	0.0284	0.00909	0.0279	0.00512	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00922	0.00767	0.0071	0.02	0.04399
135.167	2.251	0.0226	0.00443	0.028	0.009	0.0273	0.00503	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00905	0.0075	0.00692	0.02	0.04347
135.25	2.233	0.0223	0.00443	0.0275	0.00892	0.0268	0.00495	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00888	0.00733	0.00675	0.02	0.04296
135.333	2.216	0.022	0.00443	0.0271	0.00885	0.0263	0.00486	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00872	0.00717	0.0066	0.02	0.04249
135.417	2.198	0.0217	0.00443	0.0267	0.00878	0.0258	0.00478	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00857	0.00702	0.00644	0.02	0.04203
135.5	2.181	0.0214	0.00443	0.0263	0.00871	0.0253	0.00469	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00842	0.00687	0.00629	0.02	0.04158
135.583	2.164	0.0211	0.00443	0.0259	0.00865	0.0248	0.00462	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00827	0.00672	0.00614	0.02	0.04113
135.667	2.147	0.0209	0.00443	0.0255	0.0086	0.0244	0.00455	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00811	0.00656	0.00599	0.02	0.04066
135.75	2.129	0.0206	0.00443	0.0252	0.00854	0.0239	0.00448	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00796	0.00641	0.00583	0.02	0.0402
135.833	2.112	0.0204	0.00443	0.0248	0.0085	0.0235	0.00441	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00783	0.00628	0.0057	0.02	0.03981
135.917	2.095	0.0202	0.00443	0.0245	0.00846	0.0231	0.00433	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0077	0.00615	0.00557	0.02	0.03942
136	2.077	0.0199	0.00443	0.0241	0.00841	0.0227	0.00426	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00757	0.00602	0.00544	0.02	0.03903
136.083	2.06	0.0197	0.00443	0.0238	0.00839	0.0223	0.00421	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00746	0.00591	0.00533	0.02	0.0387

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
136.167	2.043	0.0195	0.00443	0.0235	0.00836	0.0219	0.00415	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00735	0.00579	0.00522	0.02	0.03836
136.25	2.026	0.0193	0.00443	0.0232	0.00833	0.0216	0.00409	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00723	0.00568	0.00511	0.02	0.03802
136.333	2.009	0.0192	0.00443	0.023	0.00832	0.0212	0.00404	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00712	0.00557	0.005	0.02	0.03769
136.417	1.991	0.019	0.00443	0.0227	0.0083	0.0209	0.00398	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00701	0.00546	0.00488	0.02	0.03735
136.5	1.974	0.0188	0.00443	0.0224	0.00829	0.0206	0.00392	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0069	0.00535	0.00477	0.02	0.03702
136.583	1.957	0.0187	0.00443	0.0222	0.00829	0.0203	0.00388	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0068	0.00525	0.00468	0.02	0.03673
136.667	1.94	0.0186	0.00443	0.0219	0.00829	0.0199	0.00384	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00671	0.00516	0.00458	0.02	0.03645
136.75	1.923	0.0184	0.00443	0.0217	0.00829	0.0196	0.00379	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00661	0.00506	0.00448	0.02	0.03615
136.833	1.905	0.0183	0.00443	0.0214	0.00829	0.0194	0.00377	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00653	0.00497	0.0044	0.02	0.0359
136.917	1.888	0.0182	0.00443	0.0212	0.00829	0.0191	0.00374	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00644	0.00489	0.00431	0.02	0.03564
137	1.871	0.0181	0.00443	0.021	0.00829	0.0188	0.00371	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00636	0.00481	0.00423	0.02	0.0354
137.083	1.854	0.0181	0.00443	0.0208	0.00829	0.0186	0.00368	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00628	0.00472	0.00415	0.02	0.03515
137.167	1.837	0.018	0.00443	0.0206	0.00829	0.0184	0.00365	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00619	0.00464	0.00406	0.02	0.03489
137.25	1.82	0.0179	0.00443	0.0204	0.00829	0.0181	0.00362	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00611	0.00456	0.00398	0.02	0.03465
137.333	1.803	0.0179	0.00443	0.0202	0.00829	0.0179	0.00361	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00604	0.00449	0.00391	0.02	0.03444
137.417	1.786	0.0178	0.00443	0.02	0.00829	0.0177	0.00359	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00597	0.00442	0.00384	0.02	0.03423
137.5	1.769	0.0178	0.00443	0.0198	0.00829	0.0175	0.00358	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0059	0.00435	0.00377	0.02	0.03402
137.583	1.752	0.0178	0.00443	0.0197	0.00829	0.0174	0.00357	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00585	0.00429	0.00372	0.02	0.03386
137.667	1.735	0.0178	0.00443	0.0195	0.00829	0.0172	0.00355	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00579	0.00424	0.00366	0.02	0.03369
137.75	1.718	0.0178	0.00443	0.0193	0.00829	0.0171	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00573	0.00418	0.00361	0.02	0.03352
137.833	1.701	0.0178	0.00443	0.0192	0.00829	0.0169	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00568	0.00413	0.00355	0.02	0.03336
137.917	1.684	0.0178	0.00443	0.0191	0.00829	0.0168	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00562	0.00407	0.00349	0.02	0.03318
138	1.667	0.0178	0.00443	0.0189	0.00829	0.0167	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00557	0.00402	0.00344	0.02	0.03303
138.083	1.65	0.0178	0.00443	0.0188	0.00829	0.0166	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00553	0.00397	0.0034	0.02	0.0329
138.167	1.633	0.0178	0.00443	0.0187	0.00829	0.0165	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00548	0.00393	0.00335	0.02	0.03276
138.25	1.616	0.0178	0.00443	0.0186	0.00829	0.0164	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00544	0.00389	0.00331	0.02	0.03264
138.333	1.599	0.0178	0.00443	0.0185	0.00829	0.0163	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00542	0.00386	0.00329	0.02	0.03257
138.417	1.582	0.0178	0.00443	0.0184	0.00829	0.0163	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00539	0.00384	0.00326	0.02	0.03249
138.5	1.565	0.0178	0.00443	0.0183	0.00829	0.0162	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00536	0.00381	0.00323	0.02	0.0324
138.583	1.548	0.0178	0.00443	0.0183	0.00829	0.0162	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00533	0.00378	0.0032	0.02	0.03231
138.667	1.531	0.0178	0.00443	0.0182	0.00829	0.0162	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.0053	0.00375	0.00317	0.02	0.03222
138.75	1.515	0.0178	0.00443	0.0181	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00528	0.00372	0.00315	0.02	0.03215
138.833	1.498	0.0178	0.00443	0.0181	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00526	0.00371	0.00313	0.02	0.0321
138.917	1.481	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00525	0.0037	0.00312	0.02	0.03207
139	1.464	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.083	1.448	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.167	1.431	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.25	1.415	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.333	1.399	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.417	1.383	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.5	1.367	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.583	1.352	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.667	1.336	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.75	1.321	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.833	1.306	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
139.917	1.291	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140	1.276	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.083	1.262	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.167	1.247	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.25	1.233	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.333	1.219	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.417	1.205	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.5	1.191	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.583	1.177	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.667	1.163	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.75	1.15	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.833	1.137	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
140.917	1.124	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141	1.11	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.083	1.098	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.167	1.085	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.25	1.072	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.333	1.06	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
141.417	1.048	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.5	1.036	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.583	1.024	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.667	1.012	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.75	1	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.833	0.989	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
141.917	0.977	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142	0.966	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.083	0.955	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.167	0.944	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.25	0.933	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.333	0.923	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.417	0.912	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.5	0.902	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.583	0.891	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.667	0.881	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.75	0.871	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.833	0.861	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
142.917	0.852	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143	0.842	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.083	0.833	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.167	0.823	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.25	0.814	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.333	0.809	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.417	0.805	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
143.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
144.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
145.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
146.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
146.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
147.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
148.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
149.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
150.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
151.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
151.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
152.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
153.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
154.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
155.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
156.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
157.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
157.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
158.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
159.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
160.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
161.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
162.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
162.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
163.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
164.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
165.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
166.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
167.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
167.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
168.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
169.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
170.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
171.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
172.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
172.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
173.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
174.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
175.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
176.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
177.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
178.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
178.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
179.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
180.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
181.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
182.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
183.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
183.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
184.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
185.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
186.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
187.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
188.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
188.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
189.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
190.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
191.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
192.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
193.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
193.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
194.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
195.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
196.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
197.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
198.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
199.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
199.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
200.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
201.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
202.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
203.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
204.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
204.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
205.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
206.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
207.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
208.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
209.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
209.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
210.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
211.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
212.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
213.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
214.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
214.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
215.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
216.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
217.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
218.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
219.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
220.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
220.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
221.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
222.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
223.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
224.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
225.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
225.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
226.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
227.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
228.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
229.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
230.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
230.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
231.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
232.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
233.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
234.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
235.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
235.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
236.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
237.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
238.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
239.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
240.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
241.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
241.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
242.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
243.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
244.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
245.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
246.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
246.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
247.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
248.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
249.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
250.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
251.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
251.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
252.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
253.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
254.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
255.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
256.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
256.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
257.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
258.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
259.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
260.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
261.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
262.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
262.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
263.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
264.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
265.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
266.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
267.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
267.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
268.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
269.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
270.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
271.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
272.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
272.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
273.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
274.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
275.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
276.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
277.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
277.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
278.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
279.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
280.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
281.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
282.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
283.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
283.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
284.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
285.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
286.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
287.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
288.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
288.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
289.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
290.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
291.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
292.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
293.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
293.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
294.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
295.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
296.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
297.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
298.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

Flow

Time (hr)	MINS_US	MINS_WESTLE	MINS_WARKBAR	MINS_WASH	MINS_THEBERT	MINS_POTTERS	MINS_SCOTT	MINS_DOCWRA	MINS_EASTBR	LEIS_UPPER	LEIS_LOVERS	LEIS_ABBEY	LEIS_LEISTON	LEIS_SIZEW1	LEIS_SIZEW2	LEIS_SIZEW3	LEIS_SIZEW4	SEIZEWELL
298.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.083	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.167	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.25	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.333	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.417	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.5	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.583	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.667	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.75	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.833	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
299.917	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201
300	0.8	0.0178	0.00443	0.018	0.00829	0.0161	0.00354	0.01	0.00499	0.00499	0.00356	0.1	0.00947	0.00523	0.00368	0.0031	0.02	0.03201

APPENDIX E: REFH2 FEH13 FLOOD MODELLER OUTPUT REPORTS

UK Design Flood Estimation

Generated on 11 May 2021 15:59:46 by AEA_COMPUTER
Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH2)

Site details Checksum: AAB1-2957

Site name: tmp4C69

Easting: 644950

Northing: 263550

Country: England, Wales or Northern Ireland

Catchment Area (km²): 2.83

Using plot scale calculations: No

Model: ReFH2.2

Site description: None

Model run: 100 year - LEIS_ABBEY

Summary of results

Rainfall - FEH 2013 model (mm):	122.91	Total runoff (ML):	53.50
Total Rainfall (mm):	82.29	Total flow (ML):	125.27
Peak Rainfall (mm):	1.80	Peak flow (m³/s):	0.46

Parameters

Where the user has overriden a system-generated value, this original value is shown in square brackets after the value used.
** Indicates that the user locked the duration/timestep*

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	121:00:00 [09:00:00]	Yes
Timestep (hh:mm:ss)	01:00:00	No
SCF (Seasonal correction factor)	0.68	No
ARF (Areal reduction factor)	0.99	No
Seasonality	Winter	No

Loss model parameters

Name	Value	User-defined?
Cini (mm)	93.96	No
Cmax (mm)	605.86	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No
Use seasonal CIni for equations	No [Yes]	Yes

Routing model parameters

Name	Value	User-defined?
Tp (hr)	5.28	No
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m^3/s)	0.04	No
BL (hr)	47.5	No
BR	1.45	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km^2)	0.13	No
Urbext 2000	0.03	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Exporting drained area (km^2)	0.00	Yes
Sewer capacity (m^3/s)	0.00	Yes

Time series data

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
00:00:00	0.128	0.000	0.021	0.000	0.045	0.045
01:00:00	0.135	0.000	0.022	0.000	0.044	0.044
02:00:00	0.141	0.000	0.023	0.001	0.043	0.044
03:00:00	0.148	0.000	0.024	0.002	0.042	0.044
04:00:00	0.155	0.000	0.025	0.004	0.041	0.045
05:00:00	0.162	0.000	0.027	0.006	0.040	0.046
06:00:00	0.170	0.000	0.028	0.008	0.040	0.048
07:00:00	0.179	0.000	0.029	0.010	0.039	0.049
08:00:00	0.187	0.000	0.031	0.012	0.039	0.051
09:00:00	0.196	0.000	0.032	0.014	0.038	0.052
10:00:00	0.206	0.000	0.034	0.016	0.038	0.053
11:00:00	0.215	0.000	0.036	0.017	0.037	0.055
12:00:00	0.226	0.000	0.038	0.019	0.037	0.056
13:00:00	0.237	0.000	0.039	0.020	0.037	0.057
14:00:00	0.248	0.000	0.041	0.022	0.037	0.058
15:00:00	0.260	0.000	0.044	0.023	0.037	0.060
16:00:00	0.272	0.000	0.046	0.025	0.036	0.061
17:00:00	0.285	0.000	0.048	0.026	0.036	0.063
18:00:00	0.299	0.000	0.050	0.028	0.036	0.064
19:00:00	0.313	0.000	0.053	0.029	0.036	0.065
20:00:00	0.328	0.000	0.056	0.031	0.036	0.067
21:00:00	0.344	0.000	0.059	0.032	0.036	0.069
22:00:00	0.360	0.000	0.062	0.034	0.037	0.070
23:00:00	0.377	0.000	0.065	0.035	0.037	0.072
24:00:00	0.395	0.000	0.068	0.037	0.037	0.074
25:00:00	0.414	0.000	0.072	0.039	0.037	0.076
26:00:00	0.433	0.000	0.075	0.041	0.038	0.079
27:00:00	0.454	0.000	0.079	0.043	0.038	0.081
28:00:00	0.475	0.000	0.083	0.045	0.038	0.084
29:00:00	0.498	0.000	0.087	0.048	0.039	0.086
30:00:00	0.521	0.000	0.092	0.050	0.039	0.089
31:00:00	0.546	0.000	0.097	0.053	0.040	0.093
32:00:00	0.571	0.000	0.102	0.055	0.040	0.096
33:00:00	0.598	0.000	0.107	0.058	0.041	0.099
34:00:00	0.626	0.000	0.113	0.061	0.042	0.103

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
35:00:00	0.655	0.000	0.119	0.064	0.043	0.107
36:00:00	0.686	0.000	0.125	0.068	0.044	0.111
37:00:00	0.718	0.000	0.132	0.071	0.045	0.116
38:00:00	0.751	0.000	0.139	0.075	0.046	0.121
39:00:00	0.786	0.000	0.146	0.079	0.047	0.126
40:00:00	0.822	0.000	0.154	0.083	0.048	0.131
41:00:00	0.860	0.000	0.162	0.087	0.049	0.137
42:00:00	0.899	0.000	0.171	0.092	0.051	0.143
43:00:00	0.940	0.000	0.180	0.097	0.052	0.149
44:00:00	0.983	0.000	0.190	0.102	0.054	0.156
45:00:00	1.028	0.000	0.200	0.107	0.056	0.163
46:00:00	1.074	0.000	0.211	0.113	0.057	0.171
47:00:00	1.123	0.000	0.223	0.119	0.059	0.179
48:00:00	1.173	0.000	0.235	0.126	0.062	0.187
49:00:00	1.225	0.000	0.248	0.132	0.064	0.196
50:00:00	1.279	0.000	0.261	0.139	0.066	0.206
51:00:00	1.335	0.000	0.275	0.147	0.069	0.216
52:00:00	1.392	0.000	0.290	0.155	0.071	0.226
53:00:00	1.451	0.000	0.306	0.163	0.074	0.237
54:00:00	1.512	0.000	0.323	0.172	0.077	0.249
55:00:00	1.574	0.000	0.340	0.181	0.080	0.262
56:00:00	1.636	0.000	0.357	0.191	0.084	0.275
57:00:00	1.697	0.000	0.375	0.202	0.088	0.289
58:00:00	1.755	0.000	0.393	0.212	0.091	0.304
59:00:00	1.798	0.000	0.408	0.224	0.095	0.319
60:00:00	1.778	0.000	0.409	0.236	0.100	0.335
61:00:00	1.798	0.000	0.418	0.247	0.104	0.352
62:00:00	1.755	0.000	0.413	0.259	0.109	0.368
63:00:00	1.697	0.000	0.405	0.270	0.114	0.385
64:00:00	1.636	0.000	0.394	0.281	0.119	0.400
65:00:00	1.574	0.000	0.384	0.289	0.125	0.414
66:00:00	1.512	0.000	0.372	0.296	0.130	0.426
67:00:00	1.451	0.000	0.361	0.301	0.136	0.436
68:00:00	1.392	0.000	0.349	0.303	0.142	0.445
69:00:00	1.335	0.000	0.338	0.304	0.147	0.451
70:00:00	1.279	0.000	0.326	0.302	0.152	0.455

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
71:00:00	1.225	0.000	0.315	0.299	0.158	0.457
72:00:00	1.173	0.000	0.304	0.295	0.163	0.458
73:00:00	1.123	0.000	0.293	0.290	0.168	0.458
74:00:00	1.074	0.000	0.282	0.284	0.172	0.456
75:00:00	1.028	0.000	0.272	0.277	0.177	0.454
76:00:00	0.983	0.000	0.262	0.270	0.181	0.451
77:00:00	0.940	0.000	0.252	0.262	0.184	0.447
78:00:00	0.899	0.000	0.242	0.254	0.188	0.442
79:00:00	0.860	0.000	0.233	0.246	0.191	0.437
80:00:00	0.822	0.000	0.224	0.237	0.194	0.431
81:00:00	0.786	0.000	0.215	0.229	0.197	0.426
82:00:00	0.751	0.000	0.206	0.221	0.199	0.420
83:00:00	0.718	0.000	0.198	0.213	0.201	0.414
84:00:00	0.686	0.000	0.190	0.205	0.203	0.408
85:00:00	0.655	0.000	0.182	0.197	0.204	0.401
86:00:00	0.626	0.000	0.175	0.190	0.205	0.395
87:00:00	0.598	0.000	0.168	0.183	0.206	0.389
88:00:00	0.571	0.000	0.161	0.175	0.207	0.383
89:00:00	0.546	0.000	0.154	0.169	0.208	0.376
90:00:00	0.521	0.000	0.147	0.162	0.208	0.370
91:00:00	0.498	0.000	0.141	0.155	0.208	0.364
92:00:00	0.475	0.000	0.135	0.149	0.208	0.358
93:00:00	0.454	0.000	0.129	0.143	0.208	0.351
94:00:00	0.433	0.000	0.124	0.137	0.208	0.345
95:00:00	0.414	0.000	0.119	0.132	0.207	0.339
96:00:00	0.395	0.000	0.114	0.126	0.207	0.333
97:00:00	0.377	0.000	0.109	0.121	0.206	0.327
98:00:00	0.360	0.000	0.104	0.116	0.205	0.321
99:00:00	0.344	0.000	0.099	0.111	0.204	0.315
100:00:00	0.328	0.000	0.095	0.106	0.203	0.309
101:00:00	0.313	0.000	0.091	0.102	0.201	0.303
102:00:00	0.299	0.000	0.087	0.098	0.200	0.298
103:00:00	0.285	0.000	0.083	0.093	0.199	0.292
104:00:00	0.272	0.000	0.079	0.089	0.197	0.287
105:00:00	0.260	0.000	0.076	0.086	0.196	0.281
106:00:00	0.248	0.000	0.073	0.082	0.194	0.276

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
107:00:00	0.237	0.000	0.069	0.078	0.192	0.270
108:00:00	0.226	0.000	0.066	0.075	0.190	0.265
109:00:00	0.215	0.000	0.063	0.072	0.188	0.260
110:00:00	0.206	0.000	0.060	0.068	0.186	0.255
111:00:00	0.196	0.000	0.058	0.065	0.185	0.250
112:00:00	0.187	0.000	0.055	0.063	0.182	0.245
113:00:00	0.179	0.000	0.053	0.060	0.180	0.240
114:00:00	0.170	0.000	0.050	0.057	0.178	0.236
115:00:00	0.162	0.000	0.048	0.055	0.176	0.231
116:00:00	0.155	0.000	0.046	0.052	0.174	0.226
117:00:00	0.148	0.000	0.044	0.050	0.172	0.222
118:00:00	0.141	0.000	0.042	0.048	0.170	0.217
119:00:00	0.135	0.000	0.040	0.046	0.168	0.213
120:00:00	0.128	0.000	0.038	0.043	0.165	0.209
121:00:00	0.000	0.000	0.000	0.042	0.163	0.205
122:00:00	0.000	0.000	0.000	0.039	0.161	0.200
123:00:00	0.000	0.000	0.000	0.036	0.159	0.195
124:00:00	0.000	0.000	0.000	0.033	0.156	0.189
125:00:00	0.000	0.000	0.000	0.029	0.154	0.183
126:00:00	0.000	0.000	0.000	0.024	0.151	0.176
127:00:00	0.000	0.000	0.000	0.020	0.149	0.169
128:00:00	0.000	0.000	0.000	0.016	0.146	0.162
129:00:00	0.000	0.000	0.000	0.013	0.144	0.156
130:00:00	0.000	0.000	0.000	0.010	0.141	0.151
131:00:00	0.000	0.000	0.000	0.008	0.138	0.146
132:00:00	0.000	0.000	0.000	0.006	0.136	0.142
133:00:00	0.000	0.000	0.000	0.005	0.133	0.138
134:00:00	0.000	0.000	0.000	0.003	0.130	0.134
135:00:00	0.000	0.000	0.000	0.002	0.128	0.130
136:00:00	0.000	0.000	0.000	0.001	0.125	0.127
137:00:00	0.000	0.000	0.000	0.001	0.123	0.123
138:00:00	0.000	0.000	0.000	0.000	0.120	0.120
139:00:00	0.000	0.000	0.000	0.000	0.118	0.118
140:00:00	0.000	0.000	0.000	0.000	0.115	0.115
141:00:00	0.000	0.000	0.000	0.000	0.113	0.113
142:00:00	0.000	0.000	0.000	0.000	0.110	0.110

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
143:00:00	0.000	0.000	0.000	0.000	0.108	0.108
144:00:00	0.000	0.000	0.000	0.000	0.106	0.106
145:00:00	0.000	0.000	0.000	0.000	0.104	0.104
146:00:00	0.000	0.000	0.000	0.000	0.101	0.101
147:00:00	0.000	0.000	0.000	0.000	0.099	0.099
148:00:00	0.000	0.000	0.000	0.000	0.097	0.097
149:00:00	0.000	0.000	0.000	0.000	0.095	0.095
150:00:00	0.000	0.000	0.000	0.000	0.093	0.093
151:00:00	0.000	0.000	0.000	0.000	0.091	0.091
152:00:00	0.000	0.000	0.000	0.000	0.089	0.089
153:00:00	0.000	0.000	0.000	0.000	0.088	0.088
154:00:00	0.000	0.000	0.000	0.000	0.086	0.086
155:00:00	0.000	0.000	0.000	0.000	0.084	0.084
156:00:00	0.000	0.000	0.000	0.000	0.082	0.082
157:00:00	0.000	0.000	0.000	0.000	0.080	0.080
158:00:00	0.000	0.000	0.000	0.000	0.079	0.079
159:00:00	0.000	0.000	0.000	0.000	0.077	0.077
160:00:00	0.000	0.000	0.000	0.000	0.076	0.076
161:00:00	0.000	0.000	0.000	0.000	0.074	0.074
162:00:00	0.000	0.000	0.000	0.000	0.072	0.072
163:00:00	0.000	0.000	0.000	0.000	0.071	0.071
164:00:00	0.000	0.000	0.000	0.000	0.069	0.069
165:00:00	0.000	0.000	0.000	0.000	0.068	0.068
166:00:00	0.000	0.000	0.000	0.000	0.067	0.067
167:00:00	0.000	0.000	0.000	0.000	0.065	0.065
168:00:00	0.000	0.000	0.000	0.000	0.064	0.064
169:00:00	0.000	0.000	0.000	0.000	0.063	0.063
170:00:00	0.000	0.000	0.000	0.000	0.061	0.061
171:00:00	0.000	0.000	0.000	0.000	0.060	0.060
172:00:00	0.000	0.000	0.000	0.000	0.059	0.059
173:00:00	0.000	0.000	0.000	0.000	0.057	0.057
174:00:00	0.000	0.000	0.000	0.000	0.056	0.056
175:00:00	0.000	0.000	0.000	0.000	0.055	0.055
176:00:00	0.000	0.000	0.000	0.000	0.054	0.054
177:00:00	0.000	0.000	0.000	0.000	0.053	0.053
178:00:00	0.000	0.000	0.000	0.000	0.052	0.052

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
179:00:00	0.000	0.000	0.000	0.000	0.051	0.051
180:00:00	0.000	0.000	0.000	0.000	0.050	0.050
181:00:00	0.000	0.000	0.000	0.000	0.049	0.049
182:00:00	0.000	0.000	0.000	0.000	0.048	0.048
183:00:00	0.000	0.000	0.000	0.000	0.047	0.047
184:00:00	0.000	0.000	0.000	0.000	0.046	0.046

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Appendix

Catchment descriptors

Name	Value	User-defined value used?
Area (km^2)	2.83	No
ALTBAR	17	No
ASPBAR	0.47	No
ASPVAR	0	No
BFIHOST	0.63	No
DPLBAR (km)	1.52	No
DPSBAR (mkm^{-1})	11	No
FARL	1	No
LDP	2.98	No
PROPWET (mm)	0.26	No
RMED1H	10.9	No
RMED1D	29.7	No
RMED2D	37.6	No
SAAR (mm)	594	No
SAAR4170 (mm)	596	No
SPRHOST	27.83	No
Urbext2000	0.03	No
Urbext1990	0.01	No
URBCONC	0.71	No
URBLOC	0.8	No
DDF parameter C	-0.02	No
DDF parameter D1	0.3	No
DDF parameter D2	0.28	No
DDF parameter D3	0.23	No
DDF parameter E	0.31	No
DDF parameter F	2.5	No
DDF parameter C (1km grid value)	-0.02	No
DDF parameter D1 (1km grid value)	0.3	No
DDF parameter D2 (1km grid value)	0.27	No
DDF parameter D3 (1km grid value)	0.22	No
DDF parameter E (1km grid value)	0.31	No
DDF parameter F (1km grid value)	2.49	No

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UK Design Flood Estimation

Generated on 11 May 2021 15:59:15 by AEA_COMPUTER
Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH2)

Site details Checksum: 61E0-4309

Site name: tmpD573

Easting: 643000

Northing: 268100

Country: England, Wales or Northern Ireland

Catchment Area (km²): 50.16

Using plot scale calculations: No

Model: ReFH2.2

Site description: None

Model run: 100 year - MINS_US

Summary of results

Rainfall - FEH 2013 model (mm):	128.48	Total runoff (ML):	2548.74
Total Rainfall (mm):	84.81	Total flow (ML):	4315.44
Peak Rainfall (mm):	1.85	Peak flow (m³/s):	16.79

Parameters

Where the user has overriden a system-generated value, this original value is shown in square brackets after the value used.
** Indicates that the user locked the duration/timestep*

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	121:00:00 [18:00:00]	Yes
Timestep (hh:mm:ss)	01:00:00 [02:00:00]	Yes
SCF (Seasonal correction factor)	0.68	No
ARF (Areal reduction factor)	0.98	No
Seasonality	Winter	No

Loss model parameters

Name	Value	User-defined?
Cini (mm)	144.63	No
Cmax (mm)	312.39	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No
Use seasonal CIni for equations	No [Yes]	Yes

Routing model parameters

Name	Value	User-defined?
Tp (hr)	10.97	No
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m^3/s)	2.41	No
BL (hr)	50.53	No
BR	0.8	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km^2)	0.71	No
Urbext 2000	0.01	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Exporting drained area (km^2)	0.00	Yes
Sewer capacity (m^3/s)	0.00	Yes

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time series data

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
00:00:00	0.132	0.000	0.061	0.000	2.413	2.413
01:00:00	0.139	0.000	0.064	0.002	2.366	2.369
02:00:00	0.145	0.000	0.068	0.010	2.320	2.330
03:00:00	0.152	0.000	0.071	0.022	2.275	2.297
04:00:00	0.160	0.000	0.074	0.040	2.230	2.271
05:00:00	0.167	0.000	0.078	0.064	2.188	2.252
06:00:00	0.176	0.000	0.082	0.094	2.146	2.240
07:00:00	0.184	0.000	0.086	0.130	2.105	2.235
08:00:00	0.193	0.000	0.090	0.171	2.066	2.238
09:00:00	0.202	0.000	0.095	0.220	2.029	2.248
10:00:00	0.212	0.000	0.099	0.275	1.993	2.267
11:00:00	0.222	0.000	0.104	0.337	1.958	2.295
12:00:00	0.233	0.000	0.110	0.402	1.925	2.328
13:00:00	0.244	0.000	0.115	0.469	1.894	2.363
14:00:00	0.256	0.000	0.121	0.535	1.865	2.400
15:00:00	0.268	0.000	0.127	0.603	1.837	2.440
16:00:00	0.281	0.000	0.133	0.671	1.810	2.481
17:00:00	0.294	0.000	0.140	0.739	1.786	2.525
18:00:00	0.308	0.000	0.147	0.809	1.762	2.571
19:00:00	0.323	0.000	0.154	0.879	1.741	2.619
20:00:00	0.338	0.000	0.162	0.949	1.720	2.670
21:00:00	0.354	0.000	0.170	1.021	1.702	2.723
22:00:00	0.371	0.000	0.178	1.093	1.684	2.778
23:00:00	0.389	0.000	0.187	1.168	1.669	2.836
24:00:00	0.407	0.000	0.197	1.245	1.654	2.899
25:00:00	0.426	0.000	0.207	1.324	1.641	2.965
26:00:00	0.447	0.000	0.217	1.406	1.630	3.036
27:00:00	0.468	0.000	0.228	1.492	1.620	3.112
28:00:00	0.490	0.000	0.239	1.580	1.612	3.192
29:00:00	0.513	0.000	0.251	1.672	1.605	3.277
30:00:00	0.537	0.000	0.264	1.767	1.600	3.367
31:00:00	0.562	0.000	0.278	1.866	1.596	3.462
32:00:00	0.589	0.000	0.292	1.968	1.594	3.563
33:00:00	0.616	0.000	0.307	2.075	1.594	3.669
34:00:00	0.645	0.000	0.322	2.186	1.595	3.781

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
35:00:00	0.675	0.000	0.339	2.302	1.598	3.900
36:00:00	0.707	0.000	0.356	2.422	1.603	4.024
37:00:00	0.740	0.000	0.374	2.547	1.609	4.156
38:00:00	0.774	0.000	0.394	2.678	1.617	4.295
39:00:00	0.810	0.000	0.414	2.814	1.628	4.441
40:00:00	0.847	0.000	0.435	2.956	1.640	4.596
41:00:00	0.886	0.000	0.458	3.105	1.654	4.759
42:00:00	0.927	0.000	0.481	3.262	1.670	4.933
43:00:00	0.969	0.000	0.506	3.428	1.688	5.116
44:00:00	1.013	0.000	0.532	3.602	1.709	5.311
45:00:00	1.059	0.000	0.560	3.785	1.732	5.517
46:00:00	1.107	0.000	0.589	3.978	1.757	5.735
47:00:00	1.157	0.000	0.620	4.181	1.785	5.966
48:00:00	1.209	0.000	0.652	4.394	1.815	6.210
49:00:00	1.262	0.000	0.686	4.619	1.849	6.468
50:00:00	1.318	0.000	0.722	4.856	1.885	6.741
51:00:00	1.375	0.000	0.759	5.105	1.924	7.029
52:00:00	1.435	0.000	0.798	5.368	1.966	7.334
53:00:00	1.496	0.000	0.839	5.644	2.012	7.656
54:00:00	1.559	0.000	0.882	5.935	2.061	7.995
55:00:00	1.622	0.000	0.926	6.241	2.113	8.354
56:00:00	1.686	0.000	0.972	6.563	2.169	8.732
57:00:00	1.750	0.000	1.018	6.901	2.230	9.131
58:00:00	1.809	0.000	1.062	7.257	2.294	9.551
59:00:00	1.853	0.000	1.099	7.630	2.351	9.981
60:00:00	1.833	0.000	1.098	8.020	2.411	10.432
61:00:00	1.853	0.000	1.121	8.426	2.476	10.902
62:00:00	1.809	0.000	1.105	8.844	2.545	11.388
63:00:00	1.750	0.000	1.079	9.270	2.618	11.888
64:00:00	1.686	0.000	1.049	9.700	2.694	12.395
65:00:00	1.622	0.000	1.018	10.127	2.775	12.902
66:00:00	1.559	0.000	0.986	10.543	2.860	13.403
67:00:00	1.496	0.000	0.953	10.943	2.948	13.891
68:00:00	1.435	0.000	0.921	11.319	3.039	14.358
69:00:00	1.375	0.000	0.889	11.664	3.133	14.798
70:00:00	1.318	0.000	0.857	11.973	3.230	15.203

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
71:00:00	1.262	0.000	0.827	12.239	3.327	15.566
72:00:00	1.209	0.000	0.796	12.458	3.426	15.884
73:00:00	1.157	0.000	0.766	12.629	3.525	16.154
74:00:00	1.107	0.000	0.737	12.750	3.624	16.374
75:00:00	1.059	0.000	0.709	12.824	3.722	16.546
76:00:00	1.013	0.000	0.682	12.852	3.818	16.670
77:00:00	0.969	0.000	0.655	12.838	3.912	16.749
78:00:00	0.927	0.000	0.629	12.784	4.003	16.787
79:00:00	0.886	0.000	0.604	12.695	4.091	16.786
80:00:00	0.847	0.000	0.580	12.574	4.175	16.749
81:00:00	0.810	0.000	0.557	12.424	4.256	16.680
82:00:00	0.774	0.000	0.534	12.248	4.332	16.581
83:00:00	0.740	0.000	0.512	12.050	4.404	16.455
84:00:00	0.707	0.000	0.491	11.833	4.472	16.304
85:00:00	0.675	0.000	0.471	11.598	4.535	16.132
86:00:00	0.645	0.000	0.451	11.347	4.593	15.940
87:00:00	0.616	0.000	0.432	11.083	4.646	15.729
88:00:00	0.589	0.000	0.414	10.807	4.694	15.502
89:00:00	0.562	0.000	0.396	10.521	4.738	15.259
90:00:00	0.537	0.000	0.379	10.226	4.776	15.002
91:00:00	0.513	0.000	0.363	9.925	4.810	14.734
92:00:00	0.490	0.000	0.348	9.617	4.838	14.455
93:00:00	0.468	0.000	0.333	9.306	4.862	14.168
94:00:00	0.447	0.000	0.318	8.993	4.881	13.874
95:00:00	0.426	0.000	0.305	8.680	4.895	13.575
96:00:00	0.407	0.000	0.291	8.367	4.905	13.272
97:00:00	0.389	0.000	0.279	8.057	4.910	12.967
98:00:00	0.371	0.000	0.266	7.751	4.911	12.662
99:00:00	0.354	0.000	0.255	7.451	4.908	12.359
100:00:00	0.338	0.000	0.243	7.158	4.901	12.059
101:00:00	0.323	0.000	0.233	6.873	4.890	11.763
102:00:00	0.308	0.000	0.222	6.596	4.876	11.472
103:00:00	0.294	0.000	0.213	6.328	4.858	11.186
104:00:00	0.281	0.000	0.203	6.070	4.837	10.907
105:00:00	0.268	0.000	0.194	5.820	4.813	10.633
106:00:00	0.256	0.000	0.185	5.578	4.787	10.365

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
107:00:00	0.244	0.000	0.177	5.346	4.758	10.104
108:00:00	0.233	0.000	0.169	5.122	4.726	9.848
109:00:00	0.222	0.000	0.162	4.906	4.693	9.598
110:00:00	0.212	0.000	0.154	4.698	4.657	9.355
111:00:00	0.202	0.000	0.147	4.498	4.619	9.117
112:00:00	0.193	0.000	0.141	4.306	4.579	8.886
113:00:00	0.184	0.000	0.134	4.121	4.538	8.660
114:00:00	0.176	0.000	0.128	3.944	4.496	8.440
115:00:00	0.167	0.000	0.123	3.774	4.451	8.225
116:00:00	0.160	0.000	0.117	3.610	4.406	8.016
117:00:00	0.152	0.000	0.112	3.453	4.360	7.812
118:00:00	0.145	0.000	0.107	3.302	4.312	7.614
119:00:00	0.139	0.000	0.102	3.158	4.263	7.421
120:00:00	0.132	0.000	0.097	3.019	4.214	7.233
121:00:00	0.000	0.000	0.000	2.886	4.164	7.050
122:00:00	0.000	0.000	0.000	2.755	4.113	6.869
123:00:00	0.000	0.000	0.000	2.622	4.062	6.685
124:00:00	0.000	0.000	0.000	2.488	4.010	6.498
125:00:00	0.000	0.000	0.000	2.352	3.958	6.310
126:00:00	0.000	0.000	0.000	2.215	3.904	6.119
127:00:00	0.000	0.000	0.000	2.076	3.851	5.927
128:00:00	0.000	0.000	0.000	1.937	3.796	5.733
129:00:00	0.000	0.000	0.000	1.797	3.741	5.538
130:00:00	0.000	0.000	0.000	1.657	3.686	5.343
131:00:00	0.000	0.000	0.000	1.516	3.630	5.146
132:00:00	0.000	0.000	0.000	1.375	3.574	4.949
133:00:00	0.000	0.000	0.000	1.239	3.517	4.756
134:00:00	0.000	0.000	0.000	1.113	3.460	4.573
135:00:00	0.000	0.000	0.000	0.997	3.403	4.400
136:00:00	0.000	0.000	0.000	0.890	3.346	4.236
137:00:00	0.000	0.000	0.000	0.793	3.288	4.081
138:00:00	0.000	0.000	0.000	0.703	3.231	3.935
139:00:00	0.000	0.000	0.000	0.622	3.174	3.796
140:00:00	0.000	0.000	0.000	0.549	3.118	3.666
141:00:00	0.000	0.000	0.000	0.483	3.061	3.544
142:00:00	0.000	0.000	0.000	0.424	3.005	3.430

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
143:00:00	0.000	0.000	0.000	0.372	2.950	3.322
144:00:00	0.000	0.000	0.000	0.325	2.896	3.220
145:00:00	0.000	0.000	0.000	0.282	2.842	3.123
146:00:00	0.000	0.000	0.000	0.242	2.788	3.030
147:00:00	0.000	0.000	0.000	0.206	2.735	2.942
148:00:00	0.000	0.000	0.000	0.174	2.683	2.857
149:00:00	0.000	0.000	0.000	0.144	2.632	2.777
150:00:00	0.000	0.000	0.000	0.118	2.582	2.700
151:00:00	0.000	0.000	0.000	0.095	2.532	2.627
152:00:00	0.000	0.000	0.000	0.075	2.483	2.558
153:00:00	0.000	0.000	0.000	0.057	2.435	2.492
154:00:00	0.000	0.000	0.000	0.042	2.387	2.430
155:00:00	0.000	0.000	0.000	0.030	2.341	2.371
156:00:00	0.000	0.000	0.000	0.019	2.295	2.315
157:00:00	0.000	0.000	0.000	0.012	2.250	2.262
158:00:00	0.000	0.000	0.000	0.006	2.206	2.212
159:00:00	0.000	0.000	0.000	0.002	2.163	2.165
160:00:00	0.000	0.000	0.000	0.000	2.121	2.121

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Appendix

Catchment descriptors

Name	Value	User-defined value used?
Area (km^2)	50.16	No
ALTBAR	33	No
ASPBAR	0.23	No
ASPVAR	0	No
BFIHOST	0.38	No
DPLBAR (km)	8.54	No
DPSBAR (mkm^{-1})	24.6	No
FARL	0.97	No
LDP	17.1	No
PROPWET (mm)	0.26	No
RMED1H	10.9	No
RMED1D	29.4	No
RMED2D	37.4	No
SAAR (mm)	594	No
SAAR4170 (mm)	601	No
SPRHOST	41.05	No
Urbext2000	0.01	No
Urbext1990	0.01	No
URBCONC	0.59	No
URBLOC	0.79	No
DDF parameter C	-0.02	No
DDF parameter D1	0.3	No
DDF parameter D2	0.3	No
DDF parameter D3	0.25	No
DDF parameter E	0.31	No
DDF parameter F	2.49	No
DDF parameter C (1km grid value)	-0.02	No
DDF parameter D1 (1km grid value)	0.32	No
DDF parameter D2 (1km grid value)	0.28	No
DDF parameter D3 (1km grid value)	0.25	No
DDF parameter E (1km grid value)	0.31	No
DDF parameter F (1km grid value)	2.5	No

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

UK Design Flood Estimation

Generated on 11 May 2021 16:00:06 by AEA_COMPUTER
Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH2)

Site details Checksum: 371C-D1EA

Site name: tmp9C4F

Easting: 647550

Northing: 262800

Country: England, Wales or Northern Ireland

Catchment Area (km²): 1.45

Using plot scale calculations: No

Model: ReFH2.2

Site description: None

Model run: 100 year - LEIS_SIZEW1

Summary of results

Rainfall - FEH 2013 model (mm):	121.74	Total runoff (ML):	13.07
Total Rainfall (mm):	81.24	Total flow (ML):	31.66
Peak Rainfall (mm):	1.78	Peak flow (m³/s):	0.10

Parameters

Where the user has overriden a system-generated value, this original value is shown in square brackets after the value used.
** Indicates that the user locked the duration/timestep*

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	121:00:00 [11:00:00]	Yes
Timestep (hh:mm:ss)	01:00:00	No
SCF (Seasonal correction factor)	0.67	No
ARF (Areal reduction factor)	0.99	No
Seasonality	Winter	No

Loss model parameters

Name	Value	User-defined?
Cini (mm)	60.53	No
Cmax (mm)	1190.38	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No
Use seasonal CIni for equations	No [Yes]	Yes

Routing model parameters

Name	Value	User-defined?
Tp (hr)	7.15	No
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m^3/s)	0	No
BL (hr)	63.92	No
BR	2.16	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km^2)	0.2	No
Urbext 2000	0.09	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Exporting drained area (km^2)	0.00	Yes
Sewer capacity (m^3/s)	0.00	Yes

Time series data

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
00:00:00	0.127	0.000	0.010	0.000	0.000	0.000
01:00:00	0.133	0.000	0.010	0.000	0.000	0.000
02:00:00	0.139	0.000	0.011	0.000	0.000	0.000
03:00:00	0.146	0.000	0.011	0.001	0.000	0.001
04:00:00	0.153	0.000	0.012	0.001	0.000	0.001
05:00:00	0.160	0.000	0.013	0.001	0.000	0.001
06:00:00	0.168	0.000	0.013	0.002	0.000	0.002
07:00:00	0.176	0.000	0.014	0.002	0.000	0.002
08:00:00	0.185	0.000	0.015	0.003	0.000	0.003
09:00:00	0.194	0.000	0.015	0.003	0.000	0.003
10:00:00	0.203	0.000	0.016	0.004	0.000	0.004
11:00:00	0.213	0.000	0.017	0.004	0.000	0.004
12:00:00	0.223	0.000	0.018	0.004	0.000	0.005
13:00:00	0.234	0.000	0.019	0.005	0.000	0.005
14:00:00	0.245	0.000	0.020	0.005	0.000	0.005
15:00:00	0.256	0.000	0.021	0.005	0.000	0.006
16:00:00	0.269	0.000	0.022	0.006	0.001	0.006
17:00:00	0.282	0.000	0.023	0.006	0.001	0.007
18:00:00	0.295	0.000	0.024	0.006	0.001	0.007
19:00:00	0.309	0.000	0.025	0.007	0.001	0.008
20:00:00	0.324	0.000	0.026	0.007	0.001	0.008
21:00:00	0.339	0.000	0.028	0.007	0.001	0.009
22:00:00	0.355	0.000	0.029	0.008	0.001	0.009
23:00:00	0.372	0.000	0.031	0.008	0.001	0.010
24:00:00	0.390	0.000	0.032	0.009	0.001	0.010
25:00:00	0.409	0.000	0.034	0.009	0.002	0.011
26:00:00	0.428	0.000	0.036	0.010	0.002	0.011
27:00:00	0.448	0.000	0.038	0.010	0.002	0.012
28:00:00	0.469	0.000	0.040	0.011	0.002	0.013
29:00:00	0.491	0.000	0.042	0.011	0.002	0.013
30:00:00	0.515	0.000	0.044	0.012	0.002	0.014
31:00:00	0.539	0.000	0.046	0.012	0.002	0.015
32:00:00	0.564	0.000	0.048	0.013	0.003	0.016
33:00:00	0.590	0.000	0.051	0.014	0.003	0.017
34:00:00	0.618	0.000	0.054	0.014	0.003	0.017

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
35:00:00	0.647	0.000	0.057	0.015	0.003	0.018
36:00:00	0.677	0.000	0.060	0.016	0.003	0.019
37:00:00	0.709	0.000	0.063	0.017	0.004	0.020
38:00:00	0.741	0.000	0.066	0.018	0.004	0.022
39:00:00	0.776	0.000	0.070	0.018	0.004	0.023
40:00:00	0.812	0.000	0.073	0.019	0.005	0.024
41:00:00	0.849	0.000	0.077	0.020	0.005	0.025
42:00:00	0.888	0.000	0.081	0.022	0.005	0.027
43:00:00	0.928	0.000	0.086	0.023	0.005	0.028
44:00:00	0.971	0.000	0.090	0.024	0.006	0.030
45:00:00	1.015	0.000	0.095	0.025	0.006	0.031
46:00:00	1.061	0.000	0.101	0.026	0.006	0.033
47:00:00	1.108	0.000	0.106	0.028	0.007	0.035
48:00:00	1.158	0.000	0.112	0.029	0.007	0.037
49:00:00	1.209	0.000	0.118	0.031	0.008	0.039
50:00:00	1.262	0.000	0.124	0.032	0.008	0.041
51:00:00	1.317	0.000	0.131	0.034	0.009	0.043
52:00:00	1.374	0.000	0.138	0.036	0.009	0.045
53:00:00	1.433	0.000	0.146	0.038	0.010	0.048
54:00:00	1.493	0.000	0.154	0.040	0.010	0.050
55:00:00	1.554	0.000	0.162	0.042	0.011	0.053
56:00:00	1.615	0.000	0.170	0.044	0.012	0.056
57:00:00	1.676	0.000	0.179	0.047	0.012	0.059
58:00:00	1.732	0.000	0.187	0.049	0.013	0.062
59:00:00	1.775	0.000	0.195	0.052	0.014	0.066
60:00:00	1.756	0.000	0.195	0.054	0.015	0.069
61:00:00	1.775	0.000	0.200	0.057	0.015	0.073
62:00:00	1.732	0.000	0.197	0.060	0.016	0.076
63:00:00	1.676	0.000	0.193	0.062	0.017	0.080
64:00:00	1.615	0.000	0.188	0.065	0.018	0.083
65:00:00	1.554	0.000	0.183	0.067	0.019	0.086
66:00:00	1.493	0.000	0.178	0.068	0.020	0.089
67:00:00	1.433	0.000	0.172	0.070	0.022	0.091
68:00:00	1.374	0.000	0.167	0.071	0.023	0.093
69:00:00	1.317	0.000	0.161	0.071	0.024	0.095
70:00:00	1.262	0.000	0.156	0.071	0.025	0.096

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
71:00:00	1.209	0.000	0.150	0.071	0.026	0.097
72:00:00	1.158	0.000	0.145	0.070	0.027	0.098
73:00:00	1.108	0.000	0.140	0.069	0.029	0.098
74:00:00	1.061	0.000	0.135	0.068	0.030	0.098
75:00:00	1.015	0.000	0.130	0.067	0.031	0.098
76:00:00	0.971	0.000	0.125	0.066	0.032	0.098
77:00:00	0.928	0.000	0.120	0.064	0.033	0.098
78:00:00	0.888	0.000	0.116	0.063	0.034	0.097
79:00:00	0.849	0.000	0.111	0.061	0.035	0.096
80:00:00	0.812	0.000	0.107	0.060	0.036	0.096
81:00:00	0.776	0.000	0.103	0.058	0.037	0.095
82:00:00	0.741	0.000	0.099	0.056	0.038	0.094
83:00:00	0.709	0.000	0.095	0.054	0.038	0.093
84:00:00	0.677	0.000	0.091	0.052	0.039	0.091
85:00:00	0.647	0.000	0.087	0.051	0.040	0.090
86:00:00	0.618	0.000	0.084	0.049	0.040	0.089
87:00:00	0.590	0.000	0.080	0.047	0.041	0.088
88:00:00	0.564	0.000	0.077	0.045	0.041	0.087
89:00:00	0.539	0.000	0.074	0.044	0.042	0.085
90:00:00	0.515	0.000	0.070	0.042	0.042	0.084
91:00:00	0.491	0.000	0.067	0.040	0.043	0.083
92:00:00	0.469	0.000	0.065	0.039	0.043	0.082
93:00:00	0.448	0.000	0.062	0.037	0.043	0.080
94:00:00	0.428	0.000	0.059	0.036	0.043	0.079
95:00:00	0.409	0.000	0.057	0.034	0.044	0.078
96:00:00	0.390	0.000	0.054	0.033	0.044	0.077
97:00:00	0.372	0.000	0.052	0.032	0.044	0.076
98:00:00	0.355	0.000	0.050	0.030	0.044	0.074
99:00:00	0.339	0.000	0.047	0.029	0.044	0.073
100:00:00	0.324	0.000	0.045	0.028	0.044	0.072
101:00:00	0.309	0.000	0.043	0.027	0.044	0.071
102:00:00	0.295	0.000	0.042	0.026	0.044	0.070
103:00:00	0.282	0.000	0.040	0.025	0.044	0.069
104:00:00	0.269	0.000	0.038	0.023	0.044	0.067
105:00:00	0.256	0.000	0.036	0.022	0.044	0.066
106:00:00	0.245	0.000	0.035	0.022	0.044	0.065

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
107:00:00	0.234	0.000	0.033	0.021	0.044	0.064
108:00:00	0.223	0.000	0.032	0.020	0.043	0.063
109:00:00	0.213	0.000	0.030	0.019	0.043	0.062
110:00:00	0.203	0.000	0.029	0.018	0.043	0.061
111:00:00	0.194	0.000	0.028	0.017	0.043	0.060
112:00:00	0.185	0.000	0.026	0.017	0.043	0.059
113:00:00	0.176	0.000	0.025	0.016	0.042	0.058
114:00:00	0.168	0.000	0.024	0.015	0.042	0.057
115:00:00	0.160	0.000	0.023	0.014	0.042	0.056
116:00:00	0.153	0.000	0.022	0.014	0.042	0.055
117:00:00	0.146	0.000	0.021	0.013	0.041	0.054
118:00:00	0.139	0.000	0.020	0.013	0.041	0.054
119:00:00	0.133	0.000	0.019	0.012	0.041	0.053
120:00:00	0.127	0.000	0.018	0.012	0.040	0.052
121:00:00	0.000	0.000	0.000	0.011	0.040	0.051
122:00:00	0.000	0.000	0.000	0.010	0.040	0.050
123:00:00	0.000	0.000	0.000	0.010	0.039	0.049
124:00:00	0.000	0.000	0.000	0.009	0.039	0.048
125:00:00	0.000	0.000	0.000	0.008	0.038	0.046
126:00:00	0.000	0.000	0.000	0.007	0.038	0.045
127:00:00	0.000	0.000	0.000	0.006	0.038	0.044
128:00:00	0.000	0.000	0.000	0.005	0.037	0.042
129:00:00	0.000	0.000	0.000	0.004	0.037	0.041
130:00:00	0.000	0.000	0.000	0.004	0.036	0.040
131:00:00	0.000	0.000	0.000	0.003	0.036	0.039
132:00:00	0.000	0.000	0.000	0.002	0.035	0.038
133:00:00	0.000	0.000	0.000	0.002	0.035	0.037
134:00:00	0.000	0.000	0.000	0.002	0.035	0.036
135:00:00	0.000	0.000	0.000	0.001	0.034	0.035
136:00:00	0.000	0.000	0.000	0.001	0.034	0.035
137:00:00	0.000	0.000	0.000	0.001	0.033	0.034
138:00:00	0.000	0.000	0.000	0.001	0.033	0.033
139:00:00	0.000	0.000	0.000	0.001	0.032	0.033
140:00:00	0.000	0.000	0.000	0.000	0.032	0.032
141:00:00	0.000	0.000	0.000	0.000	0.031	0.031
142:00:00	0.000	0.000	0.000	0.000	0.031	0.031

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
143:00:00	0.000	0.000	0.000	0.000	0.030	0.030
144:00:00	0.000	0.000	0.000	0.000	0.030	0.030
145:00:00	0.000	0.000	0.000	0.000	0.029	0.029
146:00:00	0.000	0.000	0.000	0.000	0.029	0.029
147:00:00	0.000	0.000	0.000	0.000	0.028	0.028
148:00:00	0.000	0.000	0.000	0.000	0.028	0.028
149:00:00	0.000	0.000	0.000	0.000	0.027	0.027
150:00:00	0.000	0.000	0.000	0.000	0.027	0.027
151:00:00	0.000	0.000	0.000	0.000	0.027	0.027
152:00:00	0.000	0.000	0.000	0.000	0.026	0.026
153:00:00	0.000	0.000	0.000	0.000	0.026	0.026
154:00:00	0.000	0.000	0.000	0.000	0.025	0.025
155:00:00	0.000	0.000	0.000	0.000	0.025	0.025
156:00:00	0.000	0.000	0.000	0.000	0.025	0.025
157:00:00	0.000	0.000	0.000	0.000	0.024	0.024
158:00:00	0.000	0.000	0.000	0.000	0.024	0.024
159:00:00	0.000	0.000	0.000	0.000	0.024	0.024
160:00:00	0.000	0.000	0.000	0.000	0.023	0.023
161:00:00	0.000	0.000	0.000	0.000	0.023	0.023
162:00:00	0.000	0.000	0.000	0.000	0.022	0.022
163:00:00	0.000	0.000	0.000	0.000	0.022	0.022
164:00:00	0.000	0.000	0.000	0.000	0.022	0.022
165:00:00	0.000	0.000	0.000	0.000	0.021	0.021
166:00:00	0.000	0.000	0.000	0.000	0.021	0.021
167:00:00	0.000	0.000	0.000	0.000	0.021	0.021
168:00:00	0.000	0.000	0.000	0.000	0.020	0.020
169:00:00	0.000	0.000	0.000	0.000	0.020	0.020
170:00:00	0.000	0.000	0.000	0.000	0.020	0.020
171:00:00	0.000	0.000	0.000	0.000	0.019	0.019
172:00:00	0.000	0.000	0.000	0.000	0.019	0.019
173:00:00	0.000	0.000	0.000	0.000	0.019	0.019
174:00:00	0.000	0.000	0.000	0.000	0.019	0.019
175:00:00	0.000	0.000	0.000	0.000	0.018	0.018
176:00:00	0.000	0.000	0.000	0.000	0.018	0.018
177:00:00	0.000	0.000	0.000	0.000	0.018	0.018
178:00:00	0.000	0.000	0.000	0.000	0.017	0.017

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
179:00:00	0.000	0.000	0.000	0.000	0.017	0.017
180:00:00	0.000	0.000	0.000	0.000	0.017	0.017
181:00:00	0.000	0.000	0.000	0.000	0.017	0.017
182:00:00	0.000	0.000	0.000	0.000	0.016	0.016
183:00:00	0.000	0.000	0.000	0.000	0.016	0.016
184:00:00	0.000	0.000	0.000	0.000	0.016	0.016
185:00:00	0.000	0.000	0.000	0.000	0.016	0.016
186:00:00	0.000	0.000	0.000	0.000	0.015	0.015
187:00:00	0.000	0.000	0.000	0.000	0.015	0.015
188:00:00	0.000	0.000	0.000	0.000	0.015	0.015
189:00:00	0.000	0.000	0.000	0.000	0.015	0.015
190:00:00	0.000	0.000	0.000	0.000	0.014	0.014
191:00:00	0.000	0.000	0.000	0.000	0.014	0.014
192:00:00	0.000	0.000	0.000	0.000	0.014	0.014
193:00:00	0.000	0.000	0.000	0.000	0.014	0.014
194:00:00	0.000	0.000	0.000	0.000	0.014	0.014
195:00:00	0.000	0.000	0.000	0.000	0.013	0.013
196:00:00	0.000	0.000	0.000	0.000	0.013	0.013
197:00:00	0.000	0.000	0.000	0.000	0.013	0.013
198:00:00	0.000	0.000	0.000	0.000	0.013	0.013
199:00:00	0.000	0.000	0.000	0.000	0.013	0.013
200:00:00	0.000	0.000	0.000	0.000	0.012	0.012
201:00:00	0.000	0.000	0.000	0.000	0.012	0.012
202:00:00	0.000	0.000	0.000	0.000	0.012	0.012
203:00:00	0.000	0.000	0.000	0.000	0.012	0.012
204:00:00	0.000	0.000	0.000	0.000	0.012	0.012
205:00:00	0.000	0.000	0.000	0.000	0.011	0.011
206:00:00	0.000	0.000	0.000	0.000	0.011	0.011
207:00:00	0.000	0.000	0.000	0.000	0.011	0.011
208:00:00	0.000	0.000	0.000	0.000	0.011	0.011
209:00:00	0.000	0.000	0.000	0.000	0.011	0.011
210:00:00	0.000	0.000	0.000	0.000	0.011	0.011
211:00:00	0.000	0.000	0.000	0.000	0.010	0.010
212:00:00	0.000	0.000	0.000	0.000	0.010	0.010
213:00:00	0.000	0.000	0.000	0.000	0.010	0.010
214:00:00	0.000	0.000	0.000	0.000	0.010	0.010

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
215:00:00	0.000	0.000	0.000	0.000	0.010	0.010
216:00:00	0.000	0.000	0.000	0.000	0.010	0.010
217:00:00	0.000	0.000	0.000	0.000	0.009	0.009
218:00:00	0.000	0.000	0.000	0.000	0.009	0.009
219:00:00	0.000	0.000	0.000	0.000	0.009	0.009
220:00:00	0.000	0.000	0.000	0.000	0.009	0.009
221:00:00	0.000	0.000	0.000	0.000	0.009	0.009
222:00:00	0.000	0.000	0.000	0.000	0.009	0.009
223:00:00	0.000	0.000	0.000	0.000	0.009	0.009
224:00:00	0.000	0.000	0.000	0.000	0.009	0.009
225:00:00	0.000	0.000	0.000	0.000	0.008	0.008
226:00:00	0.000	0.000	0.000	0.000	0.008	0.008
227:00:00	0.000	0.000	0.000	0.000	0.008	0.008
228:00:00	0.000	0.000	0.000	0.000	0.008	0.008
229:00:00	0.000	0.000	0.000	0.000	0.008	0.008
230:00:00	0.000	0.000	0.000	0.000	0.008	0.008
231:00:00	0.000	0.000	0.000	0.000	0.008	0.008
232:00:00	0.000	0.000	0.000	0.000	0.008	0.008
233:00:00	0.000	0.000	0.000	0.000	0.007	0.007
234:00:00	0.000	0.000	0.000	0.000	0.007	0.007
235:00:00	0.000	0.000	0.000	0.000	0.007	0.007
236:00:00	0.000	0.000	0.000	0.000	0.007	0.007
237:00:00	0.000	0.000	0.000	0.000	0.007	0.007
238:00:00	0.000	0.000	0.000	0.000	0.007	0.007
239:00:00	0.000	0.000	0.000	0.000	0.007	0.007
240:00:00	0.000	0.000	0.000	0.000	0.007	0.007
241:00:00	0.000	0.000	0.000	0.000	0.007	0.007
242:00:00	0.000	0.000	0.000	0.000	0.006	0.006
243:00:00	0.000	0.000	0.000	0.000	0.006	0.006
244:00:00	0.000	0.000	0.000	0.000	0.006	0.006
245:00:00	0.000	0.000	0.000	0.000	0.006	0.006
246:00:00	0.000	0.000	0.000	0.000	0.006	0.006
247:00:00	0.000	0.000	0.000	0.000	0.006	0.006
248:00:00	0.000	0.000	0.000	0.000	0.006	0.006
249:00:00	0.000	0.000	0.000	0.000	0.006	0.006
250:00:00	0.000	0.000	0.000	0.000	0.006	0.006

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
251:00:00	0.000	0.000	0.000	0.000	0.006	0.006
252:00:00	0.000	0.000	0.000	0.000	0.005	0.005
253:00:00	0.000	0.000	0.000	0.000	0.005	0.005
254:00:00	0.000	0.000	0.000	0.000	0.005	0.005
255:00:00	0.000	0.000	0.000	0.000	0.005	0.005
256:00:00	0.000	0.000	0.000	0.000	0.005	0.005
257:00:00	0.000	0.000	0.000	0.000	0.005	0.005
258:00:00	0.000	0.000	0.000	0.000	0.005	0.005
259:00:00	0.000	0.000	0.000	0.000	0.005	0.005
260:00:00	0.000	0.000	0.000	0.000	0.005	0.005
261:00:00	0.000	0.000	0.000	0.000	0.005	0.005
262:00:00	0.000	0.000	0.000	0.000	0.005	0.005
263:00:00	0.000	0.000	0.000	0.000	0.005	0.005
264:00:00	0.000	0.000	0.000	0.000	0.005	0.005
265:00:00	0.000	0.000	0.000	0.000	0.004	0.004
266:00:00	0.000	0.000	0.000	0.000	0.004	0.004
267:00:00	0.000	0.000	0.000	0.000	0.004	0.004
268:00:00	0.000	0.000	0.000	0.000	0.004	0.004
269:00:00	0.000	0.000	0.000	0.000	0.004	0.004
270:00:00	0.000	0.000	0.000	0.000	0.004	0.004
271:00:00	0.000	0.000	0.000	0.000	0.004	0.004
272:00:00	0.000	0.000	0.000	0.000	0.004	0.004
273:00:00	0.000	0.000	0.000	0.000	0.004	0.004
274:00:00	0.000	0.000	0.000	0.000	0.004	0.004
275:00:00	0.000	0.000	0.000	0.000	0.004	0.004
276:00:00	0.000	0.000	0.000	0.000	0.004	0.004
277:00:00	0.000	0.000	0.000	0.000	0.004	0.004
278:00:00	0.000	0.000	0.000	0.000	0.004	0.004
279:00:00	0.000	0.000	0.000	0.000	0.004	0.004
280:00:00	0.000	0.000	0.000	0.000	0.004	0.004
281:00:00	0.000	0.000	0.000	0.000	0.003	0.003
282:00:00	0.000	0.000	0.000	0.000	0.003	0.003
283:00:00	0.000	0.000	0.000	0.000	0.003	0.003
284:00:00	0.000	0.000	0.000	0.000	0.003	0.003
285:00:00	0.000	0.000	0.000	0.000	0.003	0.003
286:00:00	0.000	0.000	0.000	0.000	0.003	0.003

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
287:00:00	0.000	0.000	0.000	0.000	0.003	0.003
288:00:00	0.000	0.000	0.000	0.000	0.003	0.003
289:00:00	0.000	0.000	0.000	0.000	0.003	0.003
290:00:00	0.000	0.000	0.000	0.000	0.003	0.003
291:00:00	0.000	0.000	0.000	0.000	0.003	0.003
292:00:00	0.000	0.000	0.000	0.000	0.003	0.003
293:00:00	0.000	0.000	0.000	0.000	0.003	0.003
294:00:00	0.000	0.000	0.000	0.000	0.003	0.003
295:00:00	0.000	0.000	0.000	0.000	0.003	0.003
296:00:00	0.000	0.000	0.000	0.000	0.003	0.003
297:00:00	0.000	0.000	0.000	0.000	0.003	0.003
298:00:00	0.000	0.000	0.000	0.000	0.003	0.003
299:00:00	0.000	0.000	0.000	0.000	0.003	0.003
300:00:00	0.000	0.000	0.000	0.000	0.003	0.003
301:00:00	0.000	0.000	0.000	0.000	0.003	0.003
302:00:00	0.000	0.000	0.000	0.000	0.003	0.003
303:00:00	0.000	0.000	0.000	0.000	0.002	0.002
304:00:00	0.000	0.000	0.000	0.000	0.002	0.002
305:00:00	0.000	0.000	0.000	0.000	0.002	0.002
306:00:00	0.000	0.000	0.000	0.000	0.002	0.002
307:00:00	0.000	0.000	0.000	0.000	0.002	0.002
308:00:00	0.000	0.000	0.000	0.000	0.002	0.002
309:00:00	0.000	0.000	0.000	0.000	0.002	0.002
310:00:00	0.000	0.000	0.000	0.000	0.002	0.002
311:00:00	0.000	0.000	0.000	0.000	0.002	0.002
312:00:00	0.000	0.000	0.000	0.000	0.002	0.002
313:00:00	0.000	0.000	0.000	0.000	0.002	0.002
314:00:00	0.000	0.000	0.000	0.000	0.002	0.002
315:00:00	0.000	0.000	0.000	0.000	0.002	0.002
316:00:00	0.000	0.000	0.000	0.000	0.002	0.002
317:00:00	0.000	0.000	0.000	0.000	0.002	0.002
318:00:00	0.000	0.000	0.000	0.000	0.002	0.002
319:00:00	0.000	0.000	0.000	0.000	0.002	0.002
320:00:00	0.000	0.000	0.000	0.000	0.002	0.002
321:00:00	0.000	0.000	0.000	0.000	0.002	0.002
322:00:00	0.000	0.000	0.000	0.000	0.002	0.002

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
323:00:00	0.000	0.000	0.000	0.000	0.002	0.002
324:00:00	0.000	0.000	0.000	0.000	0.002	0.002
325:00:00	0.000	0.000	0.000	0.000	0.002	0.002
326:00:00	0.000	0.000	0.000	0.000	0.002	0.002
327:00:00	0.000	0.000	0.000	0.000	0.002	0.002
328:00:00	0.000	0.000	0.000	0.000	0.002	0.002
329:00:00	0.000	0.000	0.000	0.000	0.002	0.002
330:00:00	0.000	0.000	0.000	0.000	0.002	0.002
331:00:00	0.000	0.000	0.000	0.000	0.002	0.002
332:00:00	0.000	0.000	0.000	0.000	0.002	0.002
333:00:00	0.000	0.000	0.000	0.000	0.002	0.002
334:00:00	0.000	0.000	0.000	0.000	0.002	0.002
335:00:00	0.000	0.000	0.000	0.000	0.001	0.001
336:00:00	0.000	0.000	0.000	0.000	0.001	0.001
337:00:00	0.000	0.000	0.000	0.000	0.001	0.001
338:00:00	0.000	0.000	0.000	0.000	0.001	0.001
339:00:00	0.000	0.000	0.000	0.000	0.001	0.001
340:00:00	0.000	0.000	0.000	0.000	0.001	0.001
341:00:00	0.000	0.000	0.000	0.000	0.001	0.001
342:00:00	0.000	0.000	0.000	0.000	0.001	0.001
343:00:00	0.000	0.000	0.000	0.000	0.001	0.001
344:00:00	0.000	0.000	0.000	0.000	0.001	0.001
345:00:00	0.000	0.000	0.000	0.000	0.001	0.001
346:00:00	0.000	0.000	0.000	0.000	0.001	0.001
347:00:00	0.000	0.000	0.000	0.000	0.001	0.001
348:00:00	0.000	0.000	0.000	0.000	0.001	0.001
349:00:00	0.000	0.000	0.000	0.000	0.001	0.001
350:00:00	0.000	0.000	0.000	0.000	0.001	0.001
351:00:00	0.000	0.000	0.000	0.000	0.001	0.001
352:00:00	0.000	0.000	0.000	0.000	0.001	0.001
353:00:00	0.000	0.000	0.000	0.000	0.001	0.001
354:00:00	0.000	0.000	0.000	0.000	0.001	0.001
355:00:00	0.000	0.000	0.000	0.000	0.001	0.001
356:00:00	0.000	0.000	0.000	0.000	0.001	0.001
357:00:00	0.000	0.000	0.000	0.000	0.001	0.001
358:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
359:00:00	0.000	0.000	0.000	0.000	0.001	0.001
360:00:00	0.000	0.000	0.000	0.000	0.001	0.001
361:00:00	0.000	0.000	0.000	0.000	0.001	0.001
362:00:00	0.000	0.000	0.000	0.000	0.001	0.001
363:00:00	0.000	0.000	0.000	0.000	0.001	0.001
364:00:00	0.000	0.000	0.000	0.000	0.001	0.001
365:00:00	0.000	0.000	0.000	0.000	0.001	0.001
366:00:00	0.000	0.000	0.000	0.000	0.001	0.001
367:00:00	0.000	0.000	0.000	0.000	0.001	0.001
368:00:00	0.000	0.000	0.000	0.000	0.001	0.001
369:00:00	0.000	0.000	0.000	0.000	0.001	0.001
370:00:00	0.000	0.000	0.000	0.000	0.001	0.001
371:00:00	0.000	0.000	0.000	0.000	0.001	0.001
372:00:00	0.000	0.000	0.000	0.000	0.001	0.001
373:00:00	0.000	0.000	0.000	0.000	0.001	0.001
374:00:00	0.000	0.000	0.000	0.000	0.001	0.001
375:00:00	0.000	0.000	0.000	0.000	0.001	0.001
376:00:00	0.000	0.000	0.000	0.000	0.001	0.001
377:00:00	0.000	0.000	0.000	0.000	0.001	0.001
378:00:00	0.000	0.000	0.000	0.000	0.001	0.001
379:00:00	0.000	0.000	0.000	0.000	0.001	0.001
380:00:00	0.000	0.000	0.000	0.000	0.001	0.001
381:00:00	0.000	0.000	0.000	0.000	0.001	0.001
382:00:00	0.000	0.000	0.000	0.000	0.001	0.001
383:00:00	0.000	0.000	0.000	0.000	0.001	0.001
384:00:00	0.000	0.000	0.000	0.000	0.001	0.001
385:00:00	0.000	0.000	0.000	0.000	0.001	0.001
386:00:00	0.000	0.000	0.000	0.000	0.001	0.001
387:00:00	0.000	0.000	0.000	0.000	0.001	0.001
388:00:00	0.000	0.000	0.000	0.000	0.001	0.001
389:00:00	0.000	0.000	0.000	0.000	0.001	0.001
390:00:00	0.000	0.000	0.000	0.000	0.001	0.001
391:00:00	0.000	0.000	0.000	0.000	0.001	0.001
392:00:00	0.000	0.000	0.000	0.000	0.001	0.001
393:00:00	0.000	0.000	0.000	0.000	0.001	0.001
394:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
395:00:00	0.000	0.000	0.000	0.000	0.001	0.001
396:00:00	0.000	0.000	0.000	0.000	0.001	0.001
397:00:00	0.000	0.000	0.000	0.000	0.001	0.001
398:00:00	0.000	0.000	0.000	0.000	0.001	0.001
399:00:00	0.000	0.000	0.000	0.000	0.001	0.001
400:00:00	0.000	0.000	0.000	0.000	0.001	0.001
401:00:00	0.000	0.000	0.000	0.000	0.001	0.001
402:00:00	0.000	0.000	0.000	0.000	0.001	0.001
403:00:00	0.000	0.000	0.000	0.000	0.001	0.001
404:00:00	0.000	0.000	0.000	0.000	0.001	0.001
405:00:00	0.000	0.000	0.000	0.000	0.001	0.001
406:00:00	0.000	0.000	0.000	0.000	0.000	0.000
407:00:00	0.000	0.000	0.000	0.000	0.000	0.000
408:00:00	0.000	0.000	0.000	0.000	0.000	0.000
409:00:00	0.000	0.000	0.000	0.000	0.000	0.000
410:00:00	0.000	0.000	0.000	0.000	0.000	0.000
411:00:00	0.000	0.000	0.000	0.000	0.000	0.000
412:00:00	0.000	0.000	0.000	0.000	0.000	0.000
413:00:00	0.000	0.000	0.000	0.000	0.000	0.000
414:00:00	0.000	0.000	0.000	0.000	0.000	0.000
415:00:00	0.000	0.000	0.000	0.000	0.000	0.000
416:00:00	0.000	0.000	0.000	0.000	0.000	0.000
417:00:00	0.000	0.000	0.000	0.000	0.000	0.000
418:00:00	0.000	0.000	0.000	0.000	0.000	0.000
419:00:00	0.000	0.000	0.000	0.000	0.000	0.000
420:00:00	0.000	0.000	0.000	0.000	0.000	0.000
421:00:00	0.000	0.000	0.000	0.000	0.000	0.000
422:00:00	0.000	0.000	0.000	0.000	0.000	0.000
423:00:00	0.000	0.000	0.000	0.000	0.000	0.000
424:00:00	0.000	0.000	0.000	0.000	0.000	0.000
425:00:00	0.000	0.000	0.000	0.000	0.000	0.000
426:00:00	0.000	0.000	0.000	0.000	0.000	0.000
427:00:00	0.000	0.000	0.000	0.000	0.000	0.000
428:00:00	0.000	0.000	0.000	0.000	0.000	0.000
429:00:00	0.000	0.000	0.000	0.000	0.000	0.000
430:00:00	0.000	0.000	0.000	0.000	0.000	0.000

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Appendix

Catchment descriptors

Name	Value	User-defined value used?
Area (km^2)	1.45	No
ALTBAR	12	No
ASPBAR	0.44	No
ASPVAR	0	No
BFIHOST	0.89	No
DPLBAR (km)	2.27	No
DPSBAR (mkm^{-1})	8.7	No
FARL	1	No
LDP	4.98	No
PROPWET (mm)	0.26	No
RMED1H	11	No
RMED1D	30.2	No
RMED2D	38.6	No
SAAR (mm)	586	No
SAAR4170 (mm)	593	No
SPRHOST	14.52	No
Urbext2000	0.09	No
Urbext1990	0.05	No
URBCONC	0.84	No
URBLOC	1.47	No
DDF parameter C	-0.02	No
DDF parameter D1	0.3	No
DDF parameter D2	0.28	No
DDF parameter D3	0.21	No
DDF parameter E	0.31	No
DDF parameter F	2.51	No
DDF parameter C (1km grid value)	0	No
DDF parameter D1 (1km grid value)	0	No
DDF parameter D2 (1km grid value)	0	No
DDF parameter D3 (1km grid value)	0	No
DDF parameter E (1km grid value)	0	No
DDF parameter F (1km grid value)	0	No

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UK Design Flood Estimation

Generated on 11 May 2021 16:01:01 by AEA_COMPUTER
Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH2)

Site details Checksum: 7722-A6A6

Site name: tmp71C1

Easting: 647550

Northing: 262800

Country: England, Wales or Northern Ireland

Catchment Area (km²): 1.02

Using plot scale calculations: No

Model: ReFH2.2

Site description: None

Model run: 100 year - LEIS_SIZEW2

Summary of results

Rainfall - FEH 2013 model (mm):	121.74	Total runoff (ML):	9.21
Total Rainfall (mm):	81.30	Total flow (ML):	22.30
Peak Rainfall (mm):	1.78	Peak flow (m³/s):	0.07

Parameters

Where the user has overriden a system-generated value, this original value is shown in square brackets after the value used.
** Indicates that the user locked the duration/timestep*

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	121:00:00 [11:00:00]	Yes
Timestep (hh:mm:ss)	01:00:00	No
SCF (Seasonal correction factor)	0.67	No
ARF (Areal reduction factor)	0.99	No
Seasonality	Winter	No

Loss model parameters

Name	Value	User-defined?
Cini (mm)	60.53	No
Cmax (mm)	1190.38	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No
Use seasonal CIni for equations	No [Yes]	Yes

Routing model parameters

Name	Value	User-defined?
Tp (hr)	7.15	No
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m^3/s)	0	No
BL (hr)	63.92	No
BR	2.16	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km^2)	0.14	No
Urbext 2000	0.09	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Exporting drained area (km^2)	0.00	Yes
Sewer capacity (m^3/s)	0.00	Yes

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time series data

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
00:00:00	0.127	0.000	0.010	0.000	0.000	0.000
01:00:00	0.133	0.000	0.010	0.000	0.000	0.000
02:00:00	0.139	0.000	0.011	0.000	0.000	0.000
03:00:00	0.146	0.000	0.011	0.000	0.000	0.000
04:00:00	0.153	0.000	0.012	0.001	0.000	0.001
05:00:00	0.161	0.000	0.013	0.001	0.000	0.001
06:00:00	0.168	0.000	0.013	0.001	0.000	0.001
07:00:00	0.176	0.000	0.014	0.002	0.000	0.002
08:00:00	0.185	0.000	0.015	0.002	0.000	0.002
09:00:00	0.194	0.000	0.015	0.002	0.000	0.002
10:00:00	0.203	0.000	0.016	0.003	0.000	0.003
11:00:00	0.213	0.000	0.017	0.003	0.000	0.003
12:00:00	0.223	0.000	0.018	0.003	0.000	0.003
13:00:00	0.234	0.000	0.019	0.003	0.000	0.004
14:00:00	0.245	0.000	0.020	0.003	0.000	0.004
15:00:00	0.257	0.000	0.021	0.004	0.000	0.004
16:00:00	0.269	0.000	0.022	0.004	0.000	0.004
17:00:00	0.282	0.000	0.023	0.004	0.000	0.005
18:00:00	0.295	0.000	0.024	0.004	0.001	0.005
19:00:00	0.309	0.000	0.025	0.005	0.001	0.005
20:00:00	0.324	0.000	0.027	0.005	0.001	0.006
21:00:00	0.340	0.000	0.028	0.005	0.001	0.006
22:00:00	0.356	0.000	0.029	0.006	0.001	0.006
23:00:00	0.373	0.000	0.031	0.006	0.001	0.007
24:00:00	0.390	0.000	0.032	0.006	0.001	0.007
25:00:00	0.409	0.000	0.034	0.006	0.001	0.008
26:00:00	0.428	0.000	0.036	0.007	0.001	0.008
27:00:00	0.448	0.000	0.038	0.007	0.001	0.008
28:00:00	0.470	0.000	0.040	0.008	0.001	0.009
29:00:00	0.492	0.000	0.042	0.008	0.002	0.009
30:00:00	0.515	0.000	0.044	0.008	0.002	0.010
31:00:00	0.539	0.000	0.046	0.009	0.002	0.010
32:00:00	0.564	0.000	0.049	0.009	0.002	0.011
33:00:00	0.591	0.000	0.051	0.010	0.002	0.012
34:00:00	0.619	0.000	0.054	0.010	0.002	0.012

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
35:00:00	0.647	0.000	0.057	0.011	0.002	0.013
36:00:00	0.678	0.000	0.060	0.011	0.002	0.014
37:00:00	0.709	0.000	0.063	0.012	0.003	0.014
38:00:00	0.742	0.000	0.066	0.012	0.003	0.015
39:00:00	0.776	0.000	0.070	0.013	0.003	0.016
40:00:00	0.812	0.000	0.073	0.014	0.003	0.017
41:00:00	0.850	0.000	0.077	0.014	0.003	0.018
42:00:00	0.889	0.000	0.081	0.015	0.004	0.019
43:00:00	0.929	0.000	0.086	0.016	0.004	0.020
44:00:00	0.972	0.000	0.091	0.017	0.004	0.021
45:00:00	1.016	0.000	0.095	0.018	0.004	0.022
46:00:00	1.061	0.000	0.101	0.019	0.005	0.023
47:00:00	1.109	0.000	0.106	0.020	0.005	0.024
48:00:00	1.159	0.000	0.112	0.021	0.005	0.026
49:00:00	1.210	0.000	0.118	0.022	0.005	0.027
50:00:00	1.263	0.000	0.125	0.023	0.006	0.029
51:00:00	1.319	0.000	0.131	0.024	0.006	0.030
52:00:00	1.376	0.000	0.138	0.025	0.006	0.032
53:00:00	1.434	0.000	0.146	0.027	0.007	0.034
54:00:00	1.494	0.000	0.154	0.028	0.007	0.035
55:00:00	1.555	0.000	0.162	0.030	0.008	0.037
56:00:00	1.617	0.000	0.171	0.031	0.008	0.039
57:00:00	1.677	0.000	0.179	0.033	0.009	0.042
58:00:00	1.734	0.000	0.188	0.035	0.009	0.044
59:00:00	1.777	0.000	0.195	0.036	0.010	0.046
60:00:00	1.757	0.000	0.195	0.038	0.010	0.049
61:00:00	1.777	0.000	0.200	0.040	0.011	0.051
62:00:00	1.734	0.000	0.197	0.042	0.012	0.054
63:00:00	1.677	0.000	0.193	0.044	0.012	0.056
64:00:00	1.617	0.000	0.188	0.046	0.013	0.059
65:00:00	1.555	0.000	0.183	0.047	0.014	0.061
66:00:00	1.494	0.000	0.178	0.048	0.014	0.063
67:00:00	1.434	0.000	0.172	0.049	0.015	0.064
68:00:00	1.376	0.000	0.167	0.050	0.016	0.066
69:00:00	1.319	0.000	0.161	0.050	0.017	0.067
70:00:00	1.263	0.000	0.156	0.050	0.018	0.068

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
71:00:00	1.210	0.000	0.151	0.050	0.019	0.068
72:00:00	1.159	0.000	0.145	0.049	0.019	0.069
73:00:00	1.109	0.000	0.140	0.049	0.020	0.069
74:00:00	1.061	0.000	0.135	0.048	0.021	0.069
75:00:00	1.016	0.000	0.130	0.047	0.022	0.069
76:00:00	0.972	0.000	0.125	0.046	0.023	0.069
77:00:00	0.929	0.000	0.120	0.045	0.023	0.069
78:00:00	0.889	0.000	0.116	0.044	0.024	0.068
79:00:00	0.850	0.000	0.111	0.043	0.025	0.068
80:00:00	0.812	0.000	0.107	0.042	0.025	0.067
81:00:00	0.776	0.000	0.103	0.041	0.026	0.067
82:00:00	0.742	0.000	0.099	0.039	0.026	0.066
83:00:00	0.709	0.000	0.095	0.038	0.027	0.065
84:00:00	0.678	0.000	0.091	0.037	0.028	0.064
85:00:00	0.647	0.000	0.087	0.036	0.028	0.064
86:00:00	0.619	0.000	0.084	0.034	0.028	0.063
87:00:00	0.591	0.000	0.080	0.033	0.029	0.062
88:00:00	0.564	0.000	0.077	0.032	0.029	0.061
89:00:00	0.539	0.000	0.074	0.031	0.029	0.060
90:00:00	0.515	0.000	0.071	0.030	0.030	0.059
91:00:00	0.492	0.000	0.068	0.028	0.030	0.058
92:00:00	0.470	0.000	0.065	0.027	0.030	0.058
93:00:00	0.448	0.000	0.062	0.026	0.030	0.057
94:00:00	0.428	0.000	0.059	0.025	0.031	0.056
95:00:00	0.409	0.000	0.057	0.024	0.031	0.055
96:00:00	0.390	0.000	0.054	0.023	0.031	0.054
97:00:00	0.373	0.000	0.052	0.022	0.031	0.053
98:00:00	0.356	0.000	0.050	0.021	0.031	0.052
99:00:00	0.340	0.000	0.048	0.020	0.031	0.052
100:00:00	0.324	0.000	0.045	0.020	0.031	0.051
101:00:00	0.309	0.000	0.043	0.019	0.031	0.050
102:00:00	0.295	0.000	0.042	0.018	0.031	0.049
103:00:00	0.282	0.000	0.040	0.017	0.031	0.048
104:00:00	0.269	0.000	0.038	0.017	0.031	0.048
105:00:00	0.257	0.000	0.036	0.016	0.031	0.047
106:00:00	0.245	0.000	0.035	0.015	0.031	0.046

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
107:00:00	0.234	0.000	0.033	0.015	0.031	0.045
108:00:00	0.223	0.000	0.032	0.014	0.031	0.044
109:00:00	0.213	0.000	0.030	0.013	0.030	0.044
110:00:00	0.203	0.000	0.029	0.013	0.030	0.043
111:00:00	0.194	0.000	0.028	0.012	0.030	0.042
112:00:00	0.185	0.000	0.026	0.012	0.030	0.042
113:00:00	0.176	0.000	0.025	0.011	0.030	0.041
114:00:00	0.168	0.000	0.024	0.011	0.030	0.040
115:00:00	0.161	0.000	0.023	0.010	0.029	0.040
116:00:00	0.153	0.000	0.022	0.010	0.029	0.039
117:00:00	0.146	0.000	0.021	0.009	0.029	0.038
118:00:00	0.139	0.000	0.020	0.009	0.029	0.038
119:00:00	0.133	0.000	0.019	0.008	0.029	0.037
120:00:00	0.127	0.000	0.018	0.008	0.028	0.036
121:00:00	0.000	0.000	0.000	0.008	0.028	0.036
122:00:00	0.000	0.000	0.000	0.007	0.028	0.035
123:00:00	0.000	0.000	0.000	0.007	0.028	0.034
124:00:00	0.000	0.000	0.000	0.006	0.027	0.034
125:00:00	0.000	0.000	0.000	0.006	0.027	0.033
126:00:00	0.000	0.000	0.000	0.005	0.027	0.032
127:00:00	0.000	0.000	0.000	0.004	0.027	0.031
128:00:00	0.000	0.000	0.000	0.004	0.026	0.030
129:00:00	0.000	0.000	0.000	0.003	0.026	0.029
130:00:00	0.000	0.000	0.000	0.003	0.026	0.028
131:00:00	0.000	0.000	0.000	0.002	0.025	0.027
132:00:00	0.000	0.000	0.000	0.002	0.025	0.027
133:00:00	0.000	0.000	0.000	0.001	0.025	0.026
134:00:00	0.000	0.000	0.000	0.001	0.024	0.025
135:00:00	0.000	0.000	0.000	0.001	0.024	0.025
136:00:00	0.000	0.000	0.000	0.001	0.024	0.024
137:00:00	0.000	0.000	0.000	0.001	0.023	0.024
138:00:00	0.000	0.000	0.000	0.001	0.023	0.023
139:00:00	0.000	0.000	0.000	0.000	0.023	0.023
140:00:00	0.000	0.000	0.000	0.000	0.022	0.023
141:00:00	0.000	0.000	0.000	0.000	0.022	0.022
142:00:00	0.000	0.000	0.000	0.000	0.022	0.022

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
143:00:00	0.000	0.000	0.000	0.000	0.021	0.021
144:00:00	0.000	0.000	0.000	0.000	0.021	0.021
145:00:00	0.000	0.000	0.000	0.000	0.021	0.021
146:00:00	0.000	0.000	0.000	0.000	0.020	0.020
147:00:00	0.000	0.000	0.000	0.000	0.020	0.020
148:00:00	0.000	0.000	0.000	0.000	0.020	0.020
149:00:00	0.000	0.000	0.000	0.000	0.019	0.019
150:00:00	0.000	0.000	0.000	0.000	0.019	0.019
151:00:00	0.000	0.000	0.000	0.000	0.019	0.019
152:00:00	0.000	0.000	0.000	0.000	0.018	0.018
153:00:00	0.000	0.000	0.000	0.000	0.018	0.018
154:00:00	0.000	0.000	0.000	0.000	0.018	0.018
155:00:00	0.000	0.000	0.000	0.000	0.018	0.018
156:00:00	0.000	0.000	0.000	0.000	0.017	0.017
157:00:00	0.000	0.000	0.000	0.000	0.017	0.017
158:00:00	0.000	0.000	0.000	0.000	0.017	0.017
159:00:00	0.000	0.000	0.000	0.000	0.017	0.017
160:00:00	0.000	0.000	0.000	0.000	0.016	0.016
161:00:00	0.000	0.000	0.000	0.000	0.016	0.016
162:00:00	0.000	0.000	0.000	0.000	0.016	0.016
163:00:00	0.000	0.000	0.000	0.000	0.016	0.016
164:00:00	0.000	0.000	0.000	0.000	0.015	0.015
165:00:00	0.000	0.000	0.000	0.000	0.015	0.015
166:00:00	0.000	0.000	0.000	0.000	0.015	0.015
167:00:00	0.000	0.000	0.000	0.000	0.015	0.015
168:00:00	0.000	0.000	0.000	0.000	0.014	0.014
169:00:00	0.000	0.000	0.000	0.000	0.014	0.014
170:00:00	0.000	0.000	0.000	0.000	0.014	0.014
171:00:00	0.000	0.000	0.000	0.000	0.014	0.014
172:00:00	0.000	0.000	0.000	0.000	0.014	0.014
173:00:00	0.000	0.000	0.000	0.000	0.013	0.013
174:00:00	0.000	0.000	0.000	0.000	0.013	0.013
175:00:00	0.000	0.000	0.000	0.000	0.013	0.013
176:00:00	0.000	0.000	0.000	0.000	0.013	0.013
177:00:00	0.000	0.000	0.000	0.000	0.012	0.012
178:00:00	0.000	0.000	0.000	0.000	0.012	0.012

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
179:00:00	0.000	0.000	0.000	0.000	0.012	0.012
180:00:00	0.000	0.000	0.000	0.000	0.012	0.012
181:00:00	0.000	0.000	0.000	0.000	0.012	0.012
182:00:00	0.000	0.000	0.000	0.000	0.012	0.012
183:00:00	0.000	0.000	0.000	0.000	0.011	0.011
184:00:00	0.000	0.000	0.000	0.000	0.011	0.011
185:00:00	0.000	0.000	0.000	0.000	0.011	0.011
186:00:00	0.000	0.000	0.000	0.000	0.011	0.011
187:00:00	0.000	0.000	0.000	0.000	0.011	0.011
188:00:00	0.000	0.000	0.000	0.000	0.011	0.011
189:00:00	0.000	0.000	0.000	0.000	0.010	0.010
190:00:00	0.000	0.000	0.000	0.000	0.010	0.010
191:00:00	0.000	0.000	0.000	0.000	0.010	0.010
192:00:00	0.000	0.000	0.000	0.000	0.010	0.010
193:00:00	0.000	0.000	0.000	0.000	0.010	0.010
194:00:00	0.000	0.000	0.000	0.000	0.010	0.010
195:00:00	0.000	0.000	0.000	0.000	0.009	0.009
196:00:00	0.000	0.000	0.000	0.000	0.009	0.009
197:00:00	0.000	0.000	0.000	0.000	0.009	0.009
198:00:00	0.000	0.000	0.000	0.000	0.009	0.009
199:00:00	0.000	0.000	0.000	0.000	0.009	0.009
200:00:00	0.000	0.000	0.000	0.000	0.009	0.009
201:00:00	0.000	0.000	0.000	0.000	0.009	0.009
202:00:00	0.000	0.000	0.000	0.000	0.008	0.008
203:00:00	0.000	0.000	0.000	0.000	0.008	0.008
204:00:00	0.000	0.000	0.000	0.000	0.008	0.008
205:00:00	0.000	0.000	0.000	0.000	0.008	0.008
206:00:00	0.000	0.000	0.000	0.000	0.008	0.008
207:00:00	0.000	0.000	0.000	0.000	0.008	0.008
208:00:00	0.000	0.000	0.000	0.000	0.008	0.008
209:00:00	0.000	0.000	0.000	0.000	0.008	0.008
210:00:00	0.000	0.000	0.000	0.000	0.007	0.007
211:00:00	0.000	0.000	0.000	0.000	0.007	0.007
212:00:00	0.000	0.000	0.000	0.000	0.007	0.007
213:00:00	0.000	0.000	0.000	0.000	0.007	0.007
214:00:00	0.000	0.000	0.000	0.000	0.007	0.007

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
215:00:00	0.000	0.000	0.000	0.000	0.007	0.007
216:00:00	0.000	0.000	0.000	0.000	0.007	0.007
217:00:00	0.000	0.000	0.000	0.000	0.007	0.007
218:00:00	0.000	0.000	0.000	0.000	0.007	0.007
219:00:00	0.000	0.000	0.000	0.000	0.006	0.006
220:00:00	0.000	0.000	0.000	0.000	0.006	0.006
221:00:00	0.000	0.000	0.000	0.000	0.006	0.006
222:00:00	0.000	0.000	0.000	0.000	0.006	0.006
223:00:00	0.000	0.000	0.000	0.000	0.006	0.006
224:00:00	0.000	0.000	0.000	0.000	0.006	0.006
225:00:00	0.000	0.000	0.000	0.000	0.006	0.006
226:00:00	0.000	0.000	0.000	0.000	0.006	0.006
227:00:00	0.000	0.000	0.000	0.000	0.006	0.006
228:00:00	0.000	0.000	0.000	0.000	0.006	0.006
229:00:00	0.000	0.000	0.000	0.000	0.006	0.006
230:00:00	0.000	0.000	0.000	0.000	0.005	0.005
231:00:00	0.000	0.000	0.000	0.000	0.005	0.005
232:00:00	0.000	0.000	0.000	0.000	0.005	0.005
233:00:00	0.000	0.000	0.000	0.000	0.005	0.005
234:00:00	0.000	0.000	0.000	0.000	0.005	0.005
235:00:00	0.000	0.000	0.000	0.000	0.005	0.005
236:00:00	0.000	0.000	0.000	0.000	0.005	0.005
237:00:00	0.000	0.000	0.000	0.000	0.005	0.005
238:00:00	0.000	0.000	0.000	0.000	0.005	0.005
239:00:00	0.000	0.000	0.000	0.000	0.005	0.005
240:00:00	0.000	0.000	0.000	0.000	0.005	0.005
241:00:00	0.000	0.000	0.000	0.000	0.005	0.005
242:00:00	0.000	0.000	0.000	0.000	0.005	0.005
243:00:00	0.000	0.000	0.000	0.000	0.004	0.004
244:00:00	0.000	0.000	0.000	0.000	0.004	0.004
245:00:00	0.000	0.000	0.000	0.000	0.004	0.004
246:00:00	0.000	0.000	0.000	0.000	0.004	0.004
247:00:00	0.000	0.000	0.000	0.000	0.004	0.004
248:00:00	0.000	0.000	0.000	0.000	0.004	0.004
249:00:00	0.000	0.000	0.000	0.000	0.004	0.004
250:00:00	0.000	0.000	0.000	0.000	0.004	0.004

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
251:00:00	0.000	0.000	0.000	0.000	0.004	0.004
252:00:00	0.000	0.000	0.000	0.000	0.004	0.004
253:00:00	0.000	0.000	0.000	0.000	0.004	0.004
254:00:00	0.000	0.000	0.000	0.000	0.004	0.004
255:00:00	0.000	0.000	0.000	0.000	0.004	0.004
256:00:00	0.000	0.000	0.000	0.000	0.004	0.004
257:00:00	0.000	0.000	0.000	0.000	0.004	0.004
258:00:00	0.000	0.000	0.000	0.000	0.004	0.004
259:00:00	0.000	0.000	0.000	0.000	0.003	0.003
260:00:00	0.000	0.000	0.000	0.000	0.003	0.003
261:00:00	0.000	0.000	0.000	0.000	0.003	0.003
262:00:00	0.000	0.000	0.000	0.000	0.003	0.003
263:00:00	0.000	0.000	0.000	0.000	0.003	0.003
264:00:00	0.000	0.000	0.000	0.000	0.003	0.003
265:00:00	0.000	0.000	0.000	0.000	0.003	0.003
266:00:00	0.000	0.000	0.000	0.000	0.003	0.003
267:00:00	0.000	0.000	0.000	0.000	0.003	0.003
268:00:00	0.000	0.000	0.000	0.000	0.003	0.003
269:00:00	0.000	0.000	0.000	0.000	0.003	0.003
270:00:00	0.000	0.000	0.000	0.000	0.003	0.003
271:00:00	0.000	0.000	0.000	0.000	0.003	0.003
272:00:00	0.000	0.000	0.000	0.000	0.003	0.003
273:00:00	0.000	0.000	0.000	0.000	0.003	0.003
274:00:00	0.000	0.000	0.000	0.000	0.003	0.003
275:00:00	0.000	0.000	0.000	0.000	0.003	0.003
276:00:00	0.000	0.000	0.000	0.000	0.003	0.003
277:00:00	0.000	0.000	0.000	0.000	0.003	0.003
278:00:00	0.000	0.000	0.000	0.000	0.003	0.003
279:00:00	0.000	0.000	0.000	0.000	0.003	0.003
280:00:00	0.000	0.000	0.000	0.000	0.002	0.002
281:00:00	0.000	0.000	0.000	0.000	0.002	0.002
282:00:00	0.000	0.000	0.000	0.000	0.002	0.002
283:00:00	0.000	0.000	0.000	0.000	0.002	0.002
284:00:00	0.000	0.000	0.000	0.000	0.002	0.002
285:00:00	0.000	0.000	0.000	0.000	0.002	0.002
286:00:00	0.000	0.000	0.000	0.000	0.002	0.002

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
287:00:00	0.000	0.000	0.000	0.000	0.002	0.002
288:00:00	0.000	0.000	0.000	0.000	0.002	0.002
289:00:00	0.000	0.000	0.000	0.000	0.002	0.002
290:00:00	0.000	0.000	0.000	0.000	0.002	0.002
291:00:00	0.000	0.000	0.000	0.000	0.002	0.002
292:00:00	0.000	0.000	0.000	0.000	0.002	0.002
293:00:00	0.000	0.000	0.000	0.000	0.002	0.002
294:00:00	0.000	0.000	0.000	0.000	0.002	0.002
295:00:00	0.000	0.000	0.000	0.000	0.002	0.002
296:00:00	0.000	0.000	0.000	0.000	0.002	0.002
297:00:00	0.000	0.000	0.000	0.000	0.002	0.002
298:00:00	0.000	0.000	0.000	0.000	0.002	0.002
299:00:00	0.000	0.000	0.000	0.000	0.002	0.002
300:00:00	0.000	0.000	0.000	0.000	0.002	0.002
301:00:00	0.000	0.000	0.000	0.000	0.002	0.002
302:00:00	0.000	0.000	0.000	0.000	0.002	0.002
303:00:00	0.000	0.000	0.000	0.000	0.002	0.002
304:00:00	0.000	0.000	0.000	0.000	0.002	0.002
305:00:00	0.000	0.000	0.000	0.000	0.002	0.002
306:00:00	0.000	0.000	0.000	0.000	0.002	0.002
307:00:00	0.000	0.000	0.000	0.000	0.002	0.002
308:00:00	0.000	0.000	0.000	0.000	0.002	0.002
309:00:00	0.000	0.000	0.000	0.000	0.002	0.002
310:00:00	0.000	0.000	0.000	0.000	0.002	0.002
311:00:00	0.000	0.000	0.000	0.000	0.002	0.002
312:00:00	0.000	0.000	0.000	0.000	0.002	0.002
313:00:00	0.000	0.000	0.000	0.000	0.001	0.001
314:00:00	0.000	0.000	0.000	0.000	0.001	0.001
315:00:00	0.000	0.000	0.000	0.000	0.001	0.001
316:00:00	0.000	0.000	0.000	0.000	0.001	0.001
317:00:00	0.000	0.000	0.000	0.000	0.001	0.001
318:00:00	0.000	0.000	0.000	0.000	0.001	0.001
319:00:00	0.000	0.000	0.000	0.000	0.001	0.001
320:00:00	0.000	0.000	0.000	0.000	0.001	0.001
321:00:00	0.000	0.000	0.000	0.000	0.001	0.001
322:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
323:00:00	0.000	0.000	0.000	0.000	0.001	0.001
324:00:00	0.000	0.000	0.000	0.000	0.001	0.001
325:00:00	0.000	0.000	0.000	0.000	0.001	0.001
326:00:00	0.000	0.000	0.000	0.000	0.001	0.001
327:00:00	0.000	0.000	0.000	0.000	0.001	0.001
328:00:00	0.000	0.000	0.000	0.000	0.001	0.001
329:00:00	0.000	0.000	0.000	0.000	0.001	0.001
330:00:00	0.000	0.000	0.000	0.000	0.001	0.001
331:00:00	0.000	0.000	0.000	0.000	0.001	0.001
332:00:00	0.000	0.000	0.000	0.000	0.001	0.001
333:00:00	0.000	0.000	0.000	0.000	0.001	0.001
334:00:00	0.000	0.000	0.000	0.000	0.001	0.001
335:00:00	0.000	0.000	0.000	0.000	0.001	0.001
336:00:00	0.000	0.000	0.000	0.000	0.001	0.001
337:00:00	0.000	0.000	0.000	0.000	0.001	0.001
338:00:00	0.000	0.000	0.000	0.000	0.001	0.001
339:00:00	0.000	0.000	0.000	0.000	0.001	0.001
340:00:00	0.000	0.000	0.000	0.000	0.001	0.001
341:00:00	0.000	0.000	0.000	0.000	0.001	0.001
342:00:00	0.000	0.000	0.000	0.000	0.001	0.001
343:00:00	0.000	0.000	0.000	0.000	0.001	0.001
344:00:00	0.000	0.000	0.000	0.000	0.001	0.001
345:00:00	0.000	0.000	0.000	0.000	0.001	0.001
346:00:00	0.000	0.000	0.000	0.000	0.001	0.001
347:00:00	0.000	0.000	0.000	0.000	0.001	0.001
348:00:00	0.000	0.000	0.000	0.000	0.001	0.001
349:00:00	0.000	0.000	0.000	0.000	0.001	0.001
350:00:00	0.000	0.000	0.000	0.000	0.001	0.001
351:00:00	0.000	0.000	0.000	0.000	0.001	0.001
352:00:00	0.000	0.000	0.000	0.000	0.001	0.001
353:00:00	0.000	0.000	0.000	0.000	0.001	0.001
354:00:00	0.000	0.000	0.000	0.000	0.001	0.001
355:00:00	0.000	0.000	0.000	0.000	0.001	0.001
356:00:00	0.000	0.000	0.000	0.000	0.001	0.001
357:00:00	0.000	0.000	0.000	0.000	0.001	0.001
358:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
359:00:00	0.000	0.000	0.000	0.000	0.001	0.001
360:00:00	0.000	0.000	0.000	0.000	0.001	0.001
361:00:00	0.000	0.000	0.000	0.000	0.001	0.001
362:00:00	0.000	0.000	0.000	0.000	0.001	0.001
363:00:00	0.000	0.000	0.000	0.000	0.001	0.001
364:00:00	0.000	0.000	0.000	0.000	0.001	0.001
365:00:00	0.000	0.000	0.000	0.000	0.001	0.001
366:00:00	0.000	0.000	0.000	0.000	0.001	0.001
367:00:00	0.000	0.000	0.000	0.000	0.001	0.001
368:00:00	0.000	0.000	0.000	0.000	0.001	0.001
369:00:00	0.000	0.000	0.000	0.000	0.001	0.001
370:00:00	0.000	0.000	0.000	0.000	0.001	0.001
371:00:00	0.000	0.000	0.000	0.000	0.001	0.001
372:00:00	0.000	0.000	0.000	0.000	0.001	0.001
373:00:00	0.000	0.000	0.000	0.000	0.001	0.001
374:00:00	0.000	0.000	0.000	0.000	0.001	0.001
375:00:00	0.000	0.000	0.000	0.000	0.001	0.001
376:00:00	0.000	0.000	0.000	0.000	0.001	0.001
377:00:00	0.000	0.000	0.000	0.000	0.001	0.001
378:00:00	0.000	0.000	0.000	0.000	0.001	0.001
379:00:00	0.000	0.000	0.000	0.000	0.001	0.001
380:00:00	0.000	0.000	0.000	0.000	0.001	0.001
381:00:00	0.000	0.000	0.000	0.000	0.001	0.001
382:00:00	0.000	0.000	0.000	0.000	0.001	0.001
383:00:00	0.000	0.000	0.000	0.000	0.000	0.000
384:00:00	0.000	0.000	0.000	0.000	0.000	0.000
385:00:00	0.000	0.000	0.000	0.000	0.000	0.000
386:00:00	0.000	0.000	0.000	0.000	0.000	0.000
387:00:00	0.000	0.000	0.000	0.000	0.000	0.000
388:00:00	0.000	0.000	0.000	0.000	0.000	0.000
389:00:00	0.000	0.000	0.000	0.000	0.000	0.000
390:00:00	0.000	0.000	0.000	0.000	0.000	0.000
391:00:00	0.000	0.000	0.000	0.000	0.000	0.000
392:00:00	0.000	0.000	0.000	0.000	0.000	0.000
393:00:00	0.000	0.000	0.000	0.000	0.000	0.000
394:00:00	0.000	0.000	0.000	0.000	0.000	0.000

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Appendix

Catchment descriptors

Name	Value	User-defined value used?
Area (km^2)	1.02	No
ALTBAR	12	No
ASPBAR	0.44	No
ASPVAR	0	No
BFIHOST	0.89	No
DPLBAR (km)	2.27	No
DPSBAR (mkm^{-1})	8.7	No
FARL	1	No
LDP	4.98	No
PROPWET (mm)	0.26	No
RMED1H	11	No
RMED1D	30.2	No
RMED2D	38.6	No
SAAR (mm)	586	No
SAAR4170 (mm)	593	No
SPRHOST	14.52	No
Urbext2000	0.09	No
Urbext1990	0.05	No
URBCONC	0.84	No
URBLOC	1.47	No
DDF parameter C	-0.02	No
DDF parameter D1	0.3	No
DDF parameter D2	0.28	No
DDF parameter D3	0.21	No
DDF parameter E	0.31	No
DDF parameter F	2.51	No
DDF parameter C (1km grid value)	0	No
DDF parameter D1 (1km grid value)	0	No
DDF parameter D2 (1km grid value)	0	No
DDF parameter D3 (1km grid value)	0	No
DDF parameter E (1km grid value)	0	No
DDF parameter F (1km grid value)	0	No

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

UK Design Flood Estimation

Generated on 11 May 2021 16:01:37 by AEA_COMPUTER
Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH2)

Site details Checksum: E712-CE06

Site name: tmpA4

Easting: 647359

Northing: 262815

Country: England, Wales or Northern Ireland

Catchment Area (km²): 0.86

Using plot scale calculations: No

Model: ReFH2.2

Site description: None

Model run: 100 year - LEIS_SIZEW3

Summary of results

Rainfall - FEH 2013 model (mm):	121.74	Total runoff (ML):	7.77
Total Rainfall (mm):	81.34	Total flow (ML):	18.81
Peak Rainfall (mm):	1.78	Peak flow (m³/s):	0.06

Parameters

Where the user has overriden a system-generated value, this original value is shown in square brackets after the value used.
** Indicates that the user locked the duration/timestep*

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	121:00:00 [11:00:00]	Yes
Timestep (hh:mm:ss)	01:00:00	No
SCF (Seasonal correction factor)	0.67	No
ARF (Areal reduction factor)	0.99	No
Seasonality	Winter	No

Loss model parameters

Name	Value	User-defined?
Cini (mm)	60.53	No
Cmax (mm)	1190.38	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No
Use seasonal CIni for equations	No [Yes]	Yes

Routing model parameters

Name	Value	User-defined?
Tp (hr)	7.15	No
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m^3/s)	0	No
BL (hr)	63.92	No
BR	2.16	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km^2)	0.12	No
Urbext 2000	0.09	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Exporting drained area (km^2)	0.00	Yes
Sewer capacity (m^3/s)	0.00	Yes

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Time series data

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
00:00:00	0.127	0.000	0.010	0.000	0.000	0.000
01:00:00	0.133	0.000	0.010	0.000	0.000	0.000
02:00:00	0.139	0.000	0.011	0.000	0.000	0.000
03:00:00	0.146	0.000	0.011	0.000	0.000	0.000
04:00:00	0.153	0.000	0.012	0.001	0.000	0.001
05:00:00	0.161	0.000	0.013	0.001	0.000	0.001
06:00:00	0.168	0.000	0.013	0.001	0.000	0.001
07:00:00	0.176	0.000	0.014	0.001	0.000	0.001
08:00:00	0.185	0.000	0.015	0.002	0.000	0.002
09:00:00	0.194	0.000	0.015	0.002	0.000	0.002
10:00:00	0.203	0.000	0.016	0.002	0.000	0.002
11:00:00	0.213	0.000	0.017	0.002	0.000	0.002
12:00:00	0.223	0.000	0.018	0.003	0.000	0.003
13:00:00	0.234	0.000	0.019	0.003	0.000	0.003
14:00:00	0.245	0.000	0.020	0.003	0.000	0.003
15:00:00	0.257	0.000	0.021	0.003	0.000	0.003
16:00:00	0.269	0.000	0.022	0.003	0.000	0.004
17:00:00	0.282	0.000	0.023	0.004	0.000	0.004
18:00:00	0.295	0.000	0.024	0.004	0.000	0.004
19:00:00	0.310	0.000	0.025	0.004	0.000	0.004
20:00:00	0.324	0.000	0.027	0.004	0.001	0.005
21:00:00	0.340	0.000	0.028	0.004	0.001	0.005
22:00:00	0.356	0.000	0.029	0.005	0.001	0.005
23:00:00	0.373	0.000	0.031	0.005	0.001	0.006
24:00:00	0.390	0.000	0.032	0.005	0.001	0.006
25:00:00	0.409	0.000	0.034	0.005	0.001	0.006
26:00:00	0.428	0.000	0.036	0.006	0.001	0.007
27:00:00	0.449	0.000	0.038	0.006	0.001	0.007
28:00:00	0.470	0.000	0.040	0.006	0.001	0.008
29:00:00	0.492	0.000	0.042	0.007	0.001	0.008
30:00:00	0.515	0.000	0.044	0.007	0.001	0.008
31:00:00	0.539	0.000	0.046	0.007	0.001	0.009
32:00:00	0.565	0.000	0.049	0.008	0.002	0.009
33:00:00	0.591	0.000	0.051	0.008	0.002	0.010
34:00:00	0.619	0.000	0.054	0.009	0.002	0.010

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
35:00:00	0.648	0.000	0.057	0.009	0.002	0.011
36:00:00	0.678	0.000	0.060	0.009	0.002	0.012
37:00:00	0.709	0.000	0.063	0.010	0.002	0.012
38:00:00	0.742	0.000	0.066	0.010	0.002	0.013
39:00:00	0.777	0.000	0.070	0.011	0.003	0.013
40:00:00	0.813	0.000	0.073	0.012	0.003	0.014
41:00:00	0.850	0.000	0.077	0.012	0.003	0.015
42:00:00	0.889	0.000	0.082	0.013	0.003	0.016
43:00:00	0.930	0.000	0.086	0.013	0.003	0.017
44:00:00	0.972	0.000	0.091	0.014	0.003	0.018
45:00:00	1.016	0.000	0.095	0.015	0.004	0.019
46:00:00	1.062	0.000	0.101	0.016	0.004	0.020
47:00:00	1.110	0.000	0.106	0.017	0.004	0.021
48:00:00	1.159	0.000	0.112	0.017	0.004	0.022
49:00:00	1.211	0.000	0.118	0.018	0.005	0.023
50:00:00	1.264	0.000	0.125	0.019	0.005	0.024
51:00:00	1.319	0.000	0.131	0.020	0.005	0.025
52:00:00	1.376	0.000	0.139	0.021	0.005	0.027
53:00:00	1.435	0.000	0.146	0.023	0.006	0.028
54:00:00	1.495	0.000	0.154	0.024	0.006	0.030
55:00:00	1.556	0.000	0.162	0.025	0.007	0.031
56:00:00	1.617	0.000	0.171	0.026	0.007	0.033
57:00:00	1.678	0.000	0.179	0.028	0.007	0.035
58:00:00	1.734	0.000	0.188	0.029	0.008	0.037
59:00:00	1.777	0.000	0.195	0.031	0.008	0.039
60:00:00	1.758	0.000	0.195	0.032	0.009	0.041
61:00:00	1.777	0.000	0.200	0.034	0.009	0.043
62:00:00	1.734	0.000	0.198	0.036	0.010	0.045
63:00:00	1.678	0.000	0.193	0.037	0.010	0.047
64:00:00	1.617	0.000	0.189	0.038	0.011	0.049
65:00:00	1.556	0.000	0.183	0.040	0.012	0.051
66:00:00	1.495	0.000	0.178	0.041	0.012	0.053
67:00:00	1.435	0.000	0.173	0.041	0.013	0.054
68:00:00	1.376	0.000	0.167	0.042	0.014	0.055
69:00:00	1.319	0.000	0.162	0.042	0.014	0.056
70:00:00	1.264	0.000	0.156	0.042	0.015	0.057

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
71:00:00	1.211	0.000	0.151	0.042	0.016	0.058
72:00:00	1.159	0.000	0.145	0.042	0.016	0.058
73:00:00	1.110	0.000	0.140	0.041	0.017	0.058
74:00:00	1.062	0.000	0.135	0.041	0.018	0.058
75:00:00	1.016	0.000	0.130	0.040	0.018	0.058
76:00:00	0.972	0.000	0.125	0.039	0.019	0.058
77:00:00	0.930	0.000	0.121	0.038	0.020	0.058
78:00:00	0.889	0.000	0.116	0.037	0.020	0.058
79:00:00	0.850	0.000	0.111	0.036	0.021	0.057
80:00:00	0.813	0.000	0.107	0.035	0.021	0.057
81:00:00	0.777	0.000	0.103	0.034	0.022	0.056
82:00:00	0.742	0.000	0.099	0.033	0.022	0.056
83:00:00	0.709	0.000	0.095	0.032	0.023	0.055
84:00:00	0.678	0.000	0.091	0.031	0.023	0.054
85:00:00	0.648	0.000	0.087	0.030	0.024	0.054
86:00:00	0.619	0.000	0.084	0.029	0.024	0.053
87:00:00	0.591	0.000	0.080	0.028	0.024	0.052
88:00:00	0.565	0.000	0.077	0.027	0.025	0.051
89:00:00	0.539	0.000	0.074	0.026	0.025	0.051
90:00:00	0.515	0.000	0.071	0.025	0.025	0.050
91:00:00	0.492	0.000	0.068	0.024	0.025	0.049
92:00:00	0.470	0.000	0.065	0.023	0.026	0.049
93:00:00	0.449	0.000	0.062	0.022	0.026	0.048
94:00:00	0.428	0.000	0.059	0.021	0.026	0.047
95:00:00	0.409	0.000	0.057	0.020	0.026	0.046
96:00:00	0.390	0.000	0.054	0.020	0.026	0.046
97:00:00	0.373	0.000	0.052	0.019	0.026	0.045
98:00:00	0.356	0.000	0.050	0.018	0.026	0.044
99:00:00	0.340	0.000	0.048	0.017	0.026	0.043
100:00:00	0.324	0.000	0.046	0.017	0.026	0.043
101:00:00	0.310	0.000	0.044	0.016	0.026	0.042
102:00:00	0.295	0.000	0.042	0.015	0.026	0.041
103:00:00	0.282	0.000	0.040	0.015	0.026	0.041
104:00:00	0.269	0.000	0.038	0.014	0.026	0.040
105:00:00	0.257	0.000	0.036	0.013	0.026	0.039
106:00:00	0.245	0.000	0.035	0.013	0.026	0.039

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
107:00:00	0.234	0.000	0.033	0.012	0.026	0.038
108:00:00	0.223	0.000	0.032	0.012	0.026	0.038
109:00:00	0.213	0.000	0.030	0.011	0.026	0.037
110:00:00	0.203	0.000	0.029	0.011	0.026	0.036
111:00:00	0.194	0.000	0.028	0.010	0.025	0.036
112:00:00	0.185	0.000	0.026	0.010	0.025	0.035
113:00:00	0.176	0.000	0.025	0.009	0.025	0.035
114:00:00	0.168	0.000	0.024	0.009	0.025	0.034
115:00:00	0.161	0.000	0.023	0.009	0.025	0.033
116:00:00	0.153	0.000	0.022	0.008	0.025	0.033
117:00:00	0.146	0.000	0.021	0.008	0.024	0.032
118:00:00	0.139	0.000	0.020	0.007	0.024	0.032
119:00:00	0.133	0.000	0.019	0.007	0.024	0.031
120:00:00	0.127	0.000	0.018	0.007	0.024	0.031
121:00:00	0.000	0.000	0.000	0.007	0.024	0.030
122:00:00	0.000	0.000	0.000	0.006	0.024	0.030
123:00:00	0.000	0.000	0.000	0.006	0.023	0.029
124:00:00	0.000	0.000	0.000	0.005	0.023	0.028
125:00:00	0.000	0.000	0.000	0.005	0.023	0.028
126:00:00	0.000	0.000	0.000	0.004	0.023	0.027
127:00:00	0.000	0.000	0.000	0.004	0.022	0.026
128:00:00	0.000	0.000	0.000	0.003	0.022	0.025
129:00:00	0.000	0.000	0.000	0.003	0.022	0.024
130:00:00	0.000	0.000	0.000	0.002	0.022	0.024
131:00:00	0.000	0.000	0.000	0.002	0.021	0.023
132:00:00	0.000	0.000	0.000	0.001	0.021	0.023
133:00:00	0.000	0.000	0.000	0.001	0.021	0.022
134:00:00	0.000	0.000	0.000	0.001	0.021	0.022
135:00:00	0.000	0.000	0.000	0.001	0.020	0.021
136:00:00	0.000	0.000	0.000	0.001	0.020	0.021
137:00:00	0.000	0.000	0.000	0.001	0.020	0.020
138:00:00	0.000	0.000	0.000	0.000	0.019	0.020
139:00:00	0.000	0.000	0.000	0.000	0.019	0.019
140:00:00	0.000	0.000	0.000	0.000	0.019	0.019
141:00:00	0.000	0.000	0.000	0.000	0.018	0.019
142:00:00	0.000	0.000	0.000	0.000	0.018	0.018

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
143:00:00	0.000	0.000	0.000	0.000	0.018	0.018
144:00:00	0.000	0.000	0.000	0.000	0.018	0.018
145:00:00	0.000	0.000	0.000	0.000	0.017	0.017
146:00:00	0.000	0.000	0.000	0.000	0.017	0.017
147:00:00	0.000	0.000	0.000	0.000	0.017	0.017
148:00:00	0.000	0.000	0.000	0.000	0.017	0.017
149:00:00	0.000	0.000	0.000	0.000	0.016	0.016
150:00:00	0.000	0.000	0.000	0.000	0.016	0.016
151:00:00	0.000	0.000	0.000	0.000	0.016	0.016
152:00:00	0.000	0.000	0.000	0.000	0.016	0.016
153:00:00	0.000	0.000	0.000	0.000	0.015	0.015
154:00:00	0.000	0.000	0.000	0.000	0.015	0.015
155:00:00	0.000	0.000	0.000	0.000	0.015	0.015
156:00:00	0.000	0.000	0.000	0.000	0.015	0.015
157:00:00	0.000	0.000	0.000	0.000	0.014	0.014
158:00:00	0.000	0.000	0.000	0.000	0.014	0.014
159:00:00	0.000	0.000	0.000	0.000	0.014	0.014
160:00:00	0.000	0.000	0.000	0.000	0.014	0.014
161:00:00	0.000	0.000	0.000	0.000	0.014	0.014
162:00:00	0.000	0.000	0.000	0.000	0.013	0.013
163:00:00	0.000	0.000	0.000	0.000	0.013	0.013
164:00:00	0.000	0.000	0.000	0.000	0.013	0.013
165:00:00	0.000	0.000	0.000	0.000	0.013	0.013
166:00:00	0.000	0.000	0.000	0.000	0.013	0.013
167:00:00	0.000	0.000	0.000	0.000	0.012	0.012
168:00:00	0.000	0.000	0.000	0.000	0.012	0.012
169:00:00	0.000	0.000	0.000	0.000	0.012	0.012
170:00:00	0.000	0.000	0.000	0.000	0.012	0.012
171:00:00	0.000	0.000	0.000	0.000	0.012	0.012
172:00:00	0.000	0.000	0.000	0.000	0.011	0.011
173:00:00	0.000	0.000	0.000	0.000	0.011	0.011
174:00:00	0.000	0.000	0.000	0.000	0.011	0.011
175:00:00	0.000	0.000	0.000	0.000	0.011	0.011
176:00:00	0.000	0.000	0.000	0.000	0.011	0.011
177:00:00	0.000	0.000	0.000	0.000	0.011	0.011
178:00:00	0.000	0.000	0.000	0.000	0.010	0.010

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
179:00:00	0.000	0.000	0.000	0.000	0.010	0.010
180:00:00	0.000	0.000	0.000	0.000	0.010	0.010
181:00:00	0.000	0.000	0.000	0.000	0.010	0.010
182:00:00	0.000	0.000	0.000	0.000	0.010	0.010
183:00:00	0.000	0.000	0.000	0.000	0.010	0.010
184:00:00	0.000	0.000	0.000	0.000	0.009	0.009
185:00:00	0.000	0.000	0.000	0.000	0.009	0.009
186:00:00	0.000	0.000	0.000	0.000	0.009	0.009
187:00:00	0.000	0.000	0.000	0.000	0.009	0.009
188:00:00	0.000	0.000	0.000	0.000	0.009	0.009
189:00:00	0.000	0.000	0.000	0.000	0.009	0.009
190:00:00	0.000	0.000	0.000	0.000	0.009	0.009
191:00:00	0.000	0.000	0.000	0.000	0.008	0.008
192:00:00	0.000	0.000	0.000	0.000	0.008	0.008
193:00:00	0.000	0.000	0.000	0.000	0.008	0.008
194:00:00	0.000	0.000	0.000	0.000	0.008	0.008
195:00:00	0.000	0.000	0.000	0.000	0.008	0.008
196:00:00	0.000	0.000	0.000	0.000	0.008	0.008
197:00:00	0.000	0.000	0.000	0.000	0.008	0.008
198:00:00	0.000	0.000	0.000	0.000	0.008	0.008
199:00:00	0.000	0.000	0.000	0.000	0.007	0.007
200:00:00	0.000	0.000	0.000	0.000	0.007	0.007
201:00:00	0.000	0.000	0.000	0.000	0.007	0.007
202:00:00	0.000	0.000	0.000	0.000	0.007	0.007
203:00:00	0.000	0.000	0.000	0.000	0.007	0.007
204:00:00	0.000	0.000	0.000	0.000	0.007	0.007
205:00:00	0.000	0.000	0.000	0.000	0.007	0.007
206:00:00	0.000	0.000	0.000	0.000	0.007	0.007
207:00:00	0.000	0.000	0.000	0.000	0.007	0.007
208:00:00	0.000	0.000	0.000	0.000	0.006	0.006
209:00:00	0.000	0.000	0.000	0.000	0.006	0.006
210:00:00	0.000	0.000	0.000	0.000	0.006	0.006
211:00:00	0.000	0.000	0.000	0.000	0.006	0.006
212:00:00	0.000	0.000	0.000	0.000	0.006	0.006
213:00:00	0.000	0.000	0.000	0.000	0.006	0.006
214:00:00	0.000	0.000	0.000	0.000	0.006	0.006

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
215:00:00	0.000	0.000	0.000	0.000	0.006	0.006
216:00:00	0.000	0.000	0.000	0.000	0.006	0.006
217:00:00	0.000	0.000	0.000	0.000	0.006	0.006
218:00:00	0.000	0.000	0.000	0.000	0.006	0.006
219:00:00	0.000	0.000	0.000	0.000	0.005	0.005
220:00:00	0.000	0.000	0.000	0.000	0.005	0.005
221:00:00	0.000	0.000	0.000	0.000	0.005	0.005
222:00:00	0.000	0.000	0.000	0.000	0.005	0.005
223:00:00	0.000	0.000	0.000	0.000	0.005	0.005
224:00:00	0.000	0.000	0.000	0.000	0.005	0.005
225:00:00	0.000	0.000	0.000	0.000	0.005	0.005
226:00:00	0.000	0.000	0.000	0.000	0.005	0.005
227:00:00	0.000	0.000	0.000	0.000	0.005	0.005
228:00:00	0.000	0.000	0.000	0.000	0.005	0.005
229:00:00	0.000	0.000	0.000	0.000	0.005	0.005
230:00:00	0.000	0.000	0.000	0.000	0.005	0.005
231:00:00	0.000	0.000	0.000	0.000	0.005	0.005
232:00:00	0.000	0.000	0.000	0.000	0.004	0.004
233:00:00	0.000	0.000	0.000	0.000	0.004	0.004
234:00:00	0.000	0.000	0.000	0.000	0.004	0.004
235:00:00	0.000	0.000	0.000	0.000	0.004	0.004
236:00:00	0.000	0.000	0.000	0.000	0.004	0.004
237:00:00	0.000	0.000	0.000	0.000	0.004	0.004
238:00:00	0.000	0.000	0.000	0.000	0.004	0.004
239:00:00	0.000	0.000	0.000	0.000	0.004	0.004
240:00:00	0.000	0.000	0.000	0.000	0.004	0.004
241:00:00	0.000	0.000	0.000	0.000	0.004	0.004
242:00:00	0.000	0.000	0.000	0.000	0.004	0.004
243:00:00	0.000	0.000	0.000	0.000	0.004	0.004
244:00:00	0.000	0.000	0.000	0.000	0.004	0.004
245:00:00	0.000	0.000	0.000	0.000	0.004	0.004
246:00:00	0.000	0.000	0.000	0.000	0.004	0.004
247:00:00	0.000	0.000	0.000	0.000	0.004	0.004
248:00:00	0.000	0.000	0.000	0.000	0.003	0.003
249:00:00	0.000	0.000	0.000	0.000	0.003	0.003
250:00:00	0.000	0.000	0.000	0.000	0.003	0.003

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
251:00:00	0.000	0.000	0.000	0.000	0.003	0.003
252:00:00	0.000	0.000	0.000	0.000	0.003	0.003
253:00:00	0.000	0.000	0.000	0.000	0.003	0.003
254:00:00	0.000	0.000	0.000	0.000	0.003	0.003
255:00:00	0.000	0.000	0.000	0.000	0.003	0.003
256:00:00	0.000	0.000	0.000	0.000	0.003	0.003
257:00:00	0.000	0.000	0.000	0.000	0.003	0.003
258:00:00	0.000	0.000	0.000	0.000	0.003	0.003
259:00:00	0.000	0.000	0.000	0.000	0.003	0.003
260:00:00	0.000	0.000	0.000	0.000	0.003	0.003
261:00:00	0.000	0.000	0.000	0.000	0.003	0.003
262:00:00	0.000	0.000	0.000	0.000	0.003	0.003
263:00:00	0.000	0.000	0.000	0.000	0.003	0.003
264:00:00	0.000	0.000	0.000	0.000	0.003	0.003
265:00:00	0.000	0.000	0.000	0.000	0.003	0.003
266:00:00	0.000	0.000	0.000	0.000	0.003	0.003
267:00:00	0.000	0.000	0.000	0.000	0.003	0.003
268:00:00	0.000	0.000	0.000	0.000	0.003	0.003
269:00:00	0.000	0.000	0.000	0.000	0.002	0.002
270:00:00	0.000	0.000	0.000	0.000	0.002	0.002
271:00:00	0.000	0.000	0.000	0.000	0.002	0.002
272:00:00	0.000	0.000	0.000	0.000	0.002	0.002
273:00:00	0.000	0.000	0.000	0.000	0.002	0.002
274:00:00	0.000	0.000	0.000	0.000	0.002	0.002
275:00:00	0.000	0.000	0.000	0.000	0.002	0.002
276:00:00	0.000	0.000	0.000	0.000	0.002	0.002
277:00:00	0.000	0.000	0.000	0.000	0.002	0.002
278:00:00	0.000	0.000	0.000	0.000	0.002	0.002
279:00:00	0.000	0.000	0.000	0.000	0.002	0.002
280:00:00	0.000	0.000	0.000	0.000	0.002	0.002
281:00:00	0.000	0.000	0.000	0.000	0.002	0.002
282:00:00	0.000	0.000	0.000	0.000	0.002	0.002
283:00:00	0.000	0.000	0.000	0.000	0.002	0.002
284:00:00	0.000	0.000	0.000	0.000	0.002	0.002
285:00:00	0.000	0.000	0.000	0.000	0.002	0.002
286:00:00	0.000	0.000	0.000	0.000	0.002	0.002

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
287:00:00	0.000	0.000	0.000	0.000	0.002	0.002
288:00:00	0.000	0.000	0.000	0.000	0.002	0.002
289:00:00	0.000	0.000	0.000	0.000	0.002	0.002
290:00:00	0.000	0.000	0.000	0.000	0.002	0.002
291:00:00	0.000	0.000	0.000	0.000	0.002	0.002
292:00:00	0.000	0.000	0.000	0.000	0.002	0.002
293:00:00	0.000	0.000	0.000	0.000	0.002	0.002
294:00:00	0.000	0.000	0.000	0.000	0.002	0.002
295:00:00	0.000	0.000	0.000	0.000	0.002	0.002
296:00:00	0.000	0.000	0.000	0.000	0.002	0.002
297:00:00	0.000	0.000	0.000	0.000	0.002	0.002
298:00:00	0.000	0.000	0.000	0.000	0.002	0.002
299:00:00	0.000	0.000	0.000	0.000	0.002	0.002
300:00:00	0.000	0.000	0.000	0.000	0.002	0.002
301:00:00	0.000	0.000	0.000	0.000	0.002	0.002
302:00:00	0.000	0.000	0.000	0.000	0.001	0.001
303:00:00	0.000	0.000	0.000	0.000	0.001	0.001
304:00:00	0.000	0.000	0.000	0.000	0.001	0.001
305:00:00	0.000	0.000	0.000	0.000	0.001	0.001
306:00:00	0.000	0.000	0.000	0.000	0.001	0.001
307:00:00	0.000	0.000	0.000	0.000	0.001	0.001
308:00:00	0.000	0.000	0.000	0.000	0.001	0.001
309:00:00	0.000	0.000	0.000	0.000	0.001	0.001
310:00:00	0.000	0.000	0.000	0.000	0.001	0.001
311:00:00	0.000	0.000	0.000	0.000	0.001	0.001
312:00:00	0.000	0.000	0.000	0.000	0.001	0.001
313:00:00	0.000	0.000	0.000	0.000	0.001	0.001
314:00:00	0.000	0.000	0.000	0.000	0.001	0.001
315:00:00	0.000	0.000	0.000	0.000	0.001	0.001
316:00:00	0.000	0.000	0.000	0.000	0.001	0.001
317:00:00	0.000	0.000	0.000	0.000	0.001	0.001
318:00:00	0.000	0.000	0.000	0.000	0.001	0.001
319:00:00	0.000	0.000	0.000	0.000	0.001	0.001
320:00:00	0.000	0.000	0.000	0.000	0.001	0.001
321:00:00	0.000	0.000	0.000	0.000	0.001	0.001
322:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
323:00:00	0.000	0.000	0.000	0.000	0.001	0.001
324:00:00	0.000	0.000	0.000	0.000	0.001	0.001
325:00:00	0.000	0.000	0.000	0.000	0.001	0.001
326:00:00	0.000	0.000	0.000	0.000	0.001	0.001
327:00:00	0.000	0.000	0.000	0.000	0.001	0.001
328:00:00	0.000	0.000	0.000	0.000	0.001	0.001
329:00:00	0.000	0.000	0.000	0.000	0.001	0.001
330:00:00	0.000	0.000	0.000	0.000	0.001	0.001
331:00:00	0.000	0.000	0.000	0.000	0.001	0.001
332:00:00	0.000	0.000	0.000	0.000	0.001	0.001
333:00:00	0.000	0.000	0.000	0.000	0.001	0.001
334:00:00	0.000	0.000	0.000	0.000	0.001	0.001
335:00:00	0.000	0.000	0.000	0.000	0.001	0.001
336:00:00	0.000	0.000	0.000	0.000	0.001	0.001
337:00:00	0.000	0.000	0.000	0.000	0.001	0.001
338:00:00	0.000	0.000	0.000	0.000	0.001	0.001
339:00:00	0.000	0.000	0.000	0.000	0.001	0.001
340:00:00	0.000	0.000	0.000	0.000	0.001	0.001
341:00:00	0.000	0.000	0.000	0.000	0.001	0.001
342:00:00	0.000	0.000	0.000	0.000	0.001	0.001
343:00:00	0.000	0.000	0.000	0.000	0.001	0.001
344:00:00	0.000	0.000	0.000	0.000	0.001	0.001
345:00:00	0.000	0.000	0.000	0.000	0.001	0.001
346:00:00	0.000	0.000	0.000	0.000	0.001	0.001
347:00:00	0.000	0.000	0.000	0.000	0.001	0.001
348:00:00	0.000	0.000	0.000	0.000	0.001	0.001
349:00:00	0.000	0.000	0.000	0.000	0.001	0.001
350:00:00	0.000	0.000	0.000	0.000	0.001	0.001
351:00:00	0.000	0.000	0.000	0.000	0.001	0.001
352:00:00	0.000	0.000	0.000	0.000	0.001	0.001
353:00:00	0.000	0.000	0.000	0.000	0.001	0.001
354:00:00	0.000	0.000	0.000	0.000	0.001	0.001
355:00:00	0.000	0.000	0.000	0.000	0.001	0.001
356:00:00	0.000	0.000	0.000	0.000	0.001	0.001
357:00:00	0.000	0.000	0.000	0.000	0.001	0.001
358:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
359:00:00	0.000	0.000	0.000	0.000	0.001	0.001
360:00:00	0.000	0.000	0.000	0.000	0.001	0.001
361:00:00	0.000	0.000	0.000	0.000	0.001	0.001
362:00:00	0.000	0.000	0.000	0.000	0.001	0.001
363:00:00	0.000	0.000	0.000	0.000	0.001	0.001
364:00:00	0.000	0.000	0.000	0.000	0.001	0.001
365:00:00	0.000	0.000	0.000	0.000	0.001	0.001
366:00:00	0.000	0.000	0.000	0.000	0.001	0.001
367:00:00	0.000	0.000	0.000	0.000	0.001	0.001
368:00:00	0.000	0.000	0.000	0.000	0.001	0.001
369:00:00	0.000	0.000	0.000	0.000	0.001	0.001
370:00:00	0.000	0.000	0.000	0.000	0.001	0.001
371:00:00	0.000	0.000	0.000	0.000	0.001	0.001
372:00:00	0.000	0.000	0.000	0.000	0.000	0.000
373:00:00	0.000	0.000	0.000	0.000	0.000	0.000
374:00:00	0.000	0.000	0.000	0.000	0.000	0.000
375:00:00	0.000	0.000	0.000	0.000	0.000	0.000
376:00:00	0.000	0.000	0.000	0.000	0.000	0.000
377:00:00	0.000	0.000	0.000	0.000	0.000	0.000
378:00:00	0.000	0.000	0.000	0.000	0.000	0.000
379:00:00	0.000	0.000	0.000	0.000	0.000	0.000
380:00:00	0.000	0.000	0.000	0.000	0.000	0.000
381:00:00	0.000	0.000	0.000	0.000	0.000	0.000
382:00:00	0.000	0.000	0.000	0.000	0.000	0.000
383:00:00	0.000	0.000	0.000	0.000	0.000	0.000
384:00:00	0.000	0.000	0.000	0.000	0.000	0.000
385:00:00	0.000	0.000	0.000	0.000	0.000	0.000
386:00:00	0.000	0.000	0.000	0.000	0.000	0.000
387:00:00	0.000	0.000	0.000	0.000	0.000	0.000
388:00:00	0.000	0.000	0.000	0.000	0.000	0.000
389:00:00	0.000	0.000	0.000	0.000	0.000	0.000
390:00:00	0.000	0.000	0.000	0.000	0.000	0.000
391:00:00	0.000	0.000	0.000	0.000	0.000	0.000
392:00:00	0.000	0.000	0.000	0.000	0.000	0.000
393:00:00	0.000	0.000	0.000	0.000	0.000	0.000
394:00:00	0.000	0.000	0.000	0.000	0.000	0.000

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
395:00:00	0.000	0.000	0.000	0.000	0.000	0.000
396:00:00	0.000	0.000	0.000	0.000	0.000	0.000
397:00:00	0.000	0.000	0.000	0.000	0.000	0.000
398:00:00	0.000	0.000	0.000	0.000	0.000	0.000
399:00:00	0.000	0.000	0.000	0.000	0.000	0.000
400:00:00	0.000	0.000	0.000	0.000	0.000	0.000
401:00:00	0.000	0.000	0.000	0.000	0.000	0.000
402:00:00	0.000	0.000	0.000	0.000	0.000	0.000
403:00:00	0.000	0.000	0.000	0.000	0.000	0.000
404:00:00	0.000	0.000	0.000	0.000	0.000	0.000
405:00:00	0.000	0.000	0.000	0.000	0.000	0.000
406:00:00	0.000	0.000	0.000	0.000	0.000	0.000
407:00:00	0.000	0.000	0.000	0.000	0.000	0.000
408:00:00	0.000	0.000	0.000	0.000	0.000	0.000
409:00:00	0.000	0.000	0.000	0.000	0.000	0.000
410:00:00	0.000	0.000	0.000	0.000	0.000	0.000
411:00:00	0.000	0.000	0.000	0.000	0.000	0.000
412:00:00	0.000	0.000	0.000	0.000	0.000	0.000
413:00:00	0.000	0.000	0.000	0.000	0.000	0.000
414:00:00	0.000	0.000	0.000	0.000	0.000	0.000
415:00:00	0.000	0.000	0.000	0.000	0.000	0.000
416:00:00	0.000	0.000	0.000	0.000	0.000	0.000
417:00:00	0.000	0.000	0.000	0.000	0.000	0.000
418:00:00	0.000	0.000	0.000	0.000	0.000	0.000
419:00:00	0.000	0.000	0.000	0.000	0.000	0.000
420:00:00	0.000	0.000	0.000	0.000	0.000	0.000
421:00:00	0.000	0.000	0.000	0.000	0.000	0.000
422:00:00	0.000	0.000	0.000	0.000	0.000	0.000
423:00:00	0.000	0.000	0.000	0.000	0.000	0.000
424:00:00	0.000	0.000	0.000	0.000	0.000	0.000
425:00:00	0.000	0.000	0.000	0.000	0.000	0.000
426:00:00	0.000	0.000	0.000	0.000	0.000	0.000
427:00:00	0.000	0.000	0.000	0.000	0.000	0.000
428:00:00	0.000	0.000	0.000	0.000	0.000	0.000
429:00:00	0.000	0.000	0.000	0.000	0.000	0.000
430:00:00	0.000	0.000	0.000	0.000	0.000	0.000

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Appendix

Catchment descriptors

Name	Value	User-defined value used?
Area (km^2)	0.86	No
ALTBAR	12	No
ASPBAR	0.44	No
ASPVAR	0	No
BFIHOST	0.89	No
DPLBAR (km)	2.27	No
DPSBAR (mkm^{-1})	8.7	No
FARL	1	No
LDP	4.98	No
PROPWET (mm)	0.26	No
RMED1H	11	No
RMED1D	30.2	No
RMED2D	38.6	No
SAAR (mm)	586	No
SAAR4170 (mm)	593	No
SPRHOST	14.52	No
Urbext2000	0.09	No
Urbext1990	0.05	No
URBCONC	0.84	No
URBLOC	1.47	No
DDF parameter C	-0.02	No
DDF parameter D1	0.3	No
DDF parameter D2	0.28	No
DDF parameter D3	0.21	No
DDF parameter E	0.31	No
DDF parameter F	2.51	No
DDF parameter C (1km grid value)	0	No
DDF parameter D1 (1km grid value)	0	No
DDF parameter D2 (1km grid value)	0	No
DDF parameter D3 (1km grid value)	0	No
DDF parameter E (1km grid value)	0	No
DDF parameter F (1km grid value)	0	No

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UK Design Flood Estimation

Generated on 11 May 2021 16:02:04 by AEA_COMPUTER
Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH2)

Site details Checksum: C0D0-3A7A

Site name: tmp674E

Easting: 647550

Northing: 262800

Country: England, Wales or Northern Ireland

Catchment Area (km²): 0.31

Using plot scale calculations: No

Model: ReFH2.2

Site description: None

Model run: 100 year - LEIS_SIZEW4

Summary of results

Rainfall - FEH 2013 model (mm):	121.74	Total runoff (ML):	2.84
Total Rainfall (mm):	81.49	Total flow (ML):	6.88
Peak Rainfall (mm):	1.78	Peak flow (m³/s):	0.02

Parameters

Where the user has overriden a system-generated value, this original value is shown in square brackets after the value used.
** Indicates that the user locked the duration/timestep*

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	121:00:00 [11:00:00]	Yes
Timestep (hh:mm:ss)	01:00:00	No
SCF (Seasonal correction factor)	0.67	No
ARF (Areal reduction factor)	1	No
Seasonality	Winter	No

Loss model parameters

Name	Value	User-defined?
Cini (mm)	60.53	No
Cmax (mm)	1190.38	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No
Use seasonal CIni for equations	No [Yes]	Yes

Routing model parameters

Name	Value	User-defined?
Tp (hr)	7.15	No
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m^3/s)	0	No
BL (hr)	63.92	No
BR	2.16	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km^2)	0.04	No
Urbext 2000	0.09	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Exporting drained area (km^2)	0.00	Yes
Sewer capacity (m^3/s)	0.00	Yes

Time series data

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
00:00:00	0.127	0.000	0.010	0.000	0.000	0.000
01:00:00	0.133	0.000	0.010	0.000	0.000	0.000
02:00:00	0.140	0.000	0.011	0.000	0.000	0.000
03:00:00	0.146	0.000	0.012	0.000	0.000	0.000
04:00:00	0.153	0.000	0.012	0.000	0.000	0.000
05:00:00	0.161	0.000	0.013	0.000	0.000	0.000
06:00:00	0.169	0.000	0.013	0.000	0.000	0.000
07:00:00	0.177	0.000	0.014	0.001	0.000	0.001
08:00:00	0.185	0.000	0.015	0.001	0.000	0.001
09:00:00	0.194	0.000	0.015	0.001	0.000	0.001
10:00:00	0.204	0.000	0.016	0.001	0.000	0.001
11:00:00	0.213	0.000	0.017	0.001	0.000	0.001
12:00:00	0.224	0.000	0.018	0.001	0.000	0.001
13:00:00	0.234	0.000	0.019	0.001	0.000	0.001
14:00:00	0.246	0.000	0.020	0.001	0.000	0.001
15:00:00	0.257	0.000	0.021	0.001	0.000	0.001
16:00:00	0.270	0.000	0.022	0.001	0.000	0.001
17:00:00	0.282	0.000	0.023	0.001	0.000	0.001
18:00:00	0.296	0.000	0.024	0.001	0.000	0.002
19:00:00	0.310	0.000	0.025	0.001	0.000	0.002
20:00:00	0.325	0.000	0.027	0.002	0.000	0.002
21:00:00	0.340	0.000	0.028	0.002	0.000	0.002
22:00:00	0.357	0.000	0.029	0.002	0.000	0.002
23:00:00	0.373	0.000	0.031	0.002	0.000	0.002
24:00:00	0.391	0.000	0.032	0.002	0.000	0.002
25:00:00	0.410	0.000	0.034	0.002	0.000	0.002
26:00:00	0.429	0.000	0.036	0.002	0.000	0.002
27:00:00	0.449	0.000	0.038	0.002	0.000	0.003
28:00:00	0.471	0.000	0.040	0.002	0.000	0.003
29:00:00	0.493	0.000	0.042	0.002	0.000	0.003
30:00:00	0.516	0.000	0.044	0.003	0.001	0.003
31:00:00	0.540	0.000	0.046	0.003	0.001	0.003
32:00:00	0.566	0.000	0.049	0.003	0.001	0.003
33:00:00	0.592	0.000	0.051	0.003	0.001	0.004
34:00:00	0.620	0.000	0.054	0.003	0.001	0.004

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
35:00:00	0.649	0.000	0.057	0.003	0.001	0.004
36:00:00	0.679	0.000	0.060	0.003	0.001	0.004
37:00:00	0.711	0.000	0.063	0.004	0.001	0.004
38:00:00	0.744	0.000	0.066	0.004	0.001	0.005
39:00:00	0.778	0.000	0.070	0.004	0.001	0.005
40:00:00	0.814	0.000	0.074	0.004	0.001	0.005
41:00:00	0.851	0.000	0.078	0.004	0.001	0.005
42:00:00	0.891	0.000	0.082	0.005	0.001	0.006
43:00:00	0.931	0.000	0.086	0.005	0.001	0.006
44:00:00	0.974	0.000	0.091	0.005	0.001	0.006
45:00:00	1.018	0.000	0.096	0.005	0.001	0.007
46:00:00	1.064	0.000	0.101	0.006	0.001	0.007
47:00:00	1.112	0.000	0.106	0.006	0.001	0.008
48:00:00	1.161	0.000	0.112	0.006	0.002	0.008
49:00:00	1.213	0.000	0.118	0.007	0.002	0.008
50:00:00	1.266	0.000	0.125	0.007	0.002	0.009
51:00:00	1.322	0.000	0.132	0.007	0.002	0.009
52:00:00	1.379	0.000	0.139	0.008	0.002	0.010
53:00:00	1.437	0.000	0.146	0.008	0.002	0.010
54:00:00	1.497	0.000	0.154	0.009	0.002	0.011
55:00:00	1.559	0.000	0.163	0.009	0.002	0.012
56:00:00	1.620	0.000	0.171	0.010	0.003	0.012
57:00:00	1.681	0.000	0.180	0.010	0.003	0.013
58:00:00	1.738	0.000	0.188	0.011	0.003	0.014
59:00:00	1.781	0.000	0.195	0.011	0.003	0.014
60:00:00	1.761	0.000	0.196	0.012	0.003	0.015
61:00:00	1.781	0.000	0.200	0.012	0.003	0.016
62:00:00	1.738	0.000	0.198	0.013	0.004	0.017
63:00:00	1.681	0.000	0.194	0.014	0.004	0.017
64:00:00	1.620	0.000	0.189	0.014	0.004	0.018
65:00:00	1.559	0.000	0.184	0.015	0.004	0.019
66:00:00	1.497	0.000	0.178	0.015	0.004	0.019
67:00:00	1.437	0.000	0.173	0.015	0.005	0.020
68:00:00	1.379	0.000	0.167	0.015	0.005	0.020
69:00:00	1.322	0.000	0.162	0.015	0.005	0.021
70:00:00	1.266	0.000	0.156	0.015	0.005	0.021

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
71:00:00	1.213	0.000	0.151	0.015	0.006	0.021
72:00:00	1.161	0.000	0.146	0.015	0.006	0.021
73:00:00	1.112	0.000	0.141	0.015	0.006	0.021
74:00:00	1.064	0.000	0.135	0.015	0.006	0.021
75:00:00	1.018	0.000	0.130	0.015	0.007	0.021
76:00:00	0.974	0.000	0.126	0.014	0.007	0.021
77:00:00	0.931	0.000	0.121	0.014	0.007	0.021
78:00:00	0.891	0.000	0.116	0.014	0.007	0.021
79:00:00	0.851	0.000	0.112	0.013	0.008	0.021
80:00:00	0.814	0.000	0.107	0.013	0.008	0.021
81:00:00	0.778	0.000	0.103	0.013	0.008	0.021
82:00:00	0.744	0.000	0.099	0.012	0.008	0.020
83:00:00	0.711	0.000	0.095	0.012	0.008	0.020
84:00:00	0.679	0.000	0.091	0.011	0.008	0.020
85:00:00	0.649	0.000	0.087	0.011	0.009	0.020
86:00:00	0.620	0.000	0.084	0.011	0.009	0.019
87:00:00	0.592	0.000	0.080	0.010	0.009	0.019
88:00:00	0.566	0.000	0.077	0.010	0.009	0.019
89:00:00	0.540	0.000	0.074	0.009	0.009	0.019
90:00:00	0.516	0.000	0.071	0.009	0.009	0.018
91:00:00	0.493	0.000	0.068	0.009	0.009	0.018
92:00:00	0.471	0.000	0.065	0.008	0.009	0.018
93:00:00	0.449	0.000	0.062	0.008	0.009	0.017
94:00:00	0.429	0.000	0.059	0.008	0.009	0.017
95:00:00	0.410	0.000	0.057	0.007	0.009	0.017
96:00:00	0.391	0.000	0.054	0.007	0.010	0.017
97:00:00	0.373	0.000	0.052	0.007	0.010	0.016
98:00:00	0.357	0.000	0.050	0.007	0.010	0.016
99:00:00	0.340	0.000	0.048	0.006	0.010	0.016
100:00:00	0.325	0.000	0.046	0.006	0.010	0.016
101:00:00	0.310	0.000	0.044	0.006	0.010	0.015
102:00:00	0.296	0.000	0.042	0.006	0.010	0.015
103:00:00	0.282	0.000	0.040	0.005	0.010	0.015
104:00:00	0.270	0.000	0.038	0.005	0.010	0.015
105:00:00	0.257	0.000	0.036	0.005	0.010	0.014
106:00:00	0.246	0.000	0.035	0.005	0.010	0.014

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
107:00:00	0.234	0.000	0.033	0.004	0.009	0.014
108:00:00	0.224	0.000	0.032	0.004	0.009	0.014
109:00:00	0.213	0.000	0.030	0.004	0.009	0.014
110:00:00	0.204	0.000	0.029	0.004	0.009	0.013
111:00:00	0.194	0.000	0.028	0.004	0.009	0.013
112:00:00	0.185	0.000	0.026	0.004	0.009	0.013
113:00:00	0.177	0.000	0.025	0.003	0.009	0.013
114:00:00	0.169	0.000	0.024	0.003	0.009	0.012
115:00:00	0.161	0.000	0.023	0.003	0.009	0.012
116:00:00	0.153	0.000	0.022	0.003	0.009	0.012
117:00:00	0.146	0.000	0.021	0.003	0.009	0.012
118:00:00	0.140	0.000	0.020	0.003	0.009	0.012
119:00:00	0.133	0.000	0.019	0.003	0.009	0.011
120:00:00	0.127	0.000	0.018	0.003	0.009	0.011
121:00:00	0.000	0.000	0.000	0.002	0.009	0.011
122:00:00	0.000	0.000	0.000	0.002	0.009	0.011
123:00:00	0.000	0.000	0.000	0.002	0.009	0.011
124:00:00	0.000	0.000	0.000	0.002	0.008	0.010
125:00:00	0.000	0.000	0.000	0.002	0.008	0.010
126:00:00	0.000	0.000	0.000	0.002	0.008	0.010
127:00:00	0.000	0.000	0.000	0.001	0.008	0.010
128:00:00	0.000	0.000	0.000	0.001	0.008	0.009
129:00:00	0.000	0.000	0.000	0.001	0.008	0.009
130:00:00	0.000	0.000	0.000	0.001	0.008	0.009
131:00:00	0.000	0.000	0.000	0.001	0.008	0.008
132:00:00	0.000	0.000	0.000	0.001	0.008	0.008
133:00:00	0.000	0.000	0.000	0.000	0.008	0.008
134:00:00	0.000	0.000	0.000	0.000	0.008	0.008
135:00:00	0.000	0.000	0.000	0.000	0.007	0.008
136:00:00	0.000	0.000	0.000	0.000	0.007	0.008
137:00:00	0.000	0.000	0.000	0.000	0.007	0.007
138:00:00	0.000	0.000	0.000	0.000	0.007	0.007
139:00:00	0.000	0.000	0.000	0.000	0.007	0.007
140:00:00	0.000	0.000	0.000	0.000	0.007	0.007
141:00:00	0.000	0.000	0.000	0.000	0.007	0.007
142:00:00	0.000	0.000	0.000	0.000	0.007	0.007

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
143:00:00	0.000	0.000	0.000	0.000	0.007	0.007
144:00:00	0.000	0.000	0.000	0.000	0.006	0.006
145:00:00	0.000	0.000	0.000	0.000	0.006	0.006
146:00:00	0.000	0.000	0.000	0.000	0.006	0.006
147:00:00	0.000	0.000	0.000	0.000	0.006	0.006
148:00:00	0.000	0.000	0.000	0.000	0.006	0.006
149:00:00	0.000	0.000	0.000	0.000	0.006	0.006
150:00:00	0.000	0.000	0.000	0.000	0.006	0.006
151:00:00	0.000	0.000	0.000	0.000	0.006	0.006
152:00:00	0.000	0.000	0.000	0.000	0.006	0.006
153:00:00	0.000	0.000	0.000	0.000	0.006	0.006
154:00:00	0.000	0.000	0.000	0.000	0.006	0.006
155:00:00	0.000	0.000	0.000	0.000	0.005	0.005
156:00:00	0.000	0.000	0.000	0.000	0.005	0.005
157:00:00	0.000	0.000	0.000	0.000	0.005	0.005
158:00:00	0.000	0.000	0.000	0.000	0.005	0.005
159:00:00	0.000	0.000	0.000	0.000	0.005	0.005
160:00:00	0.000	0.000	0.000	0.000	0.005	0.005
161:00:00	0.000	0.000	0.000	0.000	0.005	0.005
162:00:00	0.000	0.000	0.000	0.000	0.005	0.005
163:00:00	0.000	0.000	0.000	0.000	0.005	0.005
164:00:00	0.000	0.000	0.000	0.000	0.005	0.005
165:00:00	0.000	0.000	0.000	0.000	0.005	0.005
166:00:00	0.000	0.000	0.000	0.000	0.005	0.005
167:00:00	0.000	0.000	0.000	0.000	0.005	0.005
168:00:00	0.000	0.000	0.000	0.000	0.004	0.004
169:00:00	0.000	0.000	0.000	0.000	0.004	0.004
170:00:00	0.000	0.000	0.000	0.000	0.004	0.004
171:00:00	0.000	0.000	0.000	0.000	0.004	0.004
172:00:00	0.000	0.000	0.000	0.000	0.004	0.004
173:00:00	0.000	0.000	0.000	0.000	0.004	0.004
174:00:00	0.000	0.000	0.000	0.000	0.004	0.004
175:00:00	0.000	0.000	0.000	0.000	0.004	0.004
176:00:00	0.000	0.000	0.000	0.000	0.004	0.004
177:00:00	0.000	0.000	0.000	0.000	0.004	0.004
178:00:00	0.000	0.000	0.000	0.000	0.004	0.004

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
179:00:00	0.000	0.000	0.000	0.000	0.004	0.004
180:00:00	0.000	0.000	0.000	0.000	0.004	0.004
181:00:00	0.000	0.000	0.000	0.000	0.004	0.004
182:00:00	0.000	0.000	0.000	0.000	0.004	0.004
183:00:00	0.000	0.000	0.000	0.000	0.004	0.004
184:00:00	0.000	0.000	0.000	0.000	0.003	0.003
185:00:00	0.000	0.000	0.000	0.000	0.003	0.003
186:00:00	0.000	0.000	0.000	0.000	0.003	0.003
187:00:00	0.000	0.000	0.000	0.000	0.003	0.003
188:00:00	0.000	0.000	0.000	0.000	0.003	0.003
189:00:00	0.000	0.000	0.000	0.000	0.003	0.003
190:00:00	0.000	0.000	0.000	0.000	0.003	0.003
191:00:00	0.000	0.000	0.000	0.000	0.003	0.003
192:00:00	0.000	0.000	0.000	0.000	0.003	0.003
193:00:00	0.000	0.000	0.000	0.000	0.003	0.003
194:00:00	0.000	0.000	0.000	0.000	0.003	0.003
195:00:00	0.000	0.000	0.000	0.000	0.003	0.003
196:00:00	0.000	0.000	0.000	0.000	0.003	0.003
197:00:00	0.000	0.000	0.000	0.000	0.003	0.003
198:00:00	0.000	0.000	0.000	0.000	0.003	0.003
199:00:00	0.000	0.000	0.000	0.000	0.003	0.003
200:00:00	0.000	0.000	0.000	0.000	0.003	0.003
201:00:00	0.000	0.000	0.000	0.000	0.003	0.003
202:00:00	0.000	0.000	0.000	0.000	0.003	0.003
203:00:00	0.000	0.000	0.000	0.000	0.003	0.003
204:00:00	0.000	0.000	0.000	0.000	0.003	0.003
205:00:00	0.000	0.000	0.000	0.000	0.002	0.002
206:00:00	0.000	0.000	0.000	0.000	0.002	0.002
207:00:00	0.000	0.000	0.000	0.000	0.002	0.002
208:00:00	0.000	0.000	0.000	0.000	0.002	0.002
209:00:00	0.000	0.000	0.000	0.000	0.002	0.002
210:00:00	0.000	0.000	0.000	0.000	0.002	0.002
211:00:00	0.000	0.000	0.000	0.000	0.002	0.002
212:00:00	0.000	0.000	0.000	0.000	0.002	0.002
213:00:00	0.000	0.000	0.000	0.000	0.002	0.002
214:00:00	0.000	0.000	0.000	0.000	0.002	0.002

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
215:00:00	0.000	0.000	0.000	0.000	0.002	0.002
216:00:00	0.000	0.000	0.000	0.000	0.002	0.002
217:00:00	0.000	0.000	0.000	0.000	0.002	0.002
218:00:00	0.000	0.000	0.000	0.000	0.002	0.002
219:00:00	0.000	0.000	0.000	0.000	0.002	0.002
220:00:00	0.000	0.000	0.000	0.000	0.002	0.002
221:00:00	0.000	0.000	0.000	0.000	0.002	0.002
222:00:00	0.000	0.000	0.000	0.000	0.002	0.002
223:00:00	0.000	0.000	0.000	0.000	0.002	0.002
224:00:00	0.000	0.000	0.000	0.000	0.002	0.002
225:00:00	0.000	0.000	0.000	0.000	0.002	0.002
226:00:00	0.000	0.000	0.000	0.000	0.002	0.002
227:00:00	0.000	0.000	0.000	0.000	0.002	0.002
228:00:00	0.000	0.000	0.000	0.000	0.002	0.002
229:00:00	0.000	0.000	0.000	0.000	0.002	0.002
230:00:00	0.000	0.000	0.000	0.000	0.002	0.002
231:00:00	0.000	0.000	0.000	0.000	0.002	0.002
232:00:00	0.000	0.000	0.000	0.000	0.002	0.002
233:00:00	0.000	0.000	0.000	0.000	0.002	0.002
234:00:00	0.000	0.000	0.000	0.000	0.002	0.002
235:00:00	0.000	0.000	0.000	0.000	0.002	0.002
236:00:00	0.000	0.000	0.000	0.000	0.002	0.002
237:00:00	0.000	0.000	0.000	0.000	0.002	0.002
238:00:00	0.000	0.000	0.000	0.000	0.001	0.001
239:00:00	0.000	0.000	0.000	0.000	0.001	0.001
240:00:00	0.000	0.000	0.000	0.000	0.001	0.001
241:00:00	0.000	0.000	0.000	0.000	0.001	0.001
242:00:00	0.000	0.000	0.000	0.000	0.001	0.001
243:00:00	0.000	0.000	0.000	0.000	0.001	0.001
244:00:00	0.000	0.000	0.000	0.000	0.001	0.001
245:00:00	0.000	0.000	0.000	0.000	0.001	0.001
246:00:00	0.000	0.000	0.000	0.000	0.001	0.001
247:00:00	0.000	0.000	0.000	0.000	0.001	0.001
248:00:00	0.000	0.000	0.000	0.000	0.001	0.001
249:00:00	0.000	0.000	0.000	0.000	0.001	0.001
250:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
251:00:00	0.000	0.000	0.000	0.000	0.001	0.001
252:00:00	0.000	0.000	0.000	0.000	0.001	0.001
253:00:00	0.000	0.000	0.000	0.000	0.001	0.001
254:00:00	0.000	0.000	0.000	0.000	0.001	0.001
255:00:00	0.000	0.000	0.000	0.000	0.001	0.001
256:00:00	0.000	0.000	0.000	0.000	0.001	0.001
257:00:00	0.000	0.000	0.000	0.000	0.001	0.001
258:00:00	0.000	0.000	0.000	0.000	0.001	0.001
259:00:00	0.000	0.000	0.000	0.000	0.001	0.001
260:00:00	0.000	0.000	0.000	0.000	0.001	0.001
261:00:00	0.000	0.000	0.000	0.000	0.001	0.001
262:00:00	0.000	0.000	0.000	0.000	0.001	0.001
263:00:00	0.000	0.000	0.000	0.000	0.001	0.001
264:00:00	0.000	0.000	0.000	0.000	0.001	0.001
265:00:00	0.000	0.000	0.000	0.000	0.001	0.001
266:00:00	0.000	0.000	0.000	0.000	0.001	0.001
267:00:00	0.000	0.000	0.000	0.000	0.001	0.001
268:00:00	0.000	0.000	0.000	0.000	0.001	0.001
269:00:00	0.000	0.000	0.000	0.000	0.001	0.001
270:00:00	0.000	0.000	0.000	0.000	0.001	0.001
271:00:00	0.000	0.000	0.000	0.000	0.001	0.001
272:00:00	0.000	0.000	0.000	0.000	0.001	0.001
273:00:00	0.000	0.000	0.000	0.000	0.001	0.001
274:00:00	0.000	0.000	0.000	0.000	0.001	0.001
275:00:00	0.000	0.000	0.000	0.000	0.001	0.001
276:00:00	0.000	0.000	0.000	0.000	0.001	0.001
277:00:00	0.000	0.000	0.000	0.000	0.001	0.001
278:00:00	0.000	0.000	0.000	0.000	0.001	0.001
279:00:00	0.000	0.000	0.000	0.000	0.001	0.001
280:00:00	0.000	0.000	0.000	0.000	0.001	0.001
281:00:00	0.000	0.000	0.000	0.000	0.001	0.001
282:00:00	0.000	0.000	0.000	0.000	0.001	0.001
283:00:00	0.000	0.000	0.000	0.000	0.001	0.001
284:00:00	0.000	0.000	0.000	0.000	0.001	0.001
285:00:00	0.000	0.000	0.000	0.000	0.001	0.001
286:00:00	0.000	0.000	0.000	0.000	0.001	0.001

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Time (hh:mm:ss)	Rain (mm)	Sewer Loss (mm)	Net Rain (mm)	Runoff (m^3/s)	Baseflow (m^3/s)	Total Flow (m^3/s)
287:00:00	0.000	0.000	0.000	0.000	0.001	0.001
288:00:00	0.000	0.000	0.000	0.000	0.001	0.001
289:00:00	0.000	0.000	0.000	0.000	0.001	0.001
290:00:00	0.000	0.000	0.000	0.000	0.001	0.001
291:00:00	0.000	0.000	0.000	0.000	0.001	0.001
292:00:00	0.000	0.000	0.000	0.000	0.001	0.001
293:00:00	0.000	0.000	0.000	0.000	0.001	0.001
294:00:00	0.000	0.000	0.000	0.000	0.001	0.001
295:00:00	0.000	0.000	0.000	0.000	0.001	0.001
296:00:00	0.000	0.000	0.000	0.000	0.001	0.001
297:00:00	0.000	0.000	0.000	0.000	0.001	0.001
298:00:00	0.000	0.000	0.000	0.000	0.001	0.001
299:00:00	0.000	0.000	0.000	0.000	0.001	0.001
300:00:00	0.000	0.000	0.000	0.000	0.001	0.001
301:00:00	0.000	0.000	0.000	0.000	0.001	0.001
302:00:00	0.000	0.000	0.000	0.000	0.001	0.001
303:00:00	0.000	0.000	0.000	0.000	0.001	0.001
304:00:00	0.000	0.000	0.000	0.000	0.001	0.001
305:00:00	0.000	0.000	0.000	0.000	0.001	0.001
306:00:00	0.000	0.000	0.000	0.000	0.001	0.001
307:00:00	0.000	0.000	0.000	0.000	0.001	0.001
308:00:00	0.000	0.000	0.000	0.000	0.000	0.000
309:00:00	0.000	0.000	0.000	0.000	0.000	0.000
310:00:00	0.000	0.000	0.000	0.000	0.000	0.000
311:00:00	0.000	0.000	0.000	0.000	0.000	0.000
312:00:00	0.000	0.000	0.000	0.000	0.000	0.000
313:00:00	0.000	0.000	0.000	0.000	0.000	0.000
314:00:00	0.000	0.000	0.000	0.000	0.000	0.000
315:00:00	0.000	0.000	0.000	0.000	0.000	0.000
316:00:00	0.000	0.000	0.000	0.000	0.000	0.000
317:00:00	0.000	0.000	0.000	0.000	0.000	0.000
318:00:00	0.000	0.000	0.000	0.000	0.000	0.000
319:00:00	0.000	0.000	0.000	0.000	0.000	0.000
320:00:00	0.000	0.000	0.000	0.000	0.000	0.000
321:00:00	0.000	0.000	0.000	0.000	0.000	0.000
322:00:00	0.000	0.000	0.000	0.000	0.000	0.000

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Appendix

Catchment descriptors

Name	Value	User-defined value used?
Area (km²)	0.31	No
ALTBAR	12	No
ASPBAR	0.44	No
ASPVAR	0	No
BFIHOST	0.89	No
DPLBAR (km)	2.27	No
DPSBAR (mkm-¹)	8.7	No
FARL	1	No
LDP	4.98	No
PROPWET (mm)	0.26	No
RMED1H	11	No
RMED1D	30.2	No
RMED2D	38.6	No
SAAR (mm)	586	No
SAAR4170 (mm)	593	No
SPRHOST	14.52	No
Urbext2000	0.09	No
Urbext1990	0.05	No
URBCONC	0.84	No
URBLOC	1.47	No
DDF parameter C	-0.02	No
DDF parameter D1	0.3	No
DDF parameter D2	0.28	No
DDF parameter D3	0.21	No
DDF parameter E	0.31	No
DDF parameter F	2.51	No
DDF parameter C (1km grid value)	0	No
DDF parameter D1 (1km grid value)	0	No
DDF parameter D2 (1km grid value)	0	No
DDF parameter D3 (1km grid value)	0	No
DDF parameter E (1km grid value)	0	No
DDF parameter F (1km grid value)	0	No

Printed from the ReFH2 Flood Modelling software package, version 3.1.7439.12207

Following a meeting with Royal Haskoning on the 22nd April 2021 and the associated meeting minutes sent on the 30th April, 3 key points remain for the Environment Agency to action in relation to the fluvial hydrology. These are listed in points 1 to 3 below with a response provided under each heading.

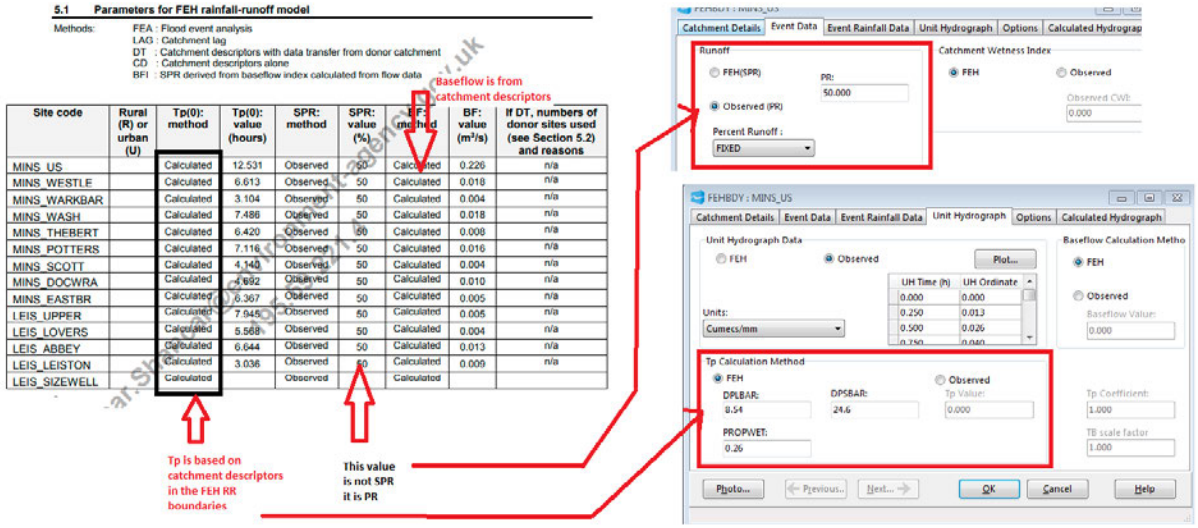
1. EA to provide a summary of the Environment Agency requirements to address and sign off the outstanding hydrological comments

The main outstanding issue is around the derivation of FEH rainfall-runoff parameters. The two key issues are listed below. I have provided the way forward in green text. I think the important thing to note here is that these are not new comments and have been reported in previous comment tracker spreadsheets.

1. Less than the minimum number of events have been used to inform rainfall runoff parameters. 3 events have been used in the study when the FEH Volume 4 states that "*At least five events should be analysed successfully for confidence in the results, the larger the number of events analysed, the greater the reliability of the derived unit hydrograph and losses model parameters* (NERC, 1975, Mawdsley and Tagg, 1981)". The Addendum report does include a qualitative assessment of 3 additional events, these being April 2018, November 2019, and December 2019 and the conclusion is that the hydrograph shape and peak "looks similar" to the other events used in the analysis of percentage runoff. Pointing out similarly in hydrograph shape between the original events and others isn't enough to convince that the parameter estimates are adequate The comment was about the large uncertainty associated with estimating parameters from fewer than the minimum number of events. As a minimum we would want to see 5 events used in the assessment (the additional events shown in the Addendum reporting would be perhaps a sensible choice - April 2018, November 2019, and December 2019). This would add confidence to the estimates. These revised estimates could be compared against those used in the modelling to demonstrate that the conclusions of the FRA would not be affected. In addition, this would add confidence to the estimates for the Nuclear Safety Case.

2. No table with flood event start and end times, antecedent rainfall (AP15), Soil Moisture Deficit (SMD), resulting Catchment Wetness Index (CWI), Percentage Runoff (PR), Dynamic Percentage Runoff (DPR), and Standard Percentage Runoff (SPR) has been provided (5 events minimum as stipulated in the FEH Vol 4) in the Addendum report as requested. Consequently it is difficult to properly scrutinise the calculations. Whilst the FEH calculation record suggests an SPR of 50% has been derived it appears as though SPR has not been calculated and only a fixed PR of 50% has been derived. This has been applied in the FEH RR boundaries as a fixed PR of 50% across all inflow boundaries. The FEH Calculation record erroneously states that SPR for all inflow catchments has been "calculated", that SPR is 50%, and that Time to Peak and Baseflow have been "calculated", this is not the case. Time to Peak and Baseflow appear to be from catchment descriptors, and the SPR value of 50% quoted in the FEH Calculation record is in fact PR (figure 1). This is not good practise. The correct approach would be to calculate SPR using PR, CWI and DPR and then use a donor transfer approach in conjunction with SPRHOST to estimate SPR for all other inflow catchments (e.g. SPRs.adj = SPRs.cds * (SPRg.obs/SPRg.cds)). Worked examples of how to do this and how to present the data are provided in Appendix A of the FEH Volume 4. An example from a modelling study for the River Leen and Day Brook (Black and Veatch, 2011) is also provided (see link below).

Figure 1: Values in the section 5.1 of the FEH calculation record which are not reported correctly. FEH RR parameters from the model hydrology files (ied) are also shown on the right of the image. The FEH calculation record implies that parameters have been calculated when in fact they are based on catchment descriptors or incorrectly quoted in the case of SPR



2. EA to provide example SPR derivation for an urbanised catchment as noted during the meeting

Please find the following link to the River Leen and Day Brook Modelling Study (Black and Veatch, 2011) which provides an example of how SPR has been calculated and how the data has been reported. Further worked examples are also included in Appendix A of the FEH Volume 4. Figure 2.2 of the FEH Volume 4 page 14 also provides a useful flow chart on the approach to parameter estimation based on data availability. When data is available at the subject site the approaches are estimating model parameters from flood event analysis as described in the comments above or to estimate model parameters from catchment LAG and BFI. For donor sites the recommended approach is to use the ratio of observed/estimated model parameters at the donor site to adjust the estimated parameters values at the subject site.

Link to hydrology calculations from the River Leen and Day Brook modelling study (Black and Veatch, 2011):
https://ea.sharefile.com/d-s5785aa00179749c287282d9f91d4149b

3. EA to discuss with internal Environment Agency colleagues data availability / approach in relation to defining the SMD and other parameters related to the derivation of SPR i.e. availability of MORECS or similar data

MORECS and MOSES data are the intellectual property of the Met Office and hence have to be requested from the Met Office for third party work. (https://www.metoffice.gov.uk/services/data/business-data). MORECS data is typically used for the derivation of SMD in studies which have improved the estimate of SMD using the FEH RR approach. The FEH Handbook Volume 4 page 160 states that "*SMD data are available in several forms for different periods. They can be obtained from the Met Office as daily estimated SMDs at synoptic weather stations using a modified Penman model. They can also be obtained as end of week or end of month areal averages over grass for 40km by 40km grid squares from the Met Office Rainfall and Evaporation Calculation System, MORECS which are usually adequate, unless the event is very localised*"

APPENDIX J

FUTURE ADAPTATION OF THE SSSI CROSSING IN THE DCO SUBMISSION

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1 FUTURE ADAPTATION OF THE SSSI CROSSING IN THE DCO SUBMISSION

1.1 Introduction

1.1.1 This paper summarises the design basis for the SSSI crossing maximum crest height presented in the DCO application (May 2020) and subsequent changes application (January 2021), and provides an update to the design basis, based on work carried out since these submissions.

1.2 Development lifetime

1.2.1 The proposed development would go through a number of phases throughout its lifetime. The proposed timings of each phase are assumed to be as follows:

- 2022: start of construction;
- 2034: end of construction and start of operation;
- 2090: end of operation;
- 2140: interim spent fuel store decommissioned; and
- 2190: theoretical maximum site lifetime.

1.3 Future adaptation

1.3.1 The Description of Development provided in **Volume 3, Chapter 2** of the **Environmental Statement Addendum** [AS-202] sets the minimum and maximum crest heights for the SSSI crossing as shown in Table 1.1.

Table 1.1: Minimum and maximum crest heights for the SSSI crossing

Details	Minimum crest height (mAOD)	Maximum crest height (mAOD)
SSSI crossing	7.3	10.5

1.3.2 The Description of Development provides the following explanation at paragraph 2.4.5:

"The Nuclear Site Licence, which is governed by the Office for Nuclear Regulation (ONR), requires flood risk to also be assessed against 1 in 10,000 and 1 in 100,000 year events for its own purposes. The Main Development Site Flood Risk Assessment … states that … by 2090 the

crest height of the SSSI Crossing is likely to need to be increased to 10.5mAOD."

1.3.3 The potential future adaptation of the SSSI crossing is further considered in **Volume 2**, **Chapter 27** of the **Environmental Statement** (Major Accidents and Disasters) [APP-344] at paragraph 27.5.7:

However, there a number of design measures which will minimise the vulnerability of Sizewell C to MA&D hazards and are also set out within the DCO application. These include the following (but exclude safety features that form part of standard UK EPR™ design):

- *Specification of a minimum platform and SSSI crossing height at 7.3m Above Ordnance Datum (AOD), which would reduce the risk of the main platform and access to it from being flooded. This has been set above the still water level for 1 in 1,000-year return period events for the theoretical maximum lifetime of Sizewell C with an allowance for sea level rise with climate change (refer to Main Development Site Flood Risk Assessment (Doc Ref. 5.2) for further information). An adaptive design for the SSSI crossing to enable future raising from 7.3m AOD to 10.5m AOD to reduce the risk of overtopping.*

1.3.4 For clarity, setting of the platform height is based on the extreme still seawater level associated with a 1 in 10,000 year return period and considering reasonably foreseeable climate change up to 2110.

1.3.5 The Main Development Site Flood Risk Assessment (MDS FRA) [APP-093] identified a coastal overtopping risk on the SSSI crossing for the 1 in 10,000-year event towards the end of operation and overall concluded coastal overtopping risk as follows:

"8.1.18 For the 2140 climate change epoch with the crossing embankment crest at 7.3m AOD the overtopping rate for the 1 in 200-year event is below the safe for vehicle operation threshold of 5l/m/s (Ref 1.49).

8.1.19 However, the overtopping rates for the 2140 epoch with the crossing embankment at 7.3m AOD are above the safe for vehicle operation threshold for the 1 in 1,000-year and 1 in 10,000-year events.

8.1.20 With the SSSI crossing adaptive defence crest at 10.5m AOD there would be no risk of overtopping for the 1 in 200-year and 1 in 1,000-year events.

8.1.21 With the adaptive defence crest at 10.5m AOD, the overtopping rates in the 1 in 10,000-year event the overtopping rates are below the safe for vehicle operation threshold allowing safe access and egress."

2 SSSI CROSSING ADAPTATION STRATEGY REVIEW

2.1 Introduction

2.1.1 In response to continued stakeholder concerns that the proposed accepted change design could adversely affect the movement of invertebrates and fish within Leiston drain, SZC Co. commissioned a design review to identify opportunities to optimise the design to further reduce environmental impact.

2.1.2 As part of this design review, SZC Co. has revisited the adaptation strategy in the context of the external hazards safety case, flood risk and planning policy. These aspects are considered further within sections 2.2 and 2.3.

2.2 External hazards safety case

2.2.1 Prior to the submission of the DCO application, SZC Co. began developing the external hazards assessment needed to support the Nuclear Site Licence application to the Office for Nuclear Regulation (ONR). Since the DCO application was submitted in May 2020, SZC Co. has continued to develop the safety case alongside the design development, including the design evolution of the SSSI crossing.

2.2.2 Sizewell C's external hazards safety case demonstrates that the 'safe shutdown state' can be achieved with no reliance on external structures, equipment or personnel. In the case of a 1:10,000-year design basis coastal flooding event under reasonably foreseeable climate change, this is achieved through on-site protection measures such as the site elevation, sea defences and surface water drainage system.

2.2.3 The nuclear plant would be autonomous and therefore would operate or be placed in a safe shutdown state for a prolonged period in the event of a severe environmental event.

2.2.4 As such the external hazards safety case makes no claim on the proposed SSSI crossing to be capable of being adapted (e.g. raised) in future to reduce overtopping rates in response to actual climate change.

2.2.5 Based on the above external hazards safety case, the SSSI crossing is classified as a non-safety critical element. As such, in line with the guidance set out in the ONR / Environment Agency Joint Advice Note (Ref. 2), it has been designed taking into consideration the 1 in 1,000 year with reasonably

foreseeable climate change allowances such that there is a safe means of access and egress up to and including this event, throughout the lifetime of the development. This is in line with the guidance set out within Appendix D of the Joint Advice Note (Ref. 2).

2.3 Planning

a) Policies and guidance

i. Overarching National Policy Statement (NPS) for Energy EN-1

2.3.1 NPS EN-1 section 5.7 requires applicants to submit a flood risk assessment (FRA) if their proposal lies within Flood Zones 2 or 3 or is more than one hectare in size and located in Flood Zone 1. Consequently, a FRA has been prepared for the Sizewell C Project.

2.3.2 Section 5.7 sets out the minimum requirements for FRAs. Decision makers are required to be satisfied that, where relevant:

- the application is supported by an appropriate FRA;
- the Sequential Test has been applied as part of site selection;
- a sequential approach has been applied at the site level to minimise risk by directing the most vulnerable uses to areas of lowest flood risk;
- the proposal is in line with any relevant national and local flood risk management strategy;
- priority has been given to the use of SuDS;
- in flood risk areas the project is appropriately flood resilient and resistant;
- safe access and escape routes are included where required; and
- residual risk can be safely managed over the lifetime of the development.

ii. National Planning Policy Framework

2.3.3 The National Planning Policy Framework (NPPF) states that "the development should be made safe for its lifetime without increasing flood risk elsewhere". For a development to be considered acceptable with regards to flood risk, the sequential test requirements must be satisfied, along with demonstrating the development meets the following criteria:

- within the site, the most vulnerable development is located in areas of lowest flood risk, unless there are overriding reasons to prefer a different location;
- it is appropriately flood resistant and resilient;
- it incorporates sustainable drainage systems, unless there is clear evidence that this would be inappropriate;
- any residual risk can be safely managed; and
- safe access and escape routes are included where appropriate, as part of an agreed emergency plan.

iii. ADEPT / Environment Agency guidance

2.3.4 Safe access and escape in the event of flooding has been subsequently defined in joint ADEPT/EA guidance (2019) [Ref. 1] as follows:

"Safe access and escape can be achieved through the provision of appropriate access and escape routes in conjunction with flood warnings. Specific measures include:

• access routes should allow occupants to safely access and exit the development in design flood conditions for all types of flooding, with an appropriate allowance for climate change

• vehicular access to allow the emergency services to safely reach the development during design flood conditions (with an appropriate allowance for climate change) will also normally be required

• wherever possible, access routes should be located above design flood levels (with an appropriate allowance for climate change) and should avoid overland flow and exceedance pathways

• where routes can't be designed to be dry and access is required through limited flood depths, signage should be provided

• evacuation triggers should be prior to the development flooding, wherever practical

• pedestrian routes should not be subject to any combination of depth and velocity that would result in a flood hazard rating of 0.75 ('danger for some') or greater. Flood water can be difficult to walk through and can hide physical hazards like drain covers, open manholes and kerbstones

• vehicular routes, including for some emergency services vehicles, should not exceed 30cm (12 inches) – less if water is fast flowing - as vehicles can become buoyant and could be swept away in flood conditions. The public should not be expected to drive vehicles through flood waters as part of an EP

• some emergency services vehicles may be able to cope with slightly greater depths, but site-specific advice from the emergency services should be sought to confirm this

• routes which are subject to a flood hazard rating of more than 2.0 ('danger for all') would be unsuitable for the emergency services"

2.3.5 For the evaluation of the flood risk at the SSSI crossing SZC Co. has applied the EurOtop overtopping thresholds as a proxy for flood hazard ratings. Specifically, the safe overtopping thresholds for pedestrians and vehicles have been taken as 1l/s/m and 5l/s/m, respectively.

2.3.6 The results of the overtopping analyses in the MDS FRA [APP-093] are presented in Table 2.1 and evaluated below for the construction, operation, spent fuel storage and nuclear decommissioning, and site decommissioning phases:

Table 2.1: Modelled mean coastal overtopping rates for the SSSI crossing

Return period (years)	Epoch – climate change scenario	Defence crest (m AOD)	Water level (m AOD)	Inshore wave height (Hs, m)	Mean overtopping rates (l/s/m)
1 in 200	2110 – 95% Medium Emissions (UKCP09)	7.3	3.92	3.21	0.01
	2140 – RCP8.5 (UKCP18)	7.3	5.00	3.73	3.72
	2190 – RCP8.5 (UKCP18)	7.3	5.83	4.03	37.01
1 in 1,000	2090 – RCP8.5 (UKCP18)	7.3	4.94	3.73	2.95
	2140 – RCP8.5 (UKCP18)	7.3	5.84	3.94	36.04

	2190 – RCP8.5 (UKCP18)	7.3	6.67	4.08	216.54

b) Construction phase (2022-2034)

2.3.7 The MDS FRA concluded that there is safe access / egress during construction in respect of 200- and 1,000-year storm events.

2.3.8 The Flood Risk Emergency Plan (FREP) [AS-170] submitted as part of the MDS FRA Addendum sets out the plan for addressing the precautionary safety of the construction workforce in respect of residual risk, although no such residual risk has been identified for the SSSI crossing during construction.

c) Operational phase (2030-2090)

2.3.9 The MDS FRA [APP-093] concluded that by 2090 the crest height of the SSSI crossing would need to be raised above 7.3m AOD, to maintain safe access and egress during a 1,000 year coastal event with allowance for reasonably foreseeable climate change.

2.3.10 Specifically, flood modelling indicates that overtopping along the SSSI crossing could potentially become a risk to pedestrians by 2090.

d) Spent fuel storage and nuclear decommissioning phase (2090-2140)

2.3.11 The MDS FRA [APP-093] concluded that that overtopping along the SSSI crossing could potentially become a risk to both pedestrians and vehicles by 2140, in respect of safe access and egress during a 1,000-year coastal event with allowance for reasonably foreseeable climate change.

e) Site decommissioning phase (2140-2190)

2.3.12 The MDS FRA concluded that overtopping rates during both 200- and 1,000-year events would exceed the EurOtop overtopping thresholds with reference to the safety of both pedestrians and vehicles.

2.3.13 After 2140 the activities on site would be related to the final non-nuclear decommissioning requirements, which would be subject to a separate and subsequent planning application. This would consider the continued need or otherwise for the SSSI crossing.

2.3.14 The site would not be required to be permanently occupied and would serve no critical function in respect of the previous energy generation at this

location. All site activities would therefore be conventional demolition and deconstruction in nature using the relevant industry standards at that time, for example relating to the final removal of buildings and reinstatement of ground conditions. Since the occupation of the site would be non-essential, the access to the site would be managed through operational systems that would prevent access from any workforce prior to and during a storm event.

2.3.15 The residual flood risk due to wave overtopping would be managed on the main platform through on and offsite administrative procedures such as site management controls, warning system and weather forecasting. A weather monitoring system would be in place to monitor extreme sea level and storm conditions and, if necessary, deconstruction would need to be halted and the site temporarily evacuated.

2.3.16 Consequently, no claim is made on the SSSI crossing to maintain accessibility during 200- and 1,000-year events after 2140.

2.4 Revised adaptive design strategy

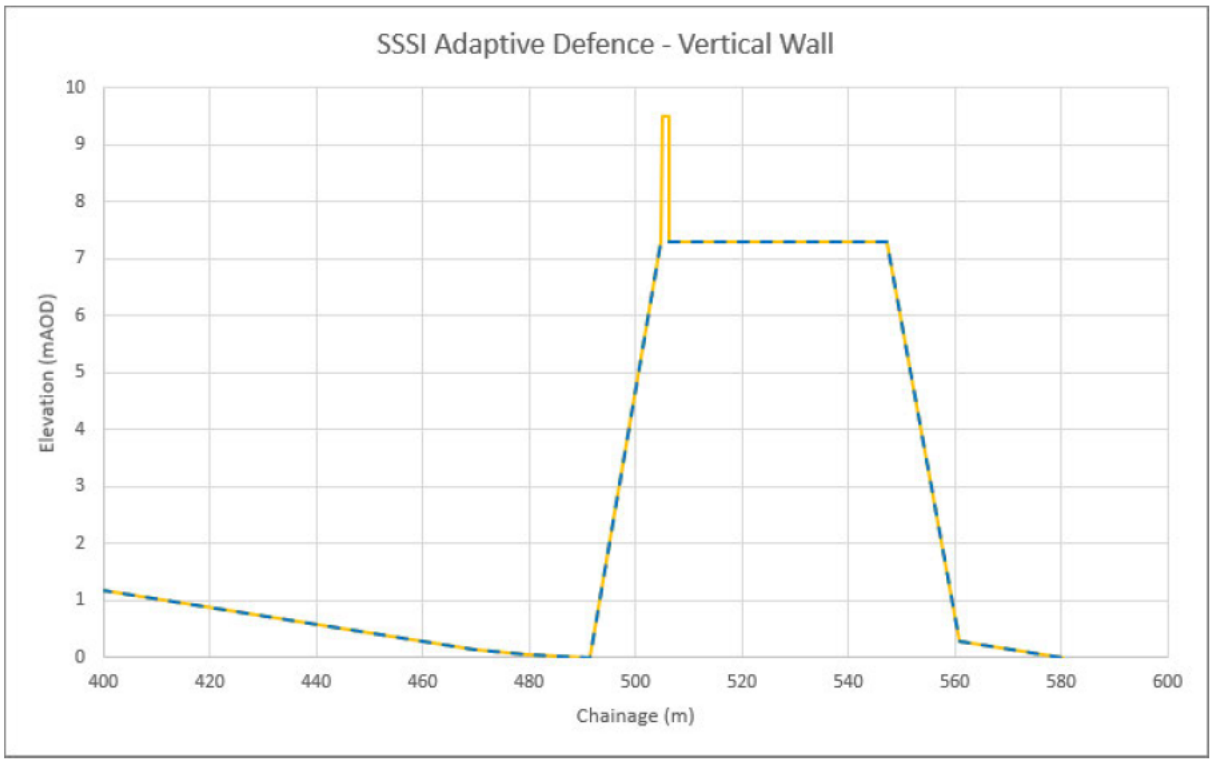
2.4.1 To address the need to enable safe access and egress up to 2140, the following minimum crest levels (Table 2.2) have been established through evaluation of coastal overtopping rates.

2.4.2 A comparative assessment of raised embankment and vertical wave wall type designs was undertaken. This work concluded that the vertical wave wall design (Plate 1) was more effective in wave reflection and consequently could be built to a lower crest level.

Table 2.2: Modelled mean coastal overtopping rates for the SSSI crossing

Return Period	Profile	Defence Crest (mAOD)	Epoch	Climate Change Scenario	Water Level (mODN)	Inshore Wave height (Hs, m)	Mean Overtopping Rate (l/s/m)
1,000 year	SSSI-VW	7.8	2090	RCP8.5 95%-ile	4.94	3.73	0.8
1,000 year	SSSI-VW	8.6	2140	RCP8.5 95%-ile	5.84	3.94	1

Plate 1: SSSI crossing adaptive defence concept (vertical wall)



2.4.3 In order to maintain safe access for pedestrians and vehicles, the results provided in Table 2.2 indicate a need to raise the adaptive defence to 7.8m AOD by 2090 and to 8.6m AOD by 2140. Consequently, a design for the SSSI crossing that provides a minimum crest height of 8.6m AOD from the outset provides safe passage for pedestrians and vehicles up to 2140.

2.4.4 The impacts of climate change and the associated changes in the sea levels would be monitored and assessed at set intervals (minimum 10 years) throughout the operational and decommissioning lifetime, to determine the trajectory of the projections and consider whether there is any change from currently considered projections.

2.4.5 Based on the analysis set out above, egress and access to Sizewell C will be maintained during all phases of the project via the SSSI crossing in the unlikely event the Emergency Plan arrangements are implemented.

REFERENCES

1. Environment Agency and Association of Directors of Environment, Economy, Planning & Transport (ADEPT). September 2019. Flood risk emergency plans for new development – A guide for planners: How to consider emergency plans for flooding as part of the planning process. September 2019.

2. ONR / Environment Agency. July 2017. Joint Advice Note on Principles for Flood and Coastal Erosion Risk Management. Version 1.

APPENDIX K

SUPPLEMENTARY RESPONSE TO NATURAL ENGLAND'S WRITTEN REPRESENTATIONS

CONTENTS

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1 OVERVIEW OF NATURAL ENGLAND'S COMMENTS

1.1 Context

1.1.15 This section has been prepared to address fish related comments raised within Issue 22 and Issue 30 of Part II of Natural England's Written Representation [REP2-153] that were not addressed at Deadline 3. For each issue the following section provides a summary of Natural England's (NE) comment and SZC Co.'s response to avoid the need to refer to the Written Representation [REP2-153]. However, where the comment provided by Natural England is extensive, cross references to the appropriate section of the Written Representation [REP2-153] are provided.

1.1.16 The focus of the comments and responses detailed below relate to the application of the relevant population units or stock areas used as a comparator against which impingement losses are compared. This represents a point of difference between NE assertions and the Applicant's approach. The Applicant considers International Council for Exploration of the Sea (ICES) stock areas to be the most robust, peer reviewed application of the evidence for determining population units for commercially harvested data-rich species. Where such evidence is available the Applicant refers to the high authority of ICES. No alternative approaches to ICES have been proposed at Sizewell. However, Natural England registers its support of Alternative Approaches proposed by the Environment Agency at Hinkley Point. In the Applicant's view the alternative area approach proposed at Hinkley is flawed as described in Section 1.2 iv. Alternative stock areas.

1.1.17 It is noteworthy that the Marine Management Organisation (MMO) in their Deadline 2 Submission to the Planning Inspectorate determined at paragraph 2.4.7 [REP2-140] (emphasis added):

"In relation to the scale of assessment, the MMO notes that the Applicant continues to justify the use of the International Council for Exploration of the Sea ("ICES") stock areas as using the best available evidence. The MMO concludes that the use of ICES stock areas for commercial fish species represents the current best scientific evidence available. There is currently no robust information that would support use of more local stock areas in the assessment. The percentage impact on a stock increases in proportion to the decrease in stock area/size used (the stock area/size is the denominator in the impact calculation). Thus, a ten-fold reduction in the stock area/size used results in a 10-fold increase in estimate impact."

1.1.18 Further that in the MMO in their Deadline 2 Submission to the Planning Inspectorate determined at paragraph 3.2.7 [REP2-140]:

"Notwithstanding these uncertainties [LVSE and FRR mitigation effectiveness]*, the entrapment estimates indicate that even in the absence of LVSE and FRR mitigation measures, only 4 species exceed the 1% threshold: bass, for which density adjustment substantially reduces assessment of impact; sand goby, for which mortality rate >1% Spawning Stock Biomass (SSB) is not a concern at population level; thin-lipped mullet, for which value is an artefact of the low level of landings and absence of SSB; and eel, for which the applied Equivalent Adult Value (EAV) of 1 is unrealistically high, and is a species most likely to benefit from the FRR. On this basis, the MMO consider there is a good level of confidence that actual impacts to all fish species will not be significant. Therefore, the MMO support the conclusions of the ES."*

1.2 Fisheries – use of ICES management units as a population baseline (Part II, issue 22)

a) Natural England comment

1.2.27 Natural England raise concerns over impacts of entrapment being *"contextualised against large ICES SSB as a proxy for population estimates"* noting that the *"exclusive use of ICES management units does not utilise best available evidence, and so risks underestimation of the fish entrapment impact"*. Whilst in acknowledgement of the differences between Sizewell and Bridgwater Bay, Natural England align their position with that taken by the Environment Agency during the Hinkley Point Inquiry.

1.2.28 Further, Natural England advise that finer population structure and highly localised behaviours is not taken into account when the following species are assessed against ICES stock units:

- Cod (*Gadus morhua*);
- Whiting (*Merlangius merlangus*);
- Seabass (*Dicentrarchus labrax*);
- Herring (*Clupea harengus*), and;
- Plaice (*Pleuronectes platessa*).

1.2.29 Natural England are critical of the Applicant's use of ICES management units suggesting inertia in the ICES process limits the ability for the latest evidence to be incorporated.

1.2.30 Natural England consider the Applicant's comparison of the station impacts as a form of fish harvesting as being imperfect due to the inability for adaptive management throughout the operational life-time of the station.

1.2.31 Natural England indicate that the *"uncertainty contained within the assessment risks adverse environmental outcomes"* that may be masked by other anthropogenic or environmental factors. Natural England state that uncertainty in fisheries management should be managed by *"robust, adaptive and precautionary"* approaches.

1.2.32 These comments are detailed in full at Part II Issue 22 [REP2-153] and reiterated in Part II Issue 30. Responses are provided here.

b) The Applicant's Response

1.2.33 The Applicant notes Natural England's position and that relevant scale of assessment for impacts on fish populations has been a point of difference throughout the consultation period. Responses to the above concerns are structured to consider firstly the robustness and applicability of ICES advice and how adaptable ICES is to emerging evidence. The species of concern are then considered individually before the existence of evidence to support smaller population units at Sizewell is considered.

1.2.34 In addition to the assessment of effects of the station in relation to the population, the Applicant has also produced a local effects assessment which provides a framework for determining localised depletion to abstraction (BEEMS Scientific Position Paper SPP103 part of the ES Addendum [AS-238]). This assessment was borne following requests from statutory stakeholders and allows questions regarding depletion of prey resources within the Greater Sizewell Bay to be addressed. A revised local effects assessment, addressing further comments, will be provided at Deadline 6 (SPP103.v5).

iii. ICES stock areas

1.2.35 Before considering the robustness of the ICES approach and suitability of the population units for determining the impacts of entrapment at Sizewell, it is worth taking note of what the impingement assessments are trying to achieve and the connection between fishes in the Greater Sizewell Bay and their wider populations.

1.2.36 The impingement of fish at Sizewell B varies seasonally and for most species is comprised predominantly of juvenile stages. As such, impingement at Sizewell reflects processes of recruitment to, and migration to and from, the Greater Sizewell Bay. To account for these processes, losses of impinged fish are represented in terms of adult equivalents.

1.2.37 The young fish impinged at Sizewell are overwhelmingly the progeny of adult fishes that have spawned elsewhere, and predominantly offshore. The proportion of eggs that hatch into larvae, and of larvae that survive to become juveniles in inshore waters, will vary considerably from year to year. Larval recruitment is driven by meteorological, oceanographic and ecological processes whereby the direction and strength of currents, temperature, growth rate, food supply, and consumption of eggs and larvae by predators will determine survival and hence the numbers of young fish joining the population each year. Variability in these factors mean the locations and numbers of young fish reaching coastal areas varies year to year. In any given year, the number of young fish in the Southern North Sea, and ultimately the proportion of these in Greater Sizewell Bay, will be driven by two main factors. First, the total fertile egg production of the spawning population. Second, the survival and distribution of eggs and larvae as they develop and drift towards the coast. Spawning population size is used as a simple but approximate measure of total egg production.

1.2.38 As the larvae begin the transformation into juveniles, they more actively seek suitable nursery habitats. Cod and whiting for example use many nursery areas across the North Sea, whereas juvenile sea bass utilise the coastal fringe, and especially estuaries and saltmarshes. The impingement of fish in the coastal waters of Sizewell is therefore driven by recruitment of larvae, utilisation of inshore nursery areas by juvenile life stages and, for older fish, by their seasonal migratory movements.

1.2.39 Natural England point to “highly localised behaviours” in some species. Indeed, in species such as seabass seasonal site fidelity can be observed. However, focusing on a single life-history stage disregards the essential connection between the fish impinged at Sizewell and the wider mixing, migrations and life histories of the populations that may enter the Greater Sizewell Bay.

1.2.40 The young fish that recruit to coastal areas including the Greater Sizewell Bay are not consistently connected to the same subset of spawning adults. Following spawning eggs may be carried passively for 10s or 100s of km over 30 days or more. The eggs and larvae will intermingle in different ways in different seasons and years, and consistent spatial differentiation between larvae from different individuals or groups within the same spawning population will not be consistently maintained. This is expected to be the case even if there is structuring and separation among individuals and groups in the spawning aggregations.

1.2.41 Therefore, when determining the relevant population to contextualise impacts it is essential to consider the full life history of the fishes. This is consistent with the ICES approach that considers the population identity

over the full life cycle and compatible with the equivalent adult methodologies.

1.2.42 Stock assessments conducted by ICES represent the consensus of experts, working within an international process. In determining the relevant stock units, ICES assesses all the available evidence across the entire life-history of the species of concern. The ICES approach is a multistage international process with internal and external peer review that brings together experts in fish biology. Methods of assessments of each stock and its structure is considered by dedicated international working groups. Meeting every 3-5 years at so-called 'Benchmarks' all the new evidence on the species ecology and distribution is taken into account. The ICES Benchmark process is in addition to annual assessments and evaluates current assessments and data methodologies and proposes improvements. The benchmark includes experts and stakeholders from outside the ICES community to broaden expertise and data pools to improve assessment quality and enhance credibility. The need and timing of particular benchmarks is decided by the working group involved in assessment of the stock. This decision is generally based on the amount of new information becoming available to fisheries assessment scientists and assigned by stock coordinators. Owing to the large numbers of scientists involved, from many countries, the process can thoroughly consider the relevance of new sources of information in the context of existing knowledge, rather than in isolation.

1.2.43 Scientific advice is submitted by a working group to ICES, and then reported to stakeholders. Many organisations and countries trust ICES to provide population information, including the European Commission, Iceland, Norway and the UK. The application of ICES advice to determine, for example, recommended stock-specific total allowable catch (TAC) into individually set TACs of particular countries is a relatively complicated process described in a publication cited by Natural England (Schuch *et al.,* 2021) [1].

1.2.44 Migratory behaviour, mixing on spawning grounds and patterns of larval dispersal and recruitment processes all factor into determining the most appropriate population or stock unit. In most cases the ICES stock units encompass the full biological elements of the population. However, there are occasions, such as horse mackerel (see below), where the biology of the species is not contained within the single management unit.

[1] Schuch *et al.*, (2021) Institutional inertia in European fisheries – Insights from the Atlantic horse mackerel case. Marine Policy; **128**, 104464.

ii. Natural England concerns with application of most current evidence

1.2.45 Natural England indicate that the ICES approach summarised in BEEMS Technical Report TR406.v7 [Section 4.10.2 of AS-238] is an oversimplification of the processes and procedures used to change ICES SSB definitions. Natural England point to the work of Schuch *et al.,* (2021) as an example of the inertia in the ICES process, using horse mackerel as a case study, limiting the ability of the Applicant to apply the latest evidence to derive more accurate population estimates if ICES units are applied, however, the Applicant feels Natural England have misinterpreted this study.

1.2.46 ICES provides the scientific advice to inform policy on fisheries management and quota allocations for horse mackerel of the North Sea stock, which is a seasonally mobile population. In Q1 and Q2 horse mackerel occurs in Divisions 3.a and 4.a (Northern North Sea, Kattegat and Skagerrak), and in Q3 and Q4 fish move to Divisions 4.b, 4.c and 7.d (Central and Southern North Sea and eastern English Channel). One of the concerns expressed in Schuch *et al.,* (2021) is not the inability for ICES to apply the latest scientific evidence to define the 'scientific area' appropriate for the assessment of the population or SSB, but the time taken for institutional reaction to implement management measures. Whilst ICES incorporate the most recent scientific evidence on stock structure and population mobility in its advice, it may take years to agree management practices with stakeholders and reallocate total allowable catches (TAC).

1.2.47 In relation to the proposed development, the seasonality of the mobile stock relative to the management units is of little concern. The TAC for horse mackerel stocks of relevance to Sizewell was recently set in 2020 by the ICES Working Group on Widely Distributed Stocks. Sizewell C unmitigated impingement of horse mackerel is predicted to be approximately 0.22t per annum relative to a mean 20,456t per annum fishery (2009-2017). Therefore, it is the Applicant's view that the ICES assessment remains the most appropriate for setting stock units for horse mackerel to compare against the predicted impingement of fish at SZC. Furthermore, concerns about ICES not incorporating the latest evidence are not valid.

iii. Species raised by Natural England

1.2.48 In response to stakeholder concerns during the pre-application process and in response to Relevant Representations, the Applicant outlined their position in relation to Allis and twaite shad, cucumber smelt, sea lamprey, sprat, seabass, sand goby, dab, flounder, thornback ray, and sand eel in

BEEMS Scientific Position Paper SPP103.v4[2]. Natural England have detailed further concerns in relation to the population structure and local behaviour of seabass, cod, whiting, herring and plaice. The following sections consider the biology of these species in more detail.

Plaice

1.2.49 The ICES stock unit for plaice is Division 4 and 3.2 subdivision 20 (North Sea & Skagerrak) (Figure 1). The SSB and landings are available for plaice populations in this stock unit and have been used as a comparator for impingement assessments.

1.2.50 Plaice is a well-studied stock by ICES. The North Sea and Skagerrak population is seasonally mobile. In summer, some plaice come to forage in Skagerrak where they represent a large share of catches in the area. Genetic and tagging studies show plaice from the North Sea & Skagerrak population mix with the western component of a smaller local resident stock (Ulrich *et al.,* 2017; ICES 2020). Some adult plaice from the North Sea & Skagerrak population migrate to the eastern English Channel during Q1 for spawning representing around half of adult fish captured there in this season before returning to the North Sea (Houghton, Harding, 1976; ICES, 2020) (Figure 1).

1.2.51 ICES stock assessments and calculations of TAC take into account this seasonal "infringement" of management borders and respective modelling (two models used) provides a reliable tool for monitoring abundance of this stock - the North Sea plaice, not the plaice in the North Sea. Models use six different seasonal survey indices covering the entire are of the stock distribution and age structure of catches.

1.2.52 Plaice was benchmarked in 2015, 2017, and recently in 2020. In spite of the recent assessment, an accumulation of evidence for further improvement of stock monitoring is underway (ICES 2020). This adaptive approach exemplifies the ability of ICES to account for the latest available evidence as soon as it becomes available.

1.2.53 The use of the North Sea plaice stock as a comparator for losses caused by Sizewell activities is robust because: a) plaice are a widely distributed and mobile stock with the widest distribution of eggs and larvae with oceanic currents; b) there is no evidence of more discrete populations that might be impinged at Sizewell nor any evidence for other stocks that might be impinged there.

[2] An earlier version of BEEMS Scientific Position Paper SPP103 (v3) was submitted as part of the ES Addendum [AS-238].

1.2.54 With FRR mitigation in place, mean annual losses of plaice equate to 0.38t from an SSB of 967,222t. The effects of impingement on plaice is therefore considered negligible.

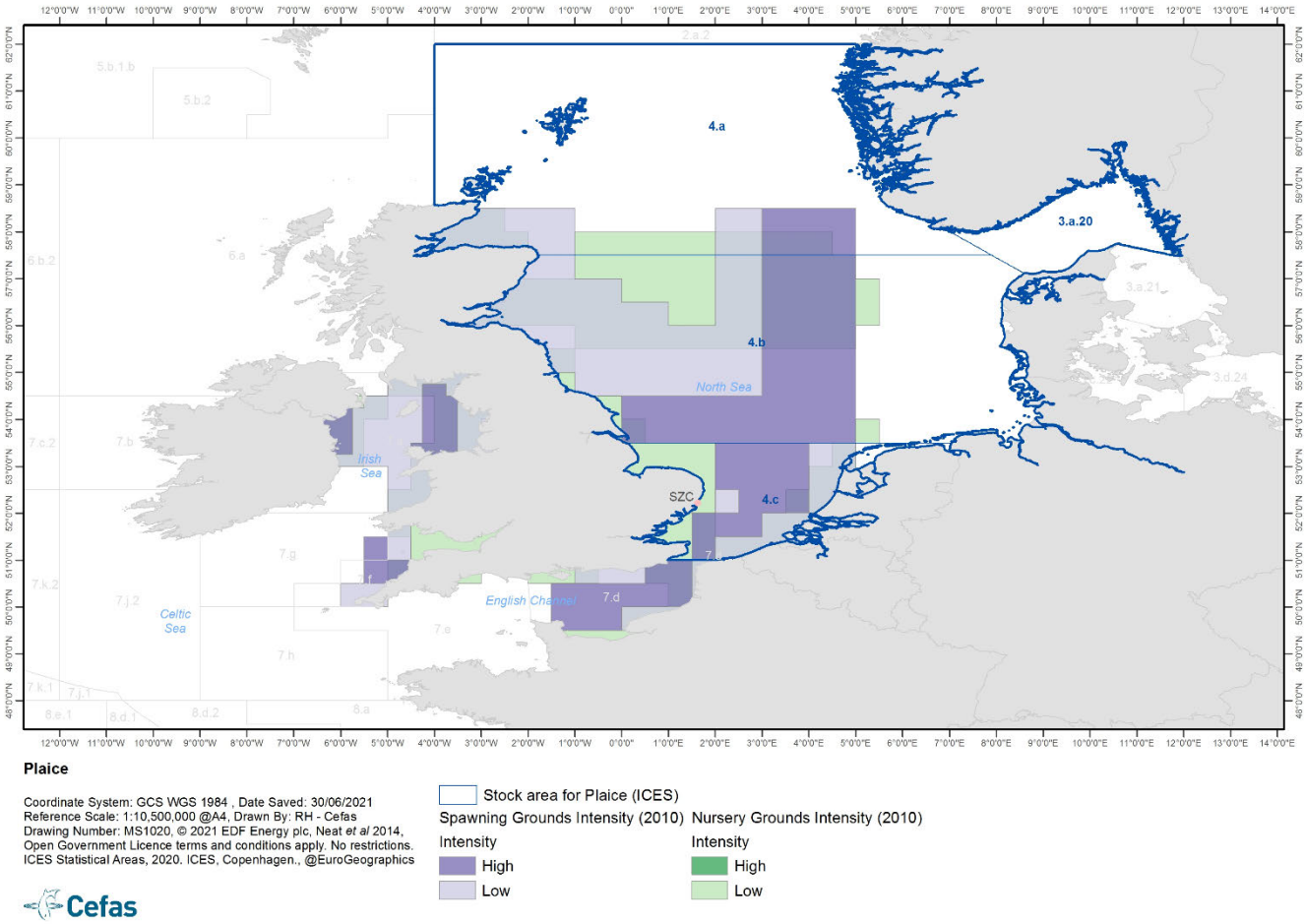

Figure 1. ICES stock area for plaice showing spawning and nursery areas relative to Sizewell C.

Cod

1.2.55 The ICES stock unit for cod used as a comparator for impingement assessments is Subarea 4 & Subdivisions 7.d & 20 (North Sea, Eastern Channel, Skagerrak & Kattegat) (Figure 2).

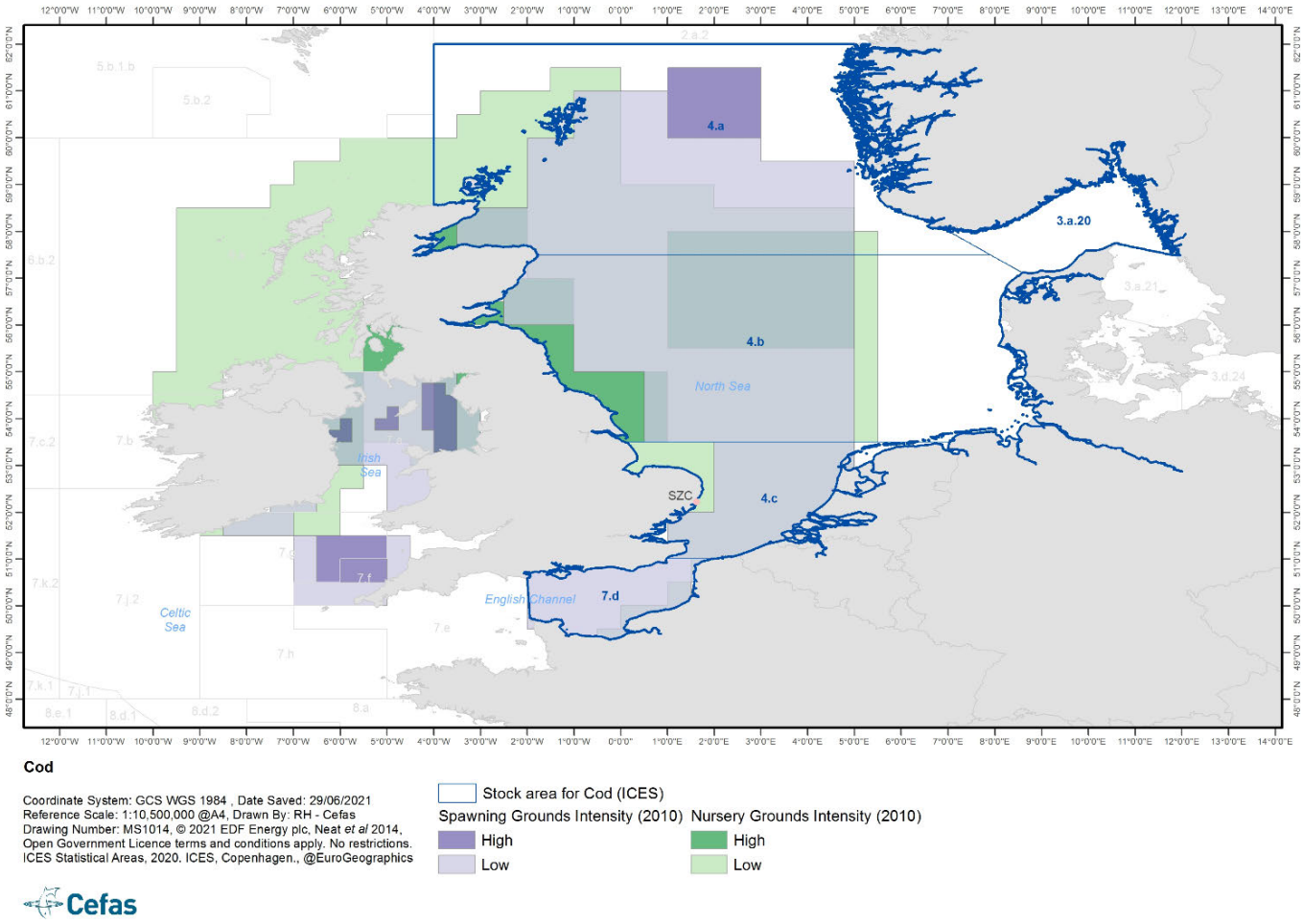

Figure 2. ICES stock area for cod showing spawning and nursery areas relative to Sizewell C.

1.2.56 The cod stock is widely distributed throughout the North Sea, but there is growing evidence of subpopulation structure inhabiting different regions of the North Sea with limited mixing (ICES 2020). The Workshop on stock Identification of North Sea Cod (WKNSCodID) was held in August 2020 and concluded that North Sea cod includes two reproductively isolated populations: Viking and Dogger cod. Viking cod inhabit the northeast North Sea (on and around Viking Bank, 4.a). The spatial distribution of Viking cod extends westward to the Shetlands (western part of 4.a) and southward to the Fischer and Jutland Banks (northern part of 4.b), with a nursery area in the Skagerrak (20). Some Viking cod juveniles also inhabit the Kattegat. The Dogger cod population inhabits the south–central North Sea (on and around Dogger Bank, 4.b), along the Scottish coast to the north of Scotland (northern part of 6.a), and in the eastern English Channel (7.d), with some adults seasonally migrating to the western English Channel (7.e–k) and the Dogger population extends into northwest of Scotland. Within the Dogger

cod, there are phenotypic differences in the northern and southern North Sea, indicating further population structure.

1.2.57 As a result of further evidence for structuring of the population in the North Sea and adjacent areas, ICES is currently developing an assessment that account for this sub-stock structure, with the aim of another benchmark assessment around 2023. Data are now being collated that are best suited for assessments of sub-stocks of cod. Figure 3 shows the latest understanding of the population structure of cod in the North Sea. Skagerrak (area 20; shaded in pink) is a nursery ground of juvenile Viking cod with some mixing of juvenile southern Dogger cod. The approximate area of distribution of northern Dogger cod is shown in blue, and southern Dogger cod in green, roughly separated by the isobath of 50 m. The sub-populations of Dogger cod exhibit differing rates of growth and maturity, with limited mixing between them resulting in some phenotypic differences.

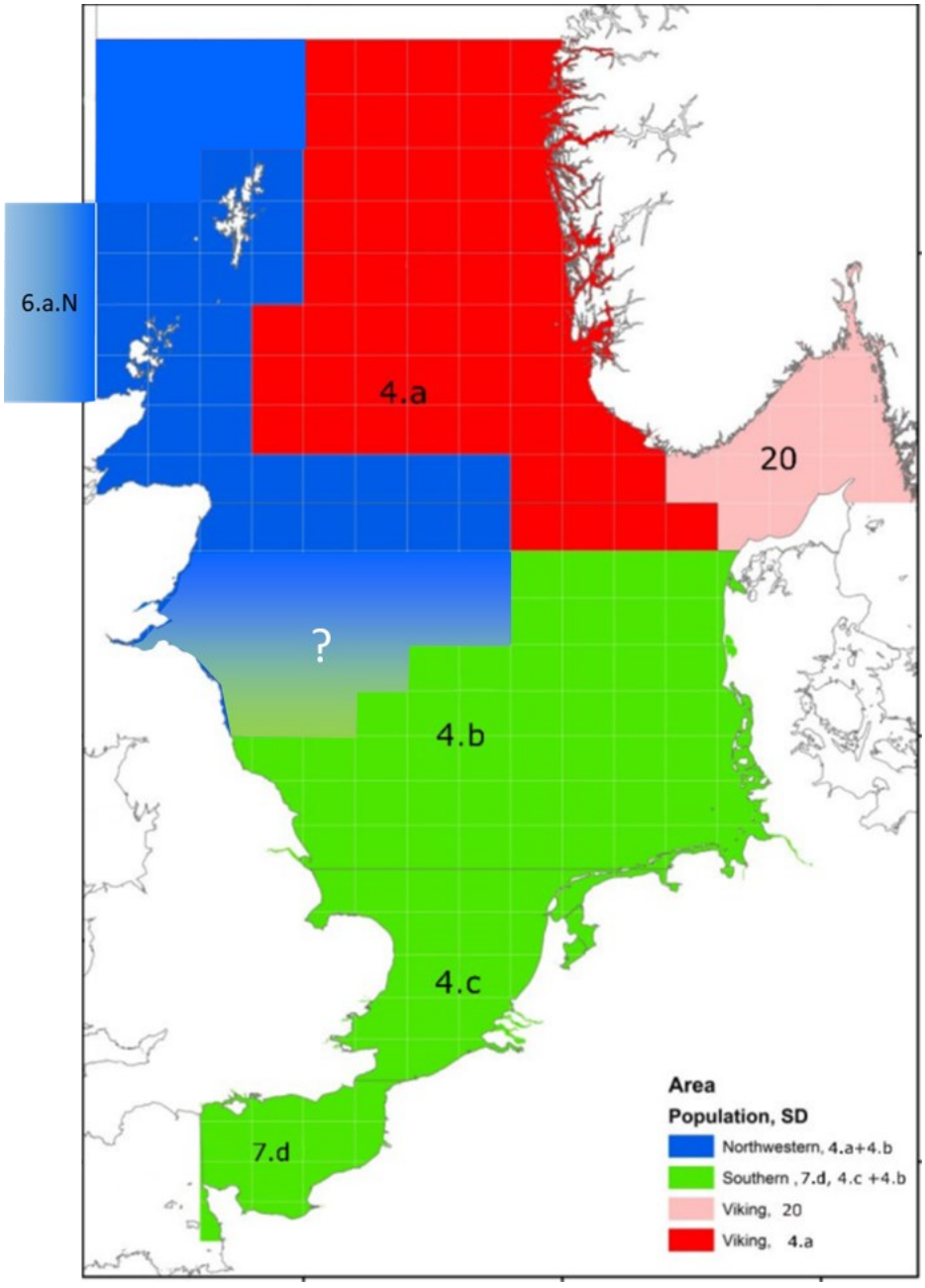

Figure 3. Sub-stock areas for the various sub-stocks: DN = Dogger North (blue), DS = Dogger South (green), V = Viking (red and pink).

1.2.58 Cod impinged at Sizewell would be part of the southern Dogger sub-population. On the basis that ICES is currently addressing the population structure within its assessments of cod, it is appropriate to readdress the comparator for impingement predictions. However, no SSB is currently available for the southern Dogger cod. In the absence of an SSB, landings

data have been used by the Applicant as a comparison. Landings in 4a would be an unknown mixture of Viking and Dogger cod. Northern Dogger cod are also known to have reduced mixing with southern Dogger cod. As such, the 20,191t per annum of landings from 4a is not considered for the assessment comparator. A precautionary landings comparator of 11,124t per annum has been calculated from landings of southern Dogger cod in 4b-c and 7d (as a rough approximation of catches of this sub-population) between 2009-2017.

1.2.59 Table 1 shows the losses of cod due to impingement from Sizewell C relative to the precautionary landings of southern Dogger cod. Following Natural England's comments, a revised precautionary landings comparator, accounting for the latest developing ICES evidence has been provided. Table 1 shows the effects of the Sizewell C station on cod are negligible at less than 0.15% of landings with no mitigation and 0.08% with FRR mitigation.

Table 1 Annual mean SZC predictions of impingement of cod compared to landings in 4b-c and 7d.

Mitigation	Mean SZC prediction	FRR mortality	EAV number	EAV weight (t)	Mean landings 2009 -2017 (t)	% of landings
Unmitigated	16,505		5,927	15.42	11,124	0.14
FRR mitigation	16,505	9,130	3,279	8.53	11,124	0.08

Herring

1.2.60 The ICES stock unit for herring is the North Sea, Skagerrak & Kattegat, Eastern Channel (Subarea 4 & Divisions 3.a & 7.d). The SSB for the herring is applied as a comparator for impingement assessments (Figure 4).

1.2.61 The current understanding of North Sea herring and the wider stock is summarised below and also described in BEEMS Technical Report TR406.v7 [Section 6.6.5 of AS-238].

1.2.62 The North Sea herring stock is generally understood as representing a complex of multiple spawning components (Iles and Sinclair, 1982; Heath *et al.,* 1997) predominantly comprised autumn/winter spawners, with small spring-spawning components (Dickey-Collas *et al.,* 2010) mainly found as coastal groups in areas such as The Wash, Thames Estuary, Danish Fjords and the now extinct Zuiderzee herring (Fox, 2001; Roel et al., 2004; Berges,

2018). The stock is commonly referred to as North Sea Autumn spawners (NSAS). The potential for impacts on Blackwater herring as part of the Thames Estuary spring spawners is considered in [Section 6.6.5 of TR406.v7 AS-238]. Blackwater herring spawning on the Eagle Bank in the greater Thames Estuary occurs in February-April, which is coincident with the period of maximum herring impingement (Q1) at Sizewell B approximately 60km to the north.

1.2.63 Autumn/winter spawning herring largely consists of four genetically homogenous components or sub-stocks (Mariani *et al.,* 2005) and contributions of these individual components to the total stock differ over time (Berges, 2018). These components are identified by their separate spawning grounds; Orkney /Shetland, Buchan, Banks (central North Sea) and Downs (southern North Sea and eastern English Channel). Mixing of autumn spawning herring and spring spawning herring occurs on summer feeding grounds.

1.2.64 The Applicant's scientific hypothesis theorises North Sea herring breed in a meta-spawning migration that includes all autumn-, winter- and spring-components spawning at their distinct grounds on route, progressing steadily southwards with time for the four main grounds and then northwards along the coast for the coastal spring-spawning grounds. The migration would start in August at Orkney/Shetland, herring would proceed via the Banks to the Downs in January, followed by northwards direction into the Thames in February and then continuing north along the East Anglia coast to The Wash and Humber. This is supported by the suggested maturation cycle; all spawning types start maturation in April-May and keep developing until autumn-spawning or stop development until just prior to winter- and spring-spawning (van Damme et al., 2009).

1.2.65 The separation of Downs and other components (including coastal spring-spawners) of the NSAS has not been implemented to date and the current definition of the North Sea stock of NSAS and winter spawners has operated well in the past despite changes to the relative strengths of different spawning components (Reiss *et al.,* 2009; Berges, 2018).

1.2.66 The most recent benchmark of the North Sea herring assessment in 2018 confirmed there was currently no need to revisit the stock identity (ICES, 2018). This herring stock can effectively be viewed as a meta-population consisting of at least four sub-stocks (and potentially more, especially when considering the coastal spring-spawners) and therefore herring impinged at Sizewell would be part of the North Sea stock. The NSAS stock components are genetically homogenous (Mariani *et al.,* 2005; Reiss et al., 2009) and consequently the Applicant considers the ICES North Sea

herring population comparator to be the most appropriate unit for assessment of impacts from the station.

1.2.67 Unmitigated losses from Sizewell C are predicted to account for approximately 0.01% of the SSB for herring. Landings of the North Sea stock between 2009-2017 equated to over 16% of the mean SSB whilst losses associated with the station are predicted to be less than 0.08% of landings. This reflects the very low impact of the station on the sustainability of herring populations.

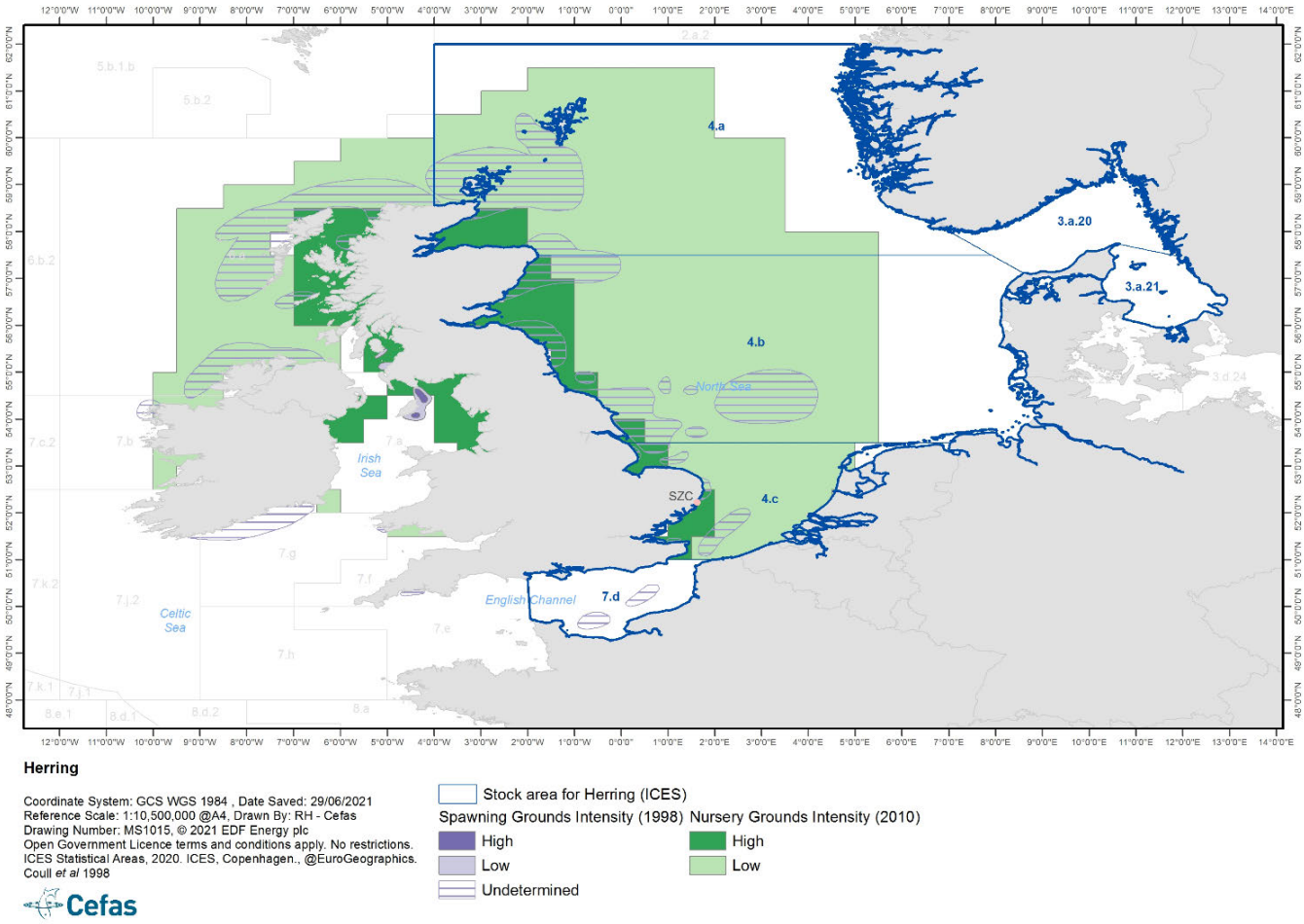

Figure 4. ICES stock area for herring showing spawning and nursery areas relative to Sizewell C.

Whiting

1.2.68 The ICES stock unit for whiting is the North Sea and Eastern Channel (Subarea 4 and 7.d), impingement assessments are compared against the SSB of this stock (Figure 5).

1.2.69 Whiting is assessed by ICES as a single stock inhabiting the North Sea and eastern English Channel. Genetic studies (Charrier *et al.,* 2007) revealed genetic structure within the North Sea, that "*may be associated with the complex oceanography of this basin and retention systems reducing larval dispersal*". The stock was benchmarked in 2018 and the workshop came to agreement that the stock consists of a northern and a southern component. The boundary between these components is suggested to occur at ~ 50 m depth (Holmes *et al.,* 2014). The northern and southern components live at different temperatures and depths and therefore exhibit slightly different life history traits and literature suggests a spatial split in spawning aggregations during spawning season.

1.2.70 The stock identity was revisited by ICES and it was concluded that the current assessment area of the North Sea and Eastern Channel should remain (ICES 2018). The two components were further considered by ICES and it was concluded that separate assessment of the northern and southern components is not considered necessary (ICES 2020) and there is no unambiguous evidence to indicate that the two components are distinct stocks.

1.2.71 On the basis of the latest ICES advice, the Applicant considers the North Sea and eastern English Channel stock to be the most appropriate unit for assessment of impacts from the Sizewell C station. Unmitigated losses from the station account for approximately 0.11% of the SSB for whiting, FRR mitigation is predicted to reduce losses to 0.06% of SSB.

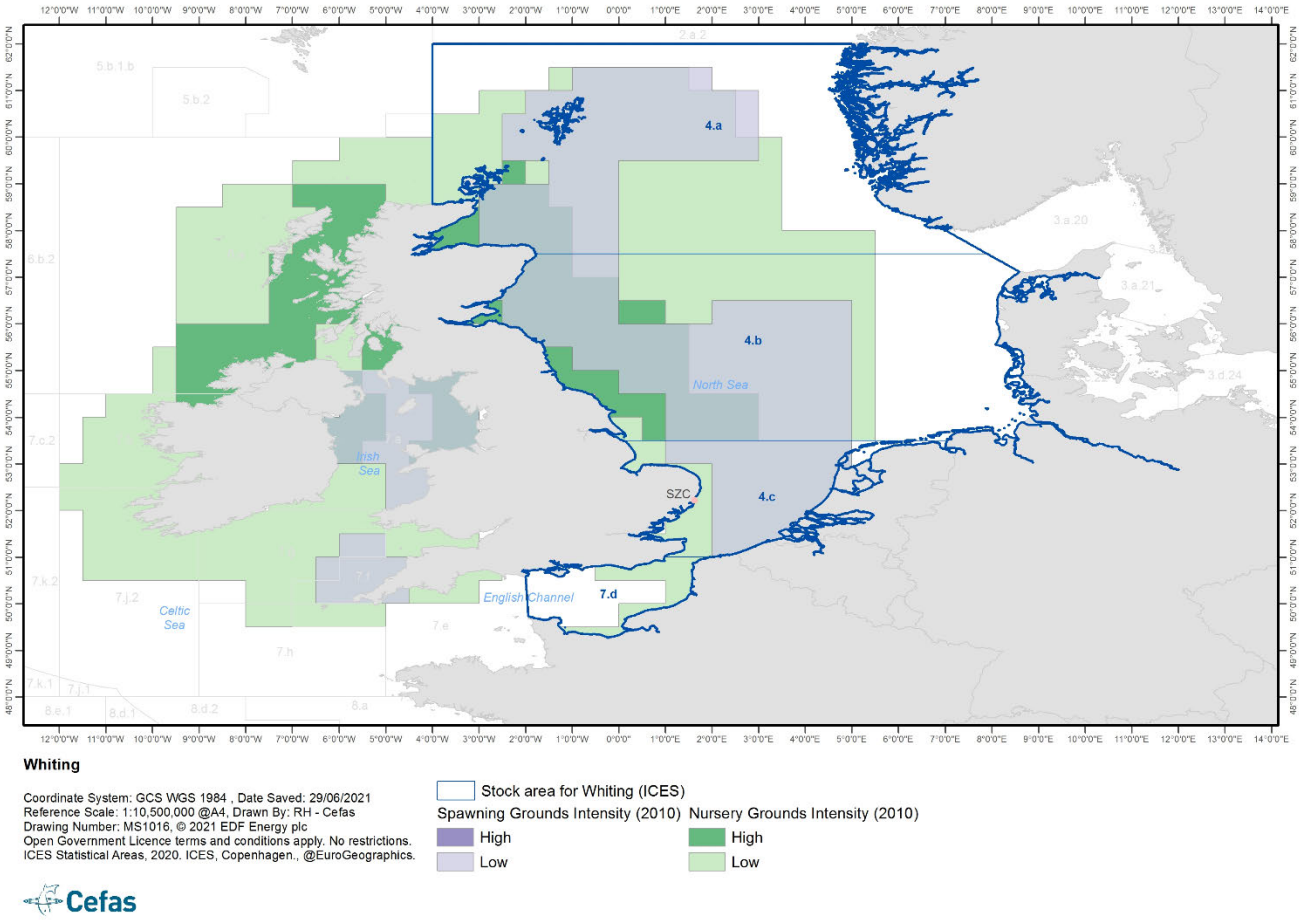

Figure 5. ICES stock area for whiting showing spawning and nursery areas relative to Sizewell C.

Seabass

1.2.72 The ICES stock unit for seabass is Divisions 4.b-c, 7.a, & 7.d-h (Central & southern North Sea, Irish Sea, English Channel, Bristol Channel & Celtic Sea) (Figure 6).

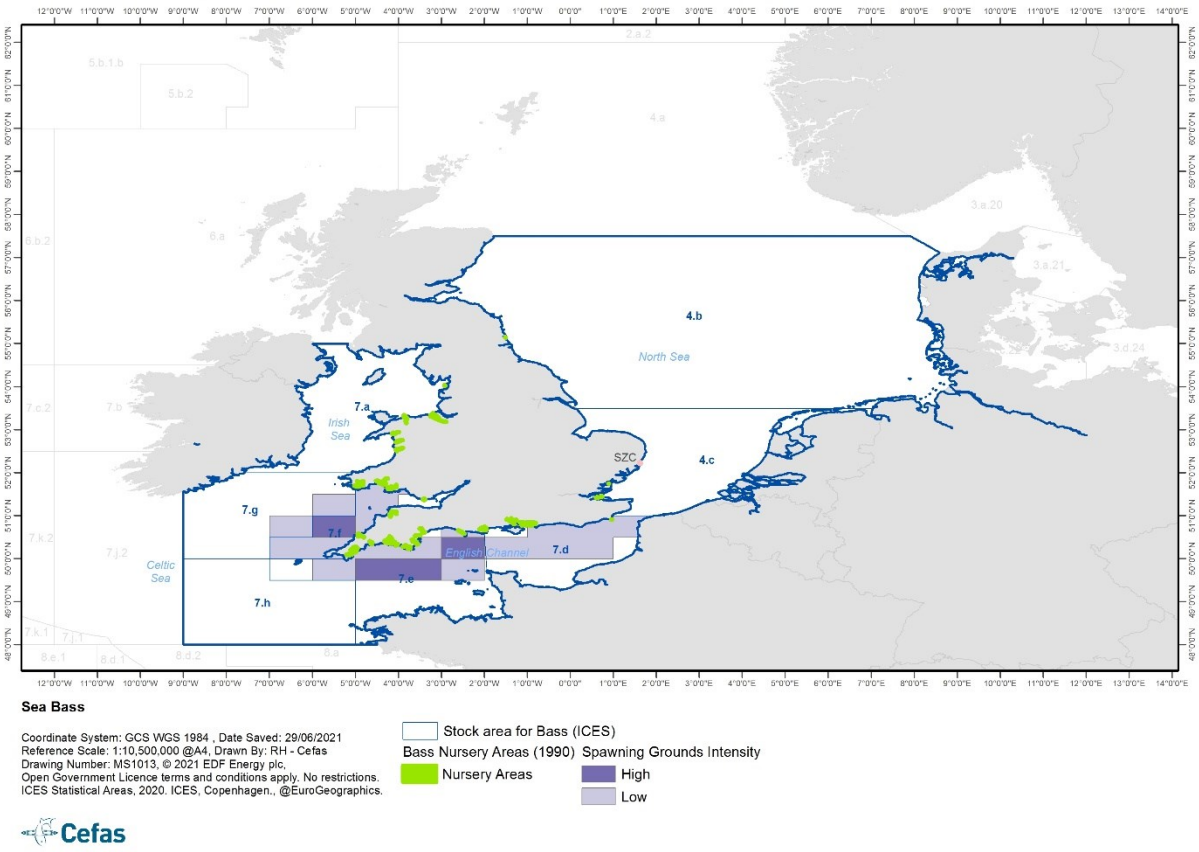

Figure 6. ICES stock area for seabass showing spawning and nursery areas relative to Sizewell C.

1.2.73 Discussions on seabass in relation to ICES advice is detailed in BEEMS Technical Report TR406.v7 [Section 4.10.2 of AS-238] and in relation to further stakeholder comments in BEEMS Scientific Position Paper SPP103.v4 (Section 2.7). The seabass stock unit incorporates both Sizewell C and Hinkley Point C developments. Therefore, the evidence provided within the recent Hinkley Point Inquiry including latest tagging data showing wide scale migratory behaviour and mixing at spawning grounds equally applies at Sizewell[3]. Bass is a migratory species. Juvenile fish spend the first 2-3 years of life in estuaries and inshore waters, and upon maturation begin to carry out seasonal migrations between inshore foraging areas in summer and moving offshore to spawn during February to July. During seasonal migrations between spawning and foraging areas bass may travel very long distances. Four selected tracks from the Cefas C-Bass project are provided in Figure 7 showing the distances of migratory movements and mixing of adult sea bass at spawning grounds. Two

[3] Proof of Evidence of Dr Simon Jennings Appendix E Biology of Relevant Species https://ea.sharefile.com/share/view/s311eef0a189a4e65b4f5243233691bfa

individuals tagged near Lowestoft on the east coast in division 4c are shown. One individual migrated from 4c across the English Channel to known spawning areas of the south west coast in divisions 7g and 7f before returning to 4c.

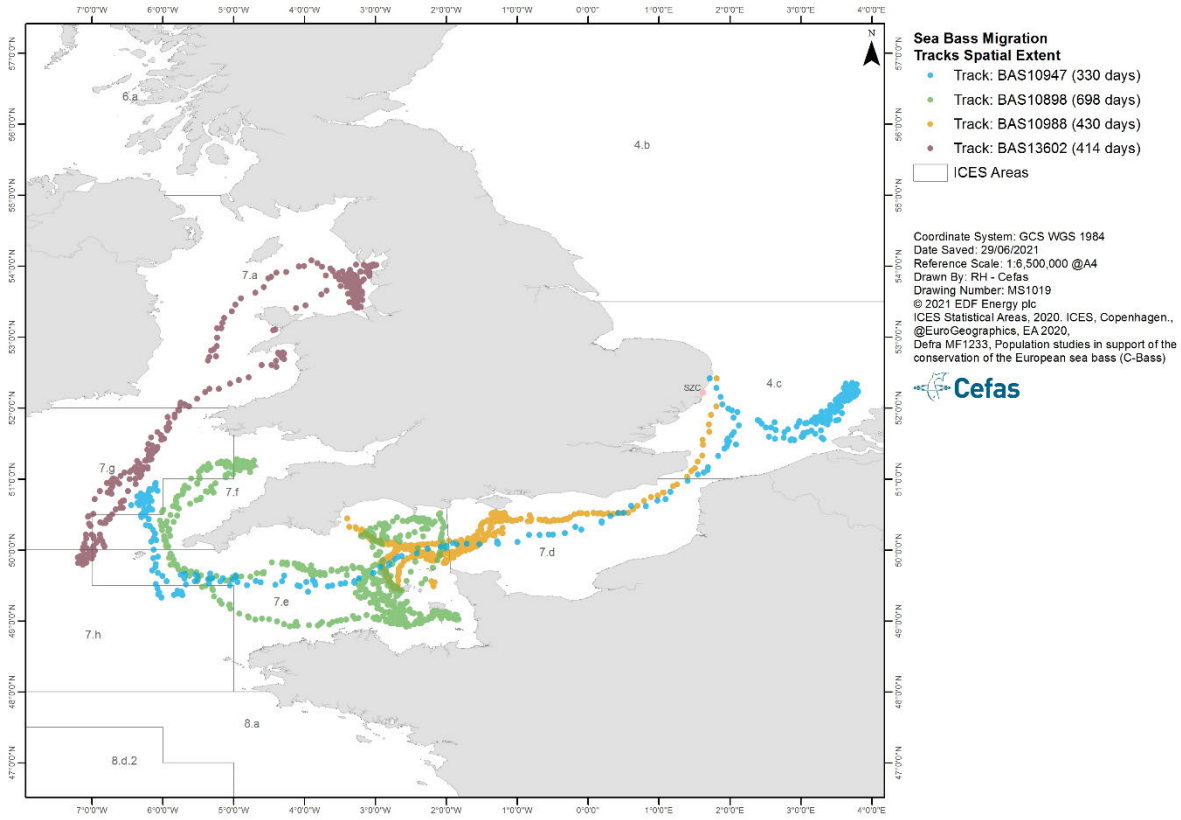

Figure 7. A selection of tracks form of four adult seabass during annual migrations determined from data storage tags employed during the C-Bass project (Ewan Hunter, pers. comm.).

1.2.74 At the ICES Benchmark Workshop on Sea Bass (ICES 2018) focus was given to whether the stock unit for seabass should be increased to incorporate the Biscay stock:

"The sea bass inhabiting the Atlantic Ocean show a remarkable homogenous genetic structure although homing based on mark–recapture data suggests some level of population structure. Off the Strait of Gibraltar (9.a) there is evidence of introgression by the Mediterranean group. Sea bass inhabiting the areas Northern (4.b&c, 7.a,d–h) and Biscay (8.a&b) represent genetically one population unit. The current management in two stocks (Northern and Biscay) can be considered a conservative and correct measure".

1.2.75 As discussed in the above BEEMS reports, the Applicant is aware of studies showing seasonal site fidelity in some life stages of seabass. However, in light of the available evidence the Applicant sees no justification to reduce or deviate from the ICES stock unit, which is described as a *"conservative and correct measure".*

iv. Alternative stock areas

1.2.76 The Applicant considers ICES stock areas to be the most robust, peer reviewed application of the evidence for determining population units for commercially harvested data-rich species. Where such evidence is available the Applicant refers to the higher authority of ICES.

1.2.77 It is noteworthy that the Applicant has not exclusively referred to ICES stock areas, as suggested by Natural England, but does apply ICES advice where data is available as this represents the most evidence-based, robust population comparator. For species that are not covered by ICES advice, or where more appropriate population comparators are available, these have been applied. BEEMS Scientific Position Paper SPP103.v4 (Table 1, therein) demonstrates the population comparators applied for each species. For the key species at Sizewell, examples where ICES areas are not applied include:

- The Anglian River District Basin silver eel biomass has been applied to contextualise losses of European eel.
- Population estimates for sand gobies have been derived from survey effort.
- The Applicant has sought to determine populations sizes of twaite shad in European rivers to contextualise impacts (see Issue 30, Section 1.3).
- Conservative estimates of regional SSB have been estimated from Environment Agency landings of smelt in the Anglian region.
- Population size estimates of the Humber catchment river lamprey estimated run numbers, provided by the Environment Agency, have been applied to contextualise losses of river lamprey.

1.2.78 Natural England aligns its position with that of the Environment Agency at the Hinkley Inquiry where Proofs of Evidence[4] were provided in support of more localised populations of cod, whiting, sea bass and herring at Bridgwater Bay. Natural England recognises the *"myriad of differences"*

[4] Proof of Evidence Adam Waugh: https://ea.sharefile.com/share/view/s65a5895fee974dbca4c13cb950a6e28f

between the projects and sites but support the approach to the application of evidence applied by the Environment Agency.

1.2.79 The Applicant does not agree with Natural England's position and has highlighted fundamental flaws in the approach adopted by the Environment Agency to redefining population boundaries and estimates of SSB within those redefined areas. The concerns with the population areas and biomass are provided in the Rebuttal Proof of Evidence of Dr Simon Jennings[5] whilst a justification of the application of ICES units at Hinkley Point was made in the main Proof of Evidence of Dr Jennings[6]. In brief,

- The 'population' areas applied at Hinkley Point did not consider the full life history of the species of concern focusing on evidence of behaviours such as seasonal site fidelity during part of the life history stage.
- The delineated population areas in some cases intersected spawning sites. These spawning sites are where mixing of adult fish occurs and the progeny of fish that recruit to the nursery areas in Bridgwater Bay are produced.
- Once the new 'population' areas were delineated, ICES biomass was simply divided by the relative difference between the delineated area and the ICES stock area. This assumes homogenous distribution of fish throughout ICES areas and ignores the biology of the species and habitat utilisation.

1.2.80 The disconnect between ICES Divisions and the species biology approach proposed by the Environment Agency at Hinkley Point is stark. ICES Divisions are created for statistical interpretation and management purposes. A species population or stock unit is determined based on the biology of the species throughout its full life-cycle including spawning migrations, larval dispersal and patterns of recruitment. When a population or stock is assigned to an ICES Divisions by the Working Group during the Benchmark process it does not suggest even distribution within such areas, or even permanent presence in a particular Division, but rather that the Divisions provide the most appropriate way of delineating the boundaries of the population (for management purposes). This is particularly pronounced in species such as seabass[7]. ICES Division 4b in the northern

[5] Rebuttal Proof of Evidence Simon Jennings: https://ea.sharefile.com/share/view/se7167ce2cd7040fab807c5d65fe76498.

[6] Proof of Evidence of Simon Jennings: https://ea.sharefile.com/share/view/se7167ce2cd7040fab807c5d65fe76498.

[7] The life-cycle and biology of sea bass in relation to ICES advice is detailed in BEEMS Technical Report TR406.v7 [Section 4.10.2 of AS-238] and in relation to further stakeholder comments in BEEMS Scientific Position Paper SPP103.v4 (Section 2.7).

North Sea accounts for approximately 46% of the total spatial area of the ICES stock unit for seabass, however, 4b is at the limit of the seabass distribution and relative biomass is low. This point can be illustrated by viewing annual landings as a relative proxy for the distribution of adult stages (Figure 8). If the total SSB was divided simply by area, the resultant unit area biomass would be misleading.

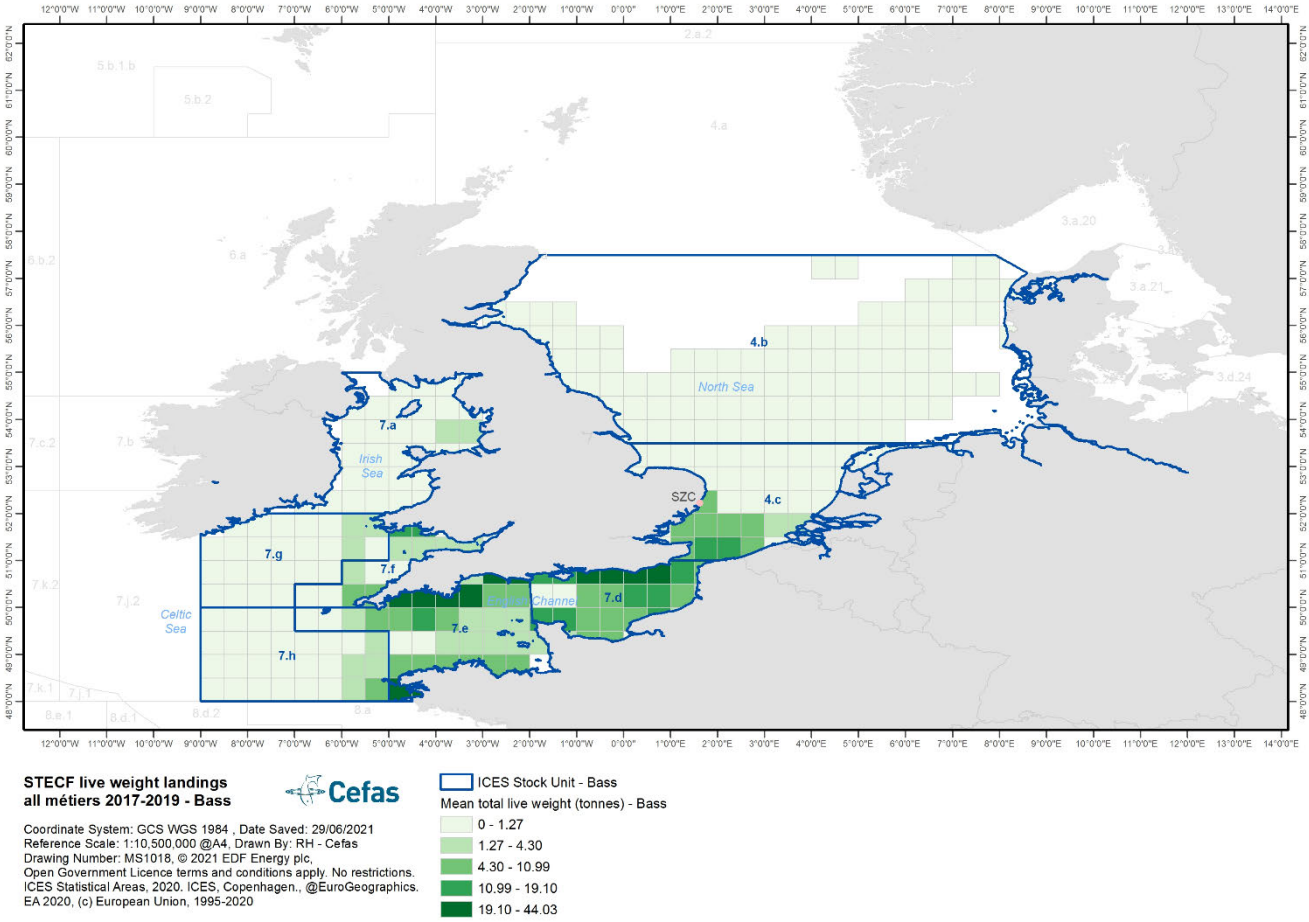

Figure 8. Seabass landings by ICES statistical rectangle as a proxy to illustrate distribution within the ICES stock unit.

1.2.81 No alternative population area has been presented in the context of Sizewell. The Applicant therefore maintains that for commercial species where ICES advice is available, this represents the best available evidence. The MMO supported this position in their Deadline 2 Submission to the Planning Inspectorate [REP2-140] at paragraph 2.4.7 (emphasis added):

"In relation to the scale of assessment, the MMO notes that the Applicant continues to justify the use of the International Council for Exploration of the Sea ("ICES") stock areas as using the best available evidence. The MMO

concludes that the use of ICES stock areas for commercial fish species represents the current best scientific evidence available. There is currently no robust information that would support use of more local stock areas in the assessment. The percentage impact on a stock increases in proportion to the decrease in stock area/size used (the stock area/size is the denominator in the impact calculation). Thus, a ten-fold reduction in the stock area/size used results in a 10-fold increase in estimate impact."

v. Adaptive management

1.2.82 Natural England have questioned the comparison of a power station as a form of harvesting, in a similar manner to fishing. The effects of a power station, although small in comparison to fishing, are fixed spatially and for the duration of the operational phase whereas fisheries managers can implement adaptive fisheries management strategies in response to changes in stock dynamics. This may include, for example, reductions in total allowable catch (TAC), closed seasons, or redistribution of fisheries effort away from sensitive areas. Such strategies are not available to a power station once operational. However, at large scales there is often a disconnect between adaptive management advice and implementation of that advice.

1.2.83 To maximise catch, fishing effort is targeted towards productive areas and fleets either operate seasonally, or fish different areas or target species at different times of the year. Whilst bycatch in some fisheries remains high, fishing effort is targeted, often at the oldest most fecund life-stages and changes in effort, gear types, or location can be employed to maximise yields. Once operational, Sizewell C would not be able to change abstraction rates or location. However, the station is a non-selective sampler i.e. rates of impingement are reflective of abundance. As a population increases, so too would impingement, conversely as a stock declines, so impingement rates would decline reflecting local abundance. Consequently, impingement numbers are likely to change through time (e.g. due to climate change) but the relative effect on the stock would only change if site utilisation changed dramatically.

vi. Uncertainty and precaution

1.2.84 Natural England indicate that the *"uncertainty contained within the assessment risks adverse environmental outcomes"* and that uncertainty in fisheries management should be managed by *"robust, adaptive and precautionary"* approaches.

1.2.85 The Applicant maintains that applying ICES population units, where available, ensures that the most robust evidence is being applied and

disagrees that the science underpinning ICES advice is not adaptive. Indeed, throughout the application process the Applicant has reviewed and altered SSB and/or landings statistics and even population units to keep abreast with developing ICES advice.

1.2.86 Precaution is central to impingement predictions. However, precautionary assumptions must consider the implications as layering of precaution can result in unrealistic results. The Applicant has recognised the request for further uncertainty analyses from both the MMO [REP2-140] and the EA which will be submitted as part of Deadline 6 material to PINS, particularly in respect to fish mitigation measures. The uncertainty analysis will consider the sensitivity of the assessments to impingement mitigation efficiency, confidence intervals in annual impingement estimates and variation in population comparators. The uncertainty analysis will also outline the precautionary measures involved in the assessment of impingement.

1.3 Intakes and Outfalls (Part II, Issue 30)

a) Natural England comment

1.3.27 Natural England raise concerns that *"the Intakes and Outfalls may have potential water quality impacts upon designated sites and species, either directly through the presence of the infrastructure itself and the chemical thermal plume or indirectly through food webs and associated displacement of prey species and bioaccumulation."*

1.3.28 Further specific comments were made in relation to:

- Twaite shad - Natural England welcomed the additional data on twaite shad in the River Elbe and Scheldt but question the methodology used to obtain the population estimate. Furthermore, Natural England disagree with the Applicant's assumption that twaite shad impinged at Sizewell B are part of a mixed southern North Sea population and likely to be captured on a pro-rata basis from their source rivers. Natural England state that this approach is not consistent with a precautionary HRA approach.

- Allis shad – Natural England welcomed the inclusion of the Tamar Allis shad population.

- Migratory Fishes and additional mitigation measures (addressed below).

- Fish as a prey for HRA bird species (response provided at Deadline 3).
- Update to baseline conditions – Marine birds (response provided at Deadline 3).
- Scale of Assessment (response provided in Section 1.2, Part II Issue 22).

b) Applicant's Response

i. Twaite shad

1.3.29 Natural England welcomed the addition of the twaite shad information and population in BEEMS Technical Report SPP100 [AS-238] and the update to the Habitats Regulations Assessment (HRA) addendum [AS-178]. The HRA has scoped in European sites designated for twaite shad where the site is recorded as having breeding populations. These include:

- Schelde - en Durmeëstuarium van de Nederlandse grens tot Gent SCI, (Scheldt) is located 197km from Sizewell C;
- Unterweser SCI – (Weser) 479km from Sizewell C;
- Weser bei Bremerhaven SCI - (Weser) 483km from Sizewell C;
- Nebenarme der Weser mit Strohauser Plate und Juliusplate SCI – (Weser) 475km from Sizewell C;
- Schleswig-Holsteinisches Elbästuar und angrenzende Flächen SCI – (Elbe) 509km from Sizewell C;
- Unterelbe SCI – (Elbe) 508km from Sizewell C.
- Mühlenberger Loch/Neßsand SCI – (Elbe) 563km from Sizewell C;
- Rapfenschutzgebiet Hamburger Stromelbe SCI – (Elbe) 565km from Sizewell C;
- Hamburger Unterelbe SCI – (Elbe) 582km from Sizewell C;
- Elbe zwischen Geesthacht und Hamburg SCI – (Elbe) 584km from Sizewell C;
- Marais du Cotentin et du Bessin - Baie des Veys SAC - 396km from Sizewell C;

- Tregor Goëlo SAC – 532km from Sizewell C.

1.3.30 Natural England recommend that consistent with a precautionary HRA approach, predicted losses of twaite shad from SZC should be assigned against each breeding population given genetic information is not available to determine the source population.

1.3.31 Natural England report Jolly et al., (2012) stating *"In particular, samples from Looe Bay and Hastings-Sizewell exhibited the strongest genetic divergence. While this suggests that movement within the marine environment is limited, the lack of significant genetic differences between the* [twaite shad] *populations of the Solway Firth and River Tywi also suggests that some migration could occur over spatial scales as great as 300 km"*. The Applicant does not refute the log-range migratory behaviour of twaite shad. The twaite shad impinged at Sizewell range from >1 yr old juveniles to sexually mature adults that are probably part of a North Sea mixed population widely dispersed across feeding grounds. Sabatino and Alexandrino (2012) showed North Sea twaite shad had low genetic diversity between fish sampled off Belgium (Scheldt) and Denmark and also the Solway Firth.

1.3.32 Fish monitoring programmes in German and Belgian estuaries are undertaken to determine trends in fish populations. However, to the best of the Applicant's knowledge, absolute population estimates are not available for the designated sites. The Wadden Sea status report (Tulp *et al.,* 2017) provides an overview of North Sea twaite shad populations in the nearby German rivers of the Ems, Eider, Elbe and Weser (summarised in BEEMS Technical Report SPP100 [AS-238]). The Elbe contributes most of the twaite shad numbers and reproduction in German estuaries. In contrast to the other Wadden Sea estuaries, numbers in the Elbe appeared to be increasing in recent years. Numbers of a small population of twaite shad in the Weser Estuary are stable without clear trends in the recent years (Tulp *et al.,* 2017). Scheldt Estuary in Belgium is exhibiting signs of "genuine improvement" (Wilson, Venerata, 2019). Twaite shad were in very poor condition in the Scheldt prior to improvements in water quality which has allowed recovery and a return of spawning adults from 2012.

1.3.33 In the absence of population estimates for the designated sites, the Applicant attempted to estimate the shad population of the Elbe and Scheldt based on data provided by European organisations. The population estimate methodology and limitations of the approach are described in BEEMS Technical Report SPP100 [AS-238]. Natural England are correct that the population numbers should be treated with a degree of uncertainty, however, as described below the level of impact from the station is well below levels that could have ecologically meaningful effects.

1.3.34 If the impacts of SZC are apportioned to each river population sequentially as requested by Natural England, the relative level of effect varies depending on the reference population. Given the distance of the proposed development from the spawning rivers (hundreds of kilometres) and the fact it is in the open coastal environment, it is highly unlikely all fish impinged at Sizewell would come from any given system. However, such a scenario is considered below for two European systems where the population estimates have been made by the Applicant: The Elbe, approximately 500km from Sizewell C, and the Scheldt approximately 200km away. Unmitigated losses of 2,693 shad by Sizewell C are predicted based on the precautionary assumption of all fish being adults (with an EAV of 1). This is considered precautionary as 46% of impinged shad are estimated to be 1- to 3-year-old fish with very low maturity rates at this age. Notwithstanding the uncertainty in the population estimate of the Elbe (ca. 5.1 million adult fish (BEEMS Technical Report SPP100 [AS-238]), unmitigated losses account for approximately 0.05% of the population if all fish impinged at Sizewell C were from this single river system.

1.3.35 The average population of the Scheldt following recovery of a breeding population in 2012 was estimated at 66,715 fish between 2012 and 2017 (BEEMS Technical Report SPP100 [AS-238]). If all the twaite shad predicted to be impinged by Sizewell C were from the Scheldt alone, the losses would account for 4% of the estimated Scheldt population. Impingement monitoring at Sizewell B has recorded twaite shad throughout the monitoring period (2009-2017), recovery in the Scheldt occurred in 2012 with no spawning adults recorded in 2011. Therefore, it is not possible that all the twaite shad impinged at Sizewell originate from this single river. It is likely that the Scheldt breeding population become re-established form fish from surrounding systems such as the Elbe.

1.3.36 The Applicant acknowledges that it is not possible to determine exactly what river system the twaite shad impinged at Sizewell originate from. However, the genetic information from North Sea shad demonstrates mixing which is consistent with the assumption that the Weser and Scheldt population recoveries have been seeded form fish originating in the Elbe.

1.3.37 The predicted scale of losses from Sizewell C are therefore considered to have negligible impacts on the breeding populations of shad in European rivers.

ii. Migratory fish

1.3.38 In light of the predicted impingement of migratory species by the proposed development, Natural England advises that further measures should be pursued to mitigate losses.

1.3.39 The Applicant acknowledges the request and a report detailing the Applicant's position in relation to the requirement for an Acoustic Fish Deterrent (AFD) has been provided at Deadline 5.

1.3.40 As part of the ongoing Eels Regulations and Water Framework Directive discussions with the Environment Agency, the Applicant is looking at the potential for further monitoring and installation of fish passes in relevant local rivers. The precise details are yet to be confirmed, but this commitment would be secured as a DCO Requirement and funded via the Deed of Obligation.

1.4 References

- Berges, B. 2018. Stock Annex: Herring (Clupea harengus) in Subarea 4 and divisions 3.a and 7.d, autumn spawners (North Sea, Skagerrak and Kattegat, eastern English Channel). Stock Annex, her. 27.3a47d. 1–62 pp. https://www.ices.dk/sites/pub/PublicationReports/StockAnnexes/2018/her.27.3a47d_SA.pdf.
- Diamond, B. Beukers-Stewart, B. D. 2011. Fisheries discards in the North Sea: waste of resources or a necessary evil? Reviews in Fisheries Science, 19: 3, 231 – 245
- Dickey-Collas, M., Nash, R. D. M., Brunel, T., van Damme, C. J. G., Marshall, C. T., Payne, M. R., Corten, A., et al. 2010. Lessons learned from stock collapse and recovery of North Sea herring: a review. ICES Journal of Marine Science, 67: 1875–1886.
- Charrier, G, Coombs, S.H., McQuinn, I.H., Laroche, J. 2007. Genetic structure of whiting *Merlangius merlangus* in the northeast Atlantic and adjacent waters. Marine Ecology Progress Series, 330: 201–211,
- Fox, C. J. 2001. Recent trends in stock-recruitment of Blackwater herring (Clupea harengus L.) in relation to larval production. ICES Journal of Marine Science, 58: 750–762.
- Hunter, E., 2016. C-Bass on the move!. [Online] Available at: https://marinescience.blog.gov.uk/2016/01/18/c-bass-on-the-move/ [Accessed 03 02 2021].
- ICES. 2018. Report of the Benchmark Workshop on Pelagic Stocks (WKPELA 2018), 12–16 February 2018, ICES HQ, Copenhagen, Denmark. ICES Advisory Committee, CM 2018/ACOM:32. 1–313 pp.
- ICES 2019. Cod (Gadus morhua) in Subarea 4, Division 7.d, and Subdivision 20 (North Sea, eastern English Channel, Skagerrak). ICES Advice on fishing

opportunities, catch, and effort Greater North Sea ecoregion Published 8 November 2019

- ICES. 2020. ICES Working Group on the Assessments of Demersal Stocks in the North Sea and Skagerrak (WGNSSK). ICES Scientific Reports. 2:61. 1249 pp. http://doi.org/10.17895/ices.pub.6092
- ICES. 2021. Benchmark Workshop on North Sea Stocks (WKNSEA). ICES Scientific Reports. 3:25. 756 pp. https://doi.org/10.17895/ices.pub.7922
- Iles, T. D., and Sinclair, M. 1982. Atlantic Herring: Stock Discreteness and Abundance. Science, 215: 627–633.
- Heath, M., Scott, B., and Bryant, A. D. 1997. Modelling the growth of herring from four different stocks in the North Sea. Journal of Sea Research, 38: 413–436.
- Hislop, J.R.G., and MacKenzie, K, 1976. Population stidues of whiting Merlangius merlangus of the northern North Sea. J.Cons. Int. Explor. Mer. 37: 98-111.
- Houghton, R.G. & Harding, D. 1976. The plaice of the English Channel: spawning and migration. ICES Journal of Marine Science, 36: 229–239.
- Mariani, S., Hutchinson, W. F., Hatfield, E. M. C., Ruzzante, D. E., Simmonds, E. J., Dahlgren, T. G., Andre, C., et al. 2005. North Sea herring population structure revealed by microsatellite analysis. Marine Ecology Progress Series, 303: 245–257.
- Reiss, H., Hoarau, G., Dickey-Collas, M., and Wolff, W. J. 2009. Genetic population structure of marine fish: Mismatch between biological and fisheries management units. Fish and Fisheries, 10: 361–395. John Wiley & Sons, Ltd.
- Roel, B. A., O'Brien, C. M., and Basson, M. 2004. Management options for the Blackwater herring, a local spring-spawning stock in the Thames Estuary. ICES Journal of Marine Science, 61: 297–307.
- Sabatino, S., & Alexandrino, P. 2012. Genetic diversity and population structure of the Eurasian shads Alosa alosa and Alosa fallax. CIBIO report AARC project - Activity 4, December 2012.
- Schuch, E., Gabbert, S., & Richter, A.P. 2021. Institutional inertia in European fisheries – Insights from the Atlantic horse mackerel case. Marine Policy; 128, 104464.
- Tulp, I., Bolle, L. J., Dänhardt, A., de Vries, P., Haslob, H., Jepsen, N., & van der Veer, H. W. 2017. Fish. Wadden Sea Quality Status Report 2017. Wilhelmshaven: Common Wadden Sea Secretariat.

- Ulrich, C., Hemmer-Hansen, J., Boje, J., Christensen, A., Hüssy, K., Sun, H., & Worsøe Clausen, L. 2016. Variability and connectivity of plaice populations from the Eastern North Sea to the Baltic Sea, part II. Biological evidence of population mixing. Journal of Sea Research, 120: 13–23.
- van Damme, C. J. G., Dickey-Collas, M., Rijnsdorp, A. D., and Kjesbu, O. S. 2009. Fecundity, atresia, and spawning strategies of Atlantic herring (Clupea harengus). Canadian Journal of Fisheries and Aquatic Sciences, 66: 2130–2141.
- Wilson, K., and Veneranta, L. (Eds). 2019. Data-limited diadromous species – review of European status. ICES Cooperative Research Report No. 348. 273 pp.

APPENDIX L

ABBEY FARM COMPENSATION SITE

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1 BACKGROUND

1.1 Abbey Farm compensation site

1.1.1 The Habitats Regulations Assessment (HRA) for the Suffolk Shoreline Management Plan II (SMP2) (Ref. 1.1) concluded that adverse effect on integrity could not be excluded for the Benacre to Easton Bavents Special Protection Area (SPA) and the Minsmere-Walberswick SPA and Ramsar site. This conclusion was reached due to predicted losses of freshwater habitats as a result of implementation of the shoreline management policies set out in the SMP2. Consequently, compensatory habitat (identified as part of the Anglian Regional Habitat Creation Programme) was created adjacent to Abbey Farm, near Snape, by the RSPB (working with the Environment Agency).

1.1.2 The compensatory habitat consists of 49ha of wetland and forms part of a larger 70ha wetland system. The site functions as reedbed habitat and supports breeding bittern and marsh harrier, but does not form part of a site protected under The Conservation of Habitats and Species Regulations 2017 (as amended).

1.1.3 The RSPB has raised concern regarding the management of water levels at the Benhall Fen Meadow site[1], which is located in the river Fromus catchment, upstream of the Abbey Farm compensation site. Specifically, the RSPB has stated that if SZC Co. needs to hold back water from the River Fromus in the summer months (when the RSPB states that the compensation site is vulnerable to water supply when river levels drop) as part of the management of the Benhall Fen Meadow site, which could exacerbate water supply issues at the Abbey Farm compensation site. The RSPB is concerned that reduced water supply could have negative effects on the habitats at the compensation site and the species that the habitats support, with particular reference to breeding bittern and marsh harrier.

1.1.4 According to Government policy (Ref 1.2), *"sites identified, or required, as **compensatory measures for adverse effects on habitats sites**[2]* [emphasis added], *potential Special Protection Areas, possible Special Areas of Conservation, and listed or proposed Ramsar sites"*, should be given the same protection as European sites. Consequently, this note

[1] Benhall Fen Meadow site is one of the sites proposed for creation of fen meadow habitat in light of the permanent loss of approximately 0.5ha of 'fen meadow' habitat from the Sizewell Marshes Site of Special Scientific Interest (SSSI).

[2] Referred to in the Shadow Habitats Regulation Assessment (HRA) Report (Doc Ref. 5.10) [APP-145 to APP-149] as European sites. These are sites included within the definition of Regulation 8 of The Conservation of Habitats and Species Regulations 2017 (as amended by The Conservation of Habitats and Species (Amendment) (EU Exit) Regulations 2019)).

considers the potential effect of the management of the Benhall Fen Meadow site on the Abbey Farm compensation site in the context of The Conservation of Habitats and Species Regulations 2017 (as amended).

1.2 Potential effect pathway

1.2.1 The **Shadow Habitats Regulation Assessment (HRA) Report** (Doc Ref. 5.10) [APP-145 to APP-149] identified 10 effect pathways (referred to as screening categories) through which the Sizewell C Project has the potential to affect European sites. The screening category relevant to the scope of this note is '*alteration of local hydrology and hydrogeology*'. This screening category encompasses potential physical effects on freshwater, including surface and groundwater resources (i.e. effects on flows and water levels, as well as any consequential indirect effects on habitats and species).

1.2.2 The detail of the works to be undertaken at the Benhall Fen Meadow site, and how the site will be managed to maximise the extent of fen meadow habitats, will be set out in the Fen Meadow Plan (in prep.) and submitted to examination at Deadline 6. The Fen Meadow Plan will be informed by (amongst other aspects):

- ecological survey;
- review of available groundwater level data and the seasonal variation in groundwater levels; and
- collection of surface water level and groundwater level data.

1.2.3 Baseline data collected to date (to May 2021) at the Benhall site was submitted to Examination at Deadline 3 [REP3-051 and REP3-052].

1.2.4 Although the development of the Fen Meadow Plan is ongoing, there would be no direct off take of water from the River Fromus and no water control structures would be placed in the river. Whilst the draft Fen Meadow Plan will provide further definition, the creation of fen meadow will depend on a combination of changes to intra-site drainage and shallow excavations within the site. Excavations will be used to remove nutrient rich top soils and potentially also to intercept the water table to enable the creation of the fen meadow habitats.

1.2.5 Future fen meadow habitat will rely on management of groundwater within the site; consequently and given the extent of the catchment, the only possible mechanism for any impact on the River Fromus would be limited to local reductions in drainage from the site itself to the river. The general

approach at all fen meadow sites is to reverse historical; agricultural improvements locally to create more natural habitats which interact with the river and its habitats corridors as they did prior to previous agricultural drainage.

1.2.6 Give the extent of the catchment, the effect on availability of water to the Abbey Farm compensation site will, therefore, be immaterial and there is negligible potential for any negative effect on habitats within the Abbey Farm compensation site and, consequently, on species supported by those habitats.

1.2.7 In conclusion, any effect on water availability would be trivial or inconsequential, with no potential for any effect on the habitats and species at the compensation site, either alone or in-combination with other plans and projects.

2 REFERENCES

Ref. 1.1 Suffolk Shoreline Management Plan II: Appropriate Assessment Report. Royal Haskoning, 2010.

Ref. 1.2 National Planning Policy Framework. Ministry of Housing, Communities and Local Government, 2019.

APPENDIX M

MARSH HARRIER AND MARINE BIRDS

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1 THE MINSMERE-WALBERSWICK SPA AND RAMSAR SITE MARSH HARRIER POPULATION

1.1 RSPB / SWT Comments and Concerns Raised

1.1.1 The main comments and concerns raised on the assessment of noise and visual disturbance to marsh harriers of the Minsmere-Walberswick SPA and Ramsar site are in relation to:

- The current SPA (and Ramsar site) population and trends.
- The sensitivity of marsh harrier to noise and visual disturbance.
- The assessment of baseline conditions, notably the current (background) noise levels and habitat usage by marsh harrier.
- The conclusions reached in the Shadow HRA Report on the effects of noise and visual impacts on the SPA (and Ramsar site) marsh harrier population.
- The calculation of the compensatory requirement for the SPA (and Ramsar site) marsh harrier population.
- The ecological considerations for the design of the compensatory marsh harrier foraging habitat.

1.2 The Applicant's Response

i. Current SPA and Ramsar site population and trends

1.2.1 The RSPB/SWT Written Representation point to a decline in the SPA (and Ramsar site) population of breeding marsh harrier, with numbers for the period 2004 to 2018 reaching a peak of 31 nests in 2007 and subsequently declining to 17 nests in 2018. The Written Representation states that this decline is apparent within the Minsmere component of the SPA (and Ramsar site) population but it is worth noting that this trend is also apparent at the Hen Reedbed and Walberswick NNR nesting sites (see **Table 6.6** in the **Shadow HRA Report** [APP-145]). This recent decline in the SPA (and Ramsar site) population should be set against the context of a population which has undergone a longer-term increase and recovery from low levels, as detailed in the Applicant's response to Bio. 1.48 in **Responses to the Examining Authority's First Written Questions, Volume 3** [REP2-110].

Also, as apparent from **Table 6.6** in the **Shadow HRA Report** [APP-145], between 2004 and 2018, there is evidence of annual fluctuations in this population, with the numbers in 2004 (at 21 nests) being similar to those in 2018, and a small increase from 13 to 17 nests between 2014 and 2018.

1.2.2 The current SPA (and Ramsar site) population is slightly above the citation population size of 15 females (recorded pre-1991) and is regarded as being in favourable condition (having a 'maintain' objective)[1]. As described in the Applicant's response to Bio. 1.48 in **Responses to the Examining Authority's First Written Questions, Volume 3** [REP2-110], more widely, numbers of breeding marsh harrier continue to increase across the UK, with the most recent estimate being 590 – 695 pairs for 2016, which compares to an estimate of 320 – 380 pairs for 2006 to 2010 (Ref. 1.1; Ref. 1.2).

ii. Marsh harrier sensitivity to noise and visual disturbance

1.2.3 The RSPB/SWT Written Representation raises several issues on the potential sensitivity of marsh harrier to noise and visual disturbance and the implications for the thresholds and buffers used for the assessment. However, despite this, there is a level of acknowledgement that the use of the 70dB L_{Amax} noise threshold is appropriate on the basis of the available evidence.

1.2.4 In relation to noise levels, the Written Representation highlights two main points, as follows:

- Avoidance may occur at a lower noise threshold than 'flushing', on the basis that this avoidance may be energetically less expensive (with foraging birds less constrained to a particular location than when at the nest).
- Harrier species are known to make significant use of their hearing to detect prey when foraging, which could mean that noise disturbance could have greater effects on their foraging than otherwise expected (with implications for the appropriateness of the threshold used).

1.2.5 Considering the first of the above points, no actual evidence is provided to support this position. Given the fact that avoidance of foraging habitat would mean birds have to use alternative foraging sites that may be less preferred (e.g. because of greater flight distances from the nest site or lower

[1] https://designatedsites.naturalengland.org.uk/Marine/SupAdvice.aspx?SiteCode=UK9009101&SiteName=minsmere&SiteNameDisplay=Minsmere-Walberswick+SPA&countyCode=&responsiblePerson=&SeaArea=&IFCAArea=

prey availability) it is perhaps more likely that there is actually a greater energetic cost to such avoidance than there is to 'flushing'. Furthermore, the monitoring undertaken at Trimley Marshes (next to the Port of Felixstowe) provided direct evidence to suggest that marsh harrier will use foraging areas where impulsive noise levels are frequently at 65dB L_{Amax} and sometimes at 70dB L_{Amax} (see **paragraphs 8.8.180 – 8.8.183** of the **Shadow HRA Report** [APP-145]). This suggests that a noise threshold of 70 dB L_{Amax} is appropriate.

1.2.6 On the issue of the reliance of foraging harriers on their hearing, this is discussed in detail in **paragraphs 8.8.175 and 8.8.184** of the **Shadow HRA Report** [APP-145] and the available evidence is taken into consideration in the assessment (and in determining the thresholds to use). As the thresholds are based upon impulsive noise, it is also the case that these represent the peak levels foraging birds would be exposed to for short time durations only (and, as such, they have limited implications in terms of reducing the ability to detect auditory cues). Again, the monitoring undertaken at Trimley Marshes suggests marsh harriers will actively forage in areas subject to noise levels of 65 - 70 dB L_{Amax}.

1.2.7 In relation to visual disturbance, the Written Representation highlights particular concerns with the evidence on the sensitivity to wind farms that is relied upon (Ref. 1.3). However, whilst pointing to the limited information which is specific to marsh harrier, the Written Representation fails to provide the fuller context around this evidence, which indicates little disturbance, more generally, to foraging raptors at wind farms. Similarly, whilst the Written Representation emphasises certain of the findings from the study by Alves et al. (2014) (Ref. 1.4), suggesting sensitivity of marsh harriers to sources of anthropogenic disturbance in agricultural landscapes, it fails to recognise some of the limitations of applying these findings to the situation at the SZC site. For example, the negative effects of the presence of agricultural machinery in fields on marsh harrier presence (as noted in paragraph 3.383 of the Written Representation) was apparent only in the non-breeding season (and not in the breeding season, nor at all in analyses of marsh harrier abundance). Additionally, the occurrence of roads had a negative effect on marsh harrier presence in the breeding season but a positive effect in the non-breeding season suggesting some complexity in the interpretation of certain relationships detected in this study, with the authors suggesting these seasonally contrasting effects of roads may have been due to competition from other raptor species which used roadside habitats as a foraging resource during the breeding season (see also **paragraph 8.8.209** of the **Shadow HRA Report** [APP-145]).

1.2.8 Ultimately, the determination of the potential visual impact zone (or visual disturbance buffer) is as described in **paragraphs 8.8.211 – 8.8.215** of the **Shadow HRA Report** [APP-145]. Thus, information regarding sensitivity to sources of anthropogenic disturbance (as described above) was taken into account, along with the recommended buffer distance for visual disturbance to marsh harrier at their nesting sites (Ref. 1.5) and consideration of marsh harrier flight behaviour and the site conditions, most notably the extent of screening which occurs around the main development site.

iii. Assessment of baseline conditions – current noise levels and habitat usage by marsh harriers

1.2.9 In relation to the current background noise levels in areas that are in the vicinity of the main development site and the wider area used by breeding marsh harriers from the Minsmere-Walberswick SPA, the RSPB/SWT Written Representation makes extensive comment on the noise monitoring data that are presented for the location near the South Hide on the Minsmere Reserve (**Plate 8.10 a**) in the **Shadow HRA Report** [APP-145]). However, it is difficult to understand the relevance of several of the points that are made in relation to the noise monitoring at this location, with these data being presented for the sole function of providing context on the types of background noise that may be experienced by marsh harriers in this area. Importantly, it is also the case that caveats on the noise monitoring data from this particular location are already detailed in **paragraph 8.8.186** of the **Shadow HRA Report** [APP-145], whilst this location represents only one of three locations at which data on background noise levels are presented (i.e. see also **Plate 8.10 b) and c)** in the **Shadow HRA Report** [APP-145]).

1.2.10 On the specifics of the comments in the Written Representation that are made on the data presented in **Plate 8.10 a)** in the **Shadow HRA Report** [APP-145], the basis for the claim that “Decay rates would indicate that noise levels of 70-80dB at South Hide would have reduced significantly at the distances that nests are likely to be from these sources” is not clear. To substantiate this, the distances from source to the nests, and source to monitoring location would need to be known, and information on this is not provided.

1.2.11 The Written Representation also provides commentary on the approach used to derive a measure of marsh harrier flight activity from the survey data and on marsh harrier flight activity over the Minsmere South Levels. The Applicant is pleased to note that RSPB/SWT agree that the more

appropriate metric for measuring flight activity has been used. However, the Applicant does not agree that the flight path length metric (as used in the assessment) is necessarily more sensitive to error in the accuracy of recording flight paths than the alternative metric (i.e. the flight path count), and would suggest that detailed consideration is required to determine whether or not this is the case. The Applicant would also emphasise that the survey method, and approaches to the treatment and analyses of the resulting data which have been used, derive from a process involving considerable stakeholder consultation. Therefore, the method which has been developed and used is considered to be appropriate for the purposes of the assessment.

1.2.12 In terms of the measured flight activity on the Minsmere South Levels, it is worth emphasising that the broad trends in usage across this area are relatively consistent in all breeding seasons for which survey data are available. Thus, **Figures 6.3 – 6.5** in the **Shadow HRA Report** [APP-145] show concentrated usage in the north-west of the Minsmere South Levels in 2014, 2015 and 2016. It is undoubtedly the case that (as indicated in the Written Representation) other parts of the Minsmere South Levels are used by, and are important for, foraging marsh harriers and this is reflected in the flight activity data presented in the **Shadow HRA Report** [APP-145] (e.g. **Table 6.7**) and **Shadow HRA Report Addendum** [AS-173] (e.g. **Table 6.5**). These data show that overall flight activity levels tend to be higher across the Minsmere South Levels than across any of the other High Visibility Areas (HVAs) that were surveyed. Thus, whilst the comments in the Written Representation on the usage of other parts of the Minsmere South Levels are likely to be valid, it is the case that the survey data provide the most reliable evidence on the usage of this area and they demonstrate a relatively consistent pattern of highest usage in the northwest of the Minsmere South Levels.

iv. Conclusions regarding noise and visual impacts on marsh harriers of the Minsmere-Walberswick SPA and Ramsar site

Noise disturbance of marsh harriers foraging over the Minsmere South Levels and Sizewell Marshes and the Acoustic fence

1.2.13 The RSPB/SWT Written Representation raises concerns about the modelling of noise levels across narrower time periods (i.e. of weeks and months) than the individual construction phases and in relation to ensuring that the 5m acoustic fence is constructed at the beginning of Phase 1 of the construction period. The Applicant has already addressed these issues in its Responses to the RSPB / SWT Written Representations at Deadline 3

[REP3-042] (see **paragraphs 14.5.12 – 14.5.16**) and these responses are not repeated here. In this context, the Written Representation also refers to there being several sources of uncertainty in the assessment requiring a high level of precaution to be used, and illustrating this with the example of the application of the 70dB L_{Amax} noise threshold. The Applicant is aware that there are uncertainties in this assessment, but this is the case with any such assessment (and the level of uncertainty in the current assessment is not considered to be unusual or unreasonable in this regard). Specifically, in relation to the application of the 70dB L_{Amax} noise threshold, this is considered to be based upon the best available evidence (as detailed in **Sections 8.8 b) iv. and 8.8 d) v**. of the **Shadow HRA Report** [APP-145]), and there is a level of acknowledgement of this in the Written Representation (as noted above). Furthermore, considerable precaution has been incorporated into the assessment of noise and visual disturbance on foraging marsh harrier (e.g. by assuming that a barrier effect prevents birds from accessing the Sizewell Marshes and that the noise levels for the worst-case phase of construction (i.e. Phase 1) apply across the whole construction period).

Barrier effects on the Sizewell Marshes

1.2.14 RSPB/SWT outline their reasons in the Written Representation for agreeing with the approach adopted in the assessment of assuming the operation of a barrier effect across the main development site, preventing access to the Sizewell Marshes by marsh harrier from the Minsmere nesting area. This means that the assessment assumes that marsh harriers are displaced from the entire area of the Sizewell Marshes for the entire length of the construction period. Whilst this is the basis on which the assessment has been undertaken, for the purposes of context, it is important to recognise the extent of precaution incorporated in this approach. For example, whilst high levels of noise may (on a precautionary basis) be assumed to prevent birds from flying over the main development site, access to the Sizewell Marshes could still be gained via indirect flight routes. This is particularly the case during the later phases of construction when there is a marked contraction in the area of the main development site across which the highest noise levels (and hence a potential barrier to movement) extend - e.g. see **Figure 8A.3** in the **Shadow HRA Report Addendum** [AS-178].

1.2.15 The Written Representation also states that the monitoring of marsh harrier flight activity at Trimley Marshes provides no evidence from which inferences can be made on whether marsh harriers from Minsmere will continue to use the Sizewell Marshes during the construction period. On

the basis that the monitoring at Trimley Marshes demonstrates a potential for foraging marsh harrier to tolerate relatively high noise levels, this is patently not the case (although the Applicant agrees that it is not sufficient evidence from which to make a direct extrapolation to the situation on accessing the Sizewell Marshes) and, for precautionary reasons, the Applicant has not made this assumption.

Visual disturbance of marsh harriers foraging over the Minsmere South Levels and Sizewell Marshes

1.2.16 The RSPB/SWT Written Representation considers there to be insufficient evidence to support the adoption of the 150m potential visual impact zone (or visual disturbance buffer), suggesting this approach risks underestimating effects on foraging marsh harrier. The basis for determining the potential visual impact zone is detailed in paragraph 1.27 above.

v. Calculation of the compensatory requirement

Lack of compensation for loss of arable habitats

1.2.17 The RSPB/SWT Written Representation highlights concerns over the approach taken by the assessment to the potential displacement of foraging marsh harriers from arable foraging habitats, and particularly in basing the calculation of the foraging resource required to compensate the 'lost' foraging areas only on wetland habitats. The Written Representation states that the loss of arable foraging is likely to be important to this population due to the level of use of these areas shown by the Applicant's surveys and based on the literature. However, the assessment justifies this approach on the basis that:

- Arable (i.e. land cultivated for crop production), overall, represents low quality foraging habitats, which are of secondary importance to wetland habitats.
- There are extensive areas of arable habitats within foraging range of the Minsmere nesting area, so they are unlikely to be limiting (in contrast to the scarcer, higher quality, wetland habitats).
- Marsh harrier are known to be a generalist predator, capable of adapting their foraging behaviour to account for variation in habitat and prey availability, so that the loss of areas of relatively low foraging value can be counteracted via behavioural mechanisms (e.g. by modifying foraging

ranges to exploit alternative areas of arable habitat, increasing foraging effort or selecting different prey types).

1.2.18 In terms of the flight activity survey data, RSPB/SWT point to the relatively high levels of flight activity recorded on some of the arable HVAs, which it is stated are higher than on some of the wetland HVAs. Although true, this statement fails to acknowledge differences in the proximity of the HVAs to the nesting area, with proximity to the nesting area known to influence foraging activity by marsh harrier (Ref. 1.6). This is reflected in the survey data and, when proximity to the nesting area is accounted for, flight activity on the wetland habitats is estimated to be approximately twice that on arable habitats (**Plate 8.11** in the **Shadow HRA Report** [APP-145]).

1.2.19 The Written Representation also highlights the variability in the flight activity levels recorded in the different HVAs on arable habitat and suggests this may be due to differences in crop types, with the inference presumably being that some crop types may provide foraging habitat of similar quality to that of the wetland habitats. However, this again fails to take any account of differences in proximity to the Minsmere nesting area (whilst it is also highly selective in that the observation is made on the basis of data from only one of four years of survey - i.e. 2020). Two of the three HVAs on arable habitat with the highest levels of flight activity in 2020 (i.e. HVAs A and D) are the closest of the six such HVAs to the Minsmere nesting area, being immediately adjacent to the north-west of the Minsmere South Levels which (as discussed above) tends to be associated with particularly high levels of flight activity. Additionally, one of the two HVAs on arable habitats on which no flight activity was recorded in the 2020 surveys is the furthest such HVA from the Minsmere nesting area (see **Table 6.6** in the **Shadow HRA Report Addendum** [AS-173] and **Figures 6.3 – 6.7** in the **Shadow HRA Report** [APP-145]). Thus, as with the earlier survey data reported in the Shadow HRA, much of the variability in flight activity recorded on the arable HVAs in 2020 may be associated with differences in the proximity to the Minsmere nesting area.

1.2.20 It is of course the case that differences in crop type (along with other aspects of the land management regime) will contribute to variation in the value of arable habitats to foraging marsh harrier. However, overall, it is clear that within the foraging range used by the marsh harriers which nest at Minsmere, arable fields provide foraging habitat of considerably lower value than the wetland habitats. As detailed above, this is demonstrated by the flight activity survey data, whilst it is also supported by the evidence

from the literature which demonstrates preferences for foraging in wetland and other less intensively managed habitats (Ref. 1.6, Ref. 1.4).

1.2.21 Given the above, it is considered highly unlikely that marsh harriers from the Minsmere nesting area are limited by the availability of arable habitats as a foraging resource. It is considered likely that there is a more than sufficient abundance of arable habitats with the foraging range to mean that the displacement of foraging marsh harrier from some areas of arable will be relatively unimportant (in terms of effects on foraging efficiency and ultimately breeding success). Therefore, contrary to the position outlined by the RSPB/SWT Written Representation, it is considered that there are robust reasons for calculating the foraging resource which is required to compensate for the 'lost' foraging areas solely on the basis of the wetland habitats from which marsh harrier are predicted (on a precautionary basis) to be displaced.

Visual disturbance

1.2.22 The RSPB/SWT Written Representation reiterates the concerns they have in relation to the visual disturbance buffer and suggest this may result in underestimation of the compensatory habitat requirement. The basis for determining the potential visual impact zone (or visual disturbance buffer) and the associated justification is detailed in paragraph 1.27 above. Therefore, the Applicant considers that the potential visual impact zone which is used provides a suitable basis for estimation of the compensatory habitat requirement.

Compensatory requirement based on levels of flight activity

1.2.23 The RSPB/SWT Written Representations outline a concern over the estimation of the required compensatory habitat requirement solely on the basis of the flight activity levels, as opposed to also accounting for the absolute area of habitat which is estimated to be 'lost'.

1.2.24 The Applicant accepts the point made in the Written Representation that the flight activity metric does not give a perfect measure of the foraging resource for a particular habitat or area of land because it does not distinguish foraging flights from commuting flights and does not account for differences in foraging success. However, as detailed above, the flight activity data strongly suggest that broad habitat type (i.e. wetland vs arable) and distance from the Minsmere nesting area both affect the foraging value of an area, and this aligns with the known foraging ecology of the species (e.g. Ref. 1.6, Ref. 1.4). Therefore, it is clearly the case that these factors

need to be accounted for when considering the foraging resource that is 'lost' due to the potential displacement (and subsequently the requirement for compensatory habitat).

1.2.25 Given the above, a simple measure of the total area of the (potentially) 'lost' habitat is clearly not in itself a good measure of the actual foraging resource that is 'lost' (because the value of the foraging resource is also strong affected by the proximity to the nesting area). Therefore, the flight activity metric is considered to be the most appropriate means of estimating the actual foraging resource. It is accepted that the flight activity metric has certain limitations but it is the most robust available method of estimating actual foraging resource.

Residual loss of foraging resource

1.2.26 The RSPB/SWT Written Representation suggests that even "small" residual losses of the total wetland foraging resource could be important and take issue with the statement in **paragraph 8.8.254** of the **Shadow HRA Report** [APP-145] that "*it is considered that a small loss of wetland resource (less than 5%) would be unlikely to have an identifiable population impact"*, stating that because of the likely difficulty in assessing the performance of the compensation area the precautionary principle must be applied. On this basis, RSPB/SWT disagree with the statement *"that if displacement and (particularly) barrier effects operate at less than 100% then the overall functional replacement (and therefore compensation) requirement is also reduced"*, stating that it would not be appropriate to take active steps to reduce the extent of the compensation area in this instance due to concerns over the adequacy of the compensation area.

1.2.27 In relation to the above issue, it is important to recognise and understand the context. Whilst it is essential to apply the precautionary principle in such assessments, it is also important to retain a perspective on what is reasonable in terms of likely outcomes and underlying assumptions. Thus, given that the potential displacement from wetland foraging habitat is: (i) relevant to a proportion (i.e. *c.*50%) of the SPA marsh harrier population only (because only the birds which use the Minsmere nesting area are potentially affected); and (ii) importantly, is temporary (albeit potentially long-term) and not permanent, then it is reasonable (and also biologically realistic) to suggest that a "small" residual loss (<5%) of wetland resource is unlikely to have an identifiable impact on the (entire) SPA population.

1.2.28 Furthermore, the calculations presented in **Table 8.15** in the **Shadow HRA Report** [APP-145] of how changes in the assumed rate of displacement

and barrier effect operation affect the estimated foraging resource that would be 'lost' (and hence the compensatory requirement) are relevant, given the highly precautionary assumptions on which the assessment is based. These figures are presented for illustrative purposes and to provide greater context. As a point of detail, it is also undeniably true that if the displacement and (particularly) barrier effects were to operate at less than 100% (i.e. so some foraging still occurs in the Sizewell Marshes or within other areas encompassed by the 70dB L_{Amax} noise contour or visual disturbance buffer, albeit at reduced levels) then the overall functional replacement (and therefore compensation) requirement would also be reduced. The Applicant would emphasise that the calculations in **Table 8.15** in the **Shadow HRA Report** [APP-145], showing how the compensatory requirement changes with changes in the assumed rate of displacement and barrier effect operation, are presented to provide further context and not for the purpose of seeking to 'actively reduce the extent of the compensation area'.

vi. Ecological considerations for the design of the compensatory marsh harrier foraging habitat

Habitat preferences of foraging marsh harriers

1.2.29 The RSPB/SWT Written Representation provides an overview of marsh harrier foraging habitats, focussing on their use of arable and other agricultural habitats. In a general sense, the applicability and relevance of the findings which are reported is not contested, but an important consideration is that these findings relate largely to agricultural systems outside the UK. The management of arable crops in Suffolk (including within the vicinity of the Minsmere-Walberswick SPA (and Ramsar site)) is particularly intensive, with fields often large and with little margins or boundary habitats, and with plastic sheeting sometimes used to force crops. Therefore, a degree of care is required in extrapolating from these findings to the situation in the Minsmere area, particularly in relation to the details of foraging habitat selection and the extent of dependence on arable (or other agricultural) habitats for foraging relative to wetland (or other, similar, extensively managed) habitats.

1.2.30 With respect to foraging habitat preferences, the Written Representation also suggests that the potential displacement from wetland foraging habitats could have a disproportionately large effect on female marsh harriers. This is on the basis that females rely more heavily on wetland habitats and take relatively large prey, so that they may be less likely to exploit smaller prey more typical of (some) dry habitats. It is proposed that

this could reduce the provisioning of prey to older chicks (because the contribution of females to the provisioning of the chicks increases in older broods).

1.2.31 However, the evidence that the greater reliance of female marsh harrier on wetland habitats is due to the associated habitat conditions and prey types is limited and often anecdotal in nature (Ref. 1.7, Ref. 1.8). It is also possible that this greater reliance on wetland habitats could result, at least in part, from the fact that during the breeding season female marsh harriers tend to use smaller foraging ranges than males. As such, a greater proportion of their foraging range is likely to comprise wetland habitats because this is where nesting sites are usually located (as at Minsmere). Consequently, there is no strong basis for inferring that the compensatory habitat being created within the EDF estate will not provide suitable foraging opportunities to female marsh harriers. Furthermore, the managements being undertaken on the compensatory habitat will include the creation of a wetland area, and also encourage larger prey types (e.g. rabbits) as well as smaller prey types (see the **Marsh Harrier Compensation Area Design Update to Include Wetland** report [REP2-119]).

Habitat components of the proposed compensation area

1.2.32 The RSPB/SWT Written Representation sets out a view on each of the different habitat components proposed for inclusion in the compensation area. The Applicant notes that RSPB/SWT are broadly supportive of the inclusion of most of these.

1.2.33 A number of issues are raised in the Written Representation on some of the habitat components, as follows:

- *'Wet woodland should not be considered as part of the compensation for marsh harrier'*: Whilst it is acknowledged that the marsh harrier report indicates that trees should be avoided in the compensatory habitat design, the wet woodland will be in the early stages of establishment, and is likely to contain as much reed as alder, during much of the construction period. During the early stages of the construction period (first 3 - 4 years) the trees will be around the same height as reed and therefore it can be assumed that the wet woodland would function, in respect of marsh harrier foraging, in a similar way to reedbed. Once the trees grow taller, they will act in the same way as hedges and scrub foci to allow harriers to surprise prey species. As a result, the Applicant considers the inclusion of woodland will not detract from the

compensatory habitat provision during the 10 - 12 year construction period.

- '*The construction for the wetland component will not occur until the first winter of the construction period, so that the reedbed will not be established and functional during the early years and, over this period, will actually represent a loss in terms of the overall compensatory habitat provided. It is proposed that the construction for this component should occur prior to the main construction period commencing or else be removed from the calculation of the area of compensatory habitat':* The reason for building the wetland component in the winter is to ensure that there are no noise impacts to breeding marsh harriers during the excavation of the wetland. The commitment to building the wetland in the first winter is to ensure the wetland is created as soon as possible once consent is received. It is true that the proposed reedbeds would not be fully established in the subsequent summer. However, the wetland is expected to be a shallow open water body at this stage, with some limited marginal vegetation and will attract small numbers of waterfowl, waders as well as small passerines drinking on its margins. The waterbody will be in close proximity to tree belts (established and new plantings), and existing long grass areas providing ambush opportunities. The wetland would therefore provide valuable marsh harrier foraging habitat during this period. By the second summer, the reedbeds can be expected to be well established. In conclusion, it would be incorrect to state that the new wetland, even in its immature state, would be on no value to foraging marsh harriers.

- *'The open water of the water resource storage area will not provide suitable forage habitat: However, this is not relevant as the water storage area is no longer part of the proposed compensatory habitat design.'* No response is required. The water resource storage area was removed from the proposals in the January 2021 changes as acknowledged in this comment.

Conclusions regarding habitat components of the compensation area

1.2.34 The RSPB/SWT Written Representation suggests that the assumptions made in respect of numbers of rabbits that would potentially be supported by the compensatory habitat is over-estimated, and subsequently present a revised prediction of numbers of small mammals that would be present by habitat type and under the baseline and proposed Option 2b scenarios. In response to these points, the Applicant notes that:

- Wood (2019), and supporting appendices (notably Amec Foster Wheeler (2015)), sought to identify appropriate prey items for marsh harrier and then to define habitat types that could be created on site that would maximise provision and availability of these to marsh harrier, particularly during the marsh harrier breeding season. The report went on to summarise the likely existing baseline condition of the compensation site (recognising that it started out as a very intensively farmed landscape) and the likely uplift in small mammal and bird numbers with the compensatory habitats. However, with the objective being to maximise the numbers, the actual numbers used in the calculations of comparison are less important than agreement that the habitats are appropriate – and RSPB/SWT agree this is the case (as indicated in paragraph 3.430 of the Written Representations).

- The Written Representations highlight the availability of the Matthews (2018) publication and query why it wasn't used to inform likely changes in prey densities. However, the metric was developed in 2015/2016. It was therefore based on references available at the time and omission of reference to Matthews (2018) is therefore related to timing of development.

- In respect of comments in the Written Representation on possible densities of rabbits used to inform the metric:

    - The figure of 2.5 rabbits/ha on arable land used by Harris, 1995 (the source used to inform the work), is an average applied across the country. The Written Representation suggests that the average arable figure used by Harris of 2.5 rabbits/ha is appropriate. However, this does not account in this location for the very intensive arable farm management that took place on the compensatory area prior to the implementation of the habitat managements, which included use of plastic sheeting to force crops when needed, lack of buffer strips and large field sizes (therefore limiting boundary habitat availability). Hence, the use of a lower baseline range for rabbit density of 0-1/ha for arable.

    - A similar situation exists with the use of a figure of 2.5 rabbits/ha for lowland grassland, which again is an average applied across the country. However, Harris also presents information indicating much higher densities than this in some locations and habitats, and given the presence of an

apparently high (although unquantified) density of rabbits present on short grassland immediately adjacent to the compensation area (Black Walks), it was considered reasonable to assume a significant increase in rabbit density would be achieved on site, by providing appropriate grassland habitat and associated cover (scrub foci and banks). Hence a range of 10-15/ha is assumed, which is within ranges stated by Harris for short grassland types elsewhere.

- Therefore, the Applicant does not agree that the ranges, and therefore the potential uplifts, are overly optimistic.

- In respect of comments in the Written Representation on possible densities of small mammals used to inform the metric:

  - In Table 4 in the Written Representation, in relation to rabbit densities per habitat type, there appears to be an error in that the figures published by Matthews for rabbits in short (improved) grassland are actually 0.48 (0.26-6)/ha, not 0.48 (0.26-0.6)/ha. When the upper range figures for the species quoted are summed therefore the figure is 11.93 small mammals (much higher than the 3.9 small mammals/ha that RSPB/SWT state, and much closer to the figures used in Wood (2019)).

  - In paragraph 3.444 of the Written Representation, it is stated that the numbers used for small mammals in Wood (2019) appear high relative to Matthews (2018), particularly in relation to the tussocky grassland and hedgerows. It should be noted that the Matthews (2018) figures for tussocky grassland and hedges are averages from a number of published studies, whilst those adopted by Wood also reflect published data. Both are therefore correct although it is recognised than an average figure is likely to be lower. If the upper range figures are summed in Table 4 of the Written Representation for tussocky grassland, the total is 92.76 small mammals/ha which is much closer to the figures used in Wood (2019). In respect of the hedgerows, the estimate adopted by Wood was based on mark-release-recapture data collected from the Sizewell estate and is therefore considered an appropriate data source to use for this study as an indicator of what can be achieved.

- Table 6 in the Written Representation highlights an inconsistency in the Wood (2019) report in respect of the number of rabbits used in the assessment for short grassland. The text in Appendix B and calculations in Appendix C use 15-20 rabbits/ha for short grassland. However, there is also reference to 10-15/ha in Appendix C. This is an error but whichever is used it does not change the overall result of the assessment in Wood (2019), that Option 2a/2b provide the greatest number of prey items for marsh harriers.

Predictions of uplift in flight activity

1.2.35 The RSPB/SWT Written Representation outlines concerns that the 48.7ha of compensatory habitat within the EDF estate will be insufficient to replace the potential 'loss' of c.100ha of wetland habitat as a result of the possible displacement of foraging birds. However, as detailed above, proximity to the nesting area has a strong effect on the extent to which marsh harrier use different areas of foraging habitat (**Plate 8.11** in the **Shadow HRA Report** [APP-145]). The Sizewell Marshes, which comprise the bulk of the 'lost' wetland foraging habitat, are at a distance of 2 – 4km from the Minsmere nesting area, whereas the compensatory habitat is only <1 – 2km from the Minsmere nesting area (**Table 8.12** in the **Shadow HRA Report** [APP-145]). Given that the managements being imposed on the compensatory habitats are predicted to provide highly suitable foraging conditions for marsh harrier, then it is reasonable to expect that this smaller area of habitat can provide sufficient foraging resource to replace the wetland foraging habitat that will (potentially) be 'lost'.

1.2.36 Although the level of flight activity that is estimated to be required on the compensatory habitat is greater than the average values for the Sizewell Marshes and Minsmere South Levels, importantly, it is well within the range of values that are recorded from the north-central parts of the Minsmere South Levels which are immediately adjacent to the area of compensatory habitat (see **paragraphs 8.8.247 – 8.8.253** and **Figures 6.3 to 6.5** in the **Shadow HRA Report** [APP-145], [APP-146]). On this basis, it is again reasonable to expect that the compensatory habitat can provide the foraging resource that is estimated to be required.

1.2.37 The rationale and justification for the approach taken to the arable foraging habitat and its exclusion from the estimated replacement foraging resource has been set out above.

vii. Additional constraints on the functionality of the compensatory habitats

1.2.38 The RSPB/SWT Written Representation highlights a number of factors that are considered to constrain the functionality of the compensatory habitat, notably:

- Additional visual disturbance because the Eastbridge to Minsmere footpath passes through the northern extremity of the area.
- Construction noise levels, which result in encroachment of the 70dB L_{Amax} threshold noise level onto parts of the compensatory habitat, particularly during Phases 1 and 2.
- An additional stockpile up to 15m above ground level to be located adjacent to the compensatory habitat.
- Noise levels associated with construction of the water storage area and flood mitigation measures during the first winter of the construction period (in particular, the risk of these works over-running and extending into the start of the breeding season).
- Timing of functionality, in particular the need to demonstrate that the implemented habitat measures are sufficiently established to provide the required level of prey provisioning by the time construction commences.

1.2.39 In relation to the above points, users of the Eastbridge to Minsmere footpath are not likely to cause any disturbance effect on marsh harrier or detract from the use of the compensatory habitat as a foraging resource due to the very low visual and noise intrusion associated with footpath use.

1.2.40 The extent of encroachment of the 70dB L_{Amax} noise threshold onto the compensatory habitat area is likely to be considerably less than as indicated by the noise modelling undertaken for these Phases when considered in their entirety (and as shown **Figure 8.3** of the **Shadow HRA Report** [APP-147] and **Figure 8A.2** of the **Shadow HRA Report Addendum** [AS-178]). This is on the basis of the modelling of noise undertaken at finer temporal resolution than the individual construction phases (e.g. at intervals of individual weeks or months), as detailed in **paragraphs 8.8.188 and 8.8.189** of the **Shadow HRA Report** [APP-145] (see also **Figure 8.9** in the **Shadow HRA Report** [APP-148]). It is noted that the RSPB/SWT Written Representation expresses concerns over the validity of modelling noise at this finer resolution but as argued in **paragraphs 14.5.12 to 14.5.15** of the

Applicant's **Comments on Written Representations** submitted at Deadline 3 [REP3-042], this further modelling is considered to be a reasonable estimate of the likely noise levels, given the stage of the project's life. Therefore, the extent of encroachment of the 70dB L_{Amax} noise threshold onto the compensatory habitat area will be limited and is expected to have little effect on its functionality.

1.2.41 With respect to the additional stockpile, **Volume 1 Environmental Statement Addendum Chapter 2 Main Development Site** [AS-181] confirms that construction activities and plant used would remain as reported in Volume 2, Chapter 11 of the ES, and the works associated with the additional stockpile would have no material effect on the conclusion of the noise assessment.

1.2.42 Construction of the water storage area and flood mitigation measures will not extend beyond February. In the event of any delays to these works they would be completed during the second winter of the construction period. Thus, in terms of the predicted noise levels for Phase 1 of the construction period, these are as shown in **Figure 8.3** in the **Shadow HRA Report** [APP-147].

1.2.43 Further information on the functionality of the compensation habitat and its sufficiency was provided at Deadline 2 (Bio. 1.48 in **Responses to the Examining Authority's First Written Questions, Volume 3** [REP2-110]).

2 REFERENCES

Ref. 1.1 Musgrove A., Aebischer N., Eaton M., Hearn R., Newson S., Noble D., Parsons M., Risely K. and Stroud D. (2013). Population estimates of birds in Great Britain and the United Kingdom. British Birds, 106, 64-100.

Ref. 1.2 Woodward, I., Aebischer, N., Burnell, D., Eaton, M., Frost, T., Hall, C., Stroud, D.A. & Noble, D. (2020). Population estimates of birds in Great Britain and the United Kingdom. British Birds, 113, 69–104.

Ref. 1.3 Madders, M. and Whitfield, D.P. (2006) Upland raptors and the assessment of wind farm impacts. Ibis, 148, 43-56.

Ref. 1.4 Alves, M., Ferreira, J.P., Torres, I., Fonseca, C. and Matos, M. (2014) Habitat use and selection of the marsh harrier *Circus aeruginosus* in an agricultural-wetland mosaic. Ardeola, 61, 351-366.

Ref. 1.5 Ruddock, M. and D. P. Whitfield, D.P. (2007) A review of disturbance distances in selected bird species. Report to SNH by Natural Research (Projects).

Ref. 1.6 Cardador et al. (2009) Short communication: Ranging behaviour of Marsh Harriers *Circus aeruginosus* in agricultural landscapes. Ibis, 151, 766-770.

Ref. 1.7 Clarke, R. The Marsh Harrier. Hamlyn Species Guides. Hamlyn, 1995.

Ref. 1.8 Witkowski, J. Breeding biology and ecology of the Marsh Harrier (*Circus aeruginosus*) in the Barycz Valley, Poland. Acta Ornithologica, 1989, 25(3), p. 223–320.

APPENDIX N

EVENING NOISE AND BIRD DISTURBANCE

CONTENTS

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1 RSPB AND SWT COMMENT

1.1.1 The RSPB and SWT Written Representation raised the following concern related to the definition of the daytime and night time periods:

> *"…assessment scenarios have been defined separately for daytime (07:00–23:00hrs) and night-time (23:00–07:00hrs) construction. However, this means that "daytime" will include a significant proportion of dark hours particularly in winter. With full construction activities ongoing until 11pm, we are concerned regarding the potential for ecological impacts of noisy activities during dark hours – e.g. potential displacement of birds arriving to roost. Impacts under the daytime scenario could therefore be greater than predicted.*
>
> *For ecological receptors 'day' is dawn to dusk and 'night' is dusk to dawn. Assessing impacts during those time periods would therefore be more relevant".*

1.1.2 The rationale behind the statement that assessment during the 'dawn to dusk' and dusk to dawn' period is more relevant is not clear from the RSPB/SWT comment. However, in this response, we understand that the RSPB/SWT's justification for this statement is that the higher 'daytime' construction noise levels will encompass hours of darkness when the baseline (ambient) noise levels are potentially lower and, as a consequence, birds may be more sensitive to construction noise with the implication that the noise disturbance thresholds applied in the **Shadow HRA Report** [APP-145] may not be appropriate for use in assessing the effect of construction noise in the dusk to dawn period.

1.1.3 To investigate the comment raised by RSPB/SWT, an analysis of the baseline noise levels has been undertaken at a number of noise monitoring locations in and adjacent to the Minsmere-Walberswick Special Protection Area (SPA) and Ramsar site, Minsmere South Levels and Sizewell Marshes Site of Special Scientific Interest (SSSI) which coincide with the areas where construction noise is predicted at levels which could cause disturbance to birds (see **section 2**) and/or which are representative of the baseline noise environment at sensitive locations.

2 ANALYSIS OF BASELINE NOISE LEVELS

2.1.1 Baseline noise levels are reported in **ES Volume 2 Appendix 11A Noise and Vibration Baseline Report** [APP-203]. The results of the noise monitoring over the daytime and night time period reported in that document [APP-203] for locations MS3, MS8, MS9 and MS17 have been analysed. These locations are shown in Figure 11A.5 in **ES Volume 2 Appendix 11A Noise and Vibration Baseline Report** [APP-203].

2.1.2 A summary of the noise monitoring data, including supplementary comment on sources contributing to the noise environment at each location, is provided in **Table 2-1**.

2.1.3 It can be seen from **Table 2-1** that the noise environment is similar between the daytime and night time periods for the noise monitoring locations within the Minsmere South Levels, Minsmere-Walberswick SPA and Ramsar site and Sizewell Marshes SSSI. The noise surveyors noted that where the baseline noise levels did decrease over the night time, it was generally because natural sounds (sea, wind/leaves and bird song) decreased.

2.1.4 One of the key areas of concern is Sizewell Marshes SSSI because, as reported in the **Shadow HRA Report** [APP-145], the likely noise level threshold at which a potentially adverse behavioural response could be initiated for wintering waterbirds (70dB L_{Amax}, with a value of 65dB L_{Amax} assumed for breeding waterbirds) encompasses a substantial part of the Sizewell Marshes. Encroachment of the 70dB LAmax footprint onto the Minsmere-Walberswick SPA and Minsmere South Levels is minimal during all construction phases (and restricted to the southern extremities of these areas). Monitoring location MS17 is representative of Sizewell Marshes and, at this location, there is no difference between baseline daytime and night time noise levels.

2.1.5 Further analysis of the pattern in change in baseline noise throughout the daytime and night time period in relation to the time of sunset has been undertaken for monitoring locations MS8 and MS9 (MS3 has been excluded because night time noise levels were recorded to be slightly higher than daytime levels, and MS17 has not been further analysed because, as reported above, there was no difference in noise levels between daytime and night time).

Table 2.1: Summary Of Baseline Noise Monitoring At Relevant Locations

Receptor Reference	Ambient Sound Level (day) (L_{Aeq}, dB)	Ambient Sound Level (night) (L_{Aeq}, dB)	Comment	Monitoring Period
MS3 (Leiston Old Abbey)	38	40	The sound climate was comprised of occasional people walking past on footpath, horses, cows, insects, birdsong from various species, distant shotguns and occasional overhead aircraft. At times a gentle breeze was noted through the reeds, and the sea on the shingle beach in the distance.	September and November, 2014
MS8 (Abbey Marshes)	45	35	The sound climate was comprised of the sea, birdsong from various species, occasional aircraft, distant industrial noises including reversing alarms and a distant hum from Sizewell B station.	August 2014
MS9 (Coast Path North)	43	41	The sound climate was comprised of the sea, birdsong from various species, occasional aircraft, walkers talking and general site activity at Sizewell B station.	August 2014
MS17 (Sizewell Marshes East)	40	40	The sound climate was comprised of birdsong from various species, insects, occasional aircraft, walkers, barking dogs, distant construction activity and a distant hum from Sizewell B station.	August 2014

2.1.6 Noise monitoring as MS8 and MS9 was undertaken over various dates in mid to late August 2014; in mid-August 2014, sunset at Sizewell was at approximately 20:15. The noise monitoring data for locations MS8 and MS9 show a decrease in baseline noise levels between approximately 21:30 and 22:00, indicating that baseline noise levels in the dusk period leading up to sunset and for at least an hour after sunset are comparable with the noise levels throughout the daytime.

3 CONCLUSION

3.1.1 The following conclusion can be drawn on the basis of the analysis of baseline in this note:

- There is no material difference between daytime and night time noise levels at locations within the Minsmere South Levels, Minsmere-Walberswick SPA and Ramsar site and Sizewell Marshes SSSI.
- A key areas of concern is Sizewell Marshes SSSI; monitoring at this location shows there is no difference between baseline daytime and night time noise levels.
- Where there is a difference between daytime and night time baseline noise levels, this is generally due to a fall-off in natural sounds; changes in sounds of this nature are not likely to affect bird behaviour or change the sensitivity of birds to other sources of sounds, such as construction noise.
- Observed declines in noise level at two of the monitoring locations occur at least 1 hour after the time of sunset, indicating that noise levels preceding, and immediately following, sunset are comparable with those prevailing throughout the daytime.

3.1.2 Given there are no substantive differences between daytime and night-time baseline noise levels, the change in noise levels which would be experienced by birds on the MSLs, arising from same construction activities, whether these are prior to and after dusk, would be the same.

3.1.3 There is no evidence to suggest that birds would be more sensitive to construction noise over the night time period compared with the daytime period in the key areas used by waterbirds around the main development site.

3.1.4 Consequently, there is no reason to suggest that a different disturbance threshold should be applied in the assessment of effects of noise disturbance on qualifying bird species in the period after dusk (i.e. evening or night time), regardless of the timing of that period throughout the year.

APPENDIX O

RESPONSE TO RSPB AND SWT ON BNG

1 BIODIVERSITY NET GAIN RESPONSE TO RSPB AND SWT

1.1.1 The table below provides a response to the points raised within Section 5 of the RSPB and SWT joint Written Representation [REP2-506] on biodiversity net gain (BNG).

Para No.	Paragraph text	SZC response
5.1	Our concerns relate to the Applicant's approach to biodiversity net gain (BNG).	N/A
5.2	Whilst we welcome the Applicant including BNG within their proposals, despite the introduction of BNG within the Environment Bill not yet being a specific requirement (due to the Bill having not passed nor the further work required to establish a BNG system) we do not agree the Application can achieve net gain due to direct adverse impact on Sizewell Marshes SSSI from loss of a significant proportion of the SSSI, nor the amount claimed by the Applicant.	The calculations demonstrate an increase in biodiversity units post development. In the most recent calculations, this distinction is clear, with an increase in biodiversity units highlighted, the client is not claiming 'biodiversity net gain' as a statutory requirement but to evidence the efficacy of the mitigation, compensation and enhancement proposed. Sizewell Marshes SSSI has been excluded from the calculation.
5.3	We are grateful to the Applicant for the discussions held and agree that the Application should take account of the requirements the new net gain system will include once established.	We will consider the value of undertaking additional work using the Biodiversity Metric 3.0 published in July 2021.

Para No.	Paragraph text	SZC response
5.4	In addition there is a Natural England requirement for NSIPs to contribute significantly to environmental net gain[451]. As such, the Application should be demonstrating a high biodiversity metric score that does not rely on protected species mitigation and compensation measures to get over the 10% uplift requirement.	Whether habitats are designed for mitigation for protected species or not this does not limit these habitats potential to deliver environmental net gain. The biodiversity unit uplift is based on the before and after status of the site post development. The **outline Landscape and Ecological Management Plan** (**oLEMP**) [REP1-010] ensures that the habitat distinctiveness and quality predicted by the biodiversity metric can and will be delivered.
5.5	The biodiversity metric 2.0[452] used for the assessment is a consultation draft that contains software bugs and grey areas. The Applicant is currently taking full advantage of all grey areas to increase the metric score including revised baselines, use of measures that are for protected sites and species mitigation and compensation, heavy use of 'fairly good' category whilst ignoring limitations and trading down. The choices made have in each case increased the claimed BNG.	The latest version of the Biodiversity Metric was used to carry out the calculations. Allowances were made for any bugs within the metric. The use of 'fairly good' and the inclusion of all areas is discussed in the response to paragraph 5.6.

5.6 bullet point 1	Our main concerns include: • use of measures that are for protected sites and species mitigation and compensation	This is a misunderstanding regarding the biodiversity unit assessment process. The biodiversity unit assessment process is a habitats driven method to demonstrate the impact of a development on biodiversity. It assesses the site before and after the proposed development and uses the metric to demonstrate a net change in biodiversity. Species and habitat receptors have also been assessed individually within the Environmental Statement. The biodiversity unit assessment using the metric does not replace these assessments, rather it complements it. Nor does it replace legal or policy obligations, it is merely a means of quantifying change with regards to overall biodiversity. The RSBP/SWT response (taken from the draft Environment Bill) supports the position that dedicated mitigation to discharge legal and policy requirements is additional but this does not mean that this mitigation cannot then be included within the biodiversity unit calculation. What it is saying is that even if the developer demonstrates net gain that the legal and policy requirements with regards to species and habitats still remain: *"The biodiversity metric does not address impacts on species, recognise the significance of site designations, take account of indirect impacts, cumulative impacts or in combination impacts. In recognition of these limitations, the biodiversity net gain requirement for development on such sites is*

Para No.	Paragraph text	SZC response
		additional to any existing legal or policy requirements for statutory protected areas and their features, including restoration and conservation of designated features and the achievement of favourable conservation status and favourable condition. These requirements will need to be dealt with separately by the developer and planning authority."

Para No.	Paragraph text	SZC response
5.6 bullet point 2	• the baseline policy is directly at odds with the biodiversity gain system to be introduced by the Environment Bill	The biodiversity unit assessment is a habitat centric metric for demonstrating change in biodiversity. It assesses the site before and after proposed development and (except for non-tradable habitats) includes all habitats before and after proposed development. Areas for mitigation, compensation and enhancement are designed to benefit a range of species and ideally to maximise ecosystem service benefits. They are not compartmentalised into a single area for reptiles, a single area of bats and so on. In protected species licences elements of mitigation proposed need to demonstrate that they will deliver favourable conservation status for European Protected Species. The carrying capacity of the habitat is assessed to ensure that it does deliver, multiple species are likely to coexist in these habitats. The same habitat may also deliver mitigation, compensation or enhancement commitments made in the ES. This is not double or triple counting, the biodiversity unit assessment merely demonstrates the overall status of the site before and after development with regards to the distinctiveness, extent and quality of the habitats.

Para No.	Paragraph text	SZC response
5.6 bullet point 3	• the time for habitats to reach target condition (temporal risk) does not take account of the construction phase	The calculation has been undertaken as per the guidance within the metric calculator for all habitats. For example, where habitats have been created in advance and are matured, neither the time to target condition nor the risk has been reduced or eliminated. Similarly, the time to target condition has not been altered where there is to be a delay in their creation. The Biodiversity Metric is designed to assess the baseline and end states of developments. The protected species licensing, legislation and ES ensures that the habitat is suitable to deliver the legal and policy requirements. Therefore, while developers are not penalised for creating habitats ahead of time, under the current biodiversity unit assessment guidelines using the biodiversity metric, nor do they benefit from the reduced risk and time to target condition that these advance works achieve. They are treated the same in the metric even though this does provide greater earlier benefit for biodiversity.

Para No.	Paragraph text	SZC response
5.6 bullet point 4	• the replacement of higher biodiversity habitats with those of lower biodiversity (trading down)	Habitat receptors have also been assessed within the Environmental Statement. The proposals target the improvement of the quality of habitats across the development. For example, the replacement of lost (largely plantation) woodland with woodland of higher quality, along with the replacement of the arable dominated landscape with the dry sandlings grassland habitat (acid grassland and heathland mosaic).
5.6 bullet point 5	• lack of evidence to support the likelihood of delivering the predicted on-site habitat conditions on post-construction soils	The **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective. The **outline Soil Management Plan** [REP3-018] provides details of how soil restoration is to provide soil profiles suitable for the reinstated land use.

Para No.	Paragraph text	SZC response
5.6 bullet point 6	• lack of evidence to support the likelihood of delivering the predicted off-site habitat conditions post development	The **oLEMP** [REP1-010] outlines the management required to deliver the targeted habitats post development. This will be evolved throughout scheme delivery and updated with monitoring results. Habitats have been designed for the ability of the site to support them from a soil, climate and biodiversity perspective.
5.6 bullet point 7	the % net change in the metric score is calculated versus the on-site baseline but it should be calculated versus the total on-site plus off-site baseline	In the Biodiversity Metric 2.0. the offsite baseline is included for calculating the unit uplift for the offsite habitat. However, when the final percentage uplift is expressed as net gain for the offsite enhancement the metric uses the total offsite uplift rather than the net change. The calculations were carried out using the Biodiversity Metric 2.0 and the appropriate guidance for that. The results are presented directly from this. The equation used by the Biodiversity Metric 2.0 is shown below. $$Change = \frac{Unit\ change\ on-site + Unit\ change\ off-site}{On-site\ baseline}$$

Para No.	Paragraph text	SZC response
5.6 bullet point 8	• the biodiversity value of existing habitats has not been adequately considered and taken account of heavy use of 'fairly good' category	Surveys have been carried out of the Sizewell Estate for many years, with large amounts of habitat and protected species data collected. Designs for mitigation and compensation were based on enhancing the existing habitats for the species that they support. Detailed condition assessments of existing habitats have also been undertaken. The proposals target the improvement of the quality of habitats across the development. For example, the replacement of lost (largely plantation) woodland with woodland of higher quality, along with the replacement of the arable dominated landscape with the dry sandlings grassland habitat (acid grassland and heathland mosaic).

Para No.	Paragraph text	SZC response
5.6 bullet point 9	• heavy use of 'fairly good' category	The 'fairly good' condition assessment has been used when considered appropriate, predominantly with regard to target habitat conditions. This assessment largely reflects the balance between having high aspirations with regards to the distinctiveness and target condition of post development habitats while ensuring that the assessment has contingency for delivery, that is the assessment does not predict high quality habitats achieving an extremely high biodiversity unit score using the biodiversity metric that may not be achievable. In practice the best quality habitat will be targeted but "fairly good" has been predicted and measured to derive the post development biodiversity units.
5.7	We consider the key finding from the Applicant's BNG proposals to be at best only just over the 10% boundary by a narrow margin, and that if any one of several marginal decisions were reversed it would fall below it. Therefore it is our view that the Application is not making the ecological contribution claimed nor that is proportional to the size of it - at best it is providing no more than the minimum standard expected of any housing development[453 454].	The rationale behind the assumptions is presented within the BNG reports and accompanying BM2.0 calculator. The BNG reports assessed the landscape design to be delivered by the **oLEMP** [REP1-010]. The results demonstrate its positive impact.

Para No.	Paragraph text	SZC response
5.8	We also consider it important to note the biodiversity metric is not suitable for tracking ecological delivery over time - it is designed to be a one-time snapshot of future commitments at the point of the planning application and does not work as a tracking tool (e.g. the score will rise over time even if condition targets are missed).	The **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective. This will be evolved throughout scheme delivery and updated with monitoring results.
5.9	We are also concerned the Applicant does not appear to have identified a legal mechanism for securing a 10% metric score in their mitigation strategy.	The end state habitats which have been assessed in the BNG reports are based on the masterplans for the four individual sites. The habitats for these are secured for the Sizewell link road and two village bypass by the **oLEMPs** for those roads (Doc Ref. 8.3 A(A) and Doc Ref. 8.3 B(A)). The end state habitats for the main development site, within the proposed order limits, are secured within the oLEMP whilst those outwith the order limits will be secured via the Estate Wide Management Plan (EWMP). The EWMP will be submitted to examination at Deadline 6

Para No.	Paragraph text	SZC response
5.10	We have engaged with the Applicant throughout the pre-application and pre-examination period. We reviewed the now superseded Biodiversity Net Gain report[455] for the main development site (MDS) submitted with the DCO application and expressed our concerns in our relevant representations [RR-1059 (RSPB) and RR-1180 (SWT)].	Additional responses are provided within this report. Responses to the written representations are provided in Table 4.19 of the **Relevant Representation Report** [REP1-013].
5.11	We have reviewed the net gain reports for the main development site[456], two village bypass[457] and Sizewell C Link Road[458] submitted at Deadline 1 and are pleased that some of our concerns around methodology have been addressed. We outline our current position below.	Please see the responses below in relation to comments on those biodiversity net gain reports submitted at Deadline 1.
5.12	Whilst the RSPB and SWT are fully aware of how the Environment Bill[459], will introduce a requirement for BNG, currently that legislation is not passed and there is a good chance it will not have done so by the time this Examination closes. In addition, the Bill purely introduces a framework for a BNG system and much more is needed before that system can get up and running.	It is acknowledged that the BNG system is currently being developed. However, the **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective. This will be evolved throughout scheme delivery and updated with monitoring results.

Para No.	Paragraph text	SZC response
5.13	For these reasons we would suggest that reference to the Bill (for example paragraph 1.5.2 of the Biodiversity Net Gain Report[460]) is premature. However it is useful to consider how BNG is described within it and its helpful explanatory notes. For example, at paragraph 1575[461] of the Bill's explanatory notes broadly excludes any development from BNG if it has a direct adverse impact on a protected site *Whilst it is generally agreed in practice that development cannot claim biodiversity net gain in cases when development results in land take from statutory protected sites (such as Sites of Special Scientific Interest, Special Protection Areas, Special Areas of Conservation, and Ramsar sites), development on such sites is not specifically exempted from the net gain requirement.*	The Biodiversity Unit calculations and demonstration of biodiversity net gain using the metric were carried out to demonstrate the biodiversity value of the post development site and the efficacy of the mitigation proposed. The Sizewell Marshes SSSI and any mitigation and/ or compensation relating to them were excluded from the calculation.

Para No.	Paragraph text	SZC response
5.14	The Bill[462] at paragraph 1575 of its explanatory notes[463] also notes the biodiversity net gain requirement for development on such sites is additional to any existing legal or policy requirements for statutory protected areas and their features *The biodiversity metric does not address impacts on species, recognise the significance of site designations, take account of indirect impacts, cumulative impacts or in combination impacts. In recognition of these limitations, the biodiversity net gain requirement for development on such sites is additional to any existing legal or policy requirements for statutory protected areas and their features, including restoration and conservation of designated features and the achievement of favourable conservation status and favourable condition. These requirements will need to be dealt with separately by the developer and planning authority.*	It is acknowledged that BNG is separate from existing legal and policy requirements. The biodiversity unit assessment process is a habitats driven method to demonstrate the impact of a development on biodiversity. It assesses the site before and after the proposed development and uses the metric to demonstrate a net change in biodiversity. Species and habitat receptors have also been assessed individually within the Environmental Statement. The biodiversity unit assessment using the metric does not replace these assessments, rather it complements it. Nor does it replace legal or policy obligations, it is merely a means of quantifying change with regards to overall biodiversity.

Para No.	Paragraph text	SZC response
5.15	The Overarching National Policy Statement for Energy (EN-1)[464] also notes at paragraph 5.3.11 where proposed development is likely to have an adverse effect on an SSSI development consent should not normally be granted *Where a proposed development on land within or outside an SSSI is likely to have an adverse effect on an SSSI (either individually or in combination with other developments), development consent should not normally be granted. Where an adverse effect, after mitigation, on the site's notified special interest features is likely, an exception should only be made where the benefits (including need) of the development at this site, clearly outweigh both the impacts that it is likely to have on the features of the site that make it of special scientific interest and any broader impacts on the national network of SSSIs. The [PINs] should use requirements and/or planning obligations to mitigate the harmful aspects of the development and, where possible, to ensure the conservation and enhancement of the site's biodiversity or geological interest.*	The assessment of the impacts to the Sizewell Marshes SSSI is presented separately to the BNG calculations. The Sizewell Marshes SSSI and any mitigation and/ or compensation relating to them were excluded from the calculation. The mitigation and compensation provided for the SSSI is presented in the **ES** and in the dedicated **Fen Meadow Strategy** [AS-209]

Para No.	Paragraph text	SZC response
5.16	As outlined in the SSSI loss section above we do not agree the Applicant has demonstrated compliance with all legal and policy requirements for justification of the principle and scale of the proposed loss of part of Sizewell Marshes SSSI against the policy tests set out in EN-1 (Overarching NPS for Energy).	The assessment of the impacts to the Sizewell Marshes SSSI is included in the Environmental Statement as is presented separately to the Biodiversity Unit calculations. The Sizewell Marshes SSSI and any mitigation and/ or the habitats compensation measures relating to the landtake of habitats to them were excluded from the calculation.. The compensatory habitat measures provided for the SSSI are presented in the ES and in the dedicated **Fen Meadow Strategy** [AS-209] and **Wet Woodland Strategy** [REP1-020].

Para No.	Paragraph text	SZC response
5.17	Although the National Planning Policy Framework*465* (NPPF) (2019) does not contain specific policies for nationally significant infrastructure projects it does note at paragraph 170 that planning decisions should minimise impacts on and provide net gains for biodiversity *Planning policies and decisions should contribute to and enhance the natural and local environment by:* …. *d) minimising impacts on and providing net gains for biodiversity, including by establishing coherent ecological networks that are more resilient to current and future pressures;* and at paragraph 175 notes opportunities to secure measurable net gains for biodiversity should be encouraged *When determining planning applications, local planning authorities should apply the following principles:* *d) opportunities to incorporate biodiversity improvements in and around developments should be encouraged, especially where this can secure measurable net gains for biodiversity.*	The Biodiversity Unit calculations demonstrate an increase in biodiversity unit value within the site. Impacts to biodiversity have been minimised where possible through the landscape design. The **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective.

Para No.	Paragraph text	SZC response
5.18	BNG Good Practice Principles for Development466 notes at section 9.5 that projects affecting statutory designated sites cannot achieve BNG *Projects negatively affecting statutory designated sites or irreplaceable habitats cannot as a project achieve BNG.*	*Please see response to paragraph 5.2.*
5.19	We do not agree the Application can achieve net gain due to direct adverse impacts on Sizewell Marshes SSSI from loss of a significant proportion of the SSSI. Despite this, we agree the Application should be meeting the requirements of the net gain system and our comments below are in relation to that achievement.	*Please see response to paragraph 5.2.*
5.20	Annex C to the Planning Inspectorate Advice Note 11467 notes *Natural England will seek opportunities for positive environmental outcomes from major infrastructure developments. NSIPs can make a significant contribution to delivering the environmental ambition in the Government's 25 Year Environment Plan (25YEP). This aims to deliver an environmental net gain through development and infrastructure.*	The Biodiversity Unit calculations demonstrate an increase in biodiversity unit value within the site. Impacts to biodiversity have been minimised where possible through the landscape design. The **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective.

Para No.	Paragraph text	SZC response
5.21	The Defra Biodiversity Offsetting Pilots guidance468 at paragraph 17 notes Offsetting should: • *contribute to enhancing England's ecological network by creating more, bigger, better and joined areas for biodiversity (as discussed in Making Space for Nature[469])*	The landscape design will increase the quality of habitat present on the site (from its largely agricultural baseline state), with efforts made to retain or improve connectivity where at all possible. The Biodiversity Unit calculations demonstrate an increase in biodiversity unit value within the site. Impacts to biodiversity have been minimised where possible through the landscape design. The **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective.

Para No.	Paragraph text	SZC response
5.22	BNG Good Practice Principles for Development[470] states at Technical Note T5 section T5.2 projects of national significance should focus on landscape scale net gains *Projects of national significance should underpin and support the delivery of UK and devolved government biodiversity commitments and should focus on landscape scale net gains and a contribution to national biodiversity targets.*	The landscape design takes a landscape scale approach, considering the wider landscape context around the EDF estate. The design aims to improve the connectivity between surrounding areas of value. The Biodiversity Unit calculations demonstrate an increase in biodiversity unit value within the site. Impacts to biodiversity have been minimised where possible through the landscape design. The outline **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective.

Para No.	Paragraph text	SZC response
5.23	Therefore the Application's BNG proposals should be focusing on landscape scale net gains and providing a functional ecological mosaic/ecotone and improving the actual ecological functionality of the surrounding area. We also query whether there may be opportunities for net gain habitat enhancements to provide habitat for protected species of bats, birds (barn owl[471], turtle dove, stone curlew, nesting terns), mammals and invertebrates.	Species receptors are assessed in the relevant section of the ES, separately to the BNG assessment. The landscape design provides an increase in the quality of habitat on site. For example, the shift from a largely arable landscape to one dominated by the dry sandlings grassland community. The woodland creation targets a more biodiverse woodland than the largely plantation woodland currently present. Habitat receptors are assessed in the relevant section of the ES. The Biodiversity Unit calculations do not supersede these assessments. However the Biodiversity Unit calculations demonstrate an increase in biodiversity unit value within the site. Impacts to biodiversity have been minimised where possible through the landscape design. The **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective.

Para No.	Paragraph text	SZC response
5.24	Table 13 of the Biodiversity Net Gain Report[472] shows arable and amenity planting provide 106.8 biodiversity units, against 758.76 total for the main development site post development. It would be expected that habitat creation would focus on maximising biodiversity and we query the inclusion of significant areas of low ecological value habitats in the metric score. If arable land is to be created, we request inclusion in highest tier agri-environment scheme or a similar commitment to biodiversity enhancements such as field margins and hedgerow management.	The arable land shown for the end state is largely land being returned to its baseline state which is owned by third parties has been temporarily used during construction. There is limited opportunity for providing biodiversity value within the built development, such as within car parks or where sight lines need to be maintained around roads. The landscape design aims to provide what biodiversity value can be in these areas, within the constraints of their use (such as car park areas).
5.25	We are concerned that potential loss of habitat for birds has not been adequately assessed by the Applicant particularly on the associated development sites (for example the two village bypass and link road as discussed below). We consider there should be sufficient bird surveys in accordance with best practice guidelines[473] to establish the current assemblage using the main development site and each associated development site to inform the assessment of potential losses and measures to retain and enhance the bird assemblage to ensure there is demonstrable net gain. Natural England also expressed concerns over the adequacy of breeding bird surveys[474].	Impacts to bird assemblages are not part of the Biodiversity Unit calculations. We have committed to but will be discussing with the RSPB how the development proposals can be optimised for birds .

Para No.	Paragraph text	SZC response
5.26	We welcome any additional measures not required for mitigation and/or compensation that would be implemented to benefit specific species.	The landscape design targets benefits to a wide range of species, maximising the value of habitats above that which is required for mitigation.
5.27	As stated above, we do not agree the Application can achieve net gain due to direct adverse impacts on Sizewell Marshes SSSI. Despite this, we agree the Application should be meeting the requirements of the net gain system and should be providing landscape scale net gain proportionate to the scale of the project in line with planning policy. As such, the Application should be demonstrating a high metric score that does not rely on protected species mitigation and/or compensation habitat to get over the 10% uplift requirement.	Please see response to paragraph 5.2 and 5.6.
5.28	We are concerned that protected sites and species mitigation and compensation measures have been double counted in the metric score without first demonstrating the adequacy of those mitigation and compensation measures and then providing net benefits for biodiversity over and above requirements for avoidance, mitigation and/or compensation measures.	The ES discuss the mitigation measures for each individual receptor. See response to paragraph 5.6.

Para No.	Paragraph text	SZC response
5.29	Paragraph 2.9.1 of the Biodiversity Net Gain Report[475] notes mitigation areas are included *Landscape design has been carried out to maximise the benefits to a range of species, maximise biodiversity value and provide ecosystem service benefits. The design is layered in this way, for example, the reptile mitigation areas also provide benefits to a range of other species, for example bats and invertebrates. BNG as presented in the biodiversity metric guidance is a holistic landscape scale assessment of the overall long-term status of the site and the habitats within. As such, it is appropriate that where mitigation for species which results in a change of habitat (such as within the Studio Fields Complex) is assessed within the biodiversity metric.*	No response required.
5.30	We consider 'no net loss' activities such as mitigation and compensation should not be relied upon to achieve the 10% metric target. We consider there should be no double counting if a mitigation or compensation area has benefit to other species unless specific measures are implemented for those other species.	Please see response to paragraph 5.6.

Para No.	Paragraph text	SZC response
5.31	Section 5.1[476] notes the marsh harrier compensation area and reptile habitat areas are included in the off-site biodiversity calculations. The marsh harrier compensation area is incorrectly described as mitigation however it provides compensatory foraging habitat for marsh harrier. The reptile habitat areas provide mitigation habitat for reptiles. One of these, Great Mount Walk, is within the marsh harrier compensation area. Therefore the Applicant is triple counting this area as reptile mitigation, marsh harrier compensation and BNG. As stated above we consider there should be no double counting (or triple counting) if a mitigation or compensation area has benefit to other species unless specific measures are implemented for those other species.	Please see response to paragraph 5.6.

5.32 – 5.33	CIEEM (2018) guidelines[477] describe the key principles of ecological impact assessment at section 1.19 as *Avoidance Seek options that avoid harm to ecological features (for example, by locating on an alternative site).* *Mitigation Negative effects should be avoided or minimised through mitigation measures, either through the design of the project or subsequent measures that can be guaranteed – for example, through a condition or planning obligation.* *Compensation Where there are significant residual negative ecological effects despite the mitigation proposed, these should be offset by appropriate compensatory measures.* *Enhancement Seek to provide net benefits for biodiversity over and above requirements for avoidance, mitigation or compensation.* The Applicant should correctly apply the mitigation hierarchy: 1. Avoidance: demonstrate measures to avoid impacts on protected species and habitats 2. Mitigation: demonstrate reptile mitigation measures are adequate and those within Great Mount Walk are additional to those for marsh harrier compensation 3. Compensation: demonstrate the marsh harrier compensation measures are adequate and additional to those required for reptile mitigation	The ecological impact assessment of each of the receptors is discussed in the relevant chapter of the ES. Please see response to paragraph 5.6.

Para No.	Paragraph text	SZC response
	4. Net gain: provide additional enhancements to benefit other species (or ecological connectivity) over and above avoidance, mitigation and compensation to provide net gain	

5.34-5.35	Paragraph 4.2 of the Marsh Harrier Mitigation Area Feasibility Report[478] describes the design objectives for creation of lowland heath at Great Mount Walk (within the marsh harrier compensation area) • Sow short sward acid grassland mix. • Spread heather brashings of local (Suffolk) provenance in suitable locations to encourage heather establishment as well as plant and invertebrate species indicative of Suffolk Sandlings heath. • Create short sward acid grassland in Great Mount Walks. • Provide log and brash piles to encourage populations of small mammals in the short term as vegetation develops. • Allow development of small areas (less than 0.5ha) of bare ground to encourage development of a diverse assemblage of arable weeds and invertebrate species. • Creation of lowland heath is a long-term process and should begin as early as is practicable to enable the establishment of vegetation and development of a good habitat structure of benefit to nesting birds and small mammals. • Management of scrub and heath will be required to maximise the populations of breeding farmland bird species that are present.	Please see response to paragraph 5.6.

Para No.	Paragraph text	SZC response
	These measures are required to provide compensatory foraging habitat for marsh harrier and cannot be counted in the metric score.	
5.36	The Reptile Mitigation Strategy Figure 14C2A.17[479] shows hay piles, log/brush piles and hibernacula within Great Mount Walk but it is not clear which of these are provided as reptile mitigation over and above requirements for the marsh harrier foraging area. Reptile mitigation also cannot be counted in the metric score.	Please see response to paragraph 5.6.

Para No.	Paragraph text	SZC response
5.37-5.38	The Biodiversity Net Gain Report[480] provides no indication of specific measures for other species over and above protected species mitigation and compensation measures. We consider 'no net loss' activities such as mitigation and compensation should not be relied upon to achieve the 10% metric target. We consider there should be no double counting (or triple counting) if a mitigation or compensation area has benefit to other species unless specific measures are implemented for those other species. We of course welcome any additional measures not specifically required for mitigation and/or compensation that would be implemented to benefit specific species without impeding the main purposes of the marsh harrier compensation area and the reptile mitigation areas, but their use within the metric target. Appendix B of the Biodiversity Net Gain Report [REP1-004] shows the offsite areas with some of the reptile mitigation areas annotated. We request that a map with all the mitigation and compensation areas clearly annotated is provided.	Please see response to paragraph 5.6. The mitigation areas for individual receptors are presented in the draft licences.

Para No.	Paragraph text	SZC response
5.39-5.41	We consider it important to note the metric is not suitable for tracking ecological delivery over time - it is designed to be a one-time snapshot of future commitments at the point of planning application and does not work as a tracking tool (e.g. the score will rise over time even if condition targets are missed). The Outline Landscape and Ecology Management Plan (oLEMP)[481] Table 7.1 notes monitoring proposals refer to biodiversity net gain which suggests the Applicant may intend to use the metric to track ecological delivery over time *monitoring with regards to achieving the desired communities and quality as demonstrated in the biodiversity net gain report (ES Volume 2 Chapter 14 Appendix 14E).* We request clarification that the Applicant does not intend to use the metric as a tracking tool.	Please see response to paragraph 5.8. The metric will not be used as a tracking tool, however monitoring will be carried out against the targets set within the metric.

5.42-5.49	We are concerned the Applicant does not appear to have identified a legal mechanism for securing a 10% metric score in their mitigation strategy. The oLEMP482 notes at paragraph 1.1.3 the Landscape and Ecological Management Plan will be secured by requirement *The oLEMP provides the framework for the Landscape and Ecological Management Plan (LEMP) which will provide further details of the management measures and implementation of the habitat created, along with ongoing monitoring arrangements. This is secured by a requirement within Schedule 2 of the Draft DCO.* and at paragraph 4.1.7 notes *The Biodiversity Net Gain report …. demonstrates that net gain would be achieved if the habitats described within this oLEMP are delivered as proposed.* and at Table 7.1 notes monitoring proposals refer to biodiversity net gain *monitoring with regards to achieving the desired communities and quality as demonstrated in the biodiversity net gain report (ES Volume 2 Chapter 14 Appendix 14E).* Requirement 14 of the draft DCO483 notes the landscape scheme for the permanent development site to be approved by East Suffolk Council must contain	Please see response to paragraph 5.9. Mitigation measures for protected species for each site are detailed within the **Mitigation Route Map** (Doc Ref. 8.12(C)), the **Code of Construction Practice** (Doc Ref. 8.11 (C)) and the relevant draft protected species licence, non-licensable method statement or mitigation strategy. A full list of these documents was provided within response to Bio.1.17 [REP2-100].

	(vii) a landscape and ecology management plan which will be prepared in general accordance with the measures set out in the Outline Landscape and Ecology Management Plan. We are however concerned that Schedule 2 of the Draft DCO[484] does not include a specific requirement for securing a 10% metric score in accordance with the draft Environment Bill [Schedule 14, 9(3) and 10(1) as currently drafted] and planning policy. EN-1 (Overarching NPS for Energy) notes at paragraph 5.3.11 the [PINs] should use requirements and/or planning obligations to ensure enhancement of biodiversity *The [PINs] should use requirements and/or planning obligations to mitigate the harmful aspects of the development and, where possible, to ensure the conservation and enhancement of the site's biodiversity or geological interest.* CIEEM (2018) guidelines[485] at paragraph 6.13 notes enhancements should be designed to deliver biodiversity objectives specified in relevant policy documents and evidence should be provided to support the likelihood of delivering the predicted benefit *Enhancement measures should be designed to deliver biodiversity objectives that are specified in relevant policy documents, and evidence should be provided to support the*	

	likelihood of delivering the predicted benefit. They should be incorporated into scheme design and assessed within the EcIA. To ensure that enhancements are enduring, their delivery and management should normally be guaranteed through a legal obligation, such as, in England and Wales, a planning obligation under section 106 of the Town and Country Planning Act 1990116 , or its equivalent provision elsewhere. Paragraph 7.12 notes *All parties should understand the actions they need to take during the implementation stages of a project. This will mean identifying and designing in detail the measures necessary to avoid, mitigate and compensate negative effects, and any measures necessary to achieve enhancements. Details of these measures will be set out in the EcIA and may be presented in an Environmental Management Plan (EMP) or similar document.* We request the Applicant provides full details of all the measures necessary for protected species mitigation and compensation and full details of additional measures to achieve enhancements for example to benefit other species. We also request evidence is provided to support the likelihood of delivering the predicted benefits. The enhancement measures must be legally secured and we consider Schedule 2 of the Draft DCO*486* should include a	

Para No.	Paragraph text	SZC response
	specific requirement for enhancement measures to secure a 10% metric score in accordance with the draft Environment Bill (Schedule 14, 9(3) and 10(1) as currently drafted) and planning policy.	
5.50	Our main concerns relate to the methodology and approach to the metric calculations and include:	A bullet by bullet response to each query is provided below.
5.50 bullet point 1	the baseline used is directly at odds with the biodiversity gain system to be introduced by the Environment Bill	Please see response to paragraph 5.6.
5.50 bullet point 2	the time for habitats to reach target condition (temporal risk) does not take account of the construction phase	Please see response to paragraph 5.6.
5.50 bullet point 3	the % net change in the metric score is calculated versus the on-site baseline but it should be calculated versus the total on-site plus off-site baseline)	Please see response to paragraph 5.6.
5.50 bullet point 4	the biodiversity value of existing habitats has not been adequately considered and taken account of	Please see response to paragraph 5.6.

Para No.	Paragraph text	SZC response
5.50 bullet point 5	lack of evidence to support the likelihood of delivering the predicted on-site habitat conditions on post-construction soils	The outline **oLEMP** [REP1-010] outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective. This will be evolved throughout scheme delivery and updated with monitoring results.
5.50 bullet point 6	lack of evidence to support the likelihood of delivering the predicted off-site habitat conditions post development	Much of the off-site habitat creation is already underway or has been completed, such as at Aldhurst Farm and the Studio Fields complex. These provide evidence of successful delivery of habitat creation. As stated in the **oLEMP** "*Planned off-site compensation habitat mitigation would be subject to site specific management plans*". As such, further detail regarding mechanisms of habitat creation, management and monitoring will be presented in the management plans of the respective areas.

Para No.	Paragraph text	SZC response
5.50 bullet point 7	the replacement of higher biodiversity[487] habitats with those of lower biodiversity (trading down)	The landscape design targets the increase in the quality of habitats across the site. The key habitat type here is woodland, with lower quality (largely) plantation woodland replaced with woodland with a higher target quality. However, woodland units have declined due to the risk multipliers but in the long term this will provide greater biodiversity value. Declines are seen in the units associated with the sand dunes and vegetated shingle habitats. However, these habitats will be restored and will be neutral or higher in the long term although Biodiversity Units have declined due to the risk multiplier. Such works were successfully carried out during the construction of Sizewell B, so successful restoration is expected to be possible. The classification of these habitat as being of good condition within the baseline demonstrates this restoration.

5.51-5.53	We welcome the inclusion (paragraph 2.3.2 to 2.3.8 of the Biodiversity Net Gain Report488) of baseline data dates for Studio Fields complex (on-site and off-site, 2011), Kenton Hills and St James Covert (off-site, 2007), Aldhurst Farm (on-site and off-site, 2015) and the remainder of the red line boundary (on-site, DCO submission). We query the baseline data date for the Marsh Harrier Habitat Improvement Area (on-site and off-site) and as have mentioned above this should be referred to as compensation. This baseline policy is directly at odds with the biodiversity gain system set out in the Environment Bill[489], which sets the baseline at the point of the planning application for on-site delivery (Schedule 14, 5(2) as currently drafted) and the point set out in the biodiversity site gain register for off-site delivery (Schedule 10, 1(b) as currently drafted). *Schedule 14* *Pre-development biodiversity value* *5 (1) In relation to any development for which planning permission is granted, the pre-development biodiversity value of the onsite habitat is the biodiversity value of the onsite habitat on the relevant date.* *(2) The relevant date is—* *(a) in a case in which planning permission is granted on application, the date of the application, and*	The baseline was taken to be the time point before which any advance habitat interventions had begun (for example, at Aldhurst Farm and the Studio Field Complex). The time points were specific for each of these areas, depending on when habitat interventions began. Advance habitat creation represents good practice by ensuring that the habitats are in place ahead of when they are required with time to mature. The applicant should not be penalised for carrying out habitat improvement works ahead of the application. The calculations demonstrate an increase in biodiversity units post development. The client is not claiming 'biodiversity net gain' to fulfil a statutory requirement but to evidence the efficacy of the mitigation, compensation and enhancement proposed. Sizewell Marshes SSSI and related compensatory habitats have been excluded from the calculation. As discussed above, the Biodiversity Unit calculations are a holistic assessment of the development, so the nomenclature of mitigation or compensation is not relevant to the Biodiversity Unit calculations.

	(b) in any other case, the date on which the planning permission is granted. *(3) But the person submitting the biodiversity gain plan for approval and the planning authority may agree that the relevant date is to be a date earlier than that specified in sub-paragraph (2)(a) or (b) (but not a date which is before the day on which this Schedule comes into force in relation to the development).* *Registered offsite biodiversity gains* *10 (1) "Registered offsite biodiversity gain" means any habitat enhancement, where—* *(a) the enhancement is required to be carried out under a conservation covenant or planning obligation, and* *(b) the enhancement is recorded in the biodiversity gain site register (as to which, see section 93 of the Environment Act 2020).* *93 Biodiversity gain site register* *(1) The Secretary of State may by regulations make provision for and in relation to a register of biodiversity gain sites ("the biodiversity gain site register").* *(2) A biodiversity gain site is land where—*	

Para No.	Paragraph text	SZC response
	(a) a person is required under a conservation covenant or planning obligation to carry out works for the purpose of habitat enhancement, *(b) that or another person is required to maintain the enhancement for at least 30 years after the completion of those works, and* The Applicant's policy to apply different on-site baseline data dates to each on-site delivery area (Studio Fields complex, Aldhurt Farm and the marsh harrier compensation area), all of them prior to the point of planning application (paragraph 2.3.2 to 2.3.8 of the Biodiversity Net Gain Report[490]) is at odds with Schedule 5 of the Bill which has no provision for different baseline data dates across the on-site delivery areas. The Applicant has also applied a baseline data date prior to the point of planning application to the off-site delivery areas. As there is currently no biodiversity site gain register, it would not be possible for the Applicant to claim an earlier baseline for off-site delivery under the biodiversity gain system.	

5.54-5.59	Paragraphs 2.5.4 – 2.5.5 of the Biodiversity Net Gain Report[491] consider the temporal risk calculation which is aimed at accounting for the time lag for a newly created or restored habitat parcel to gain target condition, where it is created prior to, or concurrently, with the development. This multiplier is designed to take account of the time between the impact of a development on a habitat and when it is replaced by habitat of equivalent biodiversity value. The on-site habitat creation starts post construction, and there will be a period of 8 – 12 years from the point of impact during construction where no habitat will be present. Therefore, the biodiversity unit value of these habitats will be zero, rather than the final figure with a time discount multiplier. The Applicant's approach is directly at odds with the biodiversity gain system set out in the Environment Bill[492], which sets the post-development biodiversity value [Schedule 14, 8(1) as currently drafted] as at the time the development is completed. *8 (1) In relation to any development for which planning permission is granted, the post-development biodiversity value of the onsite habitat is the projected value of the onsite habitat as at the time the development is completed.*	The calculation has been undertaken as per the guidance within the metric calculator for all habitats. For example, where habitats have been created in advance and are matured, neither the time to target condition nor the risk has been reduced or eliminated. Similarly, the time to target condition has not been altered where there is to be a delay in their creation. The Biodiversity Metric is designed to assess the baseline and end states of developments. The protected species licensing, legislation and ES ensures that the habitat is suitable to deliver the legal and policy requirements. Therefore, while developers are not penalised for creating habitats ahead of time, under the current biodiversity unit assessment guidelines using the biodiversity metric, nor do they benefit from the reduced risk and time to target condition that these advance works achieve. They are treated the same in the metric even though this does provide greater earlier benefit for biodiversity. The temporal risk multipliers are provided within the metric. They assess the time the habitats are predicted to reach their target state from the point of creation. Throughout consultation, it has been clear that a portion of the habitat creation will occur post-construction. The BNG assessment is a holistic assessment comparing the baseline and post-development state of an area. It is therefore appropriate to compare the baseline and end states of the habitats, using

	Since the on-site habitat creation starts post construction, when the development is completed the value of the on-site habitats will be zero. If any habitats are created before the end of development, the temporal risk calculation should consider the time when no habitat is present during construction and should therefore consider the time from the point of impact (when the current habitat is lost) to the estimated time the post construction habitat will reach target quality as noted in the Natural England Biodiversity Metric 2.0 user guide[493] at paragraph 5.19 *The time period to use in applying the Time to Target Condition multiplier to a metric calculation is the length of time (in years) between the intervention and the point in time the habitat reaches the pre-agreed target quality (i.e. distinctiveness, condition, area). This time will vary between habitat types, between change scenarios (e.g. creation typically takes longer than enhancement) and due to way the habitat is managed. Time to target condition values – based on based on good practice and typical conditions are provided for all habitats used in biodiversity metric 2.0. These values are set out in detail in the Technical Supplement.* This suggests that more offsite habitat creation should be completed to compensate for temporal losses of biodiversity	the multipliers provided within the Biodiversity Metric. The on and off-site areas are all within the EDF estate, so the habitats will be managed positively in the long term to reach and maintain target states.

Para No.	Paragraph text	SZC response
	in line with the Natural England Biodiversity Metric 2.0 user guide[494] which notes at paragraph 5.10 *A typical consequence of applying risk multipliers is to increase the size (e.g. area or length for linear features) of habitat required as compensation such that it exceeds the size of habitat lost or damaged. This is necessary:* *to compensate for temporal losses of biodiversity (e.g. where there is a period of diminished biodiversity between the point in time when a habitat is impacted and it is replaced by habitat of equivalent biodiversity value);*	
5.60	In addition, we recommend all habitat creation commences as soon as possible and we query whether there may be opportunities to transplant more mature trees to reduce time to reach target condition.	Habitat works have commenced ahead of time where possible, such as in the off-site areas at Aldhurst Farm, the Marsh Harrier Habitat Improvement Area and reptile mitigation areas. For the BNG calculations, a 'worst-case scenario' approach was taken and . As such, no benefit for any potential tree transplantations has been included. At present, no transplants of mature trees are proposed other than on the Two Village Bypass where individual specimen tree will be planted to compensate for the loss of veteran trees.

Para No.	Paragraph text	SZC response
5.61-5.62	When considering the off-site habitat creation, the Defra Biodiversity Offsetting Pilots guidance[495] notes at paragraph 69 *The number of years that time discounting should take into consideration is from the point of impact to the estimated time that it will take for the habitat to reach the pre-agreed target quality (i.e. the point at which the agreed number of units is delivered).* Where off-site habitat creation starts after the impact occurs the temporal risk calculation should also consider the time from the point of impact to the estimated time to reach target quality.	See response to paragraphs 5.54-5.59.

Para No.	Paragraph text	SZC response
5.63-5.64	The Biodiversity Net Gain Report[496] at section 8.1.1 image 4 summarises the results of the assessment and reports 18.03% net change in the metric score. Using the figures provided there, the reported 18.03 % net change is the change in the metric score versus the on-site baseline as demonstrated below. *Total baseline biodiversity units = on site 1244.45 + off-site 429.99 = 1,674.44* *Total post intervention biodiversity units = on site 918.51 + off-site 980.27 = 1,898.78* *Total net unit change = 1,898.78-1,674.44= 224.34* *Total net % change vs. on site baseline = 224.34/1244.45*100 = 18.03%* *Total net % change vs. total baseline = 224.34/ 1,674.44*100 = 13.40%* We note it is necessary for the net % change to be calculated versus the total baseline (on-site plus off-site baseline). In addition, any off-site habitat creation that requires planning permission would need to deliver an additional 10% net gain units in order to meet its own requirements under the biodiversity gain system.	See response to paragraph 5.6.

Para No.	Paragraph text	SZC response
5.65	Paragraph 2.5.1 of the Biodiversity Net Gain Report[497] considers the difficulty of creating or restoring a habitat. We request confirmation that the recommended standard difficulty scores are used for each habitat type.	The BNG calculations used the Biodiversity Metric 2.0, so the standard difficulty multipliers were used.

5.66-5.74	We have concerns over the evidence base to support the likelihood of achieving the target on-site habitat conditions post construction, in particular the target 'lowland dry acid grassland' of 'fairly good' condition in most areas of the site. Paragraphs 4.1.26 – 4.1.32 of the Biodiversity Net Gain Report[498] discuss creation of dry Sandlings grassland (DSG) on the construction site post construction. Paragraph 4.1.27 notes uncertainty over the future nature of post-construction soils *Some flexibility is required for the creation and management of this area, since there is some uncertainty over the future nature of the post-construction soils* and *The ultimate vision for the DSG (summer parched grassland) is that these develop over time into an acid grassland / heathland mosaics depending on the realities of soil pH and structure and water availability.* Paragraph 4.1.29 notes reversion of arable to acidic grassland at Aldhurst Farm can indicate future habitat creation outcomes specifically creation of 'fairly good' condition lowland dry acid grassland *It is considered to be achievable to target a 'Lowland dry acid grassland' sward in most areas of the site. Actions to revert arable habitat to an acidic grassland sward is already*	The **oLEMP** outlines the methods of habitat creation and the management required to deliver those habitats to the predicted distinctiveness and quality. This has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective. This will be evolved throughout scheme delivery and updated with monitoring results. The **outline Soil Management Plan** [REP3-018] provides details of how soil restoration is to provide soil profiles suitable for the reinstated land use. Quality habitats targeted at providing optimal habitat for reptiles and invertebrates have already been created for reptiles on former arable land, such as in the Studio Field Complex. The experiences gained from such works will be utilised to target successful habitat creation in areas where construction phase impacts may add additional challenges.

	underway within Aldhurst Farm and the Studio Fields complex. These areas are off-site, but provide an indication of what can be achieved and can be learned from for future habitat creation interventions. A species-rich sward will be targeted, with wildflower cover around 30%. Positive management will target achievement of the condition assessment criteria. As such, a condition of 'fairly good' is predicted. This reflects the challenges of creating areas of such habitat and remains realistic, while targeting a positive outcome. We have concerns around using habitat creation from arable land at Aldhurst Farm and Studio Fields to predict creation of dry Sandlings grassland of fairly good condition on land impacted by construction. Paragraph 5.3.28 of the Biodiversity Net Gain Report[499] discusses habitat creation in the marsh harrier compensation area and predicts creation of fairly good condition lowland dry acid grassland and fairly good condition lowland heathland from former arable land. It seems unlikely that a similar outcome will be achieved on post construction soils. Sizewell B was constructed from 1988 to 1995500. Paragraphs 3.1.46 - 3.4.47 of the Biodiversity Net Gain Report[501] note the impact of Sizewell B construction *3.1.46 A large area of semi-improved neutral grassland is present to the east of the main platform. This area of land*	

	was impacted by construction processes associated with the Sizewell B construction works. As a result, the habitat does not have a typical dune grassland character, due to changes to the hydrology and pedology[502] *caused by the construction works.* *3.1.47 The habitat to the east of the main platform is of semi-improved character, dominated by Cock's-foot and common herbs. Undesirable species and scrub are present across the area. As a result, this habitat is considered to be of moderate condition.* This assessment concludes that land impacted by the construction of Sizewell B suffered changes in hydrology and pedology[503] and some 25 years later is semi-improved neutral grassland of moderate condition. It seems reasonable to conclude that land impacted by the 8-12 year Sizewell C construction period is likely to suffer changes that will affect the proposed habitat creation. It would be more precautionary to use habitat creation outcomes on the Sizewell B construction site as a predictor of future habitat condition on the Sizewell C construction site instead of using outcomes from habitat creation at Aldhurst Farm. The predicted metric score is dependent on successfully creating target habitat conditions. We request evidence is provided to support the likelihood of delivering the predicted habitat conditions on land impacted by Sizewell C	

Para No.	Paragraph text	SZC response
	construction post development. We consider the target condition should take account of the difficulty of habitat creation on post construction soils.	

Para No.	Paragraph text	SZC response
5.75-5.78	We also have concerns over the evidence base to support the likelihood of achieving the target off-site habitat conditions. Paragraphs 5.3.9 - 5.3.10 of the Biodiversity Net Gain Report[504] discuss creation of acid grassland at Aldhurst Farm and notes challenges achieving the targeted level of diversity *it has been challenging to achieving the targeted level of diversity. As such, a precautionary approach is taken and it is assumed that the highest distinctiveness typology will not be achieved. The 'other lowland acid grassland' typology is therefore predicted. It is predicted that good condition can be achieved, through the positive management outlined in the Aldhurst Farm ELMP and due to a lower distinctiveness typology predicted.* Paragraph 5.3.28 discusses habitat creation in the Marsh Harrier Habitat Mitigation Area and predicts creation of fairly good condition lowland dry acid grassland and fairly good condition lowland heathland from former arable land. The predicted BNG is dependent on successfully creating the target habitat conditions. We request evidence is provided to support the likelihood of delivering the predicted off-site habitat conditions post development.	As stated in the **oLEMP** "*Planned off-site compensation habitat mitigation would be subject to site specific management plans*". As such, further detail regarding mechanisms of habitat creation, management and monitoring will be presented in the management plans of the respective areas. The **oLEMP** has been written in liaison with Landscape, Ecology and our Soils specialist. The habitats proposed have been chosen for the site's ability to deliver these habitats from a soil, climate and biodiversity perspective. This will be evolved throughout scheme delivery and updated with monitoring results. The targets were set to balance ambitious targets while remaining realistic regarding likelihood of success. The lessons learned from habitat creation regimes at Aldhurst Farm will be taken forward to inform how best to achieve targets elsewhere. Furthermore, the habitats in the Marsh Harrier Habitat Improvement Area will have time to develop into more semi-natural habitats, ahead of the transition to the long-term end-state of the area. This is expected to reduce the difficulty of habitat creation, as the shift will not be so directly from agricultural land.

Para No.	Paragraph text	SZC response
5.79-5.80	Table 13 of the Biodiversity Net Gain Report[505] notes dry Sandlings grassland of 'fairly good' condition provides 278.66 biodiversity units out of a total of 758.76 units for the on-site areas. The new metric due to be released in Summer 2021 will not include the 'fairly good' category and the condition will consequently need to be changed to moderate which will reduce the assessment for dry Sandlings grassland to 222.93 units. Table 22 of the Biodiversity Net Gain Report506 notes heathland and scrub, woodland forest and grassland of 'fairly good' condition provide 123.33 biodiversity units out of a total of 980.72 units for the off-site areas. The new metric due to be released in Summer 2021 will not include the 'fairly good' category and the condition will consequently need to be changed to moderate which will reduce the assessments for those habitats to 98.66 units.	See response to paragraph 5.6.

5.81-5.87	The metric uses distinctiveness as a collective measure of biodiversity and includes parameters such as species richness, diversity, rarity and the degree to which a habitat supports species rarely found in other habitats. Table 19 of the Biodiversity Net Gain Report[507] shows huge reductions in total biodiversity unit values of high distinctiveness habitat: sparsely vegetated coastal habitats (-94%) and woodland (-40%). The Defra Biodiversity Offsetting Pilots guidance [508] states at paragraph 22 that habitats of high distinctiveness would be expected to be offset with 'like for like' *22. One of the guiding principles for developing our approach to offsetting is that it should result in an improvement in the extent or condition of the ecological network. To do this the focus of habitat restoration or creation through offsetting should be on priority habitats. Where development is taking place on habitats in the low distinctiveness band, the offset actions should result in expansion or restoration of habitats in the medium or, preferably, high distinctiveness band. At no time should an offset result in "trading down", for instance in the replacement of habitat of high distinctiveness with creation or restoration of a habitat of medium distinctiveness. Habitats that are of high distinctiveness would generally be expected to be offset with "like for like" i.e. the compensation should involve the same habitat as was lost.*	See response to paragraphs 5.6 and 5.50 bullet point 7.

	It would be expected that habitats of high distinctiveness (such as sparsely vegetated coastal habitats and some woodland types) would not see an overall reduction in habitat unit value. In the calculations, the significant increase in grassland habitats is compensating for a loss in these habitats. The Natural England Biodiversity Metric 2.0 user guide[509] at rule 3 (section 2.23) notes trading down must be avoided *'Trading down' must be avoided. Losses of habitat are to be compensated for on a 'like for like' or 'like for better' basis. Ideally, new or restored habitats should aim to achieve a higher distinctiveness or condition than habitats lost.* And at rule 5 (section 2.23) notes it may be necessary to enhance or create a larger area of habitat than lost to fully compensate for impacts on biodiversity *It is not the area of habitat created that determines whether ecological equivalence or better has been achieved but the net change in biodiversity units. Risks associated with enhancing or creating habitats mean that it may be necessary to enhance or create a larger area of habitat than lost to fully compensate for impacts on biodiversity.* BNG Good Practice Principles for Development510 notes at section 11.4.1	

Para No.	Paragraph text	SZC response
	Good practice is achieving net gains of the same or higher biodiversity value as those affected and equivalent or better levels of ecological functionality. More habitat creation is therefore required to fully compensate for impacts on biodiversity. If sparsely vegetated coastal habitats cannot be created on-site, then off-site enhancements would be expected. In addition to the reduction in overall biodiversity unit value of woodland, semi-natural broadleaved woodland is largely being offset by mixed woodland. It would be expected that habitats of high distinctiveness (such as semi-natural broadleaved woodland) are replaced like for like as expected in paragraph 22 of the Defra Biodiversity Offsetting Pilots guidance[511]. *Habitats that are of high distinctiveness would generally be expected to be offset with "like for like" i.e. the compensation should involve the same habitat as was lost.*	
5.88	Paragraph 2.2.7 of the Biodiversity Net Gain Report[512] notes hedgerows were grouped together for assessment and it is not clear if each hedgerow was surveyed for the condition assessment. We are therefore concerned hedgerows may have been undervalued and we request clarification of the evidence base for hedgerow condition assessment.	Hedgerows of similar type were grouped together for the purposes of assessment (i.e. rather than entering hundreds of data points for hedgerow segments these were added together). Detailed survey information spanning many years was used to inform the condition assessments.

Para No.	Paragraph text	SZC response
5.89	Although a hedgerow is a linear feature, it does occupy an area and we query whether there may be double counting of hedgerow and habitat areas. We request confirmation that the area of hedgerows has been removed from the area of adjacent habitat parcels.	As required by the metric, hedgerows were treated as linear features. The hedgerows are not included again in the habitat areas. Hedgerows are not double counted.
5.90	The on-site hedgerow baseline biodiversity units reported in section 4.1.5 of the Biodiversity Net Gain Report[513] is different to the value in Table 14.	There is a typo in Table 14. The total hedgerow units cell should read 117.96 (as in section 4.1.5).

5.91-5.94	All habitat improvements funded through Sizewell B commitments should be excluded from the Sizewell C metric score calculation and we welcome the exclusion of the reversion to grassland at Retsom's Field (Sizewell B commitment) from the updated assessment (paragraph 2.10.6 of the Biodiversity Net Gain Report[514]). We also welcome the exclusion of the Sizewell Estate Woodland Management Plan that defines the management of the existing woodlands within the site and the wider EDF Energy estate from the assessment. But Studio Fields Complex, included within the EDF Energy Estate Pre-Construction Integrated Land Management Plan, remains (Table 3.1 of the Biodiversity Net Gain Report[515]). Paragraph 3.4.1 of the oLEMP[516] helpfully explains *Management of these areas would be continued as defined by those existing plans and therefore management proposals for these areas are not considered further within this oLEMP.* As mentioned above the oLEMP[517] paragraph 4.1.7 notes *The Biodiversity Net Gain report …. demonstrates that net gain would be achieved if the habitats described within this oLEMP are delivered as proposed.* We therefore request clarification that the measures at Studio Fields Complex included in the metric calculation are additional to those in the existing management plan.	The Studio Field Complex habitat interventions were started ahead of time to ensure mature optimal habitat ready to receive translocated animals and provide the best opportunity for success. These habitat works are being carried out in relation to the proposed Sizewell C development, so it is appropriate to include these areas in the Biodiversity Unit calculations.

Para No.	Paragraph text	SZC response
5.95	The baseline data date is not provided, and we assume it to be at the time of DCO submission i.e. 2020. We request confirmation of the baseline data date for the two village bypass.	No advance habitat creation works have been carried out at this site, the baseline date is taken to be the last phase 1 habitat surveys undertaken (2019).
5.96-5.97	Paragraph 2.11.1 of Biodiversity Net Gain Report Two Village Bypass[518] notes *Arcadis have used third party data as part of the assessments of the post development and off-site habitats and assumptions on the condition of the baseline habitats are inferred from existing data.* *No specific surveys or assessments were undertaken.* We request evidence to support the baseline condition assessments. There should be sufficient surveys to ensure a demonstrable 10% increase in the metric score.	The calculations used third party data in addition to existing baseline data previously collected by site survey. Detailed habitat survey data was collected for the Two Village Bypass (2019) site that was used to inform the Biodiversity Unit assessments of this area. The BNG report contains the rationale behind the habitat categorisation and the condition assessments for the baseline and post-development states. Further evidence is provided in the Phase 1 habitat surveys [APP-425, APP-426 and APP-427].

Para No.	Paragraph text	SZC response
5.98-5.99	Paragraph 3.1.7 of Biodiversity Net Gain Report Two Village Bypass[519] considers the condition of semi-natural broad-leaved woodland to be lost and notes *The woodlands are all relatively young and comprised mainly native species such as Beech (Fagus sylvatica), Hazel (Corylus avellana) and Field Maple (Acer campestre). Locally a well-developed ground-layer with species such as Dog's Mercury (Mercurialis perennis) and Bluebell (Hyacinthoides non-scripta). The age structure is not diverse enough to classify the woods as good condition, but the precautionary method was used and fairly good condition was selected.* Field maple, dog's mercury and bluebell are recognised as ancient woodland indicator plants in the east of England[520]. Their presence on site does suggest the semi-natural broadleaved woodland is of value and a precautionary approach would be to select good condition for habitat to be lost.	It is agreed that the woodland does have value, hence its assessment as being of the 'Lowland mixed deciduous woodland' typology. The value of the locally well-developed ground-layer is also stated, however, this forms just part of the condition assessment. The lack of age and structural diversity, along with regeneration mean condition assessment criteria 3 and 5 fail. The condition is therefore between good and moderate, so a fairly good condition was considered to be appropriate, following a precautionary approach and the guidance for condition assessment as per the biodiversity metric guidance.

Para No.	Paragraph text	SZC response
5.100	The predicted metric score is dependent on achieving the target habitat conditions. Paragraph 3.2.23 onwards of Biodiversity Net Gain Report Two Village Bypass[521] note proposed broadleaved woodland, neutral grassland, lowland acid grassland, infiltration basins and ponds will achieve good condition. We request evidence is provided to support the likelihood of delivering the predicted habitat conditions.	Management plans will provide greater detail regarding habitat creation and management practices.

Para No.	Paragraph text	SZC response
5.101-5.102	If is important to note that the time to target condition is 15 years for the grassland habitats and 32+ years for woodland. In addition we have concerns over long-term management to achieve these target conditions. The Two Village Bypass Outline Landscape and Ecology Management Plan[522] notes at paragraph 1.1.6 *The oLEMP and subsequent LEMP would be managed by SZC Co. for a total of five years, or until adoption by the Highways Authority. It is expected that the LEMP would contain long term management objectives for the proposed development.* We are concerned that Schedule 2 of the Draft DCO[523] does not include a specific requirement for long-term management of the habitats required for securing a 10% metric score in accordance with planning policy.	Outline Landscape and Ecology Management Plans (oLEMP) have been written and are being updated for PINS for D5 (Doc Ref. 8.3 A(A) and Doc Ref. 8.3 B(A)). These provide detail regarding habitat creation and management practices. The LEMPs will include the details of the long-term management measures required to achieve the scores defined in the BNG reports and maintain the habitats over the long term.

Para No.	Paragraph text	SZC response
5.103	We also query whether there may be opportunities for net gain habitat enhancements to provide habitat for protected species of bats and birds. The appendices are missing from the report. We will review and comment on the baseline Phase 1 map and operational masterplans when they are submitted to the Examination. We hope the Application will include an innovatively designed green bridge linking Foxburrow Wood County Wildlife Site with the woodland to the west.	The landscape design aims to provide benefits to a wide range of species. For example, the grassland, tree and pond mosaics providing benefits to bat and bird species. The appendices can be shared, if they were missing from the reports. The topic of the green bridge is separate to the topic of BNG.
5.104	The baseline data date is not provided, and we assume it to be at the time of DCO submission i.e. 2020. We request confirmation of the baseline date for the Sizewell Link Road.	No advance habitat creation works have been carried out at this site, so the baseline date is taken to be the latest phase 1 surveys undertaken (2019 and 2020) that was used to inform the Biodiversity Unit assessments of this area. The BNG report contains the rationale behind the habitat categorisation and the condition assessments for the baseline and post-development states. Further evidence is provided in the Phase 1 habitat surveys [APP-461, APP-462, APP-463 and AS-036].

Para No.	Paragraph text	SZC response
5.105-5.106	Paragraph 2.10.1 of Biodiversity Net Gain Report Sizewell Link Road[524] notes *Arcadis have used third party data as part of the assessments of the post development and off-site habitats and assumptions on the condition of the baseline habitats are inferred from existing data.* *No specific surveys or assessments were undertaken.* We request evidence to support the baseline condition assessments. There should be sufficient surveys to ensure a demonstrable 10% increase in the metric score.	The calculations used third party data in addition to existing baseline data previously collected by site survey. Detailed habitat survey data was collected for the Sizewell Link Road (2019 and 2020) site that was used to inform the Biodiversity Unit assessments of this area. The BNG report contains the rationale behind the habitat categorisation and the condition assessments for the baseline and post-development states. Further evidence is provided in the Phase 1 habitat surveys [APP-461, APP-462, APP-463 and AS-036]. The inclusion of reference to 'off-site' elements is a typo. There are no off-site elements of the Sizewell link road site.
5.107	Table 8 of Biodiversity Net Gain Report Sizewell Link Road[525] describes minor changes were made to the site boundary since the previous Biodiversity Net Gain report. Many of the post development habitat descriptions use the phrase 'appear to be'. We request clarification of the post development habitats.	Where the phrase 'appears to be' is used this refers to areas where the control of the land will be in the hands of the relevant landowner. As such while the land can be returned to the baseline state, the landowner could change the land use after the land is returned to their control.

Para No.	Paragraph text	SZC response
5.108-5.109	The predicted metric score is dependent on achieving the target habitat conditions. Paragraph 3.2.22 onwards of Biodiversity Net Gain Report Sizewell Link Road[526] note proposed broadleaved woodland, neutral grassland, infiltration basins and ponds will achieve good condition. We request evidence is provided to support the likelihood of delivering the predicted habitat conditions. The time to target condition is 15 years for the grassland habitats and 32+ years for woodland and we also have concerns over long-term management to achieve the target conditions. We are concerned that Schedule 2 of the Draft DCO[527] does not include a specific requirement for long-term management of the habitats and securing a 10% net gain score in accordance with planning policy.	Outline Landscape and Ecology Management Plans (oLEMP) have been written and are being updated for PINS for D5 (Doc Ref. 8.3 A(A) and Doc Ref. 8.3 B(A)). These provide detail regarding habitat creation and management practices. Management plans The LEMPs will include the details regarding of the long-term management measures required to achieve the scores defined in the BNG reports and maintain the habitats over the long term.
5.110	The appendices are missing from the report. We will review and comment on the baseline Phase 1 map and operational masterplans when they are submitted to the Examination.	These reports have been re-issued at deadline 5 to include the missing appendices.

Para No.	Paragraph text	SZC response
5.111	In conclusion, based on our above concerns and the information available at present, we do not agree the Application can achieve net gain due to direct adverse impact on Sizewell Marshes SSSI from loss of a significant proportion of the SSSI, nor the amount claimed by the Applicant.	Key responses above in responses to paragraphs 5.6 and 5.2.
5.112	Despite this, we agree the Application should be meeting the requirements of the net gain system and should be providing landscape scale net gain proportionate to the scale of the project in line with planning policy. As such, the Application should be demonstrating a high metric score that does not rely on protected species mitigation and/or compensation habitat to get over the 10% uplift requirement.	Key response above in response to paragraph 5.6

Para No.	Paragraph text	SZC response
5.113	Our key concerns relating to methodology and approach to the metric calculations include: • use of measures that are for protected sites and species mitigation and compensation • the baseline policy is directly at odds with the biodiversity gain system to be introduced by the Environment Bill • the time for habitats to reach target condition does not take account of the construction phase • the replacement of higher biodiversity habitats with those of lower biodiversity • lack of evidence to support the likelihood of delivering the predicted habitat conditions • the biodiversity value of existing habitats has not been adequately considered and taken account of • heavy use of 'fairly good' category • the % net change in the metric score is calculated versus the on-site baseline but it should be calculated versus the total on-site plus off-site baseline	Key response above in response to paragraph 5.6

Para No.	Paragraph text	SZC response
5.114	We consider the key finding from the Applicant's BNG proposals to be at best only just over the 10% boundary by a narrow margin, and that if any one of several marginal decisions were reversed it would fall below it. We therefore conclude the Applicant will fail to meet the claimed BNG.	The BNG assessment was a robust, holistic assessment of the change in habitats present within the sites undertaken using the latest metric and guidance available at the time. The assessments draw upon large available datasets, in the case of the main development site spanning many years. The assessment was undertaken to demonstrate the efficacy of the mitigation, compensation and enhancement and is not a planning or statutory requirement. More detailed responses to individual concerns provided above.

APPENDIX P

MARINE ECOLOGY PAPER - RESPONSE TO RSPB AND SWT

CONTENTS

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1 MARINE ECOLOGY – SITES AND SPECIES OF CONCERN

i. Indirect impacts on birds from fish mortality arising from the cooling water systems

1.1.1 The RSPB/SWT have raised concerns relating to the entrapment of marine organisms in the water abstracted by the cooling water system and the subsequent discharge of dead and moribund biota from the fish recovery and return (FRR) systems and the potential effects on the prey species of predatory birds and changes in water quality. The concerns relate to the following areas, each concern is summarised below and a response from the Applicant is provided:

- Thresholds for assessing the effects of impingement and entrainment.
- Use of Equivalent Adult Values (EAV).
- Impingement and fish nursery grounds.
- Impingement of eels.
- Assessment of sand gobies.
- Entrainment and climate change.
- Total mortality from impingement and entrainment.
- Discharge of dead and moribund biota.
- Mitigation.

Thresholds for assessing the effects of impingement and entrainment

1.1.2 The RSPB/SWT Written Representation outlines potential issues in assessing the effects of impingement / entrainment on fish populations at the scale of the Spawning Stock Biomass (SSB) because this may not reflect effects at more local scales, which could be relevant to foraging seabirds. The Written Representation acknowledges the further work that has been undertaken to model the potential fish depletion due to impingement at a range of scales, including that of the Greater Sizewell Bay (as initially reported in BEEMS report TR406 in **Vol. 3 Ch. 2 ES Addendum Marine Ecology and Fisheries Appendix 2.17.A** [AS-238]). However, RSPB / SWT disagree with the conclusion that the predicted low levels of depletion mean that effects on SPA seabird populations are highly unlikely

on the basis that these predicted depletion levels are lower than the interannual variability in the abundance of the relevant fish species in the Greater Sizewell Bay. This is because low levels of fish availability (even within the bounds of natural variability) are known to affect the breeding success of tern populations.

1.1.3 In response to these points, the Applicant notes that the assessment of impingement effects considers the effect of impingement on fish populations relative to the appropriate population comparator, for example SSB. This approach is the most appropriate means of determining impacts on fish populations relative to the relevant scale of the population. This is because this approach accounts for the full life-history of the species in questions. In addition to the effects on fish populations, a local scale assessment has been completed to determine the potential for depletion of fish as a prey resource which could lead to indirect effects to bird populations. The local effects assessment was provided in BEEMS Scientific Position Paper SPP103.v3 [AS-238].

1.1.4 Following consultation with the Environment Agency and Natural England, SPP103 (v4) was provided to statutory stakeholders along with the calculation spreadsheets. An updated version of SPP103 (v5) will be submitted at Deadline 6 addressing further Deadline 2 submissions from the RSPB/SWT and Natural England.

1.1.5 The local depletion assessment is designed to augment the Environment Impact Assessment (EIA) toolbox and is independent but complementary to the approach to determine population level effects. The local assessment determines the predicted depletion of different fish prey species due to Sizewell C operating alone and in conjunction with Sizewell B at three spatial scales; within the Greater Sizewell Bay (GSB) (i.e. the extent of and the tidal excursion around the intakes), the ICES statistical rectangle containing Sizewell (33F1), and ICES Division 4c which contains ICES rectangle 33F1. These assessment areas are smaller than the stock areas for most assessed species. The purpose of this local assessment is not to assess the effects of SZC on the long-term sustainability of each stock, but to determine if there could be any local effects that are sufficiently large to affect the conservation objectives of HRA protected species (e.g. via the prey of marine birds). The local depletion assessment provides a framework for contextualising the scale of losses of, in this case, prey availability within the assumptions of the model.

1.1.6 Amongst the marine bird species which are relevant to the Shadow HRA, the modelling of prey depletion at the scale of the Greater Sizewell Bay and tidal excursion is most relevant to the tern species and particularly to little tern, which is the species most dependent on inshore foraging areas. The

most important prey groups for the terns within the waters around Sizewell are likely to be pelagic fish such as herring, sprat and anchovy (see **section 6** of the **Shadow HRA Report** [APP-145]). Applying a range of precautionary assumptions, including no LVSE mitigation, the assessment predicts reductions of pelagic species of less than 3% within the Greater Sizewell Bay (GSB) and tidal excursion with both stations operating. It should be noted that this represents an average value across the GSB and for the area of tidal excursion and the effects would be tidally dynamic and concentrated around the intakes.

1.1.7 Local depletion in prey resources must be considered in the context of natural variability in resource availability. To contextualise the degree of spatial and temporal variability in pelagic fish biomass, a series of acoustic surveys were completed in winter and summer 2015 and 2016 off Minsmere to Thorpeness extending from the coast up to 4 nautical miles offshore. The surveys aimed to map and quantify the small pelagic fish community in the area as a potential food resource for the designated seabird populations. These surveys showed that a high degree of spatial and temporal variability occurred both between seasons (with considerably higher winter biomass) and between years. Whilst it was not an overall aim of the survey, there was no evidence of localised depletion in the vicinity of the Sizewell B intakes nor in the Sizewell sector in general (BEEMS Technical Reports TR359 and TR381; reported in SPP103 (v4)). Version 5 of SPP103 will be submitted at Deadline 6 and provides maps of the biomass of pelagic species.

1.1.8 Importantly, the predicted local depletion (at the scale of the Greater Sizewell Bay) due to impingement is orders of magnitude below natural variability in abundance to which predator-prey relationships are adapted to as estimated from the data on impingement numbers recorded at Sizewell B between 2009 and 2017 for different fish species / groups. For example, between year variability in sprat and herring abundance is estimated to average 172% and 133%, respectively over this period (with maximum values being 454% and 153%, respectively), so that the scale of the predicted local depletion from impingement (less than 3%) is trivial by comparison. Given these differences, it is considered that the predicted levels of local depletion would not have effects on the SPA tern populations. This conclusion is further strengthened by considering that the predictions from this modelling relate to the combined effects of impingement from the operation of Sizewell B together with Sizewell C (and so, essentially, incorporates part of the existing baseline situation) and that modelling at the larger scales of the ICES Statistical Rectangle 33F1 and Statistical Area 4c predicts depletion levels that are orders of magnitude lower than those predicted for the Greater Sizewell Bay and tidal excursion.

1.1.9 In terms of the long-term nature of impingement, the impacts of the station are not predicted to have significant population level effects, in the case of herring and sprat annual unmitigated losses represent 0.01% and 0.03% of annual SSB, respectively (**Table 2** of **Appendix 7L** [REP2-110]). Such a level of mortality would have no significant long-term effects on the population of these important prey species. The population size would increase or decrease at the same rate irrespective of the station. Within year depletion at the local scale of the bay would be as described above.

Use of equivalent adult values

1.1.10 The RSPB raise concerns that the application of equivalent adult values (EAV) to determine the losses of the station in terms of adult fish may not account for potential reductions in prey availability for predatory birds that consume juvenile stages. This concern is acknowledged by the Applicant and is part of the basis for providing two independent but complementary assessment approaches.

1.1.11 Firstly, assessments determine the effects of entrapment (entrainment and impingement) of the station at the fish population level. This requires EAV measures to be calculated for all life-history stages and compares losses against the relevant population units (e.g. SSB). Secondly, a local depletion assessment has been provided to determine changes in prey availability at the scale of the Greater Sizewell Bay and tidal excursion. The second approach, as described above, considers reductions in numbers without an EAV step and is consistent with the RSPB recommendation that unadjusted numbers should be applied when considering impacts on predatory birds that prey on juvenile life-history stages. An updated version of the local effects assessment SPP103 (v5) will be submitted at Deadline 6 and will include further information regarding local depletion of fish in the entrainment size spectrum.

1.1.12 The RSPB/SWT have lent their support to the Environment Agency's concerns that the EAV method does not capture the potential for future spawning opportunities in long-lived fish species and suggest the need to consider Spawner Production Foregone (SPF) figures.

1.1.13 During Issue Specific Hearing ISH7 on the 16 July 2021, the Applicant offered to provide the ExA with a technical note describing the application of EAVs and relevant stock areas. The technical note will provide a comprehensive overview of why Cefas, on behalf of the Applicant, considers the EAV method to be appropriate and precautionary. A brief summary of the EAV approach is provided below.

1.1.14 Before considering the SPF extension, it is important to consider what the EAV method is trying to achieve. Most fish have a dramatically different reproductive strategy to mammals and birds. Fish congregate at spawning sites and produce 10s of thousands to millions of eggs (**Table 6** of [APP-324]). The eggs and subsequently larval stages are transported by oceanographic currents over ranges of 10s to 100s of kilometres or more. The larvae metamorphose into juvenile stages and depending on the species juvenile stages mature over a number of years to become adults and contribute to further generations. For population stability to occur 1 for 1 replacement is required. One adult fish dies, a new fish joins the spawning population to replace it. Therefore, the thousands to millions of eggs produced by a single female have incredibly high mortality rates and very low probabilities of becoming an adult. That is not to say the eggs and larval stages are unimportant, as they provide food resources for a large number of species. As requested by the RSPB/SWT, further information on the potential local depletion of fish life stages susceptible to entrainment will be provided in SPP103 (v5) at Deadline 6. However, to determine the impact of the station on the population of fish (as opposed to local scale depletion) you must convert the lost fish at each stage of the life cycle to an equivalent adult.

1.1.15 EAV is used to convert an annual rate of loss to impingement of predominantly juvenile fish into an annual rate of loss of fish that are maturing and joining the spawning population. The Cefas EAV method involves forward projection of annul impingement mortalities, accounting for natural mortality, to give an equivalent annual rate of loss of mature fish. It is a straightforward adjustment to reflect the likelihood of impinged fish reaching maturity and contributing to the spawning population.

1.1.16 The size of a spawning population changes each year. It changes because new fish are maturing and becoming spawners and because fish that were already spawners are dying, mostly owing to predators, fishing or disease. To estimate the size of the spawning population you therefore need to understand the rate at which spawning fish are being added and the rate at which spawning fish are being taken away. The rate at which fish are added is determined by the numbers reaching maturity each year and this mostly depends on the numbers of fish in the year class. The rate at which fish are lost depends on the rate of fishing or predation each year.

1.1.17 For fishing there has been longstanding study to understand these annual rates and their effects on the population. This understanding means that we have a good idea of the annual rates of mortality that a population can and cannot sustain. For marine fishes it is well established from studies of fishing mortality that populations can sustain losses of 10-20% or more each year over and above natural mortality.

1.1.18 Estimates of annual impingement using EAV rates as a proportion of spawning population size can be used to assess if the annual rate of impingement mortality poses a risk to the population. If estimated EAV rates are low in relation to rates that are known to be sustainable (e.g. less than 1% or so) then there is a very low risk that impingement has an adverse effect on a population. For these very low values of EAV, an estimate of the actual effect on adult population size, such as would be obtained using stock assessment, is not necessary to conclude that there are very low risks posed by impingement. Thus, as an annual rate, EAV can be considered as another source of annual mortality affecting the fish population, to compare or add to other annual rates like fishing and natural mortality.

1.1.19 The EAV method is not as data demanding as more complex methods of population assessment. This is an advantage of the EAV method as it allows it to be applied to many species to screen for risks, as done by the Applicant when assessing the effects of impingement for the key species at Sizewell.

1.1.20 The conservative thresholds that have been discussed for the Cefas EAV (e.g. 1%) relate annual mortality owing to the projected effects of impingement to the size of the population (usually spawning stock biomass) from which these losses are expected to occur. These are not thresholds for changes in spawning population size attributed to impingement. They are thresholds linked to annual rates of mortality which are deemed to be sustainable. The thresholds are justified on the basis that they relate to losses of spawning fish that are an order of magnitude (or more) lower than those observed to be sustained by fished populations.

1.1.21 The SPF is an extension to the EAV approach, which the Environment Agency suggest accounts for repeat spawning. By adopting SPF by design the approach necessarily estimates a multiannual rate of impingement losses (repeat spawning) and not an annual one. Such an approach gives an inflated estimate of annual loss and annual loss as a percentage of spawning population size because it would involve projecting and summing the future numbers of mature fish over several years (a multi-annual rate of loss) rather than estimating it for a single year.

1.1.22 Critically, rates that compile losses of spawning fish over several years and report these as a percentage of spawning population size cannot be related to the thresholds for an annual rate of loss, because the rates would be multiannual. Accounting for repeat spawning would, in effect, generate a crude estimate of accumulated numbers of missing fish over many years.

1.1.23 In such a case where the EAV method showed the potential for effects, the most appropriate method for determining long-term impacts would be to apply a population model. Such approaches are applied by the International Council for Exploration of the Seas (ICES) for stock modelling for commercial exploited species. However, these sophisticated, data demanding approaches are not available for all species assessed at Sizewell and are not proportional to the predicted level of population impacts, which are well below precautionary thresholds for sustainability.

1.1.24 The applicant maintains that the EAV method is the most applicable and appropriate method for determining the impacts of the proposed development on fish populations.

Impingement and fish nursery grounds

1.1.25 The RSPB/SWT Written Representation points out that the fish species (or groups) with highest levels of predicted impingement are those known to be ecologically important (e.g. sprat, herring, whiting, seabass, sand goby and anchovy), including some which are important prey for the SPA seabird populations. It is noted that some of these fish species and groups have nursery grounds within the Greater Sizewell Bay, with Dover sole having both spawning and nursery in this area. RSPB / SWT suggest that impingement affecting these nursery grounds could affect local prey availability for seabirds, particularly little tern (due to their restricted foraging range).

1.1.26 The Applicant refers to the response provided above on the predicted local depletion with respect to food-web effects on designated features of SPAs (and Ramsar sites) (see paragraphs 1.1.2 – 1.1.9). Designated SPA bird features relevant to Sizewell include those with restricted foraging ranges from breeding sites. The species with the smallest foraging ranges of relevance to the designated sites at Sizewell is the little tern. Breeding SPA little tern from colonies at Minsmere, Dingle Marshes (both within the Minsmere-Walberswick SPA) and Slaughden (within the Alde-Ore Estuary SPA) would forage to a large extent within the GSB and tidal extent. However, based upon the expected breeding season foraging ranges of the birds from these colonies, foraging would primarily be within the Sizewell-Dunwich Bank and therefore more likely be subject to the immediate effects of Sizewell B (e.g. see the predicted little tern foraging ranges shown in **Plate 8.7** in the **Shadow HRA Report** [APP-145]). The Sizewell C intakes are located 3km offshore. BEEMS Scientific Position Paper SPP103 (v4), shows that the large interannual variability in resource availability dwarfs the predicted levels of local depletion (as detailed above).

1.1.27 Many of the species with juvenile life stages observed at Sizewell have spawning and nursery grounds distributed over wide geographic areas as described in TR406 (v7) [AS-238] and illustrated in **Figures 22.11** to **22.14** of [APP-333]. Larval recruitment of fish into and out of the bay will be largely influenced by oceanographic and meteorological processes. The offshore location of the cooling water intakes in deeper water is in part to reduce the entrapment of juvenile and larval fish stages. A number of studies point to subsurface peaks in abundance of larval stages. For example, Maes *et al.* (Ref. 1.1) showed that juvenile herring and sprat were 2 to 3 times more abundant in the top 4m of surface waters than at the bottom layers in the Zeeschedlde Estuary during both day and night. Furthermore, in the tidally dominated environment exchange rates relative to abstraction and recruitment of larvae from the wider area would dampen localised depletion. An updated version of the local effects assessment SPP103 (v5) will be submitted at Deadline 6 and will include further information regarding local depletion of fish in the entrainment size spectrum.

Impingement of eels

1.1.28 The RSPB/SWT raise concerns about the level of impingement of eels, which would exceed 1% of the River District Basin biomass of silver eels if FRR mitigation was ineffective. The concern for losses of eels pertains to the role the species plays in the diet of bittern of the Minsmere-Walberswick SPA noting that impacts of local stocks should be assessed in the Shadow HRA.

1.1.29 Entrapment of European eels at Sizewell occurs through two pathways; yellow eels that have left the freshwater environment are recorded in impingement monitoring at Sizewell B, glass eels have been identified in very low numbers and may be susceptible to entrainment.

1.1.30 The assessment of impingement losses of European eels with no mitigation is predicted to result in losses of 1.03% of the RDB biomass (**Table 2** of **Appendix 7L** [REP2-110]). However, this is highly precautionary in that no silver eels have been impingement at Sizewell B and an EAV of 1 (adult fish) has been applied to the yellow eels captured. This position was echoed by the MMO in their Deadline 2 submission (para. 3.2.7 [REP2-140]), emphasis added:

> *"Notwithstanding these uncertainties, the entrapment estimates indicate that even in the absence of LVSE and FRR mitigation measures, only 4 species exceed the 1% threshold: bass, for which density adjustment substantially reduces assessment of impact; sand goby, for which mortality rate >1% Spawning Stock Biomass (SSB) is not a*

concern at population level; thin-lipped mullet, for which value is an artefact of the low level of landings and absence of SSB; and eel, for which the applied Equivalent Adult Value (EAV) of 1 is unrealistically high, and is a species most likely to benefit from the FRR. On this basis, the MMO consider there is a good level of confidence that actual impacts to all fish species will not be significant. Therefore, the MMO support the conclusions of the ES."

1.1.31 With FRR mitigation measures in place the predicted losses fall to 0.21% (**Table 5** of **Appendix 7L** [REP2-110]). FRR mitigation is predicted to be highly effective for robust species such as eels. The Applicant has applied an FRR mortality of 20%, it is noteworthy that the Environment Agency in their uncertainty analyses for the Hinkley Point Inquiry applied an FRR mortality range of 11 to 20% (CD8.6 TB008 – FRR Mortality Rates). Therefore, the Applicant's predictions are considered precautionary.

1.1.32 Whilst there are minor impacts of impingement, it is the glass eel stages that are of relevance to bittern. Impacts from the station with the potential to reduce the numbers of glass eel recruitment to the SPA through entrainment or barriers to migration of glass eels seeking freshwater signals. Only three glass eels have been recorded in the sampling off Sizewell. SPP104 [AS-238] provided a worst case assessment of the impact of entrainment of the proposed station on glass eels. A sensitivity analysis was undertaken to estimate the scale of losses relative to the RDB biomass. Notwithstanding the uncertainty in the estimates from such a low number of eels sampled the effects were predicted to be between 0.007 and 0.024% of the RDB biomass [AS-238]. **Section 22.8.367** of [APP-317] considers the potential for commissioning discharges of hydrazine effects on glass eel recruitment to the Minsmere-Walberswick SPA and concludes no significant effects.

Assessment of entrainment of sand gobies

1.1.33 The RSPB/SWT Written Representation suggests that a threshold of 1% and not 10% of the SSB should be applied in relation to predicted losses as a result of entrainment of sand gobies. This is on the basis that sand goby should be regarded as a species of ecological importance (as they are prey to several of the seabird species which are qualifying features of the Minsmere-Walberswick SPA (and Ramsar site), Alde-Ore Estuary SPA (and Ramsar site) and Outer Thames Estuary SPA).

1.1.34 Sand gobies are a short lived, fast maturing, highly fecund species with high degrees of natural variability. Whilst they are an important prey resource

for higher trophic levels, they are resilient to the degree of depletion predicted by entrapment (impingement + entrainment) from the station.

1.1.35 Sand gobies are ubiquitous in European coastal areas to at least a depth of 20m. The species produces pelagic larvae which are dispersed by tidal currents resulting in a lack of genetic diversity over the southern North Sea (SPP103 v3 [AS-238]). For non-exploited stocks, a 1% threshold is highly precautionary based on fish population dynamics and any observed decline in stock numbers would be due to other factors beyond the influence of entrapment. For such species, a 10% screening threshold has been adopted in this assessment (TR406 v7 [AS-238]). The combined entrapment losses for sand gobies is predicted to be approximately 1.42% of the population estimate, this is considered precautionary as the small impingement fraction is assigned an EAV of 1 and total mortality is assumed for the entrainment fraction. Because of their short lifespan and early age of maturity, sand gobies have a sustainable harvesting rate of far greater than the precautionary 10% of SSB threshold applied (**Section 5.1.1** of TR406.v7 [AS-238]). Therefore, the predicted level of losses are regarded as negligible at the population level. Local depletion of prey availability, notwithstanding the retention of biomass from the FRR systems, is predicted to be minimal in comparison to very high natural variability in the species. As such, no significant reduction in the prey availability of designated HRA species is anticipated (BEEMS Technical Report TR406 v7 [AS-238]).

Entrainment and climate change

1.1.36 The RSPB/SWT Written Representation outlines concerns that climate change will result in more days per year in which entrainment temperatures are above 30°C and, therefore, at levels mortality of fish egg and larval stages increases rapidly (with consequent potential effects on the SPA seabird populations).

1.1.37 The Applicant notes that the effects of higher entrainment mortality due to future climate change on zooplankton species was considered in **Section 22.6, paragraphs 22.6.242 – 22.6.250** and for ichthyoplankton in **Section 22.8, paragraphs 22.8.519 – 22.8.527** of [APP-317]. Entrainment mimic unit (EMU) studies have shown 40% survival of bass eggs and 20% survival of Dover sole eggs and 80% survival of glass eels during entrainment, respectively [APP-324]. All other fish species and life-history stages are precautionarily assumed to incur 100% mortality in entrainment predictions. Whilst higher entrainment mortality rates may be observed under future climate change the starting point for fish entrainment assessments is precautionary. Furthermore, thermal lethality is highly species specific and adaptation to future climate conditions and/or potential species distribution

shifts may influence the ability to tolerate thermal stress (BEEMS Scientific Advisory Report SAR008).

1.1.38 An updated version of the local effects assessment SPP103 (v5) will be submitted at Deadline 6 and will include further information regarding local depletion of fish in the entrainment size spectrum. Current entrainment estimates predict very small reductions in the population sizes of zooplankton within the GSB. Whilst these values may increase slightly due to increases in entrainment temperature and prolonged seasonal chlorination, the assessment of effects would remain unchanged. In the tidally dominated environment exchange rates relative to abstraction and recruitment of from the wider area would dampen localised depletion. Therefore, even 100% mortality of long-lived zooplankton taxa in the immediate vicinity of the station would be expected to have a minimal effect on local abundance [APP-324].

Total mortality from impingement and entrainment

1.1.39 The RSPB/SWT Written Representation states that sprat and herring are the fish species predicted to be impingement and entrainment at SZC in the greatest numbers, and this is considered to be of concern because of the likely importance of these species in the diets of the breeding tern populations associated with the Minsmere-Walberswick SPA (and Ramsar site), Alde-Ore Estuary SPA (and Ramsar site) and the Outer Thames Estuary SPA. The Written Representation considers that the levels of predicted mortality on these fish species appears to be “significant” and reiterate the view that assessments at the scale of the SSB may fail to identify impacts at the local scale of the Greater Sizewell Bay. Concerns are also raised in relation to absence of “proven” mitigation and on a (suggested) lack of consideration of the effects of prey depletion on tern foraging efficiency and foraging success.

1.1.40 The Applicant understands the concerns raised by the RSPB/SWT and the fact that there are two scales of assessment relevant to the concerns. The first is whether entrapment of the station would have a significant effect on the populations of fishes impinged and/or entrained by the proposed development. The second relates to local depletion of fish and the indirect effects this depletion may have on piscivorous bird species.

1.1.41 As described in the ‘Use of Equivalent Adult Value (EAV)’ response above, the Applicant has committed to provide the ExA with a technical note describing the application of EAVs and relevant stock areas for assessing population level impacts. A summary and justification of the appropriateness of the EAV approach is provided in the response to ‘Use of Equivalent Adult Value (EAV)’. The International Council for Exploration

of the Sea (ICES) provides stock assessments for a range of species particularly those of commercial value including sprat and herring, the two most frequently impinged species at Sizewell. ICES represent the consensus of experts, working within an international process with the remit to develop science and advice to support the sustainable use of the seas and oceans. ICES is a network of approximately 5000 experts from around 700 institutes and organisations in 20 member countries and beyond, facilitated by a secretariat based in Copenhagen. ICES assesses all the available evidence across the entire life-history of the species of concern. Migratory behaviour, mixing on spawning grounds and patterns of larval dispersal and recruitment processes all factor into determining the most appropriate population or stock unit. ICES stock areas are therefore the most robust, evidence-based units for determining impacts on a population of fishes. Furthermore, by considering the full life-history of fishes it is compatible with the EAV methodology. This position was supported by the MMO in their Deadline 2 submission [REP2-140] at paragraph 2.4.7:

> *"In relation to the scale of assessment, the MMO notes that the Applicant continues to justify the use of the International Council for Exploration of the Sea ("ICES") stock areas as using the best available evidence. The MMO concludes that the use of ICES stock areas for commercial fish species represents the current best scientific evidence available. There is currently no robust information that would support use of more local stock areas in the assessment. The percentage impact on a stock increases in proportion to the decrease in stock area/size used (the stock area/size is the denominator in the impact calculation). Thus, a ten-fold reduction in the stock area/size used results in a 10-fold increase in estimate impact."*

1.1.42 In the absence of mitigation, once the biology of the species is considered, there is no indication the station would cause losses at a level that could affect population sustainability. In the case of sprat and herring, unmitigated losses represent 0.03% and 0.01% of the SSB, respectively (**Table 2 of Appendix 7L** [REP2-110]). The high absolute numbers predicted to be impinged is a reflection of the abundance of these species. In their Deadline 2 submission the MMO stated [REP2-140] at paragraph 3.2.7:

> *"Notwithstanding these uncertainties, the entrapment estimates indicate that even in the absence of LVSE and FRR mitigation measures, only 4 species exceed the 1% threshold: bass, for which density adjustment substantially reduces assessment of impact; sand goby, for which mortality rate >1% Spawning Stock Biomass (SSB) is not a concern at population level; thin-*

lipped mullet, for which value is an artefact of the low level of landings and absence of SSB; and eel, for which the applied Equivalent Adult Value (EAV) of 1 is unrealistically high, and is a species most likely to benefit from the FRR. On this basis, the MMO consider there is a good level of confidence that actual impacts to all fish species will not be significant. Therefore, the MMO support the conclusions of the ES."

1.1.43 To address the uncertainties described by the MMO, a sensitivity analysis will be submitted at Deadline 6 addressing uncertainty in FRR efficiency, confidence intervals in impingement predictions and variation in population sizes. The uncertainty analysis will precautionarily assume no benefit from the LVSE heads.

1.1.44 In relation to the potential impacts on the SPA tern populations, as detailed above (paragraph 1.1.8) and in Section 3 of BEEMS SPP103.v4, the depletion levels at the local scale of the Greater Sizewell Bay as a result of impingement are orders of magnitude lower than the estimated between-year variability in fish abundance, including for key species such as sprat and herring. Given this scale of difference, it is concluded that the depletion from impingement as a result of Sizewell C combined with Sizewell B would not have any adverse food-web effects on the SPA tern populations. The offshore location of the cooling water intakes in deeper water is in part to reduce the entrapment of juvenile and larval fish stages. A number of studies point to subsurface peaks in abundance of larval stages. For example, Maes *et al.* (Ref. 1.1) showed that juvenile herring and sprat were 2 to 3 times more abundant in the top 4m of surface waters than at the bottom layers in the Zeeschedlde Estuary during both day and night. Furthermore, in the tidally dominated environment exchange rates relative to abstraction and recruitment of larvae from the wider area would dampen localised depletion. An updated version of the local effects assessment SPP103 (v5) will be submitted at Deadline 6 and will include further information regarding local depletion of fish in the entrainment size spectrum.

1.1.45 In the context of potential effects of prey depletion on little tern foraging success, the RSPB/SWT Written Representations make reference to the documented effects on the little tern colony at Scroby Sands (Ref. 1.2). However, the Scroby Sands study documents the effects of very large reductions (i.e. several fold) in the young of the year herring as a result of "intensely noisy monopile installation during the winter spawning period" during construction of an offshore wind farm site. As such, it does not provide a suitably analogous situation to the small level of predicted depletion in fish populations in the Greater Sizewell Bay.

Discharge of dead and moribund biota

1.1.46 The RSPB/SWT Written Representation identifies concerns over the discharge of dead and moribund biota from the Fish Return and Recovery (FRR) system and the potential for synergistic effects between the resulting localised changes in water quality and other operational discharges.

1.1.47 The Applicant notes that the inter-relationship effects of the chemical and thermal plume on prey species of SPA seabird populations are considered in **Section 22.8, paragraphs 22.8.843 to 22.8.858** of [APP-317], the conclusions of which indicate that the combined or synergistic effects do not alter the overall outcome of the assessment of individual effects. The impact of organic enrichment and un-ionised ammonia from the FRR systems, is predicted to have a negligible effect on pelagic fish eggs, larvae, juveniles and adults (main prey for seabirds). Prey availability and scavenging is considered below.

1.1.48 BEEMS SPP103 (v4) recognises that the potential beneficial effect of dead and moribund biota on seabird populations is limited to those species that are scavengers. This report indicates that the biomass that is discharged by the FRR is retained within the system resulting in bottom-up effects stimulating secondary production and, in some cases, affording opportunistic feeding opportunities for seabirds (notably gulls). Whilst the majority of FRR discards sink and would therefore not be accessible to surface feeding seabirds, floating discards would represent a potential foraging opportunity to scavenging seabirds (BEEMS Technical Report TR501, Ref. 1.3). Experiments have shown seabirds can take up to 71%, 8%, 12% and 4% of discarded roundfish, flatfish, elasmobranchs and invertebrates, respectively, in the southern North Sea (Ref. 1.4). Local depletion of prey availability, notwithstanding the retention of biomass from the FRR systems, is predicted to be minimal in comparison to natural variability. As such, no significant reductions in the prey availability of designated HRA species are anticipated.

1.1.49 **Section 22.5, paragraph 22.5.26** of [APP-317] states that the FRR wash water would not be chlorinated, therefore, impinged biota would not be subjected to TRO exposure. The impact of un-ionised ammonia (decomposition of biota) from the FRR systems on pelagic fish was considered in **Section 22.8, paragraphs 22.8.833 to 22.8.836** of [APP-317] and is predicted to have a negligible effect on pelagic fish juveniles and adults. The possible effect of the commissioning discharge plume of hydrazine interacting with fish discharged from the FRR is considered in **Section 22.8, paragraph 22.8.241-22.8.242** of [APP-317]. The conclusion was that fish exposed to impingement stress may be less tolerant, to chemical stress. However, the low concentrations and transitory nature of

the plume indicated additional mortality would be minimal. Hydrazine is not indicated to bioaccumulate based on its low bioconcentration factor (BCF) in studies with fish (Ref. 1.5) and its low partition coefficient (-2.07 reported in Ref. 1.6). These properties make food chain bioaccumulation unlikely (Ref. 1.7). As there is low bioaccumulation potential of hydrazine, the indirect effects on HRA designated bird features are predicted to be minimal.

Mitigation

1.1.50 The RSPB/SWT Written Representation states that the design of the cooling water system does not comply with best practice and should include an Acoustic Fish Deterrent (AFD).

1.1.51 A report explaining why an AFD system is not considered feasible for Sizewell C was provided at Deadline 5. Notwithstanding this, the EIA demonstrates that with a Low Velocity Side Entry (LVSE) intake head and Fish Recovery and Return (FRR) system integrated into the cooling water system, but no AFD, Sizewell C will not have significant adverse effects on fish species or populations.

ii. Direct and indirect impacts on birds from the thermal plume

Increase in absolute sea temperature

1.1.52 The RSPB/SWT Written Representation outlines concerns in relation to the effects of sea temperature increases on fish communities and, potentially, on the seabirds (e.g. terns) which prey on these fish.

1.1.53 The Applicant would point out that the effects of future climate change and thermal discharges on long-term community changes in fish receptors, and therefore indirect effects on designated SPA bird populations, have been considered and assessed in **Section 22.8, paragraphs 22.8.711 to 22.8.719** of [APP-317]. The conclusion was that taxa within the GSB exposed to future temperature scenarios would have differential sensitivities to absolute thermal thresholds applied in current standards. Furthermore, once Sizewell B ceases to operate, the combined effects of climate change and thermal discharges from Sizewell C (i.e. the 2055 simulation) would be considerably smaller and further offshore than the contemporary absolute thermal exceedance of Sizewell B alone. The impact of thermal discharges under the future climate scenario (including long-term community changes), is predicted to have a minor adverse effect on cold-water fish taxa. In summary, rates of impingement are related to the abundance of fish in the populations. This is relevant when considering the long-term trends in fish populations, be they increase or decrease in abundance in response to climate variation. Impingement rates are

therefore expected to increase for populations benefitting from climate change and to decrease for those that do not. However, overall rates of impingement as a percentage of population size will be more stable, and it is these effects that predominantly determine the consequences for the population.

Uplift in sea temperature compared to baseline

1.1.54 The RSPB/SWT Written Representation outlines a range of concerns related to the assessment of the effects of the thermal plumes (as defined by the extent of the 2ºC and 3ºC temperature uplifts). These include considerations of the extent to which the plumes overlap with the predicted foraging ranges of some SPA populations (notably little tern associated with the Minsmere-Walberswick SPA (and Ramsar site)), as well as the basis for assuming that those parts of the Outer Thames Estuary SPA encompassed by the plumes hold a relatively small proportion of the SPA red-throated diver population (so that the effect is smaller than as indicated by the proportion of the SPA encompassed by the plumes). The Written Representation also suggests that the synergistic effects of the thermal plumes with chemical discharges may cause displacement of SPA bird species, either directly or via effects on prey distribution.

1.1.55 In terms of the overlap of the thermal plumes with the predicted foraging ranges of little tern from the Minsmere-Walberswick SPA (and Ramsar site), the figures presented in the Written Representations concern the overlap for the 98th percentile of the predicted plume areas for the 2ºC and 3ºC uplifts. These figures represent small to moderate absolute increases in overlap for both the Minsmere and Dingle colonies for the 3ºC uplift, when compared to the baseline situation of Sizewell B operating alone. As detailed in **paragraph 8.3.17** of the **Shadow HRA Report** [APP-145], the 3ºC uplift is considered to be a sufficiently precautionary threshold. The extent of overlap of the plumes (as predicted for the operation of SZC together with SZB) with the colony foraging ranges is substantially less when the average instantaneous plume area is considered (rather than 98th percentile), as is also the case for the absolute increases when compared with the baseline situation (see **paragraphs 8.8.285 – 8.8.292** of the **Shadow HRA Report** [APP-145]).

1.1.56 In relation to the assessment of the potential for effects on the Outer Thames Estuary SPA non-breeding red-throated diver population, the available survey data clearly show that the section of the SPA which overlaps with the marine elements of the SZC development (i.e. the north-west block – see **Figure 4.1** in the **Shadow HRA Report** [APP-145]). Thus, Natural England commissioned digital aerial surveys across the entire SPA in 2018 show considerably lower densities in the north-west block of the

SPA than in the larger southern block (Ref. 1.8). The consequences of this is that the north-west block is estimated to hold 21% of the SPA red-throated diver population, based on the peak count from the two surveys that were undertaken, and just 7% of this population during the first count. Earlier digital aerial surveys across the entire SPA, undertaken in 2013, also show this same pattern of lower densities in the northwest block than in the large southern block (Ref. 1.9). It is also the case that the distribution maps from both the 2013 and 2018 surveys show that relative to the overall densities within the northwest block of the SPA, densities in the coastal waters adjacent to the main development site tend to be low to moderate.

1.1.57 Therefore, based on the available data sources that allow comparisons of red-throated diver density across the entire SPA, it is clear that these are low within the vicinity of the main development site relative to much of the rest of the SPA. RSPB/SWT suggest that the 2012/13 and 2013/14 data from the project-specific coastal vantage point survey data suggest high numbers of red-throated diver using the Greater Sizewell Bay (based upon the data reported in s reported in the Annexes to **ES Chapter 14 Appendix 14A7** [APP-238] and also presented in **Tables 6.18 and 6.19** of the **Shadow HRA Report** [APP-145]). However, such data suffer from a wide range of potential biases (including double-counting of birds from different vantage points) and are of value only in providing a measure of relative abundance within the surveyed area. They are completely unsuitable for providing estimates of absolute abundance and it is certainly not the case that using the peak counts from these surveys can be assumed to underestimate abundance, as is stated in the Written Representations. Therefore, they cannot be used to estimate the importance of the Greater Sizewell Bay relative to other parts of the SPA.

1.1.58 Notwithstanding the issues over whether the waters in the vicinity of the main development site are of low importance for red-throated diver (relative to other parts of the SPA), it is the case that the predicted thermal plumes from the operation of SZC with SZB would encompass a small part of the SPA only. The RSPB/SWT Written Representations state this to be 4.3% of the SPA for the 2°C uplift but this is for the 100th percentile, which is accepted to be an overly precautionary estimate (**paragraph 8.3.15** of the **Shadow HRA Report** [APP-145]). More realistic estimates of the overlap resulting from the operation of SZC with SZB are presented in **Table 8.28** of the **Shadow HRA Report** [APP-145], which gives values of 1.6% and 0.3% for the maximum and average instantaneous plume areas, respectively, for the 2°C uplift and of 0.6% and 0.1% for the 3°C uplift.

1.1.59 Furthermore, it is important to consider the highly precautionary basis for the assessment of the potential effects of the thermal plumes on the SPA seabird populations, which is to assume that foraging opportunities are

substantially reduced within the areas encompassed by the plumes. However, as noted above, coastal vantage point surveys demonstrate that terns do forage within the area encompassed by the thermal plumes from Sizewell B (see **Plates 6.6 – 6.8** and **6.10** and **Plate 8.7** in the **Shadow HRA Report** [APP-145] and **Figures 6A.2 – 6A.10** in the **Shadow HRA Report Addendum** [AS-174] to [AS-177]). Also, the effects of localised displacement of fish species from temperature changes associated with the thermal plume is considered in **Section 22.8, paragraphs 22.8.708 to 22.8.710** of [APP-317]. This details how thermal plumes can potentially elicit behavioural avoidance and attraction by certain fish species. However, there is little evidence to indicate that 2ºC or 3ºC temperature increase above ambient would cause avoidance. Analysis of the length-frequency distribution of smelt impinged annually and each month showed no evidence that large fish are more likely to avoid the area of the intakes with increasing excess seabed temperatures up to 2.5°C (BEEMS Scientific Position Paper SPP101). Acoustic surveys of sprat at Sizewell have shown no apparent avoidance of the Sizewell B with a 2ºC uplift in temperature (or due to the chlorinated discharge plume) (Ref. 1.10). Thermal plume areas at temperatures likely to have foraging consequences on designated seabirds and marine mammals are small relative to the foraging range (Ref. 1.11). Localised displacement of fish receptors due to the thermal discharges from the cooling water outfalls, is predicted to have a minor adverse to minor beneficial effect on the local distribution of fish. Effects are not deemed to be significant. Thus, these conclusions in relation to fish provide strong indication of the precautionary basis to the assessment undertaken on the SPA seabird populations.

1.1.60 In terms of synergistic effects of the thermal plumes with chemical discharges, the effects of elevated temperatures associated with the thermal plume and Total Residual Oxidants (TRO) and hydrazine associated with the chemical plume on fish species (indirect effects on designated SPA bird features) are considered in **Section 22.8, paragraphs 22.8.843 to 22.8.853** of [APP-317].

1.1.61 Temperature elevation has been shown to increase toxicity of chlorine TRO in fish. In one case an approximate halving of the lethal concentration of TRO was observed with an increase of temperature between 10°C and 20°C (Ref. 1.12). However, the studies reviewed generally report temperature effects on toxicity in acute studies with durations of hours to a few days and with exposure concentrations in the 100s of micrograms. In the same review, in some cases fish were reported to actively avoid much lower TRO concentrations than would be lethal over several days' continuous exposure (Ref. 1.12). At the immediate point of discharge the maximum temperatures at the surface are between 7.5°C and 8°C above ambient. As a 98th percentile the 5°C above ambient temperature contour

is 30.6ha in a relatively symmetrical position around the outfalls. Within this area, TRO concentration above 50µg/l and 20µg/l occur over sea surface areas of approximately 9ha and 98ha, respectively as a 95th percentile. In small areas of the thermal plume with temperatures of 5°C above background and in which TRO concentrations are >20µg/l increased TRO toxicity may occur. However, the plume conditions sufficient to cause synergistic effects are transient and exposure times of actively mobile organisms or those passively moving with the tides would be short. Therefore, synergistic effects are feasible over limited spatial areas. The inter-relationship of the TRO and thermal plumes is not predicted to increase the significance of effects concluded for the pressures alone. It is unlikely that the inter-relationship between thermal and chlorinated discharges would increase the significance of the effects of localised displacement, beyond the effects predicted for the pressures individually. This conclusion applies to all fish receptors assessed.

1.1.62 The inter-relationship of the hydrazine and thermal plumes is not predicted to increase the significance of effects concluded for the pressures alone. It is unlikely that this inter-relationship would increase the significance of the effects of localised displacement, beyond the effects predicted for the individual pressures. This conclusion applies to all fish receptors assessed.

iii. Direct and indirect impacts on birds from the chemical plumes

1.1.63 The RSPB/SWT Written Representation states that the chemical discharges associated with the cooling water system at SZC have the potential to affect the prey species of SPA seabird populations from the Minsmere-Walberswick SPA, Alde-Ore Estuary SPA and Outer Thames Estuary SPA, and could also have direct displacement or toxic effects on these species.

1.1.64 In relation to the various points raised points raised on the potential indirect and direct effects on birds from the chemical plumes it should, first, be emphasised that these plumes almost invariably have very small overlaps with the predicted foraging ranges of the various SPA seabird populations of relevance (less than a fraction of 1% in most cases – e.g. see **sections 8.3 b) ii, 8.3 c) ii, 8.8 e) ii and 8.10 c) i** in the **Shadow HRA Report** [APP-145]). Therefore, there is little potential for avoidance of, or direct displacement from, the plume areas to have more than negligible effects on these SPA populations.

1.1.65 In terms of the potential for toxic effects, indirect effects on food webs through the potential of chemical bioaccumulation were considered in **Section 22.10** of [APP-317]. Bioaccumulation of hydrazine was tested on freshwater guppies (0.5mg/l test concentration). Results showed a

bioconcentration factor of 288l/kg observed (Ref. 1.13). In Europe, substances with bioconcentration factors ≥2000 are considered bioaccumulative (Ref. 1.14). Hydrazine does not meet the criteria for bioaccumulation (Ref. 1.6; Ref. 1.15) as it has a low bioconcentration factor meaning the bioaccumulation potential is low. No indirect food webs effects from hydrazine bioaccumulation are therefore predicted. Chlorination products are rapidly degraded in the marine environment and bioaccumulation is not an important consideration (Ref. 1.16). Bromoform is the most abundant chlorination by-product and has a low bioconcentration factor. The log bioconcentration factor ranges from 1-4 in most species with the exception of shrimps where values of >8 have been reported in the literature. However, studies have shown that following cessation of chlorination, depuration of bromoform was complete after two days from mussels (Ref. 1.17).

1.1.66 The potential for direct effects of toxicity on SPA seabirds was not identified as a potential effect pathway for Likely Significant Effects (LSE) and was not raised by either RSPB or SWT in the comments they provided on the Stage 1 Habitats Regulations Assessment (HRA) Screening Report in February 2019. Therefore, no assessment of this potential effect pathway is undertaken and presented in the Shadow HRA Report [APP-145].

1.1.67 In relation to some of the specific points raised on this topic in the RSPB/SWT Written Representations, the following responses are provided:

Potential for effects of hydrazine plumes to combine with those of other discharges to cause greater effects on bird prey (i.e. fish) than as assessed for the hydrazine plumes in the sHRA

1.1.68 See response above to synergistic effects of the thermal and chemical plume on fish species (and indirect effects on SPA seabird features).

1.1.69 Increases in water temperature have been shown to increase toxicity of hydrazine to fish; however, effect concentrations are orders of magnitude above the acute PNEC (Ref. 1.18). The acute PNEC is based on data for the most sensitive group of organisms tested (algae) and is derived from continuous exposure for up to 6 days. Available evidence suggests that fish are one of the less sensitive groups to hydrazine exposure.

1.1.70 At Sizewell seasonal chlorination would be applied. When hydrazine is added to chlorinated seawater, the hydrazine is oxidized to non-toxic nitrogen, sodium chloride and water. In experiments described in BEEMS Technical Report TR363 (Ref. 1.19), an initial hydrazine concentration of 69ng/l fell to 8.4ng/l in the presence of chlorinated seawater at the planned

TRO concentrations for SZC. The combination of elevated temperature and chlorine TRO would increase hydrazine degradation.

1.1.71 The elevated temperature and presence of TRO has the potential to enhance the interactions between the stressors. However, as hydrazine exposure occurs for short periods, the dynamic interaction between TRO, hydrazine and temperature causing a reduction in hydrazine concentration but also potentially contributing to synergistic effects would be temporally as well as spatially limited.

1.1.72 Synergistic effects on the toxicity of hydrazine to fish in the receiving waters would only occur in the very near field and have negligible difference beyond the effects already assessed for the pressures individually. The sensitivity of fish to operational hydrazine discharges is assessed in **Section 22.8, paragraph 22.8.788** of [APP-317] onwards, the effects of fish sensitivity to thermal discharges are assessed in **Section 22.8, paragraph 22.8.673** of [APP-317] onwards. The assessment of localised displacement due to the synergistic effects of hydrazine and temperature changes in **Section 22.8, paragraph 22.8.853** of [APP-317] are not anticipated to be greater than for the pressures alone. Localised behavioural responses to thermal discharges would override any behaviours to hydrazine.

Effects of weather/tidal conditions on hydrazine concentrations – are these sufficiently accounted for in the assessment?

1.1.73 The indirect effects on designated HRA bird features of hydrazine during the commissioning phase on migratory fish and juveniles (prey species) is considered in **Section 22.8, paragraphs 22.8.367 to 22.8.373** of [APP-317]. The proposed development, and CDO, is south of the Minsmere sluice and discharges are only transported northward on an ebb tide, when water levels are falling. Modelling results show that at the position of the Minsmere sluice, the chronic and acute PNEC concentrations at the surface and seabed are never exceeded. Furthermore, the northern tip of the 95th percentile surface plume is 1,235 m south of the east-west axis of the Minsmere sluice. Therefore, harmful concentrations of hydrazine would not enter the sluice.

1.1.74 Eels form part of the prey species for designated bittern *Botaurus stellaris* within the Minsmere to Walberswick SPA and Ramsar site. Due to this, the effects of hydrazine on migratory eels was investigated. Eels would be able to migrate both north-south along the coastline and enter/exit the Minsmere sluice travelling into the North Sea without passing through a hydrazine plume at levels above the chronic PNEC. The peak instantaneous concentration at the sluice opening is 0.12ng/l at the surface and 0.11ng/l

at the seabed (Ref. 1.20). The rapid degradation rates of hydrazine and low initial concentrations indicate negligible ecological effects due to the proposed development. It is considered highly unlikely that commissioning discharges of hydrazine would affect eel migration into/out of the sluice given the low concentration and limited potential for exposure (Ref. 1.20). As such, there would be no effects on eels as a marine prey item for bittern *Botaurus stellaris* within the Minsmere to Walberswick SPA and Ramsar site.

1.1.75 The hydrazine commissioning modelling simulation was carried out for a period of 1 month (1st-31st of May 2009), to encompass a full spring neap cycle. This is the same hydrodynamic GETM results that were used to investigate the effect of chlorination of the cooling water system to inhibit biofouling, as reported in BEEMS Technical Report TR303 (Ref. 1.21). The month of May was chosen because this is the month of highest phytoplankton growth which drives the marine ecosystem. Due to the pulse-like discharge, the interpretation of the short-term results (daily) is biased to the moment of the tidal cycle when hydrazine has been released. To evaluate this effect, an additional simulation was carried out with the release pulses starting at 18:00.

Potential for hydrazine to enter the Minsmere-Walberswick SPA/SAC/Ramsar site on ebb tides and effects of this

1.1.76 **Section 22.7, paragraph 22.7.189** of [APP-317] explains that the monthly discharge simulation indicated maximum instantaneous hydrazine concentrations of 0.12ng/l at the location of the Minsmere sluice. Seawater entering the sluice would therefore already be over three times lower than the precautionary chronic PNEC for hydrazine. The half-life in seawater is approximately 30 minutes so there would be further degradation at this rate as the seawater mixes with the brackish/freshwater in the associated watercourses. Therefore, a very low residual level of hydrazine is possible in the brackish watercourses fed by the sluice (<0.12 ng/l).

1.1.77 Degradation in soft water used in laboratory studies has been demonstrated to be much slower (10s of days) than in natural seawater (Ref. 1.6) but equivalent studies of natural river and pond water show half-life values of < a day so the hydrazine residual would remain low. A wider range of toxicity studies are available for freshwater species, and this has resulted in the derivation of a Canadian Federal Water Quality Guideline (FWQG) value for freshwater of 2.6 µg/l. Values below this FWQG are considered to have a low or no likelihood of adverse effects. Such concentrations are above the discharge concentration at the CDO.

1.1.78 Several options are available for treatment of hydrazine and the best approach to achieve the required discharge level during commissioning is currently under investigation. This discharge would be regulated via the WDA permit.

Concerns on effects of hydrazine combining with other discharges so leading to effects on bird prey despite small overlap of plumes with bird foraging ranges:

1.1.79 The synergistic and inter-relationship effects of components of the thermal and chemical plume during the operations phase have been considered and assessed for indirect effects (prey species) on designated SPA seabird features (see response above regarding synergistic effects of the thermal and chemical plume).

iv. Direct and indirect impacts on birds from the sediment plumes

1.1.80 The RSPB/SWT Written Representations suggest that there is potential for direct and indirect effects on SPA seabird populations as a consequence of the sediment plumes that result from dredging activities during the construction period. However, these sediment plumes are predicted to extend over relatively small areas only and be of a few days duration (e.g. see **Table 8.16** in the **Shadow HRA Report** [APP-145]). The Applicant considers that there is adequate assessment of the potential effects in the Shadow HRA Report.

1.1.81 In relation to the points made in the Written Representations on the dredging required for the enhanced BLF, information regarding SSC plumes from dredging required at the enhanced permanent BLF during the operational phase is provided in **Section 22d) iii) b) a)** of [AS-181] with further details provided in Ref. 1.22.

1.1.82 In terms of the information that underpins the assessment on SPA seabird populations, the assessments on prey species (i.e. the pathway to indirect effects) on SPA seabird features are based on programme information at the time of Sizewell C DCO submission. **Volume 2, Chapter 2** of the ES [APP-180] provides a description of the main development site. **Volume 2, Chapter 3** [APP-184] and **Chapter 4** [APP-187] of the ES provide a description of the construction and commissioning, and operational phases of the development, respectively. **Section 22.8, paragraph 22.8.107** of [APP-317] states that for pelagic fish species, localised egg/larvae mortality may occur within the BLF dredge plume. The losses are considered minimal compared to natural mortality and therefore eggs/larvae from pelagic fish species are not considered to be sensitive to increases in suspended sediment. Adult pelagic fish may experience stress but may still

tolerate the temporary SSC increase and remain in the presence of the plume or behaviourally avoid the plume and be locally displaced (**Section 22.8, paragraph 22.8.109** of [APP-317]). Therefore, adult pelagic fish have a low sensitivity to increases in suspended sediment. The impact of increases in suspended sediment is predicted to have a minor adverse effect on pelagic fish eggs/larvae, juveniles and adults. Effects are not significant at the sea area and regional stock/population levels.

1.1.83 In relation to prey availability through avoidance, **Section 22.8, paragraph 22.8.120** of [APP-317] states that the avoidance of fish to sediment plumes, notably pelagic species, would be influenced by factors such as motivation, mobility and condition of the fish. Satellite data for surface suspended particulate matter showed average mean values at Sizewell during April to August of 31mg/l and average monthly maximum values of 80mg/l. Between September to March, mean suspended particulate matter values of 73mg/l were recorded in the surface waters at Sizewell, with average monthly maximum values of 180mg/l. Fish within the Greater Sizewell Bay would be acclimated to a highly variable natural background. Thus, fish may exhibit limited movements away from the areas of highest SSC, remaining in proximity to the plume and utilising the area once the plume dissipates. Given that the limited magnitude and transient nature of the plume, the scope for fish to be displaced entirely from the plume area and not return is very limited. Fish are predicted to have low sensitivity with only localised and temporary displacement of sensitive taxa likely to occur. Therefore, suspended sediment plumes are predicted to have a minor adverse effect on fish displacement. No significant changes in the availability of fish as prey items for designated features and as fisheries resources are predicted.

1.1.84 The indirect effects (prey species) on designated SPA seabird features from the concurrent activities resulting in increases in suspended sediment during the construction phase have been considered in **Section 22.8, paragraphs 22.8.460 to 22.8.467** of [APP-317]. The conclusion was that considering the combined increase in SSC in the context of background conditions, it is unlikely that this inter-relationship would increase the significance of these effects. Furthermore, it is unlikely that this inter-relationship would increase the significance of the effects of localised displacement due to avoidance, beyond the effects predicted for development components alone. The conclusion of minor adverse effects applies to all fish receptor sub-groups. Effects are not significant at the sea or regional stock/population level.

v. Indirect impacts on birds from disturbance of prey species by underwater noise and vibration

Impacts of noise disturbance on fish prey of red-throated divers

1.1.85 In relation to the effects of underwater noise on the prey of SPA seabirds, this issue is only relevant to the Outer Thames Estuary SPA non-breeding red-throated diver population because BLF construction will occur outside the breeding season (so not affecting any of the SPA breeding seabird species).

1.1.86 The largest areas within which effects on fish from underwater noise are predicted to occur represent a small percentage of the total SPA area (considerably less than 1%), as noted in the RSPB/SWT Written Representations. In addition, the effects which extend out to this (largest) area are limited to behavioural effects, which will be temporary and (likely) short-term. As such, there is no basis for considering potential effects on the red-throated diver population from effects of underwater noise on their fish prey (contrary to the suggestion in the Written Representations).

1.1.87 Additionally, as described in detail above (paragraph 1.1.56) the basis on which the Applicant "asserts" that the red-throated diver densities are lower in the north-west block of the Outer Thames Estuary SPA than in the larger southern block are the data and conclusions deriving from two separate programmes of Natural England commissioned digital aerial surveys of the entire SPA area. The Applicant is aware of no other data which enable determination of the within-SPA variation in red-throated diver densities and would question why RSPB/SWT do not appear to accept the findings from these surveys.

vi. Direct disturbance of birds arising from vessel movements and other marine activity

1.1.88 The RSPB/SWT Written Representations highlight concerns in relation to the proposed deliveries to the temporary BLF during the November to March period, which would extend over eight years of the construction period. This is on the basis that the associated vessel movements could cause disturbance and displacement of non-breeding red-throated diver within the Outer Thames Estuary SPA.

1.1.89 The Applicant's position on this issue is as set out in the responses provided at Deadline 3 to Natural England's Written Representations (**paragraphs 11.21.19 – 11.21.23** in [REP3-042]). Thus, the assessment in the **Shadow HRA Addendum** [AS-173] is based on a worst-case scenario involving all vessel movements using an indicative vessel corridor that essentially maximises the potential transit route through the SPA. The consequence,

at the SPA-scale of this highly precautionary assumption is that the BLF deliveries add just 0.1 hours of vessel activity per km^2 per month within the SPA (which is a water body within which existing levels of vessel activity are considerably greater than this).

1.1.90 That wintering red-throated diver are highly sensitive to vessel traffic is widely accepted although, as with the Written Representations from Natural England [REP2-153], the RSPB/SWT Written Representations rely on the work of Mendel et al. (Ref. 1.23) (amongst other studies), with more recent work casting doubt over the details of the findings in terms of the extent of likely (maximum) displacement distances from vessels (Ref. 1.24). It should also be recognised that displacement does not mean that all birds are excluded from the affected area but rather it is the case that densities would be reduced (temporarily) within the vicinity of the transiting vessels. It is also the case that resettlement times of red-throated diver disturbed by vessels are greatest in relation to vessels moving at considerably faster speeds (i.e. >40km/hour) than the self-propelled barges that it is assumed will be used for the BLF deliveries (which are likely to have a loaded maximum speed of 18 – 24km/hour - see **Section 8.8 c) ii.** of the **Shadow HRA Report Addendum** [AS-173]).

1.1.91 The RSPB/SWT Written Representations also suggest that the assessment should apply the standard methods that are used in assessments of offshore wind farms and associated cable routes to determining the effects on the SPA red-throated diver population. It is proposed that this would involve assuming a range of displacement rates (0 – 100%) within a 5km around the BLFs and vessel route, and relate this to a range of potential mortality rates (again 0 – 100%) amongst the (assumed) displaced birds, to assess the range of mortality that may result from the disturbance effects. Such an approach is completely inappropriate in relation to the effects of concern to the Sizewell C Project because there is simply no comparability between these and the marine elements of an offshore wind farm development.

1.1.92 Thus, offshore wind farm sites are large developments (often encompassing areas of >100km^2) within which there may be close to, or in excess of, 100 large wind turbines, and for which there is considerable vessel activity associated with construction, cable laying and maintenance. This bears no relation to the marine elements of the Sizewell C Project, which comprise:

- Two BLFs which extend out from shore by c.100m (the permanent, enhanced, BLF) and c.500m (the temporary BLF).

- Approximately 200 deliveries during the relevant seasonal period (for a period of eight years), equating (under a worst-case scenario) to 2.7 vessel movements per day through the SPA.

1.1.93 It is also the case that the standard approaches described in RSPB/SWT Written Representations for determining effects of displacement on wintering red-throated diver in assessments for offshore wind farms are not applied to standard vessel transits (which, instead, are assumed to occur within shipping lanes, where red-throated diver densities are already reduced – Ref. 1.25). Rather, such approaches are only applied in relation to the wind farm site itself and to cable laying vessels (which, for the purpose of the assessment, are essentially treated as being static objects because of their very slow movement through the water).

1.1.94 The Applicant considers that the scale and extent of displacement of the SPA red-throated divers which is expected to occur as a result of the operation of the BLFs and the associated vessel movements is highly unlikely to lead to any discernible increase in mortality amongst this population. Noting the very much smaller displacement effects that are expected from the Sizewell C Project compared to those which occur at offshore wind farms (as outlined above), it is relevant to consider the findings of studies of non-breeding red-throated diver in the German North Sea. These studies show that (between 2001 – 18) there was no decline in this population, despite the erection of 20 offshore wind farms (although displacement from the offshore wind farm sites has affected red-throated diver distribution in the area) (Ref. 1.26).

1.1.95 Notwithstanding the above points, the Applicant welcomes Natural England's proposal to develop a vessel management plan in relation to the potential red-throated diver issues and, as stated in the responses to the Natural England Written Representations [REP3-042], is prepared to work with Natural England in producing this.

vii. Combined marine impacts

1.1.96 The RSPB/SWT Written Representations suggest there has been insufficient consideration of the combined marine impacts. However, in this regard, the Applicant highlights the assessments of inter-pathway effects undertaken in **Appendix 1A** of the **Shadow HRA Addendum** [AS-174]. RSPB/SWT state that this further assessment does not advance the understanding of these (potential) combined effects sufficiently. However, the stated reasons for this include the view that individual effects have been underestimated (particularly disturbance by vessel traffic) and that there is insufficient detail on known synergistic issues. On these points, the Applicant considers that there are very strong reasons for disagreeing with

the RSPB/SWT position in relation to assessing the effects of disturbance from vessel traffic (as detailed in **paragraphs 13.100.211 – 13.100.218** above), whilst further responses in relation to potential synergistic effects are provided at several points above in this section on marine ornithology.

viii. Marine impacts in-combination with other projects

1.1.97 Due to the very small change in vessel numbers due to the Sizewell C Project compared with baseline levels and the lower densities of red-throated diver in the north-western section than in the larger southern section of the Outer Thames Estuary SPA, combined with localised nature of construction noise effects, there is no realistic potential for a material effect on the red-throated diver population of the SPA.

1.1.98 Notwithstanding the above, the Applicant will produce a vessel management plan that would accommodate the requirement of enabling the winter season BLF deliveries and contribute to reducing potential disturbance to the SPA red-throated diver population.

2 REFERENCES

Ref. 1.1 Maes, J. *et al.* (1999). Diel changes in the vertical distribution of juvenile fish in the Zeeschelde Estuary. Journal of Fish Biology 54, 1329–1333.

Ref. 1.2 Perrow, M., Gilroy, J., Skeate, E. & Tomlinson, M. (2011). Effects of the construction of Scroby Sands offshore wind farm on the prey base of Little tern *Sternula albifrons* at its most important UK colony. Marine Pollution Bulletin, 62, 1661-1670.

Ref. 1.3 BEEMS Technical report TR501. Food web interactions and potential for indirect effects at Sizewell. Cefas, Lowestoft.

Ref. 1.4 Garthe, S., Camphuysen, K., & Furness, R. W. (1996). Amounts of discards by commercial fisheries and their significance as food for seabirds in the North Sea. Marine Ecology Progress Series, 136(1–3), 1–11.

Ref. 1.5 Slonim AR. (1977). Acute toxicity of selected hydrazines to the common guppy. Water Res. 11:889–895.

Ref. 1.6 Environment Canada and Health Canada. Screening Assessment for the Challenge. Hydrazine. Chemical Abstracts Service Registry Number 302-01- 2. January 2011.

Ref. 1.7 U.S. Department of Health and Human Services (1997). Toxicological Profile for Hydrazines. Agency for Toxic Substances and Disease Registry, Atlanta, Georgia.

Ref. 1.8 Irwin, C. et al. (2019) HiDef report to Natural England- Digital video aerial surveys of red-throated diver in the Outer Thames Estuary Special Protection Area 2018. Natural England Commissioned Reports, Number 260.

Ref. 1.9 APEM (2013). Aerial Bird Surveys in the Outer Thames Estuary SPA. APEM scientific report for Natural England.

Ref. 1.10 BEEMS. Acoustic Surveying of Pelagic Fish off Sizewell. BEEM Technical Report TR381. Lowestoft, UK: Cefas, 2019.

Ref. 1.11 BEEMS. Synthesis of Evidence for SZC Water Framework Directive (WFD) and Habitats Regulations Assessment (HRA) Marine Assessments. Technical Report TR483. Lowestoft, UK: Cefas, 2019.

Ref. 1.12 Cooke, S.J. and J.F. Schreer. 2001. Additive Effects of Chlorinated Biocides and Water Temperature on Fish in Thermal Effluents with Emphasis on the Great Lakes. Reviews in Fisheries Science, 2001, 9 (2), pp. 69–113.

Ref. 1.13 Slonim, A.R. and Gisclard, J.B (1976). Hydrazine Degradation in Aquatic Systems. Bulletin of Environmental Contamination and Toxicology, 1976, 16 (3), pp. 301–309.

Ref. 1.14 REACH Regulation (EC) No 1907/2006. ANNEX XIII: Criteria for the identification of persistent, bioaccumulative and toxic substances, and very persistent and very bioaccumulative substances.

Ref. 1.15 Environment Canada. Canadian Environmental Protection Act, 1999 Federal Environmental Quality Guidelines. Hydrazine. 2013Available from: http://www.ec.gc.ca/ese-ees/default.asp?lang=En&n=D66353C2-1.

Ref. 1.16 Environment Agency. Proposed EQS for Water Framework Directive Annex VIII Substances : Chlorine (Free Available). SNIFFER Report: WFD52(lv). Bristol, UK: 2007.

Ref. 1.17 BEEMS Scientific Advisory Report. BEEMS Expert Panel. 2011. Chlorination by-Products in Power Station Cooling Water. Scientific Advisory Report SAR009. Lowestoft, UK:2011.

Ref. 1.18 BEEMS Scientific Advisory Report. BEEMS Expert Panel. 2011. Thermal Standards for Cooling Water from New Build Nuclear Power Stations. Scientific Advisory Report SAR008. Lowestoft, UK; Cefas.

Ref. 1.19 BEEMS. Thermal and Chemical Effects of Antibiofouling and Process Chemicals in Power Station Cooling Water on Biomass, Abundance and Physiology of Natural Phytoplankton Communities. Technical Report TR363. Lowestoft, UK; Cefas.

Ref. 1.20 BEEMS. Sizewell C Hydrazine Commissioning Discharge Plume Modelling. Technical Report TR494. Lowestoft, UK: Cefas, 2019.

Ref. 1.21 BEEMS. Sizewell – Chemical plume modelling: TRO, CBPs, Hydrazine, DO and ammonia. Technical Report TR303. Lowestoft, UK: Cefas, 2019.

Ref. 1.22 BEEMS. Modelling of the Temporary and Permanent Beach Landing Facilities at Sizewell C. Technical Report TR543. Lowestoft, UK: Cefas, 2021.

Ref. 1.23 Mendel et al. (2019) Operational offshore wind farms and associated ship traffic cause profound changes in distribution patterns of Loons (Gavia spp.). Journal of Environmental Management, 231, 429–438.

Ref. 1.24 Dorsch et al. 2020 DIVER: German tracking study of seabirds in areas of planned Offshore Wind Farms at the example of divers. Final report on the joint project DIVER, FKZ 0325747A/B, funded by the Federal Ministry of Economics and Energy (BMWi) on the basis of a decision by the German Bundestag.

Ref. 1.25 Irwin, C. et al. (2019) HiDef report to Natural England-Digital video aerial surveys of red-throated diver in the Outer Thames Estuary Special Protection Area 2018. Natural England Commissioned Reports, Number 260.

Ref. 1.26 Vilela et al. (2021) Use of an INLA latent Gaussian modelling approach to assess bird population changes due to the development of offshore wind farms. Frontiers in Marine Science, 8: 701332. doi: 10.3389/fmars.2021.701332.

APPENDIX Q

POTENTIAL COMBINED IMPACT OF THE MDS AND SLR ON BATS

In Combination Effect Sizewell Link Road and Main Development Site on Bats

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None Provided

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Figure 2: Bat 21 - breeding female Natterer's bat - triangulation points

ANNEXE

ANNEX A. FIGURES 5

1 BACKGROUND TO THIS NOTE

1.1.1 This note provides a supplementary response to those already provided by SZC Co at Deadline 3 [REP3-044] which responded to the detailed points made by the Councils in respect of bats. That response deferred two points which required further consideration, in respect of (i) cumulative effects between the main development site and the Sizewell link road and (ii) in-combination effects arising primarily from noise and light.

1.1.2 This note provides a response to the first of these points. The second point will be addressed at Deadline 6 when new graphics will be available.

1.2 Issue (from the LIR)

1.2.1 "*In addition to the above, the Councils do not consider the cumulative impacts from the Main Development Site (including the Temporary Construction Area) and the Sizewell Link Road have been adequately considered (please also see the ecology section of the Sizewell Link Road chapter). Both developments will require the removal of habitats suitable for foraging and commuting bats and, as the two developments connect, it is highly likely that it will be the same bat population which will experience this impact. Given that the species most likely to suffer from this impact is barbastelle (and to lesser extent maybe Natterer's bat as well), this will compound the existing conclusion of a Moderate Adverse, Significant level impact and may even give rise to a Major Adverse, Significant level impact*"

1.3 SZC Co.'s Response

1.3.1 It is considered that the approach employed in relation to the in-combination effect of the main development site and the Sizewell link road adequately captures and assesses the potential combined impact of these two components of the Sizewell C Project on bats. The conclusion of the assessment is that there is no pathway for the impacts identified in the updated bat impact assessment [AS-208] and **Volume 5**, **Chapter 7** of the **ES** [APP-461] for each of the project components to combine to create a significant project-wide effect, and that this has been adequately assessed in the two ES chapters.

1.3.2 There are two key reasons for the conclusion:

- The residual effects from the main development site and the Sizewell link road are such that they are unlikely to combine to produce project-wide effects. The main residual effect on the main development site is fragmentation in the construction Phase (years 0-12) and is considered moderate adverse (significant). In contrast, fragmentation is not

considered to lead to significant effects in either the construction phase (years 0-3) or operational phase (3+) for the Sizewell link road (due to the nature of the development and embedded mitigation).

- The bat populations associated with the two project components are different (due to geographical locations and habitat types in the vicinity) and support different species assemblages. The survey information from the radio tracking surveys also suggests limited movement of bats between the two areas.

1.3.3 Each of these aspects is discussed in more detail below:

a) Point 1 – Residual Effects

1.3.4 For the Sizewell link road, no significant adverse effects are foreseen on bats, in the construction or operational phase. The main development site assessment identifies a significant adverse effects on bats in the construction phase (years 0 -12) of the Sizewell C Project, through habitat fragmentation.

Table 1: Summary of impact Assessment of potential cumulative impact pathways

Scheme	Construction	Operation
Main Development Site (ES Bat Addendum) [AS-208]	YEARS 0 -12 Moderate adverse (significant)	YEARS 12+ No residual impact
Sizewell Link Road (ES) [APP-461]	YEARS 0 -3 Minor adverse (**not significant**).	YEARS 3+ Minor beneficial (**not significant**)

1.3.5 Given this, there is no clear pathway for project-wide effect to occur or to be under-valued in the ES assessments. The pathway for the fragmentation impact within the main development site relates to the location of the construction area, which will be lit, and is likely to reduce commuting routes for bats to three dark corridor and around the site boundaries. In contrast the Sizewell link road will remain dark other than lighting provided at the A12 and B1122 roundabouts and so there is limited risk of fragmentation. The potential for fragmentation effects arising from the Sizewell link road is also considered low given that there are a number of examples of rare woodland bats 'using' road corridors as flyways. Examples include A27 Emsworth (Bechstein's), B2149 Rowlands Castle (Bechstein's), A120 west of Bishop's Stortford (Barbastelle) and A417 Cheltenham (All four annex II species).

1.3.6 In addition, once the Sizewell link road is operational, the new plantings will provide greater connectivity and this further reduces the potential for a project-wide effect from Year 3 onwards. This will become beneficial (see Table 1), once the plantings are mature.

b) Point 2

1.3.7 The bat populations associated with the main development site and the Sizewell link road area are different. Radio tracking on the main development site [APP-245] indicates that the barbastelle populations on the site are associated with the EDF estate and Minsmere to the north, with minimal usage of the areas to the west through which the Sizewell link road is located (to the north-west of the main development site). The text below is from the main development site bat impact assessment [AS-208]:

1.3.8 *'Radio-tracking surveys have identified an interchange of bats between Minsmere and the EDF Energy estate as well as the use of the EDF Energy estate by bats throughout the bat active season. Tagged barbastelle were recorded using the EDF Energy Estate all year round and moving between the two areas on a number of occasions throughout the 2014 radio-tracking survey. Of the seven female barbastelle trapped in Minsmere, four were confirmed to be active within the EDF Energy Estate, whilst of the seven females trapped within the EDF Energy Estate, at least six were confirmed to be active within Minsmere. All three of the male barbastelle trapped within the EDF Energy Estate were recorded within Minsmere (no adult males were caught within Minsmere). One tagged female was recorded roosting in both locations.'*

1.3.9 This is also true for Natterer's bats, which were associated within the Kenton Hills area and Aldhurst Farm to the west, and not the area where the Sizewell link road will be located to the north-west (accepting that only a low number of bats were tracked). The images in **Annex A** show the location of Natterer's bats tracked across the EDF site.

1.3.10 In recent surveys, the Sizewell link road site has been found to support smaller populations of Natterer's bats and barbastelle than the main development site [APP-242 to APP-246 and APP-462]. These populations are likely to form different meta populations, although there will be some population overlap.

1.3.11 Activity surveys within the Sizewell link road site boundary revealed common and soprano pipistrelle as the mostly frequently recorded species with other species recorded at very low levels [APP-462]. *Myotis* sp. had only low levels of activity identified specifically to Natterer's. Barbastelle were recorded at low levels in 2019 during activity surveys [APP-462]. No

evidence within (and low likelihood) of barbastelle breeding roosts within the site was identified [APP-462].

ANNEX A. FIGURES

N

Theberton

ERTON CP

21 MCP

22 MCP

1 MCP

2 MCP

LEISTON CP

LEISTON

RA

RB

RC

RD

RE

RF

Sizewell Belts

Dunwich Forest

Goose Hill

Power Station

Sizewell

KEY

Bat 1

Bat 2

Bat 21

Bat 22

Sizewell Bat Report 2011

Figure C37
Adult female Natterer's bat - MCP 95% comparison

January 2012
28130_A278.dwg tugwc

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KEY

- RA — Roost A
- RE — Roost E used by bat 21
- T4 — Mist net/harp trap trapping location 4 - bat 21 caught here
- 21.24 — Bat 21 joint bearing triangulation point 24
- 95% kernel analysis
- 95% cluster analysis
- 95% MCP analysis

EDF

Sizewell Bat Report 2011

Figure C22
Bat 21 - breeding female Natterer's bat - triangulation points

January 2012
28130_A263.dwg tugwc

amec

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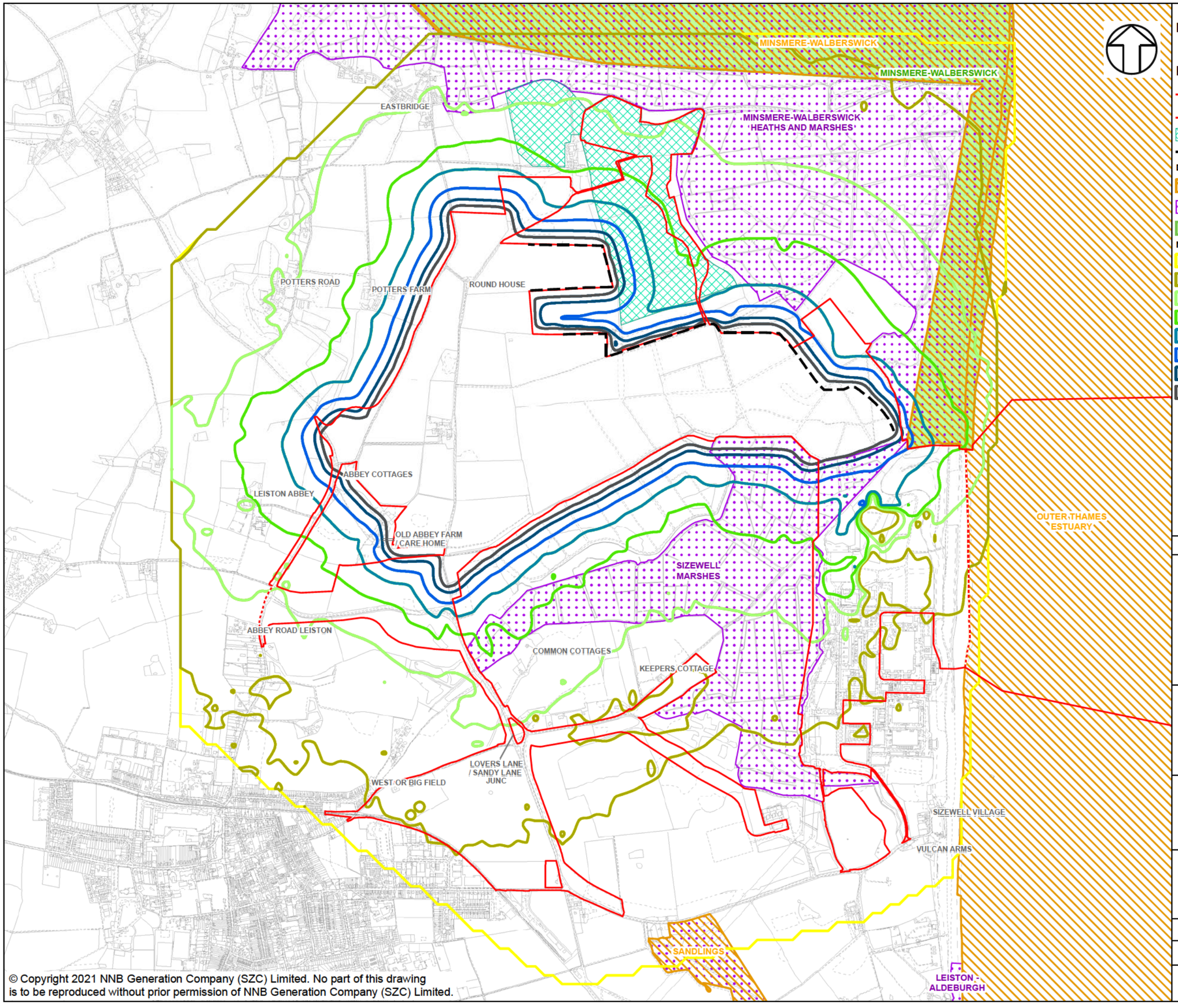
APPENDIX U

HRA FIGURE



NOTES

KEY

- SIZEWELL C MAIN DEVELOPMENT SITE BOUNDARY
- DEMARCATION LINE
- HARRIER HABITAT IMPROVEMENT AREA
- FENCE

DESIGNATIONS

- SPECIAL PROTECTION AREA (SPA)
- SITE OF SPECIAL SCIENTIFIC INTEREST (SSSI)
- RAMSAR SITE

Noise Level L_{Amax}(dB)

- <= 55
- 55 - 60
- 60 - 65
- 64 - 70
- 70 - 74
- 74 - 79
- 79 - 84
- >85

NOT PROTECTIVELY MARKED

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SizewellC
Doing the power of good for Britain
EDF CGN

DOCUMENT:
SIZEWELL C PROJECT
SHADOW HRA REPORT
CHAPTER 8
INFORMATION FOR AA:
BIRDS

DRAWING TITLE:
PREDICTED PEAK NOISE AT 3M ELEVATION FOR PHASE 5 CONSTRUCTION FOR SIZEWELL C

DRAWING NO:
FIGURE 8.6

DATE:	DRAWN:	SCALE :	REVISION:
JULY 2021	J.T.	1:16,000 @A3	1.0

SCALE BAR
0 120 240 360 480 600 Metres

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